

In July, 2006 the NRC issued draft Regulatory Guide 1144 on how to apply environmental correction factors for fatigue. The regulatory guide said to use the equations in draft NUREG-6909, which was also issued for review about this time. This sheet compares the calculations per RG-6906 and the previous guidance in Reg Guides 6583 and 5704.

The result is a slightly higher Fen for CS, a slightly lower Fen for LAS, and a much lower Fen for SS.

6909 (A.2)
6583 (6.5a)

6909 (A.4)

6909 (A.5)

6909 (A.6)

6909 (A.7)

6909 (A.8)

6583 (5.5a)

6583 (5.5b)

6583 (5.5c)

6583 (5.5d)

6909
6583

Note the new reg guide uses formula similar (but different) to NUREG-6717 without a term for ambient temperature.

CARBON STEEL

$$F_{en} = \exp(0.632 - 0.101 S^* T^* O^* \dot{\epsilon}^*)$$

$$F_{en} = \exp(0.585 - 0.00124 T - 0.101 S^* T^* O^* \dot{\epsilon}^*)$$

$$S^* = S$$

$$S^* = 0.015$$

$$T^* = 0$$

$$T^* = T - 150$$

$$O^* = 0$$

$$O^* = \ln(DO/0.04)$$

$$O^* = \ln(12.5)$$

$$\dot{\epsilon} = 0$$

$$\dot{\epsilon} = \ln(e)$$

$$\dot{\epsilon} = \ln(0.001)$$

If strain amplitude is less than 0.07% then $F_{en} = 1$

$$S^* = S$$

$$S^* = 0.015$$

$$T^* = 0$$

$$T^* = T - 150$$

$$O^* = 0$$

$$O^* = \ln(DO/0.04)$$

$$O^* = \ln(12.5)$$

$$\dot{\epsilon} = 0$$

$$\dot{\epsilon} = \ln(\dot{\epsilon})$$

$$\dot{\epsilon} = \ln(0.001)$$

Example:

S

T

O

$\dot{\epsilon}$

S^*

T^*

O^*

$\dot{\epsilon}^*$

F_{en}

F_{en}

$$\begin{array}{l} \leq S \leq 0.015 \text{ wt\%} \\ 0.015 < S \text{ wt\%} \end{array}$$

$$\begin{array}{l} T < 150 \text{ }^\circ\text{C} \\ 150 \leq T \leq 350 \text{ }^\circ\text{C} \end{array}$$

$$\begin{array}{l} DO \leq 0.04 \text{ ppm} \\ 0.04 < DO \leq 0.5 \text{ ppm} \\ 0.5 < DO \text{ ppm} \end{array}$$

$$\begin{array}{l} 1 < \dot{\epsilon} \text{ \%/s} \\ 0.001 \leq \dot{\epsilon} \leq 1 \text{ \%/s} \\ \dot{\epsilon} < 0.001 \text{ \%/s} \end{array}$$

$$\begin{array}{l} 0 < S \leq 0.015 \text{ wt\%} \\ 0.015 < S \text{ wt\%} \end{array}$$

$$\begin{array}{l} T < 150 \text{ }^\circ\text{C} \\ 150 \leq T \leq 350 \text{ }^\circ\text{C} \end{array}$$

$$\begin{array}{l} DO < 0.05 \text{ ppm} \\ 0.05 \leq DO \leq 0.5 \text{ ppm} \\ 0.5 < DO \text{ ppm} \end{array}$$

$$\begin{array}{l} 1 < \dot{\epsilon} \text{ \%/s} \\ 0.001 \leq \dot{\epsilon} \leq 1 \text{ \%/s} \\ \dot{\epsilon} < 0.001 \text{ \%/s} \end{array}$$

