

EQUIPMENT AGING

B.9.1 THERMAL AGING

B.9.1.1 Arrhenius Methodology

In general, organic materials degrade continuously after becoming fully cured, the rate of which is strongly affected by temperature and material characteristics. Per IEEE 101-1972, it has been established that the Arrhenius Equation, which describes the temperature dependence of the velocity coefficient of chemical reactions, can be adapted to approximate the relationship between material life and temperature. Since the NRC has endorsed Arrhenius methodology as an acceptable means to address the effects of time/temperature aging, the following form of the Arrhenius Equation will be used to determine the thermal degradation equivalency between the component accelerated aging conditions and SONGS 2&3 service conditions:

$$t_1 = t_2 \exp[(E_a/k_B)(1/T_1 - 1/T_2)] \quad (1)$$

where,

- t_1 = Qualified Life at T_1 , hours
- t_2 = Accelerated Aging Duration, hours
- E_a = Activation Energy, eV
- k_B = Boltzmann's Constant, $8.617E-5$ eV/K
- T_1 = Service Temperature, Kelvin (K)
- T_2 = Accelerated Aging Temperature, Kelvin (K)

Unless otherwise noted, this form of the Arrhenius Equation will be used for all qualified life calculations.

B.9.1.2 Component Service Temperatures

In general, the service temperatures specified in the EQ Topical Report (Reference 65) have been used to establish the qualified lives of safety-related equipment at SONGS 2&3. However, in this EQDP, it is very conservatively assumed, that the operating temperature of Rockbestos Firewall SIS and Firewall III cable is equal to the maximum operating temperature of the conductor as 90°C.

B.9.1.3 Limiting Activation Energies

Rockbestos Power, Control and Instrumentation cables contain two age-sensitive non-metallic materials. These materials are the Cross-Linked Polyethylene Insulation (XLPE) and the Chlorosulfonated Polyethylene (Hypalon) or Neoprene Jacket. This EQDP does not consider the cable jacket material in this aging evaluations for the following reason:

D/4

- Qualification of the jacket is not required since both type tests (References 7 and 8) utilized samples ofunjacketed singles and there was no indication of any jacket failure in a manner which would prevent proper operation of the cable. Therefore it has been established that the functional integrity of the cable is not dependant on the presence of the jacket. A Sandia Laboratory report on performance of XLPE cables (Reference 25, Page 75) indicating no adverse affect on the cable performance due to failure of jacket, reinforces the above conclusion.

B.9.1.3.1 Cross-Linked Polyethylene (XLPE)

Rockbestos Long Term Thermal Aging Characteristics for Chemically Cured XLPE (Reference 7) and Irradiation Cured XLPE (Reference 8) which provide the time-temperature relationship of Rockbestos XLPE material using an Arrhenius regression line based on 60% retention of elongation after air oven aging, are shown in Figures B.9-1 and B.9-2. These thermal aging characteristics result in an activation energy of 1.34 eV for the Rockbestos XLPE material, which is utilized throughout this package.

B.9.1.4 Test Program Aging

The cables were subjected to accelerated thermal aging for 941 hours at 150°C (Reference 7, Page 49) and 900 hours at 150°C (Reference 8, page 42) for Chemically Cross-Linked XLPE (KXL-760D) and Irradiation Cross-Linked XLPE (KXL-760G).

B.9.1.5 Thermal Qualified Life Calculations

Employing Equation (1), the accelerated aging conditions of 900 hours at 150°C (423°K) can be converted to an equivalent life at the maximum normal service temperature of 90°C (363°K):

$$\begin{aligned}t_1 &= t_2 \exp[(E_a/k_B)(1/T_1 - 1/T_2)] \\t_1 &= 900 \exp[(1.34/8.617E-5)(1/363 - 1/423)] \text{ hours} \\t_1 &= 391,949 \text{ hours or } 44 \text{ years at } 90^\circ\text{C}\end{aligned}$$

FIGURE B.9-1
 (Reference 7, page 50)

QR-5804

Data Section 3

Arrhenius Data

(Thermal Aging Characteristic)

Calculation of Arrhenius regression line based on 60% retention of elongation after air oven aging.

