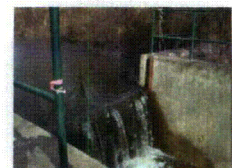
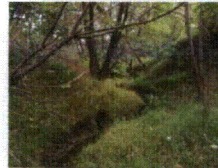


Bell Bend Nuclear Power Plant Wetland Mitigation Design Report Riverlands Site

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Rev 0, November 2010



Bell Bend Nuclear Power Plant

Wetland Mitigation Design Report – Riverlands Site

Rev 0, November 2010

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1 Introduction

The Riverlands Mitigation Site will provide 1.24 acres of compensatory wetland mitigation for unavoidable wetland impacts associated with the proposed Bell Bed Nuclear Power Plant. This mitigation site is located adjacent to the North Branch Canal, immediately south of the existing access drive to the Susquehanna Steam Electric Station intake structure (Figure 1). This project will also provide conveyance for base flow and storm flow that currently flows through the canal outfall channel which will be filled for the construction of the proposed intake structure (Figure 2). The historical alignment of the North Branch Canal has been interrupted and base flow is diverted over a weir into a heavily incised man made channel and into the North Branch of Susquehanna River. The Riverlands Mitigation Site consists of hydraulically re-connecting the North Branch Canal, restoring the original tow path, and repairing and maintaining the existing control structure that supports the Susquehanna Riverlands Wetlands Nature Area.

The Susquehanna Riverlands Wetlands Nature Area is a nature preserve that was designed and constructed in the early 1980's. The North Branch Canal flows south from the mitigation site through the Wetlands Nature Area, bisecting the constructed wetlands. Therefore, the redirection of the canal baseflow back into the canal will affect the hydrology of the constructed wetlands to a certain extent. In addition to the construction for the Riverlands Mitigation Site, the existing control structure that maintains hydraulic grade at the southernmost point of the Susquehanna Riverlands Wetlands Nature Area must be repaired and adjusted to maintain the desired water surface elevation in the wetlands.

The purpose of this narrative is to describe background data, present design methodology, and summarize design calculations involved with the restoration design of the Riverlands Mitigation Site. The specific design objectives include maintaining a stable water surface elevation in the canal, directing canal flows to the Susquehanna Riverlands Wetlands Nature Area, enhancing/restoring the historical value of the canal and tow path while enhancing 1.24 acres of existing wetlands by removing invasive species and planting native vegetation.

These objectives will be achieved by restoring the original alignment of the canal and installing a stop log structure that will be used to maintain water surface elevations upstream into the Riverlands Recreational Area adjacent to Lake Took-A-While. The project will also re-connect the original canal and tow path and create a walking trail on the original tow path and a pedestrian crossing at the stop log structure. The eroded gulleys in the canal outfall channel will be filled with amended topsoil and planted with native species of wetland plants. An overflow pipe will be installed to maintain the hydrology behind the proposed intake structure fill material.

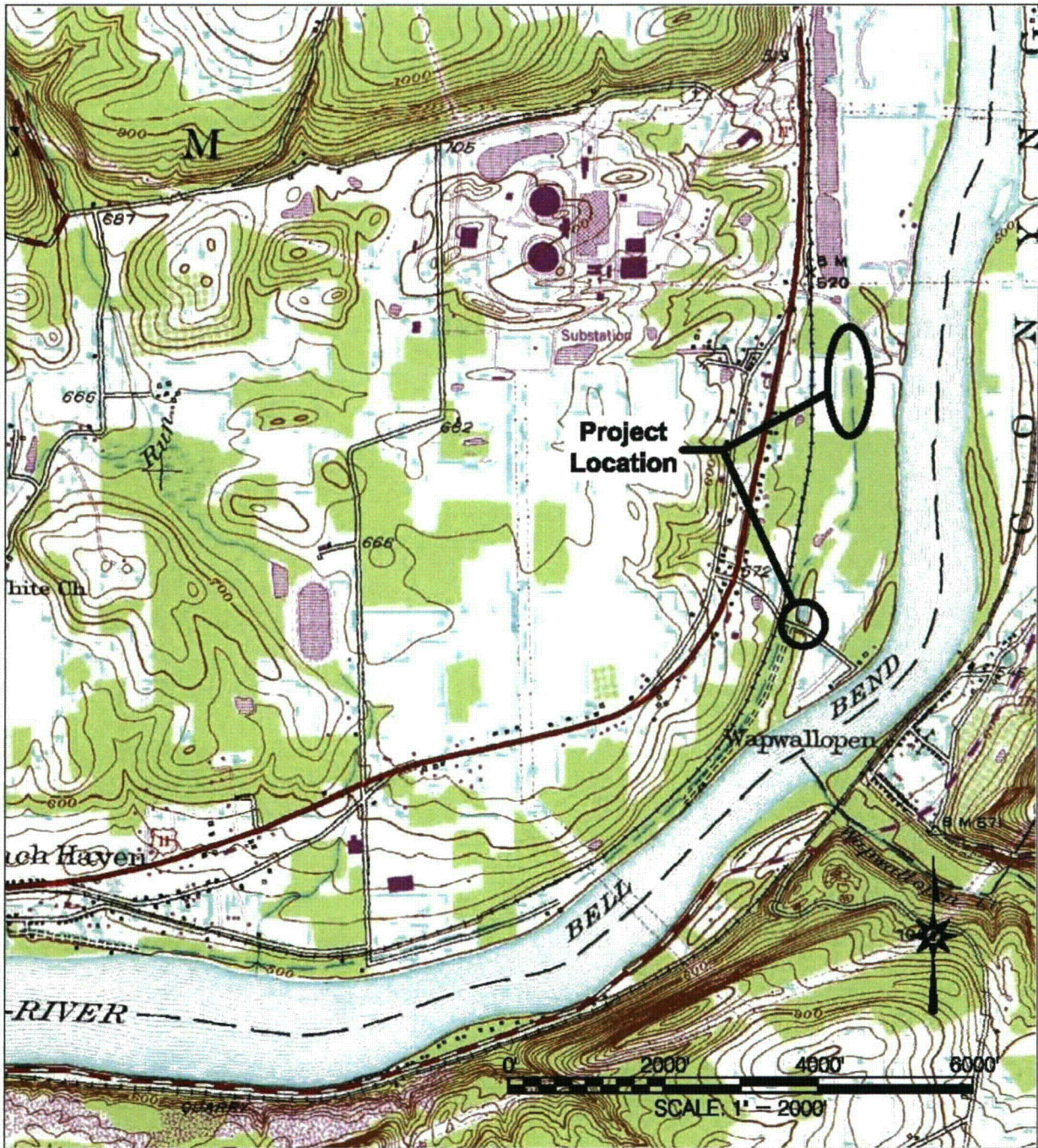


Figure 1 – Project Location Map

Riverlands Mitigation Project

Scale: 1" = 2,000'
 Location: 41° 05' 17" N 76° 08' 02" W
 Source: USGS 7.5 minute Quadrangle - Berwick, PA



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2 Physiographic Region, Geology, Hydrology and Existing Land Use

2.1 Physiographic Region

The project site is part of the Susquehanna Lowland Section of the Ridge and Valley physiographic province (see Figure 3), which is characterized by a distinctive series of linear ridges and valleys that are the result of differential erosion of folded sedimentary rocks with varying degrees of resistance to weathering and erosion. Valleys are composed of less resistant rocks such as limestone and shale, whereas ridges and uplands are composed of more resistant rocks, particularly sandstone and siltstone. The Susquehanna River has incised into and crosses these ridges as it flows generally from north to south, and its numerous tributaries form a trellis drainage network pattern as they flow along the valleys with less resistant rocks.

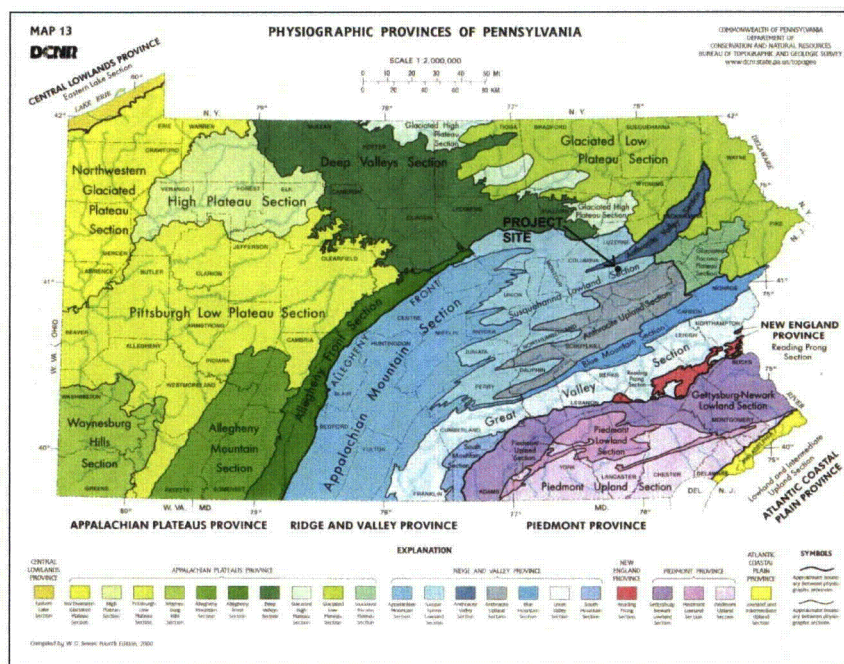


Figure 3 – Physiographic Provinces Map of Pennsylvania

2.2 Geology

This watershed consists of five different classes of surficial geology (Figure 4). A Holocene Alluvium is the most prevalent immediately around the Riverlands Mitigation project location. The watershed is primarily comprised of a Woodsfordian Kame Terrace and Outwash (undivided) and Woodsfordian Ground Moraine, both of Pleistocene Age. Woodfordian End Moraine and Eolian Mantle are also present in the watershed. The base geology of the majority of the watershed and all of the Riverlands Mitigation project site consists of a Mahantango Formation (Figure 5). The northern portion of the watershed is a Trimmers Rock Formation and there are small strips of Harrell Formation and Mahantango Formation (Tully Member), all of the Devonian Age.

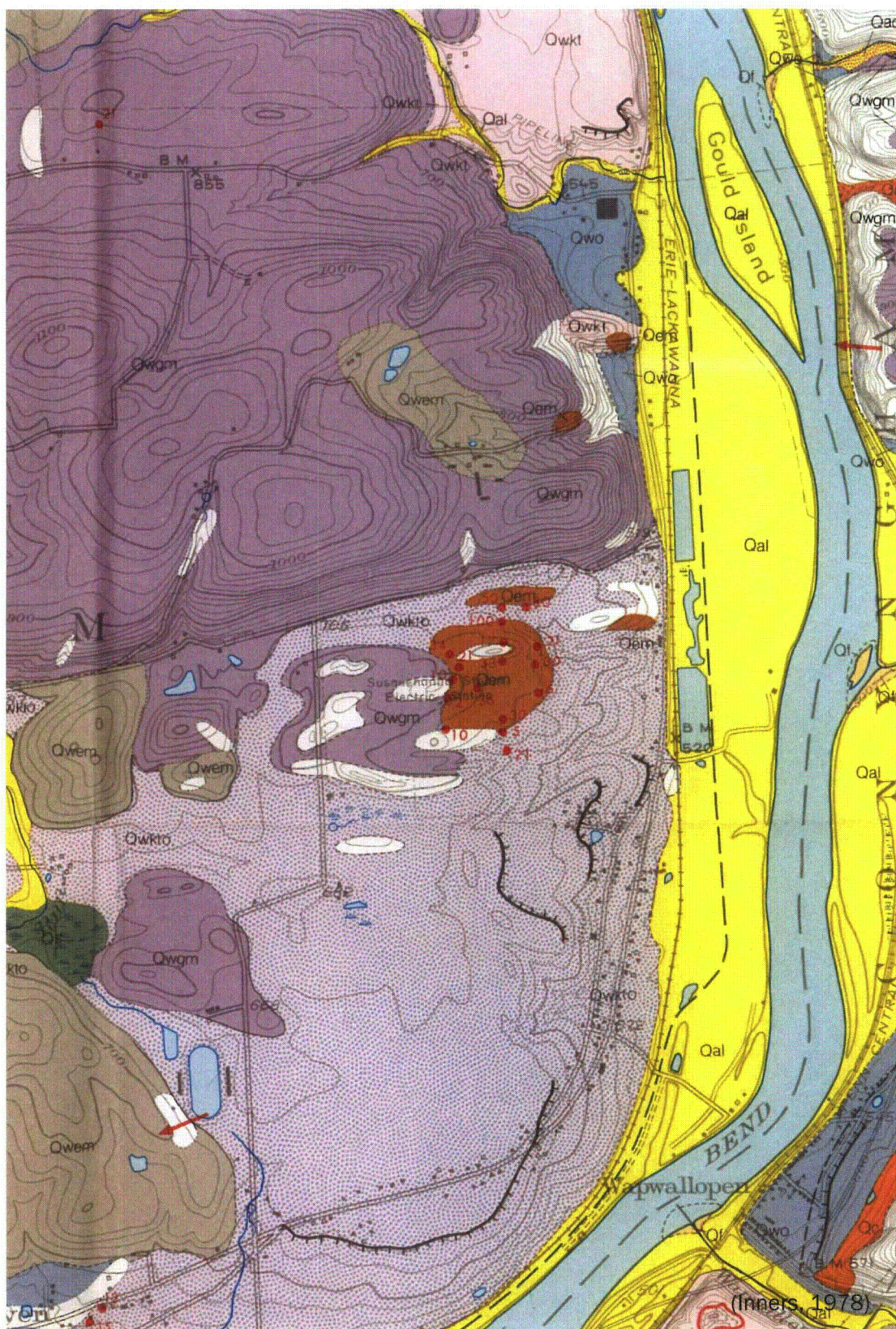


Figure 4 – Surficial Geology Map of Watershed



Figure 5 – Bedrock Geology Map of Watershed

2.3 General Site Hydrology

The Riverlands Mitigation Site watershed is approximately 1.2 square miles, consisting mainly of woods but also includes the majority of the footprint of the existing Susquehanna Steam Electric Station (SSES) and Lake Took-A-While (Figure 6). Flow in the watershed is generally in a west to east direction towards the abandoned North Branch Canal which then flows from north to south.

Stormwater flow from the SSES flows into the southern end of Lake Took-A-While via an unnamed tributary. The water surface elevation in Lake Took-A-While is controlled by a weir at the north end of the lake. The canal receives storm flow from Lake Took-A-While (Area A) as well as the forested portion of the watershed north of the SSES (Area B). The canal was used to bypass a segment of the North Branch of the Susquehanna River. The northern end of the canal is still visibly connected to the River, but the canal is filled and does not support any base flow from the River. Flood events from the Susquehanna River may overtop the earthen fill and contribute to the flow in the canal.

The water surface elevation in the canal is controlled by a weir and separate stoplog structure in a culvert south of Lake Took-A-While, near the existing SSES intake structure. The stoplog structure controls the water flowing to Riverlands Nature Area and the weir controls the flows that are directed to the North Branch of the Susquehanna River. See Figure 2 for the locations of these structures. The stoplogs for both structures are set at elevations according to the needs of the Riverlands facility operators and adjusted accordingly to maintain the desired water surface upstream into the Riverlands Recreation Area and to provide hydrology downstream to the Wetlands Nature Area. The entire site is located within the 100 year floodplain and will be inundated during a 100-year flood event.

2.4 Existing Land Use

The most significant historical land use around the Riverlands Mitigation Site is the construction and use of the canal. This segment of the canal system was known as the North Branch Canal (Columbia County Historical and Genealogical Society). Ground was first broken on July 4th, 1828 and was used until the entire 338 mile network of Pennsylvania canals were abandoned in 1901. At some point around the construction of Susquehanna Riverlands in the early 1980's, the canal was interrupted by constructing the configuration that is seen today (Figure 2).

The current watershed land use is predominantly forest, high density industrial and a lake. The land use around the proposed Riverlands Mitigation project is open water (canal), fallow fields and forest. The area is currently used for public recreation and education.

