

RS-11-137

10 CFR 50.90

August 25, 2011

U. S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
Washington, DC 20555-0001

Braidwood Station, Units 1 and 2  
Facility Operating License Nos. NPF-72 and NPF-77  
NRC Docket Nos. STN 50-456 and STN 50-457

Byron Station, Units 1 and 2  
Facility Operating License Nos. NPF-37 and NPF-66  
NRC Docket Nos. STN 50-454 and STN 50-455

Subject: Supplemental Information Supporting Request for License Amendment  
Regarding Measurement Uncertainty Recapture Power Uprate

- References:
1. Letter from Craig Lambert (Exelon Generation Company, LLC) to U. S. NRC, "Request for License Amendment Regarding Measurement Uncertainty Recapture Power Uprate," dated June 23, 2011
  2. Letter from N. J. DiFrancesco (U. S. NRC) to M. J. Pacilio (Exelon Generation Company, LLC), "Braidwood Station, Unit Nos. 1 and 2 and Byron Station, Unit Nos. 1 and 2 – Supplemental Information Needed for Acceptance of Licensing Action Regarding Measurement Uncertainty Recapture Power Uprate (TAC Nos. ME6587, ME6588, ME6589, and ME6590)," dated August 22, 2011

In Reference 1, Exelon Generation Company, LLC (EGC) requested an amendment to Facility Operating License Nos. NPF-72, NPF-77, NPF-37 and NPF-66 for Braidwood Station, Units 1 and 2, and Byron Station, Units 1 and 2, respectively. Specifically, the proposed changes revise the Operating License and Technical Specifications to implement an increase in rated thermal power of approximately 1.63%. In Reference 2, the NRC requested supplemental information to support review of the proposed changes. In response to this request, EGC is providing the attached information.

EGC has reviewed the information supporting a finding of no significant hazards consideration and the environmental consideration provided to the NRC in Reference 1. The additional information provided in this submittal does not affect the bases for concluding that the proposed license amendment does not involve a significant hazards consideration. In addition, the

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additional information provided in this submittal does not affect the bases for concluding that neither an environmental impact statement nor an environmental assessment needs to be prepared in connection with the proposed amendment.

In response to the NRC's request to provide certain information in electronic format, included with this submittal are two CDs in Attachments 6 and 7 as noted below, for submission to the Public Document Room. A second copy of these CDs is being sent to the NRC Project Manager, NRR – Braidwood and Byron Stations, for NRC Staff use.

There are no regulatory commitments contained in this letter.

Should you have any questions concerning this letter, please contact Mr. Joseph A. Bauer at (630) 657-3376.

I declare under penalty of perjury that the foregoing is true and correct. Executed on the 25<sup>th</sup> day of August 2011.

Respectfully,



Kevin F. Borton  
Manager, Licensing - Power Uprate

Attachments:

Attachment 1: Response to Request for Supplemental Information

Attachment 2: Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B, Appendix BB-5:  
"Byron PAVAN Input and Output"

Attachment 3: Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B, Appendix BB-7:  
Braidwood PAVAN Input and Output

Attachment 4: Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B, Appendix BB-1:  
Byron Joint Frequency Distribution

Attachment 5: Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B, Appendix BB-2:  
Braidwood Joint Frequency Distribution

Attachment 6: CD, "Byron and Braidwood Stations, Metrological Data Files," August 25, 2011

Attachment 7: CD, "Byron and Braidwood Stations, PAVAN Input Files," August 25, 2011

cc: NRC Regional Administrator, Region III (Attachments 1 – 5)  
NRC Senior Resident Inspector – Braidwood Station (Attachments 1 – 5)  
NRC Senior Resident Inspector – Byron Station (Attachments 1 – 5)  
Illinois Emergency Management Agency – Division of Nuclear Safety (Attachments 1 – 5)

**ATTACHMENT 1**  
**RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION**

**NRC Request 1**

*In Attachment 5 of the EGC submittal, Page III-152, Section III.17.2.1: Main Steam Line Break Dose Evaluation, states:*

*"The atmospheric dispersion factors (X/Q) values have been updated and incorporated into the dose analysis as per the current commitment to the NRC."*

- *Provide a list of the updated atmospheric dispersion factors (X/Q values) for the Main Steam Line Break (MSLB) or provide a reference if they are included in a previously docketed submittal.*
- *Identify the limiting X/Q values selected from the list that were used in the updated dose analysis that resulted in the limiting dose for the MSLB.*

*The commitment to the NRC states that X/Q values are to be updated for finer wind speed categories.*

- *Provide any updated data files, descriptions of updated assumptions, and all inputs used to calculate the updated X/Q values for the MSLB.*
- *For large data files, provide the data in electronic format suitable for use with computer codes.*
- *For data files, assumptions, and inputs that are unchanged, cite references to the docketed items.*

**Response**

**Background**

A re-evaluation of the offsite atmospheric dispersion factor (X/Q) values was performed to support the MUR Power Uprate License Amendment Request (LAR) in accordance with a commitment made to the NRC in response to a Request for Additional Information for the Alternate Source Term (AST) LAR (Reference 1). In accordance with this commitment, the X/Q calculation was revised to reevaluate the offsite X/Q values, as related to the use of the PAVAN computer model based on finer wind speed categories provided in the latest appropriate regulatory guidance. This guidance is provided in NRC Regulatory Guide 1.23, "Meteorological Monitoring Programs for Nuclear Power Plants," Revision 1, March 2007. The use of finer wind speed categories was the only change made in the re-evaluation of the offsite X/Qs.

Control room X/Q values are unchanged and remain consistent with the values noted in the NRC's Safety Evaluation for the issuance of the AST Amendment (Reference 2), Table 1, "Byron Units 1 & 2 and Braidwood Units 1 & 2 Control Room Atmospheric Dispersion Factors."

**NRC Request:**

*Provide a list of the updated atmospheric dispersion factors (X/Q values) for the Main Steam Line Break (MSLB) or provide a reference if they are included in a previously docketed submittal.*

**Response:**

The maximum bounding updated X/Q values as calculated by PAVAN using the requirements of RG 1.23 Revision 1 are shown in Table 1. All X/Q values calculated by the PAVAN computer program are provided in Attachments 2 and 3, for Byron and Braidwood Stations, respectively.

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**Table 1 Dispersion Factors**

Release Path		Recommend X/Q (sec/m <sup>3</sup> )					
Model	Release Point	Receptor/ Intake	0-2 hour	0-8 hour	8-24 hour	1-4 day	4-30 day
PAVAN	Outer Containment Wall	EAB	6.18 E-04 (SE)	3.08 E-04 (SE)	2.17 E-04 (SE)	1.02 E-04 (SE)	3.44 E-05 (SE)
PAVAN	Midpoint between two reactors	LPZ	1.10 E-04 (W)	5.13 E-05 (W)	3.51 E-05 (W)	1.53 E-05 (W)	4.68 E-06 (W)

**NRC Request:**

*Identify the limiting X/Q values selected from the list that were used in the updated dose analysis that resulted in the limiting dose for the MSLB.*

**Response:**

The Main Steam Line Break (MSLB) analysis used the following bounding set of X/Qs for the Exclusion Area Boundary (EAB) and the Low Population Zone (LPZ):

**EAB:**

X/Q = 6.18E-04 sec/m<sup>3</sup> (0-2 hours)

**LPZ:**

X/Q = 1.10E-04 sec/m<sup>3</sup> (0-2 hours) (2-hr limiting LPZ X/Q)

X/Q = 5.13E-05 sec/m<sup>3</sup> (2-8 hours) (8-hr limiting LPZ X/Q)

X/Q = 3.51E-05 sec/m<sup>3</sup> (8-24 hours) (16-hr limiting LPZ X/Q)

X/Q = 1.53E-05 sec/m<sup>3</sup> (24-96 hours) (72-hr limiting LPZ X/Q)

X/Q = 4.68E-06 sec/m<sup>3</sup> (96-720 hours) (624-hr limiting LPZ X/Q)

**NRC Request:**

*The commitment to the NRC states that X/Q values are to be updated for finer wind speed categories.*

- *Provide any updated data files, descriptions of updated assumptions, and all inputs used to calculate the updated X/Q values for the MSLB.*
- *For large data files, provide the data in electronic format suitable for use with computer codes.*
- *For data files, assumptions, and inputs that are unchanged, cite references to the docketed items.*

**Response:**

**Design Inputs for Generation of the Limiting Updated X/Q Values Used for the MSLB Updated Dose Analysis**

The 1994-1998 Byron and Braidwood Stations meteorological tower databases were utilized for the recalculation and are identical to those previously used in the original Byron and Braidwood Stations AST LAR (Reference 3). The data was provided on a CD in Attachment 8 to



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Reference 3. This original application was supplemented, without changes to any of this data, by letters dated November 28, 2005 (Reference 4), December 9, 2005 (References 5 and 6), January 27, 2006 (Reference 7), February 13, 2006 (Reference 1), March 17, 2006 (Reference 8) and July 14, 2006 (Reference 9).

This meteorological data is provided on a CD accompanying this submittal as Attachment 6.

**Design Input (PAVAN)**

**PAVAN Modeling Analysis of EAB and LPZ X/Q**

As presented in Table 4.1.2-1, "PAVAN Modeling Options," of the original AST LAR (Reference 3), the PAVAN model contains certain model options for executing the program. The same modeling options shown in Table 4.1.2-1 of Reference 3 were applied for the re-analysis of the offsite X/Q values.

**Source/Receptor Scenarios and Configurations**

Consistent with the original AST LAR (Reference 3), at each station, the outer containment wall and the midpoint between the two reactors are the assumed release points for the EAB and LPZ, respectively.

**PAVAN Meteorological Data**

Consistent with the original AST LAR (Reference 3), Byron Station and Braidwood Station meteorological data from the five-year period, 1994-1998, were used in the PAVAN analysis. The format of PAVAN meteorological input for the updated X/Q results consists of a joint wind direction (based on sixteen 22.5 degree sectors), wind speed (11 finer wind speed intervals), and stability class (7 classes) occurrence frequency distribution. Each such meteorological joint frequency distribution for input to PAVAN was prepared as in the original AST LAR (Reference 3).

The updated X/Q results utilized 11 wind speed categories as defined in Regulatory Guide 1.23, Revision 1 with the first category identified as "calm." For both stations, the minimum non-calm wind speed was fixed at to 0.8 mph. (In Section 2.3.6.2, "Meteorological Data," of the Byron and Braidwood UFSAR's, 'calm' wind speeds were assigned a value of 0.4 mph, which is one-half of the wind measurement threshold value). A midpoint was assumed between each of the Regulatory Guide 1.23, Revision 1 wind speed categories (Nos. 2-11) to be inclusive of all monitored wind speeds. Table 2 below contains the refined Regulatory Guide 1.23, Revision 1 wind speed categories.

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**Table 2 Defined Wind Speed Category Ranges for PAVAN Modeling**

Category No.	Regulatory Guide 1.23 Rev 1 Speed Interval (m/s)	PAVAN- Assumed Speed Interval (m/s)	PAVAN Assumed Speed Interval (mph)
1 (calm)	<0.5	< 0.36	< 0.80
2	0.5-1.0	≥ 0.36 - <1.05	≥ 0.80 - <2.35
3	1.1-1.5	≥ 1.05 - <1.55	≥ 2.35 - <3.47
4	1.6-2.0	≥ 1.55 - <2.05	≥ 3.47 - <4.56
5	2.1-3.0	≥ 2.05 - <3.05	≥ 4.56 - <6.82
6	3.1-4.0	≥ 3.05 - <4.05	≥ 6.82 - <9.06
7	4.1-5.0	≥ 4.05 - <5.05	≥ 9.06 - <11.30
8	5.1-6.0	≥ 5.05 - <6.05	≥ 11.30 - <13.53
9	6.1-8.0	≥ 6.05 - <8.05	≥ 13.53 - <18.01
10	8.1-10.0	≥ 8.05 - <10.0	≥ 18.01 - <22.40
11	>10.0	≥10.0	≥22.40

Attachments 4 and 5 contain the lower and upper level wind direction, wind speed (categorized as defined in Table 2 above), and stability class joint occurrence frequency distribution tables, based on the five-year lower level meteorological databases, as used for the PAVAN modeling analysis for Byron Station and Braidwood Station, respectively. (This data is provided in two formats, the number of observations and the percent occurrence frequency). Attachments 2 and 3 contain the updated PAVAN inputs and outputs for Byron and Braidwood Stations, respectively, resulting in the X/Qs of Table 1 above.

Additionally, for the updated X/Q values, the PAVAN input electronic data files utilized are provided on a CD accompanying this submittal as Attachment 7.

## **NRC Request 2**

*In attachment 5a of the EGC submittal, Page IV-8, Table IV-1a: Summary of Comparison of AST Parameters Used in Steam Generator Tube Rupture Dose Analysis, states:*

*"All offsite X/Q values were updated for finer wind speed categories per RG 1.23 Revision 1. This was also a commitment per RS-06-01."*

*With regard to the updated atmospheric dispersion factors (X/Q values) for the steam generator tube rupture:*

- *Provide any updated data files, descriptions of updated assumptions, and all inputs used to calculate the updated X/Q values.*
- *For large data files, provide the data in electronic format suitable for use with computer codes.*
- *For data files, assumptions, and inputs that are unchanged, cite references to the docketed items.*

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**Response**

Offsite X/Q values used in the Steam Generator Tube Rupture Analysis (SGTR) are the same as those used in the MSLB analysis as described in the response to NRC Request 1 above. Descriptions of updated assumptions for the X/Qs for SGTR are the same as those for the MSLB X/Qs as described in the response to NRC Request 1 above. Also as indicated in the response to Request 1 above, the updated joint occurrence frequency distribution tables and PAVAN inputs and outputs resulting in the X/Q values shown in Table 1 in response to NRC Request 1 above, are provided in Attachments 2 through 5. Consistent with the original AST LAR (Reference 3), Byron Station and Braidwood Station meteorological data from the five-year period, 1994-1998, were used in the PAVAN analysis.

The SGTR analysis used the same bounding set of X/Qs as in the MSLB analysis as described in the response to NRC Request 1 above, which are as follows:

**EAB:**

X/Q = 6.18E-04 sec/m<sup>3</sup> (0-2 hours)

**LPZ:**

X/Q = 1.10E-04 sec/m<sup>3</sup> (0-2 hours) (2-hr limiting LPZ X/Q)

X/Q = 5.13E-05 sec/m<sup>3</sup> (2-8 hours) (8-hr limiting LPZ X/Q)

X/Q = 3.51E-05 sec/m<sup>3</sup> (8-24 hours) (16-hr limiting LPZ X/Q)

X/Q = 1.53E-05 sec/m<sup>3</sup> (24-96 hours) (72-hr limiting LPZ X/Q)

X/Q = 4.68E-06 sec/m<sup>3</sup> (96-720 hours) (624-hr limiting LPZ X/Q)

Additionally, for the updated X/Q values discussed above, the PAVAN input electronic data files utilized are provided on a CD accompanying this submittal as Attachment 7.

**NRC Request 3**

*The NRC staff has become aware through the inspection program of a current nonconformance from the current licensing and design basis for the high-energy line break analysis provided in part for review of the MUR power uprate license amendment request. In general, a licensee's corrective action program addresses deviations and nonconformances with most elements of the licensing bases. NRC staff involvement in most of these situations is through the inspection, assessment, and enforcement programs. Provided the licensee is able to correct the problem and restore compliance, nonconformance from the licensing bases are not addressed by a licensing-related process. However, in order to have confidence that the related licensing and design basis information provided in your amendment request will not change and lengthen the review process, the NRC staff requires additional information.*

- *Discuss your plans for resolving the nonconformance. In particular, address the impact of resolution on the accuracy of the information provided to the NRC staff in your submittal.*

**Response**

The turbine building high energy line break (TB HELB) analysis calculations, that supported the Measurement Uncertainty (MUR) Power Uprate LAR, used thermodynamic assumptions that enveloped both current licensed thermal power (CLTP) and MUR operating conditions. The turbine building HELB analysis assumes the most limiting high energy pipe breaks in a given area and uses mitigation (i.e., damper closure) as the coping strategy, as such, there are no high energy line break elimination evaluations in the analyses of record (AOR) for the piping in

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the turbine building. No new HELB locations were identified as a result of MUR power uprate in the piping portions in the auxiliary building including the steam tunnel.

On July 6, 2011, subsequent to the submittal of the LAR, discrepancies unrelated to power level (i.e., non-conservative damper closure times) were identified in the TB HELB calculations for those breaks that could potentially affect identified auxiliary building room locations. These discrepancies were evaluated in recent Byron Station and Braidwood Station Operability Evaluations. The Operability Evaluations used the most limiting thermodynamic properties of either the CLTP or the MUR operating conditions and therefore bound the MUR operating conditions. The Operability Evaluations concluded that there is reasonable assurance that the HELB design basis requirements of protecting Class 1E and safety-related equipment in the identified rooms are maintained.

Exelon intends to maintain the design basis for the turbine building HELB and return the plant to a condition that does not require the subject Operability Evaluations. These restoration activities are being tracked in the Byron and Braidwood Stations Corrective Action Program.

Based on the above information, the conclusions stated in the MUR Power Uprate LAR HELB analyses remain valid (i.e., the qualification of Class 1E electrical equipment in the identified auxiliary building rooms are not adversely impacted by a TB HELB).

### **NRC Request 4**

*The EGC submittal, Section V.1.D, Grid Stability, for Byron Station, states the following:*

*"Power flow simulations were performed using 2012 transmission grid models for four system load conditions. The assessment concluded that with one exception, the lowest post-contingency voltage for Byron Station is 349.1 kV, which remains above the minimum required switchyard voltage of 339.8 kV. The scenario that analyzes a unit trip with the other unit in shutdown condition and with a system load level equal to 75% of the 50/50 load forecast results in a post-contingency voltage of 331.9 kV, which is lower than the minimum required voltage of 339.8 kV. This low post contingency voltage for this scenario is an existing (pre MUR) condition and is not related to the MUR Power Uprate. PJM [Pennsylvania-New Jersey-Maryland Interconnection] real-time state estimator continuously monitors and predict grid voltages under various contingencies (e.g., unit trips). If the state estimator predicts an inadequate voltage at Byron's switchyard, the station is notified and abnormal procedure is entered."*

- *According to 10 CFR Appendix A, general design criteria (GDC) 17, both offsite and onsite power must have sufficient capacity and capability. Confirm how GDC 17 requirements are met in the above-discussed contingency.*
- *Justify the acceptability of using the methodology of a Transmission Operator (PJM state estimator) notifying the licensee of any inadequate voltage prediction and then entering the abnormal procedure. The offsite power must be capable to cope with any simultaneous (N-1 grid) contingency and postulated design basis accident. Discuss your plans for resolving the above issue for pre and post MUR conditions.*

### **Response**

#### **Background**

On February 1, 2006, the NRC issued NRC Generic Letter (GL) 2006-02, "Grid Reliability and the Impact on Plant Risk and the Operability of Offsite Power." Exelon responded to the GL in a

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letter from K. R. Jury (EGC) to the NRC, "EGC/AmerGen 60-Day Response to NRC Generic Letter 2006-02, "Grid Reliability and the Impact on Plant Risk and the Operability of Offsite Power," dated April 3, 2006; as supplemented by a January 31, 2007 letter from K. R. Jury (EGC) to the NRC, "EGC/AmerGen Response to the Request for Additional Information Regarding Resolution of NRC Generic Letter 2006-02, 'Grid Reliability and the Impact on Plant Risk and the Operability of Offsite Power.'"

The GL requested information in four major areas, one specifically addressing use of protocols between the nuclear power plant (NPP) and the transmission system operator.

In EGC's response to GL 2006-02, a detailed discussion of these protocols was provided and is consistent with the discussion below. In summary, EGC's response to the GL concluded that all Exelon Stations were in compliance with GDC 17. The Byron Station power grid voltage analysis performed in support of the MUR Power Uprate LAR did not change this conclusion.

GDC 17 Compliance and Transmission Operator Protocol (Summary)

Exelon concludes, based on the evaluation of the Byron Station power grid voltage analysis, that the offsite power source has adequate capacity and capability to meet the requirements of GDC 17. Key information supporting this conclusion is presented below.

1. There are sufficient existing transmission system assets (capacitor banks) to maintain the lowest post contingency voltage at or above the Byron Station limit of 339.8 kV for the postulated scenario that analyzes a unit trip with the other unit in shutdown condition and with a system load level equal to 75% of the 50/50 load forecast. ComEd can remotely add these assets as necessary to maintain voltage. Standard operating protocol directs PJM and ComEd to implement all available non-cost options, (e.g., adding capacitor banks, raising the VAR output of other generating units in the area, and utilizing the local tap changers (LTCs) in the area), to mitigate the potential low voltage condition and maintain the required voltage.
2. In addition, there are other existing generating assets (off-cost generation) available to the Transmission Operator that can be placed in service to maintain the lowest post contingency voltage above the Byron Station limit. Exelon will authorize off-cost generation, if necessary, to maintain voltage above the Byron Station limit.
3. PJM (Transmission Operator) and ComEd (Transmission Owner) continuously monitor post-contingency voltages for Byron Station. The normal PJM operating protocol is for ComEd to notify Byron Station when the State Estimator program predicts post contingency switchyard voltage will fall below the Byron Station minimum required voltage. This operating protocol is controlled by PJM Operating Manuals and Byron Station procedures.

GDC 17 Compliance and Transmission Operator Protocol (Additional Detail)

Exelon reviewed the "2012 Power Grid Voltage Analysis for Byron Generating Station with MUR Power Uprate" (See Attachment 10b of the LAR) prepared by ComEd Transmission Planning and concluded that the offsite power source has adequate capacity and capability and therefore meets the requirements of GDC 17. In the 2012 Power Grid Voltage Analysis performed for Byron Station other generating assets could be online or offline depending on economics, therefore certain generating assets were conservatively modeled as offline in the grid voltage analysis. In addition, there are transmission system assets (e.g., capacitor banks) available that are conservatively not credited in the grid voltage analysis. These transmission assets can be switched on remotely and are sufficient to maintain the lowest post contingency voltage above

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the Byron Station limit for the above scenario. Appendix C, "Exelon Nuclear Offsite AC Sources Periodic Grid System Study Requirements" (Exelon's Procedure WC-AA-8003, Attachment 6), of the grid voltage analysis (Attachment 10b of the MUR Power Uprate LAR) which is used to perform the periodic grid system studies, allows crediting normally expected system adjustments, including remote switching operations, such as through Supervisory Control and Data Acquisition (SCADA), (i.e., switching operations that do not require dispatching crews to facilities).

This potential low voltage condition is an existing (pre-MUR) condition and is not related to the MUR power uprate. This possible scenario is acceptable because there are sufficient transmission assets and other generating assets in the area available to maintain voltage above the Byron Station limit. ComEd is expected to add capacitor banks as needed to maintain the lowest post contingency voltage above the Byron Station limit. In addition, Appendix B, "Byron Sensitivity Study Summary," in the grid voltage analysis (Attachment 10b of the MUR Power Uprate LAR) shows that post contingency voltage in the switchyard will remain above the 339.8 kV minimum value if some of these other generator assets are in service.

PJM and ComEd continuously monitor post-contingency voltages for nuclear power plants. PJM Manual 3, "Transmission Operations," Revision 38, Section 5, "Index and Operating Procedures for PJM RTO Operation," pages 116 through 118, discusses the Day-Ahead actions and Real-Time Operator actions for nuclear facilities. PJM performs day-ahead studies to identify reliability issues for the transmission system. As part of those studies, PJM will predict potential low voltage conditions at Byron Station and will inform Exelon. ComEd will add capacitors as needed to maintain the lowest post contingency voltage above the Byron Station limit and, if necessary, Exelon will authorize PJM to place other generating assets in the area online (off-cost generation) to resolve the potential low voltage conditions.

In addition, PJM and ComEd are monitoring post-contingency voltages real time and, if the State Estimator predicts a voltage below the minimum required on the contingency of a unit trip, actions will be proactively taken to maintain the voltage above the Byron Station limit and, if necessary, off-cost generation may be utilized to assure adequate switchyard voltage. PJM Manual 39, "Nuclear Plant Interface Coordination," Revision 3, Section 2.4, "Notification and Mitigation Protocols for NPRI Voltage Limits," discusses the notification and mitigation protocols for nuclear plant voltage limits. Byron Station enters Abnormal Operating Procedure OBOA ELEC-1, "Degraded Swyd Voltage," when notified that the State Estimator shows actual or predicted voltage is below the minimum required voltage. OBOA ELEC-1 directs the Byron Station Operator to perform evaluations based on actual Non-ESF 4 kV bus loading to determine if the predicted post Byron Station unit trip voltage or actual voltage reported by the State Estimator is adequate. If the Byron Station Operator determines that the predicted or actual voltage is inadequate, the appropriate limiting condition for operation (LCO) associated with Technical Specification 3.8.1, "AC Sources Operating," would be entered.

Based on the above information, there are sufficient existing transmission assets (capacitors) available to maintain Byron Station's post contingency voltage above the 339.8 kV minimum value and, if necessary, contingency actions are in place to utilize off-cost generation. Therefore, Exelon concludes that the offsite power source has adequate capacity and capability to meet the requirements of GDC 17.

**ATTACHMENT 1**  
**RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION**

**References:**

1. Letter from Joseph A. Bauer (EGC) to NRC, "Response to NRC Request for Additional Information With Respect to Request for License Amendment Related to Application of Alternative Radiological Source Term," dated February 13, 2006
2. Letter from R. F. Kuntz (NRC) to C. M. Crane (EGC), dated September 8, 2006 "Byron Station. Units Nos. 1 and 2 and Braidwood Station, Units Nos. 1 and 2 – Issuance of Amendments Re: Alternate Source Term (TAC Nos. MC6221, MC6222, MC6223, MC6224"
3. Letter from K. R. Jury (EGC) to NRC, "Request for License Amendment Related to Application of Alternate Source Term," dated February 15, 2005
4. Letter from Joseph A. Bauer (EGC) to NRC, "Response to NRC Request for Additional Information With Respect to Request for License Amendment Related to Application of Alternative Radiological Source Term," dated November 28, 2005
5. Letter from Joseph A. Bauer (EGC) to NRC, "Additional Information Related to Application of Alternative Radiological Source Term - Atmospheric Dispersion Coefficients," dated December 9, 2005
6. Letter from Joseph A. Bauer (EGC) to NRC, "Additional Information Related to Application of Alternative Radiological Source Term - Dose Calculations," dated December 9, 2005
7. Letter from Patrick R. Simpson (EGC) to NRC, "Response to NRC Request for Additional Information With Respect to Request for License Amendment Related to Application of Alternative Radiological Source Term," dated January 27, 2006
8. Letter from Joseph A. Bauer (EGC) to NRC, "Partial Withdrawal of Changes Related to Request for License Amendment Related to Application of Alternative Source Term," dated March 17, 2006
9. Letter from Joseph A. Bauer (EGC) to NRC Response to NRC Request for Additional Information With Respect to Request for License Amendment Related to Application of Alternative Radiological Source Term," dated July 14, 2006

## **ATTACHMENT 2**

### **Braidwood and Byron Stations Measurement Uncertainty Recapture Technical Evaluation**

#### **Response to NRC Acceptance Review Questions**

**Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B,  
Appendix BB-5: "Byron PAVAN Input and Output"**



## Byron PAVAN Input and Output

1 1111

Byron Ground Release  
9.1 meters 76.2-9.1 meters

Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

11	0														
2917.	60.7	10.0	9.1												
0	0	0	4	7	5	11									
1.	2.	0.	2.	2.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	
0.	0.	0.	0.	0.	3.	3.	1.	1.	3.	2.	6.	1.	1.	2.	0.
2.	2.	1.	2.	3.	2.	2.	1.	0.	1.	5.	4.	4.	3.	3.	1.
16.	9.	10.	7.	14.	8.	4.	15.	7.	11.	19.	10.	10.	16.	8.	13.
39.	21.	11.	9.	25.	14.	7.	21.	8.	12.	20.	9.	14.	30.	28.	18.
19.	21.	7.	12.	18.	9.	10.	21.	17.	19.	28.	23.	18.	32.	49.	18.
10.	18.	5.	8.	1.	4.	9.	10.	9.	20.	19.	15.	27.	19.	45.	20.
14.	7.	3.	16.	2.	6.	7.	25.	32.	33.	29.	25.	26.	46.	34.	14.
0.	2.	0.	6.	0.	0.	0.	5.	10.	13.	7.	3.	10.	4.	2.	1.
0.	0.	0.	0.	0.	0.	0.	1.	2.	4.	2.	1.	1.	0.	0.	0.
0.	2.	0.	2.	2.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	0.
3.	3.	0.	1.	3.	3.	2.	1.	2.	1.	0.	1.	1.	1.	2.	4.
5.	5.	1.	0.	3.	5.	3.	1.	0.	3.	2.	5.	4.	1.	3.	5.
19.	8.	5.	9.	14.	16.	9.	12.	9.	13.	22.	6.	11.	7.	18.	16.
22.	20.	8.	7.	21.	12.	22.	12.	20.	23.	29.	13.	16.	20.	34.	16.
39.	20.	9.	4.	15.	13.	15.	20.	12.	21.	31.	25.	28.	27.	42.	22.
13.	16.	3.	5.	4.	7.	10.	9.	14.	27.	22.	13.	21.	32.	27.	16.
10.	3.	8.	14.	2.	1.	4.	13.	17.	24.	14.	10.	19.	26.	23.	9.
2.	1.	0.	4.	0.	1.	5.	6.	5.	6.	4.	6.	10.	9.	3.	1.
3.	0.	0.	0.	0.	0.	0.	1.	3.	2.	3.	2.	0.	2.	0.	0.
2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
2.	1.	1.	1.	4.	2.	2.	1.	2.	2.	10.	2.	3.	3.	4.	4.
6.	14.	9.	4.	10.	9.	13.	7.	8.	7.	6.	8.	5.	5.	4.	10.
21.	10.	13.	12.	49.	25.	33.	12.	23.	41.	36.	19.	25.	29.	44.	25.
36.	26.	16.	9.	29.	14.	20.	26.	41.	36.	45.	22.	40.	40.	58.	35.
35.	17.	13.	17.	11.	12.	23.	31.	33.	38.	48.	33.	27.	45.	47.	34.
18.	12.	10.	7.	5.	2.	10.	25.	22.	28.	28.	13.	27.	41.	44.	16.
12.	9.	4.	10.	2.	3.	5.	8.	28.	30.	19.	23.	33.	43.	33.	14.
2.	2.	2.	1.	0.	2.	5.	2.	7.	7.	4.	7.	10.	17.	5.	0.
2.	0.	0.	0.	0.	0.	0.	5.	0.	3.	4.	4.	3.	2.	0.	1.
18.	25.	16.	17.	22.	13.	18.	6.	10.	16.	21.	29.	26.	32.	26.	15.
32.	40.	52.	45.	59.	49.	38.	34.	33.	33.	49.	50.	46.	64.	58.	65.
109.	85.	72.	53.	107.	79.	47.	48.	64.	68.	74.	75.	82.	107.	98.	95.
271.	186.	165.	158.	294.	162.	164.	184.	227.	225.	264.	212.	241.	312.	364.	303.
327.	175.	136.	188.	223.	120.	159.	225.	255.	205.	242.	221.	285.	359.	388.	287.
372.	211.	141.	272.	171.	115.	152.	227.	215.	190.	243.	227.	328.	371.	299.	272.
220.	133.	121.	191.	71.	62.	77.	164.	196.	156.	164.	154.	253.	314.	205.	127.
197.	185.	217.	232.	35.	79.	84.	202.	188.	221.	153.	191.	403.	318.	142.	103.
40.	36.	85.	37.	1.	30.	27.	56.	58.	76.	39.	81.	142.	136.	22.	17.

[illegible]

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USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PRINTOUT OF INPUT CARDS

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1      00010 01111 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 2      Byron
Ground Release
3      9.1 meters          76.2-9.1 meters
4
5      Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T          6          11 43655      0
7      0.500 2917.000      60.700      10.000      9.100
8      0.000 0.000 0.000 4.000 7.000 5.000 11.000
9      1.000 2.000 0.000 2.000 2.000 0.000 0.000 0.000 0.000 1.000 0.000 0.000 0.000 0.000 1.000 1.000
9      0.000 0.000 0.000 0.000 0.000 3.000 3.000 1.000 1.000 3.000 2.000 6.000 1.000 1.000 2.000 0.000
9      2.000 2.000 1.000 2.000 3.000 2.000 2.000 1.000 0.000 1.000 5.000 4.000 4.000 3.000 3.000 1.000
9      16.000 9.000 10.000 7.000 14.000 8.000 4.000 15.000 7.000 11.000 19.000 10.000 10.000 16.000 8.000 13.000
9      39.000 21.000 11.000 9.000 25.000 14.000 7.000 21.000 8.000 12.000 20.000 9.000 14.000 30.000 28.000 18.000
9      19.000 21.000 7.000 12.000 18.000 9.000 10.000 21.000 17.000 19.000 28.000 23.000 18.000 32.000 49.000 18.000
9      10.000 18.000 5.000 8.000 1.000 4.000 9.000 10.000 9.000 20.000 19.000 15.000 27.000 19.000 45.000 20.000
9      14.000 7.000 3.000 16.000 2.000 6.000 7.000 25.000 32.000 33.000 29.000 25.000 26.000 46.000 34.000 14.000
9      0.000 2.000 0.000 6.000 0.000 0.000 0.000 5.000 10.000 13.000 7.000 3.000 10.000 4.000 2.000 1.000
9      0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 2.000 4.000 2.000 1.000 1.000 0.000 0.000
9      0.000 2.000 0.000 2.000 2.000 0.000 0.000 0.000 1.000 0.000 0.000 0.000 0.000 1.000 1.000 0.000
9      3.000 3.000 0.000 1.000 3.000 3.000 2.000 1.000 2.000 1.000 0.000 1.000 1.000 1.000 2.000 4.000
9      5.000 5.000 1.000 0.000 3.000 5.000 3.000 1.000 0.000 3.000 2.000 5.000 4.000 1.000 3.000 5.000
9      19.000 8.000 5.000 9.000 14.000 16.000 9.000 12.000 9.000 13.000 22.000 6.000 11.000 7.000 18.000 16.000
9      22.000 20.000 8.000 7.000 21.000 12.000 22.000 12.000 20.000 23.000 29.000 13.000 16.000 20.000 34.000 16.000
9      39.000 20.000 9.000 4.000 15.000 13.000 15.000 20.000 12.000 21.000 31.000 25.000 28.000 27.000 42.000 22.000
9      13.000 16.000 3.000 5.000 4.000 7.000 10.000 9.000 14.000 27.000 22.000 13.000 21.000 32.000 27.000 16.000
9      10.000 3.000 8.000 14.000 2.000 1.000 4.000 13.000 17.000 24.000 14.000 10.000 19.000 26.000 23.000 9.000
9      2.000 1.000 0.000 4.000 0.000 1.000 5.000 6.000 5.000 6.000 4.000 6.000 10.000 9.000 3.000 1.000
9      3.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 3.000 2.000 3.000 2.000 0.000 2.000 0.000
9      2.000 1.000 0.000 0.000 1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000
9      2.000 1.000 1.000 1.000 4.000 2.000 2.000 1.000 2.000 2.000 10.000 2.000 3.000 3.000 4.000 4.000
9      6.000 14.000 9.000 4.000 10.000 9.000 13.000 7.000 8.000 7.000 6.000 8.000 5.000 5.000 4.000 10.000
9      21.000 10.000 13.000 12.000 49.000 25.000 33.000 12.000 23.000 41.000 36.000 19.000 25.000 29.000 44.000 25.000
9      36.000 26.000 16.000 9.000 29.000 14.000 20.000 26.000 41.000 36.000 45.000 22.000 40.000 40.000 58.000 35.000
9      35.000 17.000 13.000 17.000 11.000 12.000 23.000 31.000 33.000 38.000 48.000 33.000 27.000 45.000 47.000 34.000
9      18.000 12.000 10.000 7.000 5.000 2.000 10.000 25.000 22.000 28.000 28.000 13.000 27.000 41.000 44.000 16.000
9      12.000 9.000 4.000 10.000 2.000 3.000 5.000 8.000 28.000 30.000 19.000 23.000 33.000 43.000 33.000 14.000
9      2.000 2.000 2.000 1.000 0.000 2.000 5.000 2.000 7.000 7.000 4.000 7.000 10.000 17.000 5.000 0.000
9      2.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 5.000 0.000 3.000 4.000 4.000 3.000 2.000 0.000
9      18.000 25.000 16.000 17.000 22.000 13.000 18.000 6.000 10.000 16.000 21.000 29.000 26.000 32.000 26.000 15.000
9      32.000 40.000 52.000 45.000 59.000 49.000 38.000 34.000 33.000 33.000 49.000 50.000 46.000 64.000 58.000 65.000
9      109.000 85.000 72.000 53.000 107.000 79.000 47.000 48.000 64.000 68.000 74.000 75.000 82.000 107.000 98.000 95.000
9      271.000 186.000 165.000 158.000 294.000 162.000 164.000 184.000 227.000 225.000 264.000 212.000 241.000 312.000 364.000 303.000
9      327.000 175.000 136.000 188.000 223.000 120.000 159.000 225.000 255.000 205.000 242.000 221.000 285.000 359.000 388.000 287.000
9      372.000 211.000 141.000 272.000 171.000 115.000 152.000 227.000 215.000 190.000 243.000 227.000 328.000 371.000 299.000 272.000

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9	220.000	133.000	121.000	191.000	71.000	62.000	77.000	164.000	196.000	156.000	164.000	154.000	253.000	314.000	205.000	127.000		
9	197.000	185.000	232.000	35.000	79.000	84.000	202.000	188.000	221.000	153.000	191.000	403.000	318.000	142.000	103.000			
9	40.000	36.000	85.000	37.000	1.000	30.000	27.000	56.000	58.000	76.000	39.000	81.000	142.000	136.000	22.000	17.000		
9	16.000	4.000	16.000	0.000	0.000	7.000	1.000	21.000	2.000	14.000	27.000	44.000	98.000	32.000	0.000	0.000		
9	30.000	27.000	30.000	27.000	37.000	20.000	27.000	27.000	28.000	35.000	43.000	44.000	62.000	65.000	73.000	44.000		
9	50.000	34.000	31.000	43.000	94.000	47.000	44.000	42.000	60.000	71.000	95.000	75.000	104.000	103.000	105.000	57.000		
9	45.000	50.000	30.000	43.000	154.000	81.000	50.000	55.000	90.000	90.000	123.000	108.000	98.000	116.000	185.000	87.000		
9	152.000	122.000	86.000	128.000	329.000	171.000	201.000	221.000	257.000	208.000	216.000	180.000	251.000	218.000	192.000	199.000		
9	120.000	87.000	91.000	137.000	149.000	109.000	169.000	245.000	242.000	172.000	174.000	147.000	189.000	128.000	130.000	99.000		
9	46.000	28.000	51.000	110.000	40.000	71.000	113.000	190.000	219.000	159.000	132.000	103.000	154.000	65.000	44.000	30.000		
9	14.000	10.000	37.000	62.000	16.000	35.000	51.000	134.000	138.000	148.000	54.000	31.000	51.000	20.000	11.000	9.000		
9	6.000	4.000	8.000	36.000	7.000	39.000	24.000	105.000	143.000	142.000	44.000	21.000	38.000	8.000	3.000	5.000		
9	0.000	0.000	0.000	1.000	0.000	16.000	10.000	17.000	20.000	49.000	6.000	2.000	8.000	1.000	0.000	0.000		
9	0.000	0.000	0.000	0.000	0.000	6.000	1.000	6.000	1.000	1.000	0.000	0.000	0.000	4.000	0.000	0.000		
9	24.000	21.000	18.000	9.000	15.000	14.000	10.000	21.000	21.000	30.000	46.000	54.000	70.000	89.000	95.000	39.000		
9	31.000	12.000	7.000	11.000	54.000	34.000	30.000	42.000	66.000	73.000	66.000	69.000	113.000	78.000	126.000	64.000		
9	20.000	19.000	9.000	13.000	102.000	63.000	44.000	53.000	96.000	102.000	51.000	50.000	63.000	25.000	66.000	64.000		
9	39.000	32.000	14.000	26.000	116.000	160.000	212.000	275.000	234.000	86.000	43.000	16.000	37.000	18.000	15.000	42.000		
9	15.000	6.000	4.000	22.000	22.000	97.000	107.000	200.000	116.000	38.000	3.000	6.000	3.000	1.000	0.000	0.000		
9	1.000	1.000	0.000	8.000	1.000	20.000	20.000	100.000	41.000	4.000	2.000	2.000	2.000	0.000	0.000	0.000		
9	0.000	0.000	0.000	0.000	0.000	2.000	1.000	12.000	12.000	1.000	0.000	1.000	0.000	0.000	0.000	0.000		
9	0.000																	

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS A

WIND SPEED (M/S)

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.05 1.08	0.002	0.005	0.000	0.005	0.005	0.000	0.000	0.000	0.000	0.002	0.000	0.000	0.000	0.000	0.002	0.002	0.023
1.55 1.59	0.000	0.000	0.000	0.000	0.000	0.000	0.007	0.007	0.002	0.002	0.007	0.005	0.014	0.002	0.002	0.005	0.053
2.04 2.09	0.005	0.005	0.002	0.005	0.007	0.005	0.005	0.002	0.000	0.002	0.011	0.009	0.009	0.007	0.007	0.002	0.082
3.05 3.12	0.037	0.021	0.023	0.016	0.032	0.018	0.009	0.034	0.016	0.025	0.044	0.023	0.023	0.037	0.018	0.030	0.405
4.05 4.15	0.089	0.048	0.025	0.021	0.057	0.032	0.016	0.048	0.018	0.027	0.046	0.021	0.032	0.069	0.064	0.041	0.655
5.05 5.17	0.044	0.048	0.016	0.027	0.041	0.021	0.023	0.048	0.039	0.044	0.064	0.053	0.041	0.073	0.112	0.041	0.735
6.05 6.19	0.023	0.041	0.011	0.018	0.002	0.009	0.021	0.023	0.021	0.046	0.044	0.034	0.062	0.044	0.103	0.046	0.547
8.05 8.24	0.032	0.016	0.007	0.037	0.005	0.014	0.016	0.057	0.073	0.076	0.066	0.057	0.060	0.105	0.078	0.032	0.731
10.01 10.25	0.000	0.005	0.000	0.014	0.000	0.000	0.000	0.011	0.023	0.030	0.016	0.007	0.023	0.009	0.005	0.002	0.144
24.59 25.17	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.005	0.009	0.005	0.002	0.002	0.000	0.000	0.000	0.025
TOTAL	0.23	0.19	0.08	0.14	0.15	0.11	0.10	0.23	0.20	0.27	0.30	0.22	0.25	0.35	0.39	0.20	3.40

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS B

WIND SPEED (M/S)

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.05 1.08	0.000	0.005	0.000	0.005	0.005	0.000	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.002	0.002	0.000	0.021
1.55 1.59	0.007	0.007	0.000	0.002	0.007	0.007	0.005	0.002	0.005	0.002	0.000	0.002	0.002	0.002	0.005	0.009	0.064
2.04 2.09	0.011	0.011	0.002	0.000	0.007	0.011	0.007	0.002	0.000	0.007	0.005	0.011	0.009	0.002	0.007	0.011	0.105
3.05 3.12	0.044	0.018	0.011	0.021	0.032	0.037	0.021	0.027	0.021	0.030	0.050	0.014	0.025	0.016	0.041	0.037	0.444
4.05 4.15	0.050	0.046	0.018	0.016	0.048	0.027	0.050	0.027	0.046	0.053	0.066	0.030	0.037	0.046	0.078	0.037	0.676
5.05 5.17	0.089	0.046	0.021	0.009	0.034	0.030	0.034	0.046	0.027	0.048	0.071	0.057	0.064	0.062	0.096	0.050	0.786
6.05 6.19	0.030	0.037	0.007	0.011	0.009	0.016	0.023	0.021	0.032	0.062	0.050	0.030	0.048	0.073	0.062	0.037	0.547
8.05 8.24	0.023	0.007	0.018	0.032	0.005	0.002	0.009	0.030	0.039	0.055	0.032	0.023	0.044	0.060	0.053	0.021	0.451
10.01 10.25	0.005	0.002	0.000	0.009	0.000	0.002	0.011	0.014	0.011	0.014	0.009	0.014	0.023	0.021	0.007	0.002	0.144
24.59 25.17	0.007	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.007	0.005	0.007	0.005	0.000	0.005	0.000	0.000	0.037
TOTAL	0.27	0.18	0.08	0.11	0.15	0.13	0.16	0.17	0.19	0.27	0.29	0.19	0.25	0.29	0.35	0.20	3.28

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS C

WIND SPEED (M/S)

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.05 1.08	0.005	0.002	0.000	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.002	0.011
1.55 1.59	0.005	0.002	0.002	0.002	0.009	0.005	0.005	0.002	0.005	0.005	0.023	0.005	0.007	0.007	0.009	0.009	0.101
2.04 2.09	0.014	0.032	0.021	0.009	0.023	0.021	0.030	0.016	0.018	0.016	0.014	0.018	0.011	0.011	0.009	0.023	0.286
3.05 3.12	0.048	0.023	0.030	0.027	0.112	0.057	0.076	0.027	0.053	0.094	0.082	0.044	0.057	0.066	0.101	0.057	0.955

CALCULATION NO. BYR04-050, BRW-04-0044-M								MINOR REV. NO. 1B	APPENDIX BB-5								PAGE NO. 6 of 163	
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4.05	4.15	0.082	0.060	0.037	0.021	0.066	0.032	0.046	0.060	0.094	0.082	0.103	0.050	0.092	0.092	0.133	0.080	1.129
5.05	5.17	0.080	0.039	0.030	0.039	0.025	0.027	0.053	0.071	0.076	0.087	0.110	0.076	0.062	0.103	0.108	0.078	1.063
6.05	6.19	0.041	0.027	0.023	0.016	0.011	0.005	0.023	0.057	0.050	0.064	0.064	0.030	0.062	0.094	0.101	0.037	0.706
8.05	8.24	0.027	0.021	0.009	0.023	0.005	0.007	0.011	0.018	0.064	0.069	0.044	0.053	0.076	0.098	0.076	0.032	0.632
10.01	10.25	0.005	0.005	0.005	0.002	0.000	0.005	0.011	0.005	0.016	0.016	0.009	0.016	0.023	0.039	0.011	0.000	0.167
24.59	25.17	0.005	0.000	0.000	0.000	0.000	0.000	0.000	0.011	0.000	0.007	0.009	0.009	0.007	0.005	0.000	0.002	0.055
TOTAL		0.31	0.21	0.16	0.14	0.25	0.16	0.25	0.27	0.38	0.44	0.46	0.30	0.40	0.52	0.55	0.32	5.11