The equation has the form, Ref. IEEE-101A-1974,

$$\begin{aligned} \text{Life (hours)} &= A \exp B/T \\ \text{or} \\ \ln (\text{hours}) &= \ln A + B/T \end{aligned}$$

- A. For FW III Chemically Cross-Linked Insulation, KXL-760D there are three data points:

Hours	Temperature Deg. C	ln Hours	Recip Abs Temp (1/Deg K x 1000)
825	150	6.7153	2.3641
4300	136	8.3663	2.4450
12600	121	9.4414	2.5381

Linear regression analysis results:

$$\begin{aligned} \text{Slope (B)} &= 15564.38 \\ \text{Intercept (ln A)} &= 29.9439 \\ \text{Correlation Coefficient} &= .9866 \end{aligned}$$

Calculated regression point temp. for 40 years = 91.4 Deg. C

Calculated regression point temp. for 100 hours = 177.5 Deg. C

Activation Energy = 1.3412 eV

941 hours aging @ 150 Deg. C represents 412,000 hours, or 47 years
 at a 90 Degree C service temperature.

FIGURE B.9-2
 (Reference 8, page 42)

QR-5805

Data Section 3

Arrhenius Data

(Thermal Aging Characteristic)

Calculation of Arrhenius regression line based on 60% retention of elongation after air oven aging.

The equation has the form, Ref. IEEE-101A-1974,

$$\begin{aligned} \text{Life (hours)} &= A \exp B/T \\ \text{or} \\ \ln (\text{hours}) &= \ln A + B/T \end{aligned}$$

A. For FW III Irradiation Cross-Linked Insulation, KXL-760G there are three data points:

Hours	Temperature Deg. C	ln Hours	Recip Abs Temp (1/Deg K x 1000)
625	150	6.4377	2.3641
3300	136	8.1016	2.4450
9650	121	9.1747	2.5381

Linear regression analysis results:

$$\begin{aligned} \text{Slope (B)} &= 15624.9 \\ \text{Intercept (ln A)} &= 30.3618 \\ \text{Correlation Coefficient} &= .9861 \end{aligned}$$

Calculated regression point temp. for 40 years = 89.3 Deg. C
 Calculated regression point temp. for 100 hours = 173.8 Deg. C
 Activation Energy = 1.3464 eV

900 hours aging @ 150 Deg. C represents 403,490 hours, or 46 years at a 90 Degree C service temperature.

B.9.2 RADIATION AGING

As documented in the test reports data sheets (Reference 7, Page 55 and Reference 8, p. 47), Isomedix used a Cobalt 60 gamma source to apply a TID of $1.84E8$ rads (minimum applied dose due to instrumentation tolerances). Dose rates were maintained at levels which did not exceed $9.4E5$ rads/hour (Reference 17).

B.9.3 CYCLIC WEAR AGING

Cables are passive components which are not subject to cyclic wear aging. Per IEEE 383-1974, "IEEE Standard for Type Test of Class IE Electric Cables, Field Splices, and Connections for Nuclear Power Generating Stations" does not consider cyclic wear aging as part of a typical cable type test program which may be used for qualifying Class IE electric cables. Therefore, this Subsection is not applicable.

B.9.4 NONSEISMIC VIBRATION AGING

As discussed in IEEE 323-1974, the requirement to simulate the potential degradation effects of in-service mechanical vibration aging as part of a test sequence is typically associated with two categories of components:

- Equipment subject to self-induced vibration (such as the starting and running of a motor).
- Equipment subject to vibration from nearby equipment or vibration from devices which provide the mounting support for the equipment (such as pipes, generators, motors, etc).

Cables may be categorized as passive components which are not subject to self-induced vibration. Consequently, this equipment is subject only to vibrational excitation from other sources to which it may be mechanically coupled. Since the cables in use at SONGS Units 2&3 are located in trays or in conduit except for short supported runs to devices, they will not be susceptible to nonseismic vibration degradation or damage over their installed life. Therefore, a consideration of vibration aging effects is not required to demonstrate qualification.

B.9.5 SYNERGISTIC EFFECTS

One of the requirements of 10 CFR 50.49 is an assessment of the synergistic effects of radiation in combination with other environmental stresses.

A synergistic relationship is observed when two or more stresses applied simultaneously produce degradation of a different type or magnitude than the same stresses applied sequentially. A review of industry published data has revealed that research has generally been limited to electric cables used inside containment for a limited range of specific environmental conditions. Given the limited scope and applicability of available synergistic documentation, the effects of the various service conditions are typically addressed individually.

