

TABLES

Table 1. Results of Monitor Well Samples, February 2011

Well ID	MW-12	MW-9	MW-14	MW-108	MW-109	MW-74	MW-43R	MW-110	MW-111
Sample Date	2/11/2011	2/11/2011	2/11/2011	2/12/2011	2/12/2011	2/10/2011	2/12/2011	2/10/2011	2/10/2011
	Lang Draw					Northern Pathway			
Analyte									
Major Ions (mg/L)									
Calcium	883	883	824	868	552	686	739	769	520
Chloride	371	334	358	302	89	233	254	290	102
Magnesium	544	200	343	179	137	175	154	156	90
Nitrogen Nitrate + Nitrite as N	0.01	0.81	<0.01	0.06	0.13	4.4	0.05	0.01	0.04
Phosphorus Total as P	<0.005	0.006	0.058	0.013	0.029	0.008	0.009	0.064	0.01
Potassium	18	6	11	9	10	14	16	17	7
Sodium	297	257	268	180	127	122	66	43	24
Sulfate	2810	1880	2280	1620	1900	2000	1530	1720	1190
Metals Dissolved (mg/L)									
Aluminum	<0.1	<0.1	<0.1	<0.1	0.2	<0.1	<0.1	<0.1	<0.1
Arsenic	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001
Barium	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Beryllium	<0.001	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	N/A
Cadmium	<0.001	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	N/A
Chromium	<0.001	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	N/A
Iron	0.41	1.14	1.46	0.55	0.53	4.62	0.59	9.92	0.19
Manganese	6.62	0.18	1.19	0.43	0.04	2.11	1.04	0.53	<0.01
Molybdenum	<0.001	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	N/A
Nickel	0.035	0.018	0.04	0.043	0.013	0.042	0.017	0.006	0.004
Selenium	0.002	<0.001	0.004	N/A	N/A	0.021	0.003	N/A	N/A
Silica	28	23.7	25.9	26.2	14.1	29	19.6	23.6	18.1
Uranium (pCi/L)	420	195	439	135	61.3	15.4	38	1.6	17.6
Metals Total (mg/L)									
Aluminum	<0.1	<0.1	<0.1	1.2	3.1	<0.1	0.3	3	2.1
Iron	0.57	1.25	1.55	1.53	2	4.96	1.55	12.9	1.23
Manganese	6.72	0.19	1.21	0.49	0.03	2.14	1.16	0.54	0.02
Silica	31.6	25.9	27.3	18.5	29	30.9	20.8	38.7	28.2
Radionuclides Dissolved (pCi/L)									
Radium-226	0.62	0.3	0.09	0.41	0.5	2.2	1.8	2.9	0.42
Radium-228	2.4	1.9	0.8	1.6	1.3	4	3.1	7.6	1.4
Thorium-230	-0.3	-0.06	<0.1	-0.1	-0.05	-0.09	-0.07	<0.02	-0.06
Total Dissolved Solids (mg/L)	5770	4390	5050	3980	3050	3700	3410	3340	2260
pH (s.u.)	6.56	7.00	7.16	6.75	7.34	7.26	6.72	7.28	7.60

Table 2. Saturation Indices for Water Samples on Lang Draw Flow Path, 2011

Phase	Formula	MW-108	MW-109	MW-12	MW-14	MW-9
(UO ₂) ₃ (PO ₄) ₂ ·4w	(UO ₂) ₃ (PO ₄) ₂ ·4H ₂ O	-36.01	-33.17		-36.37	-38.16
Al(OH) ₃ (a)	Al(OH) ₃		-0.7			
Calcite	CaCO ₃	0.74	0.49	0.37	1.17	1.02
Chalcedony	SiO ₂	0.2	-0.07	0.23	0.2	0.16
CO ₂ (g)	CO ₂ pressure (atmos.)	-0.91	-2.13	-0.74	-1.22	-1.11
Ferrihydrite	Fe(OH) ₃	2.23	2.49	1.97	2.86	2.69
Gypsum	CaSO ₄ ·2H ₂ O	-0.01	-0.05	0.02	0.04	0.04
Magnesite	MgCO ₃	-0.19	-0.36	0.01	0.55	0.13
MnHPO ₄	MnHPO ₄	-0.28	-0.63		0.79	-0.97
Schoepite	UO ₂ (OH) ₂ ·H ₂ O	-7.67	-6.33	-6.64	-7.72	-7.88
Siderite	FeCO ₃	-7.03	-7.99	-7.12	-6.71	-6.77
U ₃ O ₈ (c)	U ₃ O ₈	-38.21	-34.19	-35.12	-38.37	-38.83
UO ₂ (OH) ₂ (beta)	UO ₂ (OH) ₂	-7.21	-5.87	-6.18	-7.27	-7.42
Uraninite(c)	UO ₂	-26.43	-25.09	-25.4	-26.48	-26.63

Note: SI less than 0 indicates undersaturation and SI greater than 0 indicates supersaturation.

Table 3. Saturation Indices for Water Samples on Northern Pathway

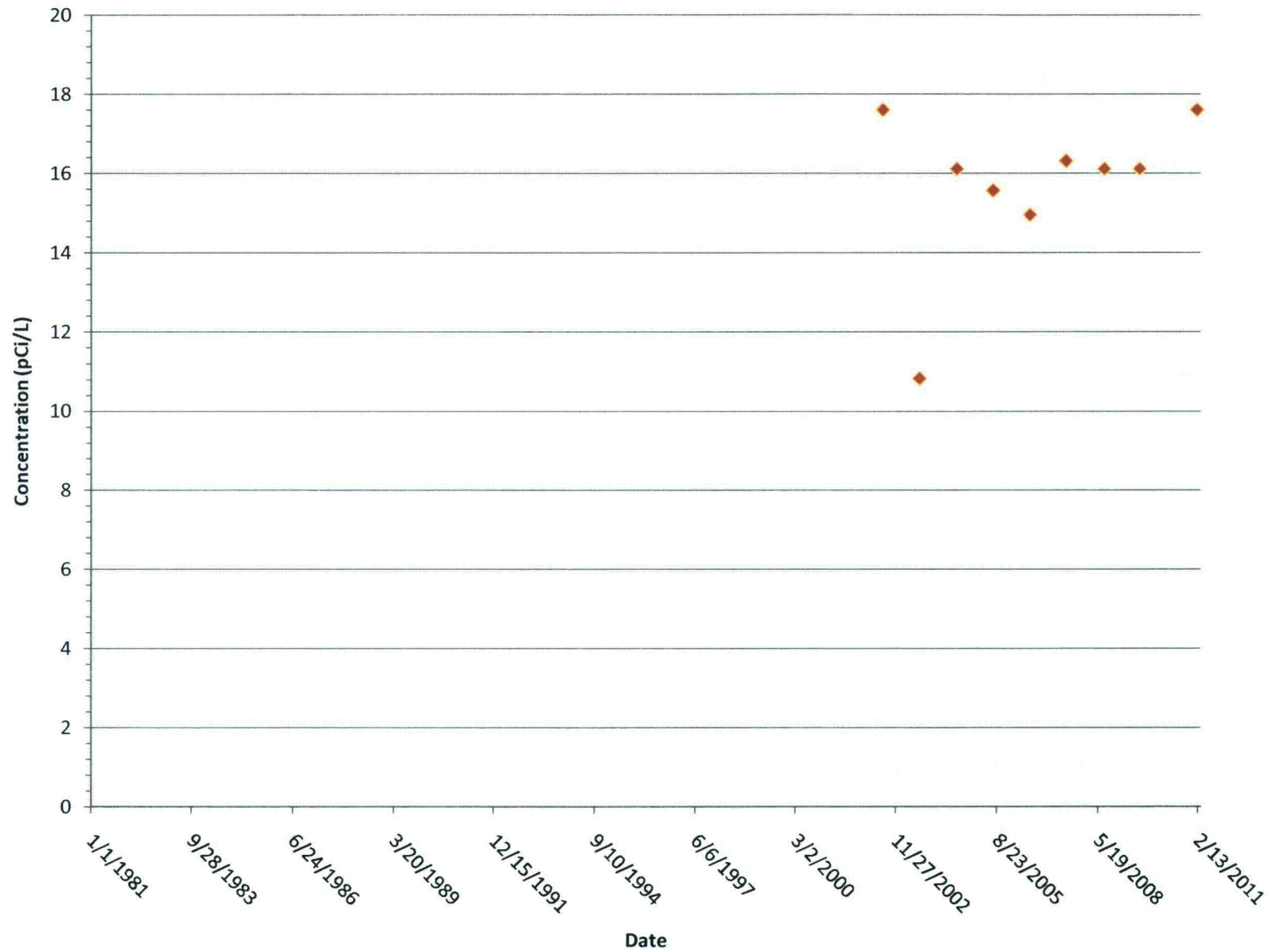
Phase	Formula	MW-110	MW-111	MW-43	MW-74
(UO ₂) ₃ (PO ₄) ₂ ·4w	(UO ₂) ₃ (PO ₄) ₂ ·4H ₂ O	-40.91	-39.97	-35.5	-36.95
Calcite	CaCO ₃	0.93	1.05	0.44	0.59
Chalcedony	SiO ₂	0.15	0.03	0.07	0.24
CO ₂ (g)	CO ₂ pressure (atmos)	-1.73	-2.14	-1.1	-1.96
Ferrihydrite	Fe(OH) ₃	3.74	2.1	2.24	3.4
Gypsum	CaSO ₄ ·2H ₂ O	0.01	-0.19	-0.04	0.02
Magnesite	MgCO ₃	-0.01	0.04	-0.48	-0.25
MnHPO ₄	MnHPO ₄	0.7		0.03	0.45
Schoepite	UO ₂ (OH) ₂ ·H ₂ O	-9.16	-7.96	-7.45	-7.28
Siderite	FeCO ₃	-6.34	-8.39	-7.2	-6.91
U ₃ O ₈ (c)	U ₃ O ₈	-42.69	-39.1	-37.54	-37.04
UO ₂ (OH) ₂ (beta)	UO ₂ (OH) ₂	-8.71	-7.51	-6.99	-6.82
Uraninite(c)	UO ₂	-27.92	-26.72	-26.2	-26.04

Note: SI less than 0 indicates undersaturation and SI greater than 0 indicates supersaturation.