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS D

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.001	0.001	0.000	0.001	0.001	0.000	0.001	0.000	0.000	0.000	0.001	0.001	0.001	0.001	0.001	0.000	0.009
1.05 1.08	0.041	0.057	0.037	0.039	0.050	0.030	0.041	0.014	0.023	0.037	0.048	0.066	0.060	0.073	0.060	0.034	0.710
1.55 1.59	0.073	0.092	0.119	0.103	0.135	0.112	0.087	0.078	0.076	0.076	0.112	0.115	0.105	0.147	0.133	0.149	1.711
2.04 2.09	0.250	0.195	0.165	0.121	0.245	0.181	0.108	0.110	0.147	0.156	0.170	0.172	0.188	0.245	0.224	0.218	2.893
3.05 3.12	0.621	0.426	0.378	0.362	0.673	0.371	0.376	0.421	0.520	0.515	0.605	0.486	0.552	0.715	0.834	0.694	8.549
4.05 4.15	0.749	0.401	0.312	0.431	0.511	0.275	0.364	0.515	0.584	0.470	0.554	0.506	0.653	0.822	0.889	0.657	8.693
5.05 5.17	0.852	0.483	0.323	0.623	0.392	0.263	0.348	0.520	0.492	0.435	0.557	0.520	0.751	0.850	0.685	0.623	8.718
6.05 6.19	0.504	0.305	0.277	0.438	0.163	0.142	0.176	0.376	0.449	0.357	0.376	0.353	0.580	0.719	0.470	0.291	5.974
8.05 8.24	0.451	0.424	0.497	0.531	0.080	0.181	0.192	0.463	0.431	0.506	0.350	0.438	0.923	0.728	0.325	0.236	6.758
10.01 10.25	0.092	0.082	0.195	0.085	0.002	0.069	0.062	0.128	0.133	0.174	0.089	0.186	0.325	0.312	0.050	0.039	2.023
24.59 25.17	0.037	0.009	0.037	0.000	0.000	0.016	0.002	0.048	0.005	0.032	0.062	0.101	0.224	0.073	0.000	0.000	0.646
TOTAL	3.67	2.47	2.34	2.73	2.25	1.64	1.76	2.67	2.86	2.76	2.92	2.94	4.36	4.69	3.67	2.94	46.68

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS E

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.002	0.002	0.002	0.001	0.016
1.05 1.10	0.069	0.062	0.069	0.062	0.085	0.046	0.062	0.062	0.064	0.080	0.098	0.101	0.142	0.149	0.167	0.101	1.418
1.55 1.63	0.115	0.078	0.071	0.098	0.215	0.108	0.101	0.096	0.137	0.163	0.218	0.172	0.238	0.236	0.241	0.131	2.417
2.04 2.14	0.103	0.115	0.069	0.098	0.353	0.186	0.115	0.126	0.206	0.206	0.282	0.247	0.224	0.266	0.424	0.199	3.218
3.05 3.20	0.348	0.279	0.197	0.293	0.754	0.392	0.460	0.506	0.589	0.476	0.495	0.412	0.575	0.499	0.440	0.456	7.172
4.05 4.25	0.275	0.199	0.208	0.314	0.341	0.250	0.387	0.561	0.554	0.394	0.399	0.337	0.433	0.293	0.298	0.227	5.470
5.05 5.30	0.105	0.064	0.117	0.252	0.092	0.163	0.259	0.435	0.502	0.364	0.302	0.236	0.353	0.149	0.101	0.069	3.562
6.05 6.34	0.032	0.023	0.085	0.142	0.037	0.080	0.117	0.307	0.316	0.339	0.124	0.071	0.117	0.046	0.025	0.021	1.881
8.05 8.44	0.014	0.009	0.018	0.082	0.016	0.089	0.055	0.241	0.328	0.325	0.101	0.048	0.087	0.018	0.007	0.011	1.450
10.01 10.50	0.000	0.000	0.000	0.002	0.000	0.037	0.023	0.039	0.046	0.112	0.014	0.005	0.018	0.002	0.000	0.000	0.298
24.59 25.77	0.000	0.000	0.000	0.000	0.000	0.014	0.002	0.014	0.002	0.002	0.000	0.000	0.000	0.009	0.000	0.000	0.044
TOTAL	1.06	0.83	0.83	1.35	1.89	1.36	1.58	2.39	2.74	2.46	2.03	1.63	2.19	1.67	1.70	1.22	26.95

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS F

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.001	0.001	0.002	0.002	0.001	0.011
1.05 1.10	0.055	0.048	0.041	0.021	0.034	0.032	0.023	0.048	0.048	0.069	0.105	0.124	0.160	0.204	0.218	0.089	1.319
1.55 1.63	0.071	0.027	0.016	0.025	0.124	0.078	0.069	0.096	0.151	0.167	0.151	0.158	0.259	0.179	0.289	0.147	2.007
2.04 2.14	0.046	0.044	0.021	0.030	0.234	0.144	0.101	0.121	0.220	0.234	0.117	0.115	0.144	0.057	0.151	0.147	1.924
3.05 3.20	0.089	0.073	0.032	0.060	0.266	0.367	0.486	0.630	0.536	0.197	0.098	0.037	0.085	0.041	0.034	0.096	3.127

4.05	4.25	0.034	0.014	0.009	0.050	0.050	0.222	0.245	0.458	0.266	0.087	0.007	0.014	0.007	0.002	0.000	0.000	1.466
5.05	5.30	0.002	0.002	0.000	0.018	0.002	0.046	0.046	0.229	0.094	0.009	0.005	0.005	0.005	0.000	0.000	0.000	0.463
6.05	6.34	0.000	0.000	0.000	0.000	0.000	0.005	0.002	0.027	0.027	0.002	0.000	0.002	0.000	0.000	0.000	0.000	0.066
8.05	8.44	0.000	0.000	0.000	0.002	0.000	0.000	0.000	0.009	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.014
10.01	10.50	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24.59	25.77	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOTAL		0.30	0.21	0.12	0.21	0.71	0.89	0.97	1.62	1.35	0.77	0.48	0.45	0.66	0.49	0.69	0.48	10.40

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS G

TOWER RELEASE	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	TOTAL
0.36 0.37	0.001	0.000	0.000	0.001	0.001	0.000	0.000	0.001	0.001	0.002	0.002	0.002	0.003	0.004	0.004	0.003	0.025
1.05 1.10	0.057	0.021	0.018	0.034	0.039	0.023	0.025	0.034	0.057	0.098	0.115	0.119	0.167	0.215	0.252	0.156	1.432
1.55 1.63	0.016	0.007	0.005	0.018	0.066	0.069	0.032	0.080	0.124	0.096	0.062	0.069	0.089	0.053	0.179	0.110	1.074
2.04 2.14	0.011	0.002	0.002	0.007	0.080	0.064	0.039	0.044	0.158	0.078	0.014	0.009	0.021	0.014	0.030	0.023	0.596
3.05 3.20	0.021	0.002	0.000	0.005	0.069	0.124	0.142	0.137	0.190	0.016	0.002	0.005	0.005	0.002	0.000	0.000	0.719
4.05 4.25	0.002	0.000	0.000	0.007	0.014	0.071	0.069	0.073	0.041	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.277
5.05 5.30	0.000	0.000	0.000	0.005	0.000	0.007	0.011	0.032	0.007	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.062
6.05 6.34	0.000	0.000	0.000	0.000	0.002	0.000	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.005
8.05 8.44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10.01 10.50	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24.59 25.77	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOTAL	0.11	0.03	0.03	0.08	0.27	0.36	0.32	0.40	0.58	0.29	0.19	0.20	0.28	0.29	0.46	0.29	4.19

WIND MEASURED AT 9.1 METERS.

WIND SPEED CORRECTED TO THE RELEASE HEIGHT OF 10.0 METERS.

OVERALL WIND DIRECTION FREQUENCY

WIND DIRECTION:	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW
FREQUENCY:	5.9	4.1	3.6	4.7	5.7	4.7	5.1	7.8	8.3	7.3	6.7	5.9	8.4	8.3	7.8	5.6

OVERALL WIND SPEED FREQUENCY AS MEASURED ON THE TOWER:

MAX.WIND SPEED (M/S):	0.358	1.051	1.551	2.039	3.049	4.050	5.052	6.048	8.051	10.014	24.587
WIND SPEED FREQUENCY:	0.06	4.93	7.43	9.11	21.37	18.37	15.39	9.73	10.04	2.78	0.81

BUILDING AND RELEASE CHARACTERISTICS:

RELEASE HEIGHT: 10.00 METERS

MIXING VOLUME COEFFICIENT: 0.50

BUILDING CROSS-SECTIONAL AREA: 2917.00 SQUARE METERS

BOUNDARY DISTANCES (METERS) FROM THE SOURCE FOR EACH DOWNWIND SECTOR:

DOWNWIND SECTOR	S	SSW	SW	WSW	W	WNW	NW	NNW	N	NNE	NE	ENE	E	ESE	SE	SSE
BOUNDARY 1	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.	445.
BOUNDARY 2	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.	4828.

THE CONVERSION FACTOR APPLIED TO THE WIND SPEED CLASSES IS 0.447

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

WINDSPEEDS ADJUSTED TO 10.0 METERS.

PERCENT OF THE TIME A GIVEN WINDSPEED IS LOWER:

WINDSPEED (METER/SEC)	CUMULATIVE FREQUENCY (PERCENT)
0.37	0.01
0.37	0.06
1.08	0.83
1.10	5.00
1.59	6.92
1.63	12.42
2.09	15.79
2.14	21.53
3.12	31.88
3.20	42.90
4.15	54.05
4.25	61.27
5.17	72.57
5.30	76.66
6.19	84.43
6.34	86.38
8.24	94.95
8.44	96.42
10.25	98.90
10.50	99.19
25.17	99.96
25.77	100.00

WINDSPEED (INTERPOLATED) (METER/SEC)	CUMULATIVE FREQUENCY (PERCENT)
0.37	0.06
1.10	5.00
1.62	12.42
2.12	21.53
3.16	42.90
4.19	61.27
5.20	76.66
6.22	86.38
8.27	96.42
10.28	99.19



25.21                  100.00

LOG-NORMAL INTERPOLATION PERCENTILES

WINDSPEED (METER/SEC)	CUMULATIVE FREQUENCY (PERCENT)
0.69	1.00
0.94	3.00
1.10	5.00
1.46	10.00
1.76	15.00
2.04	20.00
2.28	25.00
2.52	30.00
2.76	35.00
3.01	40.00
3.26	45.00
3.52	50.00
3.80	55.00
4.10	60.00
4.40	65.00
4.71	70.00
5.07	75.00
5.50	80.00
6.17	85.00
6.70	90.00

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE S SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS				
AT 10.0 METERS						CA=1459.SQ.METERS						
A	1.1	0.04	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05	
A	2.1	0.08	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.62	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	1.50	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	0.73	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	0.39	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	0.54	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
B	1.6	0.12	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.19	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.73	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	0.85	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	1.50	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.50	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.39	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
B	10.3	0.08	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06	
B	25.2	0.12	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06	
C	1.1	0.08	445.	0.	0.	51.5	29.2	51.5	1.967E-04	1.503E-04	1.503E-04	
C	1.6	0.08	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.23	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	0.81	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	1.39	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	1.35	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	0.69	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.46	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
C	10.3	0.08	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05	
C	25.2	0.08	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06	
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04	
D	1.1	0.69	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04	
D	1.6	1.23	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04	
D	2.1	4.20	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04	
D	3.1	10.44	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05	
D	4.1	12.60	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05	
D	5.2	14.33	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05	
D	6.2	8.47	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05	

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D	8.2	7.59	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	1.54	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.62	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.16	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	1.93	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	1.73	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	5.85	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	4.62	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	1.77	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	0.54	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.23	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.92	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	1.19	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	0.77	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	1.50	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.58	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.04	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
G	0.4	0.02	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.96	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.27	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.19	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.35	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	0.04	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

S SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.017	0.025	0.038	1.001	1.010	1.357	1.626	2.551	2.743	2.782
0.00101	0.00149	0.00226	0.05953	0.06006	0.08068	0.09671	0.15169	0.16314	0.16543
3.672E-04	3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.503E-04
3.976	5.131	5.902	7.404	8.097	10.023	10.601	12.334	13.567	13.605
0.23644	0.30517	0.35098	0.44032	0.48155	0.59608	0.63044	0.73352	0.80683	0.80912
1.503E-04	1.293E-04	1.289E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05
13.682	19.537	23.735	23.812	28.434	38.873	40.644	40.876	53.471	54.010
0.81370	1.16188	1.41157	1.41615	1.69103	2.31181	2.41718	2.43092	3.17998	3.21205
5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05
68.339	68.454	69.263	69.494	77.968	78.161	79.547	87.135	88.483	88.522
4.06419	4.07106	4.11916	4.13291	4.63686	4.64831	4.73078	5.18204	5.26222	5.26451
2.896E-05	2.875E-05	2.611E-05	2.164E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05
90.062	90.794	91.488	92.335	92.797	94.299	94.376	94.453	94.954	95.570
5.35613	5.39966	5.44089	5.49128	5.51877	5.60811	5.61269	5.61727	5.64705	5.68370
1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	
95.956	96.572	96.649	98.151	98.883	98.960	99.345	99.884	100.000	
5.70661	5.74326	5.74784	5.83718	5.88070	5.88528	5.90819	5.94026	5.94713	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.059  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.152  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.595  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.410  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.309  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.061  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.633

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
1	1	-6.01579	-10.51189	-1.05466
1	2	-7.09335	-12.08837	-1.54102
1	3	-7.51984	-13.67660	-2.07675
1	4	-8.45385	-12.40116	-1.56959
1	5	-8.95670	-12.27601	-1.51256
1	6	-9.26047	-13.28736	-2.01984
1	7	-9.76542	-14.81674	-2.89694
1	8	-9.94552	NUMXQ(K)= 8	
		8.309E-04	0.059	1.000
		4.885E-04	0.178	3.000
		3.480E-04	0.297	5.000
		2.134E-04	0.595	10.000
		1.696E-04	0.892	15.000
		1.430E-04	1.189	20.000
		1.249E-04	1.487	25.000
		1.119E-04	1.784	30.000
		1.017E-04	2.081	35.000
		9.281E-05	2.379	40.000
		8.382E-05	2.676	45.000
		7.638E-05	2.974	50.000
		7.013E-05	3.271	55.000
		6.478E-05	3.568	60.000
		6.016E-05	3.866	65.000
		5.557E-05	4.163	70.000
		5.058E-05	4.460	75.000
		2.420E-04	0.5	8.41

ANNUAL AVERAGE = 4.18E-06

K= 1 FIVEXQ(K)= 2.420E-04 FIVEPR(K)= 8.407

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSW SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.1	0.11	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05
A	2.1	0.11	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.50	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	1.17	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	1.17	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	1.00	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.39	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.11	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
B	1.1	0.11	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05
B	1.6	0.17	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.28	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.44	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	1.11	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	1.11	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.89	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.17	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.06	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
C	1.1	0.06	445.	0.	0.	51.5	29.2	51.5	1.967E-04	1.503E-04	1.503E-04
C	1.6	0.06	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.78	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.56	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.44	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	0.94	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.67	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.50	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.11	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
D	0.4	0.02	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	1.39	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	2.22	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	4.72	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	10.33	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	9.72	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	11.72	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	7.39	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5				PAGE NO. 15 of 163		
D	8.2	10.28	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05	
D	10.3	2.00	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05	
D	25.2	0.22	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05	
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04	
E	1.1	1.50	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04	
E	1.6	1.89	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04	
E	2.1	2.78	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04	
E	3.2	6.78	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04	
E	4.2	4.83	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05	
E	5.3	1.56	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05	
E	6.3	0.56	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05	
E	8.4	0.22	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05	
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03	
F	1.1	1.17	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04	
F	1.6	0.67	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04	
F	2.1	1.06	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04	
F	3.2	1.78	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04	
F	4.2	0.33	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04	
F	5.3	0.06	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04	
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03	
G	1.1	0.50	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04	
G	1.6	0.17	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04	
G	2.1	0.06	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04	
G	3.2	0.06	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04	

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

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TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

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SSW SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04
0.009	0.019	0.036	0.536	0.554	0.609	0.776	1.943	1.998	2.665
0.00036	0.00078	0.00148	0.02210	0.02283	0.02513	0.03200	0.08010	0.08239	0.10988
3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.503E-04	1.503E-04
4.165	5.221	6.998	8.387	10.276	10.610	13.387	15.610	15.665	15.721
0.17173	0.21525	0.28855	0.34582	0.42371	0.43745	0.55198	0.64361	0.64590	0.64819
1.293E-04	1.289E-04	1.018E-04	9.731E-05	9.511E-05	8.343E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05
22.499	27.221	27.277	32.110	42.443	42.555	44.110	44.888	54.610	55.166
0.92766	1.12237	1.12466	1.32395	1.75001	1.75460	1.81873	1.85080	2.25167	2.27458
5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05
66.888	67.055	67.611	67.833	75.222	75.500	76.944	87.222	88.166	88.278
2.75792	2.76479	2.78770	2.79686	3.10152	3.11297	3.17253	3.59631	3.63525	3.63983
2.896E-05	2.875E-05	2.611E-05	2.164E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05
90.278	90.722	91.389	92.500	93.000	94.111	94.222	94.333	95.222	95.444
3.72230	3.74062	3.76811	3.81392	3.83454	3.88035	3.88494	3.88952	3.92617	3.93533
1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	5.398E-06	4.055E-06	3.260E-06		
95.611	96.111	96.167	97.333	98.500	99.500	99.889	100.000		
3.94220	3.96282	3.96511	4.01321	4.06132	4.10255	4.11859	4.12317		

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2) = 0.022  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3) = 0.080  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4) = 0.345  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5) = 1.121  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6) = 1.748  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7) = 2.755  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8) = 3.099

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
2	1	-6.01579	-10.98864	-1.10855
2	2	-7.09335	-11.27876	-1.19111
2	3	-7.51984	-13.07995	-1.76187
2	4	-8.32075	-12.42971	-1.52115
2	5	-8.95670	-12.93457	-1.74227
2	6	-9.26047	-14.84290	-2.64721
2	7	-9.76542	-16.46581	-3.49333
2	8	-9.94552	NUMXQ(K) = 8	
		6.790E-04	0.041	1.000
		4.320E-04	0.124	3.000
		3.271E-04	0.206	5.000
		2.225E-04	0.412	10.000
		1.797E-04	0.618	15.000
		1.535E-04	0.825	20.000
		1.353E-04	1.031	25.000
		1.208E-04	1.237	30.000
		1.088E-04	1.443	35.000
		9.916E-05	1.649	40.000
		8.931E-05	1.855	45.000
		7.962E-05	2.062	50.000
		7.165E-05	2.268	55.000
		6.498E-05	2.474	60.000
		5.932E-05	2.680	65.000
		5.356E-05	2.886	70.000
		4.816E-05	3.092	75.000
		2.013E-04	0.5	12.13

ANNUAL AVERAGE = 2.90E-06

K= 2 FIVEXQ(K) = 2.013E-04 FIVEPR(K) = 12.127

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SW SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	2.1	0.06	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.63	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.69	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.44	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.31	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.19	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
B	2.1	0.06	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.31	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.50	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.57	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.19	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.50	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
C	1.6	0.06	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.57	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.82	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.01	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	0.82	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.63	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.25	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.13	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	1.01	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	3.27	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	4.53	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	10.39	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	8.57	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	8.88	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	7.62	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	13.67	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	5.35	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	1.01	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.89	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04

E	1.6	1.95	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	1.89	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	5.42	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.73	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	3.21	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	2.33	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.50	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	1.13	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	0.44	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	0.57	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	0.88	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.25	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.50	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.13	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.06	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

SW SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04	3.146E-04
0.009	0.019	0.040	0.544	0.557	0.683	1.816	1.879	2.320	4.210
0.00032	0.00068	0.00146	0.01978	0.02026	0.02484	0.06607	0.06836	0.08440	0.15312
3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.293E-04	1.289E-04	1.018E-04
4.776	5.658	6.666	8.618	8.870	10.759	14.034	19.450	23.985	24.048
0.17373	0.20580	0.24245	0.31346	0.32263	0.39135	0.51046	0.70746	0.87239	0.87468
9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.179E-05	4.895E-05	4.794E-05
29.779	40.170	43.382	43.949	52.514	54.844	63.724	64.543	65.047	72.667
1.08314	1.46110	1.57792	1.59854	1.91007	1.99483	2.31782	2.34760	2.36592	2.64309
4.299E-05	3.899E-05	3.602E-05	3.126E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	1.961E-05	1.735E-05
72.730	73.738	87.404	88.223	93.576	93.891	94.521	95.025	95.277	95.843
2.64538	2.68204	3.17912	3.20889	3.40360	3.41506	3.43796	3.45629	3.46545	3.48607
1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.061E-06	6.463E-06	5.398E-06	4.055E-06
95.906	96.032	96.221	97.229	97.733	98.363	99.055	99.496	99.811	100.000
3.48836	3.49294	3.49981	3.53646	3.55479	3.57770	3.60289	3.61893	3.63038	3.63725

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q	WITH RESPECT TO	WHEN THE WIND BLOWS
SEC/CUBIC METER	THE TOTAL TIME	INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.020  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.066  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.313  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 0.871  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 1.459  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 1.908  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 2.315  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 9)= 2.640

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
3	1	-6.01579	-11.03820	-1.11338
3	2	-7.09335	-11.65071	-1.28626
3	3	-7.51984	-13.79758	-1.95474
3	4	-8.45385	-12.31345	-1.41185
3	5	-8.95670	-12.62956	-1.54480
3	6	-9.26047	-15.00660	-2.63472
3	7	-9.54448	-15.23007	-2.74252
3	8	-9.76542	-16.16322	-3.21083
3	9	-9.94552	NUMXQ(K)= 9	
		6.727E-04	0.036	1.000
		4.068E-04	0.109	3.000
		2.998E-04	0.182	5.000
		1.987E-04	0.364	10.000
		1.635E-04	0.546	15.000
		1.415E-04	0.727	20.000
		1.259E-04	0.909	25.000
		1.132E-04	1.091	30.000
		1.034E-04	1.273	35.000
		9.536E-05	1.455	40.000
		8.444E-05	1.637	45.000
		7.548E-05	1.819	50.000
		6.795E-05	2.000	55.000
		6.153E-05	2.182	60.000
		5.588E-05	2.364	65.000
		5.048E-05	2.546	70.000
		1.706E-04	0.5	13.75

ANNUAL AVERAGE = 2.44E-06

K= 3 FIVEXQ(K)= 1.706E-04 FIVEPR(K)=13.747

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WSW SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN	HT	EFF	PLUME	HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS														
												CA=1459.SQ.METERS		
A	1.1	0.10	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05			
A	2.1	0.10	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05			
A	3.1	0.34	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05			
A	4.1	0.43	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06			
A	5.2	0.58	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06			
A	6.2	0.39	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06			
A	8.2	0.77	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06			
A	10.3	0.29	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06			
B	1.1	0.10	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05			
B	1.6	0.05	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05			
B	3.1	0.43	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05			
B	4.1	0.34	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05			
B	5.2	0.19	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05			
B	6.2	0.24	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05			
B	8.2	0.68	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05			
B	10.3	0.19	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06			
C	1.6	0.05	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04			
C	2.1	0.19	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05			
C	3.1	0.58	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05			
C	4.1	0.43	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05			
C	5.2	0.82	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05			
C	6.2	0.34	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05			
C	8.2	0.48	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05			
C	10.3	0.05	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05			
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04			
D	1.1	0.82	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04			
D	1.6	2.17	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04			
D	2.1	2.56	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04			
D	3.1	7.62	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05			
D	4.1	9.07	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05			
D	5.2	13.12	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05			
D	6.2	9.21	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05			
D	8.2	11.19	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05			
D	10.3	1.78	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05			

E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.30	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.07	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	2.07	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.18	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	6.61	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	5.31	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	2.99	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	1.74	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.05	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
F	0.4	0.00	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.43	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	0.53	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	0.63	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	1.25	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	1.06	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.39	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	8.4	0.05	445.	0.	0.	17.8	7.5	17.8	2.830E-04	9.432E-05	9.432E-05
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.72	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.39	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.14	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.10	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	0.14	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	5.3	0.10	445.	0.	0.	12.3	4.7	15.1	8.454E-04	3.454E-04	3.454E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

WSW SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.013	0.017	0.031	0.755	0.765	0.862	1.248	1.682	1.827	1.972
0.00060	0.00078	0.00148	0.03584	0.03635	0.04093	0.05925	0.07987	0.08674	0.09361
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04
2.502	2.599	3.901	4.528	5.783	6.603	8.677	9.739	11.813	13.984
0.11881	0.12339	0.18524	0.21502	0.27458	0.31352	0.41202	0.46241	0.56091	0.66399
1.503E-04	1.293E-04	1.289E-04	1.018E-04	9.731E-05	9.511E-05	9.432E-05	8.343E-05	7.802E-05	7.746E-05
14.370	20.545	23.102	23.150	29.759	37.381	37.430	37.526	42.833	43.026
0.68232	0.97553	1.09693	1.09923	1.41305	1.77498	1.77727	1.78185	2.03383	2.04299
7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	3.936E-05	3.899E-05	3.602E-05
52.095	55.086	68.208	68.257	68.835	70.572	79.786	79.835	80.269	91.461
2.47364	2.61566	3.23873	3.24102	3.26851	3.35097	3.78849	3.79078	3.81140	4.34284
3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05
92.281	92.378	94.163	94.597	94.935	95.272	95.755	95.948	96.044	96.092
4.38178	4.38636	4.47112	4.49173	4.50777	4.52380	4.54671	4.55587	4.56046	4.56275
1.449E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	5.398E-06	4.055E-06	3.260E-06	
96.334	97.009	97.347	97.540	97.974	98.553	98.939	99.711	100.000	
4.57420	4.60627	4.62230	4.63147	4.65208	4.67957	4.69790	4.73455	4.74829	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.036  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.080  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.412  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 1.096  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 1.773  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 3.236  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 3.785

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
4	1	-6.01579	-10.76639	-1.08565
4	2	-7.09335	-13.46113	-1.88215
4	3	-7.51984	-13.25366	-1.81642
4	4	-8.45385	-12.24396	-1.43432
4	5	-8.95670	-12.64402	-1.60887
4	6	-9.26047	-13.41133	-1.97373
4	7	-9.76542	-14.44795	-2.53490
4	8	-9.94552	NUMXQ(K)= 8	
		7.172E-04	0.047	1.000
		3.962E-04	0.142	3.000
		2.963E-04	0.237	5.000
		1.988E-04	0.475	10.000
		1.620E-04	0.712	15.000
		1.393E-04	0.950	20.000
		1.228E-04	1.187	25.000
		1.096E-04	1.424	30.000
		9.927E-05	1.662	35.000
		9.007E-05	1.899	40.000
		8.181E-05	2.137	45.000
		7.496E-05	2.374	50.000
		6.916E-05	2.612	55.000
		6.420E-05	2.849	60.000
		5.988E-05	3.086	65.000
		5.574E-05	3.324	70.000
		5.150E-05	3.561	75.000
		1.938E-04	0.5	10.53

ANNUAL AVERAGE = 3.13E-06

K= 4 FIVEXQ(K)= 1.938E-04 FIVEPR(K)=10.530

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE W SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS				
AT 10.0 METERS									CA=1459.SQ.METERS			
A	1.1	0.08	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05	
A	2.1	0.12	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.56	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	1.01	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	0.73	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	0.04	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	0.08	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
B	1.1	0.08	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05	
B	1.6	0.12	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.12	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.56	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	0.85	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	0.61	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.16	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.08	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
C	1.1	0.04	445.	0.	0.	51.5	29.2	51.5	1.967E-04	1.503E-04	1.503E-04	
C	1.6	0.16	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.40	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	1.98	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	1.17	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	0.44	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	0.20	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.08	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04	
D	1.1	0.89	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04	
D	1.6	2.38	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04	
D	2.1	4.32	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04	
D	3.1	11.86	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05	
D	4.1	9.00	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05	
D	5.2	6.90	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05	
D	6.2	2.87	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05	
D	8.2	1.41	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05	
D	10.3	0.04	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05	

E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.49	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	3.79	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	6.21	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	13.28	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	6.01	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	1.61	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	0.65	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.28	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.61	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.18	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	4.12	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	4.68	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.89	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.04	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.69	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.17	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	1.41	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	1.21	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	0.24	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	6.3	0.04	445.	0.	0.	12.3	4.7	12.3	8.656E-04	2.885E-04	2.885E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

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AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

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THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
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2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.012	0.017	0.034	0.720	0.732	1.942	3.112	3.718	5.130	5.372
0.00069	0.00098	0.00194	0.04088	0.04153	0.11025	0.17668	0.21105	0.29122	0.30496
3.672E-04	3.146E-04	3.038E-04	2.885E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04
7.551	9.044	13.160	13.201	17.882	18.769	22.563	23.450	29.665	32.046
0.42866	0.51342	0.74707	0.74936	1.01508	1.06547	1.28080	1.33119	1.68396	1.81911
1.503E-04	1.503E-04	1.293E-04	1.289E-04	1.018E-04	9.731E-05	9.511E-05	8.343E-05	7.802E-05	7.746E-05
32.086	32.126	45.402	49.720	49.882	55.894	67.758	67.839	69.453	69.856
1.82140	1.82369	2.57733	2.82243	2.83159	3.17290	3.84637	3.85095	3.94258	3.96548
7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.899E-05	3.602E-05
78.855	79.501	86.401	86.522	88.499	88.782	91.647	91.768	92.938	94.351
4.47631	4.51296	4.90467	4.91154	5.02378	5.03982	5.20245	5.20933	5.27576	5.35593
3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	1.961E-05	1.735E-05	1.602E-05	1.449E-05
94.794	94.875	94.915	95.480	95.682	96.530	96.610	97.216	97.337	97.498
5.38113	5.38571	5.38800	5.42007	5.43152	5.47963	5.48421	5.51857	5.52544	5.53460
1.089E-05	1.071E-05	8.061E-06	6.463E-06	5.398E-06	4.055E-06				
97.579	98.144	99.153	99.879	99.919	100.000				
5.53919	5.57125	5.62852	5.66975	5.67205	5.67663				

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.211  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.291  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.746  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.064  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.820  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.843  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.473  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.901

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
5	1	-6.01579	-10.41432	-1.01152
5	2	-7.51984	-11.06537	-1.23904
5	3	-7.64824	-11.49089	-1.39333
5	4	-8.09920	-12.20567	-1.68697
5	5	-8.32075	-12.02919	-1.61034
5	6	-8.95670	-13.13290	-2.18881
5	7	-9.26047	-16.34580	-4.00483
5	8	-9.54448	-18.12093	-5.05008
5	9	-9.76542		
			NUMXQ(K)= 9	
		8.072E-04	0.057	1.000
		5.804E-04	0.170	3.000
		4.819E-04	0.284	5.000
		3.481E-04	0.568	10.000
		2.803E-04	0.851	15.000
		2.341E-04	1.135	20.000
		2.037E-04	1.419	25.000
		1.813E-04	1.703	30.000
		1.638E-04	1.987	35.000
		1.498E-04	2.271	40.000
		1.381E-04	2.554	45.000
		1.282E-04	2.838	50.000
		1.169E-04	3.122	55.000
		1.074E-04	3.406	60.000
		9.917E-05	3.690	65.000
		8.955E-05	3.974	70.000
		7.871E-05	4.257	75.000
		6.916E-05	4.541	80.000
		5.973E-05	4.825	85.000
		3.702E-04	0.5	8.81

ANNUAL AVERAGE = 5.73E-06

K= 5 FIVEXQ(K)= 3.702E-04 FIVEPR(K)= 8.808

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WNW SECTOR.

STABILITY CLASS	WINDSPEED METER/SEC AT 10.0 METERS	FREQUENCY PERCENT	DISTANCE METERS	TERRAIN METERS	HT EFF METERS	PLUME HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
										CA=1459.SQ.METERS			
A	1.6	0.15	445.	0.	0.		90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05	
A	2.1	0.10	445.	0.	0.		90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.39	445.	0.	0.		90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	0.69	445.	0.	0.		90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	0.44	445.	0.	0.		90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	0.20	445.	0.	0.		90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	0.30	445.	0.	0.		90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
B	1.6	0.15	445.	0.	0.		67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.25	445.	0.	0.		67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.79	445.	0.	0.		67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	0.59	445.	0.	0.		67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	0.64	445.	0.	0.		67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.34	445.	0.	0.		67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.05	445.	0.	0.		67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
B	10.3	0.05	445.	0.	0.		67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06	
C	1.6	0.10	445.	0.	0.		51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.44	445.	0.	0.		51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	1.23	445.	0.	0.		51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	0.69	445.	0.	0.		51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	0.59	445.	0.	0.		51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	0.10	445.	0.	0.		51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.15	445.	0.	0.		51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
C	10.3	0.10	445.	0.	0.		51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05	
D	0.4	0.01	445.	0.	0.		36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04	
D	1.1	0.64	445.	0.	0.		36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04	
D	1.6	2.41	445.	0.	0.		36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04	
D	2.1	3.89	445.	0.	0.		36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04	
D	3.1	7.98	445.	0.	0.		36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05	
D	4.1	5.91	445.	0.	0.		36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05	
D	5.2	5.66	445.	0.	0.		36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05	
D	6.2	3.05	445.	0.	0.		36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05	
D	8.2	3.89	445.	0.	0.		36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05	
D	10.3	1.48	445.	0.	0.		36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05	
D	25.2	0.34	445.	0.	0.		36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05	

E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	0.98	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.31	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	3.99	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	8.42	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.37	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	3.50	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	1.72	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	1.92	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.79	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.30	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.69	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	1.67	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	3.10	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	7.88	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	4.78	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.98	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.10	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.49	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.48	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	1.38	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	2.66	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	1.53	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	5.3	0.15	445.	0.	0.	12.3	4.7	15.1	8.454E-04	3.454E-04	3.454E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

WNW SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.009	0.015	0.026	0.518	0.526	3.186	4.663	5.352	6.731	8.258
0.00040	0.00068	0.00120	0.02411	0.02449	0.14819	0.21691	0.24898	0.31312	0.38413
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04
9.932	10.080	11.065	14.167	22.046	22.686	25.001	29.778	33.766	36.179
0.46201	0.46888	0.51470	0.65901	1.02552	1.05530	1.16296	1.38516	1.57071	1.68295
1.503E-04	1.293E-04	1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05
37.164	45.585	49.475	49.574	49.672	55.040	63.018	66.514	66.957	72.866
1.72876	2.12047	2.30144	2.30602	2.31060	2.56028	2.93137	3.09401	3.11463	3.38951
6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05
74.590	80.253	80.401	81.632	83.552	86.606	86.852	87.640	88.329	92.219
3.46969	3.73312	3.73999	3.79725	3.88659	4.02861	4.04007	4.07672	4.10879	4.28975
3.126E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05
92.810	94.288	95.076	95.174	95.765	95.913	96.060	96.701	96.996	97.095
4.31724	4.38596	4.42261	4.42719	4.45468	4.46156	4.46843	4.49821	4.51195	4.51653
1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	5.398E-06	4.055E-06
97.193	97.538	97.882	97.932	98.326	98.375	99.064	99.508	99.705	100.000
4.52111	4.53715	4.55318	4.55547	4.57380	4.57609	4.60816	4.62878	4.63794	4.65168

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.024  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 2.299  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.929  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.386  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.730  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.025

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
6	1	-6.01579	-10.07285	-0.90896
6	2	-7.51984	-11.96591	-1.58296
6	3	-8.29770	-13.04394	-2.04816
6	4	-8.95670	-14.77618	-2.91621
6	5	-9.26047	-17.57716	-4.39711
6	6	-9.54448	-18.74329	-5.03546
6	7	-9.76542	-18.89664	-5.12147
6	8	-9.94552	NUMXQ(K)= 8	
		8.560E-04	0.047	1.000
		6.395E-04	0.140	3.000
		5.531E-04	0.233	5.000
		3.903E-04	0.465	10.000
		3.116E-04	0.698	15.000
		2.639E-04	0.930	20.000
		2.259E-04	1.163	25.000
		1.955E-04	1.396	30.000
		1.725E-04	1.628	35.000
		1.544E-04	1.861	40.000
		1.398E-04	2.093	45.000
		1.272E-04	2.326	50.000
		1.130E-04	2.558	55.000
		1.013E-04	2.791	60.000
		8.957E-05	3.024	65.000
		7.750E-05	3.256	70.000
		6.705E-05	3.489	75.000
		5.782E-05	3.721	80.000
		5.012E-05	3.954	85.000
		3.753E-04	0.5	10.75

ANNUAL AVERAGE = 4.54E-06

K= 6 FIVEXQ(K)= 3.753E-04 FIVEPR(K)=10.749

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NW SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.13	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.09	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.18	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.31	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.45	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.40	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.31	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
B	1.6	0.09	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.13	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.40	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.98	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.67	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.45	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.18	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.22	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
C	1.6	0.09	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.58	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	1.47	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	0.89	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	1.03	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.45	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.22	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.22	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.80	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.69	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	2.09	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	7.31	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	7.09	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	6.77	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	3.43	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	3.74	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	1.20	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.04	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05

E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.20	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	1.96	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	2.23	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	8.96	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	7.53	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	5.04	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	2.27	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	1.07	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.45	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.04	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.00	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.45	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	1.34	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.96	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	9.45	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	4.77	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.89	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.04	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.49	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.62	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.76	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	2.76	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	1.34	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	5.3	0.22	445.	0.	0.	12.3	4.7	15.1	8.454E-04	3.454E-04	3.454E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

NW SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.009	0.012	0.026	0.516	0.527	3.290	3.914	4.359	5.117	6.454
0.00044	0.00064	0.00134	0.02654	0.02707	0.16909	0.20116	0.22407	0.26301	0.33173
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04
7.791	8.014	9.217	11.178	20.626	21.429	23.390	28.158	30.387	32.080
0.40045	0.41191	0.47376	0.57455	1.06017	1.10140	1.20219	1.44730	1.56183	1.64888
1.503E-04	1.293E-04	1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05
32.971	41.929	44.024	44.069	44.158	51.689	58.998	64.035	64.614	71.700
1.69469	2.15512	2.26278	2.26507	2.26966	2.65678	3.03245	3.29130	3.32108	3.68530
6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05
73.973	80.747	80.836	82.307	83.377	86.808	86.942	87.388	88.279	92.023
3.80213	4.15031	4.15489	4.23048	4.28546	4.46184	4.46872	4.49162	4.53744	4.72985
3.126E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05
93.048	94.251	94.652	95.098	96.078	96.212	96.435	97.103	97.148	97.237
4.78254	4.84439	4.86501	4.88791	4.93831	4.94518	4.95663	4.99099	4.99328	4.99786
1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	5.398E-06	4.055E-06
97.460	97.905	97.950	98.128	98.306	98.529	98.841	99.287	99.688	100.000
5.00932	5.03222	5.03452	5.04368	5.05284	5.06429	5.08033	5.10324	5.12385	5.13989

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.224  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.059  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.100  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.260  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.030  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.682  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.147  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 4.458

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
7	1	-6.01579	-10.17798	-0.93681
7	2	-7.48309	-10.57407	-1.07450
7	3	-7.51984	-11.63194	-1.44666
7	4	-8.29770	-11.97206	-1.59423
7	5	-8.32075	-13.38486	-2.21109
7	6	-8.95670	-13.77576	-2.40628
7	7	-9.26047	-15.34216	-3.24104
7	8	-9.54448	-16.73736	-4.02098
7	9	-9.76542	-18.92969	-5.28538
7	10	-9.94552	NUMXQ(K)= 10	
		8.231E-04	0.051	1.000
		6.079E-04	0.154	3.000
		5.088E-04	0.257	5.000
		3.638E-04	0.514	10.000
		2.955E-04	0.771	15.000
		2.533E-04	1.028	20.000
		2.136E-04	1.285	25.000
		1.823E-04	1.542	30.000
		1.590E-04	1.799	35.000
		1.408E-04	2.056	40.000
		1.260E-04	2.313	45.000
		1.131E-04	2.570	50.000
		1.024E-04	2.827	55.000
		9.284E-05	3.084	60.000
		8.269E-05	3.341	65.000
		7.418E-05	3.598	70.000
		6.589E-05	3.855	75.000
		5.841E-05	4.112	80.000
		5.053E-05	4.369	85.000
		3.689E-04	0.5	9.73

ANNUAL AVERAGE = 4.58E-06

K= 7 FIVEXQ(K)= 3.689E-04 FIVEPR(K)= 9.728

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNW SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
									CA=1459.SQ.METERS		
AT 10.0 METERS											
A	1.6	0.03	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.03	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.44	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.62	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.62	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.30	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.74	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.15	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
A	25.2	0.03	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06
B	1.1	0.03	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05
B	1.6	0.03	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.03	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.35	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.35	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.59	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.27	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.38	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.18	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
B	25.2	0.03	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06
C	1.6	0.03	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.21	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.35	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	0.77	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	0.92	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.74	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.24	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.06	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
C	25.2	0.15	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.00	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.18	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.00	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	1.42	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	5.43	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	6.65	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05

CALCULATION NO. BYR04-050, BRW-04-0044-M			MINOR REV. NO. 1B			APPENDIX BB-5					PAGE NO. 39 of 163	
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D	5.2	6.70	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	4.84	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	5.97	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	1.65	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.62	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	0.80	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	1.24	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	1.62	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.53	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	7.24	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	5.61	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	3.96	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	3.10	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.50	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.18	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.62	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	1.24	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.57	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	8.12	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	5.91	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	2.95	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.35	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
F	8.4	0.12	445.	0.	0.	17.8	7.5	17.8	2.830E-04	9.432E-05	9.432E-05
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.44	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.03	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.56	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	1.77	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	0.95	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	5.3	0.41	445.	0.	0.	12.3	4.7	15.1	8.454E-04	3.454E-04	3.454E-04
G	6.3	0.03	445.	0.	0.	12.3	4.7	12.3	8.656E-04	2.885E-04	2.885E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

NNW SECTOR      BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.008	0.013	0.022	0.465	0.468	2.240	3.273	3.894	4.455	5.400
0.00060	0.00102	0.00172	0.03608	0.03626	0.17370	0.25387	0.30198	0.34550	0.41880
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.885E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04
6.640	7.054	7.851	9.417	9.446	17.568	17.745	18.986	24.893	26.517
0.51501	0.54708	0.60893	0.73034	0.73263	1.36257	1.37631	1.47252	1.93066	2.05665
1.648E-04	1.503E-04	1.293E-04	1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	9.432E-05	8.343E-05
27.521	30.475	37.002	38.420	38.774	38.804	46.040	51.474	51.592	51.622
2.13453	2.36360	2.86984	2.97979	3.00728	3.00957	3.57079	3.99228	4.00144	4.00373
7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05
57.234	57.440	64.086	68.043	74.748	74.777	75.132	78.233	83.077	83.106
4.43896	4.45500	4.97040	5.27735	5.79734	5.79963	5.82712	6.06764	6.44332	6.44561
3.936E-05	3.899E-05	3.602E-05	3.126E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	2.105E-05	1.961E-05
83.608	84.376	90.342	91.258	92.912	93.266	94.004	94.359	94.388	94.625
6.48455	6.54411	7.00682	7.07784	7.20611	7.23360	7.29087	7.31836	7.32065	7.33897
1.735E-05	1.603E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06
95.215	95.393	95.422	95.481	95.747	96.367	96.751	97.194	97.371	97.992
7.38479	7.39853	7.40082	7.40540	7.42602	7.47412	7.50390	7.53826	7.55201	7.60011
6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	3.260E-06	1.328E-06			
98.612	98.760	99.055	99.793	99.823	99.970	100.000			
7.64822	7.65967	7.68258	7.73984	7.74213	7.75359	7.75588			



X/Q PERCENTILES  
 (BASED ON THE UPPER ENVELOPE OF THE  
 ORDERED X/Q-FREQUENCY VALUES, AND AS  
 PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.361  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 2.977  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 3.989  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.967  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.794  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.439

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
8	1	-6.01579	-10.05396	-0.92284
8	2	-7.51984	-11.49265	-1.44676
8	3	-8.29770	-12.78726	-2.03300
8	4	-8.95670	-13.28568	-2.29753
8	5	-9.26047	-14.05019	-2.73390
8	6	-9.54448	-14.35178	-2.91689
8	7	-9.76542	-15.06350	-3.36954
8	8	-9.94552		
NUMXQ(K)= 8				
		7.983E-04	0.078	1.000
		5.862E-04	0.233	3.000
		4.808E-04	0.388	5.000
		3.386E-04	0.776	10.000
		2.721E-04	1.163	15.000
		2.245E-04	1.551	20.000
		1.869E-04	1.939	25.000
		1.601E-04	2.327	30.000
		1.400E-04	2.715	35.000
		1.237E-04	3.102	40.000
		1.096E-04	3.490	45.000
		9.810E-05	3.878	50.000
		8.740E-05	4.266	55.000
		7.808E-05	4.654	60.000
		7.017E-05	5.041	65.000
		6.313E-05	5.429	70.000
		5.708E-05	5.817	75.000
		5.115E-05	6.205	80.000
		4.241E-04	0.5	6.45

ANNUAL AVERAGE = 6.24E-06

K= 8 FIVEXQ(K)= 4.241E-04 FIVEPR(K)= 6.447

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE N SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.03	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	3.1	0.19	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.22	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.47	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.25	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.88	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.28	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
A	25.2	0.06	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06
B	1.6	0.06	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	3.1	0.25	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.55	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.33	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.39	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.47	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.14	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
B	25.2	0.08	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06
C	1.6	0.06	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.22	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.64	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.13	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	0.91	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.61	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.77	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.19	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
D	0.4	0.00	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.28	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	0.91	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	1.77	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	6.27	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	7.05	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	5.94	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	5.42	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	5.20	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	1.60	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05

D	25.2	0.06	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	0.77	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	1.66	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	2.49	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	7.10	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	6.69	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	6.05	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	3.81	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	3.95	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.55	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.03	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.58	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	1.82	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	2.65	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	6.47	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	3.21	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	1.13	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.33	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
F	8.4	0.03	445.	0.	0.	17.8	7.5	17.8	2.830E-04	9.432E-05	9.432E-05
G	0.4	0.01	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	0.69	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.49	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	1.91	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	2.29	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04
G	4.2	0.50	445.	0.	0.	12.3	4.7	21.6	7.354E-04	4.308E-04	4.308E-04
G	5.3	0.08	445.	0.	0.	12.3	4.7	15.1	8.454E-04	3.454E-04	3.454E-04

RUN DATE: 04/05/09

METEOROLOGICAL INSTRUMENTATION

WIND SENSORS HEIGHT: 9.1 meters

DELTA-T HEIGHTS: 76.2-9.1 meters

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

N SECTOR      BOUNDARY DISTANCE = 445.0 METERS

AS A FUNCTION OF DOWNWIND DISTANCE.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREOUENCY WITH RESPECT TO ALL TIME