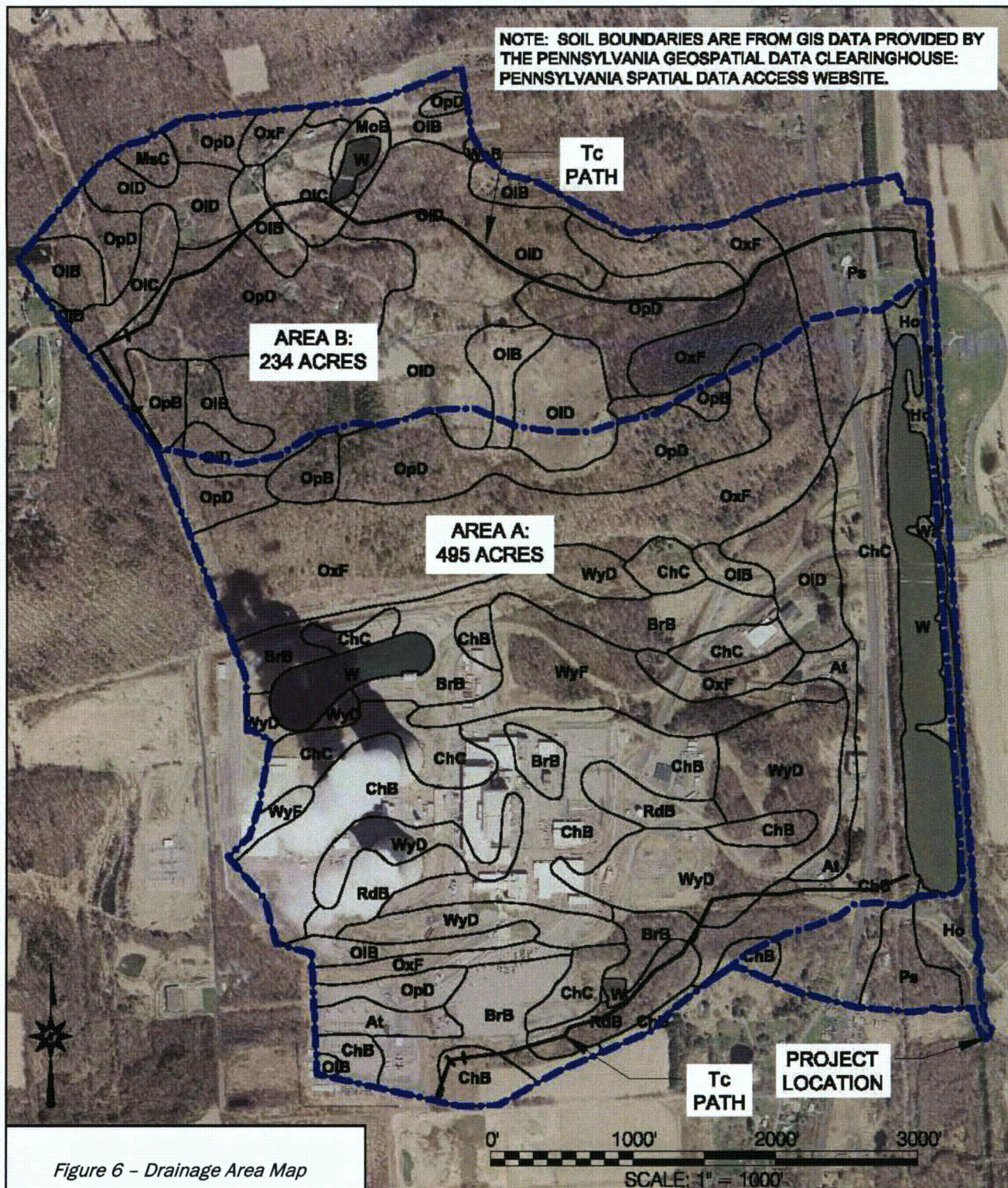


Figure 6 - Drainage Area Map



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LEGEND

- WATERSHED BOUNDARY
- + + + Tc PATH (WITH FLOW SEGMENTS)
- SOIL BOUNDARY
- ChC SOIL MAPPING UNIT
(SEE APPENDIX A FOR SOILS INFORMATION)

3 Visual Assessment of Watershed and Project Site

The land use in the upper reaches of the watershed to the mitigation area is currently a mix dominated by forest and high density industrial development. The eastern, or lower portion of the watershed is primarily mixed open space consisting of forest, lawn, open water and some cultivated land.

The project site adjacent to the canal consists of emergent and forested wetlands. The quality of these wetlands is marginal, primarily due to historic disturbance and invasive vegetation. The reach of the canal downstream of the existing weir has a significant amount of accumulated sediment. The canal outfall channel is severely eroded through most of its length and secondary ditch extends from a partial breach of the canal berm to the outfall channel.

Substrate embeddedness and composition surveys in the canal outfall channel indicate fair to poor habitat conditions near the existing weir structure and good substrate conditions near the confluence with the Susquehanna River. The habitat quality was marginal throughout the system but the macroinvertebrate community surveys reflected a fair to poor score based on the macroinvertebrate biotic index (LandStudies, Inc., 2010).

4 Design

4.1 Design Objectives

The specific design objectives include:

1. Provide an ecologically and environmentally solution to direct flow into the canal and away from the proposed intake structure.
2. Maintain a stable tailwater surface elevation in the canal while providing the flexibility to make fine adjustments to that water level on an as needed basis.
3. Enhance and restore the historical value of the canal and tow path.
4. Enhance the quality of existing wetlands at the Riverlands Mitigation Site.

4.2 Design Methodology

The design objectives will be achieved through the following tasks:

1. Re-connect the original canal and tow path and creating a trail on the original tow path.
2. Install a stop log structure and canal crossing that will be used to maintain water surface elevations in upstream reach of the canal and maintain access across the canal in this location.
3. Maintain and repair the grade control structure in PPL Riverlands Wetlands Nature Area to allow for the effective management of water surface elevations in the constructed wetlands.

4. Fill eroded gulleys in the canal outfall channel with amended soil to provide suitable growing media for wetland vegetation.
5. Remove invasive species and plant native trees and shrubs in existing wetlands adjacent to the canal.
6. Install an overflow pipe to prevent excessive ponding behind the fill for the proposed intake structure.

4.3 Hydrology and Hydraulics

The Riverlands Mitigation Site watershed is 1.24 square miles, which includes the majority of the footprint of the existing Susquehanna Seam Electric Station, Lake Took-A-While, a large portion of the North Branch Canal, and Forested and Meadow Areas. The drainage area to the site is depicted over an aerial photograph in Figure 6. The watershed hydrology was modeled using SCS TR-20 methodology using the Hydraflow Hydrographs extension of AutoCAD. This allowed the drainage area to be broken into sub watersheds and allowed the significant storage volume in Lake Took-A-While and the Canal to be routed.

The watershed was divided into "Area A," which drains to Lake Took-A-While, and "Area B," which drains to the North Branch Canal. Land cover was evaluated for both drainage areas using aerial photography and site observations, and weighted Curve Numbers were calculated using standard CN values listed in TR-55. Time of concentration paths were mapped, as shown on Figure 6, and Tc values were developed using TR-55 methods for sheet flow, shallow concentrated, channel flow. Rainfall values were obtained from NOAA Atlas 14 data.

Runoff hydrographs for the 2, 5, 10, 25, 50, and 100-year storms were developed for Areas A and B, based on the inputs described above. The Hydrograph from Area A was routed through Lake Took-A-While using the storage indication method in the Hydrographs application. Pond data was based on existing topography and field measurements of the existing two-stage weir through which the lake discharges into the canal. The resultant routed hydrograph was then added to the Area B hydrograph. Finally, canal was routed through the proposed stoplog structure and pipe.

The proposed canal crossing was also modeled in HY-8 to more accurately reflect the overtopping conditions during large storm events. The routing of the structure using the Hydrographs software has the limitation of only allowing the input of a broad crested weir at a single elevation. HY-8 allows the input of an irregular overtopping cross section, but does not support a multi-stage weir structure at the inlet of a culvert. Based on these limitations, the Hydrographs model accurately predicts flow through the proposed stoplog structure and culvert up to the overtopping elevation. At that point and above, the pipe is in an outlet control condition, rendering the stoplog structure ineffective. Therefore, the HY-8 model more accurately predicts the performance of the system once overtopping begins, even though the stoplog structure is not included, due to the more accurate overtopping cross section.

Based on both hydraulic models, the proposed crossing will overtop during an event greater than the 10-year storm. All data inputs and routings, as well as model summary output is provided in Appendix A.

4.4 Design Summary

This design is intended to take flow that would currently go to the Susquehanna River and redirect it into the lower segment of the historical canal. This is necessary because the location and orientation of the proposed intake structure will prevent higher flows from going to the Susquehanna River and would otherwise flood the area around the intake structure. The installation of a stoplog structure will maintain the backwater elevation that is necessary to keep water in the canal upstream of this location, while conveying base flow and storm flow downstream in the canal into the PPL Riverlands Wetland and Nature Area. The gulleys that are currently present on the east side of the canal tow path will be repaired by placing amended topsoil in the deepest portions of the gulleys and promoting the establishment of wetland plant species. A headwall and 18" smooth lined corrugated polyethylene pipe will be installed at the toe of the proposed intake structure fill and will provide positive relief for local runoff that would otherwise be impounded behind the fill. This eliminates the potential for this wetland area to be permanently flooded, maintaining the existing hydrology of the system.

A walking path will be established on the restored tow path of the historic North Branch Canal and a crossing will be created across the canal at the location of the stoplog structure. This stoplog structure will consist of a precast concrete drop structure with oak stop logs set to establish the desired elevation in the upstream reach of the canal. This drop structure will connect to a 48" diameter smooth lined corrugated polyethylene pipe that outlets to the lower segment of the North Branch Canal and provided conveyance under the crossing. The crown of the crossing will be constructed such that overtopping will occur on the west side of the canal and proceed into the downstream segment of the existing canal rather than towards the proposed intake structure. This will promote channel and bank stability as well as keeping the majority of the flow away from the depression behind the proposed intake structure.

Invasive species will be removed from the adjacent wetland areas. Native tree, shrub, and herbaceous species will be planted in these adjacent wetlands, including the abandoned canal outfall channel. A plant list for the proposed wetland enhancement can be found in Appendix A.

See the Wetland Mitigation Plan for the Riverlands Site for Construction Drawings, Details, Specifications, and the Landscape Plan.

5 References

- Columbia County Historical and Genealogical Society. (n.d.). *Gala Day in 1828 at Berwick as Ground Broken for Canal*. Retrieved November 4, 2010, from <http://www.colcohist-gensoc.org/Essays/berwickcanal.htm>
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Appendix A:
Hydrology and Hydraulics Data and Calculations

Hydrograph Return Period

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph ID	Hydrograph Type Origin	Inflow Hydrograph	Peak Outflow								Hydrograph Description
			1yr	2yr	3yr	4yr	5yr	10yr	20yr	50yr	
1	SCS Runoff	-----	-----	185.07	-----	314.14	461.17	698.73	930.82	1220.87	Area A
2	Reservoir	1	-----	19.79	-----	40.00	69.20	127.48	195.85	293.33	Lake Took-a-While
3	SCS Runoff	-----	-----	10.38	-----	33.35	70.09	143.65	225.78	337.54	Area B
4	Combine	2, 3	-----	23.66	-----	54.07	101.34	200.05	313.66	473.19	Combined Area A and B
5	Reservoir	4	-----	14.83	-----	34.23	56.74	121.76	202.09	323.52	Canal - Stop Log

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph ID	Hydrograph Type / Origin	Peak Flow (cfs)	Time to Peak (min)	Peak Elevation (ft)	Hydrograph Volume (cu ft)	Inflow Hydrograph	Maximum Elevation (ft)	Total Storage (cu ft)	Hydrograph Description
1	SCS Runoff	185.07	2	746	1,254,122	-----	-----	-----	Area A
2	Reservoir	19.79	2	956	1,252,985	1	508.62	669,022	Lake Took-a-While
3	SCS Runoff	10.38	2	764	158,998	-----	-----	-----	Area B
4	Combine	23.66	2	924	1,411,984	2, 3	-----	-----	Combined Area A and B
5	Reservoir	14.83	2	1454	1,380,214	4	509.27	621,088	Canal - Stop Log
Proposed Stop Log.gpw					Return Period: 2 Year			Thursday, Nov 18, 2010	

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph ID	Hydrograph Type / Origin	Peak Flow (cfs)	Time Interval (min)	Time to Peak (min)	Hydrograph Volume (cu ft)	Inflow Hydrograph	Maximum Elevation (ft)	Total Storage (cu ft)	Hydrograph Description
1	SCS Runoff	314.14	2	744	1,957,240	-----	-----	-----	Area A
2	Reservoir	40.00	2	868	1,955,889	1	508.91	997,875	Lake Took-a-While
3	SCS Runoff	33.35	2	750	331,788	-----	-----	-----	Area B
4	Combine	54.07	2	774	2,287,680	2, 3	-----	-----	Combined Area A and B
5	Reservoir	34.23	2	1148	2,251,672	4	509.53	724,971	Canal - Stop Log
Proposed Stop Log.gpw					Return Period: 5 Year			Thursday, Nov 18, 2010	

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph ID	Hydrograph Type (Origin)	Peak Flow (cfs)	Time Interval (min)	Time to Peak (min)	Hydrograph Volume (cu ft)	Time to Hydrograph (min)	Maximum Elevation (ft)	Total Storage (cu ft)	Hydrograph Description
1	SCS Runoff	461.17	2	744	2,753,967	----	----	----	Area A
2	Reservoir	69.20	2	832	2,752,453	1	509.25	1,385,064	Lake Took-a-While
3	SCS Runoff	70.09	2	746	554,710	----	----	----	Area B
4	Combine	101.34	2	766	3,307,163	2, 3	----	----	Combined Area A and B
5	Reservoir	56.74	2	1052	3,267,716	4	509.99	905,762	Canal - Stop Log
Proposed Stop Log.gpw					Return Period: 10 Year			Thursday, Nov 18, 2010	

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph ID	Hydrograph Type / Origin	Peak Flow (cfs)	Time Interval (min)	Peak Elevation (ft)	Hydrograph Volume (cu ft)	Initial Hydrograph	Maximum Elevation (ft)	Total Storage Used (cu ft)	Hydrograph Description
1	SCS Runoff	1220.87	2	744	6,933,142	----	----	----	Area A
2	Reservoir	293.33	2	790	6,931,184	1	511.04	3,428,562	Lake Took-a-While
3	SCS Runoff	337.54	2	742	1,955,443	----	----	----	Area B
4	Combine	473.19	2	758	8,886,613	2, 3	----	----	Combined Area A and B
5	Reservoir	323.52	2	826	8,838,069	4	511.26	1,494,673	Canal - Stop Log
Proposed Stop Log.gpw					Return Period: 100 Year			Thursday, Nov 18, 2010	



SWAT2002

Area: Lake Coosa file

Soil	Code	Area	Area	Area
Forest (Good)*	C	55	197.60	10,868.00
Commercial (85% imperv)	C	94	49.40	4,643.60
Commercial (85% imperv)	A	89	173.60	15,450.40
Forest (Good)	A	30	49.60	1,488.00
Water	-	100	24.80	2,480.00

Total CN*A = 34,930.00

Total Area = 2,000.00 a

Weighted

Area: SWAT2002 information enter

Soil	Code	Area	Area	Area
Forest (Good)*	C	55	187.00	10,285.00
Meadow (Good)*	C	58	47.00	2,726.00

Total CN*A = 13,011.00

Total Area = 2,000.00 a

Weighted

* Adjusted to HSG B CN values based on site observations and calibration with other runoff models