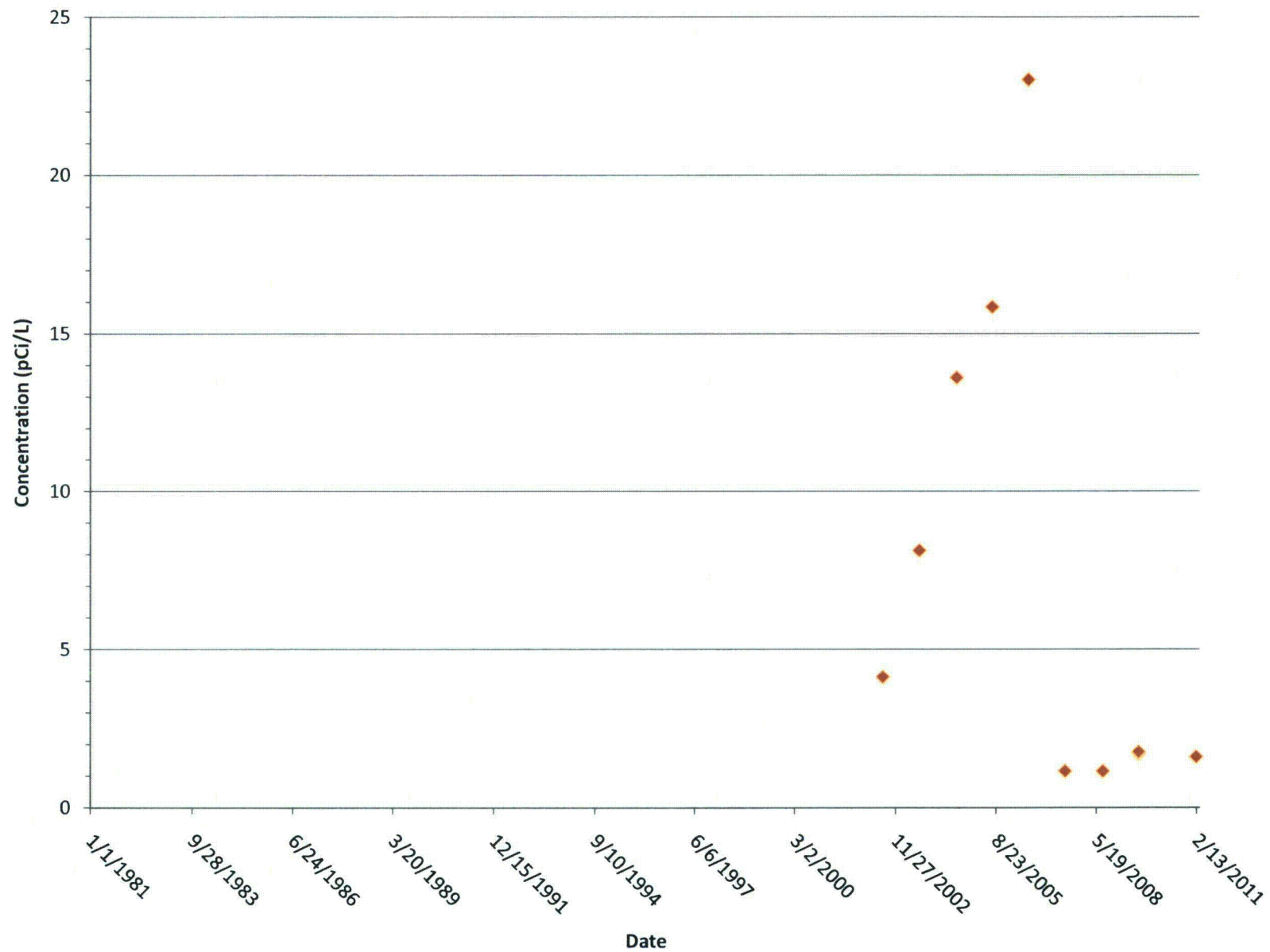
ATTACHMENT I

Temporal plots of
chemical parameters measured
in monitoring wells

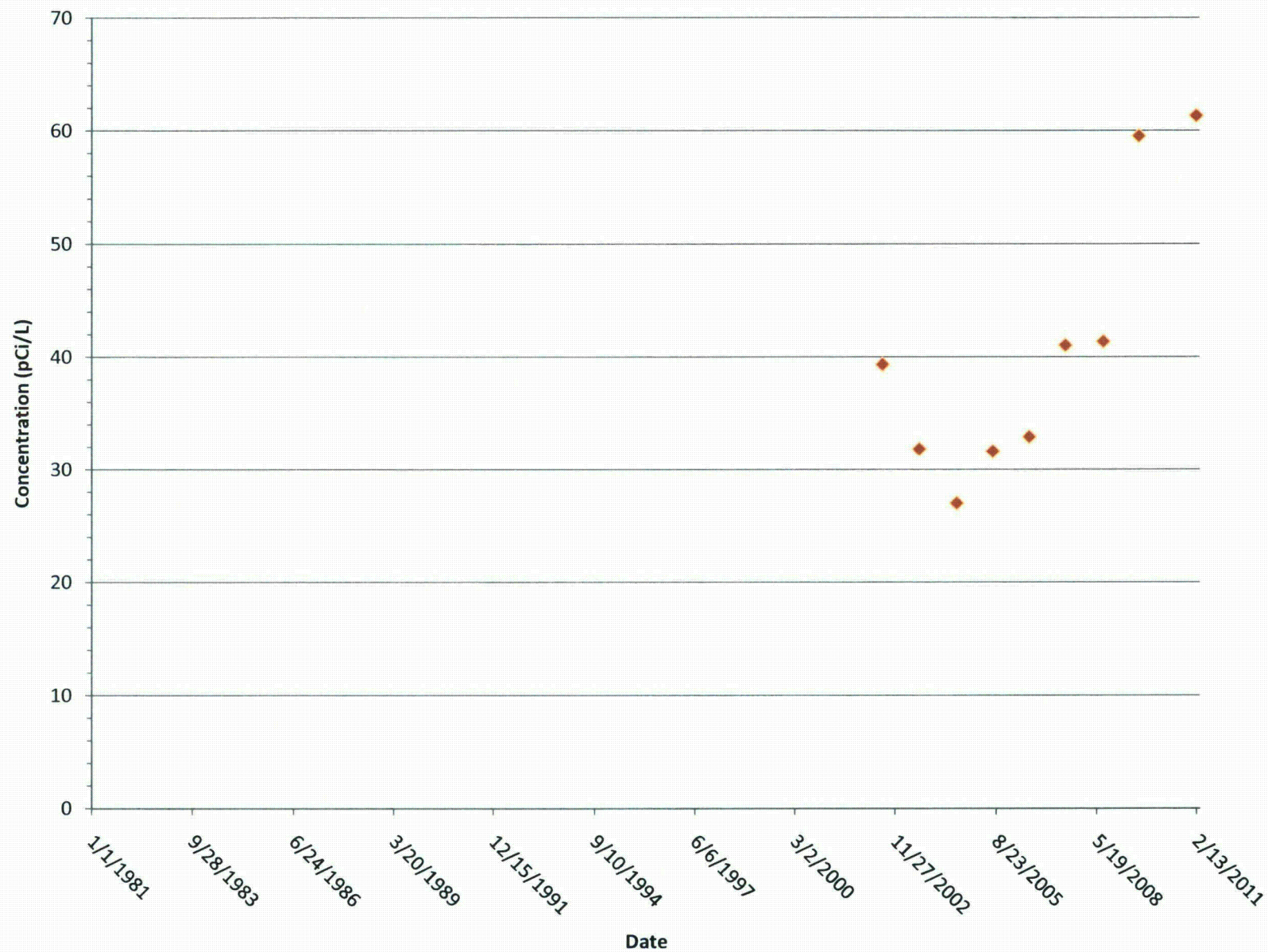
MW-111 Uranium



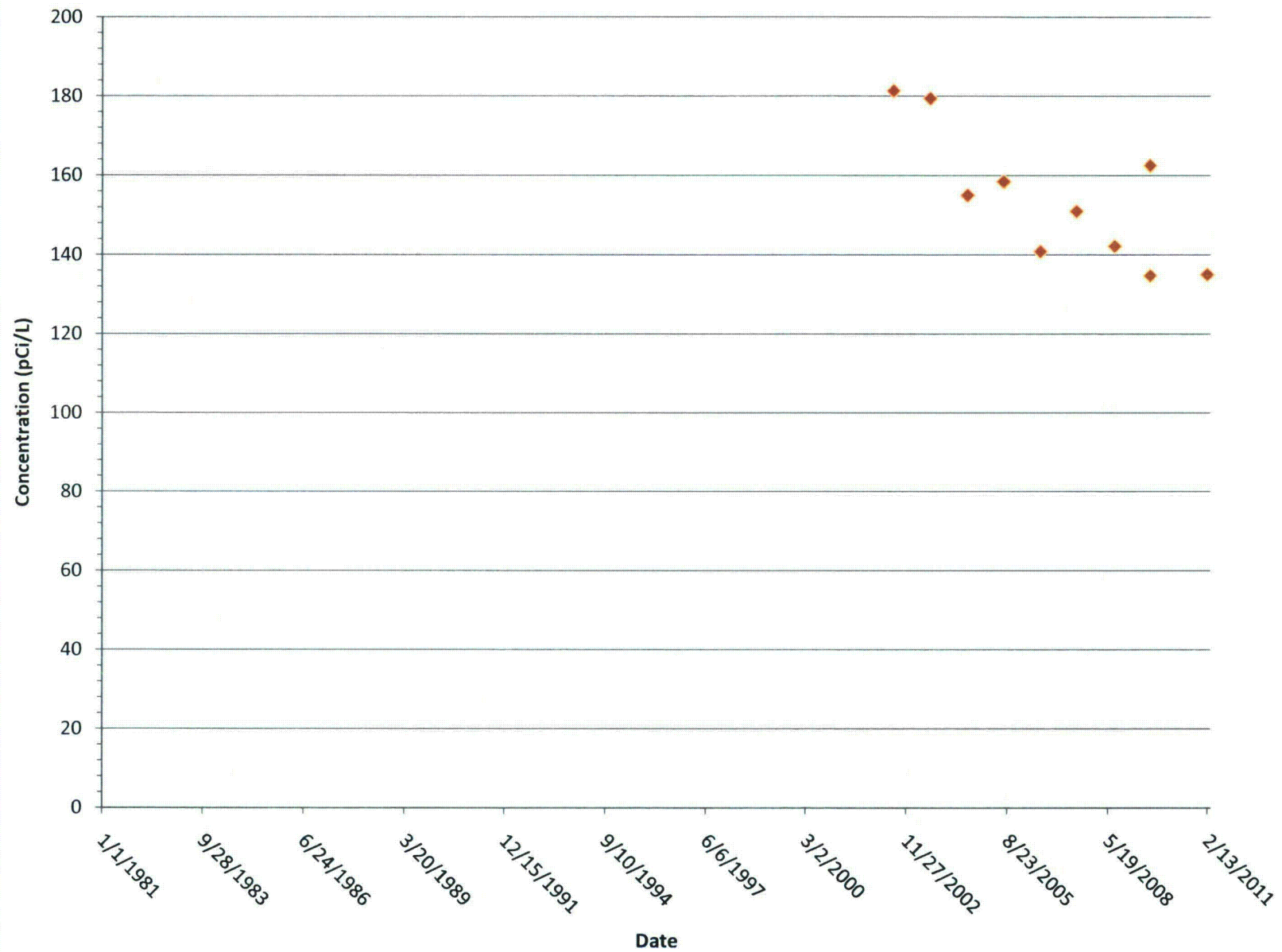
MW-110 Uranium



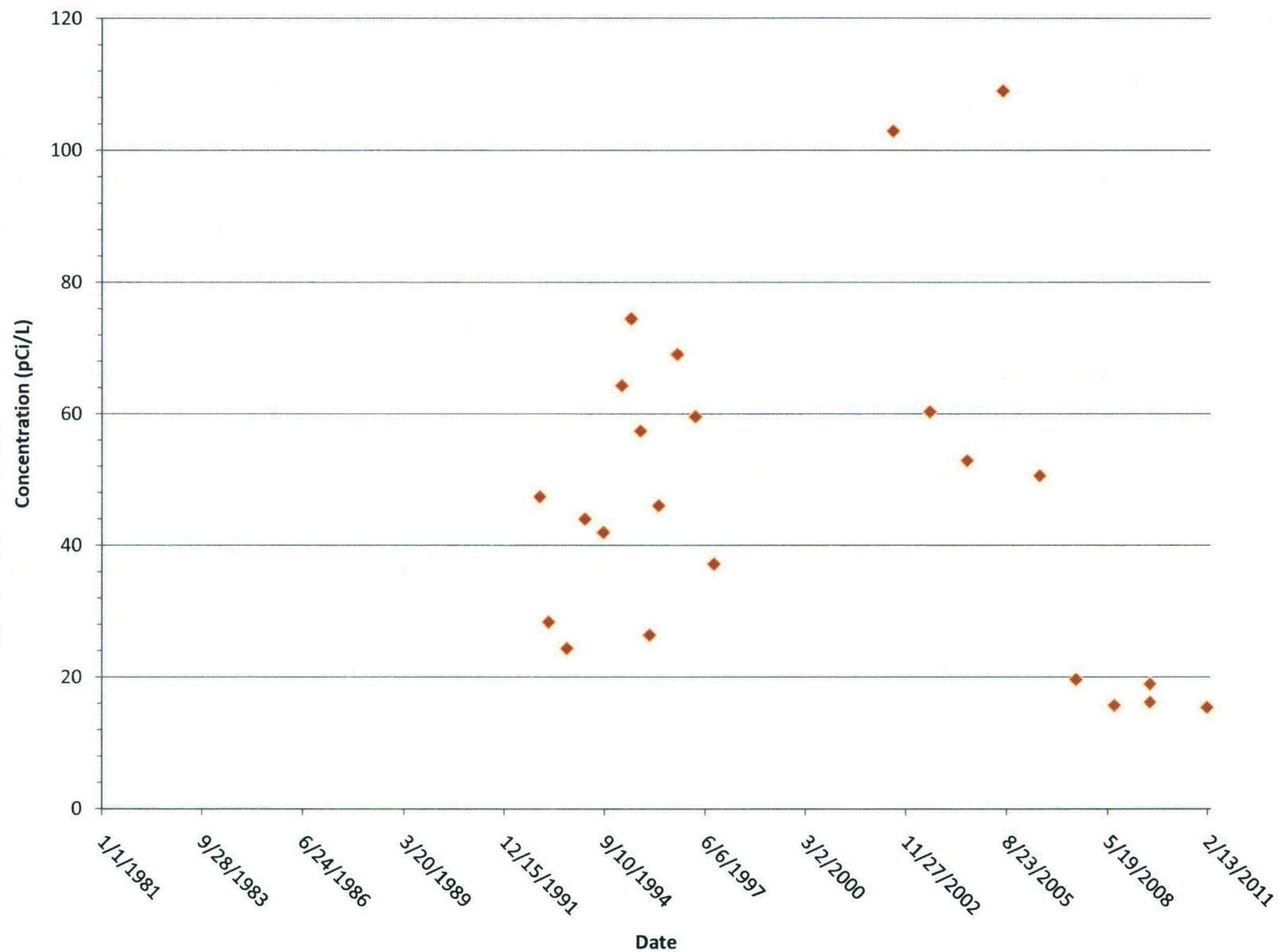
MW-109 Uranium



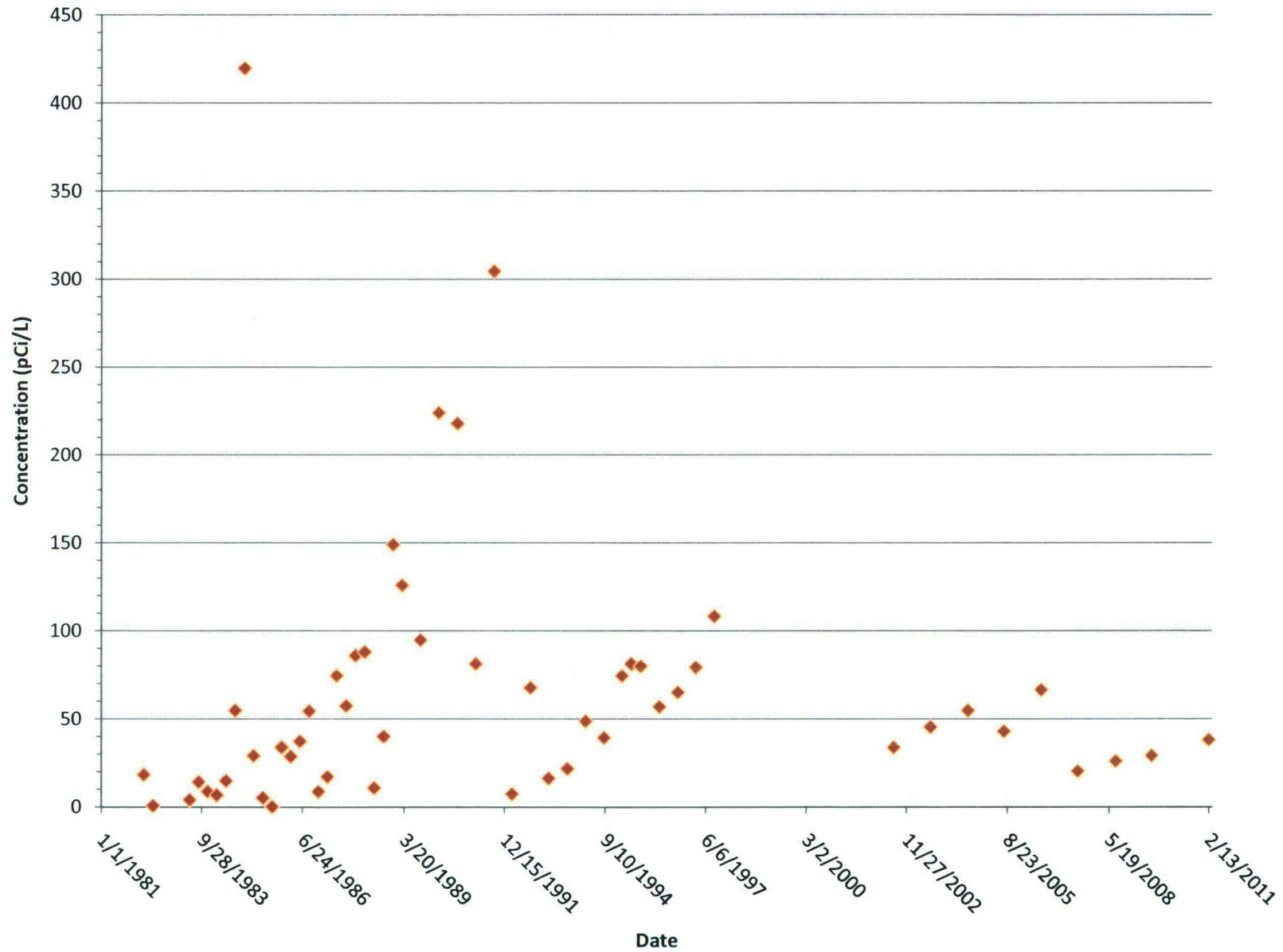
MW-108 Uranium



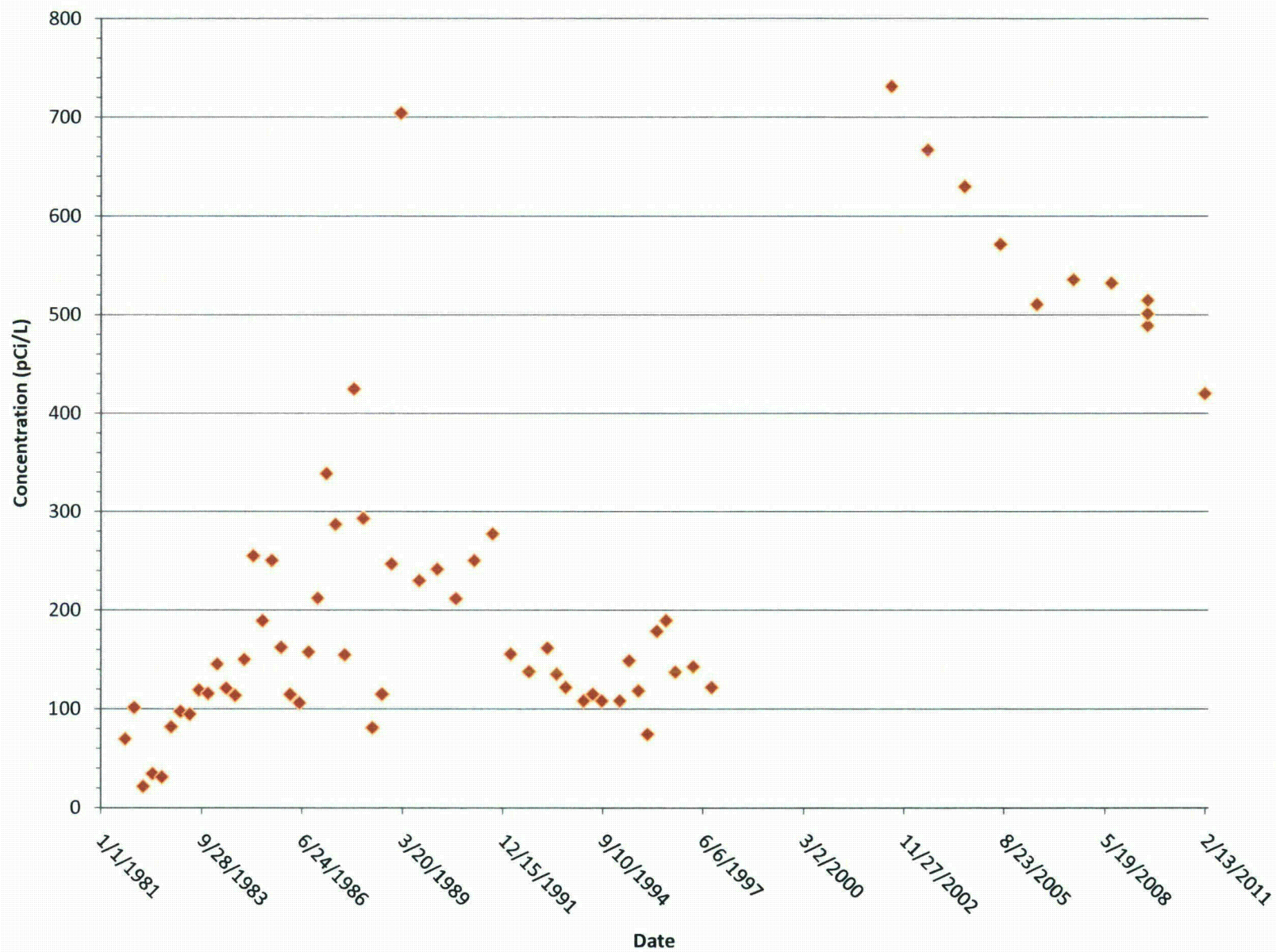
MW-74 Uranium



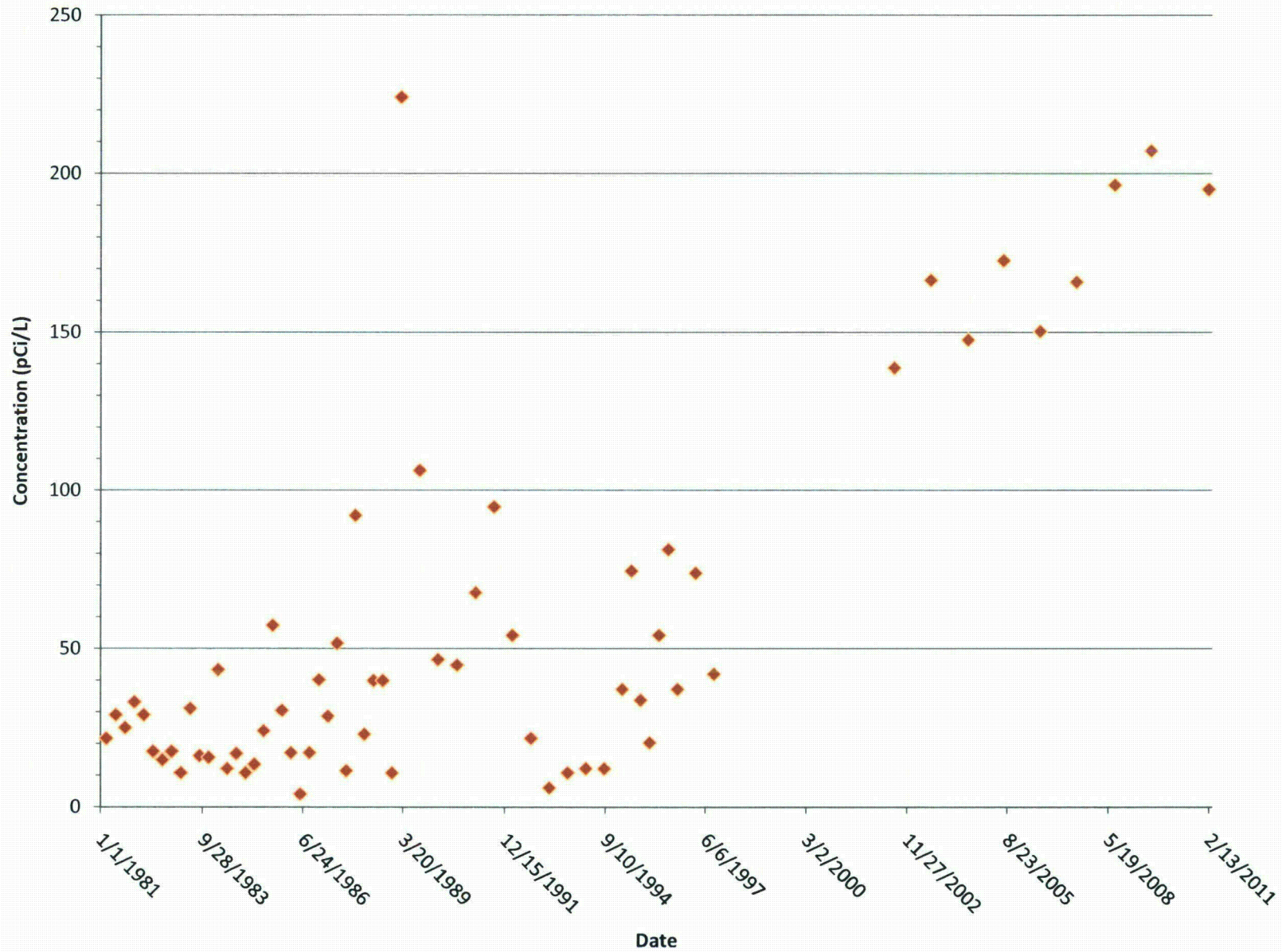
MW-43 Uranium



MW-12 Uranium



MW-9 Uranium

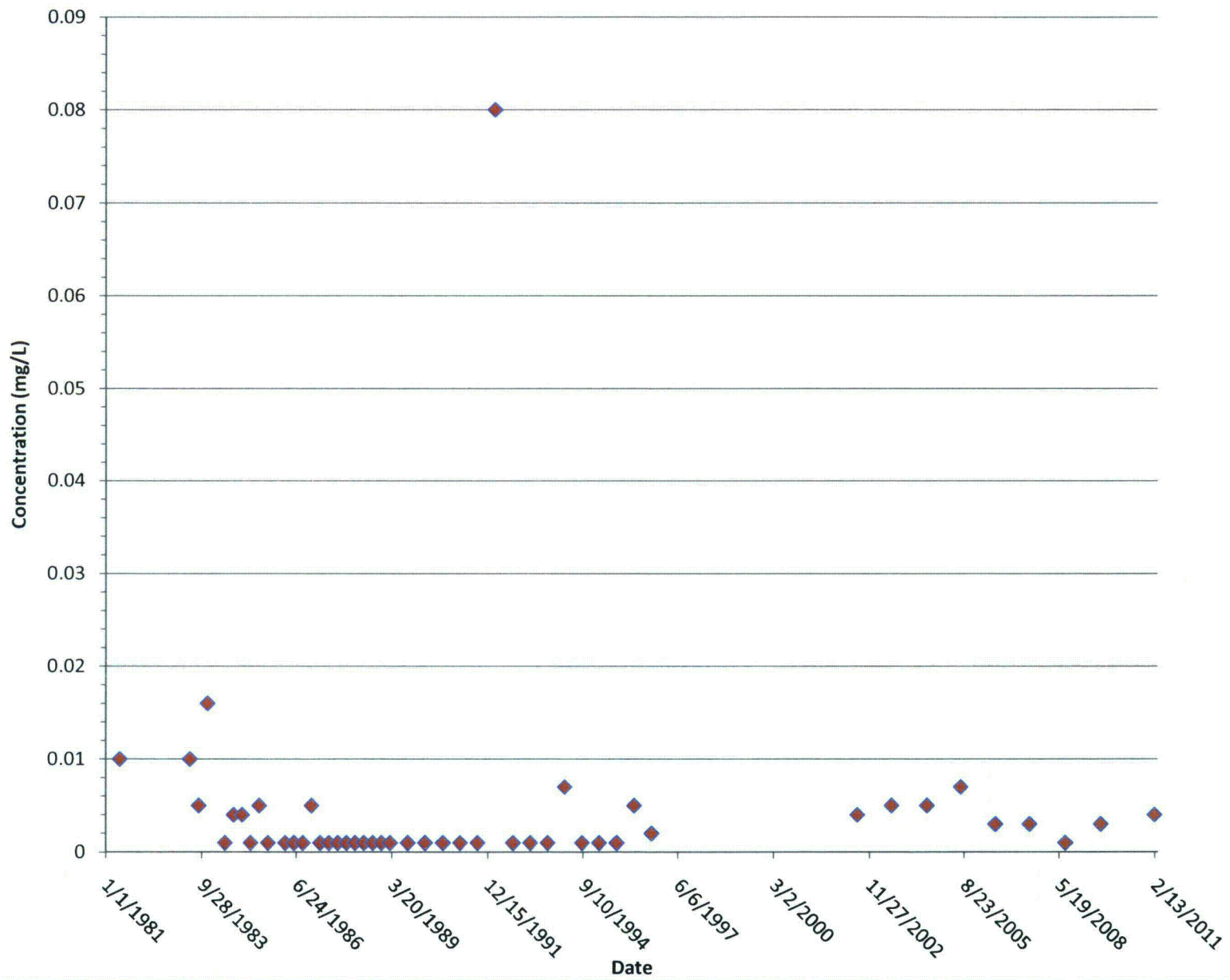


[illegible]

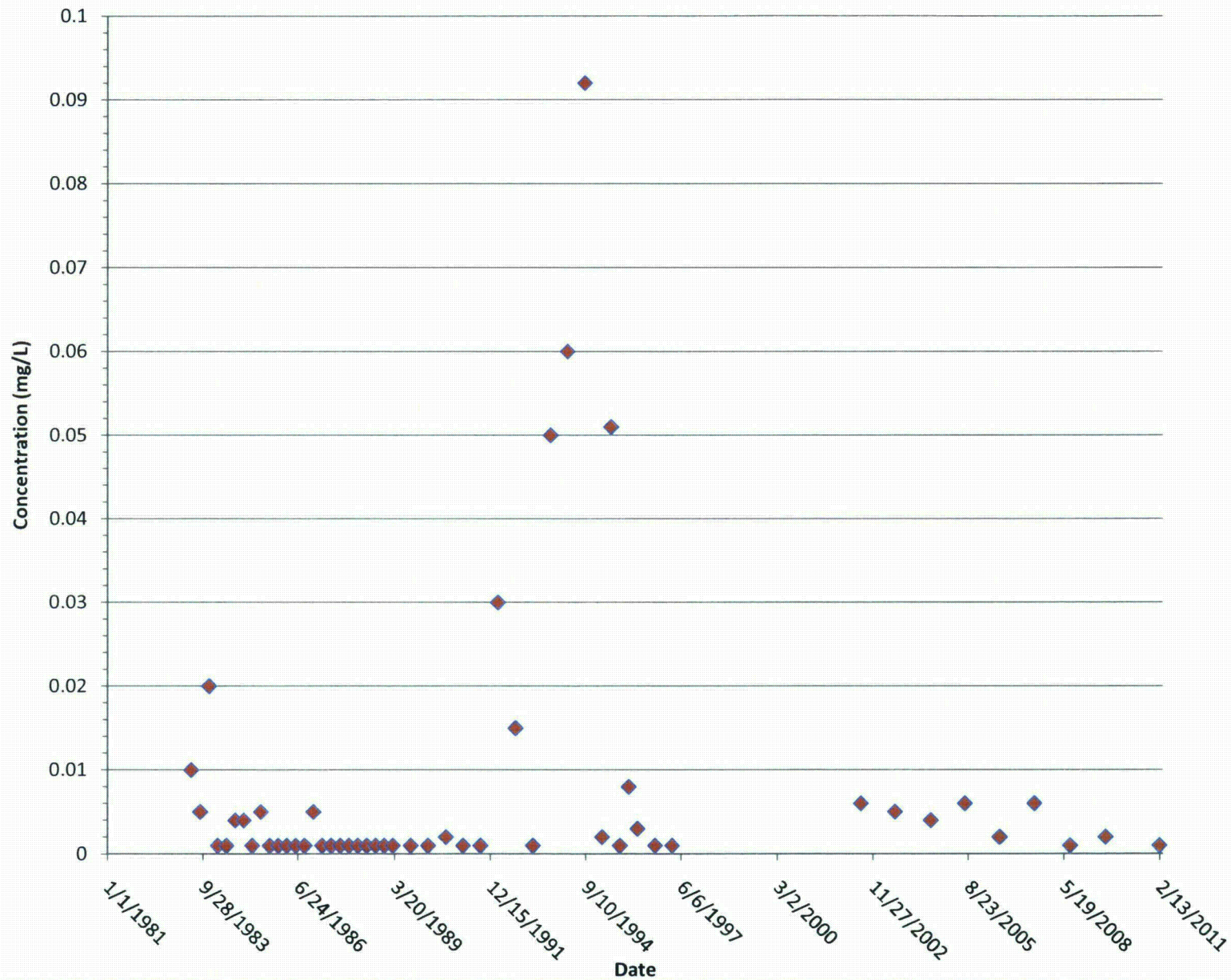
Concentration (mg/L)