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.012	0.017	0.026	0.717	0.720	3.015	4.507	5.087	6.995	7.492
0.00101	0.00143	0.00215	0.05942	0.05971	0.24984	0.37354	0.42164	0.57970	0.62093
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04
9.316	9.399	10.173	12.826	19.294	19.570	21.229	24.435	26.922	27.834
0.77212	0.77899	0.84313	1.06304	1.59906	1.62196	1.75940	2.02512	2.23129	2.30688
1.503E-04	1.293E-04	1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	9.432E-05	7.802E-05	7.746E-05
28.968	36.071	37.840	38.171	38.227	44.915	51.189	51.217	57.270	57.491
2.40080	2.98950	3.13611	3.16360	3.16818	3.72252	4.24251	4.24480	4.74646	4.76479
7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05	3.936E-05	3.899E-05	3.602E-05
64.539	68.353	74.296	74.351	74.987	78.939	84.356	84.909	86.042	91.238
5.34891	5.66503	6.15753	6.16211	6.21479	6.54236	6.99134	7.03715	7.13107	7.56172
3.126E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.577E-05
92.150	93.754	94.002	94.610	95.163	95.191	95.965	96.296	96.324	96.517
7.63731	7.77017	7.79079	7.84118	7.88700	7.88929	7.95343	7.98091	7.98320	7.99924
1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	5.398E-06	4.055E-06	3.565E-06
96.904	96.960	97.430	97.623	97.761	97.982	98.452	98.701	99.585	99.668
8.03131	8.03589	8.07483	8.09087	8.10232	8.12065	8.15959	8.18020	8.25351	8.26038
3.260E-06	1.328E-06								
99.945	100.000								
8.28329	8.28787								

X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.579  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.597  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 3.133  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.239  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.345  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.987  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 7.558

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
9	1	-6.01579	-9.95318	-0.92360
9	2	-7.51984	-10.59682	-1.16790
9	3	-7.64824	-11.96782	-1.71094
9	4	-8.29770	-13.28366	-2.32436
9	5	-8.95670	-13.05519	-2.20163
9	6	-9.26047	-13.65772	-2.55121
9	7	-9.54448	-14.31468	-2.95868
9	8	-9.94552	-20.17927	-6.93003
9	9	-10.23154	NUMXQ(K)= 9	
		8.694E-04	0.083	1.000
		6.371E-04	0.249	3.000
		5.452E-04	0.414	5.000
		3.829E-04	0.829	10.000
		2.950E-04	1.243	15.000
		2.409E-04	1.658	20.000
		1.949E-04	2.072	25.000
		1.630E-04	2.486	30.000
		1.396E-04	2.901	35.000
		1.220E-04	3.315	40.000
		1.085E-04	3.730	45.000
		9.744E-05	4.144	50.000
		8.722E-05	4.558	55.000
		7.840E-05	4.973	60.000
		7.086E-05	5.387	65.000
		6.355E-05	5.802	70.000
		5.734E-05	6.216	75.000
		5.200E-05	6.630	80.000
		4.664E-05	7.045	85.000
		3.787E-05	7.459	90.000
		5.065E-04	0.5	6.03

ANNUAL AVERAGE = 7.35E-06

K= 9      FIVEXQ(K) = 5.065E-04      FIVEPR(K) = 6.033

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS				
AT 10.0 METERS									CA=1459.SQ.METERS			
A	1.1	0.03	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05	
A	1.6	0.09	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05	
A	2.1	0.03	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.35	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	0.38	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	0.60	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	0.63	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	1.04	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
A	10.3	0.41	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06	
A	25.2	0.13	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06	
B	1.6	0.03	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.09	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.41	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	0.73	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	0.66	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.85	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.76	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
B	10.3	0.19	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06	
B	25.2	0.06	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06	
C	1.6	0.06	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.22	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	1.29	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	1.14	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	1.20	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	0.88	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.95	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
C	10.3	0.22	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05	
C	25.2	0.09	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06	
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04	
D	1.1	0.50	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04	
D	1.6	1.04	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04	
D	2.1	2.15	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04	
D	3.1	7.10	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05	
D	4.1	6.47	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05	

D	5.2	5.99	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	4.92	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	6.97	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	2.40	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.44	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.01	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.10	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.24	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	2.84	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.56	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.43	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	5.02	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	4.67	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	4.48	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	1.55	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.03	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	0.95	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.30	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	3.22	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	2.71	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	1.20	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.13	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.03	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
G	0.4	0.02	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	1.36	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.33	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	1.07	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.22	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### SITE EXCLUSION BOUNDARY CALCULATIONS:

NNE SECTOR      BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04
0.024	0.032	0.045	1.401	1.408	1.629	2.954	3.900	4.973	7.276
0.00173	0.00233	0.00324	0.10174	0.10221	0.11824	0.21445	0.28317	0.36106	0.52828
3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.503E-04	1.293E-04
8.380	11.598	14.311	14.816	17.056	18.255	21.095	22.136	22.262	28.824
0.60845	0.84210	1.03910	1.07575	1.23839	1.32544	1.53160	1.60719	1.61635	2.09282
1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05
30.970	31.001	31.064	36.491	43.589	48.606	48.827	55.294	59.964	65.958
2.24858	2.25087	2.25546	2.64945	3.16486	3.52908	3.54511	4.01470	4.35373	4.78896
5.650E-05	5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05
65.990	67.283	71.763	76.685	76.780	78.325	79.461	86.434	87.633	87.664
4.79125	4.88517	5.21044	5.56779	5.57466	5.68691	5.76937	6.27561	6.36266	6.36495
2.896E-05	2.875E-05	2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05	1.577E-05
90.062	90.472	91.355	92.081	92.176	93.122	93.785	93.816	93.848	94.069
6.53904	6.56882	6.63296	6.68565	6.69252	6.76124	6.80934	6.81164	6.81393	6.82996
1.449E-05	1.179E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06
94.921	95.362	96.119	96.466	96.656	97.034	97.634	97.728	98.359	99.401
6.89181	6.92388	6.97886	7.00405	7.01780	7.04529	7.08881	7.09568	7.14149	7.21709
3.565E-06	3.260E-06	1.328E-06							
99.464	99.874	100.000							
7.22167	7.25145	7.26061							

X/Q PERCENTILES  
 (BASED ON THE UPPER ENVELOPE OF THE  
 ORDERED X/Q-FREQUENCY VALUES, AND AS  
 PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.102  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.283  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.841  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 2.246  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.162  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 5.564  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 6.272

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
10	1	-6.01579	-10.24483	-1.02141
10	2	-7.09335	-11.22637	-1.33954
10	3	-7.51984	-11.77829	-1.53900
10	4	-8.09920	-13.42066	-2.22602
10	5	-8.95670	-13.07714	-2.05472
10	6	-9.26047	-14.06148	-2.58464
10	7	-9.94552	-17.52254	-4.75804
10	8	-10.23154	NUMXQ(K)= 8	
		9.189E-04	0.073	1.000
		6.072E-04	0.218	3.000
		4.779E-04	0.363	5.000
		3.301E-04	0.726	10.000
		2.453E-04	1.089	15.000
		1.915E-04	1.452	20.000
		1.570E-04	1.815	25.000
		1.328E-04	2.178	30.000
		1.158E-04	2.541	35.000
		1.028E-04	2.904	40.000
		9.168E-05	3.267	45.000
		8.107E-05	3.630	50.000
		7.238E-05	3.993	55.000
		6.515E-05	4.356	60.000
		5.904E-05	4.719	65.000
		5.383E-05	5.082	70.000
		4.932E-05	5.445	75.000
		4.337E-05	5.808	80.000
		3.750E-05	6.172	85.000
		4.043E-04	0.5	6.89

ANNUAL AVERAGE = 6.25E-06

K= 10 FIVEXQ(K)= 4.043E-04 FIVEPR(K)= 6.886

USNRC COMPUTER CODE~PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.07	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.17	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.65	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.69	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.96	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.65	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.99	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.24	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
A	25.2	0.07	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06
B	2.1	0.07	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.75	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.99	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	1.06	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.75	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.48	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.14	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
B	25.2	0.10	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06
C	1.6	0.34	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.21	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	1.23	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.54	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	1.64	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.96	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.65	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.14	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
C	25.2	0.14	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.72	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.68	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	2.54	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	9.05	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	8.29	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	8.33	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	5.62	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05

CALCULATION NO. BYR04-050, BRW-04-0044-M			MINOR REV. NO. 1B			APPENDIX BB-5					PAGE NO. 52 of 163	
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D	8.2	5.24	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	1.34	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.93	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.47	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	3.26	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	4.22	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	7.40	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.96	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	4.52	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	1.85	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	1.51	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.21	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	1.58	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.26	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.75	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	1.47	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.10	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.07	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
G	0.4	0.03	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	1.71	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.93	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.21	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.03	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

NE SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04
0.030	0.044	0.061	1.774	1.783	1.818	2.743	4.319	4.525	6.787
0.00202	0.00293	0.00404	0.11858	0.11920	0.12149	0.18334	0.28871	0.30245	0.45364
3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.503E-04	1.293E-04
8.260	10.008	11.482	12.201	15.457	15.560	19.775	21.454	21.523	28.925
0.55214	0.66896	0.76746	0.81557	1.03318	1.04006	1.32181	1.43405	1.43864	1.93342
1.289E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.179E-05
31.461	31.803	37.766	46.814	51.337	51.543	59.836	61.687	70.014	71.248
2.10294	2.12584	2.52442	3.12916	3.43154	3.44528	3.99963	4.12332	4.67996	4.76242
4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	2.896E-05	2.875E-05	2.611E-05
72.756	78.376	78.444	78.650	80.192	85.435	87.080	88.417	89.171	90.130
4.86322	5.23889	5.24347	5.25721	5.36030	5.71077	5.82072	5.91006	5.96046	6.02459
2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05
91.124	91.193	91.844	92.906	93.078	93.215	93.969	94.894	95.374	96.025
6.09102	6.09561	6.13913	6.21014	6.22159	6.23076	6.28115	6.34300	6.37507	6.41859
8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	3.260E-06	1.328E-06	
96.162	96.847	97.807	97.944	98.595	99.589	99.692	99.931	100.000	
6.42776	6.47357	6.53771	6.54687	6.59039	6.65683	6.66370	6.67973	6.68431	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.118  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.288  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.668  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.101  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.126  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.996  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.676  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.235  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 5.707

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
11	1	-6.01579	-10.16562	-1.01076
11	2	-7.09335	-11.74203	-1.52939
11	3	-7.51984	-13.09723	-2.02028
11	4	-8.09920	-12.91447	-1.94640
11	5	-8.95670	-12.57270	-1.77832
11	6	-9.26047	-14.00744	-2.54863
11	7	-9.54448	-14.76966	-2.98391
11	8	-9.76542	-15.29657	-3.29809
11	9	-9.94552	-20.83637	-6.71252
11	10	-10.23154	NUMXQ(K)= 10	
		9.850E-04	0.067	1.000
		6.484E-04	0.201	3.000
		4.920E-04	0.334	5.000
		3.040E-04	0.668	10.000
		2.277E-04	1.003	15.000
		1.838E-04	1.337	20.000
		1.548E-04	1.671	25.000
		1.339E-04	2.005	30.000
		1.190E-04	2.340	35.000
		1.075E-04	2.674	40.000
		9.812E-05	3.008	45.000
		8.824E-05	3.342	50.000
		7.904E-05	3.676	55.000
		7.132E-05	4.011	60.000
		6.378E-05	4.345	65.000
		5.742E-05	4.679	70.000
		5.146E-05	5.013	75.000
		4.481E-05	5.347	80.000
		3.664E-05	5.682	85.000
		3.735E-04	0.5	7.48

ANNUAL AVERAGE = 5.99E-06

K= 11 FIVEXQ(K)= 3.735E-04 FIVEPR(K)= 7.480

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ENE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.23	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.15	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.39	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.35	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.89	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.58	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.96	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.12	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
A	25.2	0.04	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06
B	1.6	0.04	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.19	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.23	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.50	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.96	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.50	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.39	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.23	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
B	25.2	0.08	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06
C	1.6	0.08	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.31	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.73	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	0.85	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	1.27	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.50	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.89	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.27	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
C	25.2	0.15	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	1.12	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.93	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	2.89	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	8.18	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	8.53	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	8.76	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05

D	6.2	5.94	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	7.37	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	3.13	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	1.70	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.70	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.89	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	4.17	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.95	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.67	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	3.97	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	1.20	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.81	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.08	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
F	0.4	0.02	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	2.08	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.66	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.93	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	0.62	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.23	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.08	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
F	6.3	0.04	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04
G	0.4	0.04	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	2.01	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.16	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.15	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.08	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04





X/Q PERCENTILES  
 (BASED ON THE UPPER ENVELOPE OF THE  
 ORDERED X/Q-FREQUENCY VALUES, AND AS  
 PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 2)=	0.123
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 3)=	0.321
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 4)=	0.703
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 5)=	1.941
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 6)=	2.770
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 7)=	3.530
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 8)=	4.120
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 9)=	4.567
HANDCHECK GRAPH:	SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE (10)=	5.071

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
12	1	-6.01579	-10.14478	-1.00791
12	2	-7.09335	-11.37061	-1.41281
12	3	-7.51984	-13.37099	-2.14673
12	4	-8.09920	-13.50362	-2.20074
12	5	-8.95670	-13.13247	-2.02110
12	6	-9.26047	-14.31232	-2.63696
12	7	-9.54448	-15.15476	-3.10289
12	8	-9.76542	-16.21500	-3.71332
12	9	-9.94552	-19.53728	-5.68105
12	10	-10.23154	NUMXQ(K)= 10	
		1.031E-03	0.059	1.000
		7.085E-04	0.178	3.000
		5.626E-04	0.297	5.000
		3.460E-04	0.594	10.000
		2.516E-04	0.890	15.000
		1.982E-04	1.187	20.000
		1.637E-04	1.484	25.000
		1.394E-04	1.781	30.000
		1.219E-04	2.078	35.000
		1.088E-04	2.374	40.000
		9.826E-05	2.671	45.000
		8.792E-05	2.968	50.000
		7.864E-05	3.265	55.000
		7.079E-05	3.561	60.000
		6.318E-05	3.858	65.000
		5.666E-05	4.155	70.000
		5.022E-05	4.452	75.000
		4.321E-05	4.749	80.000
		3.659E-05	5.045	85.000
		3.935E-04	0.5	8.42

ANNUAL AVERAGE = 5.67E-06

K= 12 FIVEXQ(K) = 3.935E-04 FIVEPR(K) = 8.424

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE E SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.03	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.11	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.27	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.38	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.49	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.74	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.71	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.27	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
A	25.2	0.03	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06
B	1.6	0.03	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.11	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.30	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.44	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.76	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.57	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.52	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.27	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
C	1.6	0.08	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.14	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.68	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.09	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	0.74	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.74	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.90	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.27	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
C	25.2	0.08	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.71	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.25	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	2.24	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	6.57	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	7.77	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	8.94	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	6.90	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05

CALCULATION NO. BYR04-050, BRW-04-0044-M			MINOR REV. NO. 1B			APPENDIX BB-5					PAGE NO. 61 of 163	
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D	8.2	10.99	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	3.87	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	2.67	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.69	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.84	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	2.67	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.84	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	5.15	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	4.20	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	1.39	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	1.04	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.22	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
F	0.4	0.02	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	1.91	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	3.08	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.72	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	1.01	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.08	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
F	5.3	0.05	445.	0.	0.	17.8	7.5	20.8	3.853E-04	1.503E-04	1.503E-04
G	0.4	0.04	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	1.99	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.06	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.25	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.05	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

E SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04
0.035	0.052	0.071	2.061	2.071	2.125	3.189	5.098	5.343	8.425
0.00294	0.00433	0.00594	0.17316	0.17393	0.17851	0.26785	0.42820	0.44881	0.70766
3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.503E-04	1.293E-04
10.116	11.834	12.843	13.552	16.388	16.470	19.142	20.397	20.451	27.296
0.84968	0.99400	1.07875	1.13831	1.37654	1.38341	1.60790	1.71327	1.71785	2.29282
1.289E-04	1.018E-04	9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05
29.532	29.614	34.768	41.341	45.540	45.677	53.449	54.840	63.784	63.812
2.48065	2.48753	2.92047	3.47252	3.82529	3.83674	4.48959	4.60641	5.35776	5.36005
5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	2.896E-05	2.875E-05
64.493	65.530	72.429	72.538	72.756	73.847	84.837	85.574	89.446	89.746
5.41732	5.50436	6.08391	6.09307	6.11139	6.20302	7.12617	7.18802	7.51330	7.53849
2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05
90.482	90.919	90.946	91.846	92.610	92.719	92.991	93.564	96.237	96.755
7.60034	7.63699	7.63928	7.71488	7.77901	7.78818	7.81108	7.85919	8.08368	8.12720
1.071E-05	8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.260E-06	1.328E-06	
97.027	97.300	97.682	98.173	98.255	98.991	99.700	99.973	100.000	
8.15011	8.17301	8.20508	8.24632	8.25319	8.31503	8.37459	8.39750	8.39979	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.428  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.993  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.478  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.469  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.486  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 5.354  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 6.080  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 7.122

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
13	1	-6.01579	-9.97386	-0.98524
13	2	-7.09335	-11.33067	-1.44932
13	3	-7.51984	-12.59195	-1.92901
13	4	-8.09920	-13.56594	-2.34720
13	5	-8.95670	-12.99187	-2.05486
13	6	-9.26047	-13.59387	-2.38639
13	7	-9.54448	-13.93364	-2.58662
13	8	-9.76542	-14.34542	-2.84215
13	9	-9.94552	-15.38862	-3.51601
13	10	-10.23154	NUMXQ(K) = 10	
		1.030E-03	0.084	1.000
		6.992E-04	0.252	3.000
		5.474E-04	0.420	5.000
		3.427E-04	0.840	10.000
		2.458E-04	1.260	15.000
		1.883E-04	1.680	20.000
		1.520E-04	2.100	25.000
		1.271E-04	2.520	30.000
		1.108E-04	2.940	35.000
		9.806E-05	3.360	40.000
		8.673E-05	3.780	45.000
		7.718E-05	4.200	50.000
		6.912E-05	4.620	55.000
		6.202E-05	5.040	60.000
		5.590E-05	5.460	65.000
		5.034E-05	5.880	70.000
		4.505E-05	6.300	75.000
		4.010E-05	6.720	80.000
		4.894E-04	0.5	5.95

ANNUAL AVERAGE = 7.63E-06

K= 13 FIVEXQ(K)= 4.894E-04 FIVEPR(K)= 5.953

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ESE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.6	0.03	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05
A	2.1	0.08	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.44	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.83	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.89	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.53	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	1.27	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.11	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
B	1.1	0.03	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05
B	1.6	0.03	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.03	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.19	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.55	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.75	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.89	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.72	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.25	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
B	25.2	0.06	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06
C	1.6	0.08	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.14	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	0.80	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.11	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	1.25	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	1.13	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	1.19	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	10.3	0.47	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05
C	25.2	0.06	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.89	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	1.77	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	2.96	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	8.63	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	9.93	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	10.27	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05



D	6.2	8.69	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	8.80	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	3.76	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
D	25.2	0.89	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.80	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.85	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	3.21	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	6.03	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	3.54	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	1.80	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	0.55	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.22	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
E	10.5	0.03	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05
E	25.8	0.11	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05
F	0.4	0.02	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	2.46	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.16	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	0.69	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	0.50	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
F	4.2	0.03	445.	0.	0.	17.8	7.5	27.5	3.636E-04	1.875E-04	1.875E-04
G	0.4	0.05	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	2.60	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	0.64	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.17	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04
G	3.2	0.03	445.	0.	0.	12.3	4.7	34.3	6.148E-04	5.724E-04	5.724E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

ESE SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04
0.046	0.067	0.088	2.689	2.700	2.728	3.364	5.827	5.993	8.152
0.00379	0.00556	0.00724	0.22257	0.22351	0.22580	0.27849	0.48236	0.49611	0.67478
3.146E-04	3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04	1.648E-04	1.293E-04	1.289E-04
9.951	10.643	11.141	12.026	14.877	14.904	18.114	19.885	25.918	28.879
0.82367	0.88094	0.92217	0.99548	1.23142	1.23371	1.49943	1.64603	2.14540	2.39050
1.018E-04	9.731E-05	9.511E-05	8.343E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05
28.962	32.505	41.139	41.166	42.965	43.103	53.038	53.592	63.859	63.886
2.39738	2.69059	3.40528	3.40757	3.55647	3.56792	4.39028	4.43609	5.28593	5.28823
5.179E-05	4.895E-05	4.794E-05	4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	2.896E-05	2.875E-05
64.689	64.910	73.600	73.627	73.655	74.762	83.562	84.807	88.571	88.765
5.35466	5.37298	6.09226	6.09455	6.09684	6.18847	6.91690	7.01999	7.33152	7.34755
2.611E-05	2.164E-05	2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05
89.899	90.453	90.480	91.670	92.417	92.528	92.611	93.082	93.967	94.853
7.44147	7.48729	7.48958	7.58808	7.64992	7.65909	7.66596	7.70490	7.77820	7.85151
1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	3.260E-06
95.572	96.015	96.264	97.094	97.980	98.035	98.561	99.834	99.889	100.000
7.91106	7.94771	7.96833	8.03705	8.11035	8.11493	8.15846	8.26383	8.26841	8.27757

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.482  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.880  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.388  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.402  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.387  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 5.282  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 6.088  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 6.913

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
14	1	-6.01579	-9.84803	-0.96838
14	2	-7.09335	-11.83253	-1.66601
14	3	-7.51984	-14.50643	-2.69896
14	4	-8.09920	-13.25958	-2.17374
14	5	-8.95670	-12.84192	-1.96275
14	6	-9.26047	-13.68046	-2.42229
14	7	-9.54448	-13.76510	-2.47186
14	8	-9.76542	-13.88789	-2.54774
14	9	-9.94552	-16.74438	-4.39374
14	10	-10.23154	NUMXQ(K) = 10	
		1.112E-03	0.083	1.000
		7.835E-04	0.248	3.000
		5.916E-04	0.414	5.000
		3.232E-04	0.828	10.000
		2.292E-04	1.242	15.000
		1.792E-04	1.656	20.000
		1.470E-04	2.069	25.000
		1.248E-04	2.483	30.000
		1.095E-04	2.897	35.000
		9.750E-05	3.311	40.000
		8.617E-05	3.725	45.000
		7.657E-05	4.139	50.000
		6.861E-05	4.553	55.000
		6.188E-05	4.967	60.000
		5.614E-05	5.380	65.000
		5.112E-05	5.794	70.000
		4.597E-05	6.208	75.000
		3.977E-05	6.622	80.000
		5.244E-04	0.5	6.04

ANNUAL AVERAGE = 7.76E-06

K= 14 FIVEXQ(K)= 5.244E-04 FIVEPR(K)= 6.040

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS				
AT 10.0 METERS												
A	1.1	0.03	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05	
A	1.6	0.06	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05	
A	2.1	0.09	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.23	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	0.82	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	1.43	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	1.32	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	1.00	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
A	10.3	0.06	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06	
CA=1459.SQ.METERS												
B	1.1	0.03	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05	
B	1.6	0.06	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.09	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.53	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	1.00	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	1.23	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.79	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.67	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
B	10.3	0.09	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06	
C	1.6	0.12	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.12	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	1.29	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	1.70	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	1.38	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	1.29	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.97	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
C	10.3	0.15	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05	
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04	
D	1.1	0.76	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04	
D	1.6	1.70	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04	
D	2.1	2.87	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04	
D	3.1	10.66	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05	
D	4.1	11.36	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05	
D	5.2	8.75	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05	
D	6.2	6.00	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05	

D	8.2	4.16	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05
D	10.3	0.64	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	2.14	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	3.07	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	5.42	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	5.62	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	3.81	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	1.29	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	0.32	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.09	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
F	0.4	0.02	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	2.78	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	3.69	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	1.93	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	0.44	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
G	0.4	0.06	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	3.22	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	2.28	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.38	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

## SITE EXCLUSION BOUNDARY CALCULATIONS:

SE SECTOR BOUNDARY DISTANCE = 445.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04	3.146E-04
0.057	0.081	0.105	3.325	3.335	5.618	8.400	8.780	12.469	14.606
0.00443	0.00632	0.00821	0.26019	0.26096	0.43963	0.65725	0.68703	0.97565	1.14287
3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.732E-04	1.648E-04	1.293E-04	1.289E-04	1.018E-04	9.731E-05
16.538	16.977	17.738	20.812	26.228	27.926	33.546	36.415	36.533	40.338
1.29406	1.32842	1.38798	1.62850	2.05228	2.18514	2.62495	2.84944	2.85860	3.15639
9.511E-05	8.343E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05
50.994	51.023	52.312	52.429	63.787	64.109	72.862	72.921	74.209	74.297
3.99020	3.99249	4.09328	4.10244	4.99123	5.01643	5.70134	5.70593	5.80672	5.81359
4.794E-05	4.299E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05
80.298	80.386	82.084	86.241	87.617	87.646	88.290	88.817	90.105	91.100
6.28318	6.29005	6.42291	6.74819	6.85585	6.85814	6.90854	6.94977	7.05056	7.12844
2.105E-05	1.961E-05	1.735E-05	1.602E-05	1.577E-05	1.449E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06
91.159	92.125	93.355	93.442	93.589	94.379	95.053	95.287	95.375	96.194
7.13302	7.20862	7.30483	7.31170	7.32315	7.38500	7.43769	7.45601	7.46288	7.52702
6.463E-06	5.398E-06	4.055E-06	3.260E-06						
97.629	98.946	99.941	100.000						
7.63927	7.74235	7.82023	7.82481						

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.656  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 1.293  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 2.847  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.987  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 4.988  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 5.698  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 9)= 6.279  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE(10)= 6.744

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
15	1	-6.01579	-9.76966	-0.95770
15	2	-7.09335	-10.88576	-1.35709
15	3	-7.51984	-13.22644	-2.30083
15	4	-8.09920	-13.98584	-2.64160
15	5	-8.95670	-12.77142	-2.00372
15	6	-9.26047	-13.94851	-2.67549
15	7	-9.54448	-15.10690	-3.37923
15	8	-9.76542	-15.58239	-3.68004
15	9	-9.94552	-21.90446	-7.80741
15	10	-10.23154	NUMXQ(K)= 10	
		1.182E-03	0.078	1.000
		8.574E-04	0.235	3.000
		6.920E-04	0.391	5.000
		4.692E-04	0.782	10.000
		3.313E-04	1.174	15.000
		2.494E-04	1.565	20.000
		1.964E-04	1.956	25.000
		1.606E-04	2.347	30.000
		1.349E-04	2.739	35.000
		1.186E-04	3.130	40.000
		1.067E-04	3.521	45.000
		9.686E-05	3.912	50.000
		8.653E-05	4.304	55.000
		7.747E-05	4.695	60.000
		6.942E-05	5.086	65.000
		6.139E-05	5.477	70.000
		5.443E-05	5.869	75.000
		4.828E-05	6.260	80.000
		3.818E-05	6.651	85.000
		6.177E-04	0.5	6.39

ANNUAL AVERAGE = 9.12E-06

K= 15 FIVEXQ(K)= 6.177E-04 FIVEPR(K)= 6.390

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
									CA=1459.SQ.METERS		
AT 10.0 METERS											
A	1.1	0.04	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05
A	2.1	0.04	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05
A	3.1	0.53	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05
A	4.1	0.73	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06
A	5.2	0.73	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06
A	6.2	0.81	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06
A	8.2	0.57	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06
A	10.3	0.04	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06
B	1.6	0.16	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05
B	2.1	0.20	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05
B	3.1	0.65	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05
B	4.1	0.65	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05
B	5.2	0.89	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05
B	6.2	0.65	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05
B	8.2	0.36	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05
B	10.3	0.04	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06
C	1.1	0.04	445.	0.	0.	51.5	29.2	51.5	1.967E-04	1.503E-04	1.503E-04
C	1.6	0.16	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04
C	2.1	0.41	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05
C	3.1	1.01	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05
C	4.1	1.42	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05
C	5.2	1.38	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05
C	6.2	0.65	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05
C	8.2	0.57	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05
C	25.2	0.04	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06
D	0.4	0.01	445.	0.	0.	36.3	16.8	72.5	7.150E-04	8.108E-04	7.150E-04
D	1.1	0.61	445.	0.	0.	36.3	16.8	72.5	2.434E-04	2.760E-04	2.434E-04
D	1.6	2.64	445.	0.	0.	36.3	16.8	72.5	1.648E-04	1.869E-04	1.648E-04
D	2.1	3.85	445.	0.	0.	36.3	16.8	70.6	1.289E-04	1.422E-04	1.289E-04
D	3.1	12.29	445.	0.	0.	36.3	16.8	54.7	1.111E-04	9.511E-05	9.511E-05
D	4.1	11.64	445.	0.	0.	36.3	16.8	45.8	1.000E-04	7.160E-05	7.160E-05
D	5.2	11.03	445.	0.	0.	36.3	16.8	39.8	9.219E-05	5.740E-05	5.740E-05
D	6.2	5.15	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05
D	8.2	4.18	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05



CALCULATION NO. BYR04-050, BRW-04-0044-M			MINOR REV. NO. 1B			APPENDIX BB-5					PAGE NO. 73 of 163
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D	10.3	0.69	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05
E	0.4	0.02	445.	0.	0.	25.8	11.9	77.3	9.242E-04	1.102E-03	9.242E-04
E	1.1	1.78	445.	0.	0.	25.8	11.9	77.3	3.146E-04	3.751E-04	3.146E-04
E	1.6	2.31	445.	0.	0.	25.8	11.9	77.3	2.131E-04	2.541E-04	2.131E-04
E	2.1	3.53	445.	0.	0.	25.8	11.9	72.4	1.732E-04	1.933E-04	1.732E-04
E	3.2	8.07	445.	0.	0.	25.8	11.9	48.4	1.732E-04	1.293E-04	1.293E-04
E	4.2	4.01	445.	0.	0.	25.8	11.9	36.4	1.732E-04	9.731E-05	9.731E-05
E	5.3	1.22	445.	0.	0.	25.8	11.9	29.2	1.732E-04	7.802E-05	7.802E-05
E	6.3	0.36	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05
E	8.4	0.20	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05
F	0.4	0.01	445.	0.	0.	17.8	7.5	71.2	1.593E-03	2.123E-03	1.593E-03
F	1.1	1.58	445.	0.	0.	17.8	7.5	71.2	5.422E-04	7.229E-04	5.422E-04
F	1.6	2.60	445.	0.	0.	17.8	7.5	71.2	3.672E-04	4.896E-04	3.672E-04
F	2.1	2.60	445.	0.	0.	17.8	7.5	65.5	3.038E-04	3.725E-04	3.038E-04
F	3.2	1.70	445.	0.	0.	17.8	7.5	39.4	3.376E-04	2.491E-04	2.491E-04
G	0.4	0.05	445.	0.	0.	12.3	4.7	73.7	2.440E-03	4.879E-03	2.440E-03
G	1.1	2.76	445.	0.	0.	12.3	4.7	73.7	8.306E-04	1.661E-03	8.306E-04
G	1.6	1.95	445.	0.	0.	12.3	4.7	73.7	5.625E-04	1.125E-03	5.625E-04
G	2.1	0.41	445.	0.	0.	12.3	4.7	66.1	4.769E-04	8.560E-04	4.769E-04

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### SITE EXCLUSION BOUNDARY CALCULATIONS:

SSE SECTOR      BOUNDARY DISTANCE = 445.0 METERS

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AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.625E-04	5.422E-04	4.769E-04	3.672E-04	3.146E-04
0.049	0.062	0.082	2.840	2.848	4.794	6.375	6.781	9.376	11.160
0.00274	0.00352	0.00466	0.16042	0.16087	0.27082	0.36016	0.38306	0.52967	0.63046
3.038E-04	2.491E-04	2.434E-04	2.131E-04	1.732E-04	1.648E-04	1.503E-04	1.293E-04	1.289E-04	1.018E-04
13.755	15.458	16.066	18.377	21.905	24.541	24.581	32.650	36.502	36.664
0.77706	0.87327	0.90763	1.03820	1.23749	1.38639	1.38868	1.84452	2.06214	2.07130
9.731E-05	9.511E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05
40.679	52.965	54.181	54.586	66.224	66.589	77.618	77.780	78.794	78.996
2.29808	2.99216	3.06088	3.08379	3.74121	3.76183	4.38490	4.39406	4.45133	4.46278
4.794E-05	4.299E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05
84.146	84.349	85.768	89.944	91.323	91.363	92.053	92.701	93.350	93.999
4.75370	4.76515	4.84532	5.08127	5.15915	5.16144	5.20038	5.23703	5.27368	5.31034
1.961E-05	1.735E-05	1.602E-05	1.449E-05	1.089E-05	1.071E-05	8.752E-06	8.061E-06	6.463E-06	6.422E-06
94.567	95.459	95.499	96.148	96.513	97.040	97.081	97.810	98.540	98.581
5.34240	5.39280	5.39509	5.43174	5.45236	5.48214	5.48443	5.52566	5.56689	5.56918
5.398E-06	4.055E-06	3.260E-06							
99.392	99.959	100.000							
5.61500	5.64707	5.64936							

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.360  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.776  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.060  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.989  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.738  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.381  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.750

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
16	1	-6.01579	-10.01595	-0.99160
16	2	-7.09335	-11.93428	-1.64247
16	3	-7.51984	-13.33558	-2.16384
16	4	-8.09920	-13.58273	-2.26597
16	5	-8.95670	-12.85332	-1.90869
16	6	-9.26047	-14.58379	-2.82799
16	7	-9.54448	-14.87237	-2.98994
16	8	-9.76542	-17.76390	-4.68283
16	9	-9.94552	NUMXQ(K) = 9	
		1.128E-03	0.056	1.000
		8.077E-04	0.169	3.000
		6.185E-04	0.282	5.000
		3.886E-04	0.565	10.000
		2.827E-04	0.847	15.000
		2.215E-04	1.130	20.000
		1.822E-04	1.412	25.000
		1.546E-04	1.695	30.000
		1.340E-04	1.977	35.000
		1.198E-04	2.260	40.000
		1.089E-04	2.542	45.000
		9.981E-05	2.825	50.000
		9.073E-05	3.107	55.000
		8.128E-05	3.390	60.000
		7.334E-05	3.672	65.000
		6.633E-05	3.955	70.000
		6.024E-05	4.237	75.000
		5.368E-05	4.519	80.000
		4.260E-04	0.5	8.85

ANNUAL AVERAGE = 6.00E-06

K= 16 FIVEXQ(K) = 4.260E-04 FIVEPR(K) = 8.851

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ALL SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS				
AT 10.0 METERS									CA=1459.SQ.METERS			
A	1.1	0.02	445.	0.	0.	90.2	100.5	90.2	3.267E-05	3.108E-05	3.108E-05	
A	1.6	0.05	445.	0.	0.	90.2	100.5	90.2	2.213E-05	2.105E-05	2.105E-05	
A	2.1	0.08	445.	0.	0.	90.2	100.5	90.2	1.684E-05	1.602E-05	1.602E-05	
A	3.1	0.41	445.	0.	0.	90.2	100.5	90.2	1.126E-05	1.071E-05	1.071E-05	
A	4.1	0.66	445.	0.	0.	90.2	100.5	90.2	8.474E-06	8.061E-06	8.061E-06	
A	5.2	0.74	445.	0.	0.	90.2	100.5	90.2	6.794E-06	6.463E-06	6.463E-06	
A	6.2	0.55	445.	0.	0.	90.2	100.5	90.2	5.675E-06	5.398E-06	5.398E-06	
A	8.2	0.73	445.	0.	0.	90.2	100.5	90.2	4.263E-06	4.055E-06	4.055E-06	
A	10.3	0.14	445.	0.	0.	90.2	100.5	90.2	3.428E-06	3.260E-06	3.260E-06	
A	25.2	0.03	445.	0.	0.	90.2	100.5	90.2	1.396E-06	1.328E-06	1.328E-06	
B	1.1	0.02	445.	0.	0.	67.8	45.5	67.8	9.599E-05	8.343E-05	8.343E-05	
B	1.6	0.06	445.	0.	0.	67.8	45.5	67.8	6.501E-05	5.650E-05	5.650E-05	
B	2.1	0.11	445.	0.	0.	67.8	45.5	67.8	4.947E-05	4.299E-05	4.299E-05	
B	3.1	0.44	445.	0.	0.	67.8	45.5	67.8	3.308E-05	2.875E-05	2.875E-05	
B	4.1	0.68	445.	0.	0.	67.8	45.5	67.8	2.490E-05	2.164E-05	2.164E-05	
B	5.2	0.79	445.	0.	0.	67.8	45.5	67.8	1.996E-05	1.735E-05	1.735E-05	
B	6.2	0.55	445.	0.	0.	67.8	45.5	67.8	1.667E-05	1.449E-05	1.449E-05	
B	8.2	0.45	445.	0.	0.	67.8	45.5	67.8	1.252E-05	1.089E-05	1.089E-05	
B	10.3	0.14	445.	0.	0.	67.8	45.5	67.8	1.007E-05	8.752E-06	8.752E-06	
B	25.2	0.04	445.	0.	0.	67.8	45.5	67.8	4.101E-06	3.565E-06	3.565E-06	
C	1.1	0.01	445.	0.	0.	51.5	29.2	51.5	1.967E-04	1.503E-04	1.503E-04	
C	1.6	0.10	445.	0.	0.	51.5	29.2	51.5	1.332E-04	1.018E-04	1.018E-04	
C	2.1	0.29	445.	0.	0.	51.5	29.2	51.5	1.014E-04	7.746E-05	7.746E-05	
C	3.1	0.96	445.	0.	0.	51.5	29.2	51.5	6.778E-05	5.179E-05	5.179E-05	
C	4.1	1.13	445.	0.	0.	51.5	29.2	51.5	5.102E-05	3.899E-05	3.899E-05	
C	5.2	1.06	445.	0.	0.	51.5	29.2	51.5	4.091E-05	3.126E-05	3.126E-05	
C	6.2	0.71	445.	0.	0.	51.5	29.2	51.5	3.416E-05	2.611E-05	2.611E-05	
C	8.2	0.63	445.	0.	0.	51.5	29.2	51.5	2.567E-05	1.961E-05	1.961E-05	
C	10.3	0.17	445.	0.	0.	51.5	29.2	51.5	2.064E-05	1.577E-05	1.577E-05	
C	25.2	0.05	445.	0.	0.	51.5	29.2	51.5	8.404E-06	6.422E-06	6.422E-06	
D	0.4	0.01	445.	0.	0.	36.3	16.8	36.3	1.430E-03	8.108E-04	8.108E-04	
D	1.1	0.71	445.	0.	0.	36.3	16.8	36.3	4.868E-04	2.760E-04	2.760E-04	
D	1.6	1.71	445.	0.	0.	36.3	16.8	36.3	3.297E-04	1.869E-04	1.869E-04	
D	2.1	2.89	445.	0.	0.	36.3	16.8	36.3	2.509E-04	1.422E-04	1.422E-04	

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5				PAGE NO. 77 of 163		
D	3.1	8.55	445.	0.	0.	36.3	16.8	36.3	1.677E-04	9.511E-05	9.511E-05	
D	4.1	8.69	445.	0.	0.	36.3	16.8	36.3	1.263E-04	7.160E-05	7.160E-05	
D	5.2	8.72	445.	0.	0.	36.3	16.8	36.3	1.012E-04	5.740E-05	5.740E-05	
D	6.2	5.97	445.	0.	0.	36.3	16.8	36.3	8.456E-05	4.794E-05	4.794E-05	
D	8.2	6.76	445.	0.	0.	36.3	16.8	36.3	6.352E-05	3.602E-05	3.602E-05	
D	10.3	2.02	445.	0.	0.	36.3	16.8	36.3	5.107E-05	2.896E-05	2.896E-05	
D	25.2	0.65	445.	0.	0.	36.3	16.8	36.3	2.080E-05	1.179E-05	1.179E-05	
E	0.4	0.02	445.	0.	0.	25.8	11.9	25.8	2.773E-03	1.102E-03	1.102E-03	
E	1.1	1.42	445.	0.	0.	25.8	11.9	25.8	9.439E-04	3.751E-04	3.751E-04	
E	1.6	2.42	445.	0.	0.	25.8	11.9	25.8	6.392E-04	2.541E-04	2.541E-04	
E	2.1	3.22	445.	0.	0.	25.8	11.9	25.8	4.864E-04	1.933E-04	1.933E-04	
E	3.2	7.17	445.	0.	0.	25.8	11.9	25.8	3.252E-04	1.293E-04	1.293E-04	
E	4.2	5.47	445.	0.	0.	25.8	11.9	25.8	2.448E-04	9.731E-05	9.731E-05	
E	5.3	3.56	445.	0.	0.	25.8	11.9	25.8	1.963E-04	7.802E-05	7.802E-05	
E	6.3	1.88	445.	0.	0.	25.8	11.9	25.8	1.639E-04	6.516E-05	6.516E-05	
E	8.4	1.45	445.	0.	0.	25.8	11.9	25.8	1.232E-04	4.895E-05	4.895E-05	
E	10.5	0.30	445.	0.	0.	25.8	11.9	25.8	9.902E-05	3.936E-05	3.936E-05	
E	25.8	0.04	445.	0.	0.	25.8	11.9	25.8	4.033E-05	1.603E-05	1.603E-05	
F	0.4	0.01	445.	0.	0.	17.8	7.5	17.8	6.371E-03	2.123E-03	2.123E-03	
F	1.1	1.32	445.	0.	0.	17.8	7.5	17.8	2.169E-03	7.229E-04	7.229E-04	
F	1.6	2.01	445.	0.	0.	17.8	7.5	17.8	1.469E-03	4.896E-04	4.896E-04	
F	2.1	1.92	445.	0.	0.	17.8	7.5	17.8	1.118E-03	3.725E-04	3.725E-04	
F	3.2	3.13	445.	0.	0.	17.8	7.5	17.8	7.473E-04	2.491E-04	2.491E-04	
F	4.2	1.47	445.	0.	0.	17.8	7.5	17.8	5.626E-04	1.875E-04	1.875E-04	
F	5.3	0.46	445.	0.	0.	17.8	7.5	17.8	4.510E-04	1.503E-04	1.503E-04	
F	6.3	0.07	445.	0.	0.	17.8	7.5	17.8	3.767E-04	1.256E-04	1.256E-04	
F	8.4	0.01	445.	0.	0.	17.8	7.5	17.8	2.830E-04	9.432E-05	9.432E-05	
G	0.4	0.03	445.	0.	0.	12.3	4.7	12.3	1.464E-02	4.879E-03	4.879E-03	
G	1.1	1.43	445.	0.	0.	12.3	4.7	12.3	4.984E-03	1.661E-03	1.661E-03	
G	1.6	1.07	445.	0.	0.	12.3	4.7	12.3	3.375E-03	1.125E-03	1.125E-03	
G	2.1	0.60	445.	0.	0.	12.3	4.7	12.3	2.568E-03	8.560E-04	8.560E-04	
G	3.2	0.72	445.	0.	0.	12.3	4.7	12.3	1.717E-03	5.724E-04	5.724E-04	
G	4.2	0.28	445.	0.	0.	12.3	4.7	12.3	1.293E-03	4.308E-04	4.308E-04	
G	5.3	0.06	445.	0.	0.	12.3	4.7	12.3	1.036E-03	3.454E-04	3.454E-04	
G	6.3	0.00	445.	0.	0.	12.3	4.7	12.3	8.656E-04	2.885E-04	2.885E-04	

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

DIRECTION-INDEPENDENT (S.R.P 2.3.4) MODEL.