Ma	ay	col	oil	erie	lo	e	hydrologi	oil	rou
At				Atherton silt loam		---		B/D	
BrB				Braceville gravelly loam		3% to 8%		C	
ChB				Chenango gravelly loam		3% to 8%		A	
ChC				Chenango gravelly loam		8% to 15%		A	
Ho				Holly silt loam		---		B/D	
MoB				Morris channery silt loam		0% to 8%		C	
MsC				Morris very stony silt loam		8% to 15%		C	
OIB				Oquaga and Lordstown channery silt loams		3% to 8%		C	
OIC				Oquaga and Lordstown channery silt loams		8% to 15%		C	
OID				Oquaga and Lordstown channery silt loams		15% to 25%		C	
OpB				Oquaga and Lordstown extremely stony silt loams		3% to 8%		C	
OpD				Oquaga and Lordstown extremely stony silt loams		8% to 25%		C	
OxF				Oquaga and Lordstown extremely stony silt loams		Steep		C	
Ps				Pope soils		---		B	
RdB				Rexford loam		3% to 8%		C	
W				Water		---		---	
Wa				Wayland silt loam		---		C/D	
WeB				Weikert and Klinesville channery silt loams		3% to 8%		C/D	
WyD				Wyoming gravelly loam		15% to 25%		A	

Sources: Pennsylvania College of Agricultural Sciences Cooperative Extension and United States Department of Agriculture Soil Conservation Service



POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



Pennsylvania 41.0868 N 76.1595 W 685 feet
from "Precipitation-Frequency Atlas of the United States" NOAA Atlas 14, Volume 2, Version 3
G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley
NOAA, National Weather Service, Silver Spring, Maryland, 2004
Extracted: Thu Mar 18 2010

Confidence Limits	Seasonality	Location Maps	Other Info.	GIS data	Maps	Docs	Return to State Map
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Precipitation Frequency Estimates (inches)																		
ARI* (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
1	0.33	0.52	0.63	0.84	1.02	1.20	1.32	1.64	2.03	2.38	2.81	3.15	3.71	4.29	5.83	7.27	9.20	11.07
2	0.40	0.62	0.75	1.01	1.24	1.45	1.58	1.97	2.42	2.86	3.37	3.75	4.42	5.09	6.88	8.53	10.72	12.87
5	0.47	0.72	0.89	1.22	1.52	1.79	1.95	2.41	2.99	3.54	4.16	4.60	5.37	6.12	8.04	9.81	12.13	14.44
10	0.52	0.80	0.98	1.37	1.74	2.08	2.27	2.80	3.48	4.15	4.87	5.35	6.20	7.02	9.04	10.90	13.32	15.78
25	0.59	0.90	1.11	1.56	2.03	2.50	2.74	3.38	4.23	5.12	6.00	6.54	7.52	8.40	10.56	12.53	15.07	17.73
50	0.64	0.97	1.20	1.72	2.26	2.87	3.16	3.90	4.91	6.01	7.04	7.63	8.72	9.64	11.89	13.93	16.56	19.39
100	0.70	1.05	1.30	1.88	2.51	3.29	3.65	4.50	5.69	7.07	8.28	8.93	10.12	11.07	13.38	15.48	18.17	21.17
200	0.76	1.13	1.41	2.05	2.78	3.77	4.20	5.19	6.60	8.33	9.75	10.45	11.77	12.72	15.08	17.20	19.92	23.10
500	0.84	1.24	1.55	2.30	3.18	4.51	5.08	6.29	8.05	10.37	12.13	12.91	14.39	15.31	17.66	19.78	22.48	25.91
1000	0.92	1.33	1.67	2.50	3.51	5.17	5.86	7.26	9.37	12.26	14.35	15.18	16.78	17.63	19.91	21.98	24.62	28.23

* These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval.
Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting forces estimates near zero to appear as zero.

* Upper bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																		
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
1	0.37	0.57	0.70	0.93	1.14	1.34	1.48	1.86	2.29	2.66	3.17	3.50	4.12	4.72	6.32	7.84	9.86	11.79
2	0.44	0.69	0.84	1.12	1.38	1.62	1.77	2.22	2.73	3.19	3.80	4.18	4.92	5.61	7.45	9.19	11.50	13.71
5	0.52	0.80	0.99	1.35	1.70	2.01	2.19	2.72	3.36	3.95	4.69	5.11	5.97	6.74	8.69	10.56	13.00	15.38
10	0.58	0.89	1.09	1.52	1.93	2.32	2.54	3.15	3.91	4.61	5.47	5.93	6.88	7.71	9.75	11.72	14.27	16.80
25	0.65	0.99	1.23	1.74	2.25	2.79	3.07	3.80	4.74	5.65	6.70	7.20	8.30	9.19	11.36	13.44	16.13	18.88
50	0.71	1.08	1.34	1.91	2.52	3.21	3.54	4.38	5.50	6.60	7.83	8.39	9.59	10.53	12.77	14.93	17.71	20.62
100	0.78	1.17	1.45	2.09	2.80	3.69	4.09	5.05	6.38	7.73	9.18	9.77	11.11	12.06	14.36	16.57	19.42	22.50
200	0.84	1.26	1.57	2.29	3.10	4.23	4.72	5.84	7.42	9.06	10.76	11.41	12.87	13.82	16.15	18.40	21.27	24.55
500	0.95	1.39	1.74	2.58	3.56	5.08	5.73	7.12	9.11	11.22	13.33	14.02	15.67	16.61	18.88	21.13	23.98	27.54
1000	1.03	1.50	1.88	2.81	3.95	5.87	6.66	8.26	10.65	13.19	15.71	16.43	18.24	19.09	21.27	23.47	26.26	30.03

* The **upper** bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are **greater** than.

** These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval.

Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

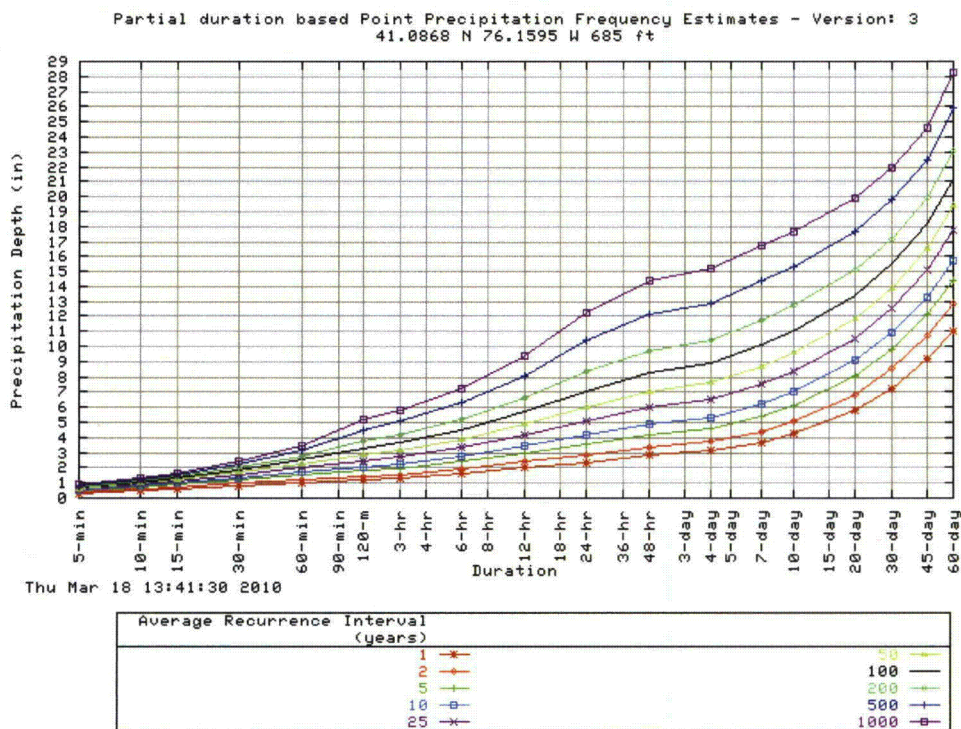
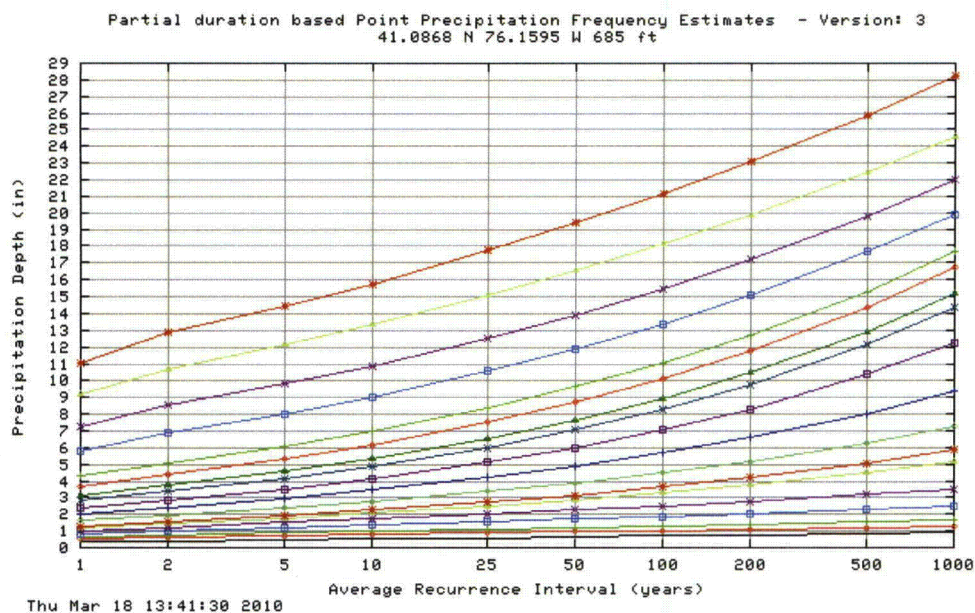
* Lower bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																		
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
1	0.30	0.47	0.57	0.75	0.92	1.08	1.18	1.47	1.82	2.16	2.53	2.87	3.38	3.93	5.43	6.80	8.64	10.45
2	0.35	0.55	0.68	0.91	1.11	1.30	1.42	1.76	2.17	2.59	3.04	3.42	4.03	4.67	6.39	7.96	10.07	12.15
5	0.42	0.65	0.80	1.09	1.37	1.61	1.75	2.16	2.68	3.21	3.75	4.19	4.89	5.61	7.46	9.15	11.38	13.63
10	0.47	0.72	0.88	1.23	1.56	1.86	2.03	2.49	3.10	3.74	4.37	4.86	5.63	6.40	8.37	10.14	12.49	14.88
25	0.52	0.80	0.99	1.39	1.81	2.22	2.44	2.99	3.74	4.57	5.34	5.89	6.79	7.62	9.73	11.63	14.10	16.70
50	0.57	0.86	1.07	1.52	2.01	2.54	2.79	3.43	4.31	5.33	6.23	6.84	7.83	8.71	10.92	12.90	15.46	18.22
100	0.61	0.93	1.15	1.66	2.22	2.89	3.19	3.91	4.95	6.21	7.26	7.94	9.02	9.94	12.24	14.28	16.92	19.85
200	0.66	0.99	1.23	1.80	2.44	3.28	3.64	4.47	5.67	7.25	8.46	9.21	10.40	11.33	13.72	15.79	18.49	21.60
500	0.73	1.08	1.34	1.99	2.75	3.87	4.32	5.32	6.80	8.90	10.39	11.24	12.55	13.49	15.93	18.03	20.75	24.11
1000	0.79	1.14	1.43	2.14	3.01	4.37	4.92	6.07	7.79	10.38	12.13	13.06	14.47	15.41	17.83	19.91	22.63	26.16

* The **lower** bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are **less** than.

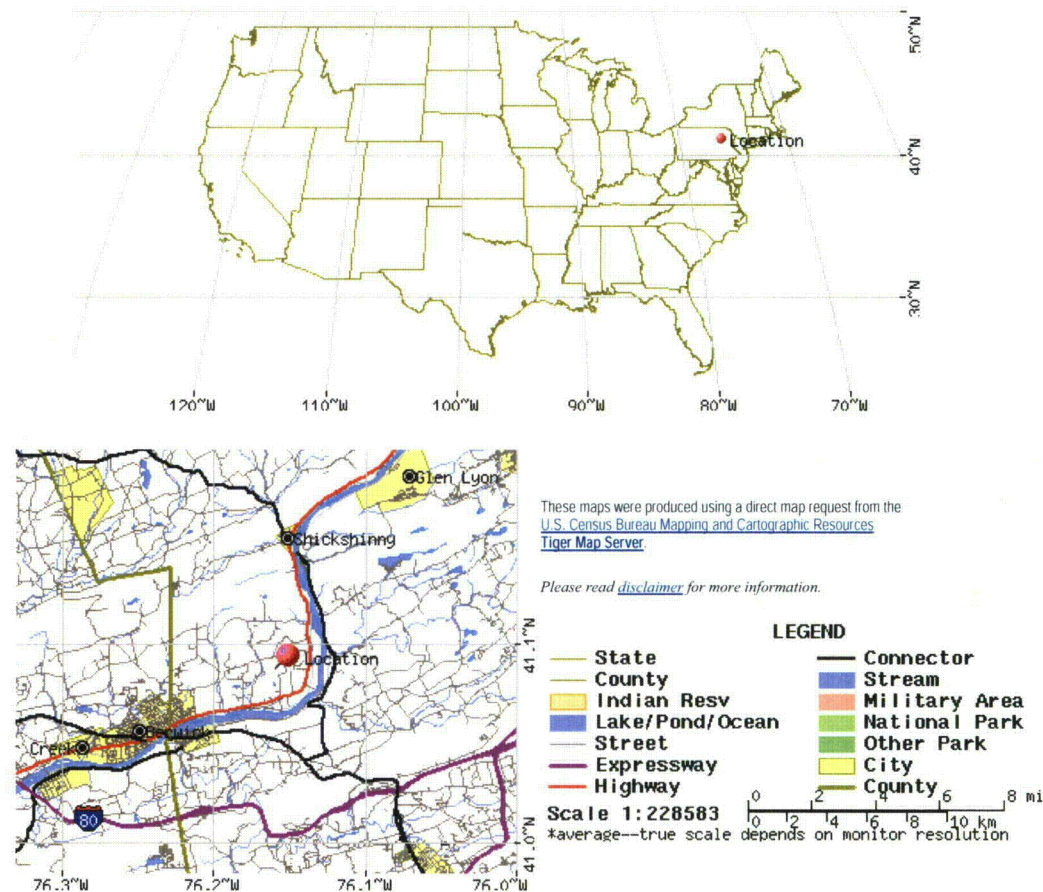
** These precipitation frequency estimates are based on a partial duration maxima series. ARI is the Average Recurrence Interval.

Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

Text version of tables



Maps -



Other Maps/Photographs -

[View USGS digital orthophoto quadrangle \(DOQ\)](#) covering this location from TerraServer; [USGS Aerial Photograph](#) may also be available from this site. A DOQ is a computer-generated image of an aerial photograph in which image displacement caused by terrain relief and camera tilts has been removed. It combines the image characteristics of a photograph with the geometric qualities of a map. Visit the [USGS](#) for more information.

Watershed/Stream Flow Information -

[Find the Watershed](#) for this location using the U.S. Environmental Protection Agency's site.

Climate Data Sources -

Precipitation frequency results are based on data from a variety of sources, but largely NCDC. The following links provide general information about observing sites in the area, regardless of if their data was used in this study. For detailed information about the stations used in this study, please refer to [NOAA Atlas 14 Document](#).

Using the [National Climatic Data Center's \(NCDC\)](#) station search engine, locate other climate stations within:

...OR...

of this location (41.0868/-76.1595). Digital ASCII data can be obtained directly from [NCDC](#).