Date _____

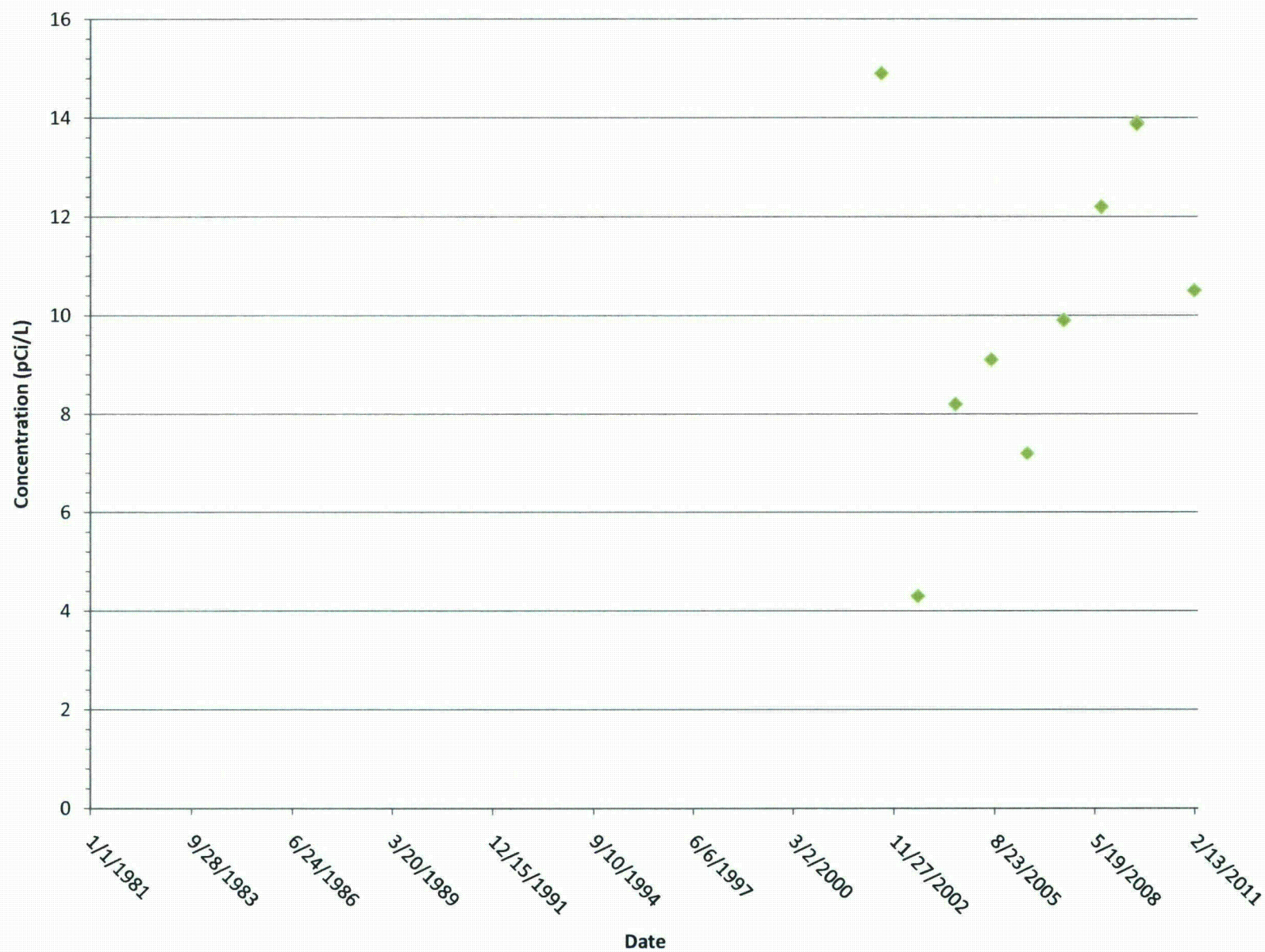
MW-14 Selenium



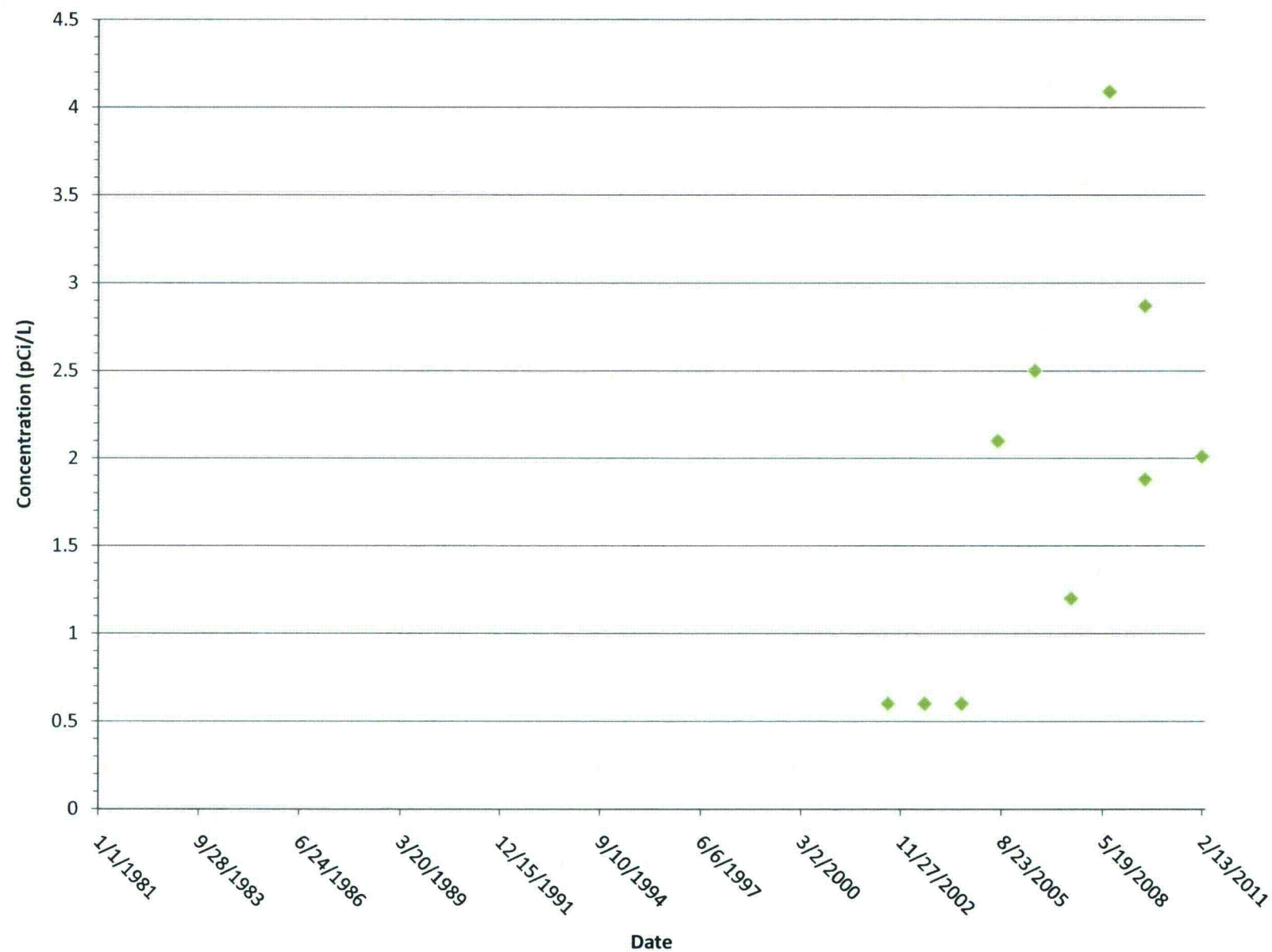
MW-9 Selenium



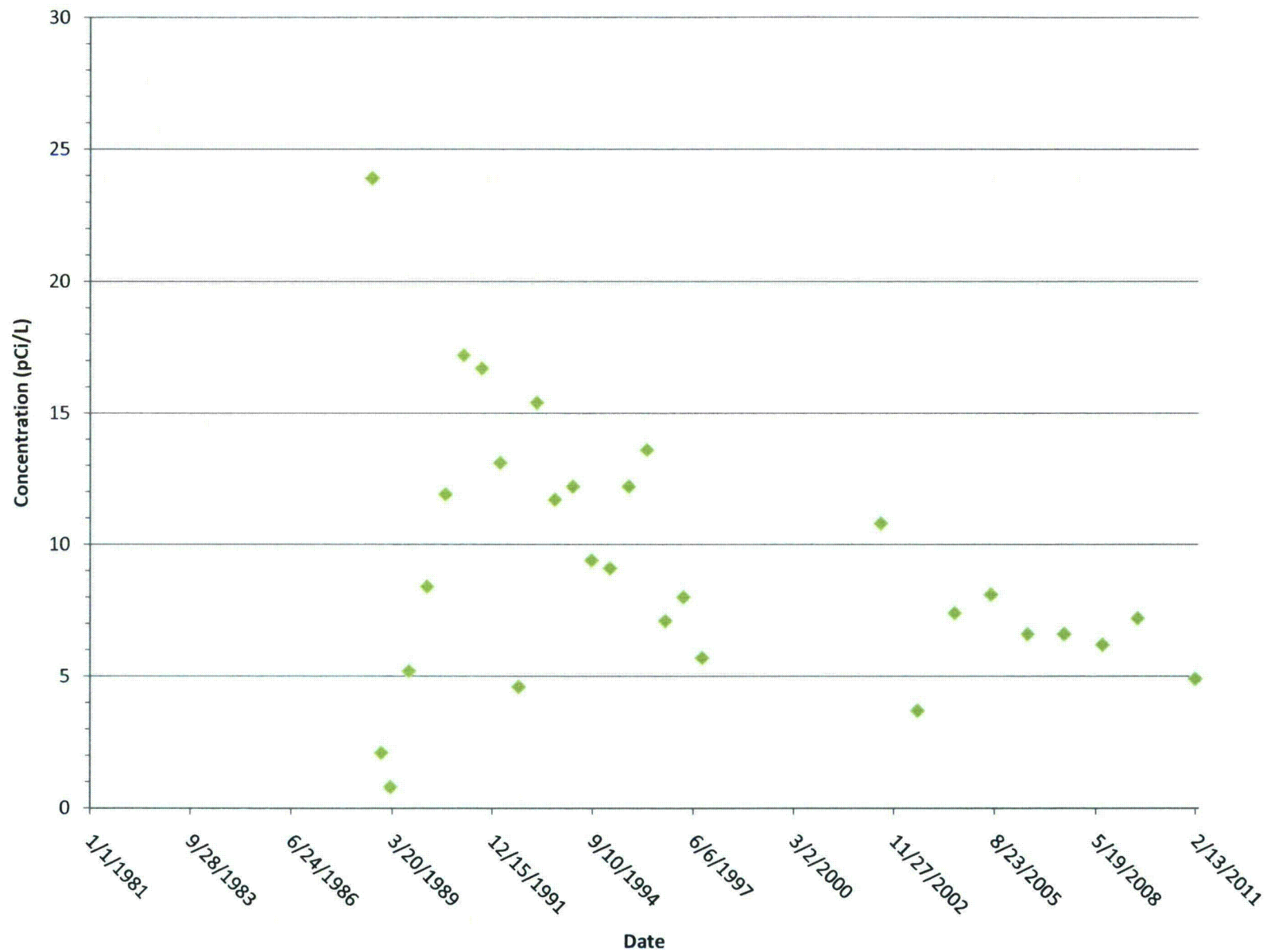
MW-110 Combined Radium 226 and 228



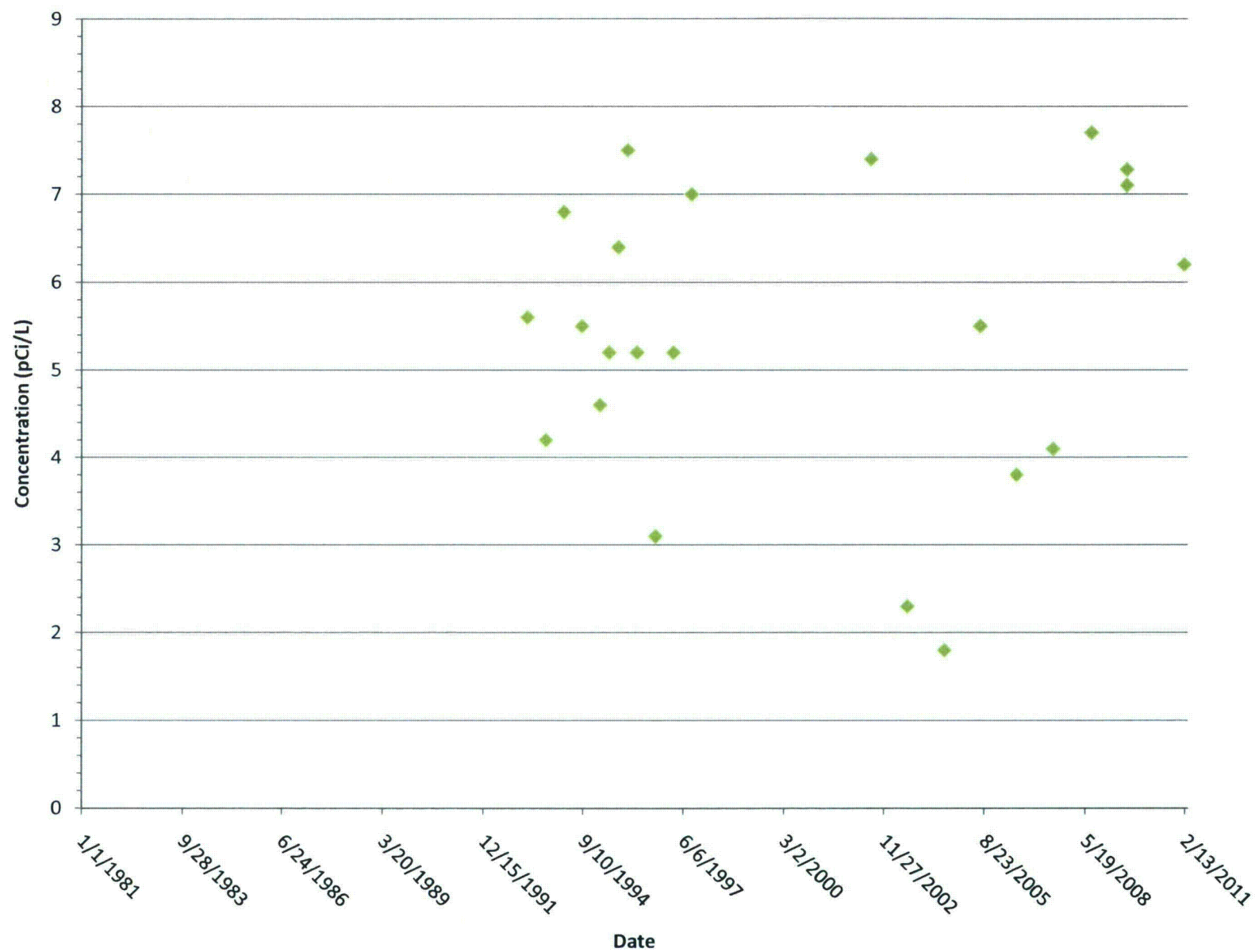
MW-108 Combined Radium 226 and 228



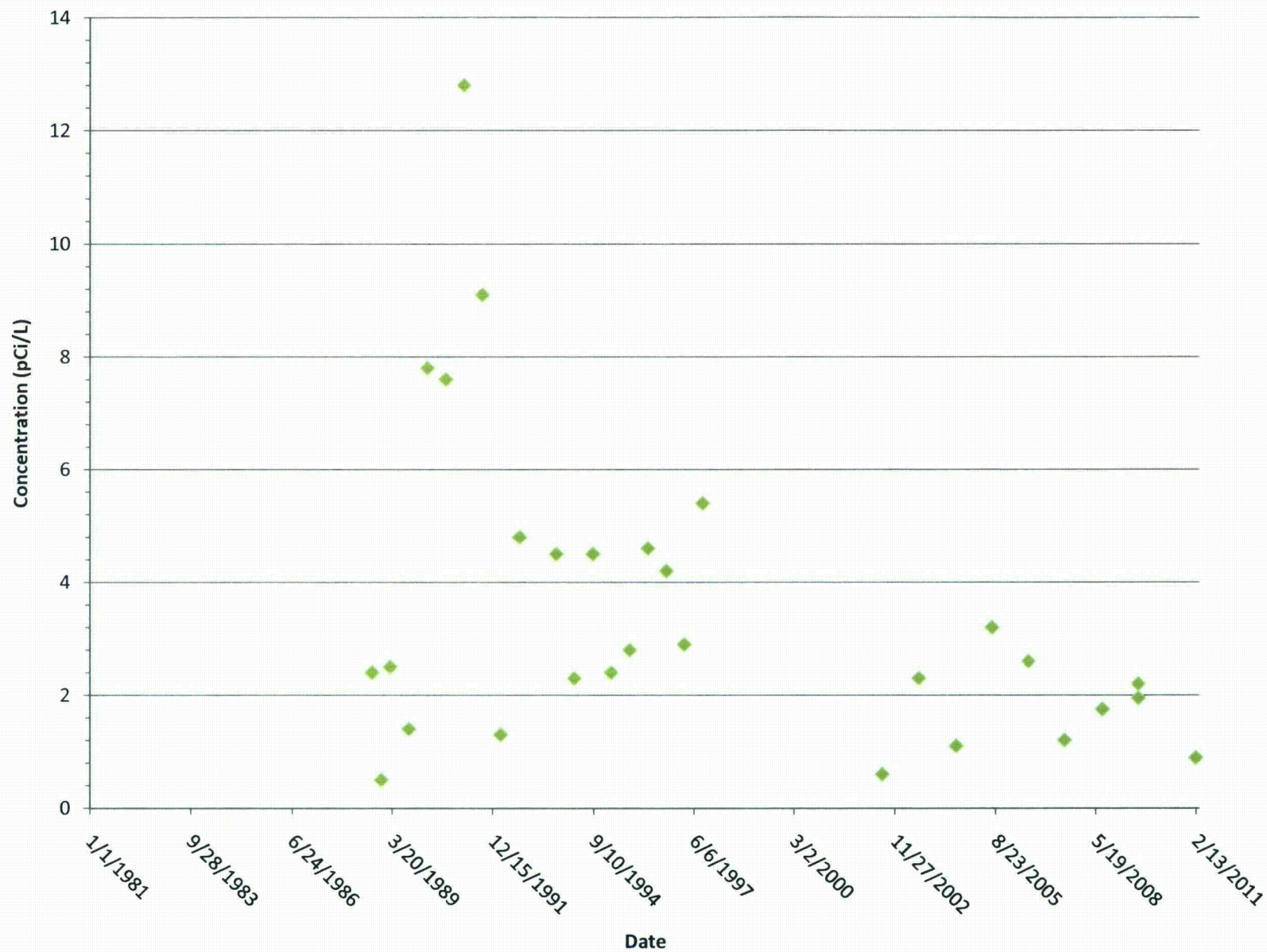
MW-43 Combined Radium 226 and 228



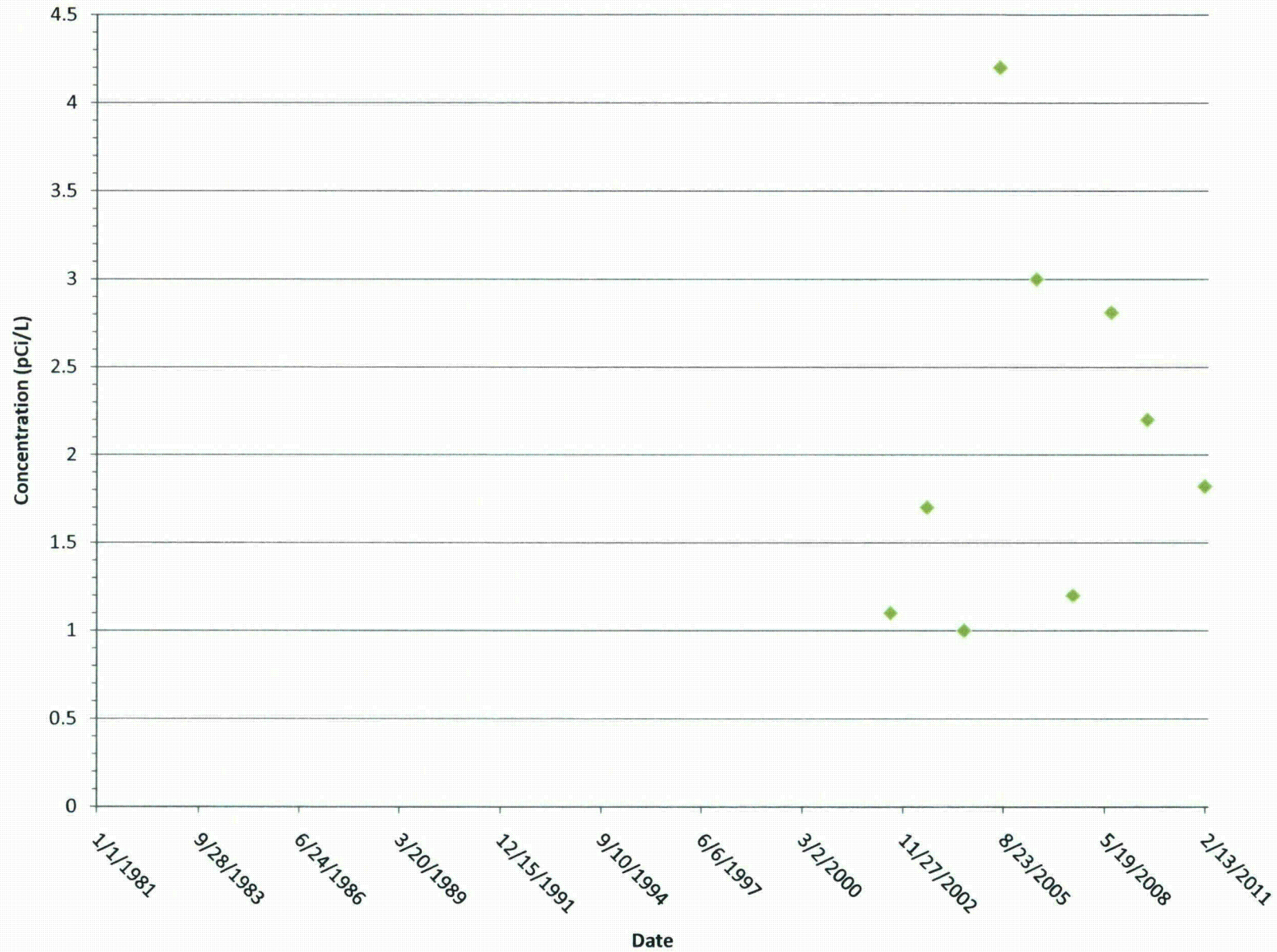
MW-74 Combined Radium 226 and 228



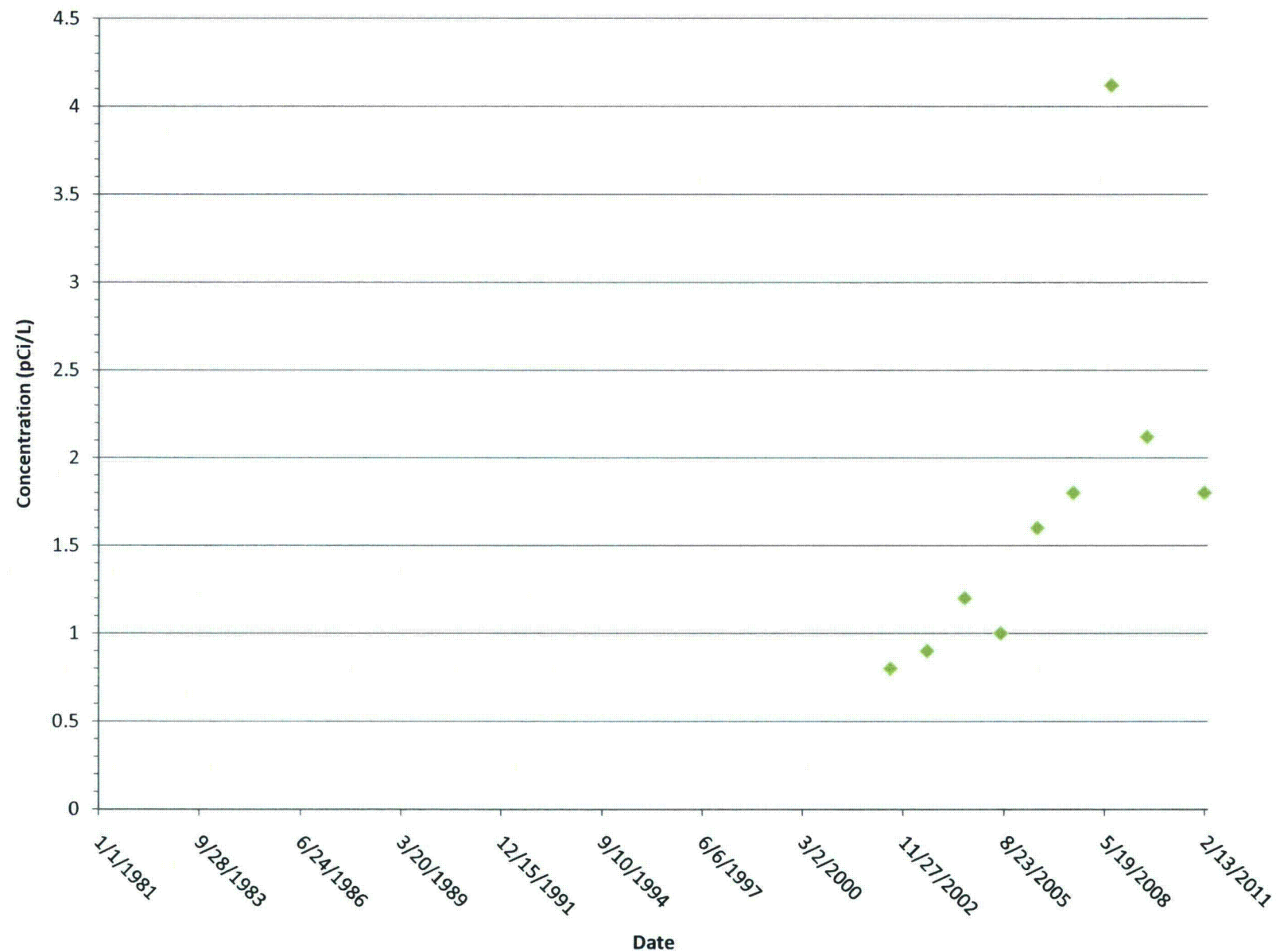
MW-14 Combined Radium 226 and 228



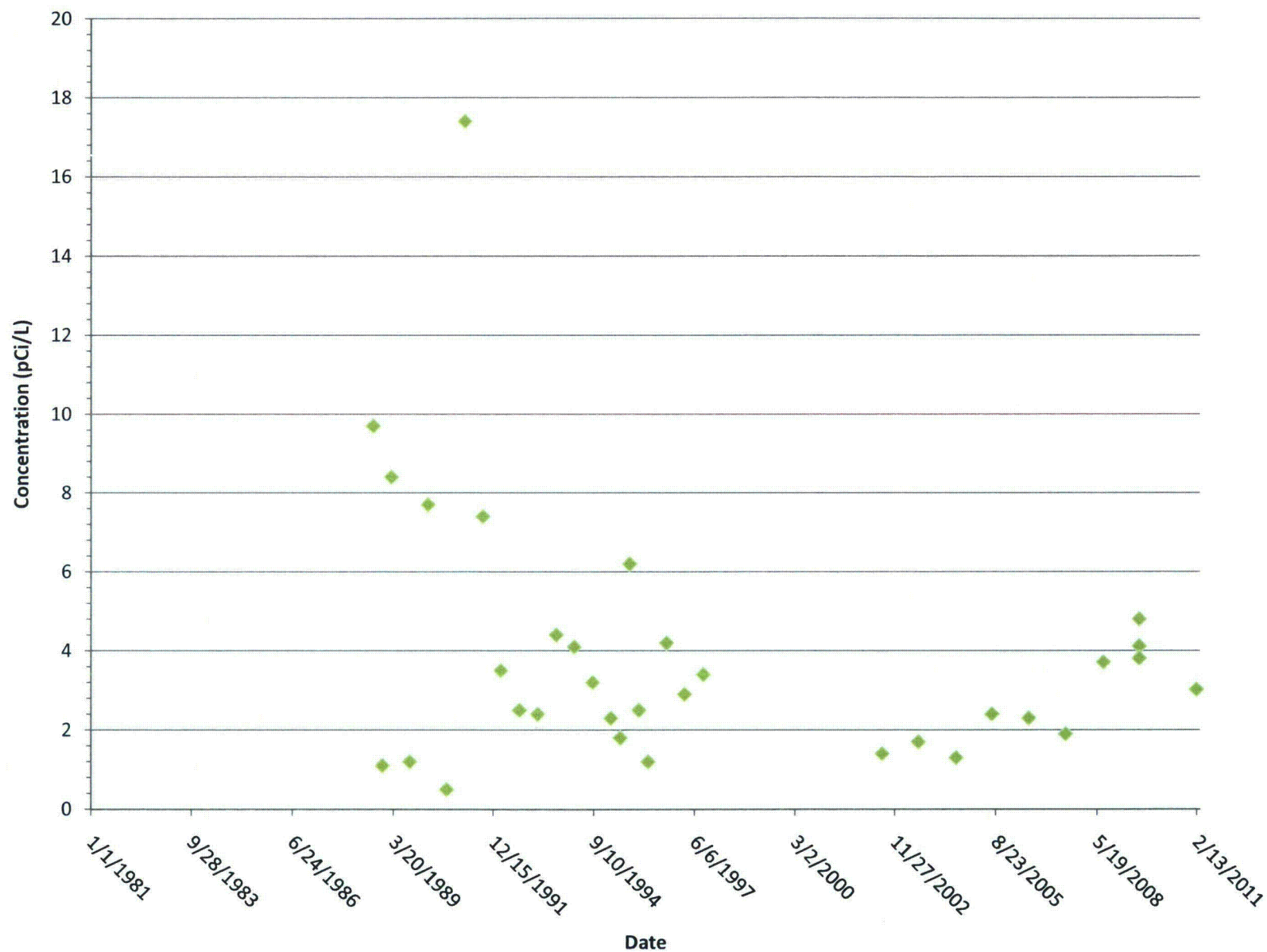
MW-111 Combined Radium 226 and 228



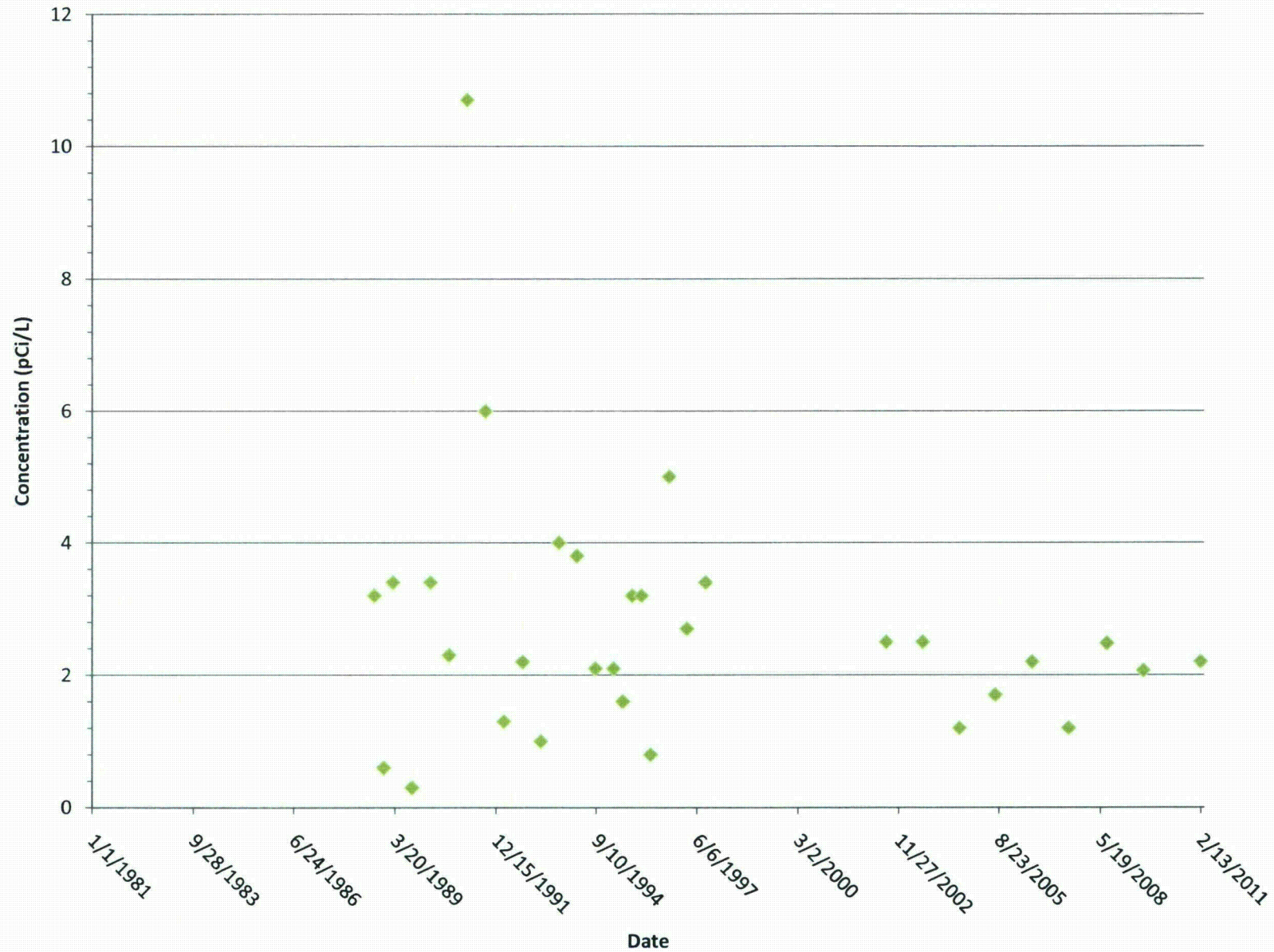