MINIMUM BOUNDARY DISTANCE = 445.0 METERS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

4.879E-03	2.123E-03	1.661E-03	1.125E-03	1.102E-03	8.560E-04	8.108E-04	7.229E-04	5.724E-04	4.896E-04
0.025	0.037	1.468	2.543	2.559	3.154	3.163	4.483	5.202	7.209
0.02520	0.03665	1.46833	2.54266	2.55870	3.15428	3.16344	4.48288	5.20215	7.20880
4.308E-04	3.751E-04	3.725E-04	3.454E-04	2.885E-04	2.760E-04	2.541E-04	2.491E-04	1.933E-04	1.875E-04
7.486	8.904	10.828	10.890	10.895	11.605	14.021	17.148	20.367	21.833
7.48597	8.90391	10.82808	10.88993	10.89451	11.60463	14.02131	17.14810	20.36651	21.83255
1.869E-04	1.503E-04	1.503E-04	1.422E-04	1.293E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	9.432E-05
23.544	24.006	24.018	26.911	34.083	34.150	34.250	39.721	48.269	48.283
23.54370	24.00642	24.01787	26.91101	34.08316	34.14959	34.25038	39.72054	48.26939	48.28313
8.343E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05
48.304	51.866	52.152	60.845	62.726	71.444	71.509	72.464	73.914	79.888
48.30375	51.86576	52.15210	60.84526	62.72592	71.44428	71.50842	72.46363	73.91364	79.88776
4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05
79.993	80.291	81.420	88.178	89.241	89.264	91.286	91.731	92.436	93.112
79.99313	80.29092	81.42023	88.17776	89.24064	89.26353	91.28622	91.73061	92.43615	93.11190
2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05
93.165	93.797	94.583	94.626	94.709	94.876	95.423	96.069	96.521	96.926
93.16459	93.79682	94.58253	94.62605	94.70852	94.87574	95.42322	96.06918	96.52045	96.92590
8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	3.260E-06	1.328E-06	
97.070	97.726	98.461	98.516	99.063	99.794	99.831	99.975	100.000	
97.07021	97.72535	98.46066	98.51564	99.06312	99.79384	99.83049	99.97480	100.00000	

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 7.205  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 10.825

1.878E-03	1.000	1.000
1.001E-03	3.000	3.000
6.701E-04	5.000	5.000
3.939E-04	10.000	10.000
2.852E-04	15.000	15.000
2.197E-04	20.000	20.000
1.784E-04	25.000	25.000
1.536E-04	30.000	30.000
1.337E-04	35.000	35.000
1.172E-04	40.000	40.000
1.032E-04	45.000	45.000
9.176E-05	50.000	50.000
8.270E-05	55.000	55.000
7.441E-05	60.000	60.000
6.670E-05	65.000	65.000
5.944E-05	70.000	70.000
5.343E-05	75.000	75.000
6.700E-04	5.0	5.00

K= 17 FIVEXQ(K)= 6.700E-04 FIVEPR(K)= 5.000

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

FIVE PERCENT OVERALL SITE LIMIT

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

2.440E-03	1.593E-03	9.242E-04	8.306E-04	7.150E-04	5.724E-04	5.625E-04	5.422E-04	4.769E-04	4.308E-04
0.025	0.037	0.053	1.484	1.494	2.213	3.287	4.607	5.202	5.479
0.02520	0.03665	0.05269	1.48437	1.49353	2.21281	3.28714	4.60658	5.20216	5.47933
3.672E-04	3.454E-04	3.146E-04	3.038E-04	2.885E-04	2.491E-04	2.434E-04	2.131E-04	1.875E-04	1.732E-04
7.486	7.548	8.966	10.890	10.895	14.021	14.731	17.148	18.614	21.833
7.48597	7.54782	8.96576	10.88993	10.89452	14.02130	14.73142	17.14809	18.61414	21.83255
1.648E-04	1.503E-04	1.503E-04	1.293E-04	1.289E-04	1.256E-04	1.018E-04	9.731E-05	9.511E-05	9.432E-05
23.544	24.006	24.018	31.190	34.083	34.150	34.250	39.721	48.269	48.283
23.54369	24.00641	24.01787	31.19001	34.08315	34.14957	34.25035	39.72052	48.26936	48.28310
8.343E-05	7.802E-05	7.746E-05	7.160E-05	6.516E-05	5.740E-05	5.650E-05	5.179E-05	4.895E-05	4.794E-05
48.304	51.866	52.152	60.845	62.726	71.444	71.509	72.464	73.914	79.888
48.30371	51.86574	52.15207	60.84523	62.72588	71.44425	71.50838	72.46359	73.91360	79.88772
4.299E-05	3.936E-05	3.899E-05	3.602E-05	3.126E-05	3.108E-05	2.896E-05	2.875E-05	2.611E-05	2.164E-05
79.993	80.291	81.420	88.178	89.241	89.264	91.286	91.731	92.436	93.112
79.99308	80.29086	81.42016	88.17770	89.24059	89.26347	91.28616	91.73054	92.43606	93.11181
2.105E-05	1.961E-05	1.735E-05	1.603E-05	1.602E-05	1.577E-05	1.449E-05	1.179E-05	1.089E-05	1.071E-05
93.165	93.797	94.583	94.626	94.709	94.876	95.423	96.069	96.520	96.926
93.16448	93.79671	94.58242	94.62593	94.70837	94.87557	95.42304	96.06902	96.52026	96.92571
8.752E-06	8.061E-06	6.463E-06	6.422E-06	5.398E-06	4.055E-06	3.565E-06	3.260E-06	1.328E-06	
97.070	97.725	98.461	98.516	99.063	99.794	99.830	99.975	100.000	
97.07000	97.72513	98.46043	98.51540	99.06287	99.79359	99.83023	99.97453	99.99971	

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 14.731

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
18	1	-6.01579	-8.89020	-0.82626
18	2	-7.09335	-8.98596	-0.87029
18	3	-7.51984	-9.63928	-1.25811
18	4	-8.32075	-9.36496	-0.99635
18	5	-8.95670	-9.29635	-0.82890
18	6	-9.26047	-9.29634	-0.82871
18	7	-9.76542	-9.38980	-0.66359
18	8	-9.94552	NUMXQ(K)= 8	
		9.418E-04	1.000	1.000
		6.434E-04	3.000	3.000
		5.160E-04	5.000	5.000
		3.266E-04	10.000	10.000
		2.406E-04	15.000	15.000
		1.981E-04	20.000	20.000
		1.677E-04	25.000	25.000
		1.444E-04	30.000	30.000
		1.262E-04	35.000	35.000
		1.132E-04	40.000	40.000
		1.018E-04	45.000	45.000
		9.176E-05	50.000	50.000
		8.270E-05	55.000	55.000
		7.441E-05	60.000	60.000
		6.670E-05	65.000	65.000
		5.944E-05	70.000	70.000
		5.343E-05	75.000	75.000
		5.160E-04	5.0	5.00

K= 18 FIVEXQ(K)= 5.160E-04 FIVEPR(K)= 5.000

K	HIGHPR	PR	GRNDVT(K)
1	-3.04916	0.11475	5.94713
2	-1.83433	3.33028	4.12317
3	-3.31283	0.04618	3.63725
4	-3.22587	0.06280	4.74829
5	-2.99031	0.13936	5.67663
6	-2.95204	0.15785	4.65168
7	-2.97652	0.14578	5.13989
8	-2.88717	0.19437	7.75588
9	-2.77568	0.27544	8.28787
10	-2.86428	0.20899	7.26061
11	-2.84589	0.22144	6.68431
12	-2.81782	0.24176	5.93576

13	-2.71927	0.32713	8.39979
14	-2.66683	0.38286	8.27757
15	-2.57624	0.49942	7.82481
16	-2.76701	0.28287	5.64936

K	HOURS (K)	TOTHR
1	10.05218	10.05218
2	291.73240	301.78460
3	4.04552	305.83010
4	5.50123	311.33130
5	12.20756	323.53880
6	13.82722	337.36610
7	12.77042	350.13650
8	17.02688	367.16340
9	24.12846	391.29180
10	18.30716	409.59900
11	19.39842	428.99740
12	21.17786	450.17520
13	28.65695	478.83220
14	33.53841	512.37060
15	43.74879	556.11940
16	24.77956	580.89890

K	FIVEXQ	SVANN	SLTIME	TIMINT	I	TIME	XQT
1	2.420E-04	4.177E-06	-0.4841	-7.9908	1	8.0	-8.99755
					2	16.0	-9.33311
					3	72.0	-10.06128
					4	624.0	-11.10673
2	2.013E-04	2.896E-06	-0.5058	-8.1603	1	8.0	-9.21211
					2	16.0	-9.56272
					3	72.0	-10.32353
					4	624.0	-11.41587
3	1.706E-04	2.443E-06	-0.5064	-8.3252	1	8.0	-9.37819
					2	16.0	-9.72918
					3	72.0	-10.49081
					4	624.0	-11.58432
4	1.938E-04	3.129E-06	-0.4920	-8.2078	1	8.0	-9.23095
					2	16.0	-9.57201
					3	72.0	-10.31209
					4	624.0	-11.37466
5	3.702E-04	5.727E-06	-0.4972	-7.5567	1	8.0	-8.59060
					2	16.0	-8.93524
					3	72.0	-9.68307
					4	624.0	-10.75677
6	3.753E-04	4.542E-06	-0.5264	-7.5229	1	8.0	-8.61764

CALCULATION NO. BYR04-050, BRW-04-0044-M					MINOR REV. NO. 1B	APPENDIX BB-5	PAGE NO. 83 of 163
7	3.689E-04	4.584E-06	-0.5233	-7.5423	2	16.0	-8.98255
					3	72.0	-9.77436
					4	624.0	-10.91120
					1	8.0	-8.63045
8	4.241E-04	6.242E-06	-0.5031	-7.4167	2	16.0	-8.99317
					3	72.0	-9.78025
					4	624.0	-10.91031
					1	8.0	-8.46294
9	5.065E-04	7.354E-06	-0.5047	-7.2382	2	16.0	-8.81168
					3	72.0	-9.56843
					4	624.0	-10.65494
					1	8.0	-8.28775
10	4.043E-04	6.253E-06	-0.4972	-7.4688	2	16.0	-8.63761
					3	72.0	-9.39677
					4	624.0	-10.48675
					1	8.0	-8.50271
11	3.735E-04	5.989E-06	-0.4929	-7.5509	2	16.0	-8.84733
					3	72.0	-9.59514
					4	624.0	-10.66881
					1	8.0	-8.57585
12	3.935E-04	5.674E-06	-0.5056	-7.4901	2	16.0	-8.91751
					3	72.0	-9.65890
					4	624.0	-10.72334
					1	8.0	-8.54136
13	4.894E-04	7.632E-06	-0.4962	-7.2784	2	16.0	-8.89178
					3	72.0	-9.65218
					4	624.0	-10.74393
					1	8.0	-8.31026
14	5.244E-04	7.757E-06	-0.5025	-7.2050	2	16.0	-8.65420
					3	72.0	-9.40054
					4	624.0	-10.47209
					1	8.0	-8.24992
15	6.177E-04	9.122E-06	-0.5027	-7.0411	2	16.0	-8.59824
					3	72.0	-9.35407
					4	624.0	-10.43925
					1	8.0	-8.08648
16	4.260E-04	6.000E-06	-0.5084	-7.4086	2	16.0	-8.43493
					3	72.0	-9.19106
					4	624.0	-10.27667
					1	8.0	-8.08648
					2	16.0	-8.81816

	3	72.0	-9.58281
	4	624.0	-10.68066
17 6.700E-04 9.122E-06 -0.5124 -6.9530			
	1	8.0	-8.01853
	2	16.0	-8.37372
	3	72.0	-9.14445
	4	624.0	-10.25102
18 5.160E-04 9.122E-06 -0.4813 -7.2358			
	1	8.0	-8.23661
	2	16.0	-8.57020
	3	72.0	-9.29406
	4	624.0	-10.33335

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

DOWNWIND DISTANCE SECTOR (METERS)		RELATIVE CONCENTRATION (X/Q) VALUES (SEC/CUBIC METER) VERSUS AVERAGING TIME						HOURS PER YEAR MAX 0-2 HR X/Q IS EXCEEDED		DOWNWIND SECTOR
		0-2 HOURS	0-8 HOURS	8-24 HOURS	1-4 DAYS	4-30 DAYS	ANNUAL AVERAGE	IN SECTOR		
S	445.	2.42E-04	1.24E-04	8.84E-05	4.27E-05	1.50E-05	4.18E-06	10.1		S
SSW	445.	2.01E-04	9.98E-05	7.03E-05	3.29E-05	1.10E-05	2.90E-06	291.7		SSW
SW	445.	1.71E-04	8.45E-05	5.95E-05	2.78E-05	9.31E-06	2.44E-06	4.0		SW
WSW	445.	1.94E-04	9.80E-05	6.97E-05	3.32E-05	1.15E-05	3.13E-06	5.5		WSW
W	445.	3.70E-04	1.86E-04	1.32E-04	6.23E-05	2.13E-05	5.73E-06	12.2		W
WNW	445.	3.75E-04	1.81E-04	1.26E-04	5.69E-05	1.83E-05	4.54E-06	13.8		WNW
NW	445.	3.69E-04	1.79E-04	1.24E-04	5.66E-05	1.83E-05	4.58E-06	12.8		NW
NNW	445.	4.24E-04	2.11E-04	1.49E-04	6.99E-05	2.36E-05	6.24E-06	17.0		NNW
N	445.	5.06E-04	2.52E-04	1.77E-04	8.30E-05	2.79E-05	7.35E-06	24.1		N
NNE	445.	4.04E-04	2.03E-04	1.44E-04	6.81E-05	2.33E-05	6.25E-06	18.3		NNE
NE	445.	3.74E-04	1.89E-04	1.34E-04	6.39E-05	2.20E-05	5.99E-06	19.4		NE
ENE	445.	3.93E-04	1.95E-04	1.38E-04	6.43E-05	2.16E-05	5.67E-06	21.2		ENE
E	445.	4.89E-04	2.46E-04	1.74E-04	8.27E-05	2.83E-05	7.63E-06	28.7		E
ESE	445.	5.24E-04	2.61E-04	1.84E-04	8.66E-05	2.93E-05	7.76E-06	33.5		ESE
SE	445.	6.18E-04	3.08E-04	2.17E-04	1.02E-04	3.44E-05	9.12E-06	43.7		SE
SSE	445.	4.26E-04	2.11E-04	1.48E-04	6.89E-05	2.30E-05	6.00E-06	24.8		SSE
MAX X/Q		6.18E-04					TOTAL HOURS AROUND SITE:		580.9	
SRP 2.3.4	445.	6.70E-04	3.29E-04	2.31E-04	1.07E-04	3.53E-05	9.12E-06			
SITE LIMIT		5.16E-04	2.65E-04	1.90E-04	9.20E-05	3.25E-05	9.12E-06			

THE FIVE-PERCENT-FOR-THE-ENTIRE-SITE X/Q IS LIMITING.

\*\*NOTE\*\*: VALUES ON THIS PAGE ARE APPROXIMATIONS ONLY.  
CHECK THE REASONABLENESS OF THE ENVELOPES  
COMPUTED FOR THE 0-2 HOUR VALUES. FOR ANY  
FAULTY ENVELOPES, ADJUST THE ABOVE VALUES.

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE S SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.1	0.04	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	2.1	0.08	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.62	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	1.50	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.73	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.39	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.54	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
B	1.6	0.12	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.19	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.73	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.85	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	1.50	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.50	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.39	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.08	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.12	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.1	0.08	4828.	0.	0.	443.4	256.4	443.4	2.603E-06	2.592E-06	2.592E-06
C	1.6	0.08	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.23	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.81	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.39	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	1.35	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.69	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.46	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.08	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.08	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.69	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	1.23	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	4.20	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	10.44	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	12.60	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	14.33	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	8.47	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 87 of 163	
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D	8.2	7.59	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.54	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.62	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.16	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	1.93	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	1.73	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	5.85	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	4.62	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	1.77	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	0.54	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.23	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.92	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	1.19	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	0.77	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	1.50	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.58	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.04	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
G	0.4	0.02	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.96	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.27	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.19	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.35	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	0.04	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

S SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.017	0.025	0.988	1.001	1.271	1.463	2.388	2.734	2.773	2.782
0.00101	0.00149	0.05875	0.05953	0.07556	0.08702	0.14199	0.16261	0.16490	0.16543
2.327E-05	1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06	6.898E-06
3.976	4.746	5.902	7.404	7.982	9.907	9.946	10.639	12.373	18.227
0.23644	0.28226	0.35098	0.44032	0.47468	0.58921	0.59150	0.63273	0.73581	1.08400
6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.592E-06	2.216E-06
19.460	24.082	28.280	30.052	30.591	41.030	41.261	53.856	53.933	68.262
1.15730	1.43218	1.68187	1.78724	1.81931	2.44009	2.45383	3.20289	3.20747	4.05960
1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07
76.735	76.812	84.400	84.631	86.172	86.981	88.368	88.483	89.831	90.448
4.56355	4.56814	5.01940	5.03315	5.12477	5.17288	5.25534	5.26222	5.34239	5.37904
4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07	2.720E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07
91.141	91.334	91.372	91.834	92.566	92.643	93.491	93.568	95.070	95.570
5.42027	5.43173	5.43402	5.46150	5.50503	5.50961	5.56000	5.56459	5.65392	5.68370
1.313E-07	1.108E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.536E-08	
96.187	96.264	96.649	98.151	98.228	98.960	99.345	99.884	100.000	
5.72035	5.72493	5.74784	5.83718	5.84176	5.88528	5.90819	5.94026	5.94713	

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.059  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.162  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.440  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.431  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 1.785  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.056  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.560

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
1	1	-8.57707	-13.08970	-1.05854
1	2	-9.65463	-16.98518	-2.25895
1	3	-10.33672	-17.23053	-2.34231
1	4	-11.09395	-17.12962	-2.30380
1	5	-12.08707	-16.52718	-2.02856
1	6	-12.26668	-16.70947	-2.11535
1	7	-13.01987	-18.64922	-3.22747
1	8	-13.19770	NUMXQ(K)= 8	
		6.363E-05	0.059	1.000
		3.030E-05	0.178	3.000
		2.067E-05	0.297	5.000
		1.196E-05	0.595	10.000
		8.536E-06	0.892	15.000
		6.651E-06	1.189	20.000
		5.466E-06	1.487	25.000
		4.713E-06	1.784	30.000
		4.122E-06	2.081	35.000
		3.661E-06	2.379	40.000
		3.290E-06	2.676	45.000
		2.985E-06	2.974	50.000
		2.730E-06	3.271	55.000
		2.512E-06	3.568	60.000
		2.325E-06	3.866	65.000
		2.133E-06	4.163	70.000
		1.921E-06	4.460	75.000
		1.375E-05	0.5	8.41

ANNUAL AVERAGE = 1.17E-07

K= 1 FIVEXQ(K)= 1.375E-05 FIVEPR(K)= 8.407

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSW SECTOR.

CLASS	METER/SEC	PERCENT	METERS	TERRAIN HT METERS	EFF PLUME HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	** CHI/Q VALUES (SEC/CUBIC METER)		
									MEANDER	BLDG WAKE	USED
									CA=1459.SQ.METERS		
AT 10.0 METERS											
A	1.1	0.11	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	2.1	0.11	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.50	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	1.17	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	1.17	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	1.00	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.39	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.11	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
B	1.1	0.11	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07
B	1.6	0.17	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.28	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.44	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	1.11	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	1.11	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.89	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.17	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.06	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
C	1.1	0.06	4828.	0.	0.	443.4	256.4	443.4	2.603E-06	2.592E-06	2.592E-06
C	1.6	0.06	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.78	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.56	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.44	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.94	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.67	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.50	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.11	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
D	0.4	0.02	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	1.39	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	2.22	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	4.72	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	10.33	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	9.72	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	11.72	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	7.39	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 91 of 163	
D	8.2	10.28	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06	
D	10.3	2.00	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06	
D	25.2	0.22	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07	
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05	
E	1.1	1.50	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05	
E	1.6	1.89	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05	
E	2.1	2.78	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06	
E	3.2	6.78	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06	
E	4.2	4.83	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06	
E	5.3	1.56	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06	
E	6.3	0.56	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06	
E	8.4	0.22	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06	
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04	
F	1.1	1.17	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05	
F	1.6	0.67	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05	
F	2.1	1.06	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05	
F	3.2	1.78	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05	
F	4.2	0.33	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05	
F	5.3	0.06	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05	
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04	
G	1.1	0.50	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05	
G	1.6	0.17	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05	
G	2.1	0.06	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05	
G	3.2	0.06	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05	

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SSW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.665E-05	2.327E-05
0.009	0.019	0.519	0.536	0.703	0.758	1.925	1.980	1.998	2.665
0.00036	0.00078	0.02140	0.02210	0.02897	0.03126	0.07936	0.08165	0.08239	0.10988
1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06
3.721	5.221	6.998	7.332	9.221	9.276	10.665	13.443	20.221	22.443
0.15340	0.21525	0.28855	0.30230	0.38018	0.38247	0.43974	0.55427	0.83374	0.92537
5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.592E-06	2.216E-06	1.855E-06
27.277	31.999	33.554	34.110	44.443	44.666	54.388	54.444	66.166	73.555
1.12466	1.31936	1.38350	1.40641	1.83248	1.84164	2.24251	2.24480	2.72814	3.03280
1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07
73.611	83.889	84.666	86.666	87.222	87.333	88.778	88.944	89.889	90.111
3.03509	3.45887	3.49094	3.57340	3.59631	3.60089	3.66045	3.66732	3.70626	3.71543
4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07	2.720E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07
90.778	91.055	91.167	91.667	92.111	92.222	93.333	93.444	94.555	95.444
3.74291	3.75437	3.75895	3.77956	3.79789	3.80247	3.84829	3.85287	3.89868	3.93533
1.313E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08		
95.944	96.111	97.278	97.333	98.500	99.500	99.889	100.000		
3.95595	3.96282	4.01092	4.01322	4.06132	4.10255	4.11859	4.12317		

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.021  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.079  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.288  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.123  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 1.382  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 2.725  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.030  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 3.456

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
2	1	-8.57707	-13.59395	-1.11837
2	2	-9.65463	-15.69505	-1.71486
2	3	-10.27864	-16.75494	-2.05043
2	4	-11.09395	-16.82408	-2.07547
2	5	-12.08707	-17.21115	-2.24506
2	6	-12.26668	-18.19933	-2.69375
2	7	-13.01987	-20.39588	-3.83614
2	8	-13.19770	-22.33334	-4.86867
2	9	-13.48372	NUMXQ(K) = 9	
		4.728E-05	0.041	1.000
		2.623E-05	0.124	3.000
		1.897E-05	0.206	5.000
		1.188E-05	0.412	10.000
		8.881E-06	0.618	15.000
		7.163E-06	0.825	20.000
		6.031E-06	1.031	25.000
		5.189E-06	1.237	30.000
		4.501E-06	1.443	35.000
		3.901E-06	1.649	40.000
		3.430E-06	1.855	45.000
		3.052E-06	2.062	50.000
		2.741E-06	2.268	55.000
		2.482E-06	2.474	60.000
		2.262E-06	2.680	65.000
		2.017E-06	2.886	70.000
		1.779E-06	3.092	75.000
		1.546E-06	3.299	80.000
		1.036E-05	0.5	12.13

ANNUAL AVERAGE = 8.25E-08

K= 2 FIVEXQ(K) = 1.036E-05 FIVEPR(K) = 12.127

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SW SECTOR.

STABILITY CLASS	WINDSPEED METER/SEC	FREQUENCY PERCENT	DISTANCE METERS	TERRAIN METERS	HT METERS	EFF METERS	PLUME METERS	HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	** CHI/Q VALUES (SEC/CUBIC METER)		
												MEANDER	BLDG WAKE	USED
AT 10.0 METERS														
CA=1459.SQ.METERS														
A	2.1	0.06	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07			
A	3.1	0.63	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07			
A	4.1	0.69	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08			
A	5.2	0.44	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08			
A	6.2	0.31	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08			
A	8.2	0.19	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08			
B	2.1	0.06	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07			
B	3.1	0.31	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07			
B	4.1	0.50	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07			
B	5.2	0.57	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07			
B	6.2	0.19	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07			
B	8.2	0.50	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07			
C	1.6	0.06	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06			
C	2.1	0.57	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06			
C	3.1	0.82	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07			
C	4.1	1.01	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07			
C	5.2	0.82	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07			
C	6.2	0.63	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07			
C	8.2	0.25	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07			
C	10.3	0.13	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07			
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05			
D	1.1	1.01	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06			
D	1.6	3.27	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06			
D	2.1	4.53	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06			
D	3.1	10.39	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06			
D	4.1	8.57	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06			
D	5.2	8.88	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06			
D	6.2	7.62	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06			
D	8.2	13.67	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06			
D	10.3	5.35	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06			
D	25.2	1.01	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07			
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05			
E	1.1	1.89	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05			

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 95 of 163	
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E	1.6	1.95	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	1.89	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	5.42	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.73	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	3.21	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	2.33	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.50	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	1.13	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	0.44	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	0.57	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	0.88	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.25	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.50	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.13	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.06	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	2.665E-05	2.327E-05	1.844E-05
0.009	0.019	0.523	0.544	0.670	0.733	1.866	1.879	2.320	2.887
0.00032	0.00068	0.01901	0.01978	0.02436	0.02666	0.06789	0.06836	0.08440	0.10501
1.684E-05	1.520E-05	1.280E-05	1.140E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06	5.632E-06	4.717E-06
4.776	5.658	5.910	7.862	8.870	10.759	16.176	19.450	25.182	29.716
0.17373	0.20580	0.21496	0.28598	0.32263	0.39135	0.58835	0.70746	0.91592	1.08084
4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06
32.928	35.258	45.650	46.153	54.718	63.598	71.219	71.282	84.948	85.515
1.19767	1.28243	1.66039	1.67871	1.99025	2.31324	2.59041	2.59270	3.08978	3.11039
1.120E-06	8.932E-07	6.724E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.383E-07	2.851E-07	2.720E-07
90.868	91.687	92.694	93.513	94.521	95.151	95.214	95.466	95.780	95.906
3.30510	3.33488	3.37153	3.40131	3.43796	3.46087	3.46316	3.47232	3.48378	3.48836
2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.080E-07	9.881E-08	7.923E-08	6.617E-08	4.971E-08
96.410	96.473	97.040	97.229	97.859	98.363	99.055	99.496	99.811	100.000
3.50668	3.50897	3.52959	3.53646	3.55937	3.57769	3.60289	3.61893	3.63038	3.63725

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY



HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.019  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.068  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.206  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.196  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 1.659  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 2.311  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 2.588

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
3	1	-8.57707	-13.65483	-1.12565
3	2	-9.65463	-15.99180	-1.78327
3	3	-10.27864	-18.09280	-2.43907
3	4	-11.09395	-16.60010	-1.91887
3	5	-12.26668	-17.98582	-2.53248
3	6	-12.59163	-19.26928	-3.13504
3	7	-13.01987	-20.36619	-3.68531
3	8	-13.19770	NUMXQ(K)= 8	
		4.698E-05	0.036	1.000
		2.447E-05	0.109	3.000
		1.672E-05	0.182	5.000
		1.066E-05	0.364	10.000
		8.172E-06	0.546	15.000
		6.718E-06	0.727	20.000
		5.744E-06	0.909	25.000
		5.038E-06	1.091	30.000
		4.434E-06	1.273	35.000
		3.885E-06	1.455	40.000
		3.450E-06	1.637	45.000
		3.030E-06	1.819	50.000
		2.680E-06	2.000	55.000
		2.393E-06	2.182	60.000
		2.142E-06	2.364	65.000
		1.906E-06	2.546	70.000
		8.661E-06	0.5	13.75

ANNUAL AVERAGE = 7.07E-08

K= 3 FIVEXQ(K)= 8.661E-06 FIVEPR(K)=13.747

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WSW SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y SIGMA-Z MEANDER-SY			** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.1	0.10	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	2.1	0.10	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.34	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.43	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.58	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.39	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.77	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.29	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
B	1.1	0.10	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07
B	1.6	0.05	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	3.1	0.43	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.34	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.19	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.24	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.68	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.19	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
C	1.6	0.05	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.19	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.58	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	0.43	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.82	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.34	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.48	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.05	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.82	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	2.17	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	2.56	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	7.62	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	9.07	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	13.12	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	9.21	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	11.19	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.78	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06

E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.30	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.07	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	2.07	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.18	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	6.61	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	5.31	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	2.99	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.74	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.05	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
F	0.4	0.00	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.43	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	0.53	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	0.63	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	1.25	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	1.06	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.39	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	8.4	0.05	4828.	0.	0.	153.2	34.5	153.2	7.136E-06	6.560E-06	6.560E-06
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.72	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.39	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.14	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.10	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	0.14	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	5.3	0.10	4828.	0.	0.	105.8	21.5	110.5	2.536E-05	2.199E-05	2.199E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

WSW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.013	0.017	0.740	0.755	1.141	1.286	1.720	1.816	1.961	1.972
0.00060	0.00078	0.03514	0.03584	0.05417	0.06104	0.08166	0.08624	0.09311	0.09361
2.327E-05	2.199E-05	1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06
2.502	2.599	3.226	4.528	5.783	6.844	8.918	9.304	10.124	12.199
0.11881	0.12339	0.15317	0.21502	0.27458	0.32497	0.42347	0.44180	0.48074	0.57924
6.898E-06	6.560E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06
18.374	18.422	20.593	27.202	29.759	35.066	38.057	45.679	47.416	56.485
0.87245	0.87474	0.97782	1.29164	1.41305	1.66503	1.80705	2.16898	2.25144	2.68209
2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	8.275E-07	6.724E-07
56.534	69.656	78.870	78.918	90.110	90.303	92.088	92.667	92.764	93.198
2.68438	3.30745	3.74497	3.74726	4.27870	4.28786	4.37262	4.40011	4.40469	4.42530
5.604E-07	5.391E-07	4.503E-07	3.810E-07	3.383E-07	2.851E-07	2.720E-07	2.146E-07	1.963E-07	1.721E-07
93.246	94.066	94.404	94.500	94.983	95.417	95.465	95.803	95.899	96.092
4.42759	4.46654	4.48257	4.48715	4.51006	4.53068	4.53297	4.54900	4.55358	4.56275
1.437E-07	1.313E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	
96.334	96.671	97.347	97.781	97.974	98.553	98.939	99.711	100.000	
4.57420	4.59023	4.62230	4.64292	4.65208	4.67957	4.69790	4.73455	4.74829	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.035  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.082  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.274  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.290  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 1.663  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.304  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.742

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
4	1	-8.57707	-13.35368	-1.09160
4	2	-9.65463	-18.52216	-2.61683
4	3	-10.27864	-17.16181	-2.18500
4	4	-11.09395	-16.12766	-1.81261
4	5	-12.08707	-16.07988	-1.79117
4	6	-12.26668	-17.77572	-2.58776
4	7	-13.01987	-18.81989	-3.15591
4	8	-13.19770	NUMXQ(K)= 8	
		5.155E-05	0.047	1.000
		2.389E-05	0.142	3.000
		1.685E-05	0.237	5.000
		1.091E-05	0.475	10.000
		8.426E-06	0.712	15.000
		6.962E-06	0.950	20.000
		5.974E-06	1.187	25.000
		5.259E-06	1.424	30.000
		4.712E-06	1.662	35.000
		4.098E-06	1.899	40.000
		3.613E-06	2.137	45.000
		3.221E-06	2.374	50.000
		2.899E-06	2.612	55.000
		2.629E-06	2.849	60.000
		2.400E-06	3.086	65.000
		2.200E-06	3.324	70.000
		1.994E-06	3.561	75.000
		1.057E-05	0.5	10.53

ANNUAL AVERAGE = 8.99E-08

K= 4 FIVEXQ(K)= 1.057E-05 FIVEPR(K)=10.530

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE W SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.1	0.08	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	2.1	0.12	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.56	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	1.01	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.73	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.04	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.08	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
B	1.1	0.08	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07
B	1.6	0.12	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.12	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.56	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.85	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.61	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.16	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.08	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
C	1.1	0.04	4828.	0.	0.	443.4	256.4	443.4	2.603E-06	2.592E-06	2.592E-06
C	1.6	0.16	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.40	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	1.98	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.17	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.44	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.20	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.08	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.89	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	2.38	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	4.32	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	11.86	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	9.00	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	6.90	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	2.87	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	1.41	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	0.04	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06

E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.49	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	3.79	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	6.21	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	13.28	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	6.01	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	1.61	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	0.65	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.28	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.61	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.18	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	4.12	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	4.68	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.89	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.04	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.69	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.17	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	1.41	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	1.21	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	0.24	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	6.3	0.04	4828.	0.	0.	105.8	21.5	105.8	2.212E-05	1.837E-05	1.837E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

W SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.012	0.017	0.703	0.720	1.890	3.303	3.908	5.119	5.361	5.372
0.00069	0.00098	0.03993	0.04088	0.10731	0.18749	0.22185	0.29057	0.30431	0.30496
2.327E-05	1.844E-05	1.837E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06
7.551	11.667	11.708	13.201	17.882	18.769	22.563	22.603	23.491	29.705
0.42866	0.66231	0.66460	0.74936	1.01508	1.06547	1.28080	1.28309	1.33348	1.68625
6.898E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.592E-06
42.981	45.362	51.375	55.692	57.307	57.952	69.816	70.098	79.097	79.138
2.43989	2.57504	2.91635	3.16145	3.25308	3.28973	3.96319	3.97923	4.49005	4.49234
2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	8.275E-07	6.724E-07	5.604E-07
86.038	88.903	89.064	90.477	90.880	90.921	92.898	92.979	94.149	94.270
4.88405	5.04669	5.05585	5.13603	5.15893	5.16122	5.27347	5.27805	5.34448	5.35135
5.391E-07	4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07
94.714	94.916	95.037	95.117	95.198	95.763	96.610	96.731	97.337	97.498
5.37655	5.38800	5.39487	5.39945	5.40404	5.43610	5.48421	5.49108	5.52544	5.53460
1.313E-07	1.080E-07	9.881E-08	7.923E-08	6.617E-08	4.971E-08				
98.063	98.144	99.153	99.879	99.919	100.000				
5.56667	5.57126	5.62852	5.66975	5.67205	5.67663				

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.040  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.290  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.014  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.437  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.914  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.960  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.487  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.880

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
5	1	-8.57707	-13.28677	-1.08308
5	2	-9.65463	-13.49956	-1.14653
5	3	-10.33672	-15.11195	-1.73103
5	4	-11.09395	-16.32996	-2.25577
5	5	-11.88432	-17.06474	-2.62861
5	6	-12.08707	-18.99617	-3.64855
5	7	-12.59163	-19.74597	-4.07570
5	8	-12.83023	-20.82331	-4.71062
5	9	-13.01987	NUMXQ(K)= 9	
		5.727E-05	0.057	1.000
		3.941E-05	0.170	3.000
		3.271E-05	0.284	5.000
		2.190E-05	0.568	10.000
		1.702E-05	0.851	15.000
		1.382E-05	1.135	20.000
		1.137E-05	1.419	25.000
		9.654E-06	1.703	30.000
		8.377E-06	1.987	35.000
		7.388E-06	2.271	40.000
		6.551E-06	2.554	45.000
		5.810E-06	2.838	50.000
		5.046E-06	3.122	55.000
		4.378E-06	3.406	60.000
		3.834E-06	3.690	65.000
		3.383E-06	3.974	70.000
		2.967E-06	4.257	75.000
		2.611E-06	4.541	80.000
		2.278E-06	4.825	85.000
		2.364E-05	0.5	8.81

ANNUAL AVERAGE = 1.62E-07

K= 5 FIVEXQ(K)= 2.364E-05 FIVEPR(K)= 8.808

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WNW SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y SIGMA-Z MEANDER-SY			** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.6	0.15	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.10	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.39	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.69	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.44	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.20	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.30	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
B	1.6	0.15	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.25	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.79	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.59	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.64	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.34	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.05	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.05	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
C	1.6	0.10	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.44	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	1.23	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	0.69	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.59	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.10	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.15	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.10	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.64	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	2.41	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	3.89	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	7.98	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	5.91	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	5.66	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	3.05	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	3.89	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.48	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.34	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07

E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	0.98	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.31	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	3.99	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	8.42	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.37	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	3.50	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	1.72	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.92	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.79	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.30	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.69	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	1.67	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	3.10	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	7.88	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	4.78	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.98	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.10	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.49	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.48	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	1.38	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	2.66	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	1.53	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	5.3	0.15	4828.	0.	0.	105.8	21.5	110.5	2.536E-05	2.199E-05	2.199E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

WNW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.009	0.015	0.507	0.518	1.996	3.374	4.064	6.723	8.250	8.258
0.00040	0.00068	0.02359	0.02411	0.09283	0.15697	0.18904	0.31273	0.38374	0.38413
2.327E-05	2.199E-05	1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06
9.932	10.080	13.182	14.167	22.046	26.823	29.137	30.122	30.762	34.751
0.46201	0.46888	0.61320	0.65901	1.02552	1.24772	1.35538	1.40119	1.43097	1.61652
8.732E-06	6.898E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06
34.850	43.271	45.684	51.051	54.941	58.438	60.161	68.139	70.059	75.969
1.62110	2.01281	2.12505	2.37474	2.55570	2.71834	2.79851	3.16961	3.25894	3.53383
2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	9.669E-07	8.932E-07	6.724E-07
76.757	82.420	85.473	85.571	89.462	89.905	91.382	91.678	92.909	93.598
3.57048	3.83391	3.97593	3.98051	4.16147	4.18209	4.25081	4.26455	4.32182	4.35389
5.604E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07
93.746	94.337	94.682	94.780	95.026	95.174	95.962	96.060	96.208	96.799
4.36076	4.38825	4.40429	4.40887	4.42032	4.42719	4.46385	4.46843	4.47530	4.50279
1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08
96.898	97.538	97.882	98.276	98.326	99.015	99.064	99.508	99.705	100.000
4.50737	4.53715	4.55318	4.57151	4.57380	4.60587	4.60816	4.62878	4.63794	4.65168

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.312  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.024  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.246  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.372  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.716  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.167  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.531  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 3.831  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 3.973

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
6	1	-8.57707	-13.11985	-1.01779
6	2	-10.33672	-15.30008	-1.81509
6	3	-11.09395	-16.41983	-2.29830
6	4	-11.26578	-18.34265	-3.15572
6	5	-12.08707	-18.22916	-3.09847
6	6	-12.26668	-21.53285	-4.81528
6	7	-12.59163	-21.65345	-4.88022
6	8	-12.83023	-22.03122	-5.08917
6	9	-13.01987	-31.74827	-10.57689
6	10	-13.19770	NUMXQ(K)= 10	
		5.830E-05	0.047	1.000
		4.206E-05	0.140	3.000
		3.575E-05	0.233	5.000
		2.545E-05	0.465	10.000
		1.966E-05	0.698	15.000
		1.624E-05	0.930	20.000
		1.363E-05	1.163	25.000
		1.116E-05	1.396	30.000
		9.202E-06	1.628	35.000
		7.760E-06	1.861	40.000
		6.657E-06	2.093	45.000
		5.791E-06	2.326	50.000
		5.103E-06	2.558	55.000
		4.453E-06	2.791	60.000
		3.761E-06	3.024	65.000
		3.207E-06	3.256	70.000
		2.756E-06	3.489	75.000
		2.376E-06	3.721	80.000
		1.906E-06	3.954	85.000
		2.433E-05	0.5	10.75

ANNUAL AVERAGE = 1.26E-07

K= 6 FIVEXQ(K)= 2.433E-05 FIVEPR(K)=10.749

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NW SECTOR.

STABILITY CLASS	WINDSPEED METER/SEC AT 10.0 METERS	FREQUENCY PERCENT	DISTANCE METERS	TERRAIN METERS	HT METERS	PLUME METERS	HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	** CHI/Q VALUES (SEC/CUBIC METER)		
											MEANDER	BLDG WAKE	USED
											CA=1459.SQ.METERS		
A	1.6	0.13	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07		
A	2.1	0.09	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07		
A	3.1	0.18	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07		
A	4.1	0.31	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08		
A	5.2	0.45	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08		
A	6.2	0.40	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08		
A	8.2	0.31	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08		
B	1.6	0.09	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07		
B	2.1	0.13	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07		
B	3.1	0.40	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07		
B	4.1	0.98	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07		
B	5.2	0.67	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07		
B	6.2	0.45	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07		
B	8.2	0.18	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07		
B	10.3	0.22	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08		
C	1.6	0.09	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06		
C	2.1	0.58	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06		
C	3.1	1.47	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07		
C	4.1	0.89	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07		
C	5.2	1.03	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07		
C	6.2	0.45	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07		
C	8.2	0.22	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07		
C	10.3	0.22	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07		
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05		
D	1.1	0.80	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06		
D	1.6	1.69	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06		
D	2.1	2.09	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06		
D	3.1	7.31	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06		
D	4.1	7.09	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06		
D	5.2	6.77	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06		
D	6.2	3.43	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06		
D	8.2	3.74	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06		
D	10.3	1.20	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06		
D	25.2	0.04	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07		

E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.20	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	1.96	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	2.23	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	8.96	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	7.53	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	5.04	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	2.27	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.07	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.45	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.04	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.00	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.45	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	1.34	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	1.96	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	9.45	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	4.77	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.89	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.04	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.49	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.62	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.76	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	2.76	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	1.34	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	5.3	0.22	4828.	0.	0.	105.8	21.5	110.5	2.536E-05	2.199E-05	2.199E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

NW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.009	0.012	0.503	0.516	1.140	1.898	2.344	5.107	6.444	6.454
0.00044	0.00064	0.02584	0.02654	0.05861	0.09755	0.12046	0.26248	0.33120	0.33173
2.327E-05	2.199E-05	1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06
7.791	8.014	9.975	11.178	20.626	25.395	27.356	28.247	29.050	31.278
0.40045	0.41191	0.51270	0.57455	1.06017	1.30528	1.40607	1.45188	1.49311	1.60765
8.732E-06	6.898E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06
31.322	40.280	41.974	49.506	51.600	56.636	58.909	66.218	67.288	74.374
1.60994	2.07037	2.15741	2.54454	2.65220	2.91105	3.02787	3.40355	3.45852	3.82274
2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	9.669E-07	8.932E-07	6.724E-07
74.820	81.594	85.026	85.115	88.858	89.438	90.641	90.686	92.156	93.048
3.84565	4.19383	4.37022	4.37480	4.56722	4.59699	4.65884	4.66113	4.73673	4.78254
5.604E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07
93.137	94.162	94.206	94.652	94.786	95.008	95.410	95.632	95.766	96.747
4.78712	4.83981	4.84210	4.86501	4.87188	4.88333	4.90395	4.91540	4.92227	4.97267
1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08
96.836	97.504	97.950	98.128	98.306	98.618	98.841	99.287	99.688	100.000
4.97725	5.01161	5.03452	5.04368	5.05284	5.06888	5.08033	5.10324	5.12385	5.13989

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.262  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.059  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.304  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.542  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.908  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.190  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.367

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
7	1	-8.57707	-13.31160	-1.06563
7	2	-10.33672	-14.67844	-1.55524
7	3	-11.09395	-16.06300	-2.15597
7	4	-11.26578	-17.97814	-3.01668
7	5	-12.08707	-18.09517	-3.07661
7	6	-12.26668	-20.89125	-4.55254
7	7	-13.01987	-28.88731	-9.17720
7	8	-13.19770	NUMXQ(K)= 8	
		5.473E-05	0.051	1.000
		3.877E-05	0.154	3.000
		3.266E-05	0.257	5.000
		2.285E-05	0.514	10.000
		1.827E-05	0.771	15.000
		1.548E-05	1.028	20.000
		1.297E-05	1.285	25.000
		1.051E-05	1.542	30.000
		8.716E-06	1.799	35.000
		7.387E-06	2.056	40.000
		6.366E-06	2.313	45.000
		5.558E-06	2.570	50.000
		4.895E-06	2.827	55.000
		4.191E-06	3.084	60.000
		3.562E-06	3.341	65.000
		3.058E-06	3.598	70.000
		2.648E-06	3.855	75.000
		2.311E-06	4.112	80.000
		1.857E-06	4.369	85.000
		2.319E-05	0.5	9.73

ANNUAL AVERAGE = 1.28E-07

K= 7 FIVEXQ(K)= 2.319E-05 FIVEPR(K)= 9.728

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNW SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
									CA=1459.SQ.METERS		
AT 10.0 METERS											
A	1.6	0.03	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.03	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.44	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.62	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.62	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.30	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.74	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.15	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.03	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	1.1	0.03	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07
B	1.6	0.03	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.03	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.35	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.35	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.59	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.27	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.38	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.18	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.03	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.6	0.03	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.21	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.35	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	0.77	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.92	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.74	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.24	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.06	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.15	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.00	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.18	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	1.00	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	1.42	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	5.43	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	6.65	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06

D	5.2	6.70	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	4.84	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	5.97	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.65	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.62	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	0.80	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	1.24	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	1.62	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.53	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	7.24	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	5.61	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	3.96	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	3.10	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.50	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.18	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.62	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	1.24	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	1.57	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	8.12	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	5.91	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	2.95	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.35	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
F	8.4	0.12	4828.	0.	0.	153.2	34.5	153.2	7.136E-06	6.560E-06	6.560E-06
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.44	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.03	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.56	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	1.77	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	0.95	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	5.3	0.41	4828.	0.	0.	105.8	21.5	110.5	2.536E-05	2.199E-05	2.199E-05
G	6.3	0.03	4828.	0.	0.	105.8	21.5	105.8	2.212E-05	1.837E-05	1.837E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

NNW SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.008	0.013	0.456	0.465	1.499	2.060	2.680	4.452	5.398	5.400
0.00060	0.00102	0.03538	0.03608	0.11626	0.15978	0.20788	0.34532	0.41863	0.41880
2.327E-05	2.199E-05	1.844E-05	1.837E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06
6.640	7.054	8.619	8.649	9.446	17.568	23.475	24.716	27.669	27.846
0.51501	0.54708	0.66849	0.67078	0.73263	1.36257	1.82071	1.91691	2.14598	2.15973
8.921E-06	8.732E-06	6.898E-06	6.560E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06
29.471	29.825	36.352	36.471	37.475	44.711	46.128	51.740	55.698	61.132
2.28572	2.31320	2.81945	2.82861	2.90649	3.46771	3.57766	4.01289	4.31985	4.74133
2.953E-06	2.679E-06	2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	9.669E-07
64.233	70.879	71.381	78.085	82.929	82.958	88.924	89.131	90.785	90.962
4.98186	5.49726	5.53620	6.05619	6.43186	6.43415	6.89687	6.91291	7.04118	7.05493
8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.383E-07	2.851E-07
91.317	91.346	92.114	92.144	93.059	93.680	94.418	94.447	94.684	95.038
7.08242	7.08471	7.14427	7.14656	7.21757	7.26567	7.32294	7.32523	7.34356	7.37104
2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.108E-07	1.080E-07	9.881E-08
95.097	95.127	95.481	95.511	96.101	96.367	96.810	96.958	97.342	97.962
7.37562	7.37791	7.40540	7.40769	7.45351	7.47412	7.50848	7.51994	7.54972	7.59782
8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	3.536E-08	1.628E-08			
98.139	98.760	99.055	99.793	99.941	99.970	100.000			
7.61157	7.65967	7.68258	7.73984	7.75130	7.75359	7.75588			

X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.345  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.819  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 3.465  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 4.010  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 5.493  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 6.052  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.428

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
8	1	-8.57707	-13.17650	-1.05111
8	2	-10.33672	-14.45838	-1.52558
8	3	-11.26578	-17.48852	-2.97352
8	4	-12.08707	-16.96167	-2.68349
8	5	-12.26668	-18.80489	-3.73701
8	6	-12.83023	-19.09670	-3.91953
8	7	-13.01987	-22.03260	-5.81318
8	8	-13.19770	NUMXQ(K)= 8	
		5.277E-05	0.078	1.000
		3.712E-05	0.233	3.000
		3.056E-05	0.388	5.000
		2.112E-05	0.776	10.000
		1.677E-05	1.163	15.000
		1.413E-05	1.551	20.000
		1.186E-05	1.939	25.000
		9.460E-06	2.327	30.000
		7.774E-06	2.715	35.000
		6.532E-06	3.102	40.000
		5.588E-06	3.490	45.000
		4.910E-06	3.878	50.000
		4.230E-06	4.266	55.000
		3.626E-06	4.654	60.000
		3.139E-06	5.041	65.000
		2.741E-06	5.429	70.000
		2.399E-06	5.817	75.000
		2.063E-06	6.205	80.000
		2.677E-05	0.5	6.45

ANNUAL AVERAGE = 1.75E-07

K= 8 FIVEXQ(K)= 2.677E-05 FIVEPR(K)= 6.447

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE N SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.6	0.03	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	3.1	0.19	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.22	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.47	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.25	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.88	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.28	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.06	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	1.6	0.06	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	3.1	0.25	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.55	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.33	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.39	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.47	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.14	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.08	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.6	0.06	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.22	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.64	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.13	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.91	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.61	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.77	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.19	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
D	0.4	0.00	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.28	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	0.91	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	1.77	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	6.27	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	7.05	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	5.94	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	5.42	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	5.20	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.60	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 119 of 163
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D	25.2	0.06	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	0.77	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	1.66	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	2.49	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	7.10	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	6.69	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	6.05	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	3.81	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	3.95	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.55	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.03	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.58	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	1.82	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	2.65	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	6.47	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	3.21	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	1.13	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.33	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
F	8.4	0.03	4828.	0.	0.	153.2	34.5	153.2	7.136E-06	6.560E-06	6.560E-06
G	0.4	0.01	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	0.69	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.49	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	1.91	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	2.29	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05
G	4.2	0.50	4828.	0.	0.	105.8	21.5	121.6	2.874E-05	2.743E-05	2.743E-05
G	5.3	0.08	4828.	0.	0.	105.8	21.5	110.5	2.536E-05	2.199E-05	2.199E-05

RUN DATE: 04/05/09

METEOROLOGICAL INSTRUMENTATION

WIND SENSORS HEIGHT: 9.1 meters

DELTA-T HEIGHTS: 76.2-9.1 meters

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

N SECTOR      BOUNDARY DISTANCE = 4828.0 METERS

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/O AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.012	0.017	0.708	0.717	2.209	4.117	4.697	6.991	7.488	7.492
0.00101	0.00143	0.05869	0.05942	0.18312	0.34117	0.38928	0.57940	0.62064	0.62093
2.327E-05	2.199E-05	1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06
9.316	9.399	12.053	12.826	19.294	22.500	24.158	25.292	25.568	28.056
0.77212	0.77899	0.99890	1.06304	1.59906	1.86478	2.00222	2.09614	2.11904	2.32520
8.732E-06	6.898E-06	6.560E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06
28.387	35.490	35.518	36.430	43.119	44.888	50.941	54.755	61.029	64.981
2.35269	2.94140	2.94369	3.01928	3.57363	3.72023	4.22189	4.53801	5.05800	5.38556
2.679E-06	2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	9.669E-07	8.932E-07
72.029	72.582	78.524	83.942	83.997	89.193	89.414	91.017	91.045	91.681
5.96969	6.01550	6.50800	6.95698	6.96156	7.39221	7.41053	7.54339	7.54568	7.59837
6.724E-07	5.604E-07	5.391E-07	4.563E-07	4.503E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07
92.814	92.869	93.781	93.836	94.445	95.218	95.467	95.661	95.688	96.241
7.69229	7.69687	7.77246	7.77704	7.82744	7.89158	7.91219	7.92823	7.93052	7.97633
1.721E-07	1.437E-07	1.313E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08
96.573	96.960	97.153	97.623	97.844	97.982	98.452	98.701	99.585	99.862
8.00382	8.03589	8.05192	8.09087	8.10919	8.12065	8.15959	8.18020	8.25351	8.27641
3.536E-08	1.628E-08								
99.945	100.000								
8.28329	8.28787								