The synergistic relationship between multiple stresses usually cannot be deduced from physical principles, rather, an experimental approach must be employed. Synergistic stresses usually require extensive testing to reveal their magnitudes, since most interaction effects are minute by comparison to the primary effects, and thus require significantly more experimental evidence to identify. Current research indicates that synergistic effects can typically be categorized under two main headings:

- Test Sequence Effects - The sequence in which radiation and thermal aging exposures occur is an important consideration. Radiation combined with elevated temperatures or radiation followed by elevated temperatures typically produces more material degradation than when thermal aging precedes radiation exposure (References 4 and 5).
- Radiation Dose Rate Effects - For many materials, it has been observed that lower dose rates produce significantly more degradation than a higher dose rate for the same total applied dose (Reference 6).

Although most IEEE Standards pertaining to equipment qualification (323, 334, 382, 383, etc.) specify a test sequence where accelerated thermal aging precedes radiation exposure, recent studies indicate that radiation exposure prior to thermal aging is the most conservative test sequence for the majority of organic materials (note that synergistic degradation mechanisms have not been established for inorganic and metallic materials operating within the specified range of service conditions).

However, in accordance with IEEE 323-1974, the Rockbestos test program selected a sequence where the normal radiation exposure was applied after accelerated thermal aging and combined with the accident radiation exposure. The LOCA simulation was performed after the thermal and radiation aging (Reference 7, Page 1 and Reference 8, page 1). The combination of LOCA environment with thermal and radiation conditions more than adequately simulates the sequence of radiation followed by elevated temperatures.

Per IEEE 383-1974, paragraph 2.4.2, the maximum allowed radiation dose rate on cable specimens is 1.0E6 rads per hour. The dose rate used on both type Rockbestos tests for Firewall SIS and Firewall III XLPE cables is 0.94E6 rads per hour. This is a 6% more conservative dose rate than the maximum allowed by IEEE 383-1974.

Reference 25 also confirmed that there is no significant difference between the single conductor and multiconductor cable insulation resistance. As an additional conservatism, the combination of environmental stresses impressed upon the test specimens during the qualification program are judged of sufficient severity to adequately account for any unknown or unaccounted for synergistic degradation mechanisms. Since the multiconductor cables in use at SONGS Units 2&3 are being applied well within their design ratings, synergistic effects are considered an insignificant degradation mechanism over the specified range of environmental conditions.

EQ Document M38773 Rev. 6 for Power Cable, Subsection B.9
Thermal Qualified Life Calculations

$$t_1 = t_2 \exp\{ (E_a / K_b) * (1/T_1 - T_2) \}$$

t_1 = Qualified Life at T_1 , hours
 t_2 = Qualified Life at T_2 , hours
 E_a = Activation Energy, eV
 K_b = Boltzmann's Constant, 8.617E-5eV/k
 T_1 = Service Temperature, Kelvin (k) 90°C +273
 T_2 = Accelerated Aging Temperature, Kelvin (k)

Test Program Aging as described on page B.9-2		$t_1 =$ t_2 Hours	E_a K_b	T_1 T_2
		391,941 900	1.34 8.617E-5 (E_a / K_b) 15551 exp 435.499 391949 or 44 years at 90°C	363 423 ($1/T_1 - T_2$) 0.000391
During Abnormal condition the aging would be as follows:				
scenario	Description			
1	Abnormal Load Current 129A Conductor temperature will be 132°C in 5 Hours Calculate aging at this temperature.	900	1.34 8.617E-5 (E_a / K_b) 15551 exp 5.123825 4611 or six months at 132°C	405 423 ($1/T_1 - T_2$) 0.000105
2	Abnormal Load Current 180A Conductor temperature will be 238°C in 5 Hours Calculate aging at this temperature.	900	1.34 8.617E-5 (E_a / K_b) 15551 exp 0.00178 2 Hours at 238°C	511 423 ($1/T_1 - T_2$) -0.000407

BREAKERS: 3B0405 (Pump 3P1911) 3B0413 (Pump 3P1901)