MW-109 Combined Radium 226 and 228



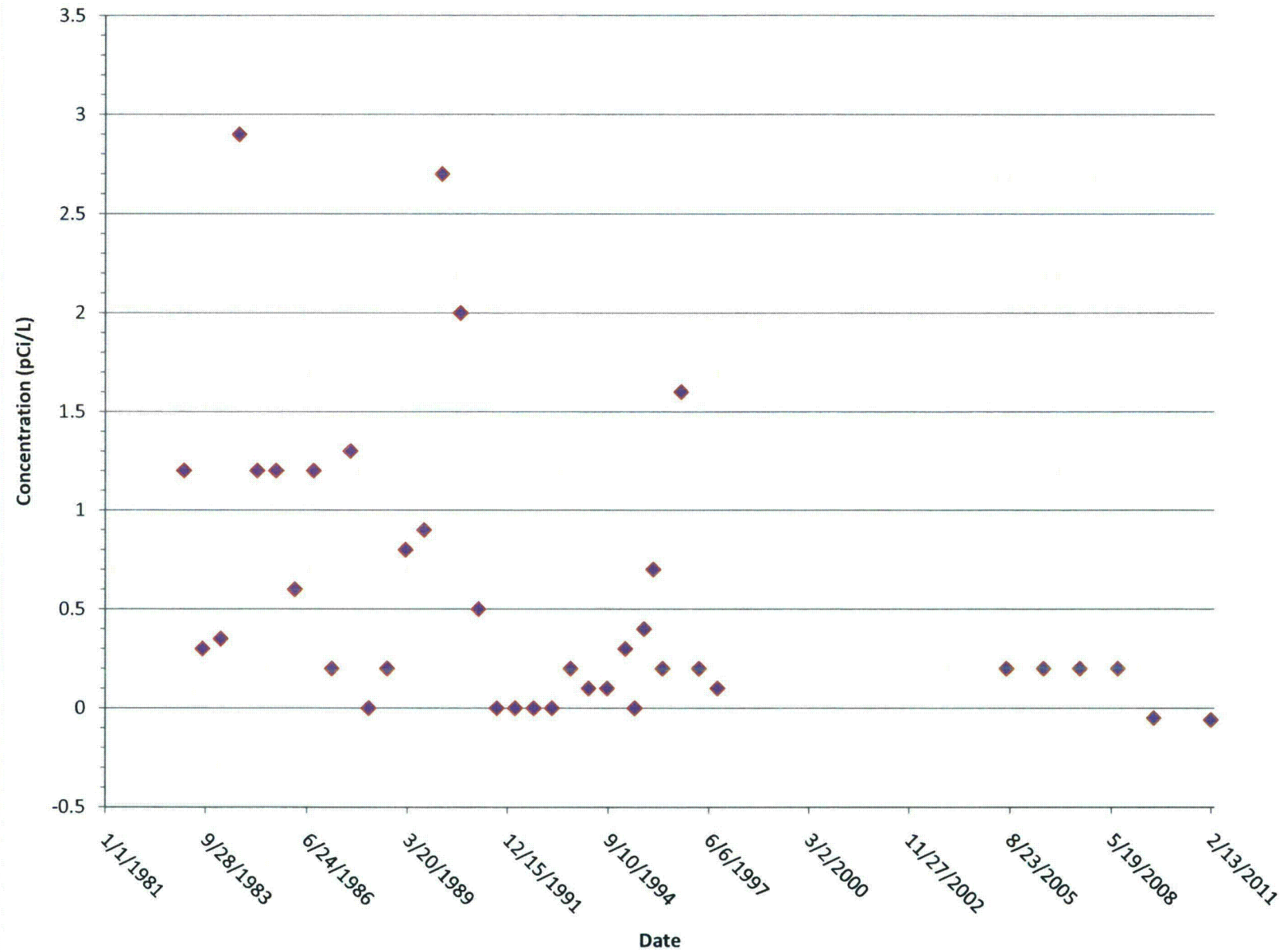
MW-12 Combined Radium 226 and 228



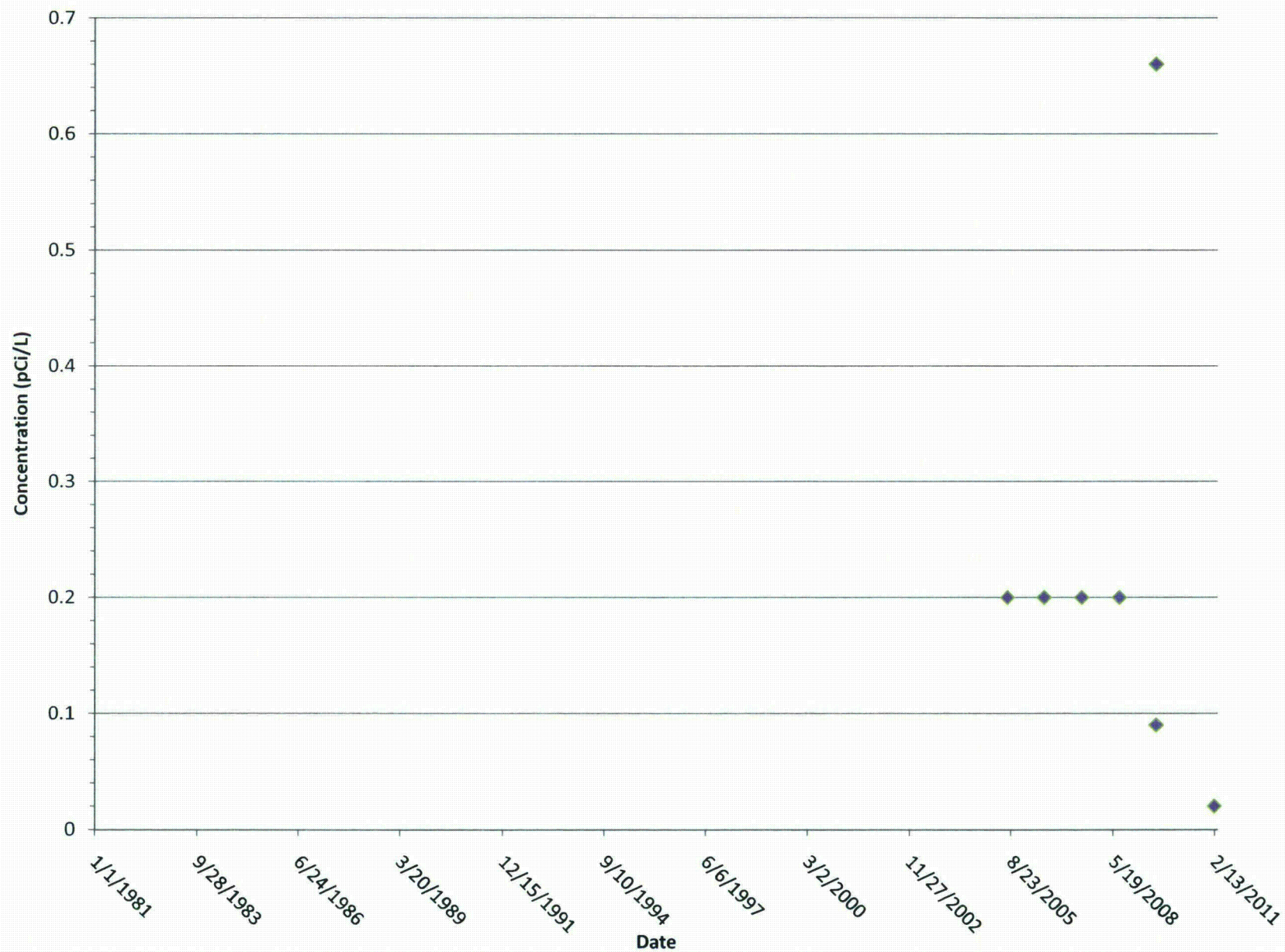
MW-9 Combined Radium 226 and 228



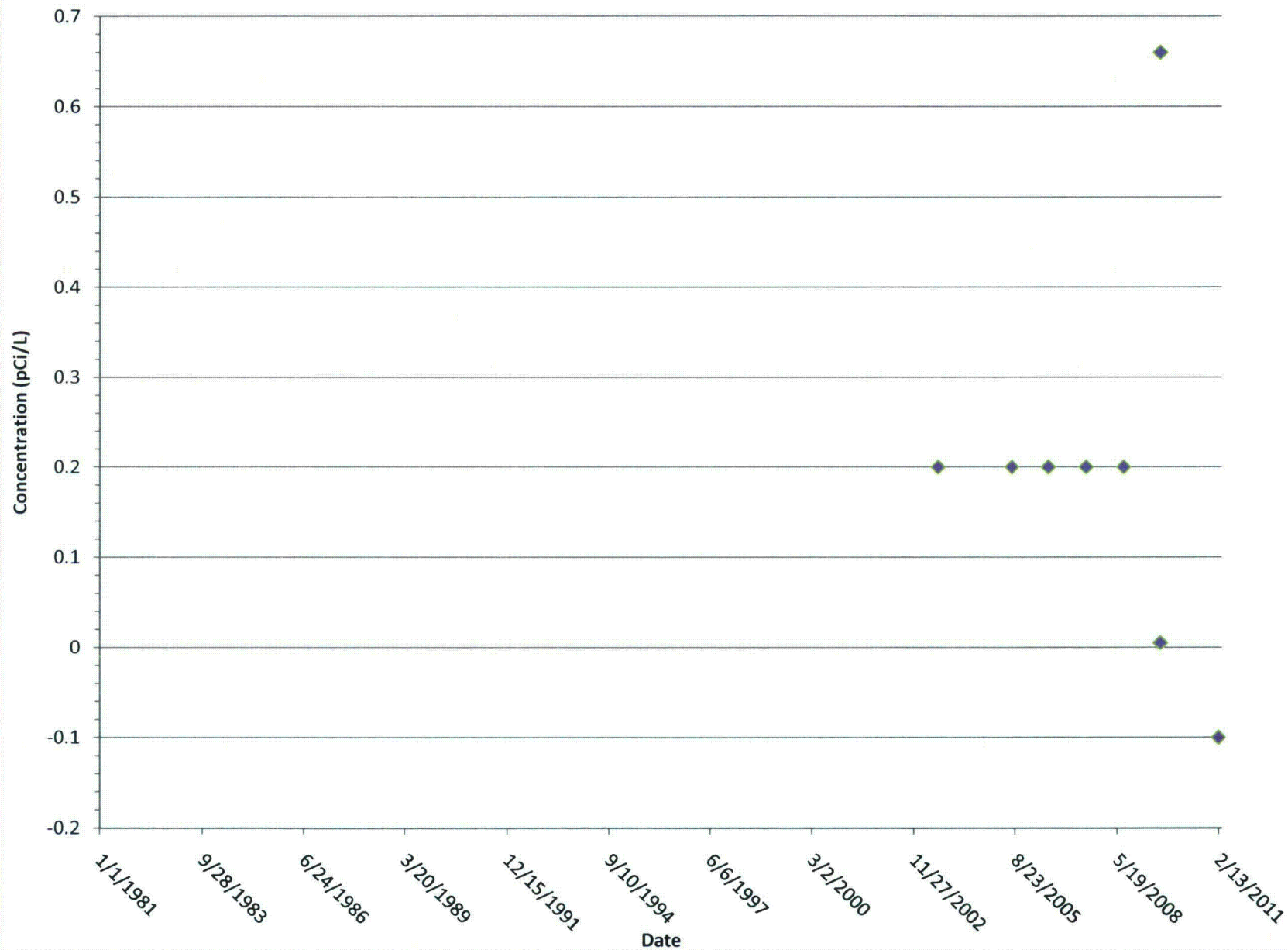
MW-9 Thorium 230



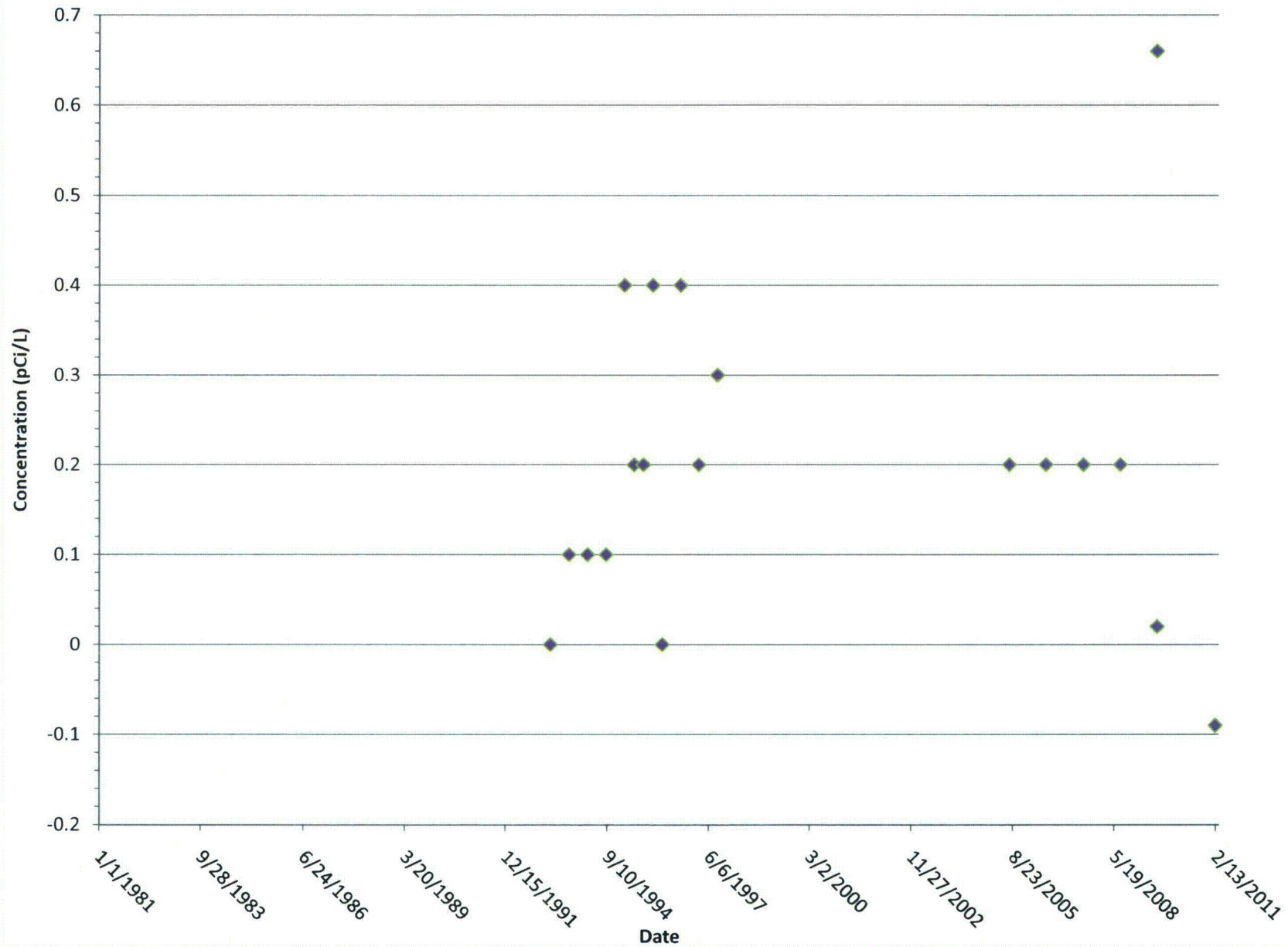
MW-110 Thorium 230



MW-108 Thorium 230



MW-74 Thorium 230



MW-43 Thorium 230

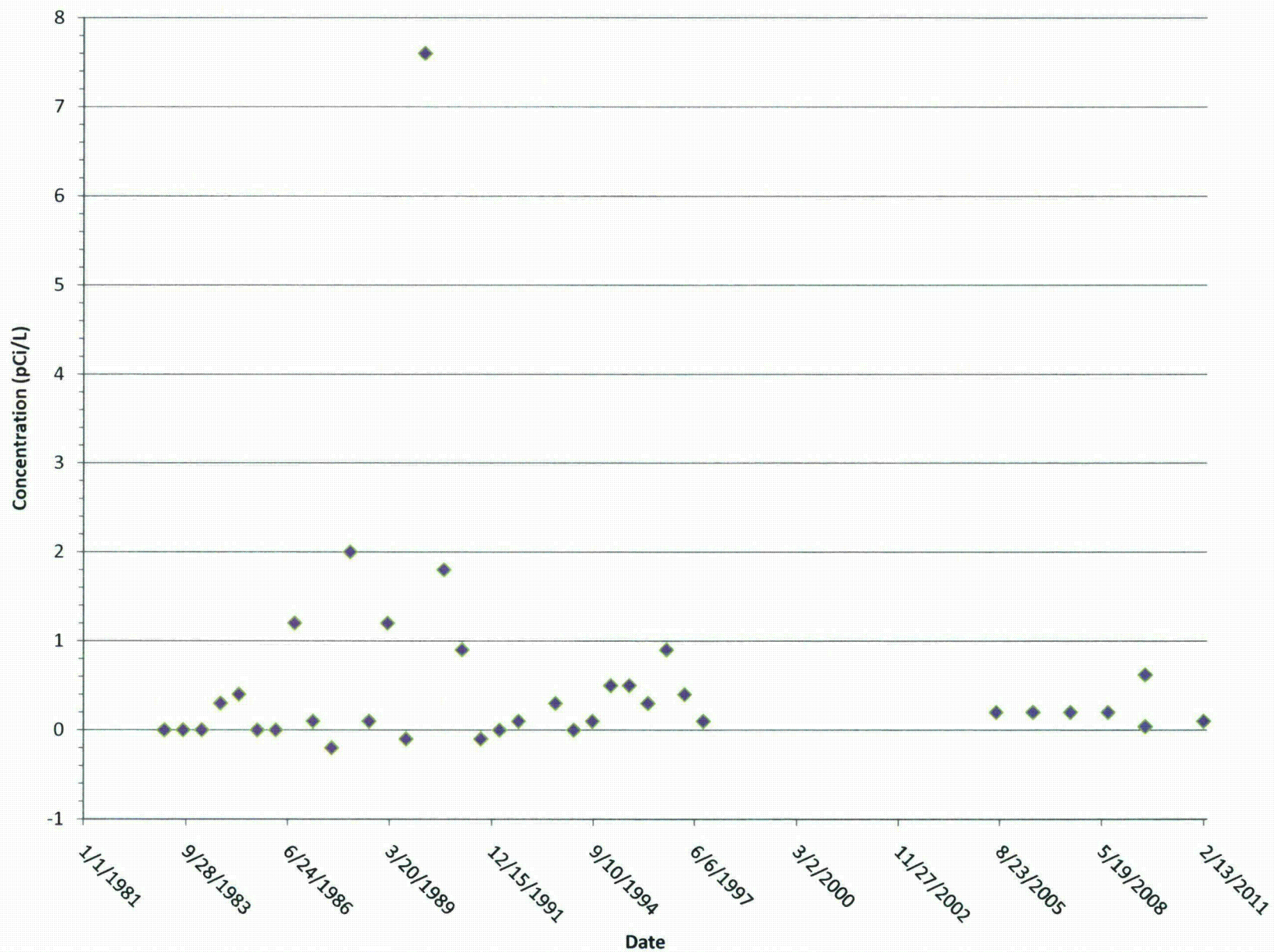
Concentration (pCi/L)

Date

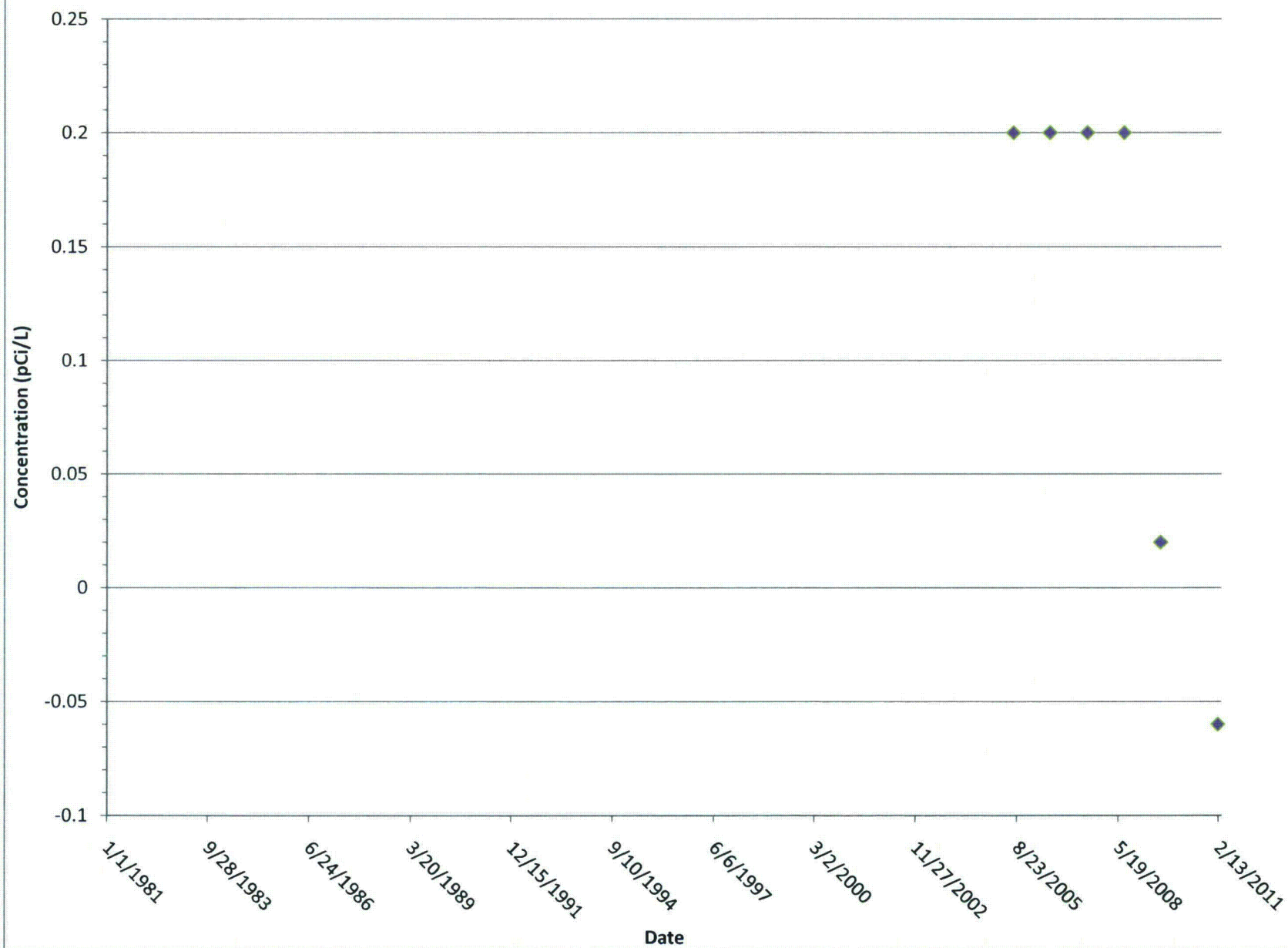
Date	Concentration (pCi/L)
1/1/1981	9.5
9/28/1983	5.8
6/24/1986	9.0
3/20/1989	3.5
12/15/1991	0.1
9/10/1994	1.4
6/6/1997	-0.2
8/23/2005	0.2
5/19/2008	0.2
2/13/2011	-0.1

