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U.S. Nuclear Regulatory Commission
Attn: Document Control Desk
Washington, D. C. 20555-0001

Re: Turkey Point Unit 3
Docket No. 50-250
Core Operating Limits Report

In accordance with Technical Specification 6.9.1.7, the attached Core Operating Limits Report (COLR) is provided for Turkey Point Unit 3. These curves are applicable for Unit 3 Cycle 26.

Should there be any questions, please contact Robert Tomonto, Licensing Manager, at 305-246-7327.

Very truly yours,

A handwritten signature in black ink, appearing to read 'Michael Kiley', is written over a horizontal line.

Michael Kiley
Site Vice President
Turkey Point Nuclear Plant

Attachment

cc: Regional Administrator, Region II, USNRC
Senior Resident Inspector, USNRC, Turkey Point Plant

A001
MRR

Appendix A

**Turkey Point Unit 3 Cycle 26
Core Operating Limits Report (COLR)**

TURKEY POINT UNIT 3 CYCLE 26 COLR

1.0 INTRODUCTION

This Core Operating Limits Report for Turkey Point Unit 3 Cycle 26 has been prepared in accordance with the requirements of Technical Specification 6.9.1.7.

The Technical Specifications (TS) affected by this report are listed below with the section and page for each one of the TS addressed in this COLR document.

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2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in the Introduction are presented below and listed sequentially by Technical Specification (TS). These limits have been developed using the NRC-approved methodologies specified in TS 6.9.1.7.

2.1 Reactor Core Safety Limits – Three Loops in Operation (TS 2.1.1)

- **Figure A1**(page 14A-A7) In Modes 1 and 2, the combination of Thermal Power, reactor coolant system highest loop average temperature and pressurizer pressure shall not exceed the limits in Figure A1.

2.2 Reactor Trip System Instrumentation Setpoints (TS 2.2.1)

NOTE 1 on TS Table 2.2-1 Overtemperature ΔT

- $\tau_1 = 0s, \tau_2 = 0s$ Lead/Lag compensator on measured ΔT
- $\tau_3 = 2s$ Lag compensator on measured ΔT
- $K_1 = 1.31$
- $K_2 = 0.023/^\circ F$
- $\tau_4 = 25s, \tau_5 = 3s$ Time constants utilized in the lead-lag compensator for T_{avg}
- $\tau_6 = 2s$ Lag compensator on measured T_{avg}
- $T' \leq 583.0^\circ F$ Indicated Loop T_{avg} at RATED THERMAL POWER
- $K_3 = 0.00116/psi$
- $P' \geq 2235\text{ psig}$ Nominal RCS operating pressure
- $f_1(\Delta I) = 0$ for $q_t - q_b$ between -18% and $+7\%$.

For each percent that the magnitude of $q_t - q_b$ exceeds -18% , the ΔT Trip Setpoint shall be automatically reduced by 3.51% of its value at RATED THERMAL POWER; and

For each percent that the magnitude of $q_t - q_b$ exceeds $+7\%$, the ΔT Trip Setpoint shall be automatically reduced by 2.37% of its value at RATED THERMAL POWER.

Where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER.

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NOTE 2 on TS Table 2.2-1 Overtemperature ΔT

The Overtemperature ΔT function Allowable Value shall not exceed the nominal trip setpoint by more than 0.5% ΔT span for the ΔT channel, 0.2% ΔT span for the Pressurizer Pressure channel, and 0.4% ΔT span for the $f(\Delta I)$ channel. No separate Allowable Value is provided for T_{avg} because this function is part of the ΔT value.