0.015

185

0.1

0.001

0.015

35

0.916290732

-6.907755279

2.631679883

2.434210274

LOW ALLOY STEEL

$$6909 \text{ (A.3)} \quad F_{en} = \exp(0.702 - 0.101 S^* T^* O^* \dot{\epsilon}^*)$$

$$6583 \text{ (6.5b)} \quad F_{en} = \exp(0.929 - 0.00124 T - 0.101 S^* T^* O^* \dot{\epsilon}^*)$$

$$6909 \text{ (A.4)} \quad \begin{array}{l} S^* = S \\ S^* = 0.015 \end{array}$$

$$6909 \text{ (A.5)} \quad \begin{array}{l} T^* = 0 \\ T^* = T - 150 \end{array}$$

$$6909 \text{ (A.6)} \quad \begin{array}{l} O^* = 0 \\ O^* = \ln(DO/0.04) \\ O^* = \ln(12.5) \end{array}$$

$$6909 \text{ (A.7)} \quad \begin{array}{l} \dot{\epsilon} = 0 \\ \dot{\epsilon} = \ln(e) \\ \dot{\epsilon} = \ln(0.001) \end{array}$$

6909 (A.8) If strain amplitude is less than 0.07% then $F_{en} = 1$

$$6583 \text{ (5.5a)} \quad \begin{array}{l} S^* = S \\ S^* = 0.015 \end{array}$$

$$6583 \text{ (5.5b)} \quad \begin{array}{l} T^* = 0 \\ T^* = T - 150 \end{array}$$

$$6583 \text{ (5.5c)} \quad \begin{array}{l} O^* = 0 \\ O^* = \ln(DO/0.04) \\ O^* = \ln(12.5) \end{array}$$

$$6583 \text{ (5.5d)} \quad \begin{array}{l} \dot{\epsilon} = 0 \\ \dot{\epsilon} = \ln(\dot{\epsilon}) \\ \dot{\epsilon} = \ln(0.001) \end{array}$$

Example:

S

T

O

$\dot{\epsilon}$

S^*

T^*

O^*

$\dot{\epsilon}^*$

6909 F_{en}

6583 F_{en}

Stainless Steel

6909 (A.3) $F_{en} = \exp(0.734 - T' O' \dot{\epsilon}')$

5704 (13) $F_{en} = \exp(0.935 - T' O' \dot{\epsilon}')$

$$\begin{aligned} & \leq S \leq 0.015 \text{ wt\%} \\ 0.015 & < S & \text{wt\%} \end{aligned}$$

$$\begin{aligned} & T < 150 \text{ }^{\circ}\text{C} \\ 150 & \leq T \leq 350 \text{ }^{\circ}\text{C} \end{aligned}$$

$$\begin{aligned} & DO \leq 0.04 \text{ ppm} \\ 0.04 & < DO \leq 0.5 \text{ ppm} \\ 0.5 & < DO & \text{ppm} \end{aligned}$$

$$\begin{aligned} & 1 < \dot{\epsilon} \text{ \% / s} \\ 0.001 & \leq \dot{\epsilon} \leq 1 \text{ \% / s} \\ & \dot{\epsilon} < 0.001 \text{ \% / s} \end{aligned}$$

$$\begin{aligned} 6909 \text{ (A.10)} \quad & T' = 0 \\ & T' = (T - 150) / 175 \\ & T' = 1 \end{aligned}$$

6909 (A.12) $O' = 0.281$

$$\begin{aligned} 6909 \text{ (A.11)} \quad & \dot{\epsilon}' = 0 \\ & \dot{\epsilon}' = \ln(e/0.4) \\ & \dot{\epsilon}' = \ln(0.0004/0.4) \end{aligned}$$

6909 (A.13) If strain amplitude is less than 0.10% then $F_{en} = 1$

$$\begin{aligned} & T < 150 \text{ }^{\circ}\text{C} \\ 150 & \leq T \leq 325 \text{ }^{\circ}\text{C} \\ 325 & < T \end{aligned}$$

all DO all ppm

$$\begin{aligned} & 0.4 < \dot{\epsilon} \text{ \% / s} \\ 0.0004 & \leq \dot{\epsilon} \leq 0.4 \text{ \% / s} \\ & \dot{\epsilon} < 0.0004 \text{ \% / s} \end{aligned}$$

$$\begin{aligned} & 0 < S \leq 0.015 \text{ wt\%} \\ 0.015 & < S & \text{wt\%} \end{aligned}$$