Date _____

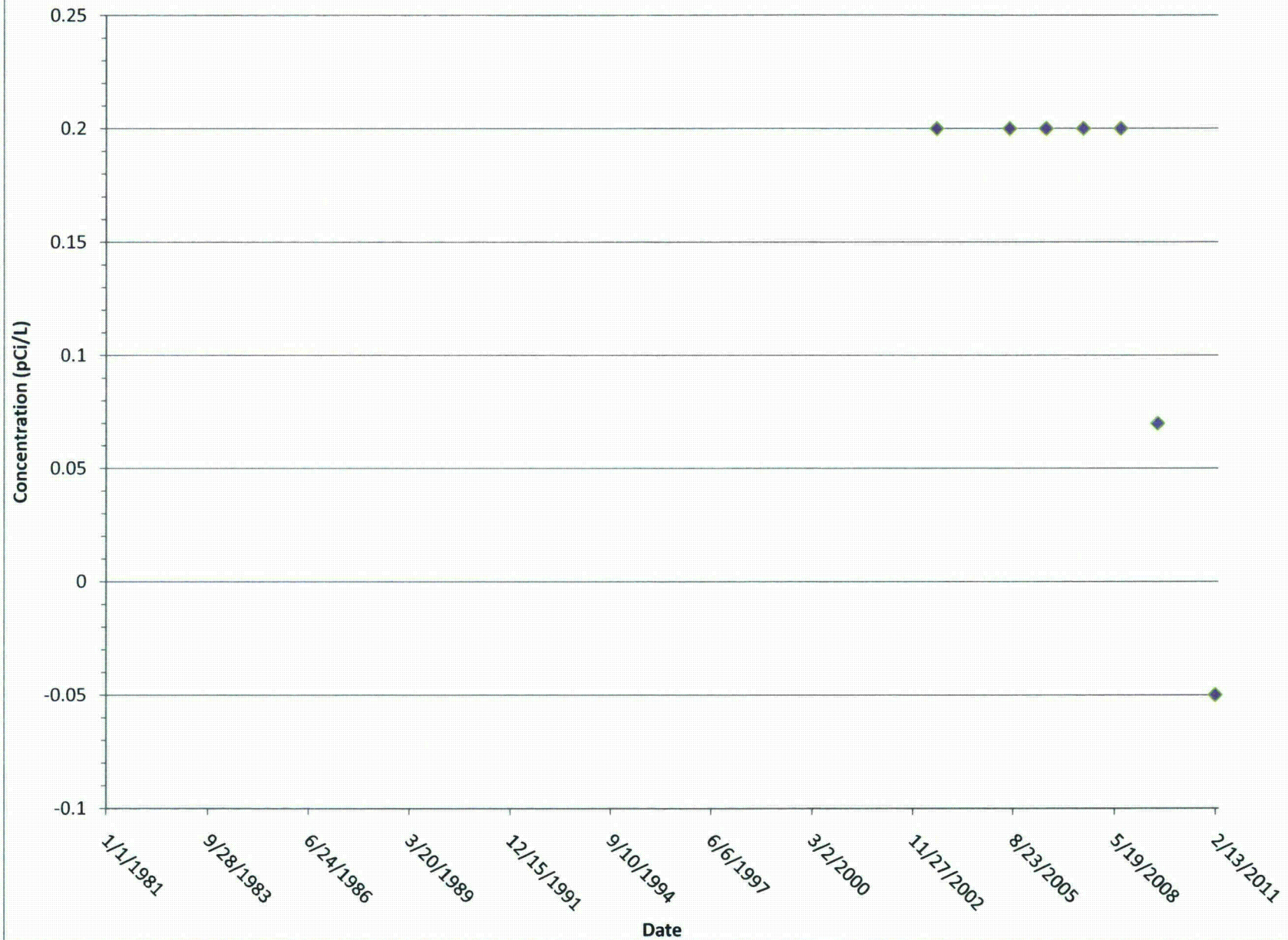
MW-14 Thorium 230



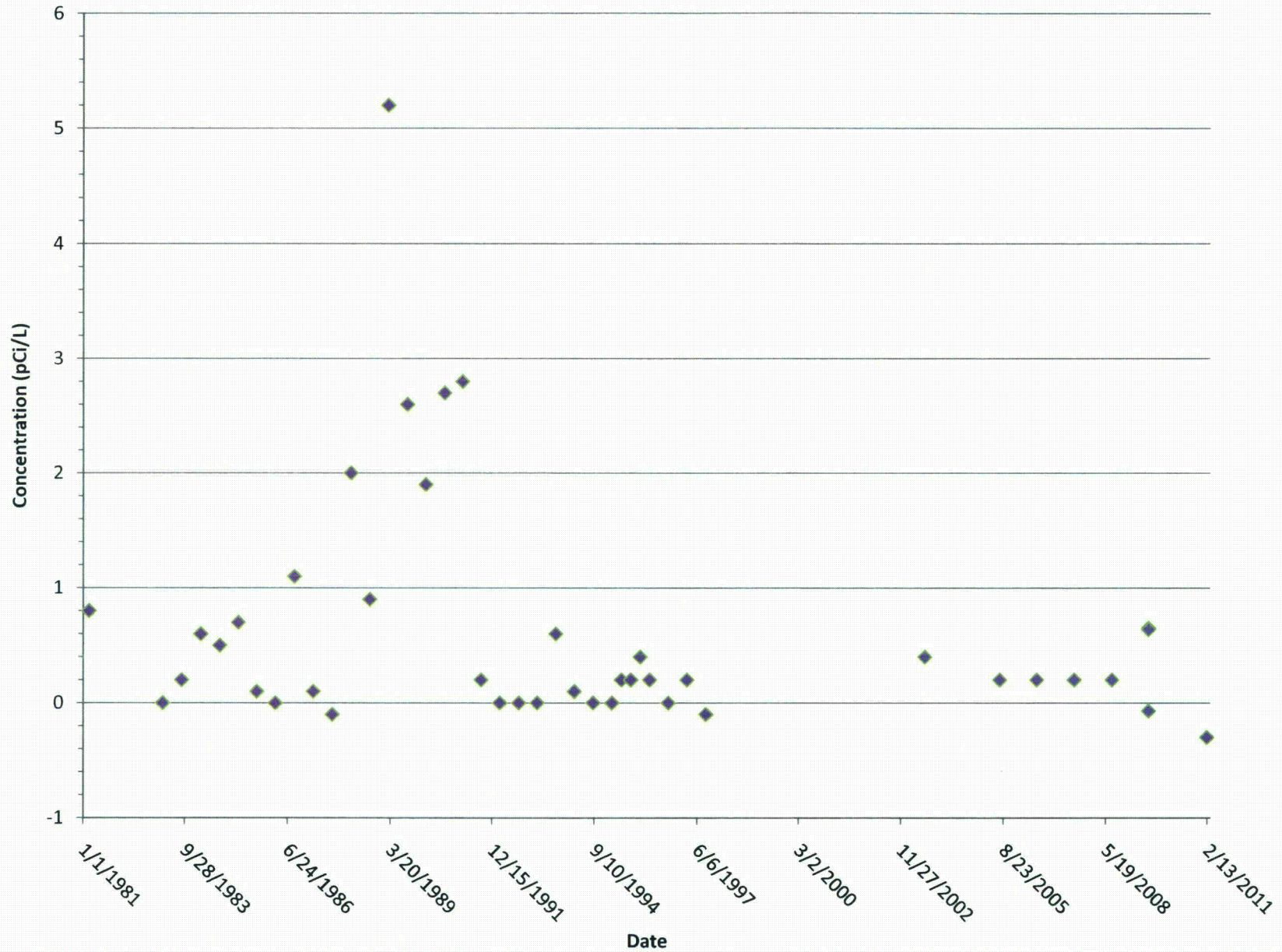
MW-111 Thorium 230



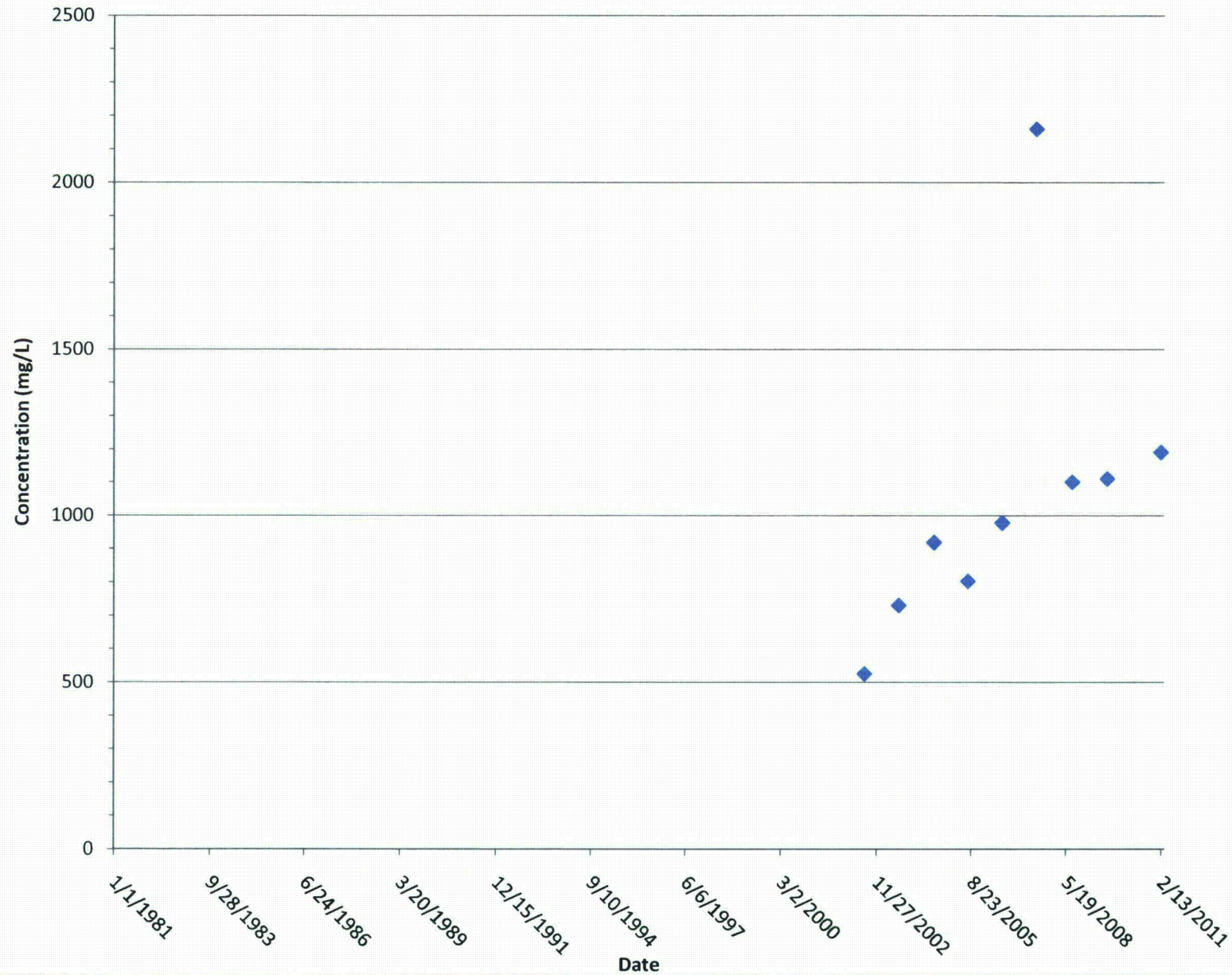
MW-109 Thorium 230



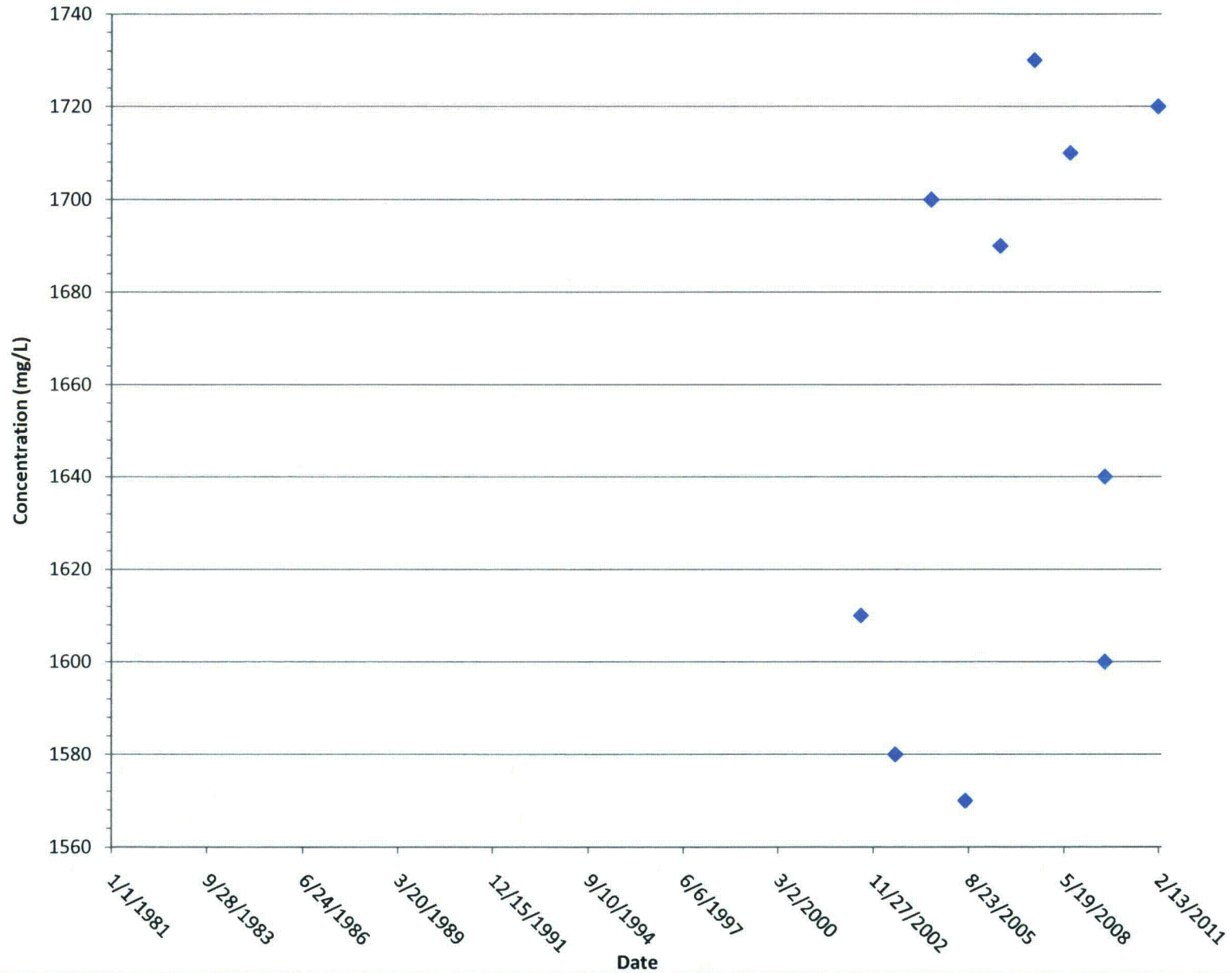
MW-12 Thorium 230



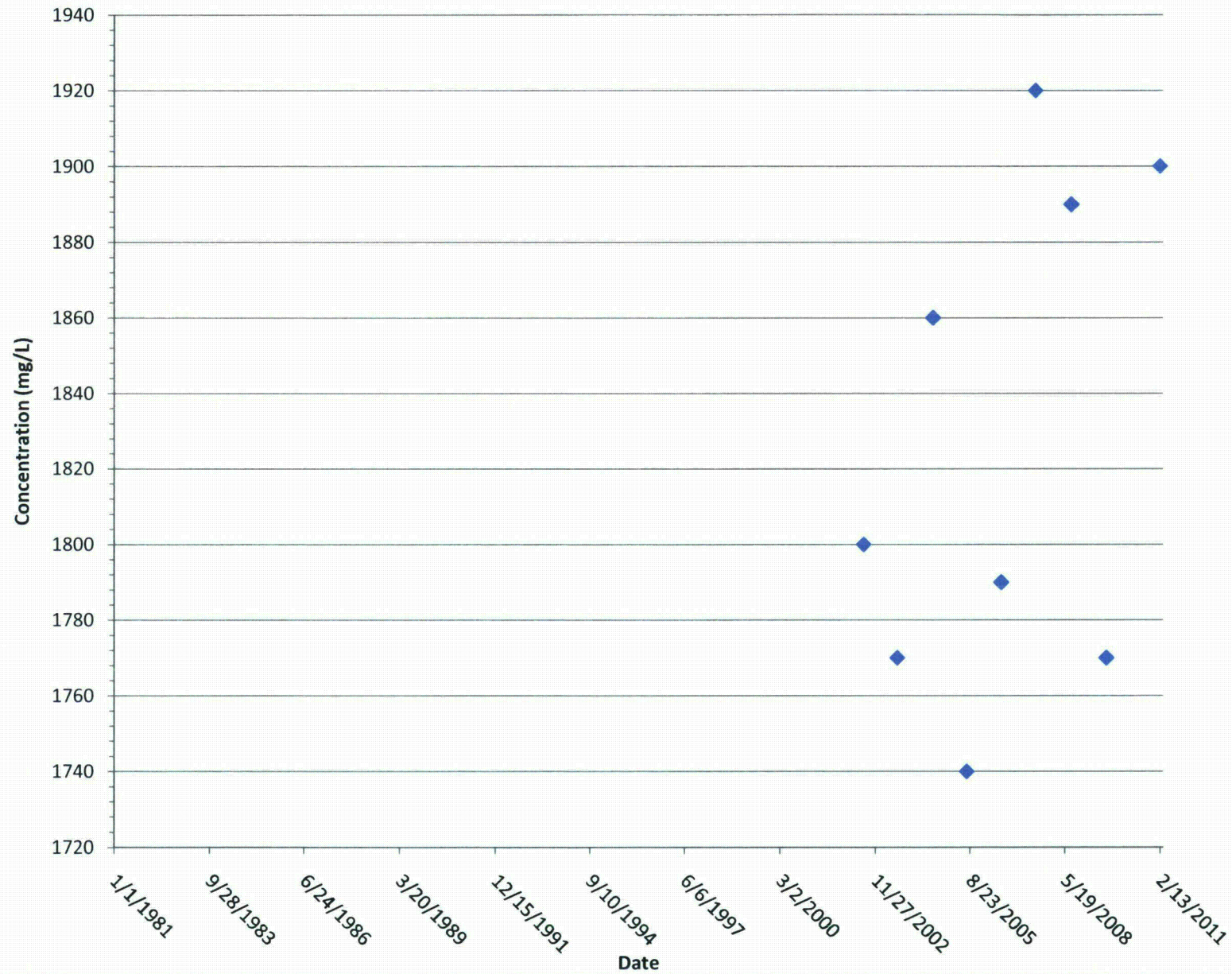
MW-111 Sulfate



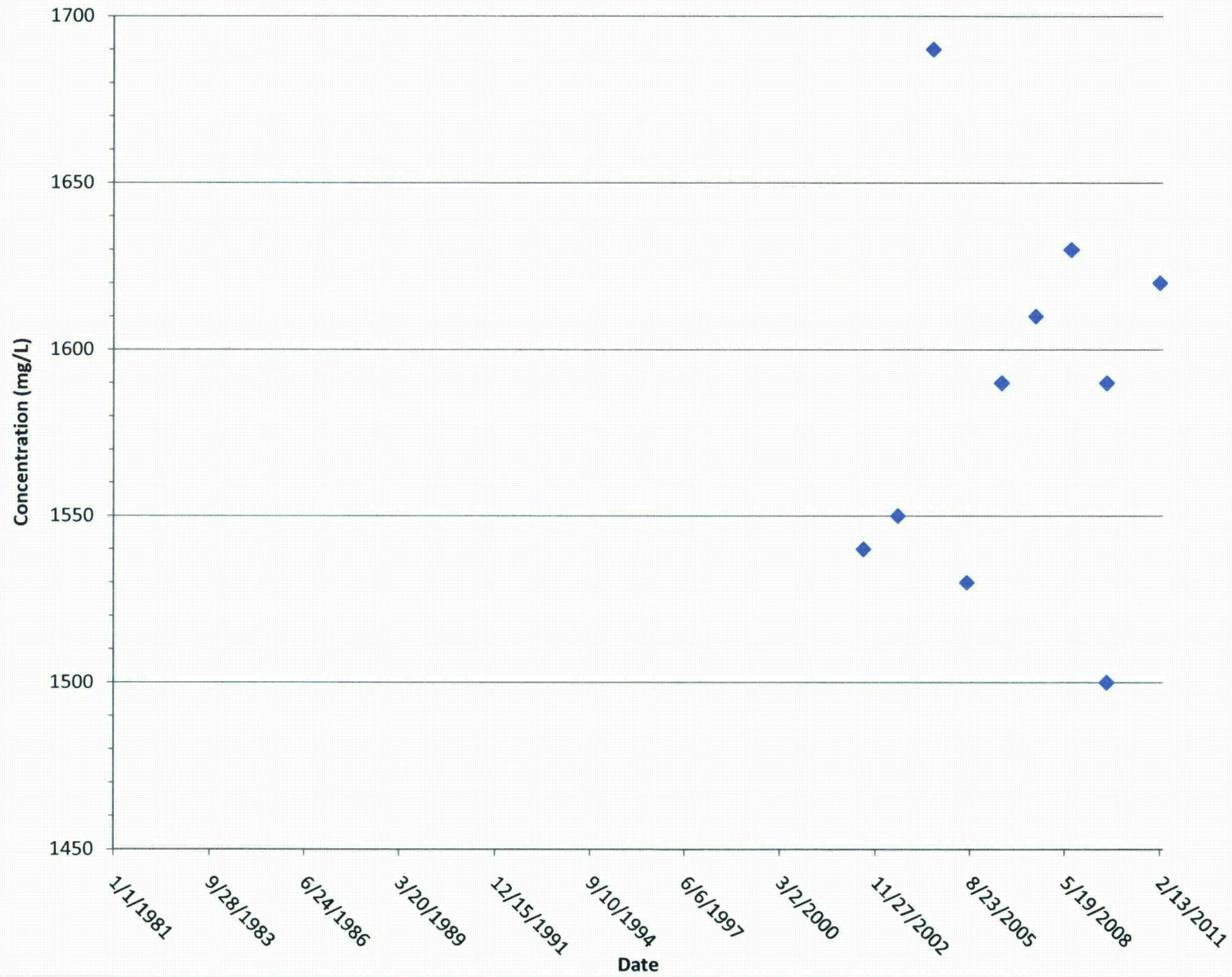
MW-110 Sulfate



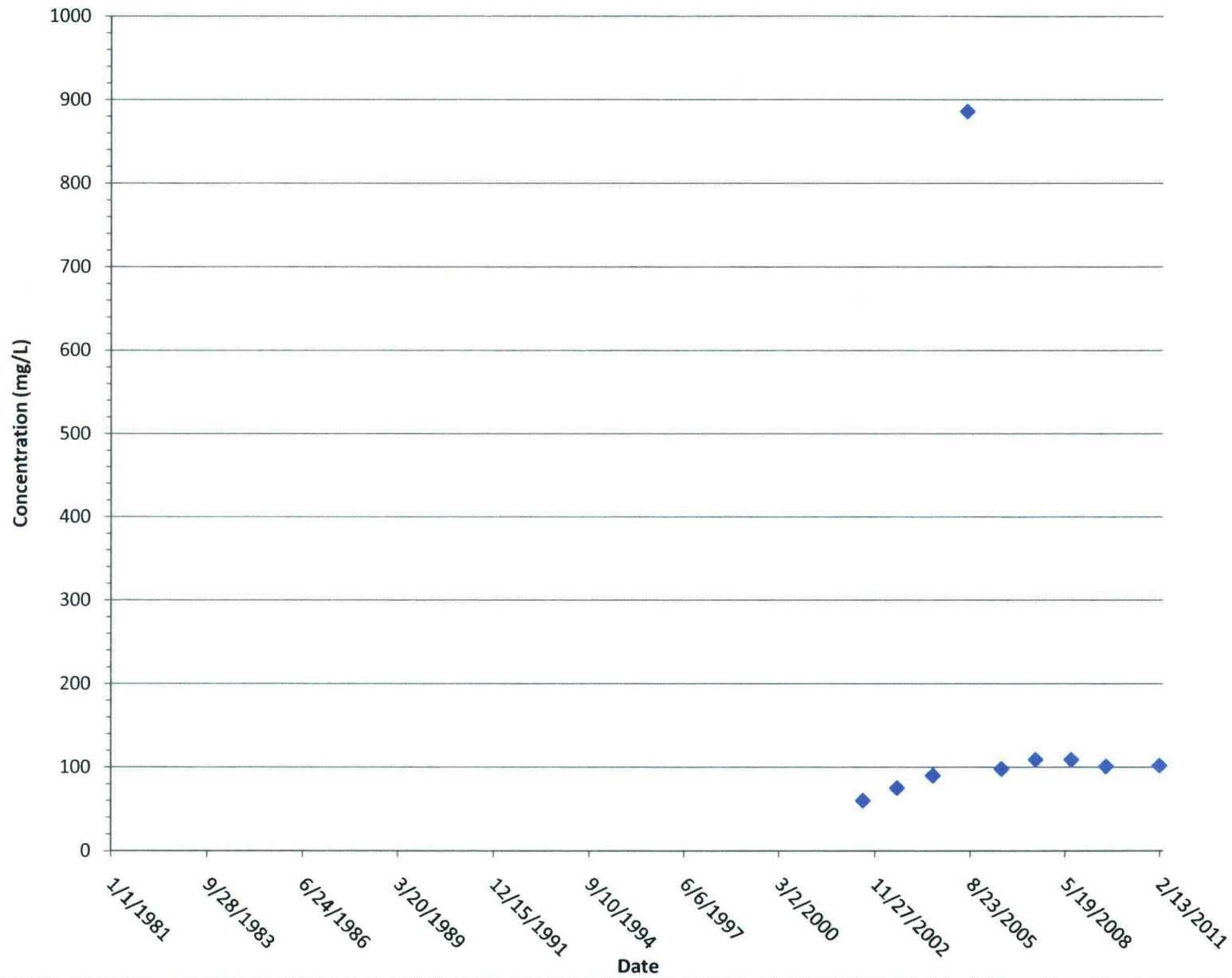
MW-109 Sulfate



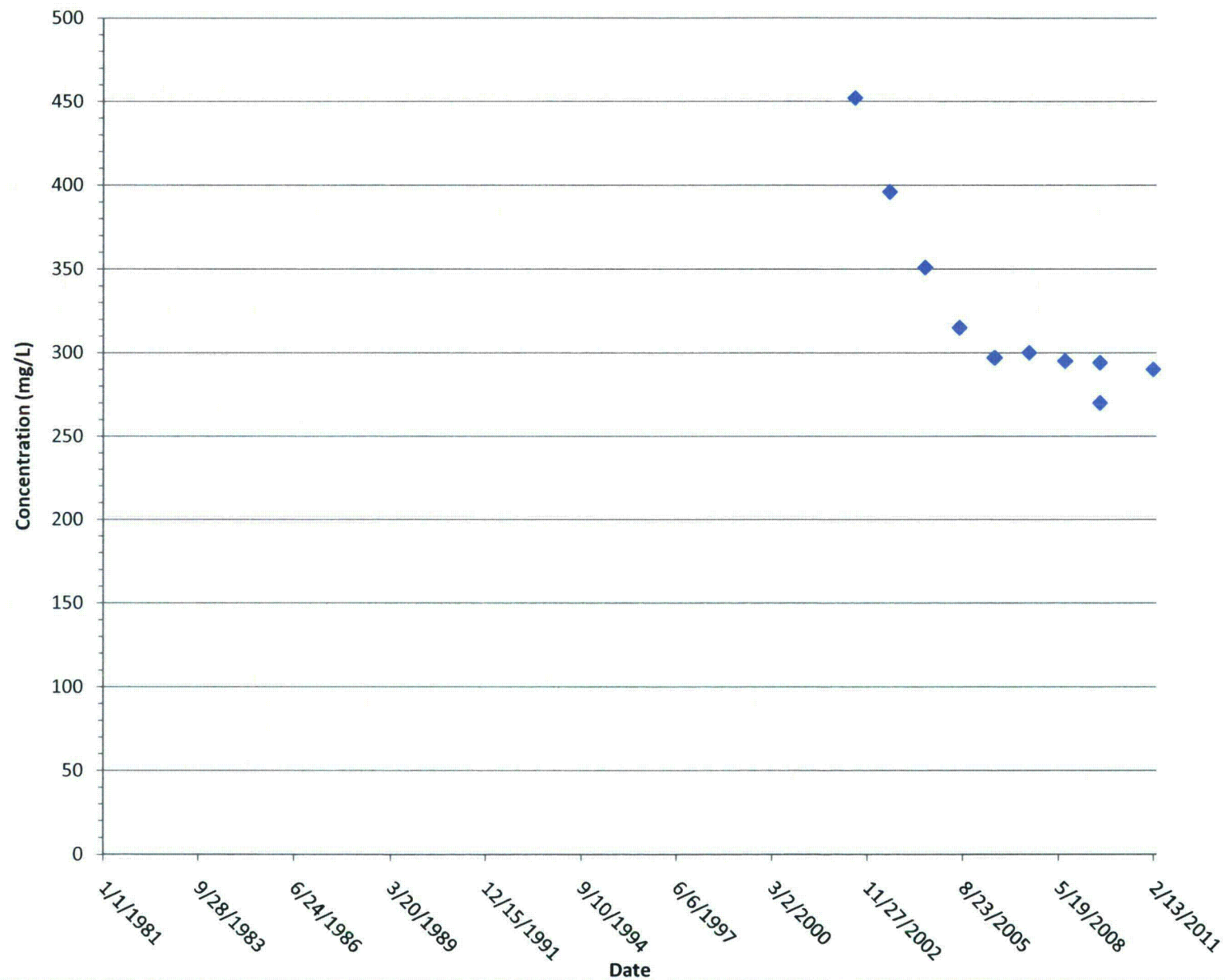
MW-108 Sulfate



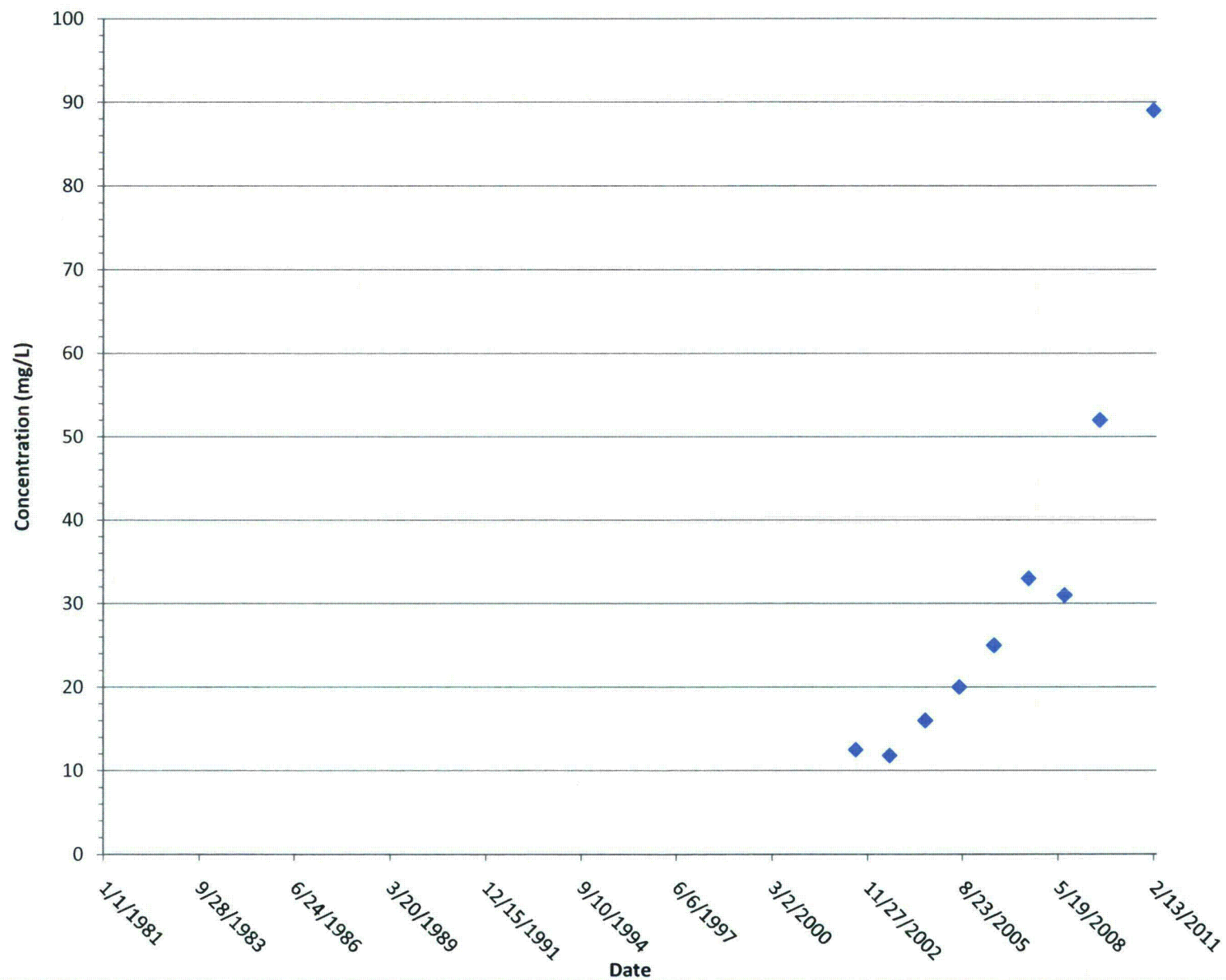
MW-111 Chloride



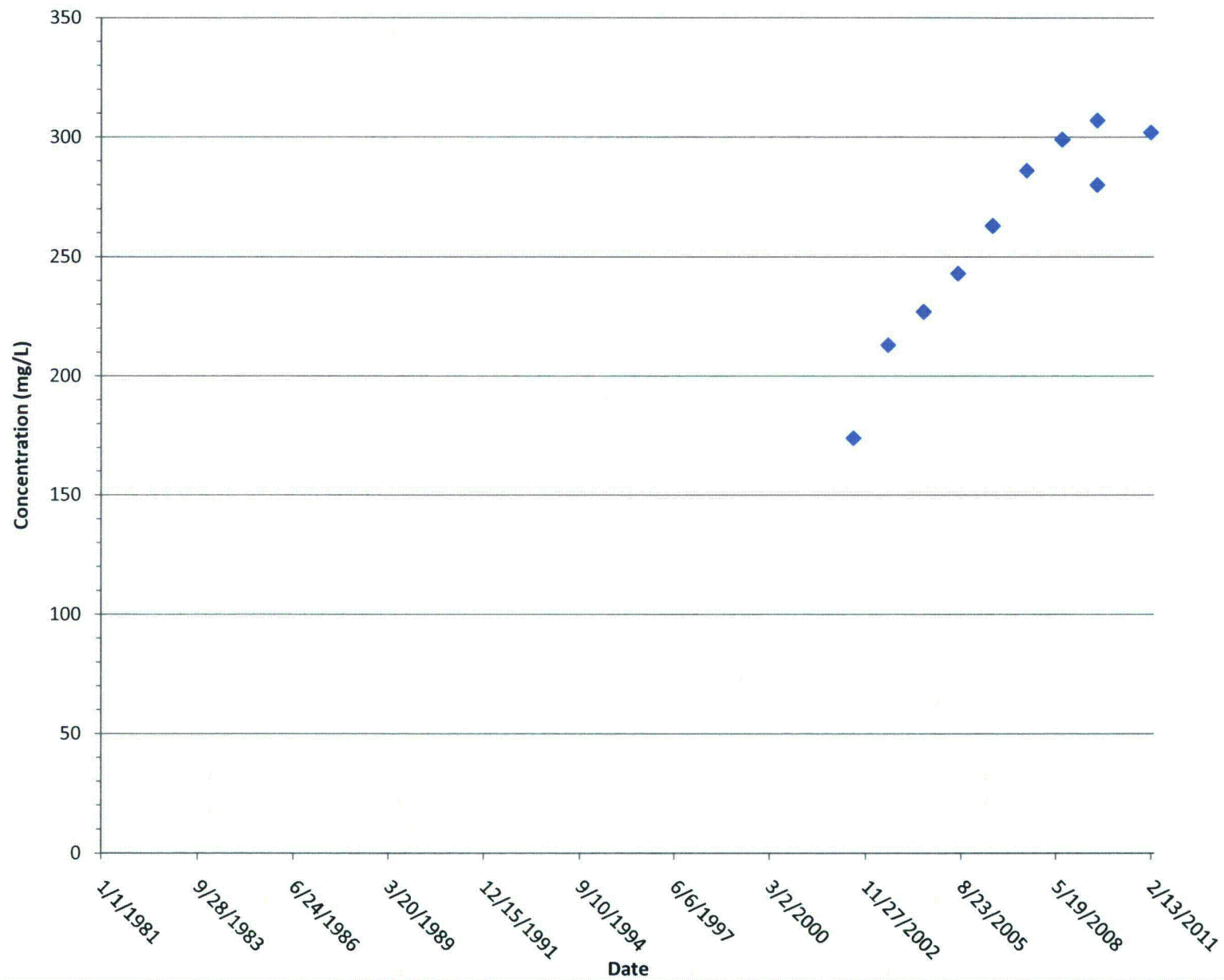
MW-110 Chloride



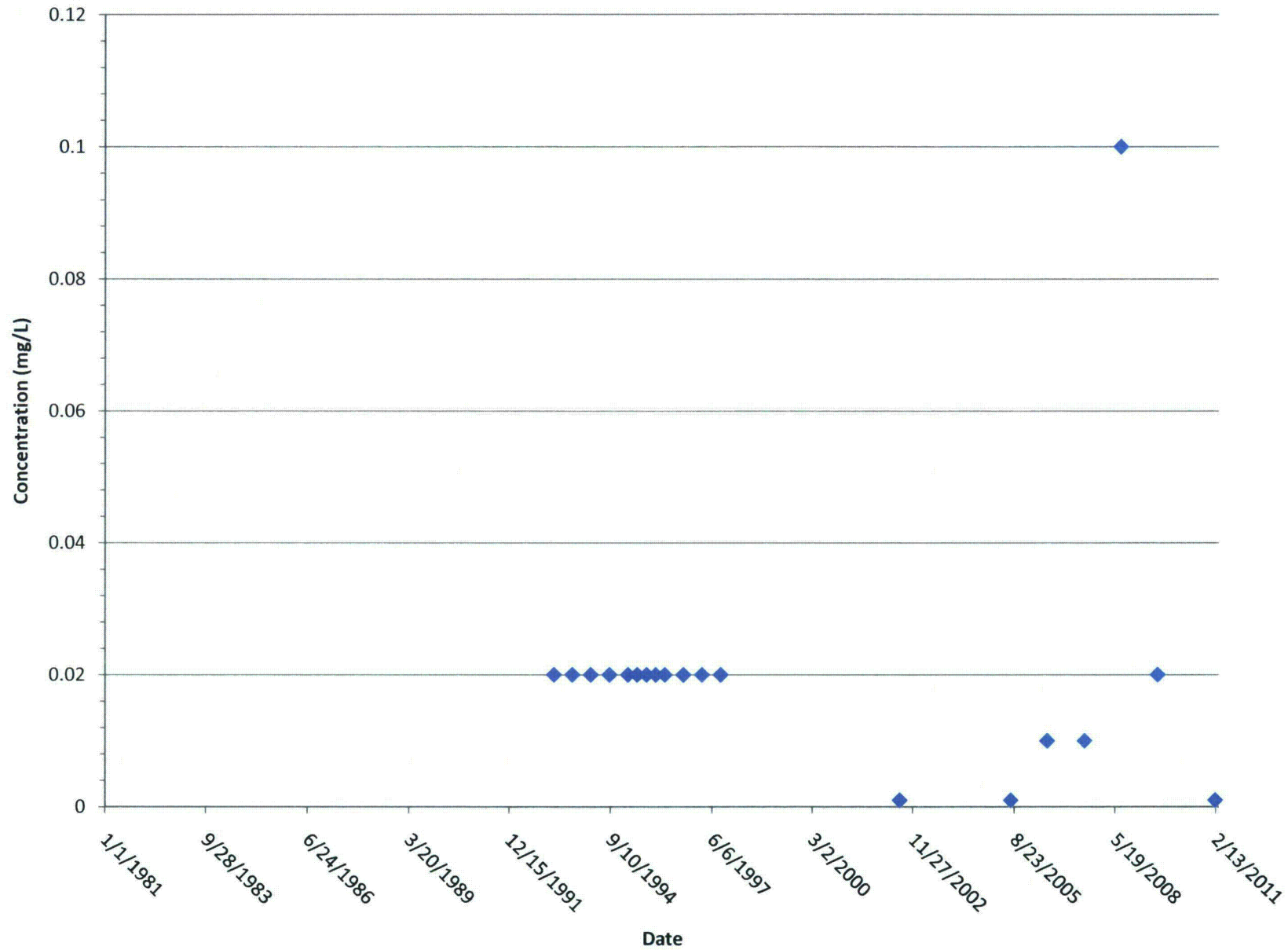
MW-109 Chloride



MW-108 Chloride



MW-74 Molybdenum

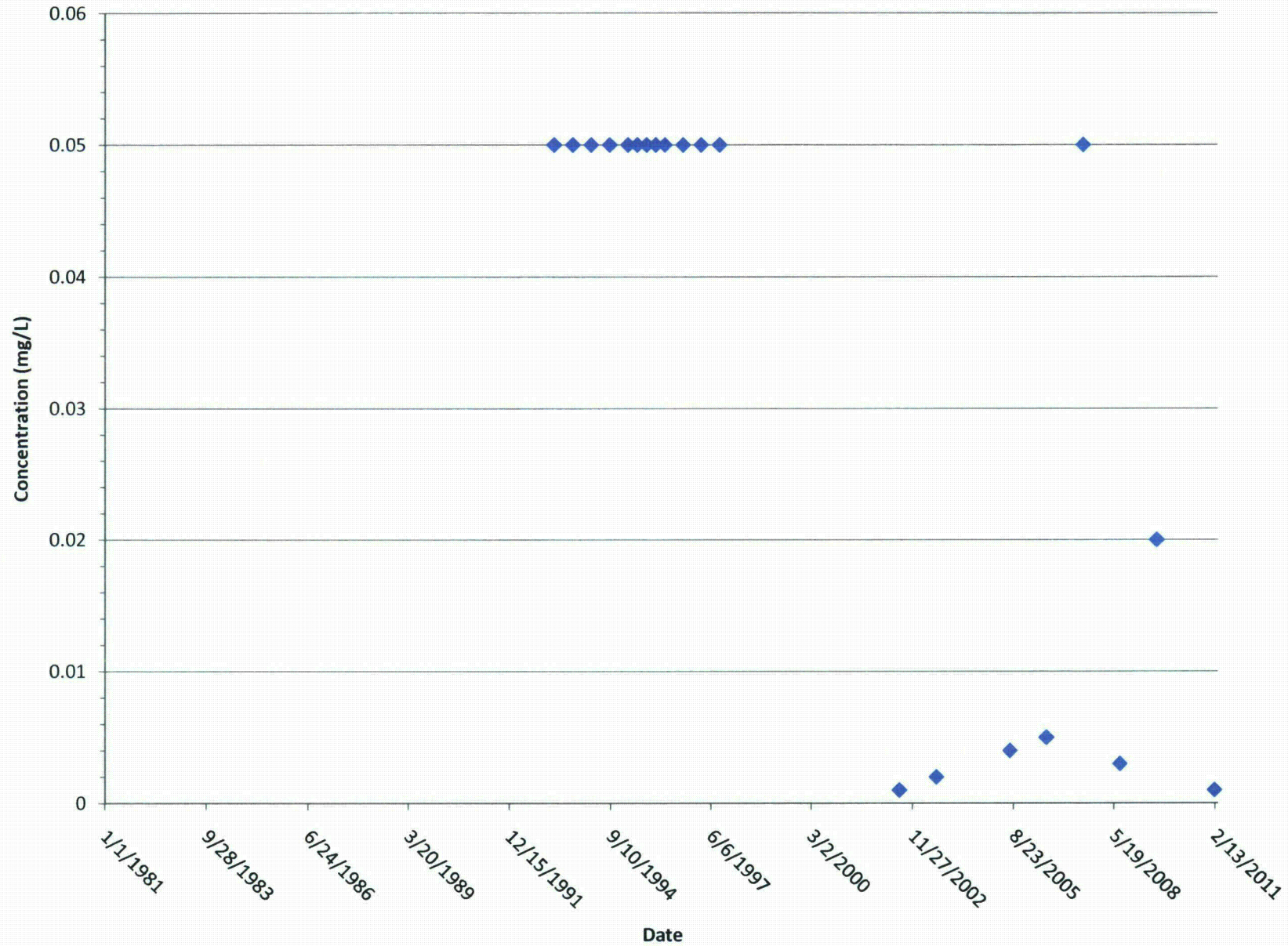


The scatter plot, titled "MW-12 Molybdenum", displays the concentration of molybdenum in mg/L over time from 1981 to 2011. The y-axis ranges from 0 to 0.12 mg/L with major gridlines every 0.02 units. The x-axis shows dates from 1/1/1981 to 2/13/2011. The data points are