NOTE 3 on TS Table 2.2-1 Overpower ΔT

- $K_4 = 1.10$
- $K_5 \geq 0.0/^\circ\text{F}$ For increasing average temperature
- $K_5 = 0.0/^\circ\text{F}$ For decreasing average temperature
- $\tau_7 \geq 0 \text{ s}$ Time constants utilized in the lead-lag compensator for T_{avg}
- $K_6 = 0.0016/^\circ\text{F}$ For $T > T''$
- $K_6 = 0.0$ For $T \leq T''$
- $T'' \leq 583.0^\circ\text{F}$ Indicated Loop T_{avg} at RATED THERMAL POWER
- $f_2(\Delta I) = 0$ For all ΔI

NOTE 4 on TS Table 2.2-1 Overpower ΔT

The Overpower ΔT function Allowable Value shall not exceed the nominal trip setpoint by more than 0.5% ΔT span for the ΔT channel. No separate Allowable Value is provided for T_{avg} because this function is part of the ΔT value.

2.3 Shutdown Margin Limit for MODES 1, 2, 3 and 4 (TS 3.1.1.1)

- Figure A2 (page 14A-A8)

2.4 Shutdown Margin Limit for MODE 5 (TS 3.1.1.2)

- $\geq 1.77 \% \Delta k/k$

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2.5 Moderator temperature coefficient (MTC) (TS 3.1.1.3)

- $\leq + 5.0 \times 10^{-5} \Delta k/k/^{\circ}F$ BOL, HZP, ARO and, from HZP to 70% Rated Thermal Power (RTP)
- From 70% RTP to 100% RTP the MTC decreasing linearly from $\leq + 5.0 \times 10^{-5} \Delta k/k/^{\circ}F$ to $\leq 0.0 \times 10^{-5} \Delta k/k/^{\circ}F$
- Less negative than $- 41.0 \times 10^{-5} \Delta k/k/^{\circ}F$ EOL, RTP, ARO

2.6 Moderator temperature coefficient (MTC) Surveillance at 300 ppm (TS 4.1.1.3)

- Less negative than $- 35.0 \times 10^{-5} \Delta k/k/^{\circ}F$ Within 7 EFPD of reaching equilibrium boron concentration of 300 ppm.

2.7 Analog Rod Position Indication System (TS 3.1.3.2)

- **Figure A3** (page 14A-A9) The All Rods Out (ARO) position for all shutdown Banks and Control Banks is defined to be 229 steps withdrawn.

2.8 Control Rod Insertion Limits (TS 3.1.3.6)

- **Figure A3** (page 14A-A9) The control rod banks shall be limited in physical insertion as specified in Figure A3 for ARO = 229 steps withdrawn.

2.9 Axial Flux Difference (TS 3.2.1)

- **Figure A4** (page 14A-A10)

2.10 Heat Flux Hot Channel Factor $F_Q(Z)$ (TS 3.2.2)

- $[F_Q]^L = 2.30$
- $K(z) = 1.0$ For $0' \leq z \leq 12'$ where z is core height in ft

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2.11 Nuclear Enthalpy Rise Hot Channel Factor (TS 3.2.3)

- $F_{\Delta H}^{RTP} = 1.248$ $PF_{\Delta H} = 0.3$ DRFA Fuel
- $F_{\Delta H}^{RTP} = 1.600$ $PF_{\Delta H} = 0.3$ Upgrade Fuel