$$\begin{aligned} & T < 150 \text{ }^{\circ}\text{C} \\ 150 & \leq T \leq 350 \text{ }^{\circ}\text{C} \end{aligned}$$

$$\begin{aligned} & DO < 0.05 \text{ ppm} \\ 0.05 & \leq DO \leq 0.5 \text{ ppm} \\ 0.5 & < DO & \text{ppm} \end{aligned}$$

$$\begin{aligned} & 1 < \dot{\epsilon} \text{ \% / s} \\ 0.001 & \leq \dot{\epsilon} \leq 1 \text{ \% / s} \\ & \dot{\epsilon} < 0.001 \text{ \% / s} \end{aligned}$$

$$\begin{aligned} 5704 \text{ (8a)} \quad & T' = 0 \\ & T' = 1 \end{aligned}$$

$$\begin{aligned} 5704 \text{ (8c)} \quad & O' = 0.260 \\ & O' = 0.172 \end{aligned}$$

$$\begin{aligned} 5704 \text{ (8b)} \quad & \dot{\epsilon}^* = 0 \\ & \dot{\epsilon}^* = \ln(\dot{\epsilon}/0.04) \\ & \dot{\epsilon}^* = \ln(0.004/0.4) \end{aligned}$$

$$\begin{aligned} & T < 200 \text{ }^{\circ}\text{C} \\ 200 & \leq T & \text{ }^{\circ}\text{C} \end{aligned}$$

$$\begin{aligned} & DO < 0.05 \text{ ppm} \\ 0.05 & \leq DO & \text{ppm} \end{aligned}$$

$$\begin{aligned} & 0.4 < \dot{\epsilon} \text{ \% / s} \\ 0.0004 & \leq \dot{\epsilon} \leq 0.4 \text{ \% / s} \\ & \dot{\epsilon} < 0.0004 \text{ \% / s} \end{aligned}$$

Example:

0.015
185
0.1
0.001

0.015
35
0.916290732
-6.907755279

T
O
 $\dot{\epsilon}$
6909 T'
6909 O'
6909 $\dot{\epsilon}'$
6583 T'
6583 O'
6583 $\dot{\epsilon}'$

6909 F_{en}
6583 F_{en}

280
0.005
0.001
0.742857143
0.281
-6.91
1
0.26
-6.91

8.81
15.34847887

Location	Unit 2
Bottom head to shell	0.004
Primary nozzles - inlet	0.05
Primary nozzles - outlet	0.281
Surge Line	
Charging system nozzle	
Safety Injection nozzle	
RHR piping	

Per NUREG/CR-6583
Low Alloy Steel (Bottom head to shell, Inlet Nozzle, Outlet Nozzle)

	Parameter	INPUTs
All	Ambient Temp	25
Bottom Head	Sulfur Content	0.025
Inlet Nozzle	Sulfur Content	0.020
Outlet Nozzle	Sulfur Content	0.020
Bottom Head	Outlet Temp	538.2
		281
Inlet Nozzle	Inlet Temp	538.2
		281
Outlet Nozzle	Vessel Temp	609
		321
All	Diss. Oxygen	0.005
All	Strain Rate	0.001
	Environmental Correction Factor (Fen) for Low Alloy Steel:	
Bottom Head		Fen = 2.45
Inlet Nozzle		Fen = 2.45
Outlet Nozzle		Fen = 2.45

Per NUREG/CR-5704
Austinitic Stainless Steel (Surge Line, Charging system nozzle, SI nozzle, RHR piping)

	Parameter	INPUTs
	Surge line Temperature	653
		345
Charging system nozzle	Temperature	538.2
		281
Safety Injection nozzle	Temperature	538.2
		281
RHR piping	Temperature	605.8
		319
All	Diss. Oxygen	0.005
All	Strain Rate	0.0004
	Environmental Correction Factor (Fen) for Stainless Steel:	
Surge line		Fen = 15.35
Charging system nozzle		Fen = 15.35
Safety Injection nozzle		Fen = 15.35
RHR piping		Fen = 15.35