represented by blue diamonds. Most measurements are at a concentration of 0.02 mg/L, spanning from approximately 1989 to 2008. There are two notable higher concentrations: one at approximately 0.09 mg/L in early 1989 and another at approximately 0.10 mg/L in late 1989. Several measurements are at or near 0 mg/L, starting around 2005 and continuing through 2008.

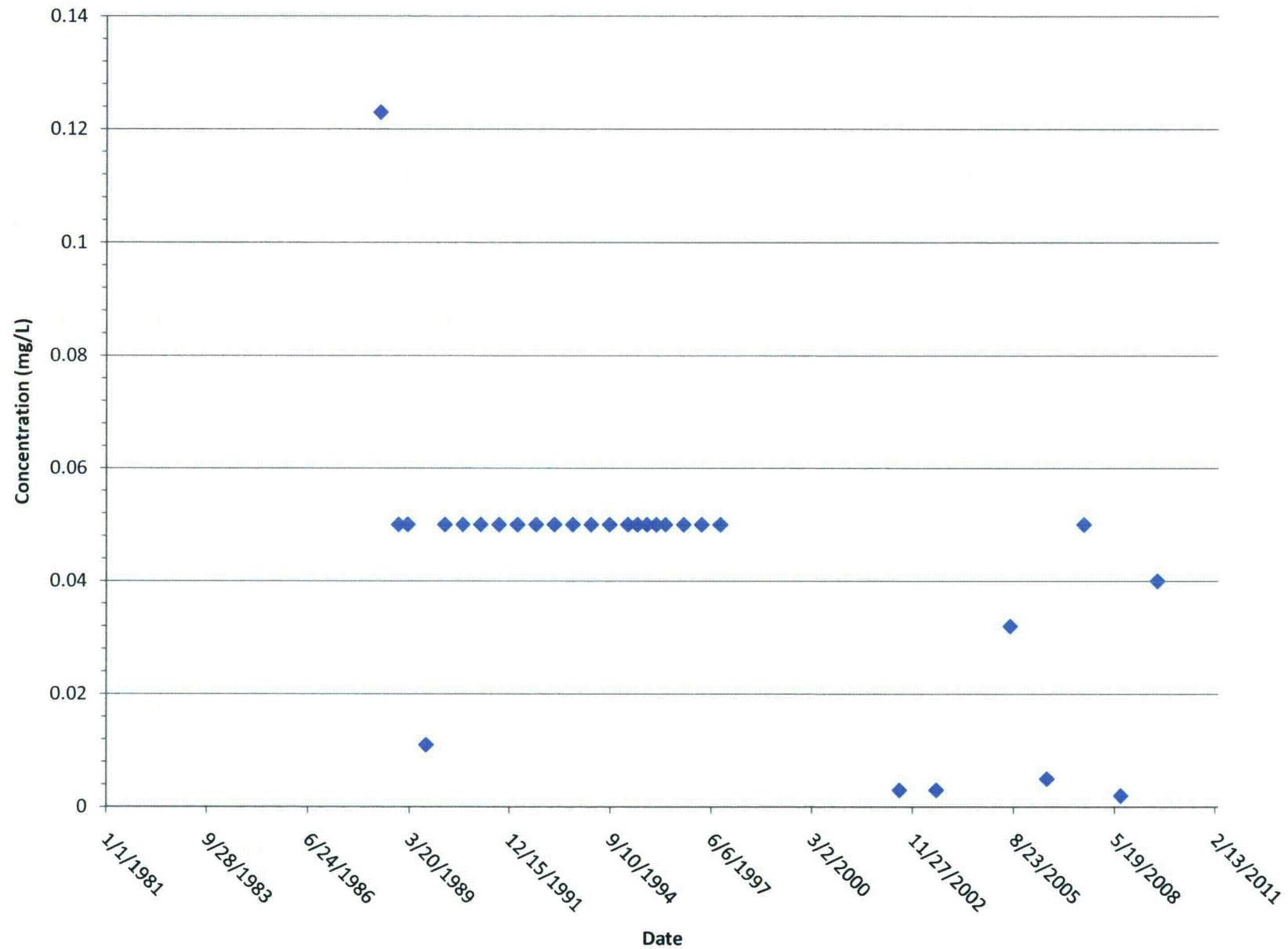
Date	Concentration (mg/L)
1/1/1981	0.010
1/1/1982	0.032
1/1/1983	0.048
9/28/1983	0.065
6/24/1986	0.051
3/20/1989	0.090
3/20/1989	0.100
3/20/1989	0.020
6/6/1997	0.020
8/23/2005	0.001
8/23/2005	0.001
5/19/2008	0.010
5/19/2008	0.010
2/13/2011	0.020

Date _____

MW-74 Chromium



MW-12 Chromium



MW-74 Cadmium

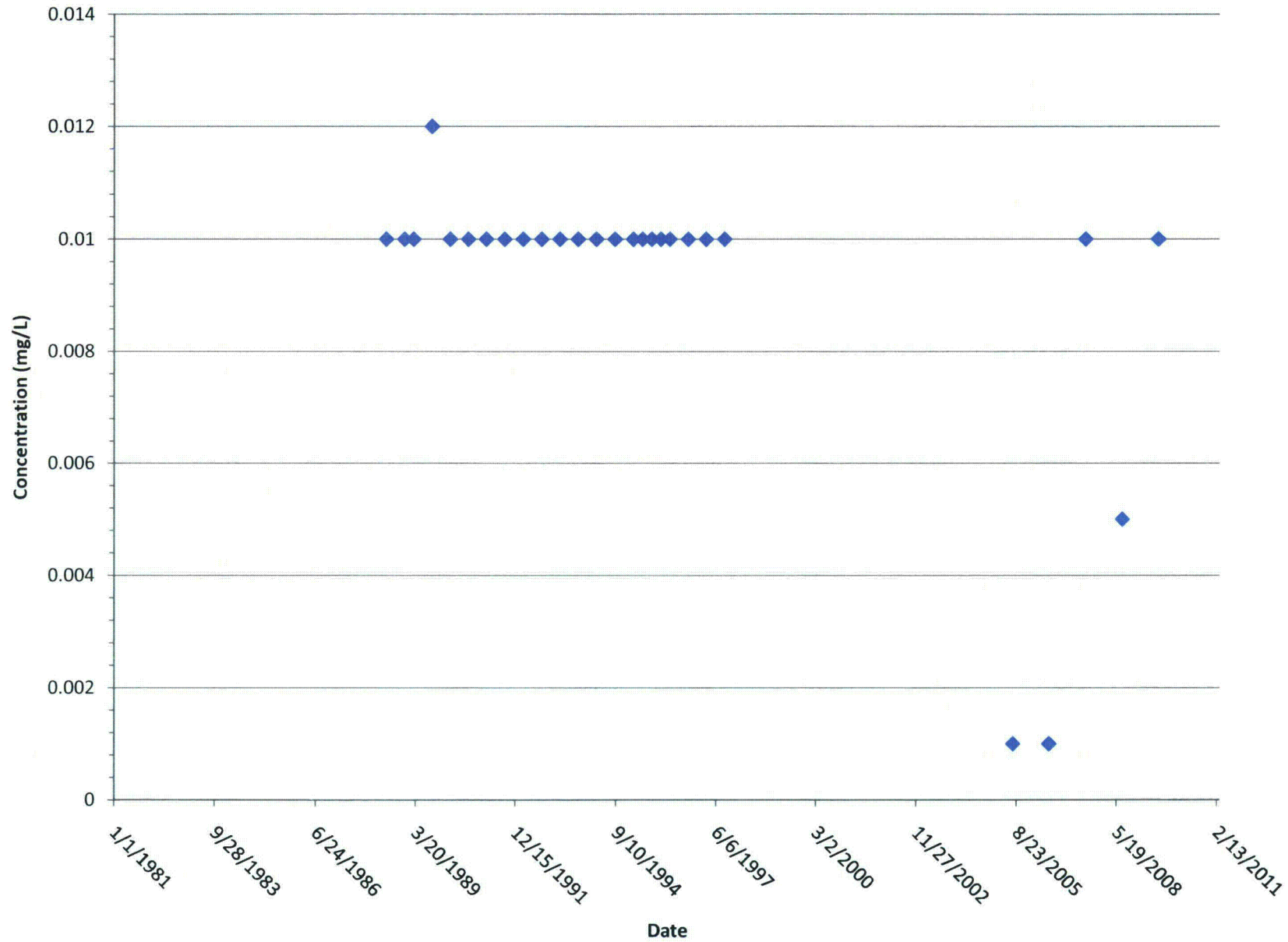
Concentration (mg/L)

Date

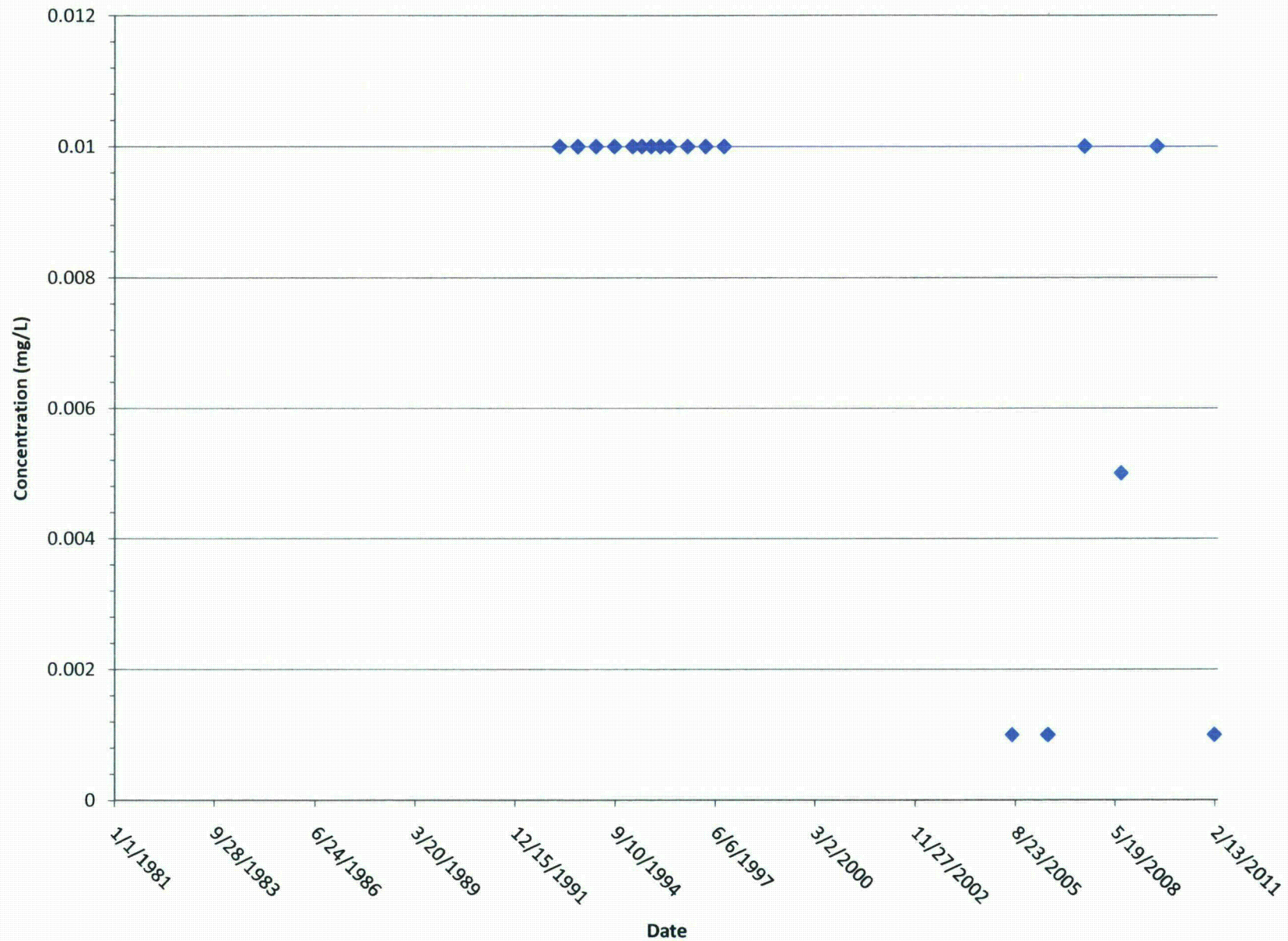
Date	Concentration (mg/L)
1/1/1981	0.012
9/28/1983	0.008
6/24/1986	0.007
3/20/1989	0.006
12/15/1991	0.009
9/10/1994	0.010
6/6/1997	0.010
8/23/2005	0.001
5/19/2008	0.005
2/13/2011	0.001

Concentration (mg/L)