Hydrometeorological Design Studies Center
DOC/NOAA/National Weather Service
1325 East-West Highway
Silver Spring, MD 20910
(301) 713-1669
Questions?: HDSC.Questions@noaa.gov

[Disclaimer](#)

or sheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydrograph

Area A

Definition

Sheet Flow

Manning's n-value	= 0.170	0.011	0.011
Flow length (ft)	= 300.0	0.0	0.0
Two-year 24-hr precip. (in)	= 2.89	0.00	0.00
Land slope (%)	= 1.00	0.00	0.00

Travel time in

2

Channel Concentrated Flow

Flow length (ft)	= 100.00	0.00	0.00
Watercourse slope (%)	= 2.00	0.00	0.00
Surface description	= Unpaved	Paved	Paved
Average velocity (ft/s)	=2.28	0.00	0.00

Travel time in

Channel Flow

X sectional flow area (sqft)	= 3.00	0.00	0.00
Wetted perimeter (ft)	= 5.00	0.00	0.00
Channel slope (%)	= 2.20	0.00	0.00
Manning's n-value	= 0.035	0.015	0.015
Velocity (ft/s)	=4.48		

0.00

0.00

Flow length (ft)

{0}3600.0

0.0

0.0

Travel time in

Total Travel time

2 in

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Hydrograph

Area A

Hydrograph type	= SCS Runoff	Peak discharge	= 461.17 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 2,753,967 cuft
Drainage area	= 495.000 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 50.3 min
Total precip.	= 4.20 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Hydrograph Discharge Table

(Printed values >= 10.00% of Qp. Print interval = 5)

Time (hr)	Discharge (cfs)	Time (hr)	Discharge (cfs)
11.83	54.79	14.83	47.47
12.00	171.73		
12.17	321.85	...End	
12.33	443.95		
12.50	440.20		
12.67	377.45		
12.83	299.15		
13.00	212.37		
13.17	133.89		
13.33	100.52		
13.50	87.05		
13.67	77.70		
13.83	70.86		
14.00	65.10		
14.17	60.14		
14.33	55.92		
14.50	52.39		
14.67	49.63		

Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Pond Location: Lake Coosa file

Pond Data

Contour: User-defined contour areas. Conic method used for volume calculation. Beginning Elevation = 508.03 ft

Storage Table

Stage (ft)	Elevation (ft)	Contour area (sq ft)	Incremental storage (cu ft)	Total storage (cu ft)
0.00	508.03	1,043,909	0	0
5.00	513.03	1,233,733	5,686,933	5,686,933

Culvert/Orifice Structure

	IC	OC	IC	OC
Size (in)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00
Barrel	= 0	0	0	0
Inlet Control	= 0.00	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Flow	= 0.00	0.00	0.00	n/a
Value	= .013	.013	.013	n/a
Orifice Coefficient	= 0.60	0.60	0.60	0.60
Multi-stage	= n/a	No	No	No

Weir Structure

	IC	OC	IC	OC
Ret Len (ft)	= 6.00	12.00	0.00	0.00
Ret Elevation	= 508.03	508.23	0.00	0.00
Weir Coefficient	= 3.33	3.33	3.33	3.33
Weir Type	= Rect	Rect	---	---
Multi-stage	= No	No	No	No
Orifice Inlet	= 0.000 (by Contour)			
Orifice Outlet	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Storage Incremental Storage Table

Stage (ft)	Storage (cu ft)	Elevation (ft)	IC	OC	IC	OC	Pr	IC	OC	IC	OC	IC	OC	Total
0.00	0	508.03	---	---	---	---	---	0.00	0.00	---	---	---	---	0.000
5.00	5,686,933	513.03	---	---	---	---	---	223.39	420.23	---	---	---	---	643.62

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Hydrograph 2

Lake Took-a-While

Hydrograph type	= Reservoir	Peak discharge	= 69.20 cfs
Storm frequency	= 10 yrs	Time to peak	= 13.87 hrs
Time interval	= 2 min	Hyd. volume	= 2,752,453 cuft
Inflow hyd. No.	= 1 - Area A	Reservoir name	= Lake Took-a-While
Max. Elevation	= 509.25 ft	Max. Storage	= 1,385,064 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 20.00% of Qp. Print interval = 5)

Time	Inflow	Elevation	Storage	Peak	Rate	Rate	Rate	Rate	Rate	Rate	Rate	Rate
Time	Inflow	Elevation	Storage	Peak	Rate	Rate	Rate	Rate	Rate	Rate	Rate	Rate
12.50	440.20	508.68	----	----	----	----	10.93	13.17	----	----	----	24.10
12.67	377.45	508.88	----	----	----	----	16.10	21.97	----	----	----	38.07
12.83	299.15	509.04	----	----	----	----	20.17	28.94	----	----	----	49.11
13.00	212.37	509.14	----	----	----	----	23.72	35.45	----	----	----	59.17
13.17	133.89	509.20	----	----	----	----	25.65	38.98	----	----	----	64.62
13.33	100.52	509.22	----	----	----	----	26.48	40.50	----	----	----	66.98
13.50	87.05	509.24	----	----	----	----	26.93	41.33	----	----	----	68.26
13.67	77.70	509.24	----	----	----	----	27.17	41.76	----	----	----	68.94
13.83	70.86	509.25	----	----	----	----	27.26	41.93	----	----	----	69.19
14.00	65.10	509.25	----	----	----	----	27.24	41.89	----	----	----	69.13
14.17	60.14	509.24	----	----	----	----	27.12	41.68	----	----	----	68.80
14.33	55.92	509.24	----	----	----	----	26.94	41.34	----	----	----	68.28
14.50	52.39	509.23	----	----	----	----	26.69	40.89	----	----	----	67.58
14.67	49.63	509.22	----	----	----	----	26.41	40.37	----	----	----	66.77
14.83	47.47	509.21	----	----	----	----	26.09	39.79	----	----	----	65.88
15.00	45.70	509.20	----	----	----	----	25.76	39.18	----	----	----	64.94
15.17	44.17	509.19	----	----	----	----	25.42	38.55	----	----	----	63.96
15.33	42.75	509.18	----	----	----	----	25.06	37.90	----	----	----	62.96
15.50	41.33	509.17	----	----	----	----	24.70	37.24	----	----	----	61.94
15.67	39.90	509.16	----	----	----	----	24.33	36.57	----	----	----	60.90

Continues on next page...

Hydrographic Chart

Depth Feet	Depth Meters	Elevation Feet	Latitude N	Latitude S	Longitude W	Pressure Feet	Bar Feet	Bar Meters	Bar Feet	Bar Meters	Bar Feet	Bar Meters
15.83	38.44	509.15	----	----	----	----	23.96	35.89	----	----	----	59.84
16.00	36.97	509.14	----	----	----	----	23.58	35.19	----	----	----	58.77
16.17	35.51	509.13	----	----	----	----	23.19	34.48	----	----	----	57.67
16.33	34.12	509.11	----	----	----	----	22.80	33.76	----	----	----	56.55
16.50	32.90	509.10	----	----	----	----	22.40	33.03	----	----	----	55.43
16.67	31.91	509.09	----	----	----	----	22.00	32.30	----	----	----	54.31
16.83	31.11	509.08	----	----	----	----	21.61	31.58	----	----	----	53.19
17.00	30.46	509.07	----	----	----	----	21.23	30.88	----	----	----	52.10
17.17	29.90	509.06	----	----	----	----	20.85	30.18	----	----	----	51.03
17.33	29.38	509.04	----	----	----	----	20.48	29.51	----	----	----	49.99
17.50	28.86	509.03	----	----	----	----	20.12	28.85	----	----	----	48.97
17.67	28.34	509.02	----	----	----	----	19.82	28.32	----	----	----	48.13
17.83	27.81	509.01	----	----	----	----	19.55	27.86	----	----	----	47.41
18.00	27.28	509.00	----	----	----	----	19.28	27.40	----	----	----	46.69
18.17	26.75	508.99	----	----	----	----	19.02	26.95	----	----	----	45.98
18.33	26.21	508.98	----	----	----	----	18.76	26.51	----	----	----	45.27
18.50	25.67	508.97	----	----	----	----	18.50	26.07	----	----	----	44.57
18.67	25.13	508.96	----	----	----	----	18.24	25.63	----	----	----	43.88
18.83	24.58	508.95	----	----	----	----	17.99	25.20	----	----	----	43.19
19.00	24.03	508.94	----	----	----	----	17.74	24.77	----	----	----	42.50
19.17	23.48	508.93	----	----	----	----	17.49	24.34	----	----	----	41.83
19.33	22.93	508.92	----	----	----	----	17.24	23.92	----	----	----	41.15
19.50	22.37	508.91	----	----	----	----	16.99	23.49	----	----	----	40.48
19.67	21.81	508.90	----	----	----	----	16.74	23.07	----	----	----	39.82
19.83	21.24	508.90	----	----	----	----	16.50	22.66	----	----	----	39.15
20.00	20.68	508.89	----	----	----	----	16.26	22.24	----	----	----	38.50
20.17	20.12	508.88	----	----	----	----	16.01	21.83	----	----	----	37.84
20.33	19.60	508.87	----	----	----	----	15.77	21.42	----	----	----	37.19

Continues on next page...

Hydrographic Sounding Log

Time	Lat	Long	Depth	Temp	Sal	Pressure	Surf	1m	2m	3m	4m	5m	Bottom
20.50	19.16	508.86	----	----	----	----	15.53	21.01	----	----	----	----	36.54
20.67	18.83	508.85	----	----	----	----	15.30	20.61	----	----	----	----	35.91
20.83	18.60	508.84	----	----	----	----	15.07	20.22	----	----	----	----	35.29
21.00	18.43	508.83	----	----	----	----	14.84	19.83	----	----	----	----	34.68
21.17	18.30	508.82	----	----	----	----	14.63	19.46	----	----	----	----	34.09
21.33	18.20	508.81	----	----	----	----	14.41	19.10	----	----	----	----	33.52
21.50	18.10	508.81	----	----	----	----	14.21	18.75	----	----	----	----	32.96
21.67	18.00	508.80	----	----	----	----	14.01	18.41	----	----	----	----	32.42
21.83	17.90	508.79	----	----	----	----	13.82	18.08	----	----	----	----	31.90
22.00	17.80	508.78	----	----	----	----	13.63	17.76	----	----	----	----	31.39
22.17	17.69	508.78	----	----	----	----	13.45	17.45	----	----	----	----	30.89
22.33	17.59	508.77	----	----	----	----	13.27	17.15	----	----	----	----	30.41
22.50	17.49	508.76	----	----	----	----	13.10	16.85	----	----	----	----	29.95
22.67	17.39	508.76	----	----	----	----	12.93	16.57	----	----	----	----	29.50
22.83	17.28	508.75	----	----	----	----	12.77	16.29	----	----	----	----	29.05
23.00	17.18	508.74	----	----	----	----	12.61	16.02	----	----	----	----	28.63
23.17	17.07	508.74	----	----	----	----	12.45	15.76	----	----	----	----	28.21
23.33	16.97	508.73	----	----	----	----	12.30	15.50	----	----	----	----	27.81
23.50	16.86	508.73	----	----	----	----	12.16	15.25	----	----	----	----	27.41
23.67	16.76	508.72	----	----	----	----	12.02	15.01	----	----	----	----	27.03
23.83	16.65	508.72	----	----	----	----	11.88	14.78	----	----	----	----	26.65
24.00	16.54	508.71	----	----	----	----	11.74	14.55	----	----	----	----	26.29
24.17	15.63	508.71	----	----	----	----	11.61	14.32	----	----	----	----	25.92
24.33	13.38	508.70	----	----	----	----	11.46	14.06	----	----	----	----	25.51
24.50	9.802	508.69	----	----	----	----	11.27	13.74	----	----	----	----	25.01
24.67	6.194	508.68	----	----	----	----	11.04	13.35	----	----	----	----	24.40
24.83	3.416	508.67	----	----	----	----	10.78	12.90	----	----	----	----	23.68
25.00	1.461	508.66	----	----	----	----	10.49	12.42	----	----	----	----	22.91

Continues on next page...

Hydrograph of discharge table

Time hr	Discharge cfs	Elevation ft	Flow cfs	Flow cfs	Flow cfs	Power hp	Flow cfs	Flow cfs	Flow cfs	Flow cfs	Flow cfs	Output hp
25.17	0.324	508.65	----	----	----	----	10.20	11.91	----	----	----	22.11
25.33	0.000	508.64	----	----	----	----	9.905	11.41	----	----	----	21.32
25.50	0.000	508.63	----	----	----	----	9.620	10.92	----	----	----	20.54
25.67	0.000	508.62	----	----	----	----	9.345	10.46	----	----	----	19.80
25.83	0.000	508.61	----	----	----	----	9.080	10.00	----	----	----	19.08
26.00	0.000	508.60	----	----	----	----	8.825	9.569	----	----	----	18.39
26.17	0.000	508.59	----	----	----	----	8.578	9.148	----	----	----	17.73
26.33	0.000	508.58	----	----	----	----	8.342	8.745	----	----	----	17.09
26.50	0.000	508.57	----	----	----	----	8.113	8.355	----	----	----	16.47
26.67	0.000	508.56	----	----	----	----	7.893	7.979	----	----	----	15.87
26.83	0.000	508.55	----	----	----	----	7.680	7.617	----	----	----	15.30
27.00	0.000	508.55	----	----	----	----	7.476	7.267	----	----	----	14.74
27.17	0.000	508.54	----	----	----	----	7.278	6.931	----	----	----	14.21

...End

or sheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Hydro

Area B

Description

Sheet Flow

Manning's n-value	= 0.240	0.011	0.011
Flow length (ft)	= 300.0	0.0	0.0
Two-year 24-hr precip. (in)	= 2.89	0.00	0.00
Land slope (%)	= 3.00	0.00	0.00

Travel time in

Channel Concentrated Flow

Flow length (ft)	= 730.00	0.00	0.00
Watercourse slope (%)	= 9.50	0.00	0.00
Surface description	= Unpaved	Paved	Paved
Average velocity (ft/s)	=4.97	0.00	0.00

Travel time in

2

Channel Flow

X sectional flow area (sqft)	= 3.00	0.00	0.00
Wetted perimeter (ft)	= 5.00	0.00	0.00
Channel slope (%)	= 7.00	0.00	0.00
Manning's n-value	= 0.035	0.015	0.015
Velocity (ft/s)	=8.00		

0.00

0.00

Flow length (ft)

{0}6453.0

0.0

0.0

Travel time in

Total Travel time in

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Hydrograph

Area B

Hydrograph type	= SCS Runoff	Peak discharge	= 70.09 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.43 hrs
Time interval	= 2 min	Hyd. volume	= 554,710 cuft
Drainage area	= 234.000 ac	Curve number	= 56
Basin Slope	= 7.8 %	Hydraulic length	= 7140 ft
Tc method	= TR55	Time of conc. (Tc)	= 46.6 min
Total precip.	= 4.20 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Hydrograph Discharge Table

(Printed values >= 10.00% of Qp. Print interval = 5)

Time (hrs)	Discharge (cfs)	Time (hrs)	Discharge (cfs)	Time (hrs)	Discharge (cfs)
11.93	7.090	14.93	12.00	17.93	7.587
12.10	29.76	15.10	11.66	18.10	7.456
12.27	56.64	15.27	11.35	18.27	7.322
12.43	70.09	15.43	11.02	18.43	7.187
		15.60	10.68	18.60	7.049
12.60	65.45	15.77	10.33		
12.77	56.33	15.93	9.976		...End
12.93	43.77	16.10	9.612		
13.10	30.02	16.27	9.259		
13.27	24.29	16.43	8.945		
13.43	21.37	16.60	8.693		
13.60	19.35	16.77	8.497		
13.77	17.84	16.93	8.342		
13.93	16.54	17.10	8.212		
14.10	15.40	17.27	8.091		
14.27	14.40	17.43	7.968		
14.43	13.56	17.60	7.844		
14.60	12.90	17.77	7.717		
14.77	12.40				

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Hydrograph

Combined Area A and B

Hydrograph type	= Combine	Peak discharge	= 101.34 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.77 hrs
Time interval	= 2 min	Hyd. volume	= 3,307,163 cuft
Inflow hyds.	= 2, 3	Contrib. drain. area	= 234.000 ac

Hydrograph Discharge Table

(Printed values >= 20.00% of Qp. Print interval = 5)

Time hr:min	Hyd 2 cfs	Hyd 3 cfs	Util %
12.17	5.974	40.17	46.15
12.33	11.43	65.97	77.40
12.50	24.10	68.82	92.92
12.67	38.07	62.29	100.36
12.83	49.11	51.65	100.76
13.00	59.17	38.08	97.25
13.17	64.62	26.70	91.33
13.33	66.98	23.00	89.98
13.50	68.26	20.47	88.73
13.67	68.94	18.71	87.65
13.83	69.19	17.30	86.49
14.00	69.13	16.06	85.19
14.17	68.80	14.98	83.79
14.33	68.28	14.04	82.32
14.50	67.58	13.27	80.86
14.67	66.77	12.69	79.46
14.83	65.88	12.23	78.12
15.00	64.94	11.86	76.80
15.17	63.96	11.54	75.50
15.33	62.96	11.22	74.18
15.50	61.94	10.88	72.83