X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.579  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 1.597  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 1.863  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 3.570  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 4.218  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 5.966  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 6.504  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 9)= 6.953

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
9	1	-8.57707	-12.89270	-1.01233
9	2	-10.33672	-15.37105	-1.99391
9	3	-11.09395	-17.02617	-2.76549
9	4	-11.26578	-17.37355	-2.93226
9	5	-12.08707	-16.29315	-2.33299
9	6	-12.26668	-18.04802	-3.34979
9	7	-12.83023	-19.56366	-4.32282
9	8	-13.01987	-20.82581	-5.15660
9	9	-13.19770	NUMXQ(K) = 9	
		6.079E-05	0.083	1.000
		4.323E-05	0.249	3.000
		3.645E-05	0.414	5.000
		2.510E-05	0.829	10.000
		1.852E-05	1.243	15.000
		1.461E-05	1.658	20.000
		1.127E-05	2.072	25.000
		9.000E-06	2.486	30.000
		7.400E-06	2.901	35.000
		6.221E-06	3.315	40.000
		5.381E-06	3.730	45.000
		4.803E-06	4.144	50.000
		4.168E-06	4.558	55.000
		3.624E-06	4.973	60.000
		3.179E-06	5.387	65.000
		2.810E-06	5.802	70.000
		2.452E-06	6.216	75.000
		2.109E-06	6.630	80.000
		3.415E-05	0.5	6.03

ANNUAL AVERAGE = 2.03E-07

K= 9      FIVEXQ(K) = 3.415E-05      FIVEPR(K) = 6.033

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNE SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						** CHI/Q VALUES (SEC/CUBIC METER)					
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	SIGMA-Y	SIGMA-Z	MEANDER-SY	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.1	0.03	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	1.6	0.09	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.03	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.35	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.38	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.60	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.63	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	1.04	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.41	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.13	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	1.6	0.03	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.09	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.41	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.73	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.66	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.85	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.76	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.19	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.06	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.6	0.06	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.22	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	1.29	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.14	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	1.20	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.88	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.95	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.22	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.09	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.50	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	1.04	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	2.15	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	7.10	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	6.47	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 124 of 163	
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D	5.2	5.99	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	4.92	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	6.97	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	2.40	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.44	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.01	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.10	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.24	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	2.84	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.56	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.43	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	5.02	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	4.67	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	4.48	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	1.55	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.03	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	0.95	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.30	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	3.22	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	2.71	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	1.20	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.13	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.03	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
G	0.4	0.02	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	1.36	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.33	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	1.07	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.22	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

NNE SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.665E-05	2.327E-05
0.024	0.032	1.389	1.401	2.726	3.799	4.745	4.966	4.973	7.276
0.00173	0.00233	0.10083	0.10174	0.19795	0.27583	0.34455	0.36058	0.36106	0.52828
1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06	8.732E-06	6.898E-06
10.494	11.598	14.311	15.510	17.750	17.877	18.381	21.221	21.252	27.815
0.76193	0.84210	1.03910	1.12615	1.28879	1.29795	1.33460	1.54076	1.54305	2.01952
6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.374E-06	2.216E-06
28.856	34.282	36.428	41.444	46.113	53.212	57.692	64.160	65.706	71.700
2.09511	2.48911	2.64487	3.00909	3.34811	3.86352	4.18880	4.65839	4.77063	5.20586
1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06	9.669E-07	8.932E-07	6.724E-07	5.604E-07	5.391E-07
76.622	76.685	83.657	83.878	86.276	86.308	87.601	88.737	88.768	89.967
5.56321	5.56779	6.07403	6.09007	6.26416	6.26645	6.36037	6.44283	6.44513	6.53217
4.563E-07	4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07
90.409	91.292	91.387	91.419	92.365	92.775	92.996	93.091	93.816	93.848
6.56424	6.62838	6.63525	6.63754	6.70626	6.73604	6.75208	6.75895	6.81164	6.81393
1.721E-07	1.437E-07	1.313E-07	1.108E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08
94.510	95.362	95.709	95.804	96.561	96.940	97.129	97.728	98.359	99.401
6.86203	6.92388	6.94908	6.95595	7.01093	7.03841	7.05216	7.09568	7.14149	7.21709
3.997E-08	3.536E-08	1.628E-08							
99.811	99.874	100.000							
7.24687	7.25145	7.26061							

X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.101  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.344  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.038  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.487  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.006  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.655  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 5.202  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.559  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE(10)= 6.070  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE(11)= 6.260

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
10	1	-8.57707	-12.81680	-1.02400
10	2	-9.65463	-14.65183	-1.61823
10	3	-10.27864	-15.92686	-2.09003
10	4	-11.09395	-17.65345	-2.83671
10	5	-12.08707	-16.36502	-2.18011
10	6	-12.26668	-17.54812	-2.80946
10	7	-12.83023	-18.75804	-3.52995
10	8	-13.01987	-21.86278	-5.43990
10	9	-13.19770	-23.56004	-6.50544
10	10	-13.48372	-35.10695	-13.96030
10	11	-13.70185	NUMXQ(K)= 11	
		7.077E-05	0.073	1.000
		4.373E-05	0.218	3.000
		3.313E-05	0.363	5.000
		2.004E-05	0.726	10.000
		1.446E-05	1.089	15.000
		1.054E-05	1.452	20.000
		8.183E-06	1.815	25.000
		6.610E-06	2.178	30.000
		5.524E-06	2.541	35.000
		4.869E-06	2.904	40.000
		4.246E-06	3.267	45.000
		3.715E-06	3.630	50.000
		3.284E-06	3.993	55.000
		2.929E-06	4.356	60.000
		2.620E-06	4.719	65.000
		2.309E-06	5.082	70.000
		1.965E-06	5.445	75.000
		1.613E-06	5.808	80.000
		1.245E-06	6.172	85.000

2.639E-05

0.5

6.89

ANNUAL AVERAGE = 1.73E-07

K= 10 FIVEXQ(K)= 2.639E-05 FIVEPR(K)= 6.886

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NE SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						** CHI/Q VALUES (SEC/CUBIC METER)					
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	SIGMA-Y	SIGMA-Z	MEANDER-SY	MEANDER	BLDG WAKE	USED
AT 10.0 METERS						CA=1459.SQ.METERS					
A	1.6	0.07	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.17	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.65	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.69	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.96	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.65	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.99	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.24	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.07	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	2.1	0.07	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.75	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.99	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	1.06	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.75	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.48	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.14	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.10	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.6	0.34	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.21	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	1.23	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.54	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	1.64	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.96	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.65	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.14	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.14	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.72	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	1.68	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	2.54	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	9.05	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	8.29	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	8.33	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	5.62	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06



D	8.2	5.24	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	1.34	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.93	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.47	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	3.26	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	4.22	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	7.40	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.96	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	4.52	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	1.85	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.51	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.21	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	1.58	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.26	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	1.75	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	1.47	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.10	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.07	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
G	0.4	0.03	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	1.71	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.93	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.21	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.03	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

NE SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.665E-05	2.327E-05
0.030	0.044	1.757	1.774	2.699	2.905	4.481	4.516	4.525	6.787
0.00202	0.00293	0.11746	0.11858	0.18043	0.19417	0.29954	0.30183	0.30245	0.45364
1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06
8.534	10.008	11.482	11.584	14.840	14.909	15.628	19.843	27.246	28.925
0.57047	0.66896	0.76746	0.77434	0.99195	0.99653	1.04464	1.32639	1.82118	1.93342
5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.374E-06	2.216E-06	1.855E-06
34.888	37.424	41.947	43.798	52.845	54.353	62.646	62.852	71.179	76.799
2.33200	2.50152	2.80389	2.92758	3.53233	3.63312	4.18746	4.20121	4.75784	5.13352
1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	6.724E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07
77.142	82.385	82.591	83.928	85.161	86.703	88.348	89.274	90.233	90.302
5.15642	5.50690	5.52064	5.60998	5.69244	5.79553	5.90548	5.96733	6.03147	6.03605
3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.108E-07
90.953	91.707	91.844	91.912	92.906	93.078	94.140	94.894	95.545	95.682
6.07957	6.12997	6.13913	6.14371	6.21014	6.22159	6.29260	6.34300	6.38652	6.39569
1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	3.536E-08	1.628E-08	
96.162	96.847	96.984	97.944	98.595	99.589	99.829	99.931	100.000	
6.42776	6.47357	6.48273	6.54687	6.59039	6.65682	6.67286	6.67973	6.68431	

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.117  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.299  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.767  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.330  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.801  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.184  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.754  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.130  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 5.503

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
11	1	-8.57707	-12.73798	-1.01346
11	2	-9.65463	-16.11759	-2.12429
11	3	-10.27864	-17.19110	-2.51485
11	4	-11.09395	-16.63585	-2.28583
11	5	-12.08707	-16.60370	-2.26968
11	6	-12.26668	-18.21169	-3.11118
11	7	-12.83023	-18.24765	-3.13197
11	8	-13.01987	-21.09208	-4.83607
11	9	-13.19770	-26.73759	-8.29449
11	10	-13.48372	NUMXQ(K)= 10	
		7.586E-05	0.067	1.000
		4.519E-05	0.201	3.000
		3.138E-05	0.334	5.000
		1.723E-05	0.668	10.000
		1.213E-05	1.003	15.000
		9.436E-06	1.337	20.000
		7.711E-06	1.671	25.000
		6.506E-06	2.005	30.000
		5.614E-06	2.340	35.000
		4.932E-06	2.674	40.000
		4.276E-06	3.008	45.000
		3.695E-06	3.342	50.000
		3.231E-06	3.676	55.000
		2.852E-06	4.011	60.000
		2.537E-06	4.345	65.000
		2.272E-06	4.679	70.000
		1.961E-06	5.013	75.000
		1.571E-06	5.347	80.000
		2.227E-05	0.5	7.48

ANNUAL AVERAGE = 1.67E-07

K= 11 FIVEXQ(K)= 2.227E-05 FIVEPR(K)= 7.480

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ENE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN	HT	EFF	PLUME	HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS												CA=1459.SQ.METERS		
A	1.6	0.23	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07			
A	2.1	0.15	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07			
A	3.1	0.39	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07			
A	4.1	0.35	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08			
A	5.2	0.89	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08			
A	6.2	0.58	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08			
A	8.2	0.96	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08			
A	10.3	0.12	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08			
A	25.2	0.04	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08			
B	1.6	0.04	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07			
B	2.1	0.19	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07			
B	3.1	0.23	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07			
B	4.1	0.50	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07			
B	5.2	0.96	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07			
B	6.2	0.50	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07			
B	8.2	0.39	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07			
B	10.3	0.23	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08			
B	25.2	0.08	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08			
C	1.6	0.08	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06			
C	2.1	0.31	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06			
C	3.1	0.73	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07			
C	4.1	0.85	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07			
C	5.2	1.27	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07			
C	6.2	0.50	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07			
C	8.2	0.89	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07			
C	10.3	0.27	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07			
C	25.2	0.15	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07			
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05			
D	1.1	1.12	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06			
D	1.6	1.93	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06			
D	2.1	2.89	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06			
D	3.1	8.18	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06			
D	4.1	8.53	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06			
D	5.2	8.76	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06			

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 133 of 163	
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D	6.2	5.94	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	7.37	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	3.13	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	1.70	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.70	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.89	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	4.17	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.95	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.67	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	3.97	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	1.20	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.81	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.08	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
F	0.4	0.02	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	2.08	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.66	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	1.93	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	0.62	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.23	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.08	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
F	6.3	0.04	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
G	0.4	0.04	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	2.01	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.16	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.15	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.08	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05



X/Q PERCENTILES  
 (BASED ON THE UPPER ENVELOPE OF THE  
 ORDERED X/Q-FREQUENCY VALUES, AND AS  
 PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 2)=	0.122
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 3)=	0.325
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 4)=	0.703
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 5)=	1.657
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 6)=	2.108
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 7)=	2.516
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 8)=	4.150
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE ( 9)=	4.503
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES.	XSAVE (10)=	4.945

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
12	1	-8.57707	-12.71690	-1.01056
12	2	-9.65463	-15.78453	-2.02288
12	3	-10.27864	-17.57358	-2.68018
12	4	-10.99177	-17.72768	-2.74294
12	5	-11.88432	-16.27337	-2.06027
12	6	-12.08707	-16.97881	-2.40745
12	7	-12.26668	-18.85408	-3.36553
12	8	-13.01987	-21.04370	-4.62864
12	9	-13.19770	-24.00276	-6.37429
12	10	-13.48372	NUMXQ(K) = 10	
		7.944E-05	0.059	1.000
		5.078E-05	0.178	3.000
		3.650E-05	0.297	5.000
		1.981E-05	0.594	10.000
		1.331E-05	0.890	15.000
		9.890E-06	1.187	20.000
		7.792E-06	1.484	25.000
		6.503E-06	1.781	30.000
		5.708E-06	2.078	35.000
		4.999E-06	2.374	40.000
		4.320E-06	2.671	45.000
		3.701E-06	2.968	50.000
		3.210E-06	3.265	55.000
		2.813E-06	3.561	60.000
		2.487E-06	3.858	65.000
		2.214E-06	4.155	70.000
		1.905E-06	4.452	75.000
		1.582E-06	4.749	80.000
		2.326E-05	0.5	8.42

ANNUAL AVERAGE = 1.58E-07

K= 12      FIVEXQ(K) = 2.326E-05      FIVEPR(K) = 8.424



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE E SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT						SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS									CA=1459.SQ.METERS		
A	1.6	0.03	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.11	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.27	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.38	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.49	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.74	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.71	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.27	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.03	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	1.6	0.03	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.11	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.30	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.44	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.76	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.57	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.52	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.27	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
C	1.6	0.08	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.14	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.68	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.09	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	0.74	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.74	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.90	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.27	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.08	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.71	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	1.25	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	2.24	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	6.57	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	7.77	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	8.94	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	6.90	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 138 of 163	
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D	8.2	10.99	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	3.87	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	2.67	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.69	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.84	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	2.67	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.84	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	5.15	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	4.20	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	1.39	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.04	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.22	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
F	0.4	0.02	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	1.91	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	3.08	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	1.72	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	1.01	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.08	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
F	5.3	0.05	4828.	0.	0.	153.2	34.5	158.4	1.100E-05	1.045E-05	1.045E-05
G	0.4	0.04	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	1.99	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.06	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.25	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.05	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

E SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.665E-05	2.327E-05
0.035	0.052	2.042	2.061	3.125	3.370	5.279	5.334	5.343	8.425
0.00294	0.00433	0.17156	0.17316	0.26250	0.28311	0.44346	0.44804	0.44881	0.70766
1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06
10.143	11.834	12.843	12.924	15.761	15.815	16.524	19.197	26.042	27.296
0.85197	0.99400	1.07875	1.08562	1.32386	1.32844	1.38799	1.61248	2.18745	2.29282
5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.374E-06	2.216E-06	1.855E-06
32.450	34.686	38.886	40.277	46.849	47.886	55.658	55.876	64.821	71.720
2.72576	2.91359	3.26636	3.38318	3.93524	4.02229	4.67513	4.69346	5.44480	6.02435
1.756E-06	1.393E-06	1.336E-06	1.120E-06	8.932E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07	4.503E-07
71.802	82.792	82.928	86.801	87.483	88.574	88.601	89.337	92.010	92.746
6.03122	6.95437	6.96582	7.29110	7.34837	7.43999	7.44228	7.50413	7.72862	7.79047
4.265E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07
92.855	93.755	94.055	94.328	94.355	94.791	94.900	95.664	96.237	96.509
7.79963	7.87522	7.90042	7.92333	7.92562	7.96227	7.97143	8.03557	8.08368	8.10658
1.108E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	1.628E-08	
96.591	97.109	97.491	97.764	98.255	98.991	99.700	99.973	100.000	
8.11345	8.15698	8.18905	8.21195	8.25319	8.31503	8.37459	8.39750	8.39979	

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.443  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.707  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 0.993  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.723  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.263  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 5.441  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 6.020  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 6.951

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
13	1	-8.57707	-12.54565	-0.98786
13	2	-9.65463	-15.56285	-2.01884
13	3	-10.27864	-16.51121	-2.38116
13	4	-10.66838	-17.03023	-2.59268
13	5	-10.99177	-17.27662	-2.69846
13	6	-12.08707	-16.41974	-2.25290
13	7	-12.26668	-18.05416	-3.13952
13	8	-13.01987	-18.67047	-3.52387
13	9	-13.19770	-19.23569	-3.88782
13	10	-13.48372	NUMXQ(K) = 10	
		7.933E-05	0.084	1.000
		5.016E-05	0.252	3.000
		3.567E-05	0.420	5.000
		1.980E-05	0.840	10.000
		1.320E-05	1.260	15.000
		9.717E-06	1.680	20.000
		7.595E-06	2.100	25.000
		6.170E-06	2.520	30.000
		5.228E-06	2.940	35.000
		4.522E-06	3.360	40.000
		3.823E-06	3.780	45.000
		3.279E-06	4.200	50.000
		2.846E-06	4.620	55.000
		2.495E-06	5.040	60.000
		2.205E-06	5.460	65.000
		1.936E-06	5.880	70.000
		1.698E-06	6.300	75.000
		1.493E-06	6.720	80.000
		3.115E-05	0.5	5.95

ANNUAL AVERAGE = 2.12E-07

K= 13 FIVEXQ(K)= 3.115E-05 FIVEPR(K)= 5.953

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ESE SECTOR.

CLASS	METER/SEC	PERCENT	METERS	TERRAIN HT METERS	EFF PLUME HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	** CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
AT 10.0 METERS												
A	1.6	0.03	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07	
A	2.1	0.08	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07	
A	3.1	0.44	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07	
A	4.1	0.83	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08	
A	5.2	0.89	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08	
A	6.2	0.53	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08	
A	8.2	1.27	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08	
A	10.3	0.11	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08	
B	1.1	0.03	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07	
B	1.6	0.03	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07	
B	2.1	0.03	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07	
B	3.1	0.19	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07	
B	4.1	0.55	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07	
B	5.2	0.75	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07	
B	6.2	0.89	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07	
B	8.2	0.72	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07	
B	10.3	0.25	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08	
B	25.2	0.06	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08	
C	1.6	0.08	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06	
C	2.1	0.14	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06	
C	3.1	0.80	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07	
C	4.1	1.11	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07	
C	5.2	1.25	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07	
C	6.2	1.13	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07	
C	8.2	1.19	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07	
C	10.3	0.47	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07	
C	25.2	0.06	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07	
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05	
D	1.1	0.89	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06	
D	1.6	1.77	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06	
D	2.1	2.96	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06	
D	3.1	8.63	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06	
D	4.1	9.93	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06	
D	5.2	10.27	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06	

CA=1459.SQ.METERS

D	6.2	8.69	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	8.80	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	3.76	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.89	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.80	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.85	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	3.21	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	6.03	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	3.54	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	1.80	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	0.55	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.22	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.03	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.11	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.02	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	2.46	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.16	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	0.69	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	0.50	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
F	4.2	0.03	4828.	0.	0.	153.2	34.5	169.8	1.280E-05	1.304E-05	1.280E-05
G	0.4	0.05	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	2.60	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	0.64	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.17	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05
G	3.2	0.03	4828.	0.	0.	105.8	21.5	143.2	3.242E-05	3.643E-05	3.242E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

ESE SECTOR      BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.665E-05	2.327E-05
0.046	0.067	2.668	2.689	3.325	3.491	5.954	5.982	5.993	8.152
0.00379	0.00556	0.22088	0.22257	0.27525	0.28900	0.49287	0.49516	0.49611	0.67478
1.844E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06	5.632E-06
8.844	10.643	11.141	11.168	14.019	14.904	18.114	24.147	25.918	29.460
0.73205	0.88094	0.92217	0.92446	1.16041	1.23371	1.49943	1.99880	2.14540	2.43861
4.717E-06	4.706E-06	3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.374E-06	2.216E-06	1.855E-06	1.756E-06
32.421	34.220	34.774	43.408	43.629	53.564	53.592	63.858	72.548	72.631
2.68371	2.83261	2.87842	3.59312	3.61144	4.43380	4.43609	5.28593	6.00521	6.01208
1.393E-06	1.336E-06	1.120E-06	9.669E-07	8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07
81.431	81.569	85.333	85.444	86.246	86.274	87.381	87.409	88.654	89.539
6.74052	6.75198	7.06351	7.07267	7.13910	7.14139	7.23302	7.23531	7.33839	7.41169
4.503E-07	4.265E-07	3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07
90.674	90.702	91.892	92.085	92.556	92.584	93.137	93.220	93.967	94.853
7.50561	7.50790	7.60640	7.62244	7.66138	7.66367	7.70948	7.71635	7.77820	7.85151
1.313E-07	1.108E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	3.536E-08
95.296	95.351	96.070	96.901	97.150	98.035	98.561	99.834	99.945	100.000
7.88816	7.89274	7.95230	8.02102	8.04163	8.11493	8.15846	8.26383	8.27299	8.27757

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.492  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.880  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.436  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 5.282  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 6.001  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.737  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 7.060

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
14	1	-8.57707	-12.41765	-0.97049
14	2	-9.65463	-16.33760	-2.34734
14	3	-10.27864	-19.16112	-3.44122
14	4	-10.99177	-17.44459	-2.71816
14	5	-12.08707	-17.29661	-2.64308
14	6	-13.01987	-17.55618	-2.80350
14	7	-13.19770	-20.73894	-4.85074
14	8	-13.48372	-26.89186	-8.96449
14	9	-13.70185	NUMXQ(K)= 9	
		8.573E-05	0.083	1.000
		5.873E-05	0.248	3.000
		3.953E-05	0.414	5.000
		1.822E-05	0.828	10.000
		1.184E-05	1.242	15.000
		8.704E-06	1.656	20.000
		6.795E-06	2.069	25.000
		5.518E-06	2.483	30.000
		4.626E-06	2.897	35.000
		3.956E-06	3.311	40.000
		3.435E-06	3.725	45.000
		3.020E-06	4.139	50.000
		2.681E-06	4.553	55.000
		2.401E-06	4.967	60.000
		2.162E-06	5.380	65.000
		1.951E-06	5.794	70.000
		1.710E-06	6.208	75.000
		1.457E-06	6.622	80.000
		1.141E-06	7.036	85.000
		3.378E-05	0.5	6.04

ANNUAL AVERAGE = 2.14E-07

K= 14 FIVEXQ(K)= 3.378E-05 FIVEPR(K)= 6.040



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SE SECTOR.

CLASS	METER/SEC	PERCENT	METERS	TERRAIN HT METERS	EFF PLUME HT METERS	SIGMA-Y METERS	SIGMA-Z METERS	MEANDER-SY METERS	** CHI/Q VALUES (SEC/CUBIC METER)	MEANDER	BLDG WAKE	USED
									CA=1459.SQ.METERS			
AT 10.0 METERS												
A	1.1	0.03	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07	
A	1.6	0.06	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07	
A	2.1	0.09	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07	
A	3.1	0.23	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07	
A	4.1	0.82	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08	
A	5.2	1.43	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08	
A	6.2	1.32	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08	
A	8.2	1.00	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08	
A	10.3	0.06	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08	
B	1.1	0.03	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07	
B	1.6	0.06	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07	
B	2.1	0.09	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07	
B	3.1	0.53	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07	
B	4.1	1.00	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07	
B	5.2	1.23	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07	
B	6.2	0.79	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07	
B	8.2	0.67	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07	
B	10.3	0.09	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08	
C	1.6	0.12	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06	
C	2.1	0.12	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06	
C	3.1	1.29	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07	
C	4.1	1.70	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07	
C	5.2	1.38	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07	
C	6.2	1.29	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07	
C	8.2	0.97	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07	
C	10.3	0.15	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07	
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05	
D	1.1	0.76	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06	
D	1.6	1.70	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06	
D	2.1	2.87	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06	
D	3.1	10.66	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06	
D	4.1	11.36	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06	
D	5.2	8.75	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06	
D	6.2	6.00	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06	

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 146 of 163	
D	8.2	4.16	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06	
D	10.3	0.64	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06	
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05	
E	1.1	2.14	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05	
E	1.6	3.07	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05	
E	2.1	5.42	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06	
E	3.2	5.62	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06	
E	4.2	3.81	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06	
E	5.3	1.29	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06	
E	6.3	0.32	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06	
E	8.4	0.09	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06	
F	0.4	0.02	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04	
F	1.1	2.78	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05	
F	1.6	3.69	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05	
F	2.1	1.93	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05	
F	3.2	0.44	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05	
G	0.4	0.06	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04	
G	1.1	3.22	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05	
G	1.6	2.28	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05	
G	2.1	0.38	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05	

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

SE SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	2.665E-05	2.327E-05	1.844E-05
0.057	0.081	3.301	3.325	5.609	5.989	8.770	8.780	12.469	14.401
0.00443	0.00632	0.25830	0.26019	0.43886	0.46864	0.68626	0.68703	0.97565	1.12684
1.684E-05	1.520E-05	1.140E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06
16.538	16.977	20.051	20.812	26.228	31.849	33.546	37.352	40.221	41.509
1.29406	1.32842	1.56894	1.62850	2.05228	2.49209	2.62495	2.92274	3.14723	3.24802
3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06
41.831	52.487	52.575	63.934	72.687	78.688	78.805	82.962	83.079	83.723
3.27321	4.10703	4.11390	5.00268	5.68760	6.15719	6.16635	6.49163	6.50079	6.55119
8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07
85.011	85.041	86.739	86.797	88.173	89.461	89.549	89.578	90.544	91.071
6.65198	6.65427	6.78713	6.79171	6.89937	7.00016	7.00704	7.00933	7.08492	7.12615
2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.080E-07	9.881E-08	8.681E-08
91.218	91.276	92.271	92.359	93.589	94.379	94.613	95.287	96.106	96.194
7.13761	7.14219	7.22007	7.22694	7.32315	7.38500	7.40332	7.45601	7.52015	7.52702
7.923E-08	6.617E-08	4.971E-08	3.997E-08						
97.629	98.946	99.941	100.000						
7.63927	7.74235	7.82023	7.82481						

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.685  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.293  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.920  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.999  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.684  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.153  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 6.488  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 6.996

K	I	XQSAVE(K,I)	XQINT(K,I)	XQSLOP(K,I)
15	1	-8.57707	-12.33881	-0.95971
15	2	-9.65463	-14.91057	-1.87923
15	3	-10.27864	-17.71504	-3.01704
15	4	-10.99177	-18.26170	-3.26235
15	5	-12.08707	-17.76460	-2.99971
15	6	-12.83023	-17.77685	-3.00715
15	7	-13.01987	-20.07746	-4.46150
15	8	-13.19770	-29.55655	-10.60866
15	9	-13.48372	-57.36961	-28.96629
15	10	-14.61346	NUMXQ(K) = 10	
		9.110E-05	0.078	1.000
		6.605E-05	0.235	3.000
		4.958E-05	0.391	5.000
		2.978E-05	0.782	10.000
		1.886E-05	1.174	15.000
		1.320E-05	1.565	20.000
		9.826E-06	1.956	25.000
		7.666E-06	2.347	30.000
		6.179E-06	2.739	35.000
		5.143E-06	3.130	40.000
		4.389E-06	3.521	45.000
		3.798E-06	3.912	50.000
		3.323E-06	4.304	55.000
		2.936E-06	4.695	60.000
		2.615E-06	5.086	65.000
		2.344E-06	5.477	70.000
		2.066E-06	5.869	75.000
		1.697E-06	6.260	80.000
		9.708E-07	6.651	85.000
		4.236E-05	0.5	6.39

ANNUAL AVERAGE = 2.48E-07

K= 15 FIVEXQ(K)= 4.236E-05 FIVEPR(K)= 6.390

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSE SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS			CA=1459.SQ.METERS								
A	1.1	0.04	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	2.1	0.04	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.53	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.73	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.73	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.81	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.57	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.04	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
B	1.6	0.16	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.20	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.65	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.65	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.89	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.65	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.36	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.04	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
C	1.1	0.04	4828.	0.	0.	443.4	256.4	443.4	2.603E-06	2.592E-06	2.592E-06
C	1.6	0.16	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.41	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	1.01	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.42	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	1.38	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.65	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.57	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	25.2	0.04	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	373.8	2.665E-05	3.137E-05	2.665E-05
D	1.1	0.61	4828.	0.	0.	312.2	87.3	373.8	9.072E-06	1.068E-05	9.072E-06
D	1.6	2.64	4828.	0.	0.	312.2	87.3	373.8	6.144E-06	7.232E-06	6.144E-06
D	2.1	3.85	4828.	0.	0.	312.2	87.3	370.5	4.717E-06	5.504E-06	4.717E-06
D	3.1	12.29	4828.	0.	0.	312.2	87.3	343.6	3.400E-06	3.680E-06	3.400E-06
D	4.1	11.64	4828.	0.	0.	312.2	87.3	328.4	2.679E-06	2.770E-06	2.679E-06
D	5.2	11.03	4828.	0.	0.	312.2	87.3	318.2	2.216E-06	2.221E-06	2.216E-06
D	6.2	5.15	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	4.18	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06

D	10.3	0.69	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
E	0.4	0.02	4828.	0.	0.	222.0	55.4	309.6	4.947E-05	6.647E-05	4.947E-05
E	1.1	1.78	4828.	0.	0.	222.0	55.4	309.6	1.684E-05	2.263E-05	1.684E-05
E	1.6	2.31	4828.	0.	0.	222.0	55.4	309.6	1.140E-05	1.532E-05	1.140E-05
E	2.1	3.53	4828.	0.	0.	222.0	55.4	301.1	8.921E-06	1.166E-05	8.921E-06
E	3.2	8.07	4828.	0.	0.	222.0	55.4	260.4	6.898E-06	7.797E-06	6.898E-06
E	4.2	4.01	4828.	0.	0.	222.0	55.4	240.1	5.632E-06	5.869E-06	5.632E-06
E	5.3	1.22	4828.	0.	0.	222.0	55.4	227.8	4.759E-06	4.706E-06	4.706E-06
E	6.3	0.36	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	0.20	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
F	0.4	0.01	4828.	0.	0.	153.2	34.5	243.9	1.009E-04	1.477E-04	1.009E-04
F	1.1	1.58	4828.	0.	0.	153.2	34.5	243.9	3.436E-05	5.027E-05	3.436E-05
F	1.6	2.60	4828.	0.	0.	153.2	34.5	243.9	2.327E-05	3.405E-05	2.327E-05
F	2.1	2.60	4828.	0.	0.	153.2	34.5	234.2	1.844E-05	2.591E-05	1.844E-05
F	3.2	1.70	4828.	0.	0.	153.2	34.5	189.9	1.520E-05	1.732E-05	1.520E-05
G	0.4	0.05	4828.	0.	0.	105.8	21.5	210.1	1.884E-04	3.106E-04	1.884E-04
G	1.1	2.76	4828.	0.	0.	105.8	21.5	210.1	6.413E-05	1.057E-04	6.413E-05
G	1.6	1.95	4828.	0.	0.	105.8	21.5	210.1	4.343E-05	7.161E-05	4.343E-05
G	2.1	0.41	4828.	0.	0.	105.8	21.5	197.3	3.520E-05	5.449E-05	3.520E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SSE SECTOR BOUNDARY DISTANCE = 4828.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	2.665E-05	2.327E-05	1.844E-05
0.049	0.062	2.820	2.840	4.786	5.191	6.773	6.781	9.376	11.971
0.00274	0.00352	0.15928	0.16042	0.27038	0.29328	0.38262	0.38306	0.52967	0.67627
1.684E-05	1.520E-05	1.140E-05	9.072E-06	8.921E-06	6.898E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06
13.755	15.458	17.769	18.377	21.905	29.974	32.610	36.624	40.476	41.692
0.77706	0.87327	1.00384	1.03820	1.23749	1.69334	1.84223	2.06901	2.28663	2.35535
3.930E-06	3.400E-06	2.953E-06	2.679E-06	2.592E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06
42.057	54.343	54.546	66.183	66.224	77.253	82.402	82.564	86.741	87.146
2.37596	3.07004	3.08149	3.73892	3.74121	4.36428	4.65520	4.66436	4.90030	4.92321
1.120E-06	8.932E-07	6.724E-07	5.604E-07	5.391E-07	4.503E-07	4.265E-07	3.810E-07	3.383E-07	2.851E-07
87.836	88.849	90.269	90.431	91.809	92.458	92.661	92.701	93.269	93.918
4.96215	5.01942	5.09959	5.10875	5.18664	5.22329	5.23474	5.23703	5.26910	5.30575
2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.108E-07	1.080E-07	9.881E-08	8.681E-08	7.923E-08
94.567	94.607	95.499	96.148	96.675	96.716	97.081	97.810	97.851	98.581
5.34240	5.34470	5.39509	5.43174	5.46152	5.46381	5.48443	5.52566	5.52795	5.56918
6.617E-08	4.971E-08	3.997E-08							
99.392	99.959	100.000							
5.61500	5.64707	5.64936							

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.382  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.872  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.067  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.361  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.652  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.897

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
16	1	-8.57707	-12.58535	-0.99361
16	2	-9.65463	-16.17842	-2.21179
16	3	-10.27864	-17.77187	-2.80916
16	4	-11.09395	-18.09831	-2.94648
16	5	-12.08707	-17.85621	-2.82781
16	6	-13.01987	-22.94043	-5.80057
16	7	-13.19770	-32.68114	-11.59994
16	8	-13.48372	NUMXQ(K)= 8	
		8.698E-05	0.056	1.000
		6.146E-05	0.169	3.000
		4.290E-05	0.282	5.000
		2.360E-05	0.565	10.000
		1.568E-05	0.847	15.000
		1.144E-05	1.130	20.000
		8.870E-06	1.412	25.000
		7.163E-06	1.695	30.000
		5.952E-06	1.977	35.000
		5.074E-06	2.260	40.000
		4.405E-06	2.542	45.000
		3.872E-06	2.825	50.000
		3.439E-06	3.107	55.000
		3.081E-06	3.390	60.000
		2.780E-06	3.672	65.000
		2.524E-06	3.955	70.000
		2.305E-06	4.237	75.000
		2.013E-06	4.519	80.000
		1.561E-06	4.802	85.000
		2.659E-05	0.5	8.85

ANNUAL AVERAGE = 1.64E-07

K= 16 FIVEXQ(K)= 2.659E-05 FIVEPR(K)= 8.851



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ALL SECTOR.

STABILITY	WINDSPEED	FREQUENCY	DISTANCE	TERRAIN HT	EFF PLUME HT	SIGMA-Y	SIGMA-Z	MEANDER-SY	** CHI/Q VALUES (SEC/CUBIC METER)		
CLASS	METER/SEC	PERCENT	METERS	METERS	METERS	METERS	METERS	METERS	MEANDER	BLDG WAKE	USED
AT 10.0 METERS			CA=1459.SQ.METERS								
A	1.1	0.02	4828.	0.	0.	776.3	1000.0	776.3	3.812E-07	3.810E-07	3.810E-07
A	1.6	0.05	4828.	0.	0.	776.3	1000.0	776.3	2.582E-07	2.580E-07	2.580E-07
A	2.1	0.08	4828.	0.	0.	776.3	1000.0	776.3	1.964E-07	1.963E-07	1.963E-07
A	3.1	0.41	4828.	0.	0.	776.3	1000.0	776.3	1.313E-07	1.313E-07	1.313E-07
A	4.1	0.66	4828.	0.	0.	776.3	1000.0	776.3	9.887E-08	9.881E-08	9.881E-08
A	5.2	0.74	4828.	0.	0.	776.3	1000.0	776.3	7.927E-08	7.923E-08	7.923E-08
A	6.2	0.55	4828.	0.	0.	776.3	1000.0	776.3	6.621E-08	6.617E-08	6.617E-08
A	8.2	0.73	4828.	0.	0.	776.3	1000.0	776.3	4.974E-08	4.971E-08	4.971E-08
A	10.3	0.14	4828.	0.	0.	776.3	1000.0	776.3	3.999E-08	3.997E-08	3.997E-08
A	25.2	0.03	4828.	0.	0.	776.3	1000.0	776.3	1.629E-08	1.628E-08	1.628E-08
B	1.1	0.02	4828.	0.	0.	583.8	611.7	583.8	8.286E-07	8.275E-07	8.275E-07
B	1.6	0.06	4828.	0.	0.	583.8	611.7	583.8	5.611E-07	5.604E-07	5.604E-07
B	2.1	0.11	4828.	0.	0.	583.8	611.7	583.8	4.270E-07	4.265E-07	4.265E-07
B	3.1	0.44	4828.	0.	0.	583.8	611.7	583.8	2.855E-07	2.851E-07	2.851E-07
B	4.1	0.68	4828.	0.	0.	583.8	611.7	583.8	2.149E-07	2.146E-07	2.146E-07
B	5.2	0.79	4828.	0.	0.	583.8	611.7	583.8	1.723E-07	1.721E-07	1.721E-07
B	6.2	0.55	4828.	0.	0.	583.8	611.7	583.8	1.439E-07	1.437E-07	1.437E-07
B	8.2	0.45	4828.	0.	0.	583.8	611.7	583.8	1.081E-07	1.080E-07	1.080E-07
B	10.3	0.14	4828.	0.	0.	583.8	611.7	583.8	8.693E-08	8.681E-08	8.681E-08
B	25.2	0.04	4828.	0.	0.	583.8	611.7	583.8	3.540E-08	3.536E-08	3.536E-08
C	1.1	0.01	4828.	0.	0.	443.4	256.4	443.4	2.603E-06	2.592E-06	2.592E-06
C	1.6	0.10	4828.	0.	0.	443.4	256.4	443.4	1.763E-06	1.756E-06	1.756E-06
C	2.1	0.29	4828.	0.	0.	443.4	256.4	443.4	1.341E-06	1.336E-06	1.336E-06
C	3.1	0.96	4828.	0.	0.	443.4	256.4	443.4	8.969E-07	8.932E-07	8.932E-07
C	4.1	1.13	4828.	0.	0.	443.4	256.4	443.4	6.751E-07	6.724E-07	6.724E-07
C	5.2	1.06	4828.	0.	0.	443.4	256.4	443.4	5.413E-07	5.391E-07	5.391E-07
C	6.2	0.71	4828.	0.	0.	443.4	256.4	443.4	4.521E-07	4.503E-07	4.503E-07
C	8.2	0.63	4828.	0.	0.	443.4	256.4	443.4	3.396E-07	3.383E-07	3.383E-07
C	10.3	0.17	4828.	0.	0.	443.4	256.4	443.4	2.731E-07	2.720E-07	2.720E-07
C	25.2	0.05	4828.	0.	0.	443.4	256.4	443.4	1.112E-07	1.108E-07	1.108E-07
D	0.4	0.01	4828.	0.	0.	312.2	87.3	312.2	3.190E-05	3.137E-05	3.137E-05
D	1.1	0.71	4828.	0.	0.	312.2	87.3	312.2	1.086E-05	1.068E-05	1.068E-05
D	1.6	1.71	4828.	0.	0.	312.2	87.3	312.2	7.356E-06	7.232E-06	7.232E-06
D	2.1	2.89	4828.	0.	0.	312.2	87.3	312.2	5.597E-06	5.504E-06	5.504E-06

CALCULATION NO. BYR04-050, BRW-04-0044-M				MINOR REV. NO. 1B		APPENDIX BB-5					PAGE NO. 154 of 163	
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D	3.1	8.55	4828.	0.	0.	312.2	87.3	312.2	3.743E-06	3.680E-06	3.680E-06
D	4.1	8.69	4828.	0.	0.	312.2	87.3	312.2	2.817E-06	2.770E-06	2.770E-06
D	5.2	8.72	4828.	0.	0.	312.2	87.3	312.2	2.259E-06	2.221E-06	2.221E-06
D	6.2	5.97	4828.	0.	0.	312.2	87.3	312.2	1.886E-06	1.855E-06	1.855E-06
D	8.2	6.76	4828.	0.	0.	312.2	87.3	312.2	1.417E-06	1.393E-06	1.393E-06
D	10.3	2.02	4828.	0.	0.	312.2	87.3	312.2	1.139E-06	1.120E-06	1.120E-06
D	25.2	0.65	4828.	0.	0.	312.2	87.3	312.2	4.641E-07	4.563E-07	4.563E-07
E	0.4	0.02	4828.	0.	0.	222.0	55.4	222.0	6.898E-05	6.647E-05	6.647E-05
E	1.1	1.42	4828.	0.	0.	222.0	55.4	222.0	2.348E-05	2.263E-05	2.263E-05
E	1.6	2.42	4828.	0.	0.	222.0	55.4	222.0	1.590E-05	1.532E-05	1.532E-05
E	2.1	3.22	4828.	0.	0.	222.0	55.4	222.0	1.210E-05	1.166E-05	1.166E-05
E	3.2	7.17	4828.	0.	0.	222.0	55.4	222.0	8.091E-06	7.797E-06	7.797E-06
E	4.2	5.47	4828.	0.	0.	222.0	55.4	222.0	6.091E-06	5.869E-06	5.869E-06
E	5.3	3.56	4828.	0.	0.	222.0	55.4	222.0	4.883E-06	4.706E-06	4.706E-06
E	6.3	1.88	4828.	0.	0.	222.0	55.4	222.0	4.079E-06	3.930E-06	3.930E-06
E	8.4	1.45	4828.	0.	0.	222.0	55.4	222.0	3.064E-06	2.953E-06	2.953E-06
E	10.5	0.30	4828.	0.	0.	222.0	55.4	222.0	2.464E-06	2.374E-06	2.374E-06
E	25.8	0.04	4828.	0.	0.	222.0	55.4	222.0	1.003E-06	9.669E-07	9.669E-07
F	0.4	0.01	4828.	0.	0.	153.2	34.5	153.2	1.606E-04	1.477E-04	1.477E-04
F	1.1	1.32	4828.	0.	0.	153.2	34.5	153.2	5.469E-05	5.027E-05	5.027E-05
F	1.6	2.01	4828.	0.	0.	153.2	34.5	153.2	3.704E-05	3.405E-05	3.405E-05
F	2.1	1.92	4828.	0.	0.	153.2	34.5	153.2	2.818E-05	2.591E-05	2.591E-05
F	3.2	3.13	4828.	0.	0.	153.2	34.5	153.2	1.884E-05	1.732E-05	1.732E-05
F	4.2	1.47	4828.	0.	0.	153.2	34.5	153.2	1.419E-05	1.304E-05	1.304E-05
F	5.3	0.46	4828.	0.	0.	153.2	34.5	153.2	1.137E-05	1.045E-05	1.045E-05
F	6.3	0.07	4828.	0.	0.	153.2	34.5	153.2	9.499E-06	8.732E-06	8.732E-06
F	8.4	0.01	4828.	0.	0.	153.2	34.5	153.2	7.136E-06	6.560E-06	6.560E-06
G	0.4	0.03	4828.	0.	0.	105.8	21.5	105.8	3.741E-04	3.106E-04	3.106E-04
G	1.1	1.43	4828.	0.	0.	105.8	21.5	105.8	1.274E-04	1.057E-04	1.057E-04
G	1.6	1.07	4828.	0.	0.	105.8	21.5	105.8	8.626E-05	7.161E-05	7.161E-05
G	2.1	0.60	4828.	0.	0.	105.8	21.5	105.8	6.564E-05	5.449E-05	5.449E-05
G	3.2	0.72	4828.	0.	0.	105.8	21.5	105.8	4.389E-05	3.643E-05	3.643E-05
G	4.2	0.28	4828.	0.	0.	105.8	21.5	105.8	3.304E-05	2.743E-05	2.743E-05
G	5.3	0.06	4828.	0.	0.	105.8	21.5	105.8	2.649E-05	2.199E-05	2.199E-05
G	6.3	0.00	4828.	0.	0.	105.8	21.5	105.8	2.212E-05	1.837E-05	1.837E-05

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

DIRECTION-INDEPENDENT (S.R.P 2.3.4) MODEL.