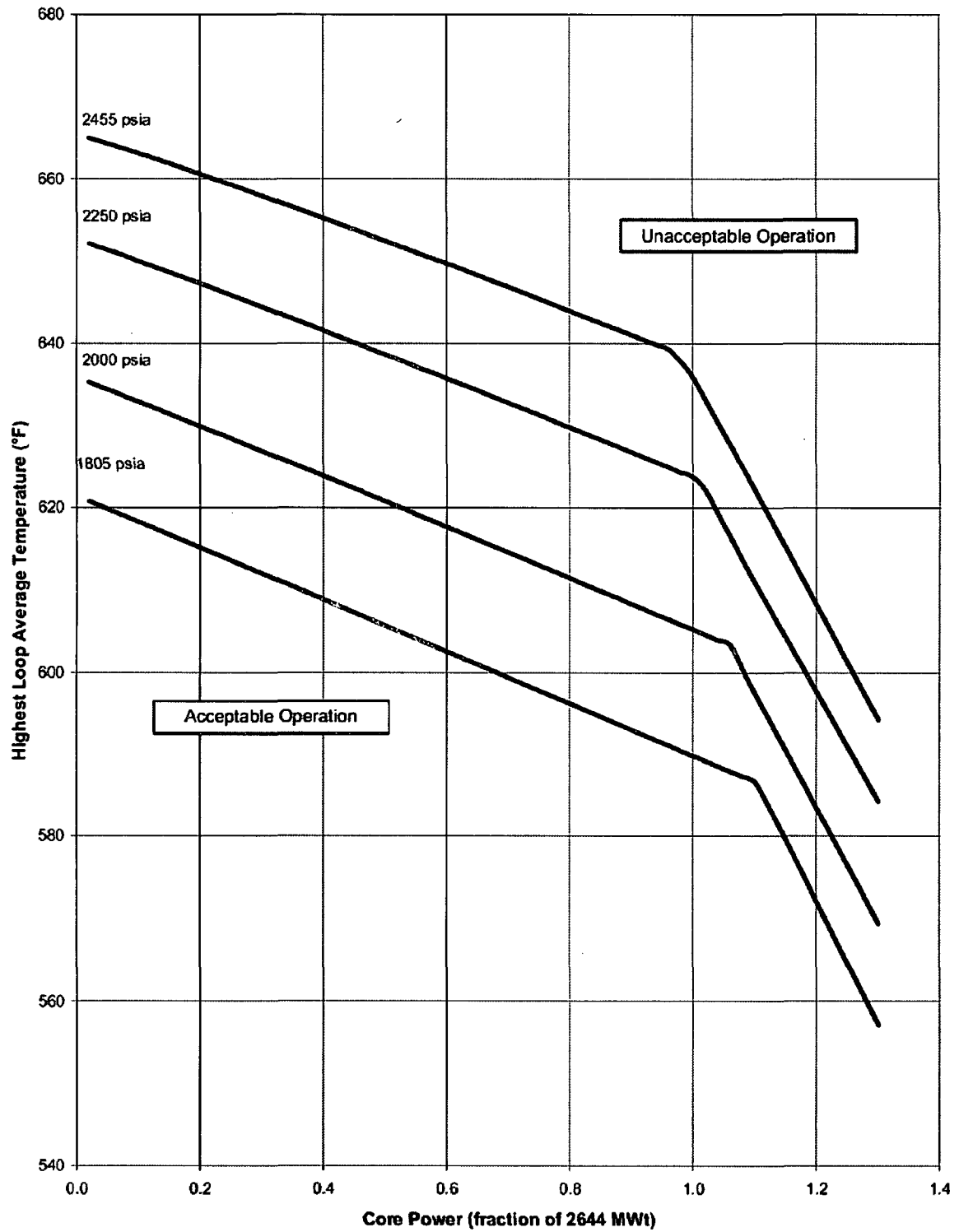
2.12 DNB Parameters (TS 3.2.5)