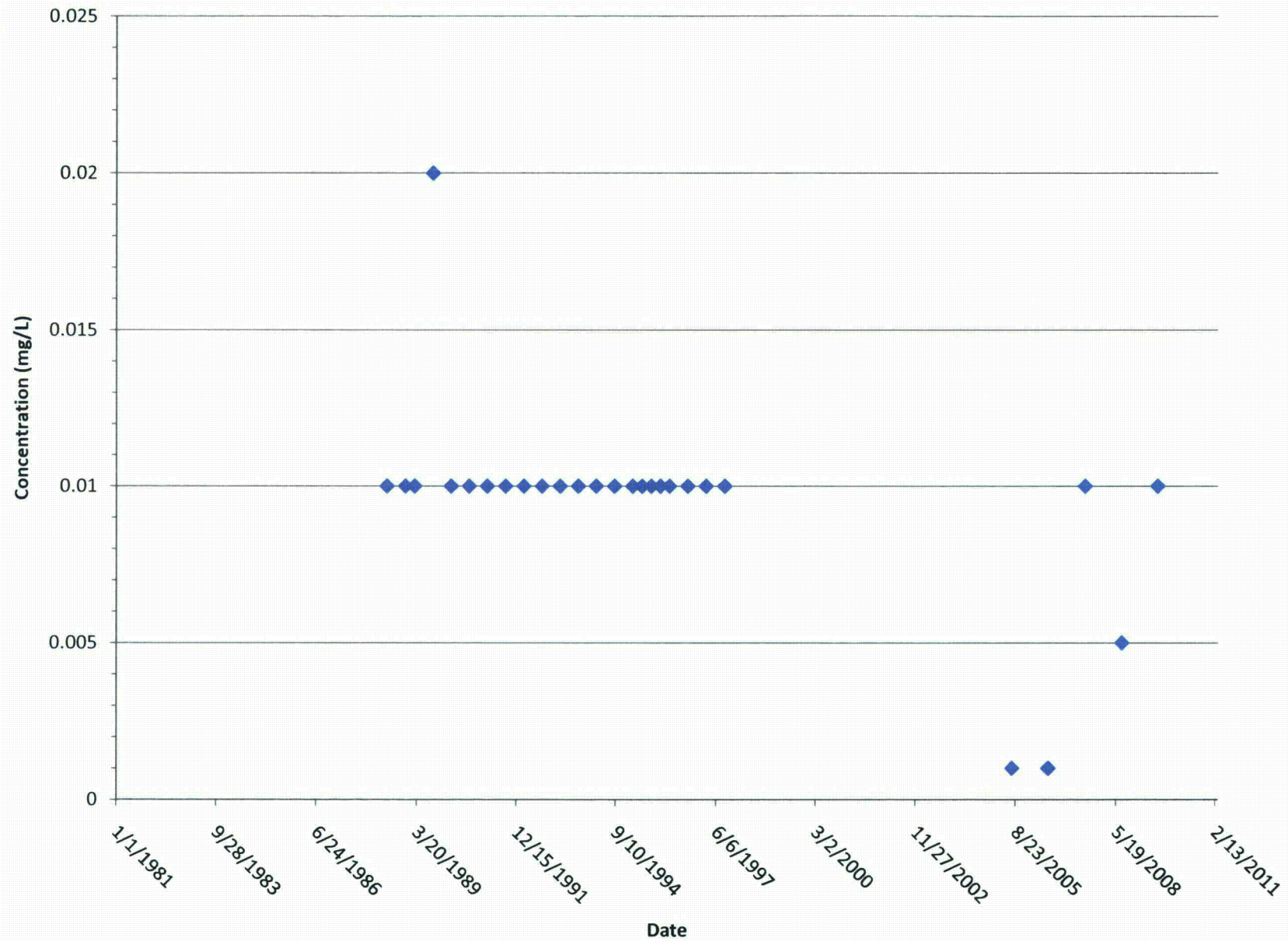
MW-12 Cadmium



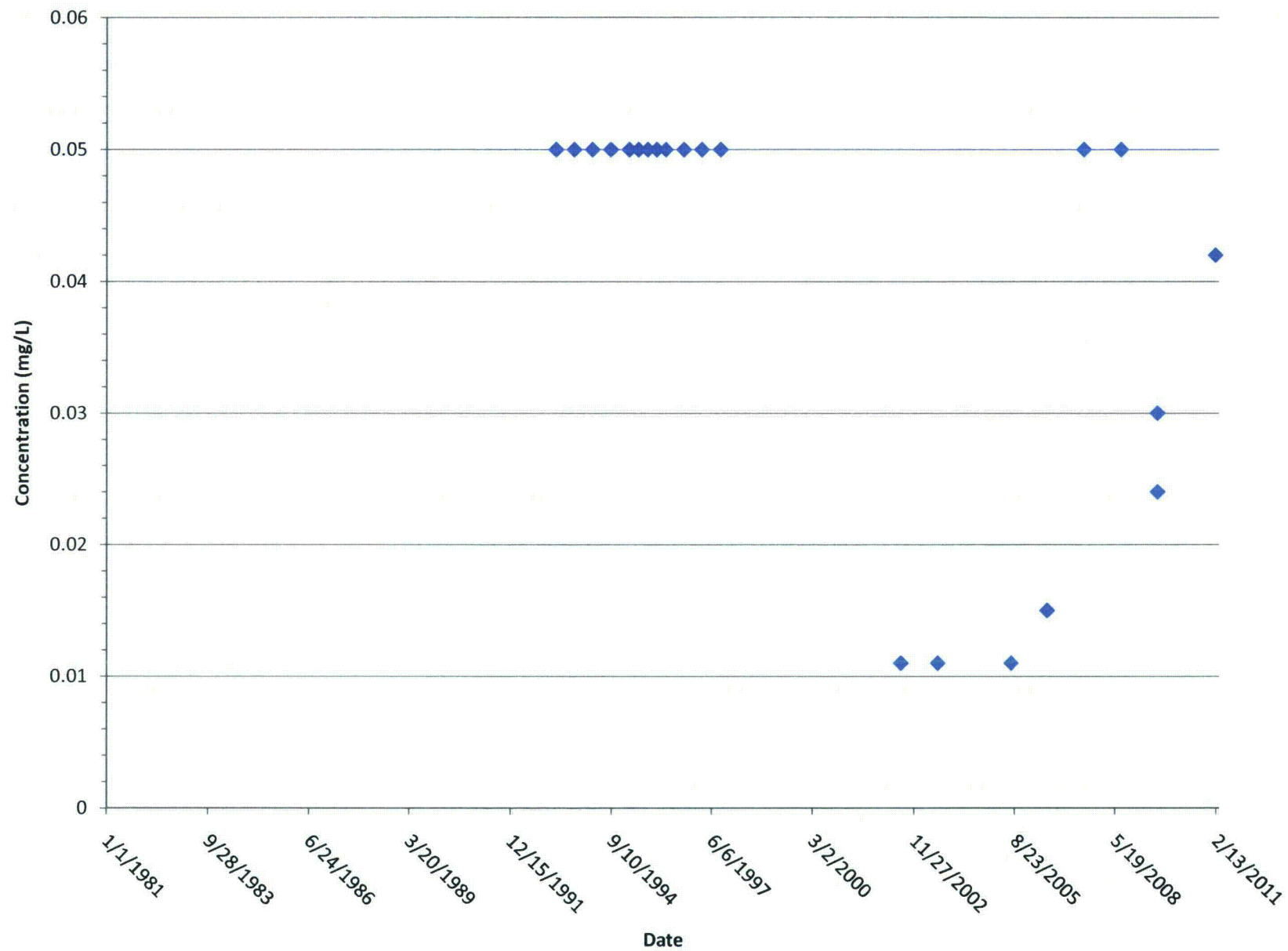
MW-74 Beryllium



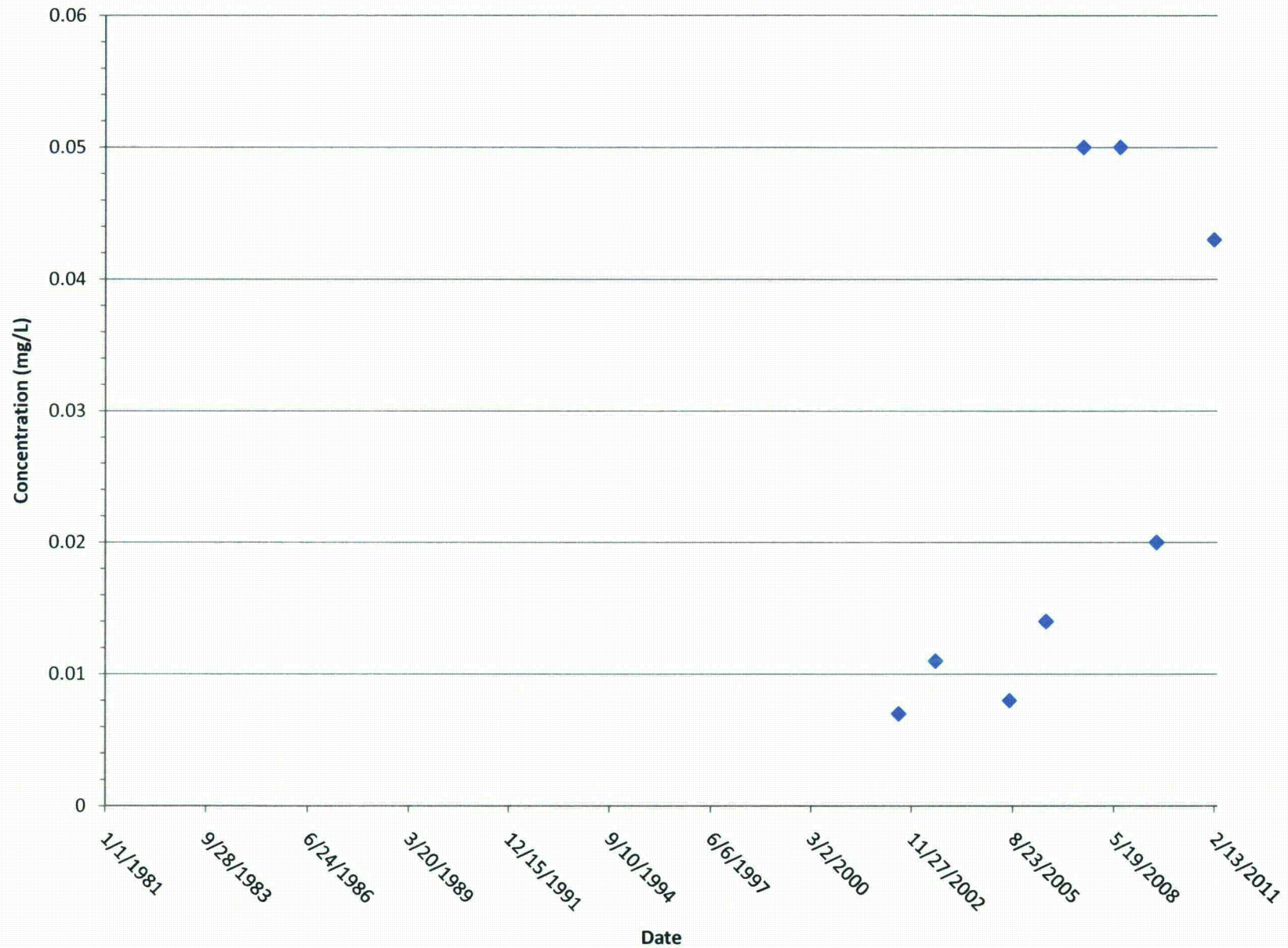
MW-12 Beryllium

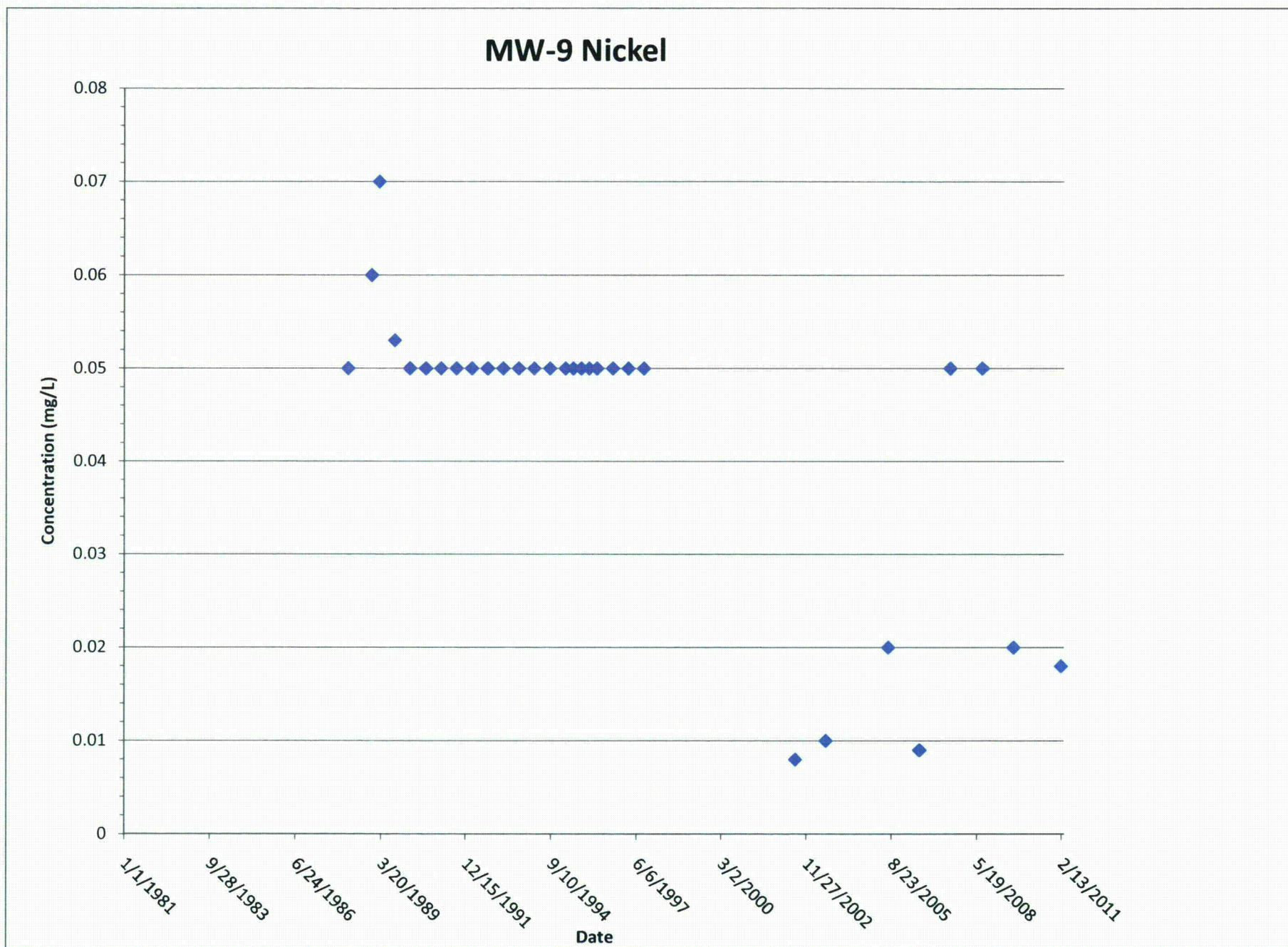


MW-74 Nickel



MW-108 Nickel



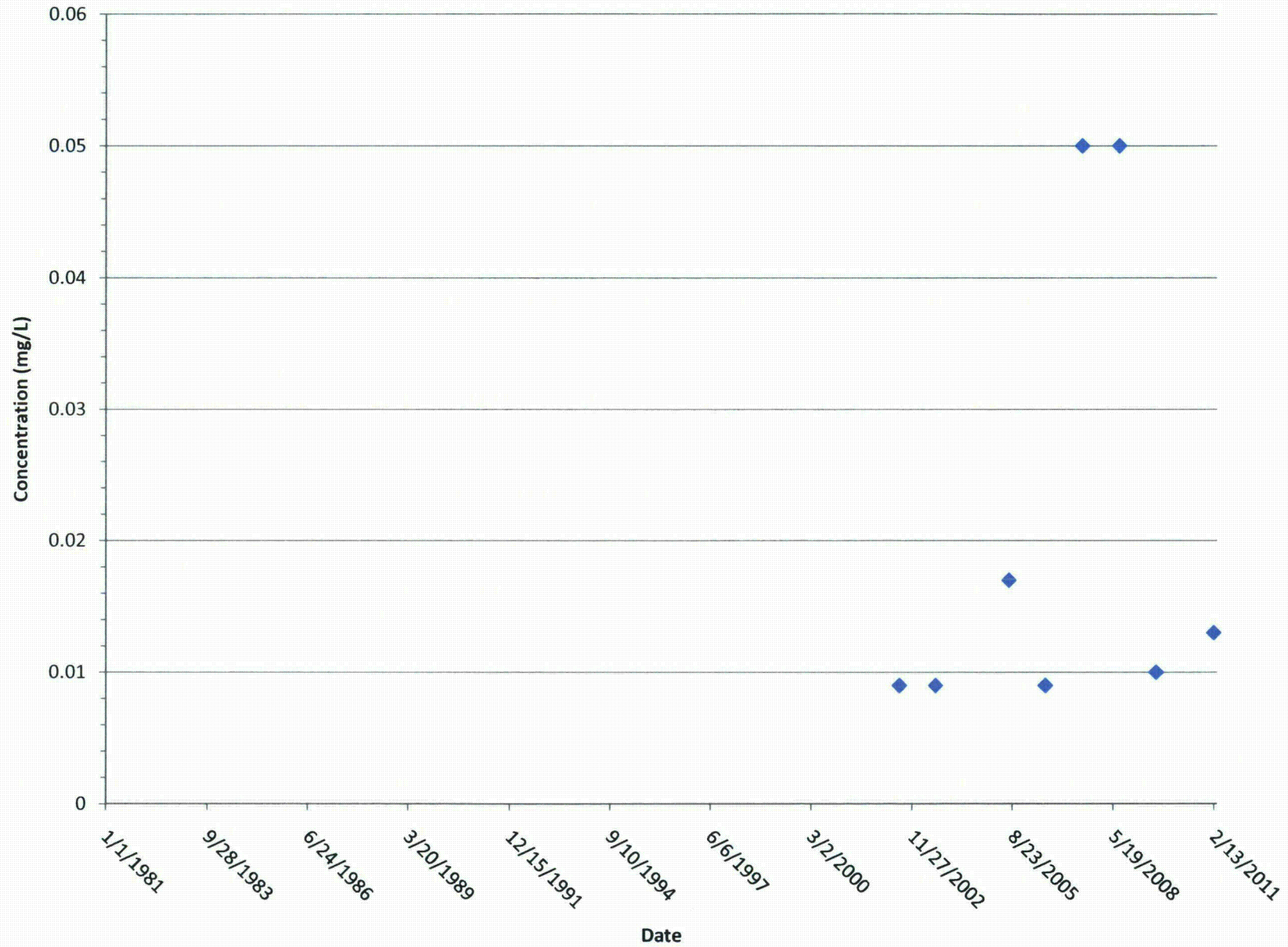


MW-14 Nickel

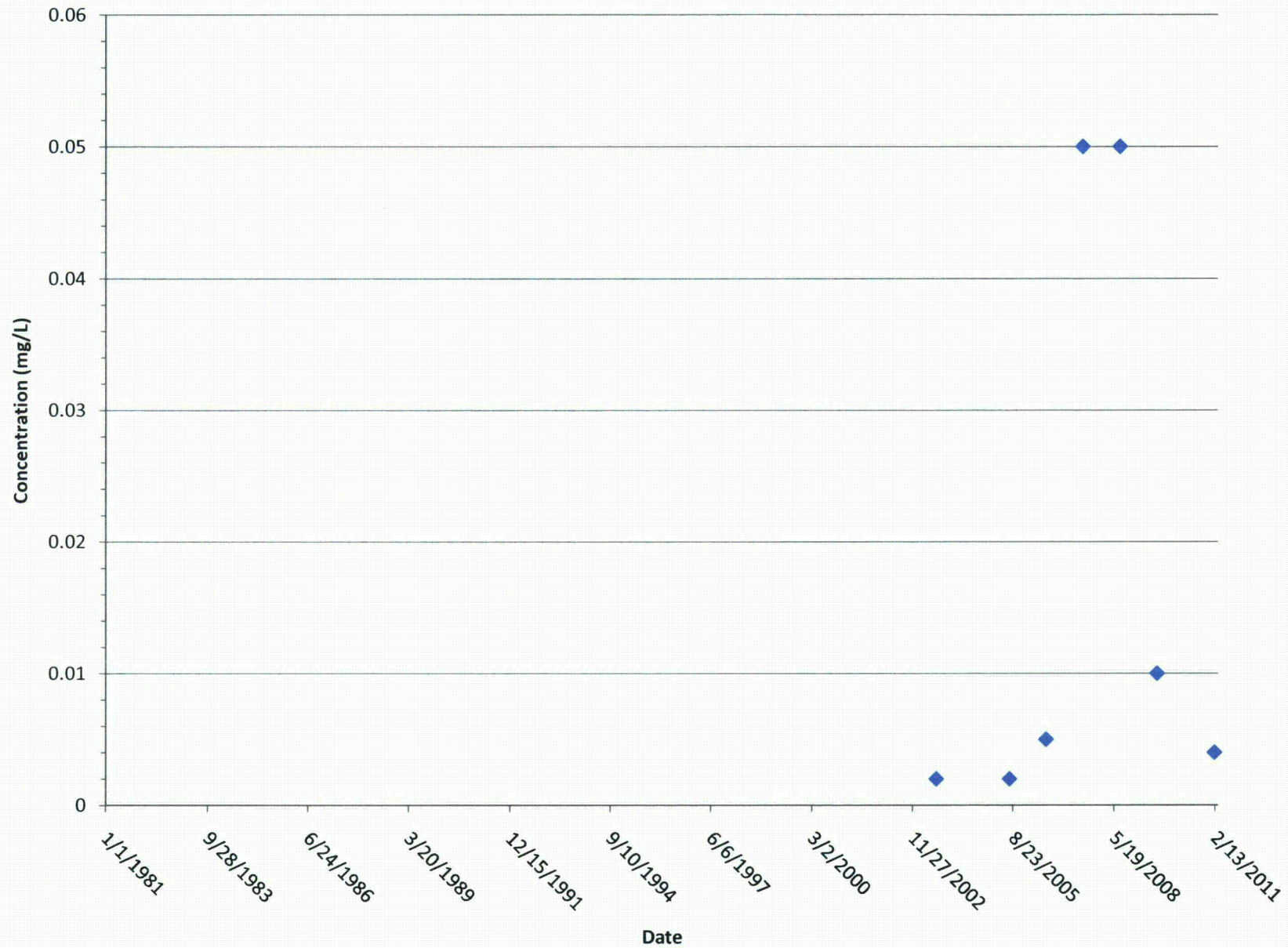
Date	Concentration (mg/L)
3/20/1989	0.080
3/20/1989	0.050
4/18/1989	0.050
5/16/1989	0.050
6/13/1989	0.050
7/11/1989	0.050
8/8/1989	0.050
9/5/1989	0.050
10/3/1989	0.050
10/31/1989	0.050
11/28/1989	0.050
12/26/1989	0.050
1/23/1990	0.050
2/20/1990	0.050
3/18/1990	0.050
4/15/1990	0.050
5/13/1990	0.050
6/10/1990	0.050
7/8/1990	0.050
8/5/1990	0.050
9/2/1990	0.050
10/1/1990	0.050
10/29/1990	0.050
11/26/1990	0.050
12/24/1990	0.050
1/21/1991	0.050
2/18/1991	0.050
3/16/1991	0.050
4/13/1991	0.050
5/11/1991	0.050
6/8/1991	0.050
7/6/1991	0.050
8/3/1991	0.050
9/1/1991	0.050
10/29/1991	0.050
11/26/1991	0.050
12/24/1991	0.050
1/21/1992	0.050
2/18/1992	0.050
3/16/1992	0.050
4/13/1992	0.050
5/11/1992	0.050
6/8/1992	0.050
7/6/1992	0.050
8/3/1992	0.050
9/1/1992	0.050
10/29/1992	0.050
11/26/1992	0.050
12/24/1992	0.050
1/21/1993	0.050
2/18/1993	0.050
3/16/1993	0.050
4/13/1993	0.050
5/11/1993	0.050
6/8/1993	0.050
7/6/1993	0.050
8/3/1993	0.050
9/1/1993	0.050
10/29/1993	0.050
11/26/1993	0.050
12/24/1993	0.050
1/21/1994	0.050
2/18/1994	0.050
3/16/1994	0.050
4/13/1994	0.050
5/11/1994	0.050
6/8/1994	0.050
7/6/1994	0.050
8/3/1994	0.050
9/1/1994	0.050
10/29/1994	0.050
11/26/1994	0.050
12/24/1994	0.050
1/21/1995	0.050
2/18/1995	0.050
3/16/1995	0.050
4/13/1995	0.050
5/11/1995	0.050
6/8/1995	0.050
7/6/1995	0.050
8/3/1995	0.050
9/1/1995	0.050
10/29/1995	0.050
11/26/1995	0.050
12/24/1995	0.050
1/21/1996	0.050
2/18/1996	0.050
3/16/1996	0.050
4/13/1996	0.050
5/11/1996	0.050
6/8/1996	0.050
7/6/1996	0.050
8/3/1996	0.050
9/1/1996	0.050
10/29/1996	0.050
11/26/1996	0.050
12/24/1996	0.050
1/21/1997	0.050
2/18/1997	0.050
3/16/1997	0.050
4/13/1997	0.050
5/11/1997	0.050
6/8/1997	0.050
7/6/1997	0.050
8/3/1997	0.050
9/1/1997	0.050
10/29/1997	0.050
11/26/1997	0.050
12/24/1997	0.050
1/21/1998	0.050
2/18/1998	0.050
3/16/1998	0.050
4/13/1998	0.050
5/11/1998	0.050
6/8/1998	0.050
7/6/1998	0.050
8/3/1998	0.050
9/1/1998	0.050
10/29/1998	

Date _____

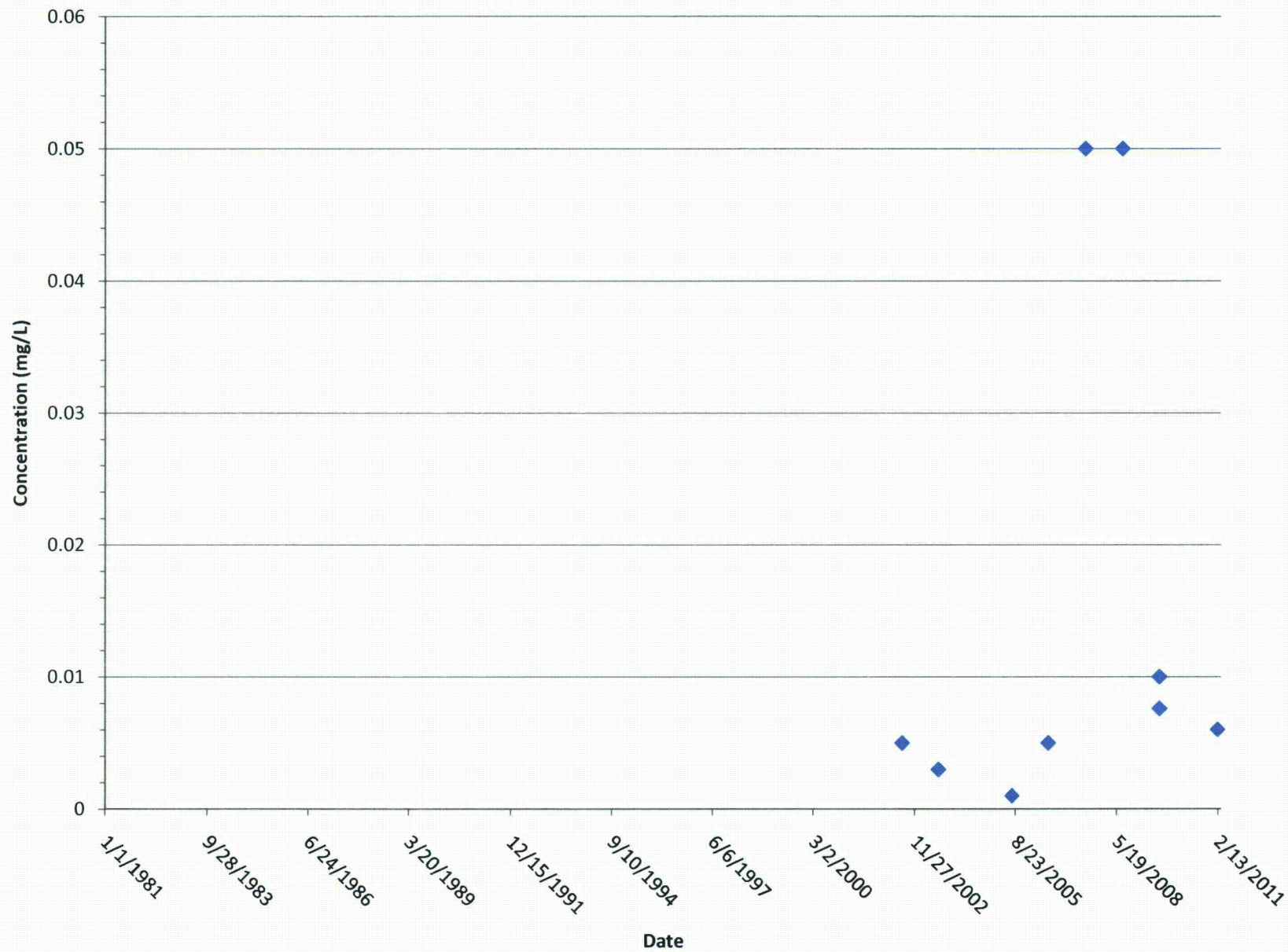
MW-109 Nickel



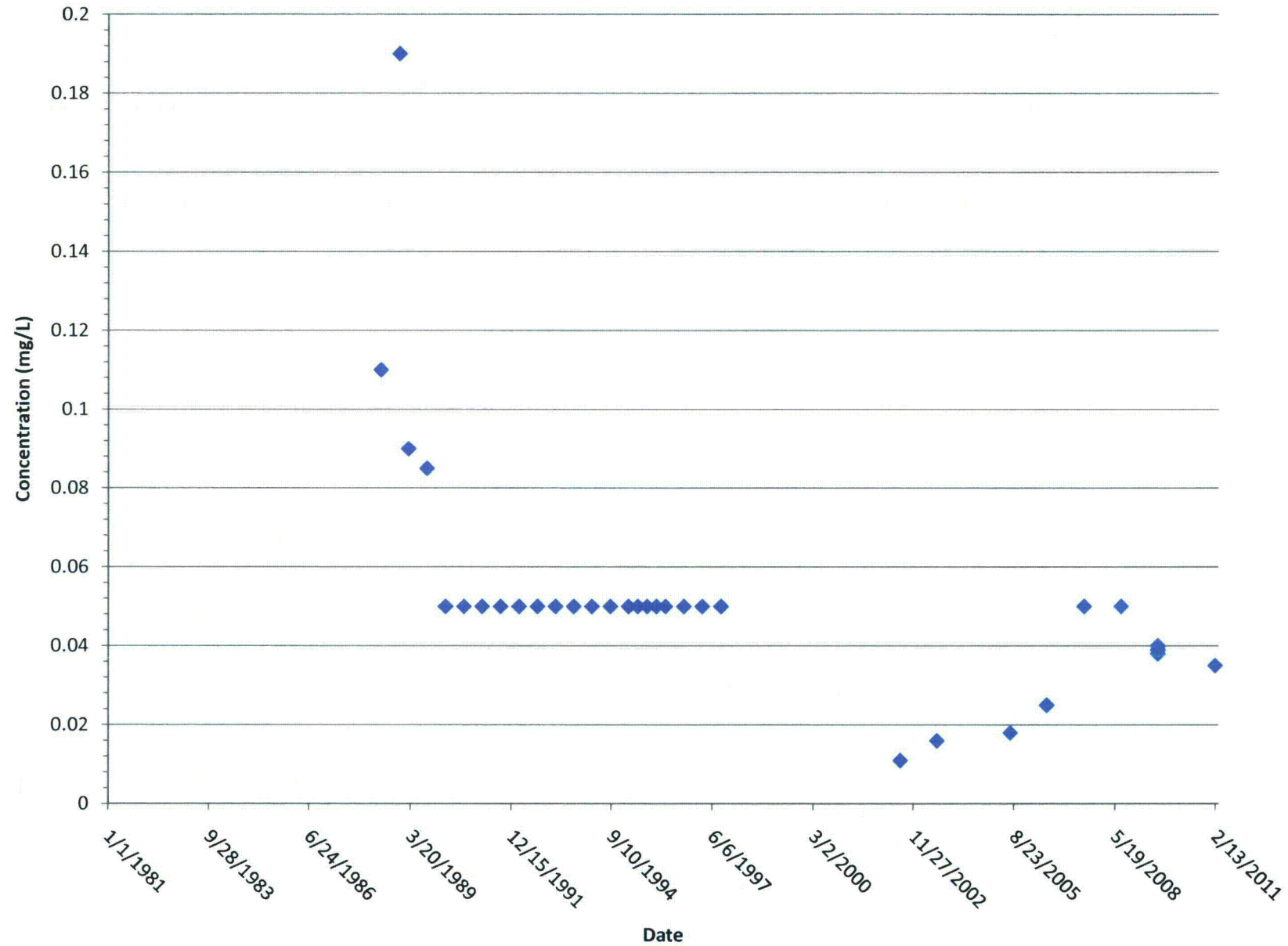
MW-111 Nickel



MW-110 Nickel



MW-12 Nickel



ATTACHMENT II

Input PHREEQC data set for
Long Draw

DATABASE Phreeqcm.dat

Input dataset for Lang Draw model

USER PUNCH

```

-headings U pCi/L Radium pCi/L CELL DISTANCE m TIME YEARS DATE step
ALKALINITY U_ppm pH Ferri Cl_ppm S(6)_ppm Ra2(pCi/L) Ni_ppm
-start
5 USPECIES = MOL("Ca2UO2(CO3)3")+ MOL("CaUO2(CO3)3-2") + MOL("UO2+2")+
MOL("UO2CO3") + MOL("UO2Cl+") + MOL("UO2Cl2") + MOL("UO2(CO3)2-2")+
MOL("UO2(CO3)3-4") + MOL("UO2(OH)3-") + MOL("UO2(OH)2") + MOL("UO2OH+") +
MOL("UO2(OH)4-2")+MOL("UO2SO4")+ MOL("UO2(SO4)2-2") + MOL("(UO2)2(OH)2+2")
10 SURFCOMP = MOL("Hfo_wOUO2+") + MOL("Hfo_sOUO2+") + MOL("Hfo_wOUO2(CO3)2-3")
+ MOL("Hfo_wOUO2CO3-")
15 PUNCH USPECIES*238*1000*.67*1000
#Uranium in pCi/L
20 PUNCH (TOT("Ra")*226*1000)/(226*2.8E-15*1600)
#Radium in pCi/L
25 PUNCH CELL NO
30 PUNCH CELL NO*4
35 PUNCH TOTAL TIME/(3600*24*365)
40 PUNCH (TOTAL TIME/(3600*24)+34578) # you
can install an actual date by changing the 34578 value, WHICH is currently
set for Sept 1 1994.
45 PUNCH step no # puts
step number in column 7
50 PUNCH ALK*50000
55 PUNCH TOT("U")*238*1000
60 PUNCH -LA("H+")
65 PUNCH EQUI("Fe(OH)3(a)")
70 PUNCH TOT("CL")*1000*35.453
75 PUNCH TOT("S(6)")*1000*96.064
80 SURFCOMP = MOL("Hfo_wOUO2+") + MOL("Hfo_sOUO2+") + MOL("Hfo_wOUO2(CO3)2-3")
+ MOL("Hfo_wOUO2CO3-")
85 PUNCH TOT("Ra")*226*1.0E12 # Ra in pCi/L
90 PUNCH TOT("Ni")*1000*58.69

-end

```

TITLE Transport: Bear Creek Lang Draw Model Phreeqc 2.0

```

SOLUTION 1000 solution MW-86 # Solution to mix with upgradient
(MW-36) water for upgradient boundary condition
units mg/L
# Samplename MW-86
pH 4.5
pe 12
temp 25
Ca 420
Mg 700
Na 278 charge
K 42
Fe 926
Mn 35.9
Al 230
S(6) 9040
Cl 600
C(4)
F 0.1
P 0.01
Si 21.4 #as SiO2
Ni 0.08
U 3.303662 # U-natural (pCi/L) 2038
Ra 4.5e-09

```

END

SOLUTION 2000 MW-36 background groundwater
clean water

#THIS IS WATER FROM MW-36

units mg/L
Samplename MW-36
pH 7.8
pe 12
temp 25
Ca 158
Mg 21
Na 61
K 7
Fe 0.1
Mn 0.11
Al 0.5
S(6) 425
Cl 25
C(4) 153
Ni 0.01
U 0.003
Ra 0.5E-09

END

SOLUTION 3000 MW-14
units mg/L
Samplename MW-14
pH 7.4
pe 12
temp 25
Ca 440
Mg 59
Na 34 charge
K 2
Fe 0.1
Mn 0.49
Al 0.5
S(6) 1053
Cl 90
C(4) 331
Ni 0.01
U 0.054
U-natural (pCi/L)
Ra 1.2E-09