MINIMUM BOUNDARY DISTANCE = 4828.0 METERS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

3.106E-04	1.477E-04	1.057E-04	7.161E-05	6.647E-05	5.449E-05	5.027E-05	3.643E-05	3.405E-05	3.137E-05
0.025	0.037	1.468	2.543	2.559	3.154	4.474	5.193	7.200	7.209
0.02520	0.03665	1.46833	2.54266	2.55870	3.15428	4.47371	5.19299	7.19963	7.20880
2.743E-05	2.591E-05	2.263E-05	2.199E-05	1.837E-05	1.732E-05	1.532E-05	1.304E-05	1.166E-05	1.068E-05
7.486	9.410	10.828	10.890	10.895	14.021	16.438	17.904	21.122	21.833
7.48597	9.41015	10.82808	10.88993	10.89452	14.02131	16.43798	17.90402	21.12244	21.83255
1.045E-05	8.732E-06	7.797E-06	7.232E-06	6.560E-06	5.869E-06	5.504E-06	4.706E-06	3.930E-06	3.680E-06
22.295	22.362	29.534	31.245	31.259	36.729	39.622	43.184	45.065	53.614
22.29527	22.36170	29.53385	31.24499	31.25874	36.72890	39.62204	43.18406	45.06472	53.61356
2.953E-06	2.770E-06	2.592E-06	2.374E-06	2.221E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06
55.064	63.757	63.768	64.066	72.784	78.759	78.859	85.617	85.903	87.926
55.06357	63.75673	63.76818	64.06597	72.78432	78.75845	78.85924	85.61677	85.90310	87.92578
9.669E-07	8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.810E-07
87.970	88.925	88.945	90.075	90.139	91.202	91.848	92.553	92.659	92.681
87.96931	88.92452	88.94514	90.07444	90.13858	91.20146	91.84743	92.55297	92.65833	92.68124
3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.108E-07
93.314	93.758	93.925	93.978	94.654	94.736	95.522	96.069	96.475	96.530
93.31347	93.75787	93.92509	93.97778	94.65353	94.73600	95.52171	96.06918	96.47463	96.52961
1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	3.536E-08	1.628E-08	
96.981	97.636	97.781	98.516	99.063	99.794	99.938	99.975	100.000	
96.98087	97.63601	97.78032	98.51563	99.06311	99.79383	99.93814	99.97479	99.99999	

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 4.470  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 7.196  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 16.439

1.195E-04	1.000	1.000
6.670E-05	3.000	3.000
4.605E-05	5.000	5.000
2.533E-05	10.000	10.000
1.691E-05	15.000	15.000
1.251E-05	20.000	20.000
9.724E-06	25.000	25.000
7.758E-06	30.000	30.000
6.293E-06	35.000	35.000
5.449E-06	40.000	40.000
4.781E-06	45.000	45.000
4.204E-06	50.000	50.000
3.697E-06	55.000	55.000
3.243E-06	60.000	60.000
2.833E-06	65.000	65.000
2.456E-06	70.000	70.000
2.106E-06	75.000	75.000
1.770E-06	80.000	80.000
1.434E-06	85.000	85.000
4.605E-05	5.0	5.00

K= 17 FIVEXQ(K)= 4.605E-05 FIVEPR(K)= 5.000

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

#### FIVE PERCENT OVERALL SITE LIMIT

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

1.884E-04	1.009E-04	6.413E-05	4.947E-05	4.343E-05	3.520E-05	3.436E-05	3.242E-05	2.743E-05	2.665E-05
0.025	0.037	1.468	1.484	2.559	3.154	4.474	5.193	5.470	5.479
0.02520	0.03665	1.46833	1.48437	2.55870	3.15428	4.47371	5.19299	5.47017	5.47933
2.327E-05	2.199E-05	1.844E-05	1.837E-05	1.684E-05	1.520E-05	1.280E-05	1.140E-05	1.045E-05	9.072E-06
7.486	7.548	9.472	9.477	10.895	14.021	15.487	17.904	18.367	19.077
7.48597	7.54782	9.47200	9.47658	10.89452	14.02131	15.48735	17.90402	18.36674	19.07686
8.921E-06	8.732E-06	6.898E-06	6.560E-06	6.144E-06	5.632E-06	4.717E-06	4.706E-06	3.930E-06	3.400E-06
22.295	22.362	29.534	29.548	31.259	36.729	39.622	43.184	45.065	53.614
22.29527	22.36171	29.53385	29.54760	31.25874	36.72891	39.62204	43.18407	45.06472	53.61356
2.953E-06	2.679E-06	2.592E-06	2.374E-06	2.216E-06	1.855E-06	1.756E-06	1.393E-06	1.336E-06	1.120E-06
55.064	63.757	63.768	64.066	72.785	78.759	78.859	85.617	85.903	87.926
55.06357	63.75673	63.76818	64.06596	72.78434	78.75845	78.85921	85.61675	85.90307	87.92575
9.669E-07	8.932E-07	8.275E-07	6.724E-07	5.604E-07	5.391E-07	4.563E-07	4.503E-07	4.265E-07	3.810E-07
87.969	88.925	88.945	90.075	90.139	91.202	91.848	92.553	92.658	92.681
87.96926	88.92448	88.94508	90.07438	90.13850	91.20139	91.84737	92.55289	92.65825	92.68114
3.383E-07	2.851E-07	2.720E-07	2.580E-07	2.146E-07	1.963E-07	1.721E-07	1.437E-07	1.313E-07	1.108E-07
93.314	93.758	93.925	93.978	94.654	94.736	95.522	96.069	96.475	96.530
93.31336	93.75774	93.92494	93.97762	94.65337	94.73581	95.52152	96.06899	96.47444	96.52941
1.080E-07	9.881E-08	8.681E-08	7.923E-08	6.617E-08	4.971E-08	3.997E-08	3.536E-08	1.628E-08	
96.981	97.636	97.780	98.516	99.063	99.794	99.938	99.975	100.000	
96.98066	97.63579	97.78008	98.51538	99.06285	99.79356	99.93786	99.97450	99.99969	

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 5.189  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 14.021

K	I	XQSAVE(K, I)	XQINT(K, I)	XQSLOP(K, I)
18	1	-8.57707	-11.46096	-0.82898
18	2	-9.65463	-12.34616	-1.23523
18	3	-10.33672	-12.58715	-1.38337
18	4	-11.09395	-12.66818	-1.45844
18	5	-11.88432	-12.43229	-1.01955
18	6	-12.08707	-12.42146	-0.98756
18	7	-13.01987	-12.45841	-0.92658
18	8	-13.19770	NUMXQ(K) = 8	
		7.249E-05	1.000	1.000
		4.439E-05	3.000	3.000
		3.317E-05	5.000	5.000
		2.012E-05	10.000	10.000
		1.428E-05	15.000	15.000
		1.075E-05	20.000	20.000
		8.420E-06	25.000	25.000
		6.804E-06	30.000	30.000
		5.904E-06	35.000	35.000
		5.175E-06	40.000	40.000
		4.563E-06	45.000	45.000
		4.031E-06	50.000	50.000
		3.562E-06	55.000	55.000
		3.140E-06	60.000	60.000
		2.757E-06	65.000	65.000
		2.403E-06	70.000	70.000
		2.080E-06	75.000	75.000
		3.317E-05	5.0	5.00

K= 18 FIVEXQ(K) = 3.317E-05 FIVEPR(K) = 5.000

K	HIGHPR	PR	GRNDVT(K)
1	-3.06158	0.11010	5.94713
2	-1.84332	3.26408	4.12317
3	-3.32118	0.04482	3.63725
4	-3.23022	0.06185	4.74829
5	-2.99191	0.13862	5.67663
6	-2.99731	0.13619	4.65168
7	-3.04268	0.11725	5.13989
8	-2.95619	0.15574	7.75588
9	-2.78909	0.26429	8.28787
10	-2.83186	0.23140	7.26061
11	-2.84724	0.22051	6.68431

12	-2.82533	0.23617	5.93576
13	-2.72118	0.32525	8.39979
14	-2.67041	0.37879	8.27757
15	-2.57624	0.49942	7.82481
16	-2.76210	0.28716	5.64936

K	HOURS (K)	TOTHR
1	9.64439	9.64439
2	285.93350	295.57790
3	3.92647	299.50440
4	5.41821	304.92260
5	12.14333	317.06590
6	11.93030	328.99620
7	10.27095	339.26720
8	13.64291	352.91010
9	23.15154	376.06170
10	20.27039	396.33210
11	19.31645	415.64850
12	20.68810	436.33660
13	28.49195	464.82860
14	33.18231	498.01090
15	43.74879	541.75960
16	25.15498	566.91460

K	FIVEXQ	SVANN	SLTIME	TIMINT	I	TIME	XQT
1	1.375E-05	1.171E-07	-0.5684	-10.8005	1	8.0	-11.98241
					2	16.0	-12.37636
					3	72.0	-13.23121
					4	624.0	-14.45857
2	1.036E-05	8.248E-08	-0.5765	-11.0776	1	8.0	-12.27631
					2	16.0	-12.67587
					3	72.0	-13.54290
					4	624.0	-14.78774
3	8.661E-06	7.068E-08	-0.5735	-11.2591	1	8.0	-12.45162
					2	16.0	-12.84912
					3	72.0	-13.71165
					4	624.0	-14.95004
4	1.057E-05	8.991E-08	-0.5685	-11.0639	1	8.0	-12.24600
					2	16.0	-12.64002
					3	72.0	-13.49501
					4	624.0	-14.72258
5	2.364E-05	1.618E-07	-0.5945	-10.2403	1	8.0	-11.47654
					2	16.0	-11.88861
					3	72.0	-12.78277
					4	624.0	-14.06655
6	2.433E-05	1.261E-07	-0.6276	-10.1890			

7	2.319E-05	1.282E-07	-0.6199	-10.2421	1	8.0	-11.49395
					2	16.0	-11.92893
					3	72.0	-12.87282
					4	624.0	-14.22800
8	2.677E-05	1.750E-07	-0.6000	-10.1123	1	8.0	-11.53118
					2	16.0	-11.96089
					3	72.0	-12.89332
					4	624.0	-14.23207
9	3.415E-05	2.035E-07	-0.6110	-9.8612	1	8.0	-11.35983
					2	16.0	-11.77569
					3	72.0	-12.67806
					4	624.0	-13.97365
10	2.639E-05	1.732E-07	-0.5994	-10.1269	1	8.0	-11.13171
					2	16.0	-11.55521
					3	72.0	-12.47418
					4	624.0	-13.79358
11	2.227E-05	1.667E-07	-0.5837	-10.3076	1	8.0	-11.37341
					2	16.0	-11.78890
					3	72.0	-12.69048
					4	624.0	-13.98492
12	2.326E-05	1.582E-07	-0.5952	-10.2562	1	8.0	-11.52147
					2	16.0	-11.92608
					3	72.0	-12.80406
					4	624.0	-14.06462
13	3.115E-05	2.125E-07	-0.5948	-9.9645	1	8.0	-11.49390
					2	16.0	-11.90646
					3	72.0	-12.80167
					4	624.0	-14.08698
14	3.378E-05	2.139E-07	-0.6037	-9.8773	1	8.0	-11.20140
					2	16.0	-11.61370
					3	72.0	-12.50838
					4	624.0	-13.79291
15	4.236E-05	2.476E-07	-0.6132	-9.6442	1	8.0	-11.13259
					2	16.0	-11.55103
					3	72.0	-12.45900
					4	624.0	-13.76263
16	2.659E-05	1.638E-07	-0.6070	-10.1140	1	8.0	-10.91937
					2	16.0	-11.34444
					3	72.0	-12.26682
					4	624.0	-13.59112
					1	8.0	-11.37634



				2	16.0	-11.79712
				3	72.0	-12.71016
				4	624.0	-14.02106
17	4.605E-05	2.476E-07	-0.6232	-9.5537		
				1	8.0	-10.84964
				2	16.0	-11.28162
				3	72.0	-12.21898
				4	624.0	-13.56479
18	3.317E-05	2.476E-07	-0.5841	-9.9091		
				1	8.0	-11.12363
				2	16.0	-11.52847
				3	72.0	-12.40695
				4	624.0	-13.66822

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Byron

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 9.1 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 76.2-9.1 meters

SOURCE OF DATA:

COMMENTS: Byron, 94-98 met (r4), 11 ws cats, 30' wind, 30'-250' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

RELATIVE CONCENTRATION (X/Q) VALUES (SEC/CUBIC METER)  
VERSUS

AVERAGING TIME

HOURS PER YEAR MAX  
0-2 HR X/Q IS

EXCEEDED

DOWNWIND

DOWNWIND DISTANCE SECTOR (METERS)	0-2 HOURS	0-8 HOURS	8-24 HOURS	1-4 DAYS	4-30 DAYS ANNUAL AVERAGE	IN SECTOR	SECTOR
S 4828.	1.37E-05	6.25E-06	4.22E-06	1.79E-06	5.26E-07	1.17E-07	S
SSW 4828.	1.04E-05	4.66E-06	3.13E-06	1.31E-06	3.78E-07	8.25E-08	SSW
SW 4828.	8.66E-06	3.91E-06	2.63E-06	1.11E-06	3.22E-07	7.07E-08	SW
WSW 4828.	1.06E-05	4.80E-06	3.24E-06	1.38E-06	4.04E-07	8.99E-08	WSW
W 4828.	2.36E-05	1.04E-05	6.87E-06	2.81E-06	7.78E-07	1.62E-07	W
WNW 4828.	2.43E-05	1.02E-05	6.60E-06	2.57E-06	6.62E-07	1.26E-07	WNW
NW 4828.	2.32E-05	9.82E-06	6.39E-06	2.51E-06	6.59E-07	1.28E-07	NW
NNW 4828.	2.68E-05	1.17E-05	7.69E-06	3.12E-06	8.54E-07	1.75E-07	NNW
N 4828.	3.42E-05	1.46E-05	9.59E-06	3.82E-06	1.02E-06	2.03E-07	N
NNE 4828.	2.64E-05	1.15E-05	7.59E-06	3.08E-06	8.44E-07	1.73E-07	NNE
NE 4828.	2.23E-05	9.91E-06	6.62E-06	2.75E-06	7.79E-07	1.67E-07	NE
ENE 4828.	2.33E-05	1.02E-05	6.75E-06	2.76E-06	7.62E-07	1.58E-07	ENE
E 4828.	3.11E-05	1.37E-05	9.04E-06	3.70E-06	1.02E-06	2.12E-07	E
ESE 4828.	3.38E-05	1.46E-05	9.63E-06	3.88E-06	1.05E-06	2.14E-07	ESE
SE 4828.	4.24E-05	1.81E-05	1.18E-05	4.71E-06	1.25E-06	2.48E-07	SE
SSE 4828.	2.66E-05	1.15E-05	7.53E-06	3.02E-06	8.14E-07	1.64E-07	SSE
MAX X/Q	4.24E-05				TOTAL HOURS AROUND SITE: 566.9		
SRP 2.3.4 4828.	4.61E-05	1.94E-05	1.26E-05	4.94E-06	1.28E-06	2.48E-07	
SITE LIMIT	3.32E-05	1.48E-05	9.85E-06	4.09E-06	1.16E-06	2.48E-07	

THE FIVE-PERCENT-FOR-THE-ENTIRE-SITE X/Q IS LIMITING.

**\*\*NOTE\*\*:** VALUES ON THIS PAGE ARE APPROXIMATIONS ONLY.  
CHECK THE REASONABLENESS OF THE ENVELOPES  
COMPUTED FOR THE 0-2 HOUR VALUES. FOR ANY  
FAULTY ENVELOPES, ADJUST THE ABOVE VALUES.



**ATTACHMENT 3**

**Braidwood and Byron Stations  
Measurement Uncertainty Recapture Technical Evaluation**

**Response to NRC Acceptance Review Questions**

**Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B,  
Appendix BB-7: "Braidwood PAVAN Input and Output"**

1	1111											Ground Release			
Braidwood															
10.4 meters	61.9-10.4 meters														
Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T															
11	0														
2917.	60.7	10.0	10.4												
0	0	0	0	3	20	19									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		
0.	0.	2.	3.	0.	1.	3.	2.	0.	3.	0.	0.	1.			
0.	5.	14.	16.	21.	6.	14.	7.	7.	8.	0.	7.	2.			
27.	15.	67.	44.	45.	28.	32.	51.	46.	24.	19.	26.	34.			
33.	41.	55.	19.	20.	14.	19.	38.	32.	31.	30.	38.	46.			
31.	40.	25.	3.	8.	7.	6.	10.	31.	62.	33.	25.	29.			
12.	10.	5.	1.	0.	3.	2.	7.	21.	27.	20.	19.	21.			
2.	1.	0.	0.	0.	0.	7.	12.	18.	32.	7.	5.	11.			
0.	0.	0.	0.	0.	0.	0.	3.	6.	2.	0.	0.	0.			
0.	0.	0.	0.	0.	0.	0.	1.	3.	7.	1.	0.	0.			
0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.			
0.	1.	4.	6.	6.	1.	1.	3.	4.	0.	0.	0.	1.			
3.	3.	9.	15.	20.	12.	10.	11.	5.	4.	4.	6.	2.			
21.	17.	31.	35.	29.	27.	32.	29.	21.	21.	20.	19.	53.			
23.	26.	34.	14.	15.	10.	12.	19.	19.	27.	18.	27.	21.			
10.	20.	13.	4.	4.	1.	7.	15.	20.	28.	28.	24.	30.			
9.	12.	3.	3.	0.	0.	0.	8.	22.	20.	18.	13.	8.			
2.	0.	1.	0.	0.	0.	5.	11.	9.	17.	18.	7.	12.			
0.	0.	0.	0.	0.	0.	0.	1.	6.	2.	0.	0.	4.			
0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	0.			
0.	0.	0.	2.	1.	0.	1.	0.	0.	0.	0.	0.	0.			
1.	3.	3.	10.	10.	6.	5.	2.	4.	2.	1.	3.	3.			
11.	13.	23.	20.	24.	18.	13.	14.	13.	11.	7.	11.	16.			
21.	25.	40.	41.	49.	35.	39.	41.	20.	23.	26.	33.	48.			
27.	27.	36.	14.	16.	10.	16.	35.	27.	35.	35.	37.	56.			
19.	18.	23.	2.	4.	0.	9.	13.	27.	31.	37.	38.	35.			
10.	12.	4.	0.	0.	4.	5.	19.	17.	29.	31.	18.	12.			
4.	4.	0.	0.	0.	0.	5.	14.	18.	35.	11.	13.	12.			
1.	0.	0.	0.	0.	0.	0.	1.	2.	10.	0.	1.	1.			
0.	0.	0.	0.	0.	0.	0.	1.	0.	6.	0.	0.	0.			
9.	21.	15.	36.	23.	7.	4.	4.	3.	1.	6.	4.	8.			
31.	51.	90.	131.	128.	43.	24.	19.	12.	12.	19.	28.	41.			
71.	70.	129.	195.	164.	93.	66.	54.	35.	40.	33.	58.	85.			
167.	222.	315.	343.	197.	166.	190.	203.	115.	97.	145.	224.	318.			
166.	196.	262.	203.	106.	89.	132.	217.	128.	150.	228.	228.	266.			
100.	194.	196.	92.	26.	57.	97.	147.	155.	179.	239.	201.	261.			
71.	148.	111.	20.	3.	32.	81.	133.	143.	179.	154.	115.	192.			
33.	66.	13.	0.	1.	7.	39.	107.	205.	253.	166.	85.	192.			
10.	1.	0.	0.	0.	0.	0.	18.	60.	111.	33.	22.	51.			
0.	0.	0.	0.	0.	0.										

43. 50. 85. 124. 140. 34. 21. 13. 10. 13. 9. 20. 23. 51. 47. 37.  
 84. 94. 146. 263. 285. 159. 60. 38. 19. 17. 20. 45. 118. 171. 130. 82.  
 99. 125. 156. 235. 201. 192. 125. 105. 55. 32. 50. 140. 180. 165. 172. 89.  
 188. 238. 202. 262. 175. 269. 355. 422. 233. 187. 224. 421. 298. 310. 183. 215.  
 125. 129. 153. 97. 56. 88. 254. 317. 319. 350. 299. 249. 200. 244. 130. 153.  
 46. 87. 66. 34. 13. 50. 100. 223. 310. 388. 186. 114. 134. 165. 61. 85.  
 39. 52. 47. 15. 2. 25. 37. 136. 216. 264. 79. 61. 75. 88. 23. 30.  
 27. 71. 75. 6. 0. 3. 35. 77. 185. 236. 61. 46. 71. 84. 19. 23.  
 14. 14. 3. 0. 0. 0. 2. 5. 81. 44. 19. 27. 43. 16. 0. 0.  
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 45. 30. 37. 75. 144. 147. 68. 36. 16. 25. 22. 54. 128. 199. 114. 68.  
 45. 24. 10. 11. 28. 150. 77. 44. 21. 27. 37. 103. 164. 93. 44. 28.  
 21. 9. 4. 4. 6. 49. 71. 72. 43. 62. 43. 259. 128. 37. 10. 12.  
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 52. 44. 53. 81. 91. 46. 27. 18. 13. 12. 19. 17. 43. 81. 77. 66.  
 18. 20. 10. 14. 65. 48. 15. 4. 9. 9. 11. 31. 73. 91. 39. 28.  
 8. 3. 0. 3. 25. 30. 11. 1. 4. 8. 6. 30. 47. 21. 5. 9.  
 1. 1. 0. 1. 0. 6. 5. 3. 2. 6. 1. 111. 22. 1. 2. 1.  
 1. 0. 0. 0. 0. 0. 0. 1. 2. 4. 2. 3. 0. 0. 0. 0.  
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USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PRINTOUT OF INPUT CARDS

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1      00010 01111 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 00000 2      Braidwood
Ground Release
3      10.4 meters          61.9-10.4 meters
4
5      Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T          6          11 43730          0
7      0.500 2917.000      60.700      10.000      10.400
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9      33.000 41.000 55.000 19.000 20.000 14.000 19.000 38.000 32.000 31.000 30.000 38.000 46.000 36.000 41.000 49.000
9      31.000 40.000 25.000 3.000 8.000 7.000 6.000 10.000 31.000 62.000 33.000 25.000 29.000 33.000 62.000 58.000
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9      31.000 51.000 90.000 131.000 128.000 43.000 24.000 19.000 12.000 12.000 19.000 28.000 41.000 70.000 72.000 39.000
9      71.000 70.000 129.000 195.000 164.000 93.000 66.000 54.000 35.000 40.000 33.000 58.000 85.000 81.000 133.000 91.000
9      167.000 222.000 315.000 343.000 197.000 166.000 190.000 203.000 115.000 97.000 145.000 224.000 318.000 306.000 323.000 276.000
9      166.000 196.000 262.000 203.000 106.000 89.000 132.000 217.000 128.000 150.000 228.000 228.000 266.000 302.000 279.000 213.000
9      100.000 194.000 196.000 92.000 26.000 57.000 97.000 147.000 155.000 179.000 239.000 201.000 261.000 286.000 193.000 207.000

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USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS A

WIND SPEED (M/S)

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.05  | 1.04    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.55  | 1.54    | 0.000 | 0.000 | 0.005 | 0.007 | 0.000 | 0.002 | 0.007 | 0.005 | 0.000 | 0.007 | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.034 |
| 2.04  | 2.02    | 0.000 | 0.011 | 0.032 | 0.037 | 0.048 | 0.014 | 0.032 | 0.016 | 0.016 | 0.018 | 0.000 | 0.016 | 0.005 | 0.007 | 0.000 | 0.007 | 0.258 |
| 3.05  | 3.02    | 0.062 | 0.034 | 0.153 | 0.101 | 0.103 | 0.064 | 0.073 | 0.117 | 0.105 | 0.055 | 0.043 | 0.059 | 0.078 | 0.050 | 0.066 | 0.032 | 1.196 |
| 4.05  | 4.01    | 0.075 | 0.094 | 0.126 | 0.043 | 0.046 | 0.032 | 0.043 | 0.087 | 0.073 | 0.071 | 0.069 | 0.087 | 0.105 | 0.082 | 0.094 | 0.112 | 1.239 |
| 5.05  | 5.00    | 0.071 | 0.091 | 0.057 | 0.007 | 0.018 | 0.016 | 0.014 | 0.023 | 0.071 | 0.142 | 0.075 | 0.057 | 0.066 | 0.075 | 0.142 | 0.133 | 1.059 |
| 6.05  | 5.99    | 0.027 | 0.023 | 0.011 | 0.002 | 0.000 | 0.007 | 0.005 | 0.016 | 0.048 | 0.062 | 0.046 | 0.043 | 0.048 | 0.085 | 0.043 | 0.043 | 0.510 |
| 8.05  | 7.97    | 0.005 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.016 | 0.027 | 0.041 | 0.073 | 0.016 | 0.011 | 0.025 | 0.069 | 0.034 | 0.018 | 0.338 |
| 10.01 | 9.92    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.014 | 0.005 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.027 |
| 24.59 | 24.35   | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.007 | 0.016 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.027 |
| TOTAL |         | 0.24  | 0.26  | 0.38  | 0.20  | 0.21  | 0.13  | 0.19  | 0.30  | 0.38  | 0.45  | 0.25  | 0.27  | 0.33  | 0.37  | 0.38  | 0.35  | 4.69  |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS B

WIND SPEED (M/S)

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.05  | 1.04    | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.005 |
| 1.55  | 1.54    | 0.000 | 0.002 | 0.009 | 0.014 | 0.014 | 0.002 | 0.002 | 0.007 | 0.009 | 0.000 | 0.000 | 0.000 | 0.002 | 0.002 | 0.002 | 0.002 | 0.069 |
| 2.04  | 2.02    | 0.007 | 0.007 | 0.021 | 0.034 | 0.046 | 0.027 | 0.023 | 0.025 | 0.011 | 0.009 | 0.009 | 0.014 | 0.005 | 0.014 | 0.011 | 0.002 | 0.265 |
| 3.05  | 3.02    | 0.048 | 0.039 | 0.071 | 0.080 | 0.066 | 0.062 | 0.073 | 0.066 | 0.048 | 0.048 | 0.046 | 0.043 | 0.121 | 0.064 | 0.064 | 0.062 | 1.002 |
| 4.05  | 4.01    | 0.053 | 0.059 | 0.078 | 0.032 | 0.034 | 0.023 | 0.027 | 0.043 | 0.043 | 0.062 | 0.041 | 0.062 | 0.048 | 0.098 | 0.098 | 0.071 | 0.874 |
| 5.05  | 5.00    | 0.023 | 0.046 | 0.030 | 0.009 | 0.009 | 0.002 | 0.016 | 0.034 | 0.046 | 0.064 | 0.064 | 0.055 | 0.069 | 0.089 | 0.064 | 0.075 | 0.695 |
| 6.05  | 5.99    | 0.021 | 0.027 | 0.007 | 0.007 | 0.000 | 0.000 | 0.000 | 0.018 | 0.050 | 0.046 | 0.041 | 0.030 | 0.018 | 0.055 | 0.046 | 0.039 | 0.405 |
| 8.05  | 7.97    | 0.005 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.011 | 0.025 | 0.021 | 0.039 | 0.041 | 0.016 | 0.027 | 0.041 | 0.009 | 0.016 | 0.254 |
| 10.01 | 9.92    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.014 | 0.005 | 0.000 | 0.000 | 0.009 | 0.007 | 0.000 | 0.000 | 0.037 |
| 24.59 | 24.35   | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.002 | 0.005 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.009 |
| TOTAL |         | 0.16  | 0.18  | 0.22  | 0.18  | 0.17  | 0.12  | 0.15  | 0.22  | 0.24  | 0.28  | 0.24  | 0.22  | 0.30  | 0.37  | 0.29  | 0.27  | 3.61  |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION

ATMOSPHERIC STABILITY CLASS C

WIND SPEED (M/S)

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.05  | 1.04    | 0.000 | 0.000 | 0.000 | 0.005 | 0.002 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.009 |
| 1.55  | 1.54    | 0.002 | 0.007 | 0.007 | 0.023 | 0.023 | 0.014 | 0.011 | 0.005 | 0.009 | 0.005 | 0.002 | 0.007 | 0.007 | 0.002 | 0.005 | 0.000 | 0.128 |
| 2.04  | 2.02    | 0.025 | 0.030 | 0.053 | 0.046 | 0.055 | 0.041 | 0.030 | 0.032 | 0.030 | 0.025 | 0.016 | 0.025 | 0.037 | 0.027 | 0.011 | 0.021 | 0.503 |
| 3.05  | 3.02    | 0.048 | 0.057 | 0.091 | 0.094 | 0.112 | 0.080 | 0.089 | 0.094 | 0.046 | 0.053 | 0.059 | 0.075 | 0.110 | 0.112 | 0.110 | 0.064 | 1.294 |

|       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4.05  | 4.01  | 0.062 | 0.062 | 0.082 | 0.032 | 0.037 | 0.023 | 0.037 | 0.080 | 0.062 | 0.080 | 0.080 | 0.085 | 0.128 | 0.133 | 0.117 | 0.094 | 1.191 |
| 5.05  | 5.00  | 0.043 | 0.041 | 0.053 | 0.005 | 0.009 | 0.000 | 0.021 | 0.030 | 0.062 | 0.071 | 0.085 | 0.087 | 0.080 | 0.107 | 0.114 | 0.075 | 0.883 |
| 6.05  | 5.99  | 0.023 | 0.027 | 0.009 | 0.000 | 0.000 | 0.000 | 0.009 | 0.011 | 0.043 | 0.039 | 0.066 | 0.071 | 0.041 | 0.027 | 0.048 | 0.050 | 0.494 |
| 8.05  | 7.97  | 0.009 | 0.009 | 0.000 | 0.000 | 0.000 | 0.000 | 0.011 | 0.032 | 0.041 | 0.080 | 0.025 | 0.030 | 0.027 | 0.055 | 0.016 | 0.018 | 0.354 |
| 10.01 | 9.92  | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.005 | 0.023 | 0.000 | 0.002 | 0.002 | 0.011 | 0.000 | 0.000 | 0.048 |
| 24.59 | 24.35 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 | 0.014 | 0.000 | 0.000 | 0.000 | 0.007 | 0.000 | 0.000 | 0.023 |
| TOTAL |       | 0.21  | 0.23  | 0.29  | 0.20  | 0.24  | 0.17  | 0.21  | 0.32  | 0.29  | 0.42  | 0.34  | 0.35  | 0.42  | 0.50  | 0.42  | 0.30  | 4.93  |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS D

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.05  | 1.04    | 0.021 | 0.048 | 0.034 | 0.082 | 0.053 | 0.016 | 0.009 | 0.009 | 0.007 | 0.002 | 0.014 | 0.009 | 0.018 | 0.025 | 0.034 | 0.037 | 0.418 |
| 1.55  | 1.54    | 0.071 | 0.117 | 0.206 | 0.300 | 0.293 | 0.098 | 0.055 | 0.043 | 0.027 | 0.027 | 0.043 | 0.064 | 0.094 | 0.160 | 0.165 | 0.089 | 1.852 |
| 2.04  | 2.02    | 0.162 | 0.160 | 0.295 | 0.446 | 0.375 | 0.213 | 0.151 | 0.123 | 0.080 | 0.091 | 0.075 | 0.133 | 0.194 | 0.185 | 0.304 | 0.208 | 3.197 |
| 3.05  | 3.02    | 0.382 | 0.508 | 0.720 | 0.784 | 0.450 | 0.380 | 0.434 | 0.464 | 0.263 | 0.222 | 0.332 | 0.512 | 0.727 | 0.700 | 0.739 | 0.631 | 8.248 |
| 4.05  | 4.01    | 0.380 | 0.448 | 0.599 | 0.464 | 0.242 | 0.204 | 0.302 | 0.496 | 0.293 | 0.343 | 0.521 | 0.521 | 0.608 | 0.691 | 0.638 | 0.487 | 7.238 |
| 5.05  | 5.00    | 0.229 | 0.444 | 0.448 | 0.210 | 0.059 | 0.130 | 0.222 | 0.336 | 0.354 | 0.409 | 0.547 | 0.460 | 0.597 | 0.654 | 0.441 | 0.473 | 6.014 |
| 6.05  | 5.99    | 0.162 | 0.338 | 0.254 | 0.046 | 0.007 | 0.073 | 0.185 | 0.304 | 0.327 | 0.409 | 0.352 | 0.263 | 0.439 | 0.519 | 0.155 | 0.318 | 4.153 |
| 8.05  | 7.97    | 0.075 | 0.151 | 0.030 | 0.000 | 0.002 | 0.016 | 0.089 | 0.245 | 0.469 | 0.579 | 0.380 | 0.194 | 0.439 | 0.453 | 0.110 | 0.204 | 3.435 |
| 10.01 | 9.92    | 0.023 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.041 | 0.137 | 0.254 | 0.075 | 0.050 | 0.117 | 0.114 | 0.005 | 0.048 | 0.867 |
| 24.59 | 24.35   | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.030 | 0.037 | 0.034 | 0.002 | 0.023 | 0.007 | 0.000 | 0.007 | 0.146 |
| TOTAL |         | 1.50  | 2.22  | 2.59  | 2.33  | 1.48  | 1.13  | 1.45  | 2.07  | 1.99  | 2.37  | 2.37  | 2.21  | 3.26  | 3.51  | 2.59  | 2.50  | 35.57 |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS E

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.000 | 0.000 | 0.001 | 0.001 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 |
| 1.05  | 1.03    | 0.098 | 0.114 | 0.194 | 0.284 | 0.320 | 0.078 | 0.048 | 0.030 | 0.023 | 0.030 | 0.021 | 0.046 | 0.053 | 0.117 | 0.107 | 0.085 | 1.646 |
| 1.55  | 1.52    | 0.192 | 0.215 | 0.334 | 0.601 | 0.652 | 0.364 | 0.137 | 0.087 | 0.043 | 0.039 | 0.046 | 0.103 | 0.270 | 0.391 | 0.297 | 0.188 | 3.958 |
| 2.04  | 2.00    | 0.226 | 0.286 | 0.357 | 0.537 | 0.460 | 0.439 | 0.286 | 0.240 | 0.126 | 0.073 | 0.114 | 0.320 | 0.412 | 0.377 | 0.393 | 0.204 | 4.850 |
| 3.05  | 2.99    | 0.430 | 0.544 | 0.462 | 0.599 | 0.400 | 0.615 | 0.812 | 0.965 | 0.533 | 0.428 | 0.512 | 0.963 | 0.681 | 0.709 | 0.418 | 0.492 | 9.563 |
| 4.05  | 3.97    | 0.286 | 0.295 | 0.350 | 0.222 | 0.128 | 0.201 | 0.581 | 0.725 | 0.729 | 0.800 | 0.684 | 0.569 | 0.457 | 0.558 | 0.297 | 0.350 | 7.233 |
| 5.05  | 4.95    | 0.105 | 0.199 | 0.151 | 0.078 | 0.030 | 0.114 | 0.229 | 0.510 | 0.709 | 0.887 | 0.425 | 0.261 | 0.306 | 0.377 | 0.139 | 0.194 | 4.715 |
| 6.05  | 5.93    | 0.089 | 0.119 | 0.107 | 0.034 | 0.005 | 0.057 | 0.085 | 0.311 | 0.494 | 0.604 | 0.181 | 0.139 | 0.172 | 0.201 | 0.053 | 0.069 | 2.719 |
| 8.05  | 7.89    | 0.062 | 0.162 | 0.172 | 0.014 | 0.000 | 0.007 | 0.080 | 0.176 | 0.423 | 0.540 | 0.139 | 0.105 | 0.162 | 0.192 | 0.043 | 0.053 | 2.330 |
| 10.01 | 9.82    | 0.032 | 0.032 | 0.007 | 0.000 | 0.000 | 0.000 | 0.005 | 0.011 | 0.185 | 0.101 | 0.043 | 0.062 | 0.098 | 0.037 | 0.000 | 0.000 | 0.613 |
| 24.59 | 24.11   | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.023 | 0.027 | 0.023 | 0.034 | 0.030 | 0.053 | 0.007 | 0.000 | 0.005 | 0.204 |
| TOTAL |         | 1.52  | 1.97  | 2.13  | 2.37  | 2.00  | 1.88  | 2.26  | 3.08  | 3.29  | 3.52  | 2.20  | 2.60  | 2.66  | 2.97  | 1.75  | 1.64  | 37.84 |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS F

| TOWER RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36 0.35     | 0.003 | 0.002 | 0.004 | 0.006 | 0.007 | 0.003 | 0.002 | 0.001 | 0.001 | 0.001 | 0.001 | 0.002 | 0.003 | 0.004 | 0.004 | 0.003 | 0.046 |
| 1.05 1.03     | 0.146 | 0.103 | 0.192 | 0.261 | 0.327 | 0.137 | 0.073 | 0.053 | 0.039 | 0.043 | 0.043 | 0.071 | 0.128 | 0.188 | 0.181 | 0.119 | 2.104 |
| 1.55 1.52     | 0.103 | 0.069 | 0.085 | 0.172 | 0.329 | 0.336 | 0.155 | 0.082 | 0.037 | 0.057 | 0.050 | 0.123 | 0.293 | 0.455 | 0.261 | 0.155 | 2.762 |
| 2.04 2.00     | 0.103 | 0.055 | 0.023 | 0.025 | 0.064 | 0.343 | 0.176 | 0.101 | 0.048 | 0.062 | 0.085 | 0.236 | 0.375 | 0.213 | 0.101 | 0.064 | 2.072 |
| 3.05 2.99     | 0.048 | 0.021 | 0.009 | 0.009 | 0.014 | 0.112 | 0.162 | 0.165 | 0.098 | 0.142 | 0.098 | 0.592 | 0.293 | 0.085 | 0.023 | 0.027 | 1.898 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M | MINOR REV. NO. 1B | APPENDIX BB-7 | PAGE NO. 7 of 160 |
|--|-------------------|---------------|-------------------|
|--|-------------------|---------------|-------------------|

|       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4.05  | 3.97  | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.002 | 0.011 | 0.062 | 0.039 | 0.167 | 0.082 | 0.085 | 0.030 | 0.007 | 0.002 | 0.000 | 0.489 |
| 5.05  | 4.95  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.002 | 0.016 | 0.107 | 0.023 | 0.000 | 0.002 | 0.000 | 0.000 | 0.002 | 0.155 |
| 6.05  | 5.93  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.023 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.023 |
| 8.05  | 7.89  | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 | 0.000 | 0.007 |
| 10.01 | 9.82  | 0.000 | 0.009 | 0.018 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.027 |
| 24.59 | 24.11 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.039 | 0.002 | 0.000 | 0.000 | 0.000 | 0.041 |
| TOTAL |       | 0.40  | 0.26  | 0.34  | 0.47  | 0.74  | 0.93  | 0.58  | 0.47  | 0.28  | 0.60  | 0.38  | 1.15  | 1.13  | 0.95  | 0.57  | 0.37  | 9.62  |

JOINT FREQUENCY DISTRIBUTION OF WIND SPEED AND DIRECTION  
WIND SPEED (M/S)

ATMOSPHERIC STABILITY CLASS G

| TOWER | RELEASE | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | TOTAL |
|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.36  | 0.35    | 0.003 | 0.003 | 0.003 | 0.005 | 0.005 | 0.003 | 0.002 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.003 | 0.005 | 0.005 | 0.004 | 0.043 |
| 1.05  | 1.03    | 0.119 | 0.101 | 0.121 | 0.185 | 0.208 | 0.105 | 0.062 | 0.041 | 0.030 | 0.027 | 0.043 | 0.039 | 0.098 | 0.185 | 0.176 | 0.151 | 1.692 |
| 1.55  | 1.52    | 0.041 | 0.046 | 0.023 | 0.032 | 0.149 | 0.110 | 0.034 | 0.009 | 0.021 | 0.021 | 0.025 | 0.071 | 0.167 | 0.208 | 0.089 | 0.064 | 1.109 |
| 2.04  | 2.00    | 0.018 | 0.007 | 0.000 | 0.007 | 0.057 | 0.069 | 0.025 | 0.002 | 0.009 | 0.018 | 0.014 | 0.069 | 0.107 | 0.048 | 0.011 | 0.021 | 0.483 |
| 3.05  | 2.99    | 0.002 | 0.002 | 0.000 | 0.002 | 0.000 | 0.014 | 0.011 | 0.007 | 0.005 | 0.014 | 0.002 | 0.254 | 0.050 | 0.002 | 0.005 | 0.002 | 0.373 |
| 4.05  | 3.97    | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.005 | 0.009 | 0.005 | 0.007 | 0.000 | 0.000 | 0.000 | 0.000 | 0.030 |
| 5.05  | 4.95    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 |
| 6.05  | 5.93    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.05  | 7.89    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 10.01 | 9.82    | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 24.59 | 24.11   | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| TOTAL |         | 0.19  | 0.16  | 0.15  | 0.23  | 0.42  | 0.30  | 0.13  | 0.06  | 0.07  | 0.10  | 0.09  | 0.44  | 0.43  | 0.45  | 0.29  | 0.24  | 3.74  |

WIND MEASURED AT 10.4 METERS.

WIND SPEED CORRECTED TO THE RELEASE HEIGHT OF 10.0 METERS.

OVERALL WIND DIRECTION FREQUENCY

| WIND DIRECTION: | N   | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| FREQUENCY:      | 4.2 | 5.3 | 6.1 | 6.0 | 5.3 | 4.7 | 5.0 | 6.5 | 6.5 | 7.7 | 5.9 | 7.2 | 8.5 | 9.1 | 6.3 | 5.7 |

OVERALL WIND SPEED FREQUENCY AS MEASURED ON THE TOWER:

|                       |       |       |       |       |       |       |       |       |       |        |        |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|
| MAX.WIND SPEED (M/S): | 0.358 | 1.051 | 1.551 | 2.039 | 3.049 | 4.050 | 5.052 | 6.048 | 8.051 | 10.014 | 24.587 |
| WIND SPEED FREQUENCY: | 0.10  | 5.87  | 9.91  | 11.63 | 23.57 | 18.29 | 13.53 | 8.30  | 6.72  | 1.62   | 0.45   |

BUILDING AND RELEASE CHARACTERISTICS:

RELEASE HEIGHT: 10.00 METERS

MIXING VOLUME COEFFICIENT: 0.50

BUILDING CROSS-SECTIONAL AREA: 2917.00 SQUARE METERS

BOUNDARY DISTANCES (METERS) FROM THE SOURCE FOR EACH DOWNWIND SECTOR:

| DOWNWIND SECTOR | S     | SSW   | SW    | WSW   | W     | WNW   | NW    | NNW   | N     | NNE   | NE    | ENE   | E     | ESE   | SE    | SSE   |
|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| BOUNDARY 1      | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  | 485.  |
| BOUNDARY 2      | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. | 1810. |

THE CONVERSION FACTOR APPLIED TO THE WIND SPEED CLASSES IS 0.447

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

WINDSPEEDS ADJUSTED TO 10.0 METERS.