Unit 3		
0.02	BH	LAS
0.049	PIN	LAS
0.259	PON	LAS
		SS
		SS
		SS
		SS

units	Factor	Value	Basis		
deg C					
wt %		0.015	Highest sulphur for Lower Shell, don't have lower head sulphur (RVID2)		
wt %	S* =	0.015	Highest sulphur for Intermediate Shell, Need Inlet Nozzle Sulphur (RVID2)		
wt %		0.015	Highest sulphur for Intermediate Shell, Need Outlet Nozzle Sulphur (RVID2)		
deg F	T* =	131.2	FSAR Table 3.2-6, vessel inlet		
deg C					
deg F	T* =	131.2	FSAR Table 3.2-6, vessel inlet		
deg C					
deg F	T* =	170.6	FSAR Table 3.2-6, vessel inlet		
deg C					
ppm	O* =	0.0	≤5 ppb per CH-SQ-13.017, Rev 2		
%/w	e* =	-6.91	assume bounding value of 0.001		
				CUFs	Fen EAF CUF
Bottom Head to shell				0.004	2.45 0.01
Inlet Nozzle				0.050	2.45 0.12
Outlet Nozzle				0.281	2.45 0.69

units	Factor	Value	Basis		
deg F	T' =	1	FSAR Table 4.1-3		
deg C					
deg F	T' =	1	FSAR Table 3.2-6, cold leg temp		
deg C					
deg F	T' =	1	FSAR Table 3.2-6, cold leg temp		
deg C					
deg F	T' =	1	FSAR Table 3.2-6, hot leg temp		
deg C					
ppm	O* =	0.260	≤5 ppb per CH-SQ-13.017, Rev 2		
%/w	e' =	-6.91	assume bounding value of 0.0004		
				CUF	Fen EAF CUF
Surge line				15.35	0.00
Charging system nozzle				15.35	0.00
Safety Injection nozzle				15.35	0.00
RHR piping				15.35	0.00

Per NUREG/CR-6909

Low Alloy Steel (Bottom head to shell, Inlet Nozzle, Outlet Nozzle)

	Parameter	INPUTs	units	Factor	Value
All					
Bottom Head	Sulfur Content	0.025	wt %		0.015
Inlet Nozzle	Sulfur Content	0.020	wt %	S*	0.015
Outlet Nozzle	Sulfur Content	0.020	wt %		0.015
Bottom Head	Outlet Temp	538.2	deg F	T*	131
		281	deg C		
Inlet Nozzle	Inlet Temp	538.2	deg F	T*	131
		281	deg C		
Outlet Nozzle	Vessel Temp	538.2	deg F	T*	131
		281	deg C		
All	Diss. Oxygen	0.005	ppm	O*	0.0
All	Strain Rate	0.001	%/w	e*	-6.9
	Environmental Correction Factor (Fen) for Low Alloy Steel:				
Bottom Head		Fen = 2.02	Bottom Head to shell		
Inlet Nozzle		Fen = 2.02	Inlet Nozzle		
Outlet Nozzle		Fen = 2.02	Outlet Nozzle		

Per NUREG/CR-6909

Austenitic Stainless Steel (Surge Line, Charging system nozzle, SI nozzle, RHR piping)

	Parameter	INPUTs	units	Factor	Value
	Surge line Temperature	653	deg F	T'	1.00
		345	deg C		
Charging system nozzle	Temperature	538.2	deg F	T'	0.75
		281	deg C		
Safety Injection nozzle	Temperature	538.2	deg F	T'	0.75
		281	deg C		
RHR piping	Temperature	605.8	deg F	T'	0.96
		319	deg C		
All	Diss. Oxygen	NA	ppm	O*	0.281
All	Strain Rate	0.0004	%/w	e'	-6.91
	Environmental Correction Factor (Fen) for Stainless Steel:				
Surge line		Fen = 14.51	Surge line		
Charging system nozzle		Fen = 8.93	Charging system nozzle		
Safety Injection nozzle		Fen = 8.93	Safety Injection nozzle		
RHR piping		Fen = 13.55	RHR piping		