IE	IN	IO	TO	TN	TA	K	I	TE	FLA	Time	92.4	101.0	128.3	160.0
											CONDUCTOR TEMPERATURE			
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.08	56.8	0.00	55.6	58.1	80.4	95	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.17	57.7	0.05	55.5	60.3	84.8	102	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.25	64.5	0.10	55.4	62.4	89.2	109	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.33	67.0	0.15	55.3	64.3	93.3	112	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.42	69.5	0.20	55.2	66.2	97.2	115	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.50	71.8	0.25	55.1	67.9	100.8	118	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.58	73.9	0.30	55.0	69.5	104.4	121	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.67	75.9	0.35	54.9	71.0	107.9	124	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.75	77.8	0.40	54.8	72.4	111.4	127	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.83	79.6	0.45	54.8	73.7	114.9	130	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	0.92	81.2	0.50	54.7	74.9	118.4	133	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.00	82.7	0.55	54.7	76.0	121.9	136	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.08	84.2	0.60	54.6	77.1	125.4	139	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.17	85.5	0.65	54.6	78.1	128.9	142	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.25	86.7	0.70	54.5	79.0	132.4	145	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.33	87.9	0.75	54.5	79.8	135.9	148	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.42	89.0	0.80	54.4	80.6	139.4	151	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.50	90.0	0.85	54.4	81.3	142.9	154	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.58	90.9	0.90	54.3	82.0	146.4	157	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.67	91.7	0.95	54.3	82.8	149.9	160	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.75	92.5	1.00	54.2	83.2	153.4	163	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.83	93.3	1.05	54.2	83.7	156.9	166	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	1.92	93.9	1.10	54.2	84.2	160.4	169	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.00	94.6	1.15	54.2	84.7	163.9	172	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.08	95.1	1.20	54.2	85.1	167.4	175	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.17	95.7	1.25	54.2	85.5	170.9	178	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.25	96.2	1.30	54.2	85.8	174.4	181	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.33	96.8	1.35	54.2	86.1	177.9	184	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.42	97.0	1.40	54.2	86.4	181.4	187	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.50	97.4	1.45	54.2	86.7	184.9	190	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.58	97.8	1.50	54.1	87.0	188.4	193	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.67	98.1	1.55	54.1	87.2	191.9	196	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.75	98.4	1.60	54.1	87.4	195.4	199	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.83	98.7	1.65	54.1	87.6	198.9	202	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	2.92	99.0	1.70	54.1	87.8	202.4	205	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.00	99.2	1.75	54.1	88.0	205.9	208	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.08	99.4	1.80	54.1	88.2	209.4	211	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.17	99.6	1.85	54.1	88.3	212.9	214	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.25	99.8	1.90	54.1	88.4	216.4	217	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.33	100.0	1.95	54.1	88.5	219.9	220	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.42	100.2	2.00	54.1	88.7	223.4	223	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.50	100.3	2.05	54.1	88.8	226.9	226	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.58	100.4	2.10	54.0	88.9	230.4	229	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.67	100.6	2.15	54.0	89.0	233.9	232	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.75	100.7	2.20	54.0	89.1	237.4	235	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.83	100.8	2.25	54.0	89.1	240.9	238	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	3.92	100.9	2.30	54.0	89.2	244.4	241	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.00	101.0	2.35	54.0	89.3	247.9	244	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.08	101.1	2.40	54.0	89.3	251.4	247	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.17	101.1	2.45	54.0	89.4	254.9	250	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.25	101.2	2.50	54.0	89.4	258.4	253	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.33	101.3	2.55	54.0	89.5	261.9	256	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.42	101.3	2.60	54.0	89.5	265.4	259	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.50	101.4	2.65	54.0	89.6	268.9	262	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.58	101.4	2.70	54.0	89.6	272.4	265	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.67	101.5	2.75	54.0	89.6	275.9	268	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.75	101.5	2.80	54.0	89.7	279.4	271	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.83	101.6	2.85	54.0	89.7	282.9	274	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	4.92	101.6	2.90	54.0	89.7	286.4	277	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.00	101.6	2.95	54.0	89.7	289.9	280	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.08	101.7	3.00	54.0	89.7	293.4	283	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.17	101.7	3.05	54.0	89.8	296.9	286	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.25	101.7	3.10	54.0	89.8	300.4	289	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.33	101.7	3.15	54.0	89.8	303.9	292	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.42	101.8	3.20	54.0	89.8	307.4	295	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.50	101.8	3.25	54.0	89.8	310.9	298	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.58	101.8	3.30	54.0	89.8	314.4	301	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.67	101.8	3.35	54.0	89.9	317.9	304	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.75	101.8	3.40	54.0	89.9	321.4	307	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.83	101.8	3.45	54.0	89.9	324.9	310	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	5.92	101.9	3.50	54.0	89.9	328.4	313	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.00	101.9	3.55	54.0	89.9	331.9	316	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.08	101.9	3.60	54.0	89.9	335.4	319	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.17	101.9	3.65	54.0	89.9	338.9	322	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.25	101.9	3.70	54.0	89.9	342.4	325	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.33	101.9	3.75	54.0	89.9	345.9	328	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.42	101.9	3.80	54.0	89.9	349.4	331	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.50	101.9	3.85	54.0	89.9	352.9	334	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.58	101.9	3.90	54.0	89.9	356.4	337	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.67	101.9	3.95	54.0	89.9	359.9	340	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.75	101.9	4.00	54.0	89.9	363.4	343	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.83	101.9	4.05	54.0	89.9	366.9	346	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	6.92	102.0	4.10	54.0	89.9	370.4	349	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	7.00	102.0	4.15	54.0	89.9	373.9	352	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	7.08	102.0	4.20	54.0	89.9	377.4	355	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	7.17	102.0	4.25	54.0	89.9	380.9	358	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	7.25	102.0	4.30	54.0	89.9	384.4	361	
180.0	184.6	92.4	40.0	90.0	40.0	1.0	7.33	102.0	4.35	54.0	89.9	387.9	364	
180.0	184.													