PERCENT OF THE TIME A GIVEN WINDSPEED IS LOWER:

| WINDSPEED<br>(METER/SEC) | CUMULATIVE FREQUENCY<br>(PERCENT) |
|--------------------------|-----------------------------------|
|--------------------------|-----------------------------------|

|       |        |
|-------|--------|
| 0.35  | 0.10   |
| 0.35  | 0.10   |
| 1.03  | 5.54   |
| 1.04  | 5.97   |
| 1.52  | 13.80  |
| 1.54  | 15.88  |
| 2.00  | 23.29  |
| 2.02  | 27.51  |
| 2.99  | 39.35  |
| 3.02  | 51.09  |
| 3.97  | 58.84  |
| 4.01  | 69.38  |
| 4.95  | 74.26  |
| 5.00  | 82.91  |
| 5.93  | 85.65  |
| 5.99  | 91.21  |
| 7.89  | 93.55  |
| 7.97  | 97.93  |
| 9.82  | 98.57  |
| 9.92  | 99.55  |
| 24.11 | 99.79  |
| 24.35 | 100.00 |

| WINDSPEED<br>(INTERPOLATED) | CUMULATIVE FREQUENCY |
|-----------------------------|----------------------|
|-----------------------------|----------------------|

| (METER/SEC) | (PERCENT) |
|-------------|-----------|
|-------------|-----------|

|      |       |
|------|-------|
| 0.35 | 0.10  |
| 1.03 | 5.97  |
| 1.52 | 15.88 |
| 2.01 | 27.51 |
| 3.00 | 51.09 |
| 3.99 | 69.38 |
| 4.98 | 82.91 |
| 5.97 | 91.21 |
| 7.95 | 97.93 |
| 9.88 | 99.55 |

24.22      100.00

ERROR IN NORMAL TRANSFORMATION FOR A( 11)= 100.00000

LOG-NORMAL INTERPOLATION PERCENTILES

| WINDSPEED<br>(METER/SEC) | CUMULATIVE FREQUENCY<br>(PERCENT) |
|--------------------------|-----------------------------------|
| 0.60                     | 1.00                              |
| 0.82                     | 3.00                              |
| 0.97                     | 5.00                              |
| 1.25                     | 10.00                             |
| 1.49                     | 15.00                             |
| 1.70                     | 20.00                             |
| 1.90                     | 25.00                             |
| 2.10                     | 30.00                             |
| 2.30                     | 35.00                             |
| 2.51                     | 40.00                             |
| 2.72                     | 45.00                             |
| 2.95                     | 50.00                             |
| 3.19                     | 55.00                             |
| 3.44                     | 60.00                             |
| 3.72                     | 65.00                             |
| 4.03                     | 70.00                             |
| 4.34                     | 75.00                             |
| 4.72                     | 80.00                             |
| 5.28                     | 85.00                             |
| 5.78                     | 90.00                             |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE S SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 3.0       | 1.46      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.78      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 1.68      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.65      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.11      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
| B              | 2.0       | 0.16      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.14      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 1.24      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.54      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.49      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.11      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| C              | 1.5       | 0.05      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.59      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.14      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.46      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 1.03      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.54      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.22      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C              | 9.9       | 0.05      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
| D              | 1.0       | 0.49      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 1.68      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 3.84      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 9.03      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 8.98      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 5.41      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 3.84      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 1.78      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D              | 9.9       | 0.54      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
| E              | 0.4       | 0.01      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E              | 1.0       | 2.33      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E              | 1.5       | 4.54      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |
| E              | 2.0       | 5.35      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |
| E              | 3.0       | 10.17     | 485.     | 0.         | 0.           | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |

|  |  |  |  |  |  |                   |  |               |  |  |                    |  |
|--|--|--|--|--|--|-------------------|--|---------------|--|--|--------------------|--|
| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  | PAGE NO. 11 of 160 |  |
|--|--|--|--|--|--|-------------------|--|---------------|--|--|--------------------|--|

|   |      |      |      |    |    |      |      |      |           |           |           |
|---|------|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 4.0  | 6.76 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 2.49 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 2.11 | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 1.46 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 0.76 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.05 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
|   |      |      |      |    |    |      |      |      |           |           |           |
| F | 0.4  | 0.08 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 3.46 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 2.43 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 2.43 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 1.14 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
|   |      |      |      |    |    |      |      |      |           |           |           |
| G | 0.4  | 0.07 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 2.81 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 0.97 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.43 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.05 | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |
| G | 4.0  | 0.05 | 485. | 0. | 0. | 13.3 | 5.1  | 26.0 | 6.091E-04 | 3.979E-04 | 3.979E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

S SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.072     | 0.147     | 0.157     | 2.970     | 3.943     | 3.997     | 7.459     | 7.513     | 7.946     | 10.379    |
| 0.00305   | 0.00623   | 0.00664   | 0.12556   | 0.16672   | 0.16900   | 0.31536   | 0.31764   | 0.33594   | 0.43884   |
| 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 12.705    | 15.139    | 16.275    | 16.762    | 21.305    | 26.659    | 28.336    | 38.504    | 42.344    | 49.105    |
| 0.53717   | 0.64008   | 0.68810   | 0.70868   | 0.90077   | 1.12716   | 1.19805   | 1.62796   | 1.79032   | 2.07616   |
| 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 4.933E-05 | 4.743E-05 | 4.551E-05 |
| 49.159    | 58.191    | 60.679    | 61.274    | 70.253    | 72.362    | 77.771    | 79.231    | 80.367    | 84.207    |
| 2.07845   | 2.46034   | 2.56553   | 2.59068   | 2.97028   | 3.05947   | 3.28814   | 3.34989   | 3.39791   | 3.56027   |
| 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 |
| 84.964    | 85.126    | 86.587    | 88.371    | 89.399    | 89.940    | 91.076    | 91.617    | 92.861    | 93.077    |
| 3.59228   | 3.59914   | 3.66089   | 3.73635   | 3.77980   | 3.80266   | 3.85069   | 3.87355   | 3.92615   | 3.93530   |
| 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.291E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |
| 93.131    | 93.672    | 93.726    | 94.213    | 94.321    | 95.781    | 97.566    | 99.243    | 99.892    | 100.000   |
| 3.93758   | 3.96045   | 3.96274   | 3.98332   | 3.98789   | 4.04963   | 4.12510   | 4.19599   | 4.22343   | 4.22800   |

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY



HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2) = 0.125  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3) = 0.315  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4) = 0.900  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5) = 1.626  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6) = 2.458  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7) = 3.057  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8) = 3.557

| K | I | XQSAVE(K, I) | XQINT(K, I)  | XQSLOP(K, I) |
|---|---|--------------|--------------|--------------|
| 1 | 1 | -6.09537     | -10.47460    | -1.09243     |
| 1 | 2 | -7.17293     | -11.58799    | -1.46083     |
| 1 | 3 | -7.59738     | -14.55324    | -2.54630     |
| 1 | 4 | -8.52936     | -12.85459    | -1.82828     |
| 1 | 5 | -8.94587     | -13.53938    | -2.14859     |
| 1 | 6 | -9.31262     | -15.92579    | -3.36167     |
| 1 | 7 | -9.63092     | -19.73417    | -5.39547     |
| 1 | 8 | -9.99767     | NUMXQ(K) = 8 |              |
|   |   | 1.083E-03    | 0.042        | 1.000        |
|   |   | 7.636E-04    | 0.127        | 3.000        |
|   |   | 6.060E-04    | 0.211        | 5.000        |
|   |   | 3.909E-04    | 0.423        | 10.000       |
|   |   | 2.732E-04    | 0.634        | 15.000       |
|   |   | 2.097E-04    | 0.846        | 20.000       |
|   |   | 1.771E-04    | 1.057        | 25.000       |
|   |   | 1.559E-04    | 1.268        | 30.000       |
|   |   | 1.396E-04    | 1.480        | 35.000       |
|   |   | 1.261E-04    | 1.691        | 40.000       |
|   |   | 1.137E-04    | 1.903        | 45.000       |
|   |   | 1.036E-04    | 2.114        | 50.000       |
|   |   | 9.505E-05    | 2.325        | 55.000       |
|   |   | 8.639E-05    | 2.537        | 60.000       |
|   |   | 7.692E-05    | 2.748        | 65.000       |
|   |   | 6.898E-05    | 2.960        | 70.000       |
|   |   | 6.027E-05    | 3.171        | 75.000       |
|   |   | 5.157E-05    | 3.382        | 80.000       |
|   |   | 3.377E-04    | 0.5          | 11.83        |

ANNUAL AVERAGE = 4.55E-06

K= 1 FIVEXQ(K) = 3.377E-04 FIVEPR(K) = 11.826

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN | HT | EFF | PLUME  | HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|---------|----|-----|--------|----|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS  |    |     | METERS |    | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |         |    |     |        |    |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 2.0       | 0.22      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 0.65      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.78      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 1.74      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.43      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.04      | 485.     | 0.      |    | 0.  |        |    | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
|                |           |           |          |         |    |     |        |    |         |         |            |                                   |           |           |
| B              | 1.5       | 0.04      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.13      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 0.74      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 1.13      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.87      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.52      | 485.     | 0.      |    | 0.  |        |    | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
|                |           |           |          |         |    |     |        |    |         |         |            |                                   |           |           |
| C              | 1.5       | 0.13      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.56      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.08      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.17      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 0.78      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.52      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.17      | 485.     | 0.      |    | 0.  |        |    | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
|                |           |           |          |         |    |     |        |    |         |         |            |                                   |           |           |
| D              | 1.0       | 0.91      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 2.21      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 3.04      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 9.63      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 8.51      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 8.42      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 6.42      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 2.86      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D              | 9.9       | 0.04      | 485.     | 0.      |    | 0.  |        |    | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
|                |           |           |          |         |    |     |        |    |         |         |            |                                   |           |           |
| E              | 0.4       | 0.01      | 485.     | 0.      |    | 0.  |        |    | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E              | 1.0       | 2.17      | 485.     | 0.      |    | 0.  |        |    | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E              | 1.5       | 4.08      | 485.     | 0.      |    | 0.  |        |    | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |
| E              | 2.0       | 5.42      | 485.     | 0.      |    | 0.  |        |    | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |
| E              | 3.0       | 10.33     | 485.     | 0.      |    | 0.  |        |    | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |     |      |      |    |    | MINOR REV. NO. 1B |      | APPENDIX BB-7 |           |           | PAGE NO. 15 of 160 |  |
|--|-----|------|------|----|----|-------------------|------|---------------|-----------|-----------|--------------------|--|
| E  | 4.0 | 5.60 | 485. | 0. | 0. | 27.9              | 12.7 | 42.1          | 1.503E-04 | 9.806E-05 | 9.806E-05          |  |
| E  | 5.0 | 3.78 | 485. | 0. | 0. | 27.9              | 12.7 | 33.8          | 1.503E-04 | 7.863E-05 | 7.863E-05          |  |
| E  | 5.9 | 2.26 | 485. | 0. | 0. | 27.9              | 12.7 | 28.2          | 1.503E-04 | 6.567E-05 | 6.567E-05          |  |
| E  | 7.9 | 3.08 | 485. | 0. | 0. | 27.9              | 12.7 | 27.9          | 1.142E-04 | 4.933E-05 | 4.933E-05          |  |
| E  | 9.8 | 0.61 | 485. | 0. | 0. | 27.9              | 12.7 | 27.9          | 9.182E-05 | 3.966E-05 | 3.966E-05          |  |
| F  | 0.4 | 0.04 | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 1.474E-03 | 1.965E-03 | 1.474E-03          |  |
| F  | 1.0 | 1.95 | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 5.018E-04 | 6.690E-04 | 5.018E-04          |  |
| F  | 1.5 | 1.30 | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 3.398E-04 | 4.530E-04 | 3.398E-04          |  |
| F  | 2.0 | 1.04 | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 2.586E-04 | 3.447E-04 | 2.586E-04          |  |
| F  | 3.0 | 0.39 | 485. | 0. | 0. | 19.2              | 8.0  | 46.3          | 2.871E-04 | 2.305E-04 | 2.305E-04          |  |
| F  | 9.8 | 0.17 | 485. | 0. | 0. | 19.2              | 8.0  | 19.2          | 2.106E-04 | 7.018E-05 | 7.018E-05          |  |
| G  | 0.4 | 0.05 | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 2.253E-03 | 4.506E-03 | 2.253E-03          |  |
| G  | 1.0 | 1.91 | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 7.671E-04 | 1.534E-03 | 7.671E-04          |  |
| G  | 1.5 | 0.87 | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 5.195E-04 | 1.039E-03 | 5.195E-04          |  |
| G  | 2.0 | 0.13 | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 3.953E-04 | 7.905E-04 | 3.953E-04          |  |
| G  | 3.0 | 0.04 | 485. | 0. | 0. | 13.3              | 5.1  | 41.3          | 5.092E-04 | 5.286E-04 | 5.092E-04          |  |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### SITE EXCLUSION BOUNDARY CALCULATIONS:

SSW SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.049     | 0.091     | 0.101     | 2.010     | 2.878     | 2.921     | 4.874     | 5.004     | 6.306     | 8.476     |
| 0.00258   | 0.00482   | 0.00530   | 0.10591   | 0.15165   | 0.15394   | 0.25684   | 0.26370   | 0.33230   | 0.44664   |
|           |           |           |           |           |           |           |           |           |           |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 | 9.321E-05 |
| 9.518     | 9.908     | 10.820    | 14.899    | 20.323    | 22.537    | 32.865    | 35.903    | 41.501    | 41.631    |
| 0.50152   | 0.52210   | 0.57013   | 0.78508   | 1.07093   | 1.18755   | 1.73180   | 1.89187   | 2.18687   | 2.19373   |
|           |           |           |           |           |           |           |           |           |           |
| 9.028E-05 | 7.863E-05 | 7.093E-05 | 7.018E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 |
| 51.265    | 55.041    | 55.605    | 55.779    | 64.284    | 66.541    | 74.960    | 75.003    | 78.085    | 79.170    |
| 2.70139   | 2.90033   | 2.93006   | 2.93921   | 3.38741   | 3.50633   | 3.94996   | 3.95224   | 4.11460   | 4.17177   |
|           |           |           |           |           |           |           |           |           |           |
| 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 |
| 85.592    | 86.200    | 86.330    | 87.502    | 90.366    | 91.147    | 91.190    | 91.928    | 92.449    | 93.577    |
| 4.51021   | 4.54223   | 4.54909   | 4.61083   | 4.76176   | 4.80292   | 4.80521   | 4.84408   | 4.87152   | 4.93098   |
|           |           |           |           |           |           |           |           |           |           |
| 1.796E-05 | 1.545E-05 | 1.328E-05 | 1.291E-05 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |           |
| 93.751    | 94.619    | 94.836    | 95.357    | 96.008    | 97.787    | 99.523    | 99.957    | 100.000   |           |
| 4.94012   | 4.98586   | 4.99729   | 5.02474   | 5.05904   | 5.15279   | 5.24426   | 5.26713   | 5.26942   |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.106  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.257  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.186  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.699  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.503  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.507

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 2 | 1 | -6.09537     | -10.57124   | -1.10571     |
| 2 | 2 | -7.17293     | -11.92131   | -1.54498     |
| 2 | 3 | -7.59738     | -13.98545   | -2.28252     |
| 2 | 4 | -8.82336     | -10.68859   | -0.82475     |
| 2 | 5 | -8.94587     | -13.11250   | -1.97187     |
| 2 | 6 | -9.31262     | -14.62129   | -2.75483     |
| 2 | 7 | -9.63092     | -15.31884   | -3.13990     |
| 2 | 8 | -9.99767     | NUMXQ(K)= 8 |              |
|   |   | 9.596E-04    | 0.053       | 1.000        |
|   |   | 6.358E-04    | 0.158       | 3.000        |
|   |   | 4.924E-04    | 0.263       | 5.000        |
|   |   | 2.897E-04    | 0.527       | 10.000       |
|   |   | 2.084E-04    | 0.790       | 15.000       |
|   |   | 1.634E-04    | 1.054       | 20.000       |
|   |   | 1.425E-04    | 1.317       | 25.000       |
|   |   | 1.343E-04    | 1.581       | 30.000       |
|   |   | 1.239E-04    | 1.844       | 35.000       |
|   |   | 1.111E-04    | 2.108       | 40.000       |
|   |   | 1.008E-04    | 2.371       | 45.000       |
|   |   | 9.222E-05    | 2.635       | 50.000       |
|   |   | 8.297E-05    | 2.898       | 55.000       |
|   |   | 7.463E-05    | 3.162       | 60.000       |
|   |   | 6.761E-05    | 3.425       | 65.000       |
|   |   | 6.108E-05    | 3.689       | 70.000       |
|   |   | 5.528E-05    | 3.952       | 75.000       |
|   |   | 5.030E-05    | 4.216       | 80.000       |
|   |   | 4.598E-05    | 4.479       | 85.000       |
|   |   | 3.020E-04    | 0.5         | 9.49         |

ANNUAL AVERAGE = 4.65E-06

K= 2 FIVEXQ(K)= 3.020E-04 FIVEPR(K)= 9.489

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     |                                   |           |           |      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |      |
| A              | 1.5       | 0.07      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |      |
| A              | 2.0       | 0.52      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |      |
| A              | 3.0       | 2.51      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |      |
| A              | 4.0       | 2.06      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |      |
| A              | 5.0       | 0.94      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |      |
| A              | 6.0       | 0.19      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| B              | 1.0       | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.375E-05                         | 7.431E-05 | 7.431E-05 |      |
| B              | 1.5       | 0.15      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |      |
| B              | 2.0       | 0.34      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |      |
| B              | 3.0       | 1.16      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |      |
| B              | 4.0       | 1.27      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |      |
| B              | 5.0       | 0.49      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |      |
| B              | 6.0       | 0.11      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |      |
| B              | 8.0       | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| C              | 1.5       | 0.11      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |      |
| C              | 2.0       | 0.86      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |      |
| C              | 3.0       | 1.50      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |      |
| C              | 4.0       | 1.35      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |      |
| C              | 5.0       | 0.86      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |      |
| C              | 6.0       | 0.15      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| D              | 1.0       | 0.56      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |      |
| D              | 1.5       | 3.37      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |      |
| D              | 2.0       | 4.83      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |      |
| D              | 3.0       | 11.80     | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |      |
| D              | 4.0       | 9.82      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |      |
| D              | 5.0       | 7.34      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |      |
| D              | 6.0       | 4.16      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |      |
| D              | 8.0       | 0.49      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| E              | 0.4       | 0.01      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |      |
| E              | 1.0       | 3.19      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |      |
| E              | 1.5       | 5.47      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |      |
| E              | 2.0       | 5.85      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |      |
| E              | 3.0       | 7.57      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |      |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  | PAGE NO. 19 of 160 |  |
|--|--|--|--|--|--|-------------------|--|---------------|--|--|--------------------|--|
|--|--|--|--|--|--|-------------------|--|---------------|--|--|--------------------|--|

|   |     |      |      |    |    |      |      |      |           |           |           |
|---|-----|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 4.0 | 5.73 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0 | 2.47 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9 | 1.76 | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9 | 2.81 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8 | 0.11 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
|   |     |      |      |    |    |      |      |      |           |           |           |
| F | 0.4 | 0.07 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0 | 3.15 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 1.39 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 0.37 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 0.15 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0 | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 7.9 | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.619E-04 | 8.729E-05 | 8.729E-05 |
| F | 9.8 | 0.30 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.106E-04 | 7.018E-05 | 7.018E-05 |
|   |     |      |      |    |    |      |      |      |           |           |           |
| G | 0.4 | 0.05 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 1.99 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 0.37 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

SW SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.018E-04 | 3.398E-04 | 2.917E-04 | 2.586E-04 | 2.305E-04 |
| 0.051     | 0.119     | 0.133     | 2.119     | 2.494     | 5.641     | 7.028     | 10.213    | 10.588    | 10.738    |
| 0.00311   | 0.00729   | 0.00810   | 0.12930   | 0.15216   | 0.34425   | 0.42886   | 0.62324   | 0.64610   | 0.65525   |
| 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 |
| 11.300    | 16.771    | 16.808    | 22.654    | 26.027    | 33.597    | 38.431    | 44.164    | 44.277    | 56.081    |
| 0.68955   | 1.02342   | 1.02571   | 1.38244   | 1.58825   | 2.05017   | 2.34517   | 2.69504   | 2.70190   | 3.42223   |
| 8.729E-05 | 7.863E-05 | 7.431E-05 | 7.093E-05 | 7.018E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 |
| 56.118    | 58.592    | 58.629    | 59.491    | 59.791    | 69.609    | 71.370    | 78.715    | 78.865    | 81.675    |
| 3.42452   | 3.57544   | 3.57773   | 3.63032   | 3.64862   | 4.24775   | 4.35523   | 4.80343   | 4.81258   | 4.98409   |
| 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 |
| 83.174    | 87.334    | 87.446    | 87.784    | 89.133    | 89.620    | 90.482    | 91.643    | 91.793    | 93.067    |
| 5.07556   | 5.32939   | 5.33625   | 5.35683   | 5.43915   | 5.46888   | 5.52148   | 5.59236   | 5.60151   | 5.67926   |
| 1.746E-05 | 1.545E-05 | 1.328E-05 | 1.291E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 |           |
| 93.142    | 93.629    | 94.154    | 94.267    | 94.304    | 96.815    | 98.876    | 99.813    | 100.000   |           |
| 5.68384   | 5.71356   | 5.74558   | 5.75244   | 5.75472   | 5.90794   | 6.03371   | 6.09088   | 6.10231   |           |

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY



HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.129  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.344  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.586  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.048  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.419  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.244  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.352

| K | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|---|---|-------------|-------------|-------------|
| 3 | 1 | -6.09537    | -10.45028   | -1.08759    |
| 3 | 2 | -7.17293    | -11.28996   | -1.36624    |
| 3 | 3 | -7.59738    | -13.56830   | -2.20921    |
| 3 | 4 | -8.82336    | -11.35674   | -1.17952    |
| 3 | 5 | -8.94587    | -12.33076   | -1.65607    |
| 3 | 6 | -9.31262    | -14.51666   | -2.85548    |
| 3 | 7 | -9.59663    | -14.61973   | -2.91530    |
| 3 | 8 | -9.63092    | NUMXQ(K)= 8 |             |
|   |   | 9.754E-04   | 0.061       | 1.000       |
|   |   | 6.626E-04   | 0.183       | 3.000       |
|   |   | 5.299E-04   | 0.305       | 5.000       |
|   |   | 3.253E-04   | 0.610       | 10.000      |
|   |   | 2.352E-04   | 0.915       | 15.000      |
|   |   | 1.850E-04   | 1.220       | 20.000      |
|   |   | 1.526E-04   | 1.526       | 25.000      |
|   |   | 1.376E-04   | 1.831       | 30.000      |
|   |   | 1.267E-04   | 2.136       | 35.000      |
|   |   | 1.154E-04   | 2.441       | 40.000      |
|   |   | 1.061E-04   | 2.746       | 45.000      |
|   |   | 9.828E-05   | 3.051       | 50.000      |
|   |   | 9.160E-05   | 3.356       | 55.000      |
|   |   | 8.271E-05   | 3.661       | 60.000      |
|   |   | 7.445E-05   | 3.967       | 65.000      |
|   |   | 6.744E-05   | 4.272       | 70.000      |
|   |   | 3.794E-04   | 0.5         | 8.19        |

ANNUAL AVERAGE = 5.90E-06

K= 3 FIVEXQ(K)= 3.794E-04 FIVEPR(K)= 8.194

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WSW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN | HT     | EFF    | PLUME  | HT     | SIGMA-Y   | SIGMA-Z   | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |      |
|----------------|-----------|-----------|----------|---------|--------|--------|--------|--------|-----------|-----------|------------|-----------------------------------|-----------|------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS  | METERS | METERS | METERS | METERS | METERS    | METERS    | METERS     | MEANDER                           | BLDG WAKE | USED |
| AT 10.0 METERS |           |           |          |         |        |        |        |        |           |           |            | CA=1459.SQ.METERS                 |           |      |
| A              | 1.5       | 0.11      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 1.817E-05 | 1.746E-05 | 1.746E-05  |                                   |           |      |
| A              | 2.0       | 0.61      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 1.382E-05 | 1.328E-05 | 1.328E-05  |                                   |           |      |
| A              | 3.0       | 1.68      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 9.244E-06 | 8.882E-06 | 8.882E-06  |                                   |           |      |
| A              | 4.0       | 0.73      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 6.958E-06 | 6.686E-06 | 6.686E-06  |                                   |           |      |
| A              | 5.0       | 0.11      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 5.579E-06 | 5.361E-06 | 5.361E-06  |                                   |           |      |
| A              | 6.0       | 0.04      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 4.659E-06 | 4.477E-06 | 4.477E-06  |                                   |           |      |
|                |           |           |          |         |        |        |        |        |           |           |            |                                   |           |      |
| B              | 1.5       | 0.23      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 5.672E-05 | 5.032E-05 | 5.032E-05  |                                   |           |      |
| B              | 2.0       | 0.57      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 4.316E-05 | 3.829E-05 | 3.829E-05  |                                   |           |      |
| B              | 3.0       | 1.34      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 2.886E-05 | 2.560E-05 | 2.560E-05  |                                   |           |      |
| B              | 4.0       | 0.54      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 2.172E-05 | 1.927E-05 | 1.927E-05  |                                   |           |      |
| B              | 5.0       | 0.15      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 1.742E-05 | 1.545E-05 | 1.545E-05  |                                   |           |      |
| B              | 6.0       | 0.11      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 1.455E-05 | 1.291E-05 | 1.291E-05  |                                   |           |      |
|                |           |           |          |         |        |        |        |        |           |           |            |                                   |           |      |
| C              | 1.0       | 0.08      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 1.740E-04 | 1.376E-04 | 1.376E-04  |                                   |           |      |
| C              | 1.5       | 0.38      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 1.178E-04 | 9.321E-05 | 9.321E-05  |                                   |           |      |
| C              | 2.0       | 0.76      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 8.966E-05 | 7.093E-05 | 7.093E-05  |                                   |           |      |
| C              | 3.0       | 1.57      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 5.995E-05 | 4.743E-05 | 4.743E-05  |                                   |           |      |
| C              | 4.0       | 0.54      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 4.512E-05 | 3.570E-05 | 3.570E-05  |                                   |           |      |
| C              | 5.0       | 0.08      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 3.618E-05 | 2.862E-05 | 2.862E-05  |                                   |           |      |
|                |           |           |          |         |        |        |        |        |           |           |            |                                   |           |      |
| D              | 1.0       | 1.38      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 78.4   | 2.174E-04 | 2.620E-04 | 2.174E-04  |                                   |           |      |
| D              | 1.5       | 5.01      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 78.4   | 1.473E-04 | 1.774E-04 | 1.473E-04  |                                   |           |      |
| D              | 2.0       | 7.45      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 77.9   | 1.127E-04 | 1.350E-04 | 1.127E-04  |                                   |           |      |
| D              | 3.0       | 13.11     | 485.     | 0.      | 0.     | 39.2   | 18.0   | 60.4   | 9.715E-05 | 9.028E-05 | 9.028E-05  |                                   |           |      |
| D              | 4.0       | 7.76      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 50.5   | 8.749E-05 | 6.796E-05 | 6.796E-05  |                                   |           |      |
| D              | 5.0       | 3.52      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 43.9   | 8.063E-05 | 5.449E-05 | 5.449E-05  |                                   |           |      |
| D              | 6.0       | 0.76      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 39.2   | 7.545E-05 | 4.551E-05 | 4.551E-05  |                                   |           |      |
|                |           |           |          |         |        |        |        |        |           |           |            |                                   |           |      |
| E              | 0.4       | 0.02      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 83.6   | 8.570E-04 | 1.111E-03 | 8.570E-04  |                                   |           |      |
| E              | 1.0       | 4.74      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 83.6   | 2.917E-04 | 3.781E-04 | 2.917E-04  |                                   |           |      |
| E              | 1.5       | 10.05     | 485.     | 0.      | 0.     | 27.9   | 12.7   | 83.6   | 1.976E-04 | 2.560E-04 | 1.976E-04  |                                   |           |      |
| E              | 2.0       | 8.98      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 83.6   | 1.504E-04 | 1.948E-04 | 1.504E-04  |                                   |           |      |
| E              | 3.0       | 10.02     | 485.     | 0.      | 0.     | 27.9   | 12.7   | 55.9   | 1.503E-04 | 1.303E-04 | 1.303E-04  |                                   |           |      |
| E              | 4.0       | 3.71      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 42.1   | 1.503E-04 | 9.806E-05 | 9.806E-05  |                                   |           |      |
| E              | 5.0       | 1.30      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 33.8   | 1.503E-04 | 7.863E-05 | 7.863E-05  |                                   |           |      |
| E              | 5.9       | 0.57      | 485.     | 0.      | 0.     | 27.9   | 12.7   | 28.2   | 1.503E-04 | 6.567E-05 | 6.567E-05  |                                   |           |      |

|   |     |      |      |    |    |      |      |      |           |           |           |
|---|-----|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 7.9 | 0.23 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| F | 0.4 | 0.09 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0 | 4.36 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 2.87 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 0.42 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 0.15 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| G | 0.4 | 0.08 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 3.10 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 0.54 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0 | 0.11 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0 | 0.04 | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

WSW SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.079     | 0.174     | 0.194     | 3.290     | 3.825     | 3.864     | 8.221     | 8.336     | 11.203    | 15.943    |
| 0.00476   | 0.01042   | 0.01160   | 0.19683   | 0.22885   | 0.23113   | 0.49182   | 0.49868   | 0.67019   | 0.95375   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.504E-04 | 1.473E-04 | 1.376E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 16.363    | 16.516    | 17.892    | 27.945    | 36.928    | 41.936    | 42.012    | 52.027    | 59.481    | 63.189    |
| 0.97890   | 0.98805   | 1.07037   | 1.67179   | 2.20918   | 2.50875   | 2.51332   | 3.11245   | 3.55837   | 3.78018   |
| 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 |
| 63.571    | 76.683    | 77.982    | 78.747    | 86.506    | 87.080    | 90.597    | 90.826    | 91.055    | 92.623    |
| 3.80305   | 4.58741   | 4.66516   | 4.71090   | 5.17511   | 5.20941   | 5.41979   | 5.43351   | 5.44723   | 5.54099   |
| 4.551E-05 | 3.829E-05 | 3.570E-05 | 2.862E-05 | 2.560E-05 | 1.927E-05 | 1.746E-05 | 1.545E-05 | 1.328E-05 | 1.291E-05 |
| 93.387    | 93.960    | 94.496    | 94.572    | 95.910    | 96.445    | 96.560    | 96.713    | 97.324    | 97.439    |
| 5.58672   | 5.62103   | 5.65304   | 5.65761   | 5.73765   | 5.76967   | 5.77653   | 5.78567   | 5.82226   | 5.82912   |
| 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 |           |           |           |           |           |           |
| 99.121    | 99.847    | 99.962    | 100.000   |           |           |           |           |           |           |
| 5.92974   | 5.97319   | 5.98005   | 5.98233   |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.197  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.491  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 2.506  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 3.110  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 4.584  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 5.171  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 5.416

| K | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|---|---|-------------|-------------|-------------|
| 4 | 1 | -6.09537    | -10.22146   | -1.05722    |
| 4 | 2 | -7.17293    | -11.23096   | -1.40731    |
| 4 | 3 | -7.59738    | -12.67802   | -1.96777    |
| 4 | 4 | -8.82336    | -11.37733   | -1.30378    |
| 4 | 5 | -8.94587    | -12.78156   | -2.05674    |
| 4 | 6 | -9.31262    | -17.54883   | -4.88327    |
| 4 | 7 | -9.59663    | -25.46684   | -9.74554    |
| 4 | 8 | -9.81756    | NUMXQ(K)= 8 |             |
|   |   | 1.118E-03   | 0.060       | 1.000       |
|   |   | 7.909E-04   | 0.179       | 3.000       |
|   |   | 6.349E-04   | 0.299       | 5.000       |
|   |   | 4.386E-04   | 0.598       | 10.000      |
|   |   | 3.288E-04   | 0.897       | 15.000      |
|   |   | 2.656E-04   | 1.196       | 20.000      |
|   |   | 2.238E-04   | 1.496       | 25.000      |
|   |   | 1.938E-04   | 1.795       | 30.000      |
|   |   | 1.711E-04   | 2.094       | 35.000      |
|   |   | 1.532E-04   | 2.393       | 40.000      |
|   |   | 1.415E-04   | 2.692       | 45.000      |
|   |   | 1.333E-04   | 2.991       | 50.000      |
|   |   | 1.238E-04   | 3.290       | 55.000      |
|   |   | 1.142E-04   | 3.589       | 60.000      |
|   |   | 1.059E-04   | 3.889       | 65.000      |
|   |   | 9.864E-05   | 4.188       | 70.000      |
|   |   | 9.226E-05   | 4.487       | 75.000      |
|   |   | 8.177E-05   | 4.786       | 80.000      |
|   |   | 7.086E-05   | 5.085       | 85.000      |
|   |   | 5.624E-05   | 5.384       | 90.000      |
|   |   | 4.962E-04   | 0.5         | 8.36        |

ANNUAL AVERAGE = 7.88E-06

K= 4 FIVEXQ(K)= 4.962E-04 FIVEPR(K)= 8.358

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE W SECTOR.

| STABILITY | WINDSPEED      | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------|----------------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS     | METER/SEC      | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
|           | AT 10.0 METERS |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A         | 2.0            | 0.91      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A         | 3.0            | 1.96      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A         | 4.0            | 0.87      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A         | 5.0            | 0.35      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| B         | 1.5            | 0.26      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B         | 2.0            | 0.87      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B         | 3.0            | 1.26      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B         | 4.0            | 0.65      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B         | 5.0            | 0.17      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| C         | 1.0            | 0.04      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.740E-04                         | 1.376E-04 | 1.376E-04 |
| C         | 1.5            | 0.43      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C         | 2.0            | 1.04      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C         | 3.0            | 2.13      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C         | 4.0            | 0.70      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C         | 5.0            | 0.17      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| D         | 1.0            | 1.00      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D         | 1.5            | 5.57      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D         | 2.0            | 7.13      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D         | 3.0            | 8.57      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D         | 4.0            | 4.61      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D         | 5.0            | 1.13      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D         | 6.0            | 0.13      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D         | 8.0            | 0.04      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| E         | 0.4            | 0.03      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E         | 1.0            | 6.09      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E         | 1.5            | 12.39     | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |
| E         | 2.0            | 8.74      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |
| E         | 3.0            | 7.61      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |
| E         | 4.0            | 2.43      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 42.1       | 1.503E-04                         | 9.806E-05 | 9.806E-05 |
| E         | 5.0            | 0.57      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 33.8       | 1.503E-04                         | 7.863E-05 | 7.863E-05 |
| E         | 5.9            | 0.09      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 28.2       | 1.503E-04                         | 6.567E-05 | 6.567E-05 |
| F         | 0.4            | 0.14      | 485.     | 0.         | 0.           | 19.2    | 8.0     | 76.9       | 1.474E-03                         | 1.965E-03 | 1.474E-03 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  |  | PAGE NO. 27 of 160 |  |
|--|--|--|--|-------------------|--|---------------|--|--|--|--------------------|--|
|--|--|--|--|-------------------|--|---------------|--|--|--|--------------------|--|

|   |     |      |      |    |    |      |     |      |           |           |           |
|---|-----|------|------|----|----|------|-----|------|-----------|-----------|-----------|
| F | 1.0 | 6.22 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 6.26 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 1.22 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 0.26 | 485. | 0. | 0. | 19.2 | 8.0 | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
|   |     |      |      |    |    |      |     |      |           |           |           |
| G | 0.4 | 0.10 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 3.96 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 2.83 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0 | 1.09 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

W SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED  
AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 | 2.586E-04 |
| 0.102     | 0.237     | 0.262     | 4.219     | 7.045     | 13.262    | 14.349    | 20.610    | 26.697    | 27.914    |
| 0.00534   | 0.01245   | 0.01379   | 0.22188   | 0.37052   | 0.69753   | 0.75470   | 1.08399   | 1.40414   | 1.46817   |
| 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.504E-04 | 1.473E-04 | 1.376E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 | 9.321E-05 |
| 28.175    | 29.175    | 41.566    | 50.305    | 55.870    | 55.914    | 63.522    | 70.653    | 73.087    | 73.522    |
| 1.48189   | 1.53448   | 2.18621   | 2.64585   | 2.93855   | 2.94084   | 3.34102   | 3.71605   | 3.84411   | 3.86698   |
| 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.743E-05 | 4.551E-05 | 3.829E-05 |
| 82.087    | 82.652    | 83.696    | 88.304    | 88.391    | 89.522    | 89.783    | 91.913    | 92.044    | 92.913    |
| 4.31747   | 4.34720   | 4.40208   | 4.64447   | 4.64905   | 4.70850   | 4.72222   | 4.83427   | 4.84114   | 4.88687   |
| 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.560E-05 | 1.927E-05 | 1.545E-05 | 1.328E-05 | 8.882E-06 | 6.686E-06 | 5.361E-06 |
| 93.609    | 93.652    | 93.826    | 95.087    | 95.739    | 95.913    | 96.826    | 98.783    | 99.652    | 100.000   |
| 4.92346   | 4.92575   | 4.93489   | 5.00121   | 5.03551   | 5.04466   | 5.09268   | 5.19558   | 5.24132   | 5.25961   |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

|                  |                                    |             |       |
|------------------|------------------------------------|-------------|-------|
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE ( 2)= | 0.222 |
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE ( 3)= | 0.697 |
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE ( 4)= | 1.403 |



HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.184  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.338  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.713  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.314  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.641

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 5 | 1 | -6.09537     | -10.15304   | -1.04727     |
| 5 | 2 | -7.17293     | -10.29679   | -1.09778     |
| 5 | 3 | -7.59738     | -12.67897   | -2.06656     |
| 5 | 4 | -8.13962     | -12.91134   | -2.17235     |
| 5 | 5 | -8.52936     | -13.09867   | -2.26522     |
| 5 | 6 | -8.94587     | -14.44510   | -2.99965     |
| 5 | 7 | -9.09063     | -14.77800   | -3.18615     |
| 5 | 8 | -9.31262     | -23.37688   | -8.19903     |
| 5 | 9 | -9.59663     | NUMXQ(K)= 9 |              |
|   |   | 1.205E-03    | 0.053       | 1.000        |
|   |   | 8.579E-04    | 0.158       | 3.000        |
|   |   | 7.225E-04    | 0.263       | 5.000        |
|   |   | 5.598E-04    | 0.526       | 10.000       |
|   |   | 4.576E-04    | 0.789       | 15.000       |
|   |   | 3.671E-04    | 1.052       | 20.000       |
|   |   | 3.076E-04    | 1.315       | 25.000       |
|   |   | 2.639E-04    | 1.578       | 30.000       |
|   |   | 2.306E-04    | 1.841       | 35.000       |
|   |   | 2.046E-04    | 2.104       | 40.000       |
|   |   | 1.832E-04    | 2.367       | 45.000       |
|   |   | 1.654E-04    | 2.630       | 50.000       |
|   |   | 1.506E-04    | 2.893       | 55.000       |
|   |   | 1.380E-04    | 3.156       | 60.000       |
|   |   | 1.263E-04    | 3.419       | 65.000       |
|   |   | 1.142E-04    | 3.682       | 70.000       |
|   |   | 1.033E-04    | 3.945       | 75.000       |
|   |   | 9.383E-05    | 4.208       | 80.000       |
|   |   | 7.887E-05    | 4.471       | 85.000       |
|   |   | 5.707E-04    | 0.5         | 9.51         |

ANNUAL AVERAGE = 8.80E-06

K= 5 FIVEXQ(K)= 5.707E-04 FIVEPR(K)= 9.506

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WNW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE          | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|-------------------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS            | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           | CA=1459.SQ.METERS |            |              |         |         |            |                                   |           |           |
| A              | 1.5       | 0.05      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |
| A              | 2.0       | 0.29      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 1.37      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 0.69      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 0.34      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.15      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.05      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.59      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.33      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 0.49      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.05      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.29      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.88      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.72      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 0.49      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 6.0       | 0.20      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.34      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 2.11      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 4.57      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 8.15      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 4.37      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 2.80      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 1.57      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 0.34      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| E              | 0.4       | 0.01      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E              | 1.0       | 1.67      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E              | 1.5       | 7.81      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |
| E              | 2.0       | 9.43      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |
| E              | 3.0       | 13.21     | 485.              | 0.         | 0.           | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |
| E              | 4.0       | 4.32      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 42.1       | 1.503E-04                         | 9.806E-05 | 9.806E-05 |
| E              | 5.0       | 2.46      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 33.8       | 1.503E-04                         | 7.863E-05 | 7.863E-05 |
| E              | 5.9       | 1.23      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 28.2       | 1.503E-04                         | 6.567E-05 | 6.567E-05 |
| E              | 7.9       | 0.15      | 485.              | 0.         | 0.           | 27.9    | 12.7    | 27.9       | 1.142E-04                         | 4.933E-05 | 4.933E-05 |

|   |     |      |      |    |    |      |     |      |           |           |           |
|---|-----|------|------|----|----|------|-----|------|-----------|-----------|-----------|
| F | 0.4 | 0.06 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0 | 2.95 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 7.22 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 7.37 | 485. | 0. | 0. | 19.2 | 8.0 | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 2.41 | 485. | 0. | 0. | 19.2 | 8.0 | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0 | 0.05 | 485. | 0. | 0. | 19.2 | 8.0 | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
|   |     |      |      |    |    |      |     |      |           |           |           |
| G | 0.4 | 0.06 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 2.26 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 2.36 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0 | 1.47 | 485. | 0. | 0. | 13.3 | 5.1 | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0 | 0.29 | 485. | 0. | 0. | 13.3 | 5.1 | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

WNW SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED  
AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.058     | 0.122     | 0.129     | 2.388     | 4.744     | 5.039     | 7.985     | 9.458     | 16.676    | 18.345    |
| 0.00270   | 0.00568   | 0.00601   | 0.11120   | 0.22096   | 0.23468   | 0.37189   | 0.44049   | 0.77665   | 0.85440   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 25.710    | 28.116    | 28.460    | 36.267    | 36.316    | 45.744    | 47.855    | 61.063    | 65.629    | 69.950    |
| 1.19741   | 1.30946   | 1.32547   | 1.68906   | 1.69135   | 2.13041   | 2.22874   | 2.84388   | 3.05654   | 3.25778   |
| 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 |
| 70.245    | 78.396    | 80.851    | 81.734    | 86.104    | 87.332    | 90.131    | 90.180    | 90.327    | 92.046    |
| 3.27150   | 3.65110   | 3.76544   | 3.80660   | 4.01012   | 4.06729   | 4.19764   | 4.19992   | 4.20678   | 4.28682   |
| 4.551E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.746E-05 | 1.545E-05 | 1.328E-05 |
| 93.617    | 94.206    | 94.697    | 95.041    | 96.367    | 96.563    | 97.054    | 97.103    | 97.152    | 97.447    |
| 4.36000   | 4.38744   | 4.41031   | 4.42631   | 4.48806   | 4.49720   | 4.52007   | 4.52236   | 4.52464   | 4.53836   |
| 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 |           |           |           |           |           |           |
| 98.822    | 99.509    | 99.853    | 100.000   |           |           |           |           |           |           |
| 4.60239   | 4.63441   | 4.65042   | 4.65728   |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.111  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.371  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.776  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.196  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.841  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.648  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.064  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.356

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 6 | 1 | -6.09537     | -10.54085   | -1.10103     |
| 6 | 2 | -7.17293     | -10.57265   | -1.11143     |
| 6 | 3 | -7.59738     | -11.65968   | -1.51750     |
| 6 | 4 | -7.98712     | -12.07465   | -1.68897     |
| 6 | 5 | -8.26029     | -12.63744   | -1.93816     |
| 6 | 6 | -8.94587     | -15.20629   | -3.28687     |
| 6 | 7 | -9.31262     | -20.77899   | -6.39474     |
| 6 | 8 | -9.63092     | -29.25344   | -11.25585    |
| 6 | 9 | -9.99767     | NUMXQ(K)= 9 |              |
|   |   | 1.012E-03    | 0.047       | 1.000        |
|   |   | 7.104E-04    | 0.140       | 3.000        |
|   |   | 5.949E-04    | 0.233       | 5.000        |
|   |   | 4.469E-04    | 0.466       | 10.000       |
|   |   | 3.601E-04    | 0.699       | 15.000       |
|   |   | 3.035E-04    | 0.931       | 20.000       |
|   |   | 2.633E-04    | 1.164       | 25.000       |
|   |   | 2.302E-04    | 1.397       | 30.000       |
|   |   | 2.045E-04    | 1.630       | 35.000       |
|   |   | 1.842E-04    | 1.863       | 40.000       |
|   |   | 1.676E-04    | 2.096       | 45.000       |
|   |   | 1.539E-04    | 2.329       | 50.000       |
|   |   | 1.422E-04    | 2.562       | 55.000       |
|   |   | 1.322E-04    | 2.794       | 60.000       |
|   |   | 1.190E-04    | 3.027       | 65.000       |
|   |   | 1.068E-04    | 3.260       | 70.000       |
|   |   | 9.645E-05    | 3.493       | 75.000       |
|   |   | 8.508E-05    | 3.726       | 80.000       |
|   |   | 7.116E-05    | 3.959       | 85.000       |
|   |   | 5.606E-05    | 4.192       | 90.000       |
|   |   | 4.306E-04    | 0.5         | 10.74        |

ANNUAL AVERAGE = 6.28E-06

K= 6 FIVEXQ(K)= 4.306E-04 FIVEPR(K)=10.736

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     |                                   |           |           |      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            |                                   |           |           |      |
| A              | 1.5       | 0.14      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |      |
| A              | 2.0       | 0.64      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |      |
| A              | 3.0       | 1.47      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |      |
| A              | 4.0       | 0.87      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |      |
| A              | 5.0       | 0.28      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |      |
| A              | 6.0       | 0.09      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |      |
| A              | 8.0       | 0.32      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| B              | 1.5       | 0.05      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |      |
| B              | 2.0       | 0.46      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |      |
| B              | 3.0       | 1.47      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |      |
| B              | 4.0       | 0.55      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |      |
| B              | 5.0       | 0.32      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |      |
| B              | 8.0       | 0.23      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| C              | 1.0       | 0.05      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.740E-04                         | 1.376E-04 | 1.376E-04 |      |
| C              | 1.5       | 0.23      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |      |
| C              | 2.0       | 0.60      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |      |
| C              | 3.0       | 1.79      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |      |
| C              | 4.0       | 0.73      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |      |
| C              | 5.0       | 0.41      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |      |
| C              | 6.0       | 0.23      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |      |
| C              | 8.0       | 0.23      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| D              | 1.0       | 0.18      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |      |
| D              | 1.5       | 1.10      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |      |
| D              | 2.0       | 3.03      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |      |
| D              | 3.0       | 8.72      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |      |
| D              | 4.0       | 6.06      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |      |
| D              | 5.0       | 4.45      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |      |
| D              | 6.0       | 3.72      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |      |
| D              | 8.0       | 1.79      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| E              | 0.4       | 0.00      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |      |
| E              | 1.0       | 0.96      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |      |
| E              | 1.5       | 2.75      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |      |
| E              | 2.0       | 5.74      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |      |

CA=1459.SQ.METERS

|   |     |       |      |    |    |      |      |      |           |           |           |
|---|-----|-------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 3.0 | 16.30 | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0 | 11.66 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0 | 4.59  | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9 | 1.70  | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9 | 1.61  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8 | 0.09  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| F | 0.4 | 0.03  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0 | 1.47  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 3.12  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 3.53  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 3.26  | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0 | 0.23  | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 5.0 | 0.05  | 485. | 0. | 0. | 19.2 | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04 |
| G | 0.4 | 0.03  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 1.24  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 0.69  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0 | 0.50  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0 | 0.23  | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

NW SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.032     | 0.064     | 0.068     | 1.307     | 1.996     | 2.225     | 3.694     | 4.199     | 7.321     | 8.285     |
| 0.00159   | 0.00318   | 0.00338   | 0.06512   | 0.09942   | 0.11085   | 0.18403   | 0.20918   | 0.36468   | 0.41271   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 | 1.376E-04 | 1.303E-04 |
| 11.819    | 15.078    | 15.262    | 18.016    | 18.246    | 23.984    | 25.085    | 25.131    | 25.177    | 41.473    |
| 0.58879   | 0.75115   | 0.76029   | 0.89750   | 0.90893   | 1.19478   | 1.24966   | 1.25195   | 1.25423   | 2.06603   |
| 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 |
| 44.503    | 56.162    | 56.392    | 65.113    | 69.704    | 70.300    | 76.360    | 78.058    | 82.511    | 82.557    |
| 2.21696   | 2.79780   | 2.80923   | 3.24371   | 3.47239   | 3.50212   | 3.80397   | 3.88858   | 4.11040   | 4.11268   |
| 4.933E-05 | 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.560E-05 | 2.391E-05 |
| 84.163    | 85.954    | 89.672    | 89.764    | 90.223    | 90.957    | 92.747    | 93.160    | 94.629    | 94.859    |
| 4.19272   | 4.28190   | 4.46713   | 4.47170   | 4.49457   | 4.53116   | 4.62034   | 4.64092   | 4.71410   | 4.72553   |
| 1.927E-05 | 1.796E-05 | 1.746E-05 | 1.545E-05 | 1.328E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 |
| 95.410    | 95.639    | 95.777    | 96.098    | 96.741    | 96.970    | 98.439    | 99.311    | 99.587    | 99.679    |
| 4.75298   | 4.76441   | 4.77127   | 4.78728   | 4.81929   | 4.83073   | 4.90390   | 4.94735   | 4.96107   | 4.96564   |
| 3.363E-06 |           |           |           |           |           |           |           |           |           |
| 100.000   |           |           |           |           |           |           |           |           |           |
| 4.98165   |           |           |           |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.065  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.184  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.750  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 2.064  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.241  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 3.885  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 4.464

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 7 | 1 | -6.09537     | -10.83923   | -1.14012     |
| 7 | 2 | -7.17293     | -11.56089   | -1.36454     |
| 7 | 3 | -7.59738     | -12.38026   | -1.64663     |
| 7 | 4 | -8.37525     | -11.92020   | -1.45748     |
| 7 | 5 | -8.94587     | -12.79981   | -1.88850     |
| 7 | 6 | -9.31262     | -16.44752   | -3.86394     |
| 7 | 7 | -9.63092     | -19.59900   | -5.65033     |
| 7 | 8 | -9.99767     | NUMXQ(K)= 8 |              |
|   |   | 8.366E-04    | 0.050       | 1.000        |
|   |   | 5.480E-04    | 0.149       | 3.000        |
|   |   | 4.283E-04    | 0.249       | 5.000        |
|   |   | 2.928E-04    | 0.498       | 10.000       |
|   |   | 2.312E-04    | 0.747       | 15.000       |
|   |   | 1.981E-04    | 0.996       | 20.000       |
|   |   | 1.750E-04    | 1.245       | 25.000       |
|   |   | 1.577E-04    | 1.494       | 30.000       |
|   |   | 1.442E-04    | 1.744       | 35.000       |
|   |   | 1.331E-04    | 1.993       | 40.000       |
|   |   | 1.221E-04    | 2.242       | 45.000       |
|   |   | 1.123E-04    | 2.491       | 50.000       |
|   |   | 1.039E-04    | 2.740       | 55.000       |
|   |   | 9.668E-05    | 2.989       | 60.000       |
|   |   | 9.041E-05    | 3.238       | 65.000       |
|   |   | 7.961E-05    | 3.487       | 70.000       |
|   |   | 7.050E-05    | 3.736       | 75.000       |
|   |   | 6.158E-05    | 3.985       | 80.000       |
|   |   | 5.248E-05    | 4.234       | 85.000       |
|   |   | 2.922E-04    | 0.5         | 10.04        |

ANNUAL AVERAGE = 4.50E-06

K= 7 FIVEXQ(K)= 2.922E-04 FIVEPR(K)=10.037

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 1.5       | 0.07      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |
| A              | 2.0       | 0.25      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 1.79      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.33      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 0.35      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.25      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.42      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
| A              | 9.9       | 0.11      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 2.814E-06                         | 2.704E-06 | 2.704E-06 |
| A              | 24.3      | 0.04      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.146E-06                         | 1.101E-06 | 1.101E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.11      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.39      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.02      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 0.67      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.53      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.28      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.39      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| B              | 9.9       | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.786E-06                         | 7.796E-06 | 7.796E-06 |
| B              | 24.3      | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 3.578E-06                         | 3.175E-06 | 3.175E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.07      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.49      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.44      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.23      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 0.46      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.67      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.49      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C              | 9.9       | 0.04      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
| C              | 24.3      | 0.04      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 7.433E-06                         | 5.881E-06 | 5.881E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.14      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 0.67      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 1.89      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 7.12      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 7.61      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 5.16      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 4.67      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B | APPENDIX BB-7 |  |  |  | PAGE NO. 39 of 160 |
|--|--|--|--|--|--|-------------------|---------------|--|--|--|--------------------|
|--|--|--|--|--|--|-------------------|---------------|--|--|--|--------------------|

|   |      |       |      |    |    |      |      |      |           |           |           |
|---|------|-------|------|----|----|------|------|------|-----------|-----------|-----------|
| D | 8.0  | 3.75  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 5.674E-05 | 3.419E-05 | 3.419E-05 |
| D | 9.9  | 0.63  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 4.562E-05 | 2.749E-05 | 2.749E-05 |
| D | 24.3 | 0.11  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 1.858E-05 | 1.119E-05 | 1.119E-05 |
| E | 0.4  | 0.00  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 8.570E-04 | 1.111E-03 | 8.570E-04 |
| E | 1.0  | 0.46  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 2.917E-04 | 3.781E-04 | 2.917E-04 |
| E | 1.5  | 1.33  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.976E-04 | 2.560E-04 | 1.976E-04 |
| E | 2.0  | 3.68  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 14.80 | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 11.12 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 7.82  | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 4.77  | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 2.70  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 0.18  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.35  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
| F | 0.4  | 0.02  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 0.81  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 1.26  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 1.54  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 2.53  | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 0.95  | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 5.0  | 0.04  | 485. | 0. | 0. | 19.2 | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04 |
| G | 0.4  | 0.02  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 0.63  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 0.14  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.04  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.11  | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |
| G | 4.0  | 0.04  | 485. | 0. | 0. | 13.3 | 5.1  | 26.0 | 6.091E-04 | 3.979E-04 | 3.979E-04 |