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Hydrograph of Large Lake

Time hr	Hyd 2 mm	Hyd mm	Outflow mm
15.67	60.90	10.54	71.45
15.83	59.84	10.19	70.04
16.00	58.77	9.831	68.60
16.17	57.67	9.468	67.14
16.33	56.55	9.128	65.68
16.50	55.43	8.837	64.27
16.67	54.31	8.609	62.91
16.83	53.19	8.431	61.62
17.00	52.10	8.288	60.39
17.17	51.03	8.163	59.20
17.33	49.99	8.042	58.03
17.50	48.97	7.919	56.89
17.67	48.13	7.793	55.93
17.83	47.41	7.665	55.07
18.00	46.69	7.535	54.22
18.17	45.98	7.403	53.38
18.33	45.27	7.268	52.54
18.50	44.57	7.132	51.70
18.67	43.88	6.994	50.87
18.83	43.19	6.854	50.04
19.00	42.50	6.712	49.22
19.17	41.83	6.568	48.39
19.33	41.15	6.423	47.57
19.50	40.48	6.276	46.76
19.67	39.82	6.127	45.94
19.83	39.15	5.977	45.13
20.00	38.50	5.825	44.32

Combined Area A and B

Hydrograph of discharge rate

Time hr:min	Hyd 2 ft	Hyd 3 ft	Util ft
20.17	37.84	5.674	43.51
20.33	37.19	5.537	42.73
20.50	36.54	5.426	41.97
20.67	35.91	5.348	41.26
20.83	35.29	5.295	40.58
21.00	34.68	5.260	39.94
21.17	34.09	5.236	39.32
21.33	33.52	5.214	38.73
21.50	32.96	5.191	38.15
21.67	32.42	5.169	37.59
21.83	31.90	5.146	37.04
22.00	31.39	5.123	36.51
22.17	30.89	5.099	35.99
22.33	30.41	5.076	35.49
22.50	29.95	5.052	35.00
22.67	29.50	5.027	34.52
22.83	29.05	5.003	34.06
23.00	28.63	4.978	33.61
23.17	28.21	4.953	33.16
23.33	27.81	4.928	32.73
23.50	27.41	4.903	32.31
23.67	27.03	4.877	31.90
23.83	26.65	4.851	31.51
24.00	26.29	4.825	31.12
24.17	25.92	4.525	30.45
24.33	25.51	3.770	29.28
24.50	25.01	2.593	27.61

Continues on next page...

Combined Area A and B

hydrograph data table

Time hr	Hyd 2 mm	Hyd mm
24.67	24.40	1.524
24.83	23.68	0.738
25.00	22.91	0.234
25.17	22.11	0.011
25.33	21.32	0.000
25.50	20.54	0.000

...End

Outlet
mm

25.92

24.42

23.15

22.12

21.32

20.54

Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Pond 002 Anal

Pond Data

Contour User-defined contour areas. Conic method used for volume calculation. Beginning Elevation = 507.20 ft

Stage Storage Table

Stage (ft)	Elevation (ft)	Contour area (sq ft)	Incremental storage (cu ft)	Total storage (cu ft)
0.00	507.20	231,459	0	0
1.00	508.20	298,434	264,212	264,212
2.00	509.20	365,409	331,324	595,536
2.80	510.00	418,990	313,484	909,020
4.30	511.50	512,775	697,571	1,606,591

Culvert/Orifice Structure

	IC	OC	IC	OC	Pr
Orifice (in)	= 48.00	0.00	0.00	0.00	
Orifice (in)	= 48.00	0.00	0.00	0.00	
Orifice (in)	= 1	0	0	0	
Orifice (in)	= 505.20	0.00	0.00	0.00	
Length (ft)	= 40.00	0.00	0.00	0.00	
Orifice (in)	= 0.01	0.00	0.00	n/a	
Orifice (in)	= .012	.013	.013	n/a	
Orifice (in)	= 0.60	0.60	0.60	0.60	
Multi-stage	= n/a	No	No	No	

Orifice Structure

	IC	OC	IC	OC
Orifice Length (ft)	= 3.90	6.40	60.00	0.00
Orifice (in)	= 507.20	508.20	510.00	0.00
Orifice (in)	= 3.33	3.33	2.60	3.33
Orifice (in)	= Rect	Rect	Broad	---
Multi-stage	= Yes	Yes	No	No
Orifice (in)	= 0.000 (by Wet area)			
Orifice (in)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage Storage and Outflow Table

Stage (ft)	Storage (cu ft)	Elevation (ft)	IC	OC	Pr	Or	Or	Or	Or	Or	Or	Or	Or	Total
0.00	0	507.20	0.00	---	---	---	0.00	0.00	0.00	---	---	---	---	0.000
1.00	264,212	508.20	4.01 oc	---	---	---	4.00 s	0.00	0.00	---	---	---	---	4.005
2.00	595,536	509.20	4.94 oc	---	---	---	2.79 s	2.12 s	0.00	---	---	---	---	4.908
2.80	909,020	510.00	57.11 oc	---	---	---	28.59 s	28.51 s	0.00	---	---	---	---	57.11
4.30	1,606,591	511.50	109.94 oc	---	---	---	49.54 s	60.39 s	286.59	---	---	---	---	396.52

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2011 by Autodesk, Inc. v8

Thursday, Nov 18, 2010

Hydrograph

Canal - Stop Log

Hydrograph type	= Reservoir	Peak discharge	= 56.74 cfs
Storm frequency	= 10 yrs	Time to peak	= 17.53 hrs
Time interval	= 2 min	Hyd. volume	= 3,267,716 cuft
Inflow hyd. No.	= 4 - Combined Area A Reservoir	Reservoir name	= Canal
Max. Elevation	= 509.99 ft	Max. Storage	= 905,762 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 20.00% of Qp. Print interval = 5)

Time hr	Inflow cfs	Elevation ft	Outflow cfs	Storage cuft	Peak cfs	Time to peak hrs	Time hr	Outflow cfs	Storage cuft	Time hr	Outflow cfs	Storage cuft
14.17	83.79	509.29	18.22	----	----	----	10.15	8.070	----	----	----	18.22
14.33	82.32	509.39	25.44	----	----	----	13.91	11.53	----	----	----	25.44
14.50	80.86	509.47	30.66	----	----	----	16.52	14.13	----	----	----	30.66
14.67	79.46	509.54	34.85	----	----	----	18.55	16.29	----	----	----	34.84
14.83	78.12	509.61	38.36	----	----	----	20.21	18.13	----	----	----	38.35
15.00	76.80	509.66	41.33	----	----	----	21.59	19.73	----	----	----	41.32
15.17	75.50	509.71	43.89	----	----	----	22.77	21.12	----	----	----	43.89
15.33	74.18	509.76	46.14	----	----	----	23.78	22.35	----	----	----	46.13
15.50	72.83	509.80	48.05	----	----	----	24.64	23.41	----	----	----	48.04
15.67	71.45	509.84	49.74	----	----	----	25.39	24.34	----	----	----	49.73
15.83	70.04	509.87	51.16	----	----	----	26.01	25.14	----	----	----	51.16
16.00	68.60	509.89	52.39	----	----	----	26.55	25.83	----	----	----	52.39
16.17	67.14	509.92	53.44	----	----	----	27.01	26.42	----	----	----	53.43
16.33	65.68	509.94	54.30	----	----	----	27.38	26.91	----	----	----	54.29
16.50	64.27	509.95	55.00	----	----	----	27.68	27.31	----	----	----	54.99
16.67	62.91	509.96	55.56	----	----	----	27.92	27.63	----	----	----	55.55
16.83	61.62	509.97	56.00	----	----	----	28.12	27.88	----	----	----	56.00
17.00	60.39	509.98	56.33	----	----	----	28.26	28.07	----	----	----	56.32
17.17	59.20	509.99	56.56	----	----	----	28.36	28.20	----	----	----	56.55
17.33	58.03	509.99	56.69	----	----	----	28.41	28.27	----	----	----	56.69

Continues on next page...

Canal - Stop Log

Hydrograph of discharge at

Time hr	Discharge cfs	Elevation ft	Water ft	Stage ft	Water ft	Power ft	Rate ft	Rate ft	Rate ft	Rate ft	Rate ft	Rate ft
17.50	56.89	509.99	56.74	----	----	----	28.44	28.30	----	----	----	56.74
17.67	55.93	509.99	56.72	----	----	----	28.42	28.29	----	----	----	56.71
17.83	55.07	509.99	56.64	----	----	----	28.39	28.24	----	----	----	56.63
18.00	54.22	509.99	56.51	----	----	----	28.33	28.17	----	----	----	56.50
18.17	53.38	509.98	56.33	----	----	----	28.26	28.07	----	----	----	56.32
18.33	52.54	509.98	56.11	----	----	----	28.16	27.94	----	----	----	56.10
18.50	51.70	509.97	55.85	----	----	----	28.05	27.79	----	----	----	55.84
18.67	50.87	509.96	55.55	----	----	----	27.92	27.62	----	----	----	55.54
18.83	50.04	509.96	55.21	----	----	----	27.77	27.43	----	----	----	55.21
19.00	49.22	509.95	54.85	----	----	----	27.62	27.22	----	----	----	54.84
19.17	48.39	509.94	54.45	----	----	----	27.45	27.00	----	----	----	54.44
19.33	47.57	509.93	54.02	----	----	----	27.26	26.75	----	----	----	54.02
19.50	46.76	509.92	53.57	----	----	----	27.07	26.50	----	----	----	53.57
19.67	45.94	509.91	53.08	----	----	----	26.85	26.22	----	----	----	53.08
19.83	45.13	509.90	52.57	----	----	----	26.63	25.94	----	----	----	52.57
20.00	44.32	509.89	52.04	----	----	----	26.40	25.64	----	----	----	52.04
20.17	43.51	509.87	51.49	----	----	----	26.16	25.33	----	----	----	51.49
20.33	42.73	509.86	50.93	----	----	----	25.91	25.01	----	----	----	50.92
20.50	41.97	509.85	50.35	----	----	----	25.66	24.68	----	----	----	50.34
20.67	41.26	509.84	49.75	----	----	----	25.39	24.35	----	----	----	49.74
20.83	40.58	509.82	49.13	----	----	----	25.12	24.01	----	----	----	49.13
21.00	39.94	509.81	48.51	----	----	----	24.84	23.66	----	----	----	48.50
21.17	39.32	509.80	47.89	----	----	----	24.56	23.32	----	----	----	47.88
21.33	38.73	509.78	47.27	----	----	----	24.29	22.97	----	----	----	47.26
21.50	38.15	509.77	46.66	----	----	----	24.01	22.63	----	----	----	46.64
21.67	37.59	509.76	46.04	----	----	----	23.74	22.29	----	----	----	46.03
21.83	37.04	509.75	45.41	----	----	----	23.45	21.94	----	----	----	45.40
22.00	36.51	509.73	44.78	----	----	----	23.17	21.60	----	----	----	44.77

Continues on next page...

Hydrograph of discharge table

Time hr	Time min	Elevation ft	Discharge cfs	Discharge cfs	Discharge cfs	Power hp	Rate cfs	Rate cfs	Rate cfs	Rate cfs	Rate cfs	Outlet cfs
22.17	35.99	509.72	44.16	----	----	----	22.89	21.27	----	----	----	44.15
22.33	35.49	509.71	43.55	----	----	----	22.61	20.93	----	----	----	43.54
22.50	35.00	509.70	42.94	----	----	----	22.34	20.60	----	----	----	42.94
22.67	34.52	509.68	42.35	----	----	----	22.07	20.28	----	----	----	42.35
22.83	34.06	509.67	41.75	----	----	----	21.79	19.95	----	----	----	41.74
23.00	33.61	509.66	41.14	----	----	----	21.51	19.63	----	----	----	41.14
23.17	33.16	509.65	40.56	----	----	----	21.24	19.31	----	----	----	40.55
23.33	32.73	509.64	39.98	----	----	----	20.97	19.00	----	----	----	39.97
23.50	32.31	509.63	39.41	----	----	----	20.70	18.70	----	----	----	39.41
23.67	31.90	509.62	38.86	----	----	----	20.45	18.40	----	----	----	38.85
23.83	31.51	509.61	38.32	----	----	----	20.20	18.11	----	----	----	38.31
24.00	31.12	509.59	37.77	----	----	----	19.94	17.82	----	----	----	37.76
24.17	30.45	509.58	37.22	----	----	----	19.67	17.53	----	----	----	37.20
24.33	29.28	509.57	36.63	----	----	----	19.39	17.22	----	----	----	36.62
24.50	27.61	509.56	35.98	----	----	----	19.08	16.88	----	----	----	35.96
24.67	25.92	509.55	35.24	----	----	----	18.73	16.49	----	----	----	35.22
24.83	24.42	509.53	34.43	----	----	----	18.35	16.06	----	----	----	34.41
25.00	23.15	509.52	33.56	----	----	----	17.94	15.61	----	----	----	33.55
25.17	22.12	509.50	32.62	----	----	----	17.47	15.13	----	----	----	32.60
25.33	21.32	509.49	31.67	----	----	----	17.01	14.65	----	----	----	31.66
25.50	20.54	509.47	30.74	----	----	----	16.56	14.17	----	----	----	30.73
25.67	19.80	509.45	29.83	----	----	----	16.11	13.71	----	----	----	29.82
25.83	19.08	509.44	28.92	----	----	----	15.67	13.25	----	----	----	28.92
26.00	18.39	509.42	27.94	----	----	----	15.17	12.76	----	----	----	27.94
26.17	17.73	509.41	26.98	----	----	----	14.69	12.29	----	----	----	26.98
26.33	17.09	509.40	26.06	----	----	----	14.22	11.83	----	----	----	26.05
26.50	16.47	509.38	25.16	----	----	----	13.77	11.39	----	----	----	25.16
26.67	15.87	509.37	24.29	----	----	----	13.33	10.96	----	----	----	24.29

Continues on next page...