- $RCS\ T_{avg} \leq 585.0\ ^\circ F$
- $Pressurizer\ Pressure \geq 2204\ psig$

**TURKEY POINT UNIT 3 CYCLE 26
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Figure A1

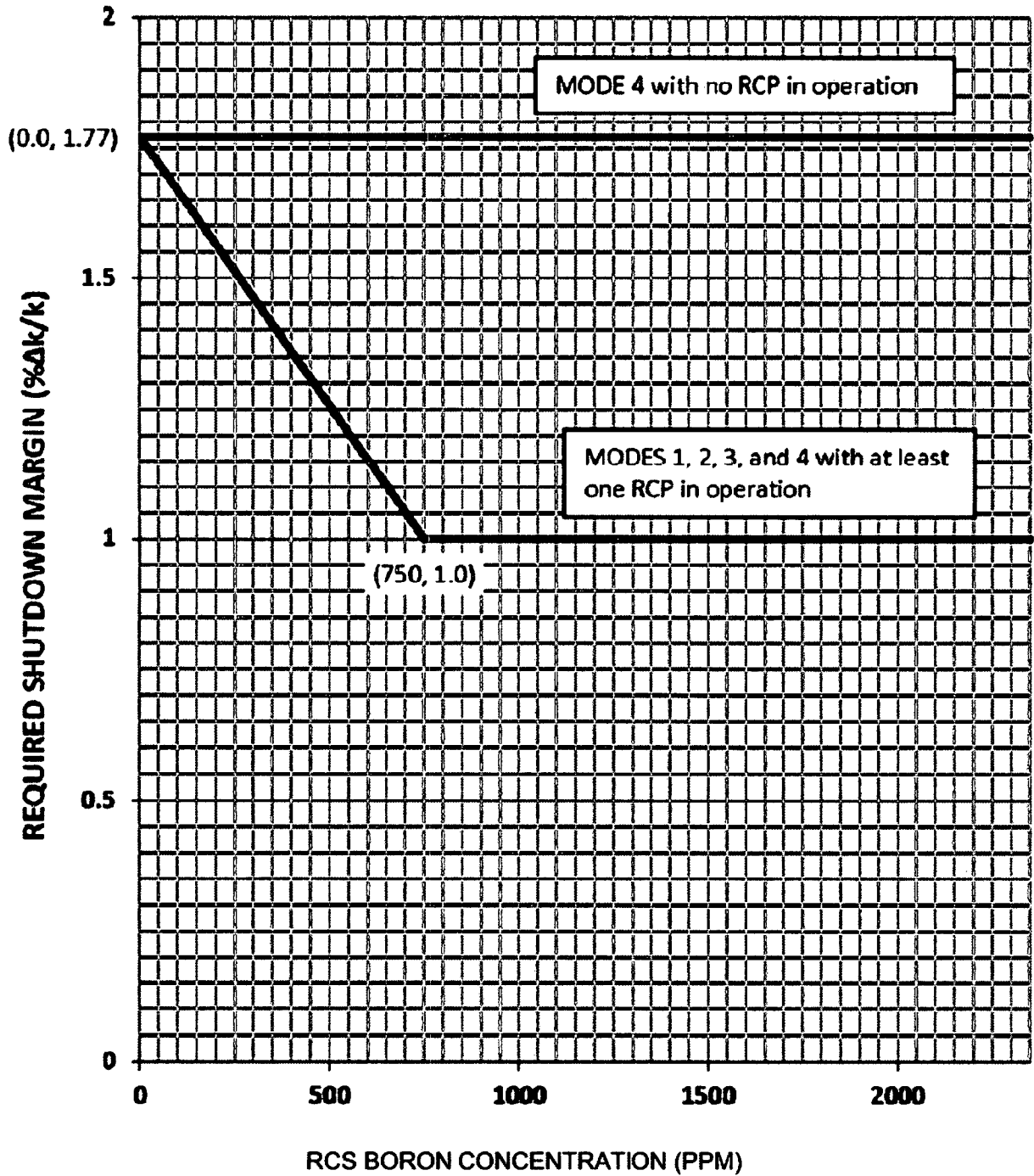
Reactor Core Safety Limit – Three Loops in Operation