Basis

Highest sulphur for Lower Shell, don't have lower head sulphur (RVID2)
Highest sulphur for Intermediate Shell, Need Nozzle Sulphur (RVID2)
Highest sulphur for Intermediate Shell, Need Nozzle Sulphur (RVID2)

FSAR Table 3.2-6, vessel inlet

FSAR Table 3.2-6, vessel inlet

FSAR Table 3.2-6, vessel inlet

≤5 ppb per CH-SQ-13.017, Rev 2

assume bounding value of 0.001

CUFs	Fen	EAFCUF
0.004	2.02	0.01
0.050	2.02	0.10
0.281	2.02	0.57

Basis

FSAR Table 4.1-3

FSAR Table 3.2-6, cold leg temp

FSAR Table 3.2-6, cold leg temp

FSAR Table 3.2-6, hot leg temp

6906 uses 0.281 for all oxygen levels.

assume bounding value of 0.0004

CUF	Fen	EAFCUF
	14.51	0.00
	8.93	0.00
	8.93	0.00
	13.55	0.00

NUREG-6260 Location

IP3 Specific Location

- Primary nozzles - inlet
- outlet
- Bottom head to shell
- Pressurizer Surge Line
- RCS Piping Charging Nozzle
- RCS Piping SIS nozzle
- RHR Class 1 Piping

Per NUREG/CR-6583
Low Alloy Steel (Bottom head to shell, Inlet Nozzle, Outlet Nozzle)

Parameter	
All	Ambient Temperature
Bottom Head	Sulfur Content
Inlet Nozzle	Sulfur Content
Outlet Nozzle	Sulfur Content
Bottom Head	Vessel Temp
Inlet Nozzle	Inlet Temp
Outlet Nozzle	Outlet Temp
All	Diss. Oxygen
All	Strain Rate
Environmental Correction Factor (Fen) for Low Alloy Steel:	
Fen =	
Fen =	
Fen =	

Per NUREG/CR-5704
Austinitic Stainless Steel (Surge Line, Charging system nozzle, SI nozzle, RHR piping)

Parameter	
Pressurizer Surge Line	Temperature
RCS piping charging system nozzle	Temperature
RCS piping safety injection nozzle	Temperature
RHR Class 1 piping	Temperature
Diss. Oxygen	
Strain Rate	
Environmental Correction Factor (Fen) for Stainless Steel:	
Pressurizer Surge Line	Fen =
RCS piping charging system nozzle	Fen =
RCS piping safety injection nozzle	Fen =
RHR Class 1 piping	Fen =

Carbon Steel

Material
Type Unit 3

0.05 0.049 LAS
0.281 0.259 LAS
0.004 0.02 LAS
SS
SS
SS
SS

INPUTs units Factor Value Basis

25 deg C
0.026 wt % 0.015 Highest sulphur for Lower Shell, don't have lower head sulphur (RVID2)
0.025 wt % S* = 0.015 Highest sulphur for Intermediate Shell, Need Inlet Nozzle Sulphur (RVID2)
0.025 wt % 0.015 Highest sulphur for Intermediate Shell, Need Outlet Nozzle Sulphur (RVID2)
540.7 deg F T* = 133 FSAR Table 4.1-4, cold leg temp
283 deg C
540.7 deg F T* = 133 FSAR Table 4.1-4, cold leg temp
283 deg C
603 deg F T* = 167 FSAR Table 4.1-4, hot leg temp
317 deg C
0.005 ppm O* = 0.0 ≤5 ppb per CH-SQ-13.017, Rev 2
0.001 %/w e* = -6.9 assume bounding value of 0.001

		CUFs	Fen	EAf CUF
2.45	Bottom Head to Shell	0.020	2.45	0.05
2.45	Inlet Nozzle	0.049	2.45	0.12
2.45	Outlet Nozzle	0.259	2.45	0.64