Canal - Stop Log

Hydrograph of Large Canal

Time Hour	Water Level	Elevation ft	Flow cfs	Flow cfs	Flow cfs	Power kW	Flow cfs	Flow cfs	Flow cfs	Flow cfs	Flow cfs	Outlet cfs
26.83	15.30	509.36	23.40	----	----	----	12.88	10.52	----	----	----	23.40
27.00	14.74	509.35	22.42	----	----	----	12.36	10.06	----	----	----	22.41
27.17	14.21	509.33	21.48	----	----	----	11.86	9.615	----	----	----	21.48
27.33	13.70	509.32	20.59	----	----	----	11.40	9.195	----	----	----	20.59
27.50	13.46	509.31	19.76	----	----	----	10.96	8.803	----	----	----	19.76
27.67	13.27	509.30	19.01	----	----	----	10.56	8.446	----	----	----	19.01
27.83	13.08	509.30	18.32	----	----	----	10.20	8.120	----	----	----	18.32
28.00	12.89	509.29	17.69	----	----	----	9.870	7.823	----	----	----	17.69
28.17	12.71	509.28	17.12	----	----	----	9.566	7.549	----	----	----	17.12
28.33	12.53	509.27	16.21	----	----	----	9.062	7.143	----	----	----	16.20
28.50	12.35	509.27	15.43	----	----	----	8.626	6.794	----	----	----	15.42
28.67	12.17	509.26	14.77	----	----	----	8.260	6.500	----	----	----	14.76
28.83	12.00	509.26	14.21	----	----	----	7.951	6.252	----	----	----	14.20
29.00	11.83	509.26	13.74	----	----	----	7.688	6.041	----	----	----	13.73
29.17	11.66	509.26	13.33	----	----	----	7.459	5.857	----	----	----	13.31
29.33	11.49	509.25	12.97	----	----	----	7.257	5.696	----	----	----	12.95
29.50	11.33	509.25	12.64	----	----	----	7.077	5.551	----	----	----	12.63
29.67	11.17	509.25	12.36	----	----	----	6.917	5.423	----	----	----	12.34
29.83	11.01	509.25	12.10	----	----	----	6.773	5.307	----	----	----	12.08
30.00	10.85	509.25	11.85	----	----	----	6.639	5.200	----	----	----	11.84
30.17	10.69	509.24	11.63	----	----	----	6.515	5.101	----	----	----	11.62
30.33	10.54	509.24	11.42	----	----	----	6.399	5.008	----	----	----	11.41

...End

Culvert Analysis Report

Table 1 Primary Culvert Flow at Routing: Proposed Anal Routing

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
506.20	0.00	0.00	0.00	1
508.44	47.32	47.32	0.00	1
510.20	94.64	93.72	0.90	7
510.82	141.96	108.15	33.71	7
511.08	189.28	113.06	76.02	6
511.27	236.60	116.45	119.86	5
511.43	283.92	119.20	164.61	5
511.55	323.52	121.19	202.13	4
511.70	378.56	123.69	254.77	4
511.82	425.88	125.63	299.86	3
511.94	473.20	125.68	347.24	3
510.00	88.56	88.56	0.00	Overtopping

Table 2 Culvert Output Primary Table: Culvert

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	506.20	0.000	1.000	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
47.32	47.32	508.44	3.057	3.245	2-M2c	4.000	2.057	2.061	0.814	7.251	1.319
94.64	93.72	510.20	4.908	5.000	2-M2c	4.000	2.925	2.935	1.229	9.485	1.709
141.96	108.15	510.82	5.618	5.565	2-M2c	4.000	3.139	3.145	1.561	10.214	1.981
189.28	113.06	511.08	5.883	5.769	2-M2c	4.000	3.209	3.211	1.849	10.455	2.195
236.60	116.45	511.27	6.073	5.910	2-M2c	4.000	3.244	3.255	2.107	10.651	2.375
283.92	119.20	511.43	6.233	6.036	3-M2t	4.000	3.273	3.345	2.344	10.653	2.531
323.52	121.19	511.55	6.351	6.141	3-M2t	4.000	3.293	3.530	2.529	10.346	2.647
378.56	123.69	511.70	6.502	6.367	7-M2t	4.000	3.319	3.771	2.770	10.145	2.793
425.88	125.63	511.82	6.622	6.566	7-M2t	4.000	3.340	3.966	2.965	10.042	2.907
473.20	125.68	511.94	6.625	6.740	4-FFf	4.000	3.340	4.000	3.151	10.002	3.011

 Inlet Elevation (invert): 505.20 ft, Outlet Elevation (invert): 505.20 ft
 Culvert Length: 40.00 ft, Culvert Slope: 0.0000

Site Data Culvert

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 505.20 ft

Outlet Station: 40.00 ft

Outlet Elevation: 505.20 ft

Number of Barrels: 1

Barrel Data Summary

Barrel Shape: Circular

Barrel Diameter: 4.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Inlet Type: Conventional

Inlet Edge Condition: Square Edge with Headwall

Inlet Depression: NONE

Flow Computation Channel Rating Curve Processing: Processed Channel Rating

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	506.20	0.00	0.00	0.00	0.00
47.32	507.01	0.81	1.32	0.05	0.26
94.64	507.43	1.23	1.71	0.08	0.28
141.96	507.76	1.56	1.98	0.10	0.29
189.28	508.05	1.85	2.20	0.12	0.30
236.60	508.31	2.11	2.38	0.13	0.30
283.92	508.54	2.34	2.53	0.15	0.31
323.52	508.73	2.53	2.65	0.16	0.31
378.56	508.97	2.77	2.79	0.17	0.32
425.88	509.17	2.97	2.91	0.19	0.32
473.20	509.35	3.15	3.01	0.20	0.32

Tailwater Channel Data Processed Channel Rating

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 42.00 ft

Side Slope (H:V): 2.50 (1:1)

Channel Slope: 0.0010

Channel Manning's n: 0.0300

Channel Invert Elevation: 506.20 ft

Load Data for Grading: Proposed Final Grading

Roadway Profile Shape: Irregular Roadway Shape (coordinates)

Irregular Roadway Cross-Section:

Coord No.	Station (ft)	Elevation (ft)
1	0.00	511.50
2	5.00	511.00
3	35.00	510.70
4	67.00	510.00
5	80.00	511.30

Roadway Surface: Gravel

Roadway Top Width: 20.00 ft

Appendix B:
Plant List

Riverlands Mitigation Site Plant List

Common Name	Size	Qty.	Spacing	I.S.	Notes
Red Maple	#15	13		FAC	
Shagbark Hickory	#15	7		FACU	Upland areas only
Black Gum	#15	10		FACW	Do not plant in areas with frequent standing water
American Sycamore	#15	7		FACW	
Swamp White Oak	#15	10		FACW	
Pin Oak	#15	20		FACW	
		65			

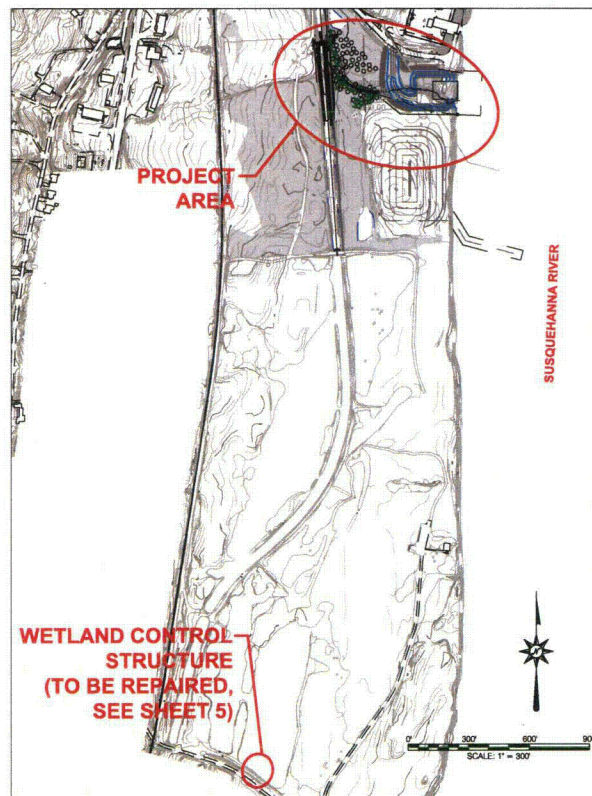
Common Name	Size	Qty.	Spacing	I.S.	Notes
Red Chokeberry	#5	21	4-6'	FACW	
Winterberry	#5	32	4-6'	FACW	1 male for every 8 females
Spicebush	#5	64	4-6'	FACW	
Highbush Blueberry	#5	54	4-6'	FACW	
Arrowwood	#5	21	4-6'	FAC	
Cranberry Bush	#5	21	4-6'	FACW	
		214			

Common Name	Size	Qty.	Spacing	I.S.	Notes
Thousand-flowered Aster	Quart	23	24"		
Soft Rush	Quart	55	24"	OBL	
Soft Stemmed Bullrush	Quart	37	24"	OBL	
Blue Flag	Quart	55	24"	OBL	
Swamp Milkweed	Quart	37	24"		
Fringed Sedge	Quart	46	24"	OBL	
Fox Sedge	Quart	46	24"	OBL	
New England Aster	Quart	37	24"		
White Turtlehead	Quart	46	24"		
New York Ironweed	Quart	37	24"		
Three-nerved Joe Pye	Quart	41	24"		
		458			

BELL BEND NUCLEAR POWER PLANT WETLAND MITIGATION PLAN RIVERLANDS SITE

SALEM TOWNSHIP, LUZERNE COUNTY, PENNSYLVANIA

PLAN DATE: OCTOBER 29, 2010
REVISION 1: AUGUST 12, 2011



SITE MAP
1" = 300'

TABLE OF CONTENTS

- SHEET 1 - COVER
- SHEET 2 - GRADING PLAN
- SHEET 3 - PROFILES & CROSS SECTIONS
- SHEET 4 - CONSTRUCTION DETAILS
- SHEET 5 - ORIGINAL CONSTRUCTION DETAILS
- SHEET 6 - E&S PLAN
- SHEET 7 - E&S NARRATIVE & DETAILS
- SHEET 8 - LANDSCAPING PLAN
- SHEET 9 - LANDSCAPING DETAILS

CLIENT ADDRESS:

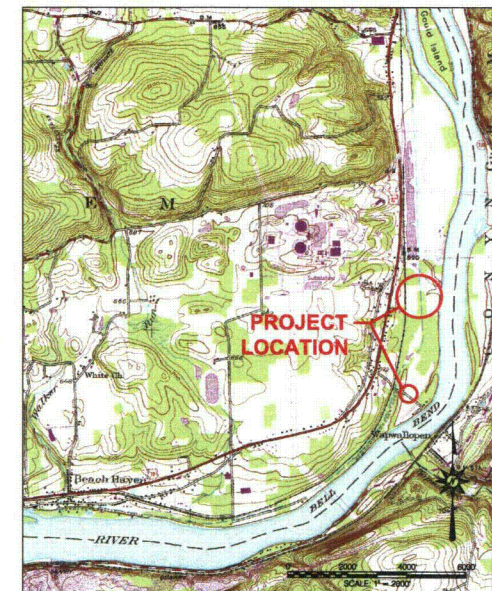
PPL BELL BEND, LLC.
38 BOMBOY LANE, SUITE 2
BERWICK, PENNSYLVANIA 18603
PHONE: (570) 802-5636
FAX: (570) 802-5639



717-627-4440
fax: 717-627-4660

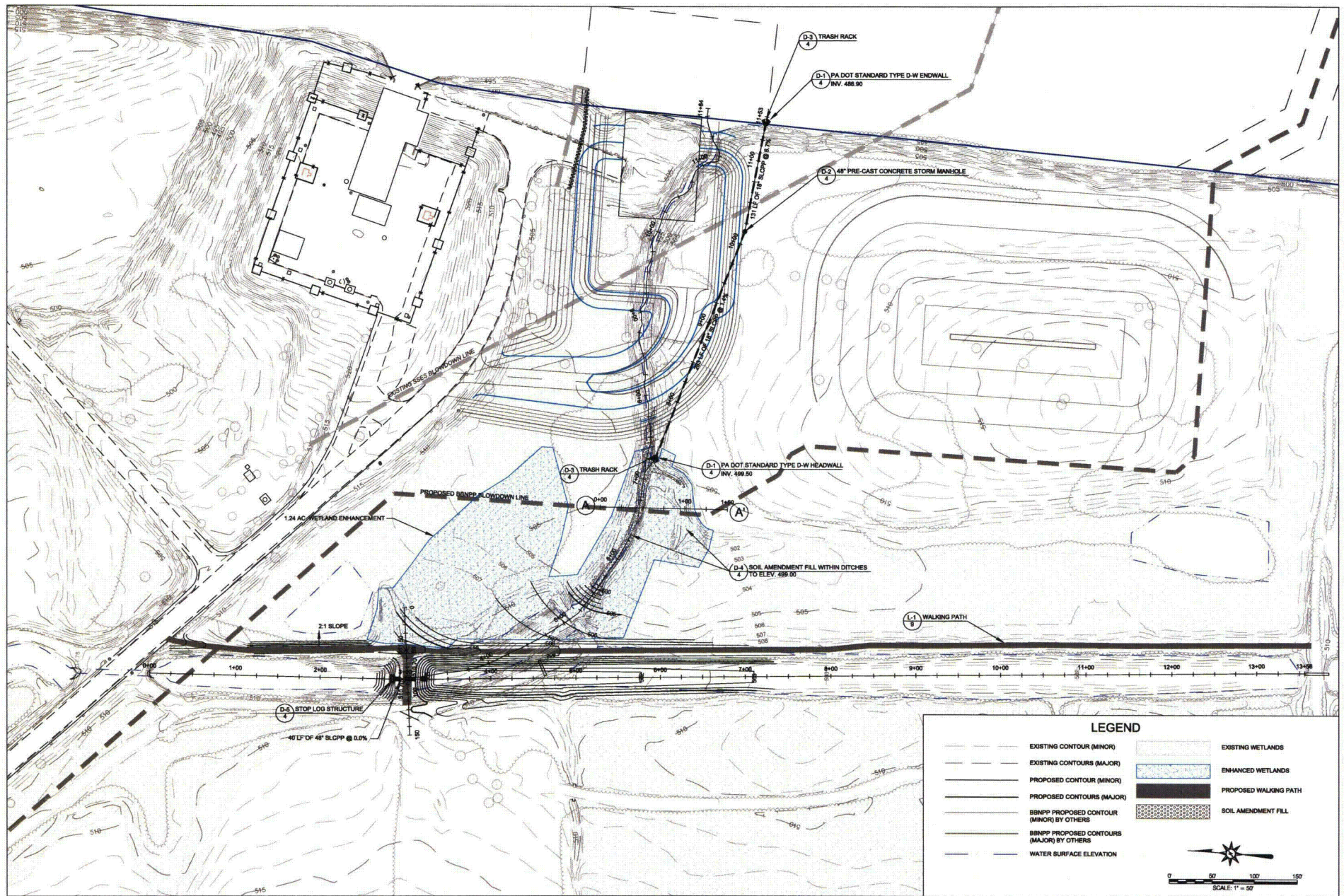
landstudies.com
land@landstudies.com

315 North Street | Lititz, PA 17543



LOCATION MAP
1" = 2,000'

NOTES:
1. BACKGROUND TOPOGRAPHIC MAPPING WAS PRODUCED BY PETERS CONSULTANTS, INC. IN NOV. 2007, JAN. 2008 AND APRIL 2010. THE HORIZONTAL COORDINATE SYSTEM SHOWN ON THIS DRAWING IS PENNSYLVANIA'S STATE PLAN COORDINATE SYSTEM, NORTH AMERICAN DATUM OF 1983 (NAD 83). THE VERTICAL COORDINATES ARE BASED ON THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD 88).
2. THE BBNPP PLOT PLAN IS FROM SARGENT & LUNDY, LLC, DRAWING SC-12198-400-001, REV. 4, REV. DATE 8-08-10.
3. THE WETLAND BOUNDARIES ARE FROM NORMANDEAU ASSOCIATES, INC. BELL BEND WETLANDS DELINEATION REPORT, REV. 3, JULY 2010.
4. EXISTING WEIR STRUCTURE DETAILS FROM KANDRA GREENLEAF HUTH, DRAWING E-18746, DATE AUGUST 1981.