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Figure A2

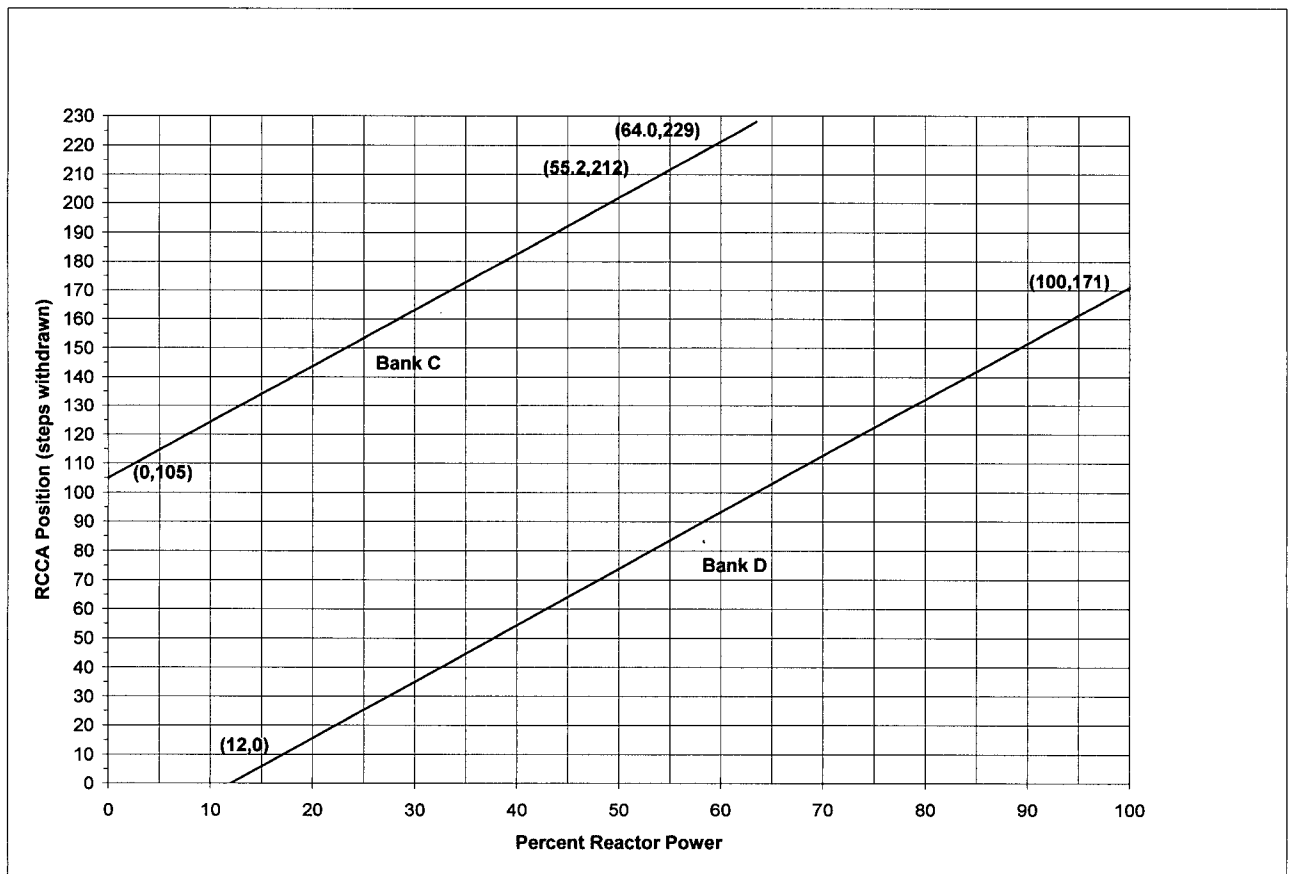
Required Shutdown Margin vs Reactor Coolant
Boron Concentration



**TURKEY POINT UNIT 3 CYCLE 26
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FIGURE A3

**Turkey Point Unit 3 Cycle 26 Rod Insertion Limits vs Thermal Power
ARO = 229 Steps Withdrawn, Overlap = 101 Steps**



**TURKEY POINT UNIT 3 CYCLE 26
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FIGURE A4

**Axial Flux Difference as a Function of Rated Thermal Power
Turkey Point Unit 3 Cycle 26**