INPUTs units Factor Value Basis

653 deg F T' = 1 FSAR Table 4.1-3, Pzr design temp
345 deg C
540.7 deg F T' = 1 FSAR Table 4.1-4, cold leg temp
283 deg C
540.7 deg F T' = 1 FSAR Table 4.1-4, cold leg temp
283 deg C
602.5 deg F T' = 1 FSAR Table 4.1-4, hot leg temp
317 deg C
0.005 ppm O* = 0.260 ≤5 ppb per CH-SQ-13.017, Rev 2
0.0004 %/w e' = -6.9078 assume bounding value of 0.0004

		CUF	Fen	EAf CUF
15.35			15.35	0.00
15.35			15.35	0.00
15.35			15.35	0.00
15.35			15.35	0.00

Per NUREG/CR-6909
Low Alloy Steel (Bottom head to shell, Inlet Nozzle, Outlet Nozzle)

Parameter		INPUTs units	
Bottom Head	Sulfur Content	0.026	wt %
Inlet Nozzle	Sulfur Content	0.025	wt %
Outlet Nozzle	Sulfur Content	0.025	wt %
Bottom Head	Vessel Temp	540.7	deg F
		283	deg C
Inlet Nozzle	Inlet Temp	540.7	deg F
		283	deg C
Outlet Nozzle	Outlet Temp	540.7	deg F
		283	deg C
All	Diss. Oxygen	0.005	ppm
All	Strain Rate	0.001	%/w
Environmental Correction Factor (Fen) for Low Alloy Steel:			
		Fen = 2.02	Bottom Head to Shell
		Fen = 2.02	Inlet Nozzle
		Fen = 2.02	Outlet Nozzle

Per NUREG/CR-6909
Austenitic Stainless Steel (Surge Line, Charging system nozzle, SI nozzle, RHR piping)

Parameter		INPUTs units	
Pressurizer Surge Line Temperature		653	deg F
		345	deg C
RCS piping charging system nozzle Temperature		540.7	deg F
		283	deg C
RCS piping safety injection nozzle Temperature		540.7	deg F
		283	deg C
RHR Class 1 piping Temperature		602.5	deg F
		317	deg C
		Diss. Oxygen	0.005 ppm
		Strain Rate	0.0004 %/w
Environmental Correction Factor (Fen) for Stainless Steel:			
Pressurizer Surge Line		Fen = 14.51	
RCS piping charging system nozzle		Fen = 9.07	
RCS piping safety injection nozzle		Fen = 9.07	
RHR Class 1 piping		Fen = 13.27	

Factor Value Basis

0.015 Highest sulphur for Lower Shell, don't have lower head sulphur (RVID2)
S* = 0.015 Highest sulphur for Intermediate Shell, Need Nozzle Sulphur (RVID2)
0.015 Highest sulphur for Intermediate Shell, Need Nozzle Sulphur (RVID2)

T* = 133 FSAR Table 4.1-4, cold leg temp
T* = 133 FSAR Table 4.1-4, cold leg temp
T* = 133 FSAR Table 4.1-4, cold leg temp

O* = 0.0 ≤5 ppb per CH-SQ-13.017, Rev 2
e* = -6.9 assume bounding value of 0.001

CUFs	Fen	EAf CUF
0.020	2.02	0.04
0.049	2.02	0.10
0.259	2.02	0.52

Factor Value Basis

T' = 1.00 FSAR Table 4.1-3, Pzr design temp

0.76 FSAR Table 4.1-4, cold leg temp

0.76 FSAR Table 4.1-4, cold leg temp

0.95 FSAR Table 4.1-4, hot leg temp

O* = 0.281
e' = -6.91 assume bounding value of 0.0004

CUF	Fen	EAf CUF
	14.51	0.00
	9.07	0.00
	9.07	0.00
	13.27	0.00

Dissolved Oxygen

CARBON STEEL

NUREG/CR-6717

O* = 0

O* = ln(DO/0.04)

O* = ln(12.5)

DO < 0.04 ppm

0.04 ≤ DO ≤ 0.5 ppm

DO > 0.5 ppm

NUREG/CR-6583

O* = 0

O* = ln(DO/0.04)

O* = ln(12.5)

DO < 0.05 ppm

0.05 ppm ≤ DO ≤ 0.5 ppm

DO > 0.5 ppm

STAINLESS STEEL

NUREG/CR-6717

O' = 0.260

O' = 0

DO < 0.05 ppm

DO ≥ 0.05 ppm

NUREG/CR-5704

O* = 0.260

O* = 00.172

DO < 0.05 ppm

DO ≥ 0.05 ppm

NOTE:

Higher Oxygen is bad for Carbon Steel but good for Stainless Steel.