717-827-4440
fax: 717-827-4680
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land@landstudies.com
315 North Street | Lititz, PA 17543



PROJECT: BELL BEND NUCLEAR POWER PLANT
PPL BELL BEND, LLC.
BERWICK, PENNSYLVANIA 18803

GRADING PLAN
WETLAND MITIGATION PLAN - RIVERLANDS SITE
LUZERNE COUNTY, PENNSYLVANIA

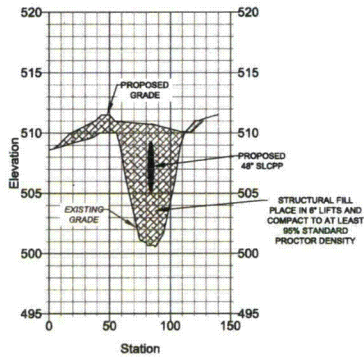
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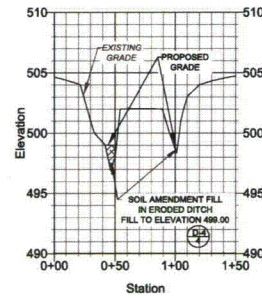
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CHECKED BY: JLB
DATE: OCTOBER 26, 2010
SCALE: 1" = 50'
REVISIONS: MTL-RL-002
SHEET NUMBER:

2
OF 9

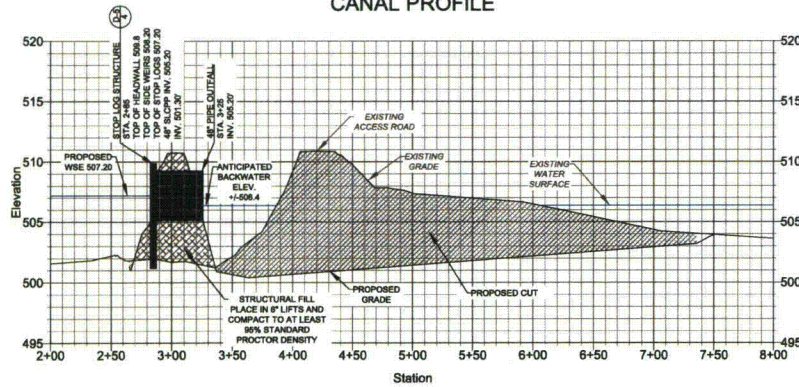
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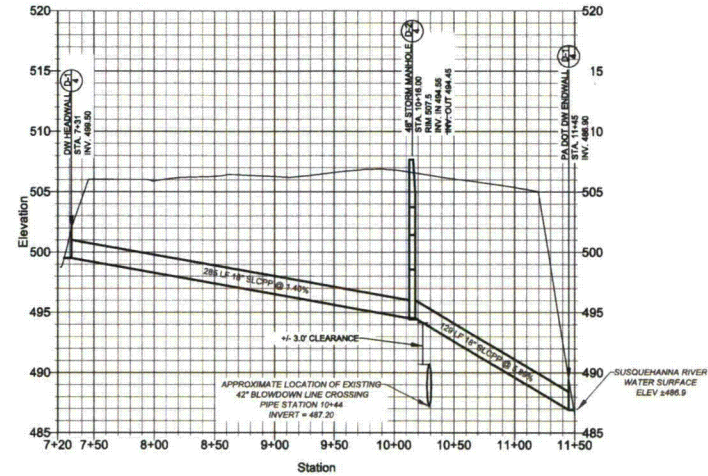
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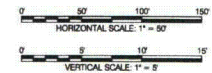
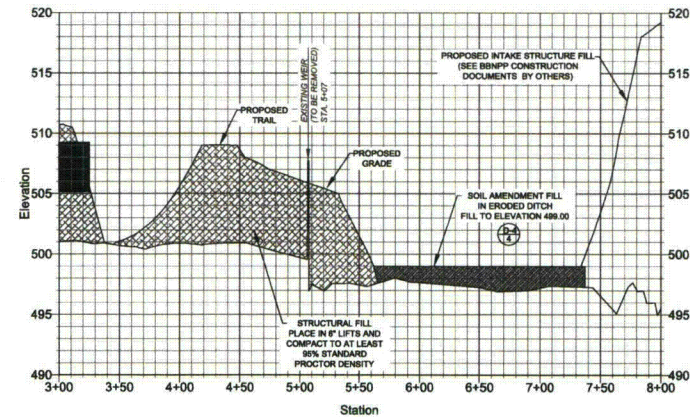
CANAL PROFILE



PIPE PROFILE



EXISTING CHANNEL PROFILE



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Fax: 717-627-4860
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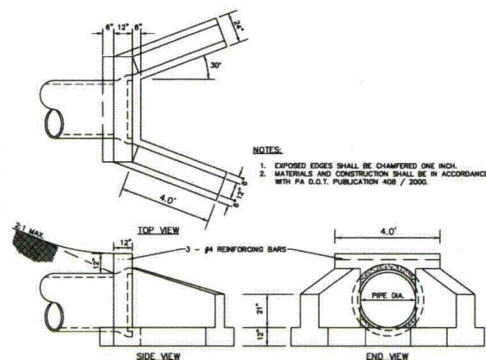
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BELL BEND NUCLEAR POWER
PLANT
PPL BELL BEND, LLC.
BERWICK, PENNSYLVANIA 18603

SHEET TITLE:
PROFILES AND CROSS SECTIONS
WETLAND MITIGATION PLAN - RIVERLANDS SITE
LUZERNE COUNTY, PENNSYLVANIA

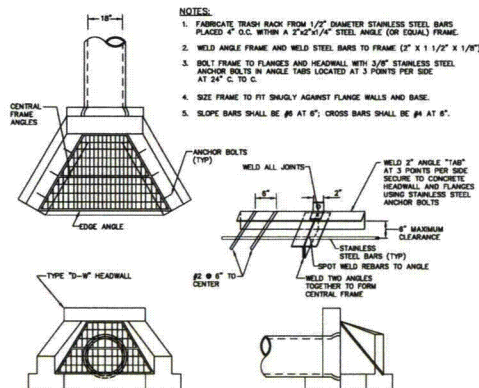
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			REVISION

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JES
CHECKED BY:
SLE
DATE:
OCTOBER 28, 2010
SCALE:
1" = 50'
DRAWING NUMBER:
MIT-RL-003
SHEET NUMBER:

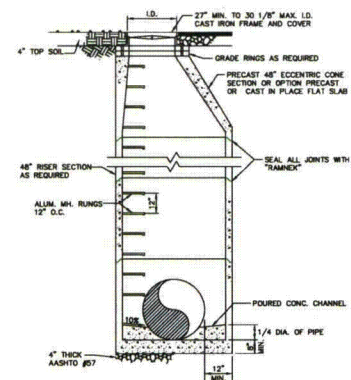
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OF 9



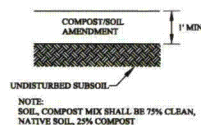
D-1
 4
 (PA D.O.T. RC-31)
STANDARD TYPE D-W ENDWALL
 NTS



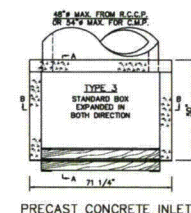
D-3
 4
TRASH RACK
 NTS



D-2
 4
48" PRE-CAST CONCRETE STORM MANHOLE
 NTS

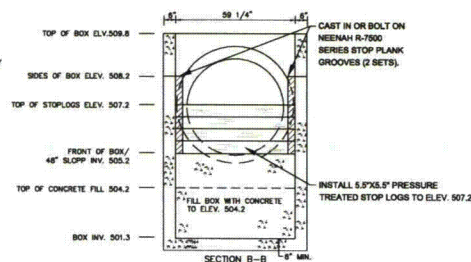
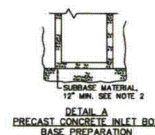


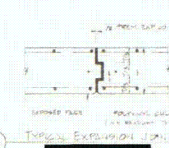
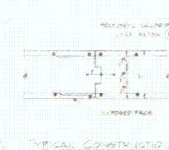
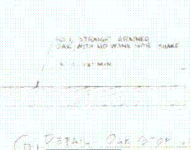
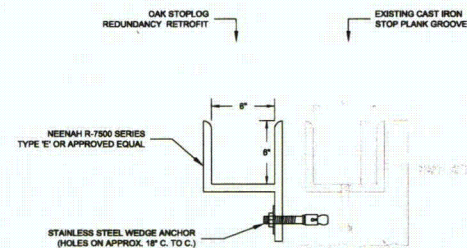
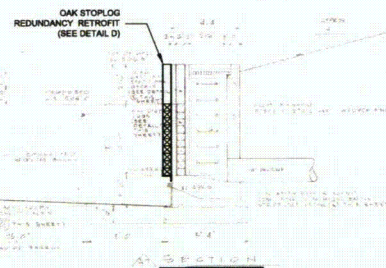
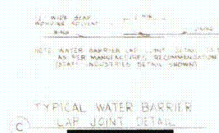
D-4
 4
SOIL AMENDMENT FILL
 NTS




NOTES:
 1. CONSTRUCT INLET BOXES IN ACCORDANCE WITH THE REQUIREMENTS OF PUBLICATION 408, SECTION 713.2(4), FOR PRECAST CEMENT CONCRETE UNITS.
 2. PLACE SUBBASE MATERIAL MEETING THE REQUIREMENTS OF PUBLICATION 408, SECTION 360.2, IN 4 INCH LAYERS, COMPACTED TO A DENSITY SATISFACTORY TO THE ENGINEER AND INCIDENTAL TO THE INLET PAY ITEM.

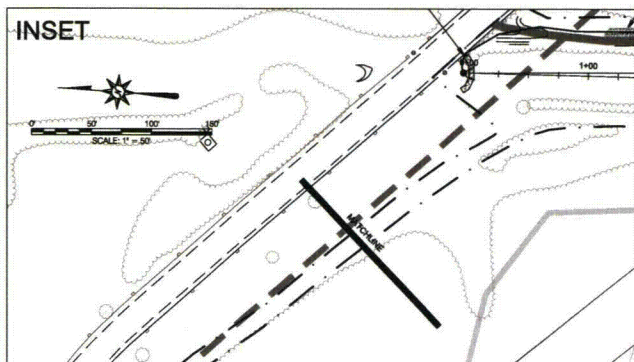
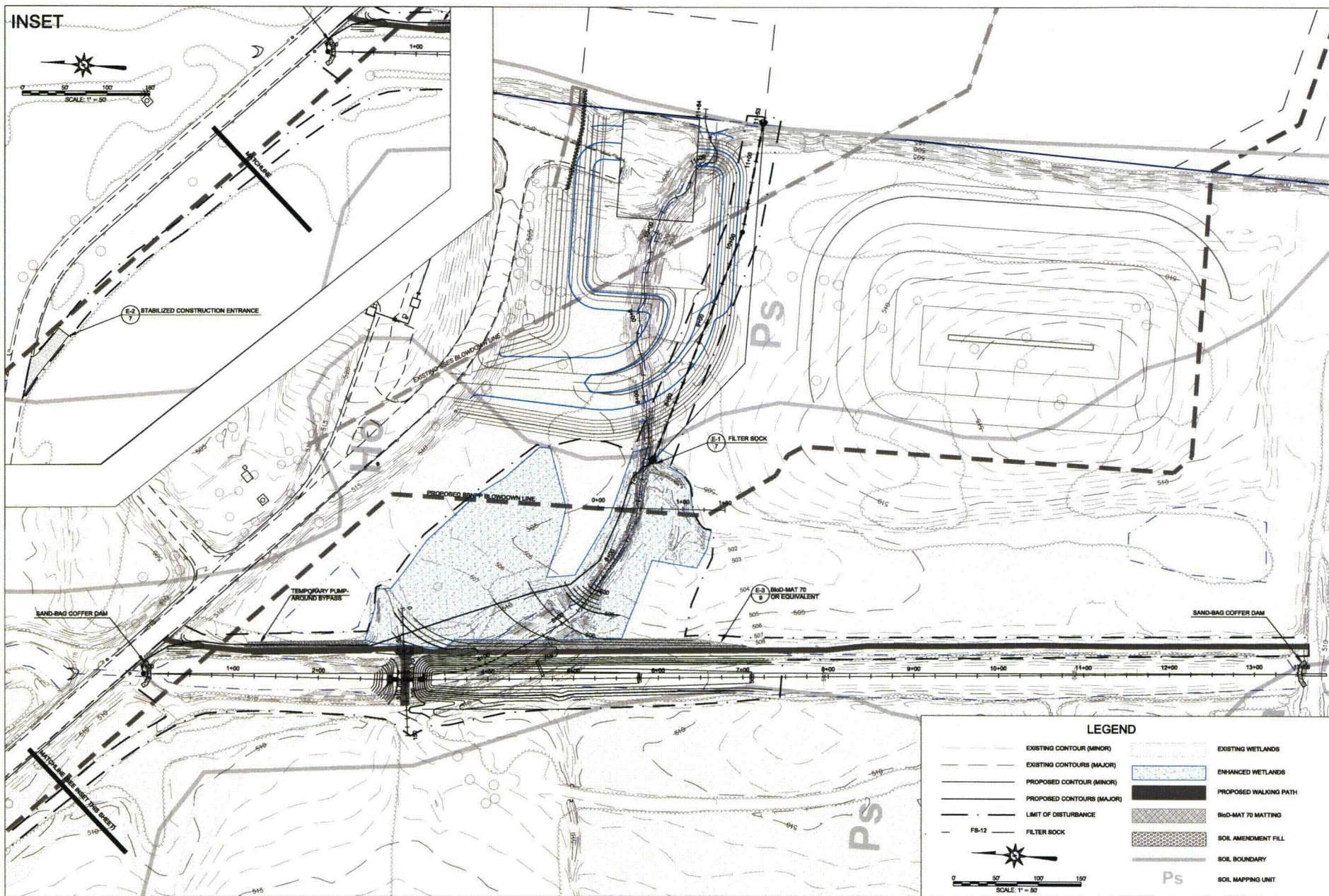
D-5
 4
STOP LOG STRUCTURE
 (MODIFIED PA DOT TYPE 3 BOX, RC-34)
 NTS





NOTE: THE EXISTING RIVERLANDS WETLAND WEIR STRUCTURE MUST BE REPAIRED TO THE ORIGINAL SPECIFICATIONS, WITH MODIFICATIONS AS SHOWN IN THE DETAILS PROVIDED ON THIS SHEET. THE STOP LOGS MAY NEED TO BE ADJUSTED AFTER THE RECONNECTION OF THE CANAL TO MAINTAIN THE EXISTING WATER SURFACE ELEVATION IN THE RIVERLANDS WETLAND AREA.

DET. 15 FLOW STRUCTURE C.		A 7	
KANDRA GREENLEAF HUTH A DIVISION OF HUTH CONSTRUCTION			
ARCHITECTS (ENGINEERS) PLANNERS			
			
3440 HAMILTON ROAD SUITE 100 ALLENTOWN, PENNSYLVANIA 18103			
BR _____ SCALE _____ DATE (RITING) DRAWING NO.	SUSQUEHANNA PHASE II U.S. ROUTE #11 LUZERNE COUNTY, PENNSYLVANIA POWER & LIGHT COMPANY ALLENTOWN, PA.		
CHECKED BY LEADER APPR. BY _____	APPROVED <div style="border: 1px solid black; padding: 5px; display: inline-block;"> E 37622 </div>		



LEGEND

EXISTING CONTOUR (MINOR)	EXISTING WETLANDS
EXISTING CONTOURS (MAJOR)	ENHANCED WETLANDS
PROPOSED CONTOUR (MINOR)	PROPOSED WALKING PATH
PROPOSED CONTOURS (MAJOR)	BIO-MAT TO MATING
LIMIT OF DISTURBANCE	SOIL AMENDMENT FILL
FB-12 FILTER SOCK	SOIL BOUNDARY
	SOIL MAPPING UNIT

SCALE: 1" = 50'

PROJECT: BELL BEND NUCLEAR POWER PLANT
CLIENT: PPL BELL BEND, LLC.
 BERWICK, PENNSYLVANIA 18803

SHEET TITLE: EROSION & SEDIMENT POLLUTION CONTROL PLAN - RIVERLANDS SITE
 WETLAND MITIGATION PLAN - PENNSYLVANIA
 LUZERNE COUNTY, PENNSYLVANIA

NO.	DATE	DESCRIPTION
1	10/26/2010	ISSUED FOR PERMIT

PROJECT NUMBER: E-725L-8
DRAWN BY: J.B.
CHECKED BY: S.M.
DATE: OCTOBER 26, 2010
SCALE: 1" = 50'
PROJECT NUMBER: MT-RL-006
SHEET NUMBER: 6 OF 9