E = Emergency operating time, A
 EI = Normal current rating (ampere), A
 EO = Operating current prior to emergency, A
 t = Time at overrated condition (hours)
 k = Constant (dependent on table entry and installation)
 234.5 Zero resistance temperature value for load:
 $k = 1$

TE_{RATED} = Emergency operating time, °C
 TE = Normal time rating, °C
 TO = Overcurrent time, same as emergency, °C
 TA = Ambient temperature, °C

TE_{RATED} 150 °C
 TA 90 °C
 TA 40 °C
 k 1.00 For 800V & 3 Cables

Table 53 Adjustment Factors for 234.5			
Category	Temperature, °C	Factor	Result
1	150	0.22	1.73
2	175	0.40	2.30
3	200	0.60	3.00

TE Calculated 189.7 °C	M	TE Calculated 281.2 °C	TE Calculated 250 °C	IE Time
IE 180.00 Amps	SP180	IE 180.00 Amps	IE 1250.00 Amps	2000
IN 101.00 Amps	Charging Pump	IN 101.00 Amps	IN 101.00 Amps	2000
IO 101.00 Amps		IO 101.00 Amps	IO 101.00 Amps	2000
TD 40.00 °C		TD 40.00 °C	TD 40.00 °C	2000
T 1.00 Hrs		T 2.00 Hrs	T 0.0001 Hrs	2000
189.7	10	189.7	189.7	189.7
TE Calculated 159.3 °C	S	TE Calculated 189.3 °C	TE Calculated 159.3 °C	159.3
IE 83.80 Amps	77000	IE 83.80 Amps	IE 84.00 Amps	159.3
IN 42.20 Amps		IN 42.20 Amps	IN 42.00 Amps	159.3
IO 42.20 Amps		IO 42.20 Amps	IO 42.00 Amps	159.3
TD 40.00 °C		TD 40.00 °C	TD 40.00 °C	159.3
T 1.00 Hrs		T 8.00 Hrs	T 8 Hrs	159.3
159.3	15	159.3	159.3	159.3
TE Calculated 107.4 °C	M	TE Calculated 120.3 °C	TE Calculated 121.3 °C	121.3
IE 51.20 Amps	8423	IE 51.20 Amps	IE 51.00 Amps	121.3
IN 42.20 Amps		IN 42.20 Amps	IN 42.00 Amps	121.3
IO 42.20 Amps		IO 42.20 Amps	IO 42.00 Amps	121.3
TD 40.00 °C		TD 40.00 °C	TD 40.00 °C	121.3
T 1.00 Hrs		T 7.00 Hrs	T 8 Hrs	121.3
107.4	25	107.4	107.4	107.4
TE Calculated 97.1 °C	M	TE Calculated 102.1 °C	TE Calculated 102.1 °C	102.1
IE 20.80 Amps	6148	IE 20.80 Amps	IE 20.00 Amps	102.1
IN 24.20 Amps		IN 24.20 Amps	IN 24.00 Amps	102.1
IO 24.20 Amps		IO 24.20 Amps	IO 24.00 Amps	102.1
TD 40.00 °C		TD 40.00 °C	TD 40.00 °C	102.1
T 1.00 Hrs		T 5.00 Hrs	T 8 Hrs	102.1
97.1	45	97.1	97.1	97.1
TE Calculated 109.3 °C	S	TE Calculated 123.1 °C	TE Calculated 124.3 °C	124.3
IE 29.80 Amps	COH1	IE 29.80 Amps	IE 30.00 Amps	124.3
IN 24.20 Amps	Shut?	IN 24.20 Amps	IN 24.00 Amps	124.3
IO 24.20 Amps	SA	IO 24.20 Amps	IO 24.00 Amps	124.3
TD 40.00 °C		TD 40.00 °C	TD 40.00 °C	124.3
T 1.00 Hrs		T 7.00 Hrs	T 8 Hrs	124.3
109.3	55	109.3	109.3	109.3
109.3	65	109.3	109.3	109.3
109.3	75	109.3	109.3	109.3
109.3	85	109.3	109.3	109.3