Assuming DO < 0.05 ppm is conservative for Stainless Steel

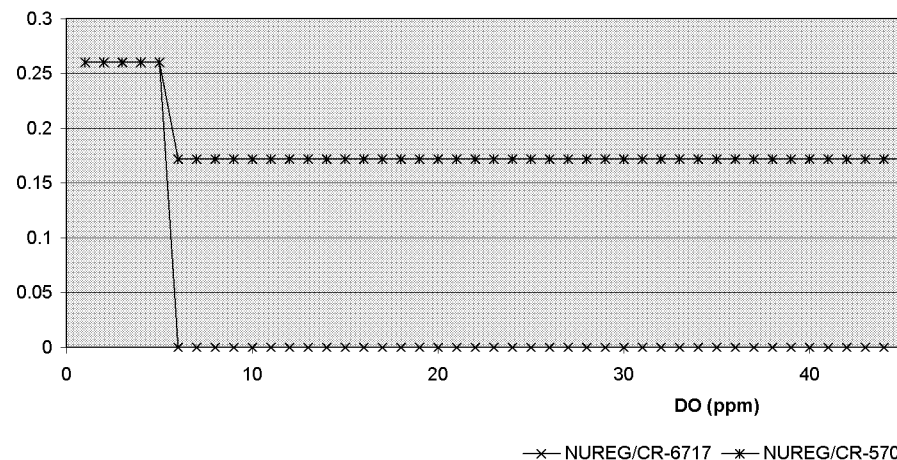
Assuming DO > 0.5 ppm is conservative for Carbon Steel

Date Submitted: December 22, 2011

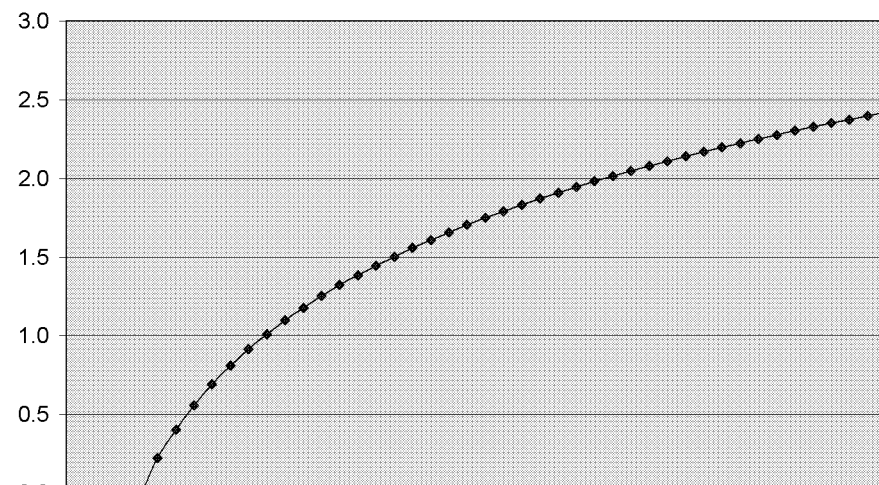
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Reg Guide	CS 6717	CS 6583	SS 6717	SS 5704
DO (ppm)	O*	O*	O'	O*
0.00	0.0	0.0	0.26	0.26
0.01	0.0	0.0	0.26	0.26
0.02	0.0	0.0	0.26	0.26
0.03	0.00	0.00	0.26	0.26
0.04	0.00	0.00	0.26	0.26
0.05	0.22	0.22	0	0.17
0.06	0.41	0.41	0	0.17
0.07	0.6	0.6	0	0.17
0.08	0.7	0.7	0	0.17
0.09	0.8	0.8	0	0.17
0.10	0.9	0.9	0	0.17
0.11	1.0	1.0	0	0.17
0.12	1.1	1.1	0	0.17
0.13	1.2	1.2	0	0.17
0.14	1.3	1.3	0	0.17
0.15	1.3	1.3	0	0.17
0.16	1.4	1.4	0	0.17
0.17	1.4	1.4	0	0.17
0.18	1.5	1.5	0	0.17
0.19	1.6	1.6	0	0.17
0.20	1.6	1.6	0	0.17
0.21	1.7	1.7	0	0.17
0.22	1.7	1.7	0	0.17
0.23	1.7	1.7	0	0.17
0.24	1.8	1.8	0	0.17
0.25	1.8	1.8	0	0.17
0.26	1.9	1.9	0	0.17
0.27	1.9	1.9	0	0.17
0.28	1.9	1.9	0	0.17
0.29	2.0	2.0	0	0.17
0.30	2.0	2.0	0	0.17
0.31	2.0	2.0	0	0.17
0.32	2.1	2.1	0	0.17
0.33	2.1	2.1	0	0.17
0.34	2.1	2.1	0	0.17
0.35	2.2	2.2	0	0.17
0.36	2.2	2.2	0	0.17
0.37	2.2	2.2	0	0.17
0.38	2.3	2.3	0	0.17
0.39	2.3	2.3	0	0.17
0.40	2.3	2.3	0	0.17
0.41	2.3	2.3	0	0.17
0.42	2.4	2.4	0	0.17
0.43	2.4	2.4	0	0.17
0.44	2.4	2.4	0	0.17
0.45	2.4	2.4	0	0.17
0.46	2.4	2.4	0	0.17
0.47	2.5	2.5	0	0.17
0.48	2.5	2.5	0	0.17
0.49	2.5	2.5	0	0.17