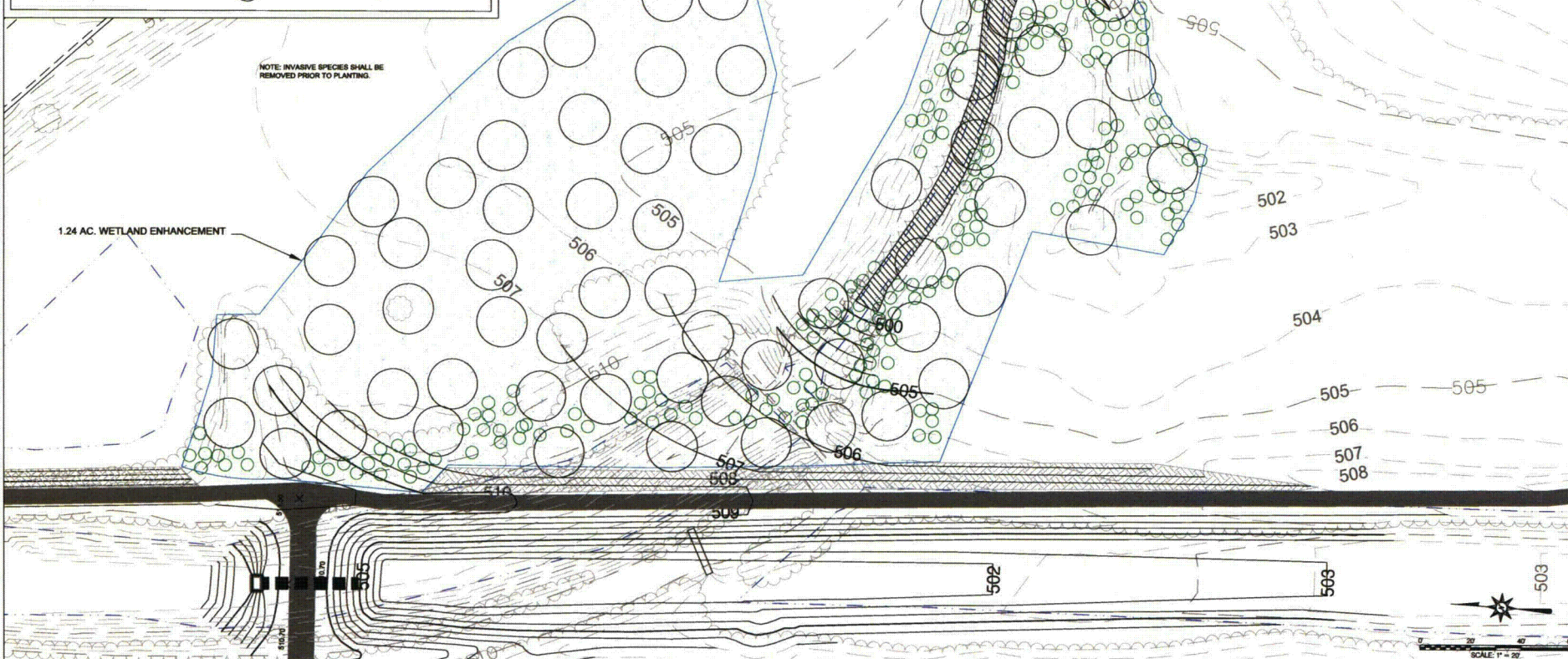
Land Studies
 717-427-4440
 fax: 717-427-4880
 landstudies.com
 landstudies@landstudies.com
 315 North Street | Lititz, PA 17543

Trees							
Key	%	Botanical Name	Common Name	Size	Qty.	Spacing	I.S.
AR	20.00%	Acer rubrum	Red Maple	#15	13		FAC
CO	30.00%	Carya ovata	Shagbark Hickory	#15	7		FACU
MS	15.00%	Myrica asplatica	Black Gum	#15	10		FACW
PO	30.00%	Platanus occidentalis	American Sycamore	#15	7		FACW
OB	15.00%	Quercus bicolor	Swamp White Oak	#15	10		FACW
OP	30.00%	Quercus palustris	Pin Oak	#15	20		FACW
	100.00%				65		

Shrubs							
Key	%	Botanical Name	Common Name	Size	Qty.	Spacing	I.S.
AA	10.00%	Aronia arbutifolia	Red Chokeberry	#5	21	4'-6'	FACW
IV	15.00%	Ilex verticillata	Winterberry	#5	32	4'-6'	FACW
IB	30.00%	Indigo berries	Spicebush	#5	64	4'-6'	FACW
VC	25.00%	Vaccinium corymbosum	Highbush Blueberry	#5	54	4'-6'	FACW
VD	10.00%	Viburnum dentatum	Arrowwood	#5	21	4'-6'	FAC
VT	10.00%	Viburnum trilobum	Cranberry Bush	#5	21	4'-6'	FACW
	100.00%				214		

Herbaceous							
Key	%	Botanical Name	Common Name	Size	Qty.	Spacing	I.S.
WA1	5.00%	Botanica asteroides	Thousand-flowered Aster	Quart	23	24"	OBL
	12.00%	Juncus effusus	Soft Rush	Quart	55	24"	OBL
	8.00%	Scirpus validus	Soft Stemmed Bulrush	Quart	37	24"	OBL
	12.00%	Eleocharis	Blue Flag	Quart	55	24"	OBL
	8.00%	Asclepias incarnata	Swamp Milkweed	Quart	37	24"	OBL
	10.00%	Carex crinita	Fringed Sedge	Quart	46	24"	OBL
	10.00%	Carex vulpinoidea	Fox Sedge	Quart	46	24"	OBL
	8.00%	Aster novae-angliae	New England Aster	Quart	37	24"	OBL
	10.00%	Chelone glabra	White Turtlehead	Quart	46	24"	OBL
	8.00%	Veronica novboracensis	New York Ironweed	Quart	37	24"	OBL
	9.00%	Eupatorium dubium	Three-nered Joe Pye	Quart	41	24"	OBL
	100.00%				458		

Wetland Mix 1 (WM1) Proposed Tree Proposed Shrub



717-827-4440
fax: 717-827-4880
landstudies.com
land@landstudies.com
315 North Street | Lutz, PA 17543

Land Studies

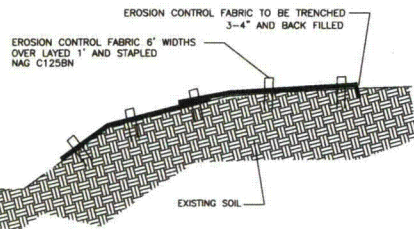
PROJECT: BELL BEND NUCLEAR POWER PLANT
PPL BELL BEND, LLC.
3000 BELL BEND ROAD
BERWICK, PENNSYLVANIA 19803

LANDSCAPING PLAN
WETLAND MITIGATION PLAN - RIVERLANDS SITE
LUZERNE COUNTY, PENNSYLVANIA

SHEET TITLE:

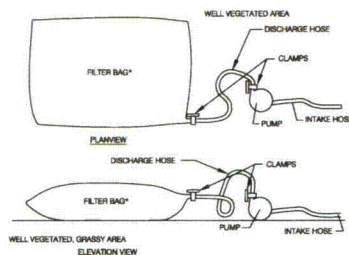
REV	DATE	DESCRIPTION
1	10/28/10	REVISED PLANS

PROJECT NUMBER: E-726-L8
DRAWN BY: AK
CHECKED BY: BUE
DATE: OCTOBER 28, 2010
SCALE: 1" = 20'
SHEET: MTT-RL-008
SHEET NUMBER: 8 OF 9



BIO-MAT 70 SPECIFICATIONS:
 ROLL SIZE 6.56' x 166'
 AREA 120 SY
 WEIGHT 23 OZ.
 MATRIX WOVEN BRISTLE COIR

E-3
 9 BIO-MAT 70 MATTING
 NTS



Filter bags shall be made from non-woven geotextile material sewn with high strength, double stitched "J" type seams. They shall be capable of trapping particles larger than 150 microns.

A suitable means of accessing the bag with machinery required for disposal purposes must be provided. Filter bags shall be replaced when they become 1/2 full. Spare bags shall be kept available for replacement of those that have failed or are filled.

Bags shall be located in well-vegetated (grassy) areas, and discharge onto stable, erosion resistant areas. Where this is not possible, a geotextile flow path shall be provided. Bags shall not be placed on slopes greater than 5%.

The pump discharge hose shall be inserted into the bags in a manner specified by the manufacturer and securely clamped.

The pumping rate shall be no greater than 750 gpm or 1/2 the maximum specified by the manufacturer, whichever is less. Pump intakes should be floating and screened.

Filter bags may be used to filter water pumped from disturbed areas prior to discharging to water of the Commonwealth. They may also be used to filter water pumped from the sediment storage areas of sediment basins.

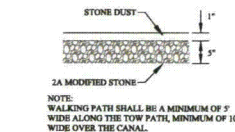
The pumping rate should be specified on the plan drawings next to the typical detail. Pumping rates will vary depending on the size of the filter bag, and the type and amount of sediment discharged to the bag.

E-4
 9 PUMPED WATER FILTER BAG
 NTS

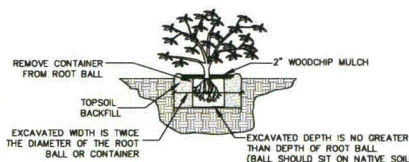
SEEDING RESTORATION TABLE				
LOCATION	TOPSOIL	STARTER FERTILIZER	LIME	SEED MIX
WETLAND	YES	N/A	N/A	FLOODPLAIN SEED MIX APPLICATION RATE: 15-20 LBS./ACRE
UPLAND	YES	N/A	N/A	CONSERVATION SEED MIX APPLICATION RATE: 15-20 LBS./ACRE
OTHER DISTURBED AREAS	NO	N/A	N/A	TEMPORARY STABILIZATION SEED MIX SEE SEED MIX FOR SEEDING

DOE TO SOIL LIMITATIONS NEITHER FERTILIZER NOR LIME WILL BE APPLIED TO THE GRADED WETLAND. IT IS ANTICIPATED THAT THE SPREADING OF TOPSOIL AND THE CLOSE PROXIMITY TO EXISTING WATER TABLE WILL PROMOTE RAPID GERMINATION OF PROPOSED SEED.

Temporary Stabilization Seed Mix				
%	Botanical Name	Common Name	Seeding Window	Application Rate
100	<i>Secale cereale</i>	Cereal Rye	Sep. 1 - Oct. 16	30 lbs./acre
100	<i>Avena sativa</i>	Oats	May 1 - Sept. 15	30 lbs./acre

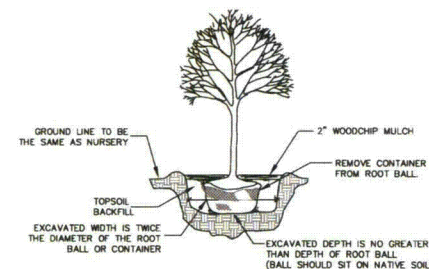


L-1
 9 WALKING PATH
 NTS

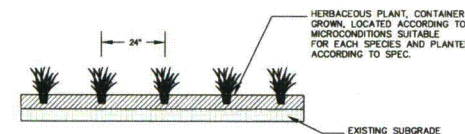


L-2
 9 TYPICAL SHRUB PLANTING - CONTAINER
 NTS

%	Botanical Name	Common Name	I.S.	%	Botanical Name	Common Name	I.S.
10	<i>Elymus virginicus</i> , PA	Virginia Wild Rye, PA Ecotype	FACW	15	<i>Schizanthus scoparium</i> , PA	Little Buerstem, PA	FACU
10	<i>Panicum rigidulum</i> , PA	Redtop Panic Grass, PA Ecotype	FACW	10	<i>Elymus virginicus</i> , PA	Virginia Wild Rye, PA Ecotype	FACW
8	<i>Elymus canadensis</i> , PA	Canada Wild Rye, PA Ecotype	FACU	8	<i>Panicum rigidulum</i> , PA	Redtop Panic Grass, PA Ecotype	FACW
5	<i>Carex vulpinoidea</i> , PA Ecotype	Fox Sedge, PA Ecotype	OBL	5	<i>Agrostis perennans</i> , APB	Autumn Bentgrass, APB	FACU
5	<i>Panicum clandestinum</i>	Deer Tongue Tioga, PA Ecotype	FAC+	5	<i>Agrostis scabra</i> , PA	Ticklegrass, PA Ecotype (rough bentgrass)	FACU
5	<i>Elymus riparius</i> , PA	Riverbank Wild Rye, PA Ecotype	FACW	5	<i>Carex scoparia</i>	Blunt Broom Sedge	FACW
5	<i>Agrostis perennans</i> , APB	Autumn Bentgrass, APB	FACU	5	<i>Elymus canadensis</i> , PA	Canada Wild Rye, PA Ecotype	FACU
5	<i>Agrostis scabra</i> , PA	Ticklegrass, PA Ecotype (rough bentgrass)	FAC	5	<i>Festuca rubra</i>	Creeping Red Fescue	FACU
5	<i>Carex scoparia</i>	Blunt Broom Sedge	FACW	5	<i>Panicum clandestinum</i>	Deer Tongue Tioga, PA Ecotype	FAC+
5	<i>Festuca rubra</i>	Creeping Red Fescue	FACU	4	<i>Chasmanthium latifolium</i> , PA	River Oats, PA Ecotype	FACU
4	<i>Carex comosa</i>	Bristly Sedge	OBL	4	<i>Lepidosperma perfoliatum</i>	Beesnest	FACW+
4	<i>Chasmanthium latifolium</i> , PA	River Oats, PA Ecotype	FACU	3	<i>Carex vulpinoidea</i> , PA Ecotype	Fox Sedge, PA Ecotype	OBL
3	<i>Carex stipata</i>	Awl Sedge	OBL	3	<i>Elymus hyemalis</i> , PA	Bottlebrush Grass, PA Ecotype	NI
3	<i>Elymus hyemalis</i> , PA	Bottlebrush Grass, PA Ecotype	NI	3	<i>Elymus riparius</i> , PA	Riverbank Wild Rye, PA Ecotype	FACW
3	<i>Juncus effusus</i> , PA	Soft Rush, PA Ecotype	FACW+	3	<i>Juncus effusus</i> , PA	Soft Rush, PA Ecotype	FACW+
2	<i>Asclepias incarnata</i>	Swamp Milkweed	OBL	2	<i>Asclepias incarnata</i>	Swamp Milkweed	OBL
2	<i>Bidens arifolia</i>	Bur Marigold, Suther' NC Ecotype	FACW+	2	<i>Asclepias tuberosa</i>	Butterfly Milkweed	NI
2	<i>Carex lurida</i>	Lurid Sedge	OBL	2	<i>Pellaea helandroides</i>	Ox Eye Sunflower	NI
2	<i>Juncus tenuis</i>	Path Rush	FAC	2	<i>Juncus tenuis</i>	Path Rush	FAC
2	<i>Poa polystris</i>	Poor Bluegrass	FACW	2	<i>Poa polystris</i>	Poor Bluegrass	FACW
1	<i>Aster prenanthoides</i>	Zigzag Aster	FAC	2	<i>Vernonia noveboracensis</i>	New York Ironweed	FACW+
1	<i>Aster brevis</i>	Smooth Blue Aster	NI	1	<i>Aster novae-angliae</i>	New England Aster	FACW+
1	<i>Aster novae-angliae</i>	New England Aster	FACW	1	<i>Aster prenanthoides</i>	Zigzag Aster	FAC
1	<i>Carex crinita</i>	Plumed Sedge	OBL	1	<i>Bidens arifolia</i>	Bur Marigold, Suther' NC Ecotype	FACW+
1	<i>Iris versicolor</i>	Blue Flag Iris	OBL	1	<i>Cnicus sensilis</i>	Sensitive Fern	FACW
1	<i>Labella cardinalis</i>	Cardinal Flower	FACW+	1	<i>Solidago rugosa</i>	Wrinkle Leaf Goldenrod	FAC
1	<i>Labella sphaerica</i>	Great Blue Lobelia	FACW+				
1	<i>Scirpus validus</i>	Soft stem Bulrush	OBL				
1	<i>Solidago rigida</i>	Rudbeck's Goldenrod	OBL				
1	<i>Solidago rugosa</i>	Wrinkle Leaf Goldenrod	FAC				



L-3
 9 TREE PLANTING DETAIL
 NTS



L-4
 9 HERBACEOUS QUART PLANTING DETAIL
 NTS

- PLANT SPECIFICATIONS:
- ALL PLANTS SHALL BE NURSERY GROWN IN A CLIMATE SIMILAR TO THAT OF THE LOCALITY OF THE PROJECT.
 - SET PLANTS AT SAME FINISHED GRADE AS GROWN IN THE NURSERY.
 - ALL PLANTS SHALL HAVE A NORMAL HART OF GROWTH AND SHALL BE SOUND, HEALTHY AND MATURE, THEY SHALL BE FREE FROM DISEASE, INSECTS, INSECT EGGS, AND LARVAE.
 - ALL PLANTING SHALL BE PERFORMED IN CONFORMANCE WITH GOOD NURSERY AND LANDSCAPE PRACTICE.