109.3	95	109.3	109.3	109.3
109.3	105	109.3	109.3	109.3
109.3	115	109.3	109.3	109.3
109.3	125	109.3	109.3	109.3
109.3	135	109.3	109.3	109.3
109.3	145	109.3	109.3	109.3
109.3	155	109.3	109.3	109.3
109.3	165	109.3	109.3	109.3
109.3	175	109.3	109.3	109.3
109.3	185	109.3	109.3	109.3
109.3	195	109.3	109.3	109.3
109.3	205	109.3	109.3	109.3
109.3	215	109.3	109.3	109.3
109.3	225	109.3	109.3	109.3
109.3	235	109.3	109.3	109.3
109.3	245	109.3	109.3	109.3
109.3	255	109.3	109.3	109.3
109.3	265	109.3	109.3	109.3
109.3	275	109.3	109.3	109.3
109.3	285	109.3	109.3	109.3
109.3	295	109.3	109.3	109.3
109.3	305	109.3	109.3	109.3
109.3	315	109.3	109.3	109.3
109.3	325	109.3	109.3	109.3
109.3	335	109.3	109.3	109.3
109.3	345	109.3	109.3	109.3
109.3	355	109.3	109.3	109.3
109.3	365	109.3	109.3	109.3
109.3	375	109.3	109.3	109.3
109.3	385	109.3	109.3	109.3
109.3	395	109.3	109.3	109.3
109.3	405	109.3	109.3	109.3
109.3	415	109.3	109.3	109.3
109.3	425	109.3	109.3	109.3
109.3	435	109.3	109.3	109.3
109.3	445	109.3	109.3	109.3
109.3	455	109.3	109.3	109.3
109.3	465	109.3	109.3	109.3
109.3	475	109.3	109.3	109.3
109.3	485	109.3	109.3	109.3
109.3	495	109.3	109.3	109.3
109.3	505	109.3	109.3	109.3
109.3	515	109.3	109.3	109.3
109.3	525	109.3	109.3	109.3
109.3	535	109.3	109.3	109.3
109.3	545	109.3	109.3	109.3
109.3	555	109.3	109.3	109.3
109.3	565	109.3	109.3	109.3
109.3	575	109.3	109.3	109.3
109.3	585	109.3	109.3	109.3
109.3	595	109.3	109.3	109.3
109.3	605	109.3	109.3	109.3
109.3	615	109.3	109.3	109.3
109.3	625	109.3	109.3	109.3
109.3	635	109.3	109.3	109.3
109.3	645	109.3	109.3	109.3
109.3	655	109.3	109.3	109.3
109.3	665	109.3	109.3	109.3
109.3	675	109.3	109.3	109.3
109.3	685	109.3	109.3	109.3
109.3	695	109.3	109.3	109.3
109.3	705	109.3	109.3	109.3
109.3	715	109.3	109.3	109.3
109.3	725	109.3	109.3	109.3
109.3	735	109.3	109.3	109.3
109.3	745	109.3	109.3	109.3
109.3	755	109.3	109.3	109.3
109.3	765	109.3	109.3	109.3
109.3	775	109.3	109.3	109.3
109.3	785	109.3	109.3	109.3
109.3	795	109.3	109.3	109.3
109.3	805	109.3	109.3	109.3
109.3	815	109.3	109.3	109.3
109.3	825	109.3	109.3	109.3
109.3	835	109.3	109.3	109.3
109.3	845	109.3	109.3	109.3
109.3	855	109.3	109.3	109.3
109.3	865	109.3	109.3	109.3
109.3	875	109.3	109.3	109.3
109.3	885	109.3	109.3	109.3
109.3	895	109.3	109.3	109.3
109.3	905	109.3	109.3	109.3
109.3	915	109.3	109.3	109.3
109.3	925	109.3	109.3	109.3
109.3	935	109.3	109.3	109.3
109.3	945	109.3	109.3	109.3
109.3	955	109.3	109.3	109.3