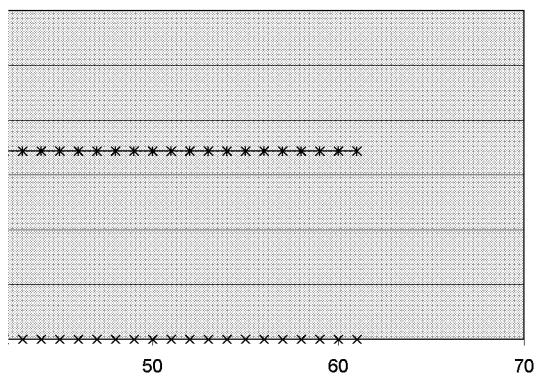
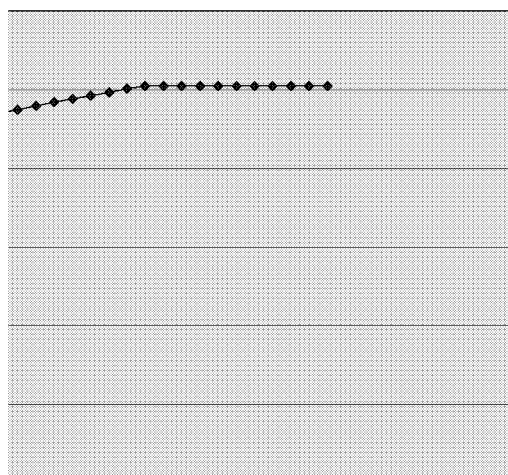
Oxygen Factor for STAINLESS STEEL



O* for CARBON STEEL



IPEC00012550

EEL**R-5704**

0.50	2.5	2.5	0	0.17
0.51	2.5	2.5	0	0.17
0.52	2.5	2.5	0	0.17
0.53	2.5	2.5	0	0.17
0.54	2.5	2.5	0	0.17
0.55	2.5	2.5	0	0.17
0.56	2.5	2.5	0	0.17
0.57	2.5	2.5	0	0.17
0.58	2.5	2.5	0	0.17
0.59	2.5	2.5	0	0.17
0.60	2.5	2.5	0	0.17