END

MIX
1000 .594427
2000 .405573
SAVE SOLUTION 0-30
END

CELL SETUP STARTS HERE FIRST SIMULATION

EQUILIBRIUM PHASES 1-30
Al(OH)3(a) -1.36 0.0
Fe(OH)3(a) 1.69 1.000000E-4
Calcite 0.0 0.0
Gypsum 0.0 0.2
SiO2(a) 0.0 0.0

SURFACE 1-30
-equilibrate with solution 1-30

Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
 Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
 surface area per mole of iron hydroxide
 Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

SAVE EQUILIBRIUM PHASES 1-30
 SAVE SURFACE 1-30
 SAVE Solution 1-30

END

SOLUTION 31-55 Initial solution for column THIS IS MW-15

	units	ppm
units mg/L		
# Samplename		MW-15
pH	6.0	
pe	12	
temp	25	
Ca	650	
Mg	250	
Na	212 charge	
K	18	
Fe	2.18	
Mn	0.35	
Al	1.33	
S(6)	2420	
Cl	375	
C(4)	1450	
F	0.3	
P	0.01	
Si	20.78	
Ba	#	
Ni	0.025	
U	1.20000000	
Ra	2.5312E-09	

#as SiO2

EQUILIBRIUM PHASES 31-55

Al(OH)3(a)	-1.36	0.1
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.01
Gypsum	0.0	0.2
SiO2(a)	0.0	0.0

SURFACE 31-55

-equilibrate with solution 31-55

Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
 Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
 surface area per mole of iron hydroxide
 Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

SAVE SURFACE 31-55
 SAVE EQUILIBRIUM PHASES 31-55
 SAVE Solution 31-55

END

SOLUTION 56-119 Initial solution for column MW-12

	units	mg/L
# Samplename		MW-12
pH	7.0	
pe	12	
temp	25	
Ca	450	
Mg	150	
Na	265 charge	
K	14	

Fe 0.69
Mn 0.07
Al 1.15
S(6) 2000
Cl 275
C(4) 878
F 0.3
P 0.01
Si 18
Ni 0.025
U 0.16
Ra 1.5E-09

#as SiO2

EQUILIBRIUM PHASES 56-119

Al(OH)3(a)	-1.36	0.01
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.0
SiO2(a)	0.0	0.0

SURFACE 56-119

-equilibrate with solution 56-119

Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

SAVE EQUILIBRIUM PHASES 56-119

SAVE SURFACE 56-119

SAVE Solution 56-119

END

SOLUTION 120-162 Initial solution for column MW-14
units mg/L

Samplename MW-14

pH 7.7
pe 12
temp 25
Ca 350
Mg 59
Na 34 charge
K 2
Fe 0.1
Mn 0.49
Al 0.5
S(6) 800
Cl 70
C(4) 331
F
P
Si
Ni 0.01
U 0.054
Ra 1.2E-09

EQUILIBRIUM PHASES 120-162

Al(OH)3(a)	-1.36	0.01
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.0
SiO2(a)	0.0	0.0

```

SURFACE 120-162
  -equilibrate with solution 120-162
Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

```

```

SAVE EQUILIBRIUM PHASES 120-162
SAVE SURFACE 120-162
SAVE Solution 120-162

```

END

```

MIX
2000 0.5
3000 0.5
SAVE SOLUTION 163-210
END

```

```

EQUILIBRIUM PHASES 163-210
  Al(OH)3(a) -1.36 0.01
  Fe(OH)3(a) 1.69 1.000000E-4
  Calcite 0.0 0.4
  Gypsum 0.0 0.0
  SiO2(a) 0.0 0.0

```

```

SURFACE 163-210
  -equilibrate with solution 163-210
Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

```

```

SAVE SURFACE 163-210
SAVE Solution 163-210

```

END

```

MIX
2000 0.8
3000 0.2
SAVE SOLUTION 211-242
END

```

```

EQUILIBRIUM PHASES 211-242
  Al(OH)3(a) -1.36 0.01
  Fe(OH)3(a) 1.69 1.000000E-4
  Calcite 0.0 0.4
  Gypsum 0.0 0.0
  SiO2(a) 0.0 0.0

```

```

SURFACE 211-242
  -equilibrate with solution 211-242
Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

```


SAVE EQUILIBRIUM PHASES 211-242
 SAVE SURFACE 211-242
 SAVE Solution 211-242

END
 PRINT

-reset false
 -surface true
 SELECTED OUTPUT
 -file BC_mod02.sel #can
 be SEL or XLS
 -reset false
 # -step true #this
 prints the time step in the first column, set to "false" in order to eliminate
 that column

#1995 through 1997 Plateau 2

MIX

1000 .594427

2000 .405573

SAVE SOLUTION 0

1994 through 1995

TRANSPORT

-cells 242 #235
 is total cells
 -length 4 #4
 meter cells .10000000 40.000000
 -shifts 9.00000 #6
 yrs*365*24*3600/2522880= 75 shifts; we start at the dam, John added a
 year for the diffence in length for the first water
 -time step 3155760.0 #This
 is 29.2 days in seconds and essentially indicates hydraulic
 conductivity
 -punch cells 1 20 52 98 121 159 181 242
 -punch frequency 1
 -flow direction forward
 -boundary conditions flux flux
 -correct disp true
 -dispersivity 235*30.0000
 -diffusion_coef 0.0e-0 #No
 diffusion
 -tempr 1.0 #No
 heat retardation

END

#1995 through 1997 Plateau 2

MIX

1000 .349935

2000 .650065

SAVE SOLUTION 0

write Solution 0

#Over-

TRANSPORT

-shifts 20.0000

END

#1997 through 2000 Plateau 3

MIX

1000 .087363

2000 .912637

SAVE SOLUTION 0

write Solution 0.

#Over-

TRANSPORT

-shifts 30.0000

END

#2000 through 2010 Plateau 4

MIX

1000 .004258

2000 .995742

SAVE SOLUTION 0

#Over-

write Solution 0.

TRANSPORT

-shifts 60.0000

END

#2006 through 2010 Plateau 5

MIX

1000 1.25E-5

2000 .999988

SAVE SOLUTION 0

#Over-

write Solution 0.

TRANSPORT

-shifts 109.000

END

END

ATTACHMENT III

Input PHREEQC data set for
Northern Pathway

DATABASE C:Phreeqcm.dat

USER PUNCH

```

-headings U pCi/L Radium pCi/L CELL DISTANCE m TIME_YEARS DATE step
ALKALINITY U_ppm pH Ferri Cl_ppm S(6)_ppm RA_pCi/L NI_ppm
-start
3 USPECIES = MOL("Ca2UO2(CO3)3")+ MOL("CaUO2(CO3)3-2") + MOL("UO2+2")+
MOL("UO2CO3") + MOL("UO2Cl+") + MOL("UO2Cl2") + MOL("UO2(CO3)2-2")+
MOL("UO2(CO3)3-4") + MOL("UO2(OH)3-") + MOL("UO2(OH)2") + MOL("UO2OH+") +
MOL("UO2(OH)4-2")+MOL("UO2SO4")+ MOL("UO2(SO4)2-2") + MOL("UO2)2(OH)2+2")
4 SURFCOMP = MOL("Hfo_wOUO2+") + MOL("Hfo_sOUO2+") + MOL("Hfo_wOUO2(CO3)2-3")
+ MOL("Hfo_wOUO2CO3-")
5 PUNCH USPECIES*238*1000*.67*1000
#Uranium in pCi/L
7 PUNCH (TOT("Ra")*226*1000)/(226*2.8E-15*1600)
#Radium in pCi/L
11 PUNCH CELL NO #if
you want to eliminate a column, you remove it from the heading, then comment
out the line that applies to that column
13 PUNCH CELL NO*4
15 PUNCH TOTAL TIME/(3600*24*365)
17 PUNCH (TOTAL TIME/(3600*24)+34578) # you
can install an actual date by changing the 34578 value, WHICH is currently
set for Sept 1 1994.
19 PUNCH step no #puts
step number in column 7
21 PUNCH ALK*50000
23 PUNCH TOT("U")*238*1000
25 PUNCH -LA("H+")
26 PUNCH EQUI("Fe(OH)3(a)")
27 PUNCH TOT("CL")*1000*35.453
28 PUNCH TOT("S(6)")*1000*96.064
30 SURFCOMP = MOL("Hfo_wOUO2+") + MOL("Hfo_sOUO2+") + MOL("Hfo_wOUO2(CO3)2-3")
+ MOL("Hfo_wOUO2CO3-")

32 PUNCH TOT("Ra")*226*1.0E12 # Ra in pCi/L
33 PUNCH TOT("Ni")*1000*58.69

-end

```

TITLE Transport: Bear Creek North Path

SOLUTION 1000 solution MW-86

units mg/L

Samplename MW-86

pH 4.5

pe 12

temp 25

Ca 420

Mg 700

Na 278 charge

K 42

Fe 926

Mn 35.9

Al 230

S(6) 9040

Cl 400

F 0.1

P 0.01

Si 21.4

Ni .1

U 0.6

Ra 1.51872E-08

END

#as SiO2

SOLUTION 2000 MW-36 background groundwater

units mg/L
Samplename MW-36
pH 7.4
pe 12
temp 25
Ca 158
Mg 21
Na 61
K 7
Fe 0.1
Mn 0.11
Al 0.5
S(6) 425
Cl 25
C(4) 153
Ni 0.01
U 0.003
Ra 2.5312E-09

END

SOLUTION 3000 MW-43

units mg/L
Samplename MW-43 11/10/94
pH 7.7
pe 12
temp 25
Ca 974.
Mg 198.
Na 71. charge
K 17.
Fe 7.91
Mn 0.85
Al 0.01
S(6) 2080
Cl 575.
C(4) 854.
F .2
Si 5.4
Ba #
Ni 0.02
U 0.0581
Ra 5.164E-09

END

MIX

1000 .334046
2000 .665954
SAVE SOLUTION 0-54
END

CELL SETUP STARTS HERE FIRST SIMULATION

EQUILIBRIUM PHASES 1-54

Al(OH)3(a)	-1.36	0.0
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.0
Gypsum	0.0	0.2
SiO2(a)	0.0	0.0

SURFACE 1-54


```

-equilibrate with solution 1-54
Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

```

```

SAVE EQUILIBRIUM PHASES 1-54
SAVE SURFACE 1-54
SAVE Solution 1-54

```

END

```

MIX
1000 .334046
2000 .665954
SAVE SOLUTION 55-84
END

```

CELL SETUP STARTS HERE FIRST SIMULATION

```

EQUILIBRIUM PHASES 55-84
Al(OH)3(a) -1.36 0.0
Fe(OH)3(a) 1.69 1.000000E-4
Calcite 0.0 0.1
Gypsum 0.0 0.2
SiO2(a) 0.0 0.0

```

SURFACE 55-84

```

-equilibrate with solution 55-84
Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

```

```

SAVE EQUILIBRIUM PHASES 55-84
SAVE SURFACE 55-84
SAVE Solution 55-84

```

END

SOLUTION 85-125 Initial solution for column THIS IS MW-74

units mg/L ppm

Sample name MW-74 9/94

```

pH 6.7
pe 12
temp 25
Ca 450.
Mg 116.
Na 67. charge
K 12.
Fe 0.66
Mn 0.48
Al 0.96
S(6) 1900.
Cl 200.
C(4) 708.
F 0.2
P 0.01
Si 15.83
Ba #
Ni 0.025
U 0.062

```

#as SiO2

#table 3-12

Ra 2.936E-09

EQUILIBRIUM PHASES 85-125

Al(OH)3(a)	-1.36	0.1
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.2
SiO2(a)	0.0	0.0

SURFACE 85-125

-equilibrate with solution 85-125

Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

SAVE SURFACE 85-125

SAVE EQUILIBRIUM PHASES 85-125

SAVE Solution 85-125

END

SOLUTION 126-170 Initial solution for column MW-43
units mg/L

Samplename MW-43 11/10/94

pH	7.7
pe	12
temp	25
Ca	974.
Mg	198.
Na	71. charge
K	17.
Fe	7.91
Mn	0.85
Al	0.01
S(6)	2080
Cl	575.
C(4)	854.
F	.2
P	
Si	5.4
Ba	#
Ni	0.02
U	0.0581
# U-natural (pCi/L)	
Ra	2.5E-9

EQUILIBRIUM PHASES 126-170

Al(OH)3(a)	-1.36	0.01
Fe(OH)3(a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.0
SiO2(a)	0.0	0.0

SURFACE 126-170

-equilibrate with solution 126-170

Hfo wOH Fe(OH)3(a) equilibrium phase 0.2 53400 # 0.2 sites per mole
of Fe(OH)3(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide
Hfo_sOH Fe(OH)3(a) equilibrium_phase 0.005

SAVE EQUILIBRIUM PHASES 126-170

SAVE SURFACE 126-170

SAVE Solution 126-170

END

MIX

2000 0.5

3000 0.5

SAVE SOLUTION 171-233

END

EQUILIBRIUM PHASES 171-233

Al(OH) ₃ (a)	-1.36	0.01
Fe(OH) ₃ (a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.0
SiO ₂ (a)	0.0	0.0

SURFACE 171-233

-equilibrate with solution 171-233

Hfo wOH Fe(OH)₃(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)₃(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide

Hfo_sOH Fe(OH)₃(a) equilibrium_phase 0.005

SAVE EQUILIBRIUM PHASES 171-233

SAVE SURFACE 171-233

SAVE Solution 171-233

END

MIX

2000 1.0

3000 0.0

SAVE SOLUTION 234-260

END

EQUILIBRIUM PHASES 234-260

Al(OH) ₃ (a)	-1.36	0.01
Fe(OH) ₃ (a)	1.69	1.000000E-4
Calcite	0.0	0.4
Gypsum	0.0	0.0
SiO ₂ (a)	0.0	0.0

SURFACE 234-260

-equilibrate with solution 234-260

Hfo wOH Fe(OH)₃(a) equilibrium phase 0.2 53400 #0.2 sites per mole of
Fe(OH)₃(a) present; 53400=600x89 (89 is formula weight for goethite) is
surface area per mole of iron hydroxide

Hfo_sOH Fe(OH)₃(a) equilibrium_phase 0.005

SAVE EQUILIBRIUM PHASES 234-260

SAVE SURFACE 234-260

SAVE Solution 234-260

END

END

PRINT

-reset false

-surface false

SELECTED OUTPUT

```

-file BC_mod02.sel #can
    be SEL or XLS
-reset false
# -step true #this
prints the time step in the first column, set to "false" in order to eliminate
that column

```

#1995 through 1997 Plateau 2

MIX

1000 .334046

2000 .665954

SAVE SOLUTION 0

1994 through 1995

TRANSPORT

```

-cells 260 #235
is total cells
-length 4 #4
meter cells .20000000 20.000000
-shifts 4.00000 #6
yrs*365*24*3600/2522880= 75 shifts; we start at the dam, John added a
year for the diffence in length for the first water
-time step 6311520.0 #This
is 29.2 days in seconds and essentially indicates hydraulic
conductivity
-punch cells 10 40 70 85 110 142 203 260
-punch frequency 1
-flow direction forward
-boundary conditions flux flux
-correct disp true
-dispersivity 260*20.000000
-diffusion_coef 0.0e-0 #No
diffusion
-tempr 1.0 #No
heat retardation

```

END

#1995 through 1997 Plateau 2

MIX

1000 .262052

2000 .737948

SAVE SOLUTION 0

write Solution 0

#Over-

TRANSPORT

-shifts 11.0000

END

#1997 through 2000 Plateau 3

MIX

1000 .166453

2000 .833547

SAVE SOLUTION 0

write Solution 0.

#Over-

TRANSPORT

-shifts 14.0000

END

#2000 through 2010 Plateau 4

MIX

1000 .069069

2000 .930931

SAVE SOLUTION 0

write Solution 0.

#Over-

TRANSPORT
-shifts 29.0000

END

#2006 through 2010 Plateau 5

MIX
1000 .010855
2000 .989145
SAVE SOLUTION 0
write Solution 0.

#Over-

TRANSPORT
-shifts 10 #00

END

END

ATTACHMENT IV

Modifications to the Thermodynamic
Database for Uranium and Radium

Modifications to the Thermodynamic Database for Uranium and Radium

by

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DATABASE

The thermodynamic database used for these calculations (summarized in Table 1) was a modified version of the WATEQ4F database provided with PHREEQC (Parkhurst and Appelo, 1999). Modifications were primarily based upon changes to the reactions in the SOLUTION_SPECIES¹ portion of the database for the uranyl (UO_2^{+2}) component. Additionally, reactions for radium were also added to the database; the solution reactions were originally taken from the MINTEQ.V4.dat database also provided with PHREEQC.

Uranium

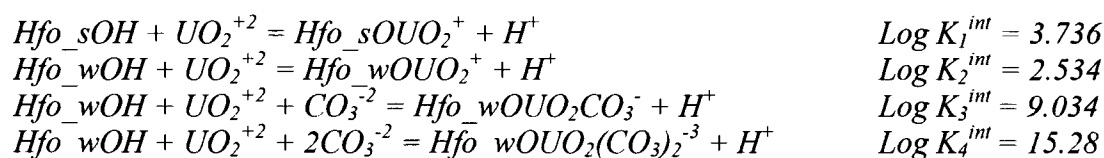
For uranium the revised data were from two sources. Reactions in solution were updated using the OECD NEA 2003 compilation (Guillaumont et al., 2003). This document is an update of an earlier compilation also done under the auspices of the NEA (Grenthe et al., 1992). The reactions that were updated primarily involved uranyl complexation reactions involving hydroxide and carbonate. Table 1 lists the NEA selected values along with the values in several of the unmodified databases included in the PHREEQC program package. The table also lists the values used in the revised database, called WATEQ_NEA.dat in Table 1.

In addition to the NEA update reactions, three ternary uranyl complexes were also added to database. These complexes included $\text{CaUO}_2(\text{CO}_3)_3^{-2}$, $\text{Ca}_2\text{UO}_2(\text{CO}_3)_3^0$, and $\text{MgUO}_2(\text{CO}_3)_3^{-2}$. The constants for these three reactions were reported in the literature after the 2003 NEA compilation was released. The values for these three complexation constants were taken from Dong and Brooks, (2006, 2008). The inclusion of these complexes will tend to increase

¹ The term SOLUTION_SPECIES is the keyword used in PHREEQC to define these reactions.

solubility concentrations estimates for uranyl and decrease adsorption of uranyl onto HFO in geochemical models (Mahoney et al., 2009b). Inclusion of the complexes improves model estimates by providing a more realistic set of complexation reactions in solution. Their presence will also tend to increase the model determined concentration of uranium in solution, which produces a more conservative model estimate. As this study was primarily aimed at adsorption reactions onto hydrous ferric oxide (HFO), no attempt was made to update uranyl bearing mineral phases in the database.

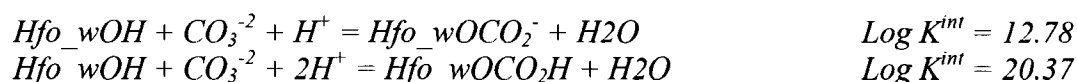
In addition to modifications to the SOLUTION_SPECIES portion of the database, the reactions that defined the surface complexation of uranyl onto hydrous ferric oxide (HFO) were updated based upon the recently published results of Mahoney et al. (2009a). This set of four reactions replaced the estimated values for the two reactions that were originally presented in Dzombak and Morel, (1990). The following surface complexation reactions were used to describe uranium (as uranyl) adsorption onto hydrous ferric oxide:



These revised set of reactions correct the values reported by Dzombak and Morel for K_1^{int} and K_2^{int} , which were not based upon comparison to laboratory derived data. Rather Dzombak and Morel used a correlation between the log K for the first metal hydroxide complex and the log K_1^{int} and K_2^{int} values. When compared to experimental measurements the Dzombak and Morel estimated values for log K_1^{int} and K_2^{int} tended to significantly overestimate the amount of uranyl adsorption at low pH conditions and tended to underestimate uranium adsorption at high pH conditions particularly when carbonate was also present in solution. The newer values, published in Mahoney et al. (2009a), were based upon model based fits to laboratory measurements. Moreover, the revised data set included two surface complexation constants for uranyl carbonate complexes (the K_3^{int} and K_4^{int} reactions). Complexation constants for any type of uranyl carbonate surface complex were not included in the original Dzombak and Morel (1990) compilation that eventually became the basis for the surface complexation portion of the database included in the PHREEQC package. The existence of uranyl carbonate surface complexes has long been known, although various groups define them differently. The

Dzombak and Morel compilation was never meant to be a definitive treatise on surface complexation reactions involving uranium, and so this shortcoming can be excused. However, any detailed study involved with uranium adsorption must consider the reactions in some form or other. The revised database does consider these reactions.

In addition to the uranyl adsorption reactions, two additional surface complexation reactions were added to the database. These reactions are defined below:



These final two reactions were defined by Appelo et al. (2002), and will influence sorption at higher partial pressures of CO₂(g). Specifically, these two additional reactions will tend to occupy sites on the surface that could complex with uranium. This will produce a concomitant increase in uranium concentrations in the pore waters (Mahoney et al., 2009b).

Radium

Speciation reaction constants for radium were also added to this database. Values were obtained from Langmuir and Riese (1985). The following reactions were added to the database.

Species	Reaction	Log K
RaOH ⁺	Ra ⁺² + H ₂ O = RaOH ⁺ + H ⁺	-13.5
RaSO ₄	Ra ⁺² + SO ₄ ⁻² = RaSO ₄	2.76
RaCO ₃	Ra ⁺² + CO ₃ ⁻² = RaCO ₃	2.5
RaCl ⁺	Ra ⁺² + Cl ⁻ = RaCl ⁺	-0.1
RaCl ₂	Ra ⁺² + 2Cl ⁻ = RaCl ₂	-0.05

Surface complexation reactions onto HFO for radium (as Ra⁺²) generally use the same values as Ba⁺². However, for this database values were recalculated and slight differences were noted. According to the model proposed by Dzombak and Morel, divalent cations form outer sphere complexes with the strong surface sites (designated as Hfo_sOH) and inner sphere complexes

with the weak sites (Hfo_wOH). Using only Ca, Ba and Sr, the correlation between $\log K_{\text{MOH}}$ the strong site surface complexes was

$$\log K_1^{\text{int}} = -0.6592 * \log K_{\text{MOH}} + 5.6719$$

a $\log K_1^{\text{int}}$ of 5.3424 was noted for radium². The $\log K_1^{\text{int}}$ value for Ba⁺² was 5.46.

The value for the $\log K_2^{\text{int}}$ Reaction ($\text{Hfo_wOH} + \text{Ra}^{+2} = \text{Hfo_wORa}^{+} + \text{H}^{+}$) was based upon the overall regression equation defined in Dzombak and Morel. The calculated value for $\log K_2^{\text{int}}$ was -7.333. The $\log K_2^{\text{int}}$ value for Ba⁺² was -7.2.

² Langmuir and Riese (1985) write the radium hydrolysis reaction as $\text{Ra}^{+2} + \text{H}_2\text{O} = \text{RaOH}^{+} + \text{H}^{+}$, however Dzombak and Morel removed water from their equations and used equations of the form $\text{Ra}^{+2} + \text{OH}^{-} = \text{RaOH}^{+}$, for their correlations. Therefore, for radium the $\log K_{\text{MOH}}$ becomes 0.5, and the corresponding $\log K_{\text{MOH}}$ for barium is 0.53.

Table 1. Continued. Surface complexation reactions for uranium adsorption onto HFO and solubility product constants for selected phases.

DATABASE COMPARISON						
SPECIES	OECD NEA UPDATE	PHREEQC Databases				
	2003 Guillaumont et al.	WATEQ4F.dat	WATEQ_NEA.dat Version for this project	lnl.dat	minteq.v4.dat	minteq.dat
SURFACE COMPLEXES						
Hfo_sOUO2+	NEA does not discuss	5.2	3.736	We are using the Mahoney, Cadle and Jakubowski (2009) constants plus two reactions for carbonate surface complexation [Hfo_wOCO2-, and Hfo_wOCO2H]		
Hfo_wOUO2+		2.8	2.534			
Hfo_wOUO2CO3-			9.034			
Hfo_wOUO2(CO3)2-3			15.28			
PHASES (limited selection listed)						
UO2SO4	Free Energy provided no value for K given			1.9681		
UO2SO4:2.5H2O	1.589			-1.4912		
UO2SO4:3.5H2O	1.585			-1.4805		
UO2SO4:3H2O *	-0.831* 0.754 (recalculated)			-1.4028		
UO2SO4:H2O				-6.0233		
Schoepite (UO3:2H2O)	UO3 · 2H2O(cr) -> UO2 + 2 + 2 OH- + H2O(l) , 10,0 log s K = - (23.19 ± 0.43). Or 4.81 in proton form	5.404	5.404	4.8333	5.994	5.404

Table 1. Comparison of uranium solution complexation reactions in various databases provided with PHREEQC and selected values included in the updated database.

DATABASE COMPARISON						
SPECIES	OECD NEA UPDATE	PHREEQC Databases				
	2003 Guillaumont et al.	WATEQ4F.dat	WATEQ_NEA.dat Version for this project	lnf.dat	minteq.v4.dat	minteq.dat
all digits retained in table to facilitate traceability	Equation signs retained as in original; data is mainly from Table 3-2. To reduce error these values were mainly copied and pasted into cells	CO3-2 is component		HCO3- is component using CO3-2 as component		
CO3-2 HCO3- reaction		10.329		-10.3288	10.329	10.33
UO2OH+	-5.250	-5.2	-5.250	-5.2073	-5.897	-5.09
UO2(OH)2(aq)	-12.150		-12.150	-10.3146		
UO2(OH)3-	-20.250	-19.2	-20.250	-19.2218		
UO2(OH)4--	-32.400	-33	-32.400	-33.0291		
UO2CO3(aq)	9.94	9.63	9.94	-0.6634	9.6654	9.6
UO2(CO3)2--	16.61	17.0	16.61	-3.7467	16.9109	16.9
UO2(CO3)3---	21.84	21.63	21.84	-9.4302	21.5562	21.6
UO2SO4(aq)	3.15	3.15	3.15	3.0703	3.18	2.709
UO2(SO4)2--	4.14	4.14	4.14	3.9806	4.3	4.183
UO2(SO4)34-	3.02					
(UO2)2OH+++	-2.700	-2.7	-2.700	-2.7072		
(UO2)2(OH)2++	-5.620	-5.62	-5.620	-5.6346	-5.574	-5.645
(UO2)3(OH)4++	-11.900	-11.9	-11.900	-11.929		
(UO2)3(OH)5+	-15.550	-15.55	-15.550	-15.5862	-15.585	-15.593
(UO2)3(OH)7-	-32.200	-31	-32.200	-31.0508		
(UO2)4(OH)7+	-21.900	-21.9	-21.900	-21.9508		
(UO2)3(CO3)6(6-)			54.00	-8.0601	53.9127	Not present
(UO2)2CO3(OH)3-	-19.010 CO2(gas) component		2UO2+2 + CO3-2 + 3H2O = (UO2)2CO3(OH)3- +3H+ log_k -0.86	-11.2229		
(UO2)3CO3(OH)3+	NOT IN NEA 2003 nor Grenthe et al. 1992					
(UO2)3(OH)5CO2+	NOT IN NEA 2003 Same as (UO2)3O(OH)2(HCO3)+			-9.6194	42.0246	
(UO2)3O(OH)2(HCO3)+	-17.500 CO2(gas) component		3UO2+2 + CO3-2 + 3H2O = (UO2)3O (OH)2(HCO3)+ +3H+ log_k 0.65	-9.7129		
(UO2)11(CO3)6(OH)12--	-72.500 CO2(gas) component		11UO2+2 + 6CO3-2 + 12H2O = (UO2)11(CO3)6(OH)12-2 +12H+ log_k 36.40	NA		
Ca2UO2(CO3)3(aq)	NEA did not select value some discussion in NEA VS they cite a range of 26.5 to 30.55, Dong and Brooks 2006 report 30.70, this value was selected		30.7			
CaUO2(CO3)3--	Dong and Brooks 2006, report 27.18 this value was selected		27.18			
MgUO2(CO3)3-2	Dong and Brooks 2006, 25.8 This value was selected		25.8			

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