109.3	965	109.3	109.3	109.3
109.3	975	109.3	109.3	109.3
109.3	985	109.3	109.3	109.3
109.3	995	109.3	109.3	109.3
109.3	1005	109.3	109.3	109.3
109.3	1015	109.3	109.3	109.3
109.3	1025	109.3	109.3	109.3
109.3	1035	109.3	109.3	109.3
109.3	1045	109.3	109.3	109.3
109.3	1055	109.3	109.3	109.3
109.3	1065	109.3	109.3	109.3
109.3	1075	109.3	109.3	109.3
109.3	1085	109.3	109.3	109.3
109.3	1095	109.3	109.3	109.3
109.3	1105	109.3	109.3	109.3
109.3	1115	109.3	109.3	109.3
109.3	1125	109.3	109.3	109.3
109.3	1135	109.3	109.3	109.3
109.3	1145	109.3	109.3	109.3
109.3	1155	109.3	109.3	109.3
109.3	1165	109.3	109.3	109.3
109.3	1175	109.3	109.3	109.3
109.3	1185	109.3	109.3	109.3
109.3	1195	109.3	109.3	109.3
109.3	1205	109.3	109.3	109.3
109.3	1215	109.3	109.3	109.3
109.3	1225	109.3	109.3	109.3
109.3	1235	109.3	109.3	109.3
109.3	1245	109.3	109.3	109.3
109.3	1255	109.3	109.3	109.3
109.3	1265	109.3	109.3	109.3
109.3	1275	109.3	109.3	109.3
109.3	1285	109.3	109.3	109.3
109.3	1295	109.3	109.3	109.3
109.3	1305	109.3	109.3	109.3
109.3	1315	109.3	109.3	109.3
109.3	1325	109.3	109.3	109.3
109.3	1335	109.3	109.3	109.3
109.3	1345	109.3	109.3	109.3
109.3	1355	109.3	109.3	109.3
109.3	1365	109.3	109.3	109.3
109.3	1375	109.3	109.3	109.3
109.3	1385	109.3	109.3	109.3
109.3	1395	109.3	109.3	109.3
109.3	1405	109.3	109.3	109.3
109.3	1415	109.3	109.3	109.3
109.3	1425	109.3	109.3	109.3
109.3	1435	109.3	109.3	109.3
109.3	1445	109.3	109.3	109.3
109.3	1455	109.3	109.3	109.3
109.3	1465	109.3	109.3	109.3
109.3	1475	109.3	109.3	109.3
109.3	1485	109.3	109.3	109.3
109.3	1495	109.3	109.3	109.3
109.3	1505	109.3	109.3	109.3
109.3	1515	109.3	109.3	109.3
109.3	1525	109.3	109.3	109.3
109.3	1535	109.3	109.3	109.3
109.3	1545	109.3	109.3	109.3
109.3	1555	109.3	109.3	109.3
109.3	1565	109.3	109.3	109.3
109.3	1575	109.3	109.3	109.3
109.3	1585	109.3	109.3	109.3
109.3	1595	109.3	109.3	109.3
109.3	1605	109.3	109.3	109.3
109.3	1615	109.3	109.3	109.3
109.3	1625	109.3	109.3	109.3
109.3	1635	109.3	109.3	109.3
109.3	1645	109.3	109.3	109.3
109.3	1655	109.3	109.3	109.3
109.3	1665	109.3	109.3	109.3
109.3	1675	109.3	109.3	109.3
109.3	1685	109.3	109.3	109.3
109.3	1695	109.3	109.3	109.3
109.3	1705	109.3	109.3	109.3
109.3	1715	109.3	109.3	109.3
109.3	1725	109.3	109.3	109.3
109.3	1735	109.3	109.3	109.3
109.3	1745	109.3	109.3	109.3
109.3	1755	109.3	109.3	109.3
109.3	1765	109.3	109.3	109.3
109.3	1775	109.3	109.3	109.3
109.3	1785	109.3	109.3	109.3