X/Q PERCENTILES  
 (BASED ON THE UPPER ENVELOPE OF THE  
 ORDERED X/Q-FREQUENCY VALUES, AND AS  
 PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

|   |            |       |
|---|------------|-------|
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 2)= | 0.043 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 3)= | 0.112 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 4)= | 0.493 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 5)= | 1.901 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 6)= | 3.217 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 7)= | 4.565 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 8)= | 5.482 |
| HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 9)= | 5.843 |

| K            | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |        |
|--------------|---|--------------|-------------|--------------|--------|
| 8            | 1 | -6.09537     | -11.06175   | -1.16788     |        |
| 8            | 2 | -7.17293     | -12.34358   | -1.55283     |        |
| 8            | 3 | -7.59738     | -12.59159   | -1.63398     |        |
| 8            | 4 | -8.37525     | -11.28701   | -1.12841     |        |
| 8            | 5 | -8.94587     | -12.32935   | -1.63081     |        |
| 8            | 6 | -9.31262     | -12.96288   | -1.97328     |        |
| 8            | 7 | -9.63092     | -16.60936   | -4.13283     |        |
| 8            | 8 | -9.99767     | -24.41187   | -9.01002     |        |
| 8            | 9 | -10.28369    |             |              |        |
| NUMXQ(K) = 9 |   |              |             |              |        |
|              |   | 6.422E-04    | 0.065       |              | 1.000  |
|              |   | 3.795E-04    | 0.196       |              | 3.000  |
|              |   | 2.899E-04    | 0.326       |              | 5.000  |
|              |   | 2.065E-04    | 0.652       |              | 10.000 |
|              |   | 1.748E-04    | 0.978       |              | 15.000 |
|              |   | 1.544E-04    | 1.304       |              | 20.000 |
|              |   | 1.398E-04    | 1.630       |              | 25.000 |
|              |   | 1.279E-04    | 1.956       |              | 30.000 |
|              |   | 1.152E-04    | 2.282       |              | 35.000 |
|              |   | 1.050E-04    | 2.608       |              | 40.000 |
|              |   | 9.655E-05    | 2.934       |              | 45.000 |
|              |   | 8.930E-05    | 3.260       |              | 50.000 |
|              |   | 8.204E-05    | 3.586       |              | 55.000 |
|              |   | 7.582E-05    | 3.912       |              | 60.000 |
|              |   | 7.044E-05    | 4.238       |              | 65.000 |
|              |   | 6.574E-05    | 4.564       |              | 70.000 |
|              |   | 5.741E-05    | 4.890       |              | 75.000 |
|              |   | 5.043E-05    | 5.216       |              | 80.000 |
|              |   | 4.350E-05    | 5.542       |              | 85.000 |
|              |   |              |             |              |        |
|              |   | 2.294E-04    | 0.5         |              | 7.67   |

ANNUAL AVERAGE = 4.28E-06

K= 8      FIVEXQ(K) = 2.294E-04      FIVEPR(K) = 7.669

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE N SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 2.0       | 0.24      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 1.61      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.12      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 1.08      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.73      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.63      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
| A              | 9.9       | 0.21      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 2.814E-06                         | 2.704E-06 | 2.704E-06 |
| A              | 24.3      | 0.10      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.146E-06                         | 1.101E-06 | 1.101E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.14      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.17      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 0.73      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 0.66      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.70      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.77      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.31      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| B              | 9.9       | 0.21      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.786E-06                         | 7.796E-06 | 7.796E-06 |
| B              | 24.3      | 0.03      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 3.578E-06                         | 3.175E-06 | 3.175E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.14      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.45      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 0.70      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 0.94      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 0.94      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.59      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.63      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C              | 9.9       | 0.07      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.10      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 0.42      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 1.22      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 4.02      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 4.48      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 5.42      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 5.00      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 7.17      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D              | 9.9       | 2.10      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |

|   |      |       |      |    |    |      |      |      |           |           |           |
|---|------|-------|------|----|----|------|------|------|-----------|-----------|-----------|
| D | 24.3 | 0.45  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 1.858E-05 | 1.119E-05 | 1.119E-05 |
| E | 0.4  | 0.00  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 8.570E-04 | 1.111E-03 | 8.570E-04 |
| E | 1.0  | 0.35  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 2.917E-04 | 3.781E-04 | 2.917E-04 |
| E | 1.5  | 0.66  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.976E-04 | 2.560E-04 | 1.976E-04 |
| E | 2.0  | 1.92  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 8.15  | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 11.15 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 10.84 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 7.55  | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 6.47  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 2.83  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.42  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
|   |      |       |      |    |    |      |      |      |           |           |           |
| F | 0.4  | 0.01  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 0.59  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 0.56  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 0.73  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 1.50  | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 0.59  | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 5.0  | 0.24  | 485. | 0. | 0. | 19.2 | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04 |
|   |      |       |      |    |    |      |      |      |           |           |           |
| G | 0.4  | 0.01  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 0.45  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 0.31  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.14  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.07  | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |
| G | 4.0  | 0.07  | 485. | 0. | 0. | 13.3 | 5.1  | 26.0 | 6.091E-04 | 3.979E-04 | 3.979E-04 |



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### SITE EXCLUSION BOUNDARY CALCULATIONS:

N SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.012     | 0.025     | 0.026     | 0.481     | 0.795     | 0.865     | 1.460     | 1.530     | 1.670     | 2.229     |
| 0.00076   | 0.00161   | 0.00170   | 0.03143   | 0.05201   | 0.05659   | 0.09546   | 0.10003   | 0.10918   | 0.14577   |
| 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 | 1.303E-04 |
| 2.579     | 3.313     | 4.817     | 4.922     | 5.586     | 6.180     | 8.104     | 8.523     | 8.768     | 16.916    |
| 0.16864   | 0.21666   | 0.31499   | 0.32185   | 0.36530   | 0.40417   | 0.52995   | 0.55739   | 0.57339   | 1.10621   |
| 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 |
| 18.140    | 29.294    | 29.434    | 33.456    | 44.296    | 44.750    | 49.226    | 56.779    | 62.199    | 62.339    |
| 1.18625   | 1.91572   | 1.92487   | 2.18785   | 2.89674   | 2.92647   | 3.21917   | 3.71311   | 4.06756   | 4.07671   |
| 4.933E-05 | 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 |
| 68.808    | 69.508    | 74.508    | 77.341    | 77.515    | 78.460    | 85.628    | 86.572    | 88.670    | 89.405    |
| 4.49976   | 4.54550   | 4.87250   | 5.05773   | 5.06916   | 5.13091   | 5.59969   | 5.66143   | 5.79864   | 5.84666   |
| 2.391E-05 | 1.927E-05 | 1.796E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 |
| 89.999    | 90.664    | 91.293    | 91.713    | 92.412    | 92.482    | 92.727    | 93.496    | 93.951    | 94.265    |
| 5.88554   | 5.92898   | 5.97015   | 5.99759   | 6.04332   | 6.04790   | 6.06390   | 6.11421   | 6.14394   | 6.16452   |
| 8.882E-06 | 7.796E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 | 3.175E-06 | 2.704E-06 | 1.101E-06 |           |
| 95.874    | 96.084    | 97.203    | 98.287    | 99.021    | 99.650    | 99.685    | 99.895    | 100.000   |           |
| 6.26971   | 6.28343   | 6.35661   | 6.42750   | 6.47552   | 6.51668   | 6.51897   | 6.53269   | 6.53955   |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.031  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.095  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.315  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.105  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.894  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.710  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.869  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.596

| K | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|---|---|-------------|-------------|-------------|
| 9 | 1 | -6.09537    | -11.24127   | -1.18987    |
| 9 | 2 | -7.17293    | -11.78222   | -1.34808    |
| 9 | 3 | -7.59738    | -14.08581   | -2.09015    |
| 9 | 4 | -8.37525    | -11.89082   | -1.28675    |
| 9 | 5 | -8.94587    | -11.89352   | -1.28793    |
| 9 | 6 | -9.45081    | -12.52216   | -1.61939    |
| 9 | 7 | -9.63092    | -14.75899   | -2.87223    |
| 9 | 8 | -9.99767    | -16.96269   | -4.20160    |
| 9 | 9 | -10.28369   | NUMXQ(K)= 9 |             |
|   |   | 5.821E-04   | 0.065       | 1.000       |
|   |   | 3.170E-04   | 0.196       | 3.000       |
|   |   | 2.269E-04   | 0.327       | 5.000       |
|   |   | 1.671E-04   | 0.654       | 10.000      |
|   |   | 1.381E-04   | 0.981       | 15.000      |
|   |   | 1.199E-04   | 1.308       | 20.000      |
|   |   | 1.070E-04   | 1.635       | 25.000      |
|   |   | 9.731E-05   | 1.962       | 30.000      |
|   |   | 8.958E-05   | 2.289       | 35.000      |
|   |   | 8.325E-05   | 2.616       | 40.000      |
|   |   | 7.775E-05   | 2.943       | 45.000      |
|   |   | 7.208E-05   | 3.270       | 50.000      |
|   |   | 6.723E-05   | 3.597       | 55.000      |
|   |   | 6.105E-05   | 3.924       | 60.000      |
|   |   | 5.484E-05   | 4.251       | 65.000      |
|   |   | 4.959E-05   | 4.578       | 70.000      |
|   |   | 4.490E-05   | 4.905       | 75.000      |
|   |   | 3.936E-05   | 5.232       | 80.000      |
|   |   | 3.471E-05   | 5.559       | 85.000      |
|   |   | 1.886E-04   | 0.5         | 7.65        |

ANNUAL AVERAGE = 3.43E-06

K= 9 FIVEXQ(K)= 1.886E-04 FIVEPR(K)= 7.646

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNE SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN | HT     | EFF    | PLUME  | HT     | SIGMA-Y   | SIGMA-Z   | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |      |
|----------------|-----------|-----------|----------|---------|--------|--------|--------|--------|-----------|-----------|------------|-----------------------------------|-----------|------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS  | METERS | METERS | METERS | METERS | METERS    | METERS    | METERS     | MEANDER                           | BLDG WAKE | USED |
| AT 10.0 METERS |           |           |          |         |        |        |        |        |           |           |            | CA=1459.SQ.METERS                 |           |      |
| A              | 1.5       | 0.09      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 1.817E-05 | 1.746E-05 | 1.746E-05  |                                   |           |      |
| A              | 2.0       | 0.24      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 1.382E-05 | 1.328E-05 | 1.328E-05  |                                   |           |      |
| A              | 3.0       | 0.71      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 9.244E-06 | 8.882E-06 | 8.882E-06  |                                   |           |      |
| A              | 4.0       | 0.92      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 6.958E-06 | 6.686E-06 | 6.686E-06  |                                   |           |      |
| A              | 5.0       | 1.83      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 5.579E-06 | 5.361E-06 | 5.361E-06  |                                   |           |      |
| A              | 6.0       | 0.80      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 4.659E-06 | 4.477E-06 | 4.477E-06  |                                   |           |      |
| A              | 8.0       | 0.95      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 3.500E-06 | 3.363E-06 | 3.363E-06  |                                   |           |      |
| A              | 9.9       | 0.06      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 2.814E-06 | 2.704E-06 | 2.704E-06  |                                   |           |      |
| A              | 24.3      | 0.21      | 485.     | 0.      | 0.     | 97.4   | 117.1  | 97.4   | 1.146E-06 | 1.101E-06 | 1.101E-06  |                                   |           |      |
| B              | 2.0       | 0.12      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 4.316E-05 | 3.829E-05 | 3.829E-05  |                                   |           |      |
| B              | 3.0       | 0.62      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 2.886E-05 | 2.560E-05 | 2.560E-05  |                                   |           |      |
| B              | 4.0       | 0.80      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 2.172E-05 | 1.927E-05 | 1.927E-05  |                                   |           |      |
| B              | 5.0       | 0.83      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 1.742E-05 | 1.545E-05 | 1.545E-05  |                                   |           |      |
| B              | 6.0       | 0.59      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 1.455E-05 | 1.291E-05 | 1.291E-05  |                                   |           |      |
| B              | 8.0       | 0.50      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 1.093E-05 | 9.696E-06 | 9.696E-06  |                                   |           |      |
| B              | 9.9       | 0.06      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 8.786E-06 | 7.796E-06 | 7.796E-06  |                                   |           |      |
| B              | 24.3      | 0.06      | 485.     | 0.      | 0.     | 73.3   | 49.9   | 73.3   | 3.578E-06 | 3.175E-06 | 3.175E-06  |                                   |           |      |
| C              | 1.5       | 0.06      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 1.178E-04 | 9.321E-05 | 9.321E-05  |                                   |           |      |
| C              | 2.0       | 0.32      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 8.966E-05 | 7.093E-05 | 7.093E-05  |                                   |           |      |
| C              | 3.0       | 0.68      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 5.995E-05 | 4.743E-05 | 4.743E-05  |                                   |           |      |
| C              | 4.0       | 1.03      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 4.512E-05 | 3.570E-05 | 3.570E-05  |                                   |           |      |
| C              | 5.0       | 0.92      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 3.618E-05 | 2.862E-05 | 2.862E-05  |                                   |           |      |
| C              | 6.0       | 0.86      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 3.022E-05 | 2.391E-05 | 2.391E-05  |                                   |           |      |
| C              | 8.0       | 1.03      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 2.270E-05 | 1.796E-05 | 1.796E-05  |                                   |           |      |
| C              | 9.9       | 0.30      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 1.825E-05 | 1.444E-05 | 1.444E-05  |                                   |           |      |
| C              | 24.3      | 0.18      | 485.     | 0.      | 0.     | 55.6   | 31.6   | 55.6   | 7.433E-06 | 5.881E-06 | 5.881E-06  |                                   |           |      |
| D              | 1.0       | 0.03      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 78.4   | 2.174E-04 | 2.620E-04 | 2.174E-04  |                                   |           |      |
| D              | 1.5       | 0.35      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 78.4   | 1.473E-04 | 1.774E-04 | 1.473E-04  |                                   |           |      |
| D              | 2.0       | 1.18      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 77.9   | 1.127E-04 | 1.350E-04 | 1.127E-04  |                                   |           |      |
| D              | 3.0       | 2.87      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 60.4   | 9.715E-05 | 9.028E-05 | 9.028E-05  |                                   |           |      |
| D              | 4.0       | 4.43      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 50.5   | 8.749E-05 | 6.796E-05 | 6.796E-05  |                                   |           |      |
| D              | 5.0       | 5.29      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 43.9   | 8.063E-05 | 5.449E-05 | 5.449E-05  |                                   |           |      |
| D              | 6.0       | 5.29      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 39.2   | 7.545E-05 | 4.551E-05 | 4.551E-05  |                                   |           |      |
| D              | 8.0       | 7.47      | 485.     | 0.      | 0.     | 39.2   | 18.0   | 39.2   | 5.674E-05 | 3.419E-05 | 3.419E-05  |                                   |           |      |

|   |      |       |      |    |    |      |      |      |           |           |           |
|---|------|-------|------|----|----|------|------|------|-----------|-----------|-----------|
| D | 9.9  | 3.28  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 4.562E-05 | 2.749E-05 | 2.749E-05 |
| D | 24.3 | 0.47  | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 1.858E-05 | 1.119E-05 | 1.119E-05 |
| E | 0.4  | 0.00  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 8.570E-04 | 1.111E-03 | 8.570E-04 |
| E | 1.0  | 0.38  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 2.917E-04 | 3.781E-04 | 2.917E-04 |
| E | 1.5  | 0.50  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.976E-04 | 2.560E-04 | 1.976E-04 |
| E | 2.0  | 0.95  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 5.52  | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 10.34 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 11.46 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 7.80  | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 6.97  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 1.30  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.30  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
| F | 0.4  | 0.01  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 0.56  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 0.74  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 0.80  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 1.83  | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 2.16  | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 5.0  | 1.39  | 485. | 0. | 0. | 19.2 | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04 |
| F | 5.9  | 0.30  | 485. | 0. | 0. | 19.2 | 8.0  | 19.5 | 3.436E-04 | 1.162E-04 | 1.162E-04 |
| F | 7.9  | 0.03  | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.619E-04 | 8.729E-05 | 8.729E-05 |
| G | 0.4  | 0.01  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 0.35  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 0.27  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.24  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.18  | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |
| G | 4.0  | 0.12  | 485. | 0. | 0. | 13.3 | 5.1  | 26.0 | 6.091E-04 | 3.979E-04 | 3.979E-04 |
| G | 5.0  | 0.09  | 485. | 0. | 0. | 13.3 | 5.1  | 18.1 | 7.002E-04 | 3.190E-04 | 3.190E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

NNE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.009     | 0.021     | 0.023     | 0.377     | 0.643     | 0.821     | 1.382     | 1.500     | 1.736     | 2.475     |
| 0.00070   | 0.00165   | 0.00177   | 0.02921   | 0.04979   | 0.06352   | 0.10696   | 0.11611   | 0.13441   | 0.19157   |
| 3.190E-04 | 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 |
| 2.564     | 2.948     | 3.745     | 5.577     | 5.607     | 6.109     | 8.266     | 9.211     | 9.566     | 10.954    |
| 0.19843   | 0.22816   | 0.28990   | 0.43168   | 0.43397   | 0.47285   | 0.63978   | 0.71296   | 0.74040   | 0.84787   |
| 1.303E-04 | 1.162E-04 | 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 8.729E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 |
| 16.479    | 16.774    | 17.956    | 28.297    | 28.356    | 31.221    | 31.251    | 42.714    | 43.039    | 47.471    |
| 1.27550   | 1.29837   | 1.38984   | 2.19020   | 2.19478   | 2.41659   | 2.41888   | 3.30614   | 3.33130   | 3.67431   |
| 6.567E-05 | 5.449E-05 | 4.933E-05 | 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 |
| 55.270    | 60.559    | 67.531    | 68.211    | 73.499    | 74.799    | 74.917    | 75.951    | 83.426    | 84.342    |
| 4.27801   | 4.68734   | 5.22702   | 5.27961   | 5.68894   | 5.78956   | 5.79871   | 5.87875   | 6.45730   | 6.52819   |
| 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 | 1.746E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 |
| 87.621    | 88.241    | 89.098    | 89.896    | 90.930    | 91.019    | 91.314    | 92.141    | 92.437    | 92.673    |
| 6.78202   | 6.83004   | 6.89635   | 6.95810   | 7.03813   | 7.04499   | 7.06786   | 7.13189   | 7.15476   | 7.17305   |
| 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 | 7.796E-06 | 6.686E-06 | 5.881E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |
| 93.264    | 93.737    | 94.239    | 94.948    | 95.007    | 95.923    | 96.100    | 97.932    | 98.730    | 99.675    |
| 7.21879   | 7.25537   | 7.29425   | 7.34913   | 7.35371   | 7.42460   | 7.43832   | 7.58009   | 7.64184   | 7.71501   |
| 3.175E-06 | 2.704E-06 | 1.101E-06 |           |           |           |           |           |           |           |
| 99.734    | 99.793    | 100.000   |           |           |           |           |           |           |           |
| 7.71959   | 7.72416   | 7.74017   |           |           |           |           |           |           |           |

X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.107  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.431  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.274  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 3.303  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.275  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.685  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.453

| K  | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|----|---|--------------|-------------|--------------|
| 10 | 1 | -6.09537     | -11.22341   | -1.18093     |
| 10 | 2 | -7.59738     | -12.97848   | -1.75253     |
| 10 | 3 | -8.37525     | -12.19300   | -1.45348     |
| 10 | 4 | -8.94587     | -11.79427   | -1.27500     |
| 10 | 5 | -9.45081     | -12.24857   | -1.52217     |
| 10 | 6 | -9.63092     | -14.20408   | -2.65931     |
| 10 | 7 | -9.99767     | -17.06856   | -4.47024     |
| 10 | 8 | -10.28369    | NUMXQ(K)= 8 |              |
|    |   | 5.615E-04    | 0.077       | 1.000        |
|    |   | 3.298E-04    | 0.232       | 3.000        |
|    |   | 2.459E-04    | 0.387       | 5.000        |
|    |   | 1.710E-04    | 0.774       | 10.000       |
|    |   | 1.373E-04    | 1.161       | 15.000       |
|    |   | 1.182E-04    | 1.548       | 20.000       |
|    |   | 1.054E-04    | 1.935       | 25.000       |
|    |   | 9.566E-05    | 2.322       | 30.000       |
|    |   | 8.794E-05    | 2.709       | 35.000       |
|    |   | 8.162E-05    | 3.096       | 40.000       |
|    |   | 7.586E-05    | 3.483       | 45.000       |
|    |   | 7.050E-05    | 3.870       | 50.000       |
|    |   | 6.590E-05    | 4.257       | 55.000       |
|    |   | 5.921E-05    | 4.644       | 60.000       |
|    |   | 5.344E-05    | 5.031       | 65.000       |
|    |   | 4.853E-05    | 5.418       | 70.000       |
|    |   | 4.350E-05    | 5.805       | 75.000       |
|    |   | 3.761E-05    | 6.192       | 80.000       |
|    |   | 2.142E-04    | 0.5         | 6.46         |

ANNUAL AVERAGE = 3.94E-06

K= 10 FIVEXQ(K)= 2.142E-04 FIVEPR(K)= 6.460

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NE SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) |           |      |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | MEANDER                           | BLDG WAKE | USED |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |      |
| A               | 3.0                                      | 0.74                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 9.244E-06            | 8.882E-06                         | 8.882E-06 |      |
| A               | 4.0                                      | 1.17                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 6.958E-06            | 6.686E-06                         | 6.686E-06 |      |
| A               | 5.0                                      | 1.28                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 5.579E-06            | 5.361E-06                         | 5.361E-06 |      |
| A               | 6.0                                      | 0.78                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 4.659E-06            | 4.477E-06                         | 4.477E-06 |      |
| A               | 8.0                                      | 0.27                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 3.500E-06            | 3.363E-06                         | 3.363E-06 |      |
| A               | 24.3                                     | 0.04                 | 485.               | 0.                | 0.               | 97.4               | 117.1             | 97.4              | 1.146E-06            | 1.101E-06                         | 1.101E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |      |
| B               | 2.0                                      | 0.16                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 4.316E-05            | 3.829E-05                         | 3.829E-05 |      |
| B               | 3.0                                      | 0.78                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 2.886E-05            | 2.560E-05                         | 2.560E-05 |      |
| B               | 4.0                                      | 0.70                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 2.172E-05            | 1.927E-05                         | 1.927E-05 |      |
| B               | 5.0                                      | 1.09                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 1.742E-05            | 1.545E-05                         | 1.545E-05 |      |
| B               | 6.0                                      | 0.70                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 1.455E-05            | 1.291E-05                         | 1.291E-05 |      |
| B               | 8.0                                      | 0.70                 | 485.               | 0.                | 0.               | 73.3               | 49.9              | 73.3              | 1.093E-05            | 9.696E-06                         | 9.696E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |      |
| C               | 1.5                                      | 0.04                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 1.178E-04            | 9.321E-05                         | 9.321E-05 |      |
| C               | 2.0                                      | 0.27                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 8.966E-05            | 7.093E-05                         | 7.093E-05 |      |
| C               | 3.0                                      | 1.01                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 5.995E-05            | 4.743E-05                         | 4.743E-05 |      |
| C               | 4.0                                      | 1.36                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 4.512E-05            | 3.570E-05                         | 3.570E-05 |      |
| C               | 5.0                                      | 1.44                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 3.618E-05            | 2.862E-05                         | 2.862E-05 |      |
| C               | 6.0                                      | 1.21                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 3.022E-05            | 2.391E-05                         | 2.391E-05 |      |
| C               | 8.0                                      | 0.43                 | 485.               | 0.                | 0.               | 55.6               | 31.6              | 55.6              | 2.270E-05            | 1.796E-05                         | 1.796E-05 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |      |
| D               | 1.0                                      | 0.23                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 78.4              | 2.174E-04            | 2.620E-04                         | 2.174E-04 |      |
| D               | 1.5                                      | 0.74                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 78.4              | 1.473E-04            | 1.774E-04                         | 1.473E-04 |      |
| D               | 2.0                                      | 1.28                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 77.9              | 1.127E-04            | 1.350E-04                         | 1.127E-04 |      |
| D               | 3.0                                      | 5.64                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 60.4              | 9.715E-05            | 9.028E-05                         | 9.028E-05 |      |
| D               | 4.0                                      | 8.87                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 50.5              | 8.749E-05            | 6.796E-05                         | 6.796E-05 |      |
| D               | 5.0                                      | 9.30                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 43.9              | 8.063E-05            | 5.449E-05                         | 5.449E-05 |      |
| D               | 6.0                                      | 5.99                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 39.2              | 7.545E-05            | 4.551E-05                         | 4.551E-05 |      |
| D               | 8.0                                      | 6.46                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 39.2              | 5.674E-05            | 3.419E-05                         | 3.419E-05 |      |
| D               | 9.9                                      | 1.28                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 39.2              | 4.562E-05            | 2.749E-05                         | 2.749E-05 |      |
| D               | 24.3                                     | 0.58                 | 485.               | 0.                | 0.               | 39.2               | 18.0              | 39.2              | 1.858E-05            | 1.119E-05                         | 1.119E-05 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |      |
| E               | 0.4                                      | 0.00                 | 485.               | 0.                | 0.               | 27.9               | 12.7              | 83.6              | 8.570E-04            | 1.111E-03                         | 8.570E-04 |      |
| E               | 1.0                                      | 0.35                 | 485.               | 0.                | 0.               | 27.9               | 12.7              | 83.6              | 2.917E-04            | 3.781E-04                         | 2.917E-04 |      |
| E               | 1.5                                      | 0.78                 | 485.               | 0.                | 0.               | 27.9               | 12.7              | 83.6              | 1.976E-04            | 2.560E-04                         | 1.976E-04 |      |
| E               | 2.0                                      | 1.94                 | 485.               | 0.                | 0.               | 27.9               | 12.7              | 83.6              | 1.504E-04            | 1.948E-04                         | 1.504E-04 |      |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |      |       |      |    |    | MINOR REV. NO. 1B |      | APPENDIX BB-7 |           |           | PAGE NO. 52 of 160 |  |
|--|------|-------|------|----|----|-------------------|------|---------------|-----------|-----------|--------------------|--|
| E  | 3.0  | 8.71  | 485. | 0. | 0. | 27.9              | 12.7 | 55.9          | 1.503E-04 | 1.303E-04 | 1.303E-04          |  |
| E  | 4.0  | 11.63 | 485. | 0. | 0. | 27.9              | 12.7 | 42.1          | 1.503E-04 | 9.806E-05 | 9.806E-05          |  |
| E  | 5.0  | 7.23  | 485. | 0. | 0. | 27.9              | 12.7 | 33.8          | 1.503E-04 | 7.863E-05 | 7.863E-05          |  |
| E  | 5.9  | 3.07  | 485. | 0. | 0. | 27.9              | 12.7 | 28.2          | 1.503E-04 | 6.567E-05 | 6.567E-05          |  |
| E  | 7.9  | 2.37  | 485. | 0. | 0. | 27.9              | 12.7 | 27.9          | 1.142E-04 | 4.933E-05 | 4.933E-05          |  |
| E  | 9.8  | 0.74  | 485. | 0. | 0. | 27.9              | 12.7 | 27.9          | 9.182E-05 | 3.966E-05 | 3.966E-05          |  |
| E  | 24.1 | 0.58  | 485. | 0. | 0. | 27.9              | 12.7 | 27.9          | 3.740E-05 | 1.615E-05 | 1.615E-05          |  |
| F  | 0.4  | 0.02  | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 1.474E-03 | 1.965E-03 | 1.474E-03          |  |
| F  | 1.0  | 0.74  | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 5.018E-04 | 6.690E-04 | 5.018E-04          |  |
| F  | 1.5  | 0.86  | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 3.398E-04 | 4.530E-04 | 3.398E-04          |  |
| F  | 2.0  | 1.44  | 485. | 0. | 0. | 19.2              | 8.0  | 76.9          | 2.586E-04 | 3.447E-04 | 2.586E-04          |  |
| F  | 3.0  | 1.67  | 485. | 0. | 0. | 19.2              | 8.0  | 46.3          | 2.871E-04 | 2.305E-04 | 2.305E-04          |  |
| F  | 4.0  | 1.40  | 485. | 0. | 0. | 19.2              | 8.0  | 32.4          | 3.093E-04 | 1.735E-04 | 1.735E-04          |  |
| F  | 5.0  | 0.39  | 485. | 0. | 0. | 19.2              | 8.0  | 24.5          | 3.277E-04 | 1.391E-04 | 1.391E-04          |  |
| G  | 0.4  | 0.02  | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 2.253E-03 | 4.506E-03 | 2.253E-03          |  |
| G  | 1.0  | 0.74  | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 7.671E-04 | 1.534E-03 | 7.671E-04          |  |
| G  | 1.5  | 0.43  | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 5.195E-04 | 1.039E-03 | 5.195E-04          |  |
| G  | 2.0  | 0.23  | 485. | 0. | 0. | 13.3              | 5.1  | 79.7          | 3.953E-04 | 7.905E-04 | 3.953E-04          |  |
| G  | 3.0  | 0.04  | 485. | 0. | 0. | 13.3              | 5.1  | 41.3          | 5.092E-04 | 5.286E-04 | 5.092E-04          |  |
| G  | 4.0  | 0.08  | 485. | 0. | 0. | 13.3              | 5.1  | 26.0          | 6.091E-04 | 3.979E-04 | 3.979E-04          |  |



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

NE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.019     | 0.035     | 0.036     | 0.776     | 1.203     | 1.242     | 1.981     | 2.059     | 2.292     | 3.148     |
| 0.00112   | 0.00206   | 0.00215   | 0.04559   | 0.07075   | 0.07304   | 0.11648   | 0.12106   | 0.13478   | 0.18509   |
| 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 | 1.303E-04 |
| 3.498     | 4.937     | 6.610     | 6.843     | 7.621     | 9.022     | 10.966    | 11.705    | 12.094    | 20.807    |
| 0.20567   | 0.29028   | 0.38861   | 0.40233   | 0.44806   | 0.53039   | 0.64473   | 0.68817   | 0.71104   | 1.22328   |
| 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 4.933E-05 |
| 22.091    | 33.721    | 33.760    | 39.400    | 46.634    | 46.907    | 55.775    | 58.848    | 68.144    | 70.517    |
| 1.29874   | 1.98248   | 1.98477   | 2.31635   | 2.74168   | 2.75769   | 3.27907   | 3.45973   | 4.00626   | 4.14575   |
| 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 |
| 71.528    | 77.518    | 78.257    | 78.413    | 79.774    | 86.231    | 87.670    | 88.953    | 89.731    | 90.937    |
| 4.20521   | 4.55737   | 4.60082   | 4.60997   | 4.69000   | 5.06961   | 5.15422   | 5.22968   | 5.27541   | 5.34630   |
| 1.927E-05 | 1.796E-05 | 1.615E-05 | 1.545E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 |
| 91.637    | 92.065    | 92.649    | 93.738    | 94.438    | 95.021    | 95.721    | 96.460    | 97.627    | 98.911    |
| 5.38747   | 5.41262   | 5.44692   | 5.51095   | 5.55211   | 5.58641   | 5.62757   | 5.67102   | 5.73963   | 5.81509   |
| 4.477E-06 | 3.363E-06 | 1.101E-06 |           |           |           |           |           |           |           |
| 99.689    | 99.961    | 100.000   |           |           |           |           |           |           |           |
| 5.86082   | 5.87683   | 5.87912   |           |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.046  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.116  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.388  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 1.222  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 2.314  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 3.457  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 4.003

| K  | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|----|---|-------------|-------------|-------------|
| 11 | 1 | -6.09537    | -11.04176   | -1.16650    |
| 11 | 2 | -7.17293    | -12.35449   | -1.56230    |
| 11 | 3 | -7.59738    | -13.78593   | -2.03241    |
| 11 | 4 | -8.37525    | -12.06225   | -1.38495    |
| 11 | 5 | -8.94587    | -12.15267   | -1.42513    |
| 11 | 6 | -9.31262    | -12.93147   | -1.81593    |
| 11 | 7 | -9.63092    | -14.67871   | -2.77724    |
| 11 | 8 | -9.81756    | NUMXQ(K)= 8 |             |
|    |   | 6.858E-04   | 0.059       | 1.000       |
|    |   | 3.876E-04   | 0.176       | 3.000       |
|    |   | 2.782E-04   | 0.294       | 5.000       |
|    |   | 1.892E-04   | 0.588       | 10.000      |
|    |   | 1.546E-04   | 0.882       | 15.000      |
|    |   | 1.330E-04   | 1.176       | 20.000      |
|    |   | 1.176E-04   | 1.470       | 25.000      |
|    |   | 1.060E-04   | 1.764       | 30.000      |
|    |   | 9.689E-05   | 2.058       | 35.000      |
|    |   | 8.923E-05   | 2.352       | 40.000      |
|    |   | 8.143E-05   | 2.646       | 45.000      |
|    |   | 7.492E-05   | 2.940       | 50.000      |
|    |   | 6.939E-05   | 3.234       | 55.000      |
|    |   | 6.408E-05   | 3.527       | 60.000      |
|    |   | 5.789E-05   | 3.821       | 65.000      |
|    |   | 2.046E-04   | 0.5         | 8.50        |

ANNUAL AVERAGE = 3.50E-06

K= 11 FIVEXQ(K)= 2.046E-04 FIVEPR(K)= 8.505

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ENE SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     |                                   |           |           |      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |      |
| A              | 2.0       | 0.22      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |      |
| A              | 3.0       | 0.82      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |      |
| A              | 4.0       | 1.20      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |      |
| A              | 5.0       | 0.79      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |      |
| A              | 6.0       | 0.60      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |      |
| A              | 8.0       | 0.16      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| B              | 2.0       | 0.19      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |      |
| B              | 3.0       | 0.60      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |      |
| B              | 4.0       | 0.85      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |      |
| B              | 5.0       | 0.76      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |      |
| B              | 6.0       | 0.41      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |      |
| B              | 8.0       | 0.22      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| C              | 1.5       | 0.09      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |      |
| C              | 2.0       | 0.35      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |      |
| C              | 3.0       | 1.04      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |      |
| C              | 4.0       | 1.17      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |      |
| C              | 5.0       | 1.20      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |      |
| C              | 6.0       | 0.57      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |      |
| C              | 8.0       | 0.41      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |      |
| C              | 9.9       | 0.03      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| D              | 1.0       | 0.13      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |      |
| D              | 1.5       | 0.88      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |      |
| D              | 2.0       | 1.83      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |      |
| D              | 3.0       | 7.07      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |      |
| D              | 4.0       | 7.20      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |      |
| D              | 5.0       | 6.35      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |      |
| D              | 6.0       | 3.63      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |      |
| D              | 8.0       | 2.68      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |      |
| D              | 9.9       | 0.69      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |      |
| D              | 24.3      | 0.03      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 1.858E-05                         | 1.119E-05 | 1.119E-05 |      |
|                |           |           |          |            |              |         |         |            |                                   |           |           |      |
| E              | 0.4       | 0.00      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |      |
| E              | 1.0       | 0.63      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |      |
| E              | 1.5       | 1.42      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |      |

|   |      |       |      |    |    |      |      |      |           |           |           |
|---|------|-------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 2.0  | 4.42  | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 13.30 | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 7.86  | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 3.60  | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 1.93  | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 1.45  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 0.85  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.41  | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
| F | 0.4  | 0.02  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 0.98  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 1.71  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 3.25  | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 8.18  | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 1.17  | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 24.1 | 0.54  | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 8.576E-05 | 2.858E-05 | 2.858E-05 |
| G | 0.4  | 0.01  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 0.54  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 0.98  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.95  | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 3.51  | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |
| G | 4.0  | 0.09  | 485. | 0. | 0. | 13.3 | 5.1  | 26.0 | 6.091E-04 | 3.979E-04 | 3.979E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

ENE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.014     | 0.035     | 0.038     | 0.575     | 1.554     | 5.060     | 6.039     | 6.133     | 7.081     | 8.786     |
| 0.00100   | 0.00254   | 0.00273   | 0.04160   | 0.11249   | 0.36632   | 0.43721   | 0.44407   | 0.51268   | 0.63616   |
| 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 |
| 9.418     | 12.671    | 20.851    | 20.978    | 22.399    | 23.568    | 27.989    | 28.874    | 42.170    | 44.002    |
| 0.68190   | 0.91743   | 1.50970   | 1.51885   | 1.62176   | 1.70637   | 2.02651   | 2.09054   | 3.05327   | 3.18590   |
| 9.806E-05 | 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 4.933E-05 | 4.743E-05 |
| 51.866    | 51.961    | 59.036    | 62.637    | 62.984    | 70.185    | 72.112    | 78.460    | 79.913    | 80.955    |
| 3.75530   | 3.76216   | 4.27440   | 4.53509   | 4.56024   | 5.08162   | 5.22112   | 5.68075   | 5.78594   | 5.86141   |
| 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.858E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 |
| 84.587    | 85.440    | 85.629    | 86.798    | 89.483    | 90.683    | 91.220    | 91.915    | 92.515    | 93.083    |
| 6.12439   | 6.18613   | 6.19985   | 6.28446   | 6.47883   | 6.56573   | 6.60460   | 6.65491   | 6.69836   | 6.73952   |
| 1.927E-05 | 1.796E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 |
| 93.936    | 94.347    | 94.757    | 95.515    | 95.547    | 95.768    | 96.178    | 96.210    | 96.431    | 97.252    |
| 6.80127   | 6.83099   | 6.86072   | 6.91560   | 6.91789   | 6.93390   | 6.96363   | 6.96591   | 6.98192   | 7.04138   |
| 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |           |           |           |           |           |           |
| 98.452    | 99.242    | 99.842    | 100.000   |           |           |           |           |           |           |
| 7.12827   | 7.18544   | 7.22889   | 7.24032   |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.508  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 3.050  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 4.271  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 5.217  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.677  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 6.121

| K  | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|----|---|--------------|-------------|--------------|
| 12 | 1 | -6.09537     | -9.99470    | -0.91421     |
| 12 | 2 | -7.59738     | -12.08720   | -1.71217     |
| 12 | 3 | -8.37525     | -12.57539   | -1.93736     |
| 12 | 4 | -8.94587     | -13.42597   | -2.39137     |
| 12 | 5 | -9.31262     | -15.01910   | -3.31757     |
| 12 | 6 | -9.63092     | -16.90946   | -4.48149     |
| 12 | 7 | -9.81756     | -17.36738   | -4.77086     |
| 12 | 8 | -9.99767     | NUMXQ(K)= 8 |              |
|    |   | 8.394E-04    | 0.072       | 1.000        |
|    |   | 6.192E-04    | 0.217       | 3.000        |
|    |   | 5.318E-04    | 0.362       | 5.000        |
|    |   | 3.707E-04    | 0.724       | 10.000       |
|    |   | 2.868E-04    | 1.086       | 15.000       |
|    |   | 2.371E-04    | 1.448       | 20.000       |
|    |   | 2.002E-04    | 1.810       | 25.000       |
|    |   | 1.730E-04    | 2.172       | 30.000       |
|    |   | 1.525E-04    | 2.534       | 35.000       |
|    |   | 1.363E-04    | 2.896       | 40.000       |
|    |   | 1.216E-04    | 3.258       | 45.000       |
|    |   | 1.085E-04    | 3.620       | 50.000       |
|    |   | 9.771E-05    | 3.982       | 55.000       |
|    |   | 8.802E-05    | 4.344       | 60.000       |
|    |   | 7.758E-05    | 4.706       | 65.000       |
|    |   | 6.890E-05    | 5.068       | 70.000       |
|    |   | 6.023E-05    | 5.430       | 75.000       |
|    |   | 5.202E-05    | 5.792       | 80.000       |
|    |   | 4.637E-04    | 0.5         | 6.91         |

ANNUAL AVERAGE = 6.08E-06

K= 12 FIVEXQ(K)= 4.637E-04 FIVEPR(K)= 6.906

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE E SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE          | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|-------------------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS            | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           | CA=1459.SQ.METERS |            |              |         |         |            |                                   |           |           |
| A              | 1.5       | 0.03      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |
| A              | 2.0       | 0.05      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 0.91      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.23      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 0.78      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.56      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.30      | 485.              | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.03      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.05      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.42      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 0.56      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.81      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.21      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.32      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| B              | 9.9       | 0.11      | 485.              | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.786E-06                         | 7.796E-06 | 7.796E-06 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.08      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.43      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.29      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.50      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 0.94      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.32      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.32      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C              | 9.9       | 0.03      | 485.              | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.21      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 1.10      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 2.28      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 8.54      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 7.14      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 7.01      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 5.15      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 5.15      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D              | 9.9       | 1.37      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
| D              | 24.3      | 0.27      | 485.              | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 1.858E-05                         | 1.119E-05 | 1.119E-05 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |      |      |      |    | MINOR REV. NO. 1B | APPENDIX BB-7 |      |      |           |           | PAGE NO. 60 of 160 |
|--|------|------|------|----|-------------------|---------------|------|------|-----------|-----------|--------------------|
| E  | 0.4  | 0.00 | 485. | 0. | 0.                | 27.9          | 12.7 | 83.6 | 8.570E-04 | 1.111E-03 | 8.570E-04          |
| E  | 1.0  | 0.62 | 485. | 0. | 0.                | 27.9          | 12.7 | 83.6 | 2.917E-04 | 3.781E-04 | 2.917E-04          |
| E  | 1.5  | 3.17 | 485. | 0. | 0.                | 27.9          | 12.7 | 83.6 | 1.976E-04 | 2.560E-04 | 1.976E-04          |
| E  | 2.0  | 4.83 | 485. | 0. | 0.                | 27.9          | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04          |
| E  | 3.0  | 8.00 | 485. | 0. | 0.                | 27.9          | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04          |
| E  | 4.0  | 5.37 | 485. | 0. | 0.                | 27.9          | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05          |
| E  | 5.0  | 3.60 | 485. | 0. | 0.                | 27.9          | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05          |
| E  | 5.9  | 2.01 | 485. | 0. | 0.                | 27.9          | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05          |
| E  | 7.9  | 1.91 | 485. | 0. | 0.                | 27.9          | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05          |
| E  | 9.8  | 1.15 | 485. | 0. | 0.                | 27.9          | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05          |
| E  | 24.1 | 0.62 | 485. | 0. | 0.                | 27.9          | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05          |
| F  | 0.4  | 0.03 | 485. | 0. | 0.                | 19.2          | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03          |
| F  | 1.0  | 1.50 | 485. | 0. | 0.                | 19.2          | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04          |
| F  | 1.5  | 3.44 | 485. | 0. | 0.                | 19.2          | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04          |
| F  | 2.0  | 4.40 | 485. | 0. | 0.                | 19.2          | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04          |
| F  | 3.0  | 3.44 | 485. | 0. | 0.                | 19.2          | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04          |
| F  | 4.0  | 0.35 | 485. | 0. | 0.                | 19.2          | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04          |
| F  | 5.0  | 0.03 | 485. | 0. | 0.                | 19.2          | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04          |
| F  | 24.1 | 0.03 | 485. | 0. | 0.                | 19.2          | 8.0  | 19.2 | 8.576E-05 | 2.858E-05 | 2.858E-05          |
| G  | 0.4  | 0.03 | 485. | 0. | 0.                | 13.3          | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03          |
| G  | 1.0  | 1.15 | 485. | 0. | 0.                | 13.3          | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04          |
| G  | 1.5  | 1.96 | 485. | 0. | 0.                | 13.3          | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04          |
| G  | 2.0  | 1.26 | 485. | 0. | 0.                | 13.3          | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04          |
| G  | 3.0  | 0.59 | 485. | 0. | 0.                | 13.3          | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04          |



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

E SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.030     | 0.062     | 0.065     | 1.219     | 3.179     | 3.769     | 5.272     | 6.534     | 9.970     | 10.587    |
| 0.00252   | 0.00531   | 0.00553   | 0.10386   | 0.27079   | 0.32110   | 0.44916   | 0.55664   | 0.84934   | 0.90194   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 | 1.303E-04 | 1.127E-04 |
| 14.989    | 18.425    | 18.640    | 21.807    | 22.156    | 26.988    | 28.089    | 28.115    | 36.115    | 38.396    |
| 1.27697   | 1.56967   | 1.58797   | 1.85780   | 1.88753   | 2.29915   | 2.39290   | 2.39519   | 3.07665   | 3.27102   |
| 9.806E-05 | 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 |
| 43.765    | 43.845    | 52.381    | 55.978    | 56.408    | 63.548    | 65.561    | 72.567    | 72.594    | 74.500    |
| 3.72837   | 3.73523   | 4.46242   | 4.76885   | 4.80544   | 5.41371   | 5.58522   | 6.18207   | 6.18435   | 6.34671   |
| 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.858E-05 | 2.749E-05 | 2.560E-05 |
| 75.788    | 80.942    | 82.096    | 82.150    | 83.653    | 88.807    | 89.746    | 89.773    | 91.142    | 92.565    |
| 6.45648   | 6.89553   | 6.99387   | 6.99844   | 7.12650   | 7.56556   | 7.64559   | 7.64788   | 7.76450   | 7.88570   |
| 2.391E-05 | 1.927E-05 | 1.796E-05 | 1.746E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 |
| 92.887    | 93.450    | 93.773    | 93.799    | 94.417    | 95.222    | 95.249    | 95.303    | 95.517    | 95.786    |
| 7.91314   | 7.96116   | 7.98861   | 7.99089   | 8.04349   | 8.11209   | 8.11438   | 8.11895   | 8.13725   | 8.16011   |
| 9.696E-06 | 8.882E-06 | 7.796E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |           |           |           |
| 96.108    | 97.020    | 97.128    | 98.363    | 99.141    | 99.705    | 100.000   |           |           |           |
| 8.18755   | 8.26530   | 8.27445   | 8.37964   | 8.44596   | 8.49398   | 8.51913   |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.449  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 1.568  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 3.074  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 4.459  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 5.581  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 6.892  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 7.562

| K  | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|----|---|-------------|-------------|-------------|
| 13 | 1 | -6.09537    | -10.32254   | -1.04289    |
| 13 | 2 | -7.59738    | -12.01038   | -1.68880    |
| 13 | 3 | -8.37525    | -12.72418   | -2.02042    |
| 13 | 4 | -8.94587    | -12.97285   | -2.15339    |
| 13 | 5 | -9.31262    | -14.28376   | -2.92463    |
| 13 | 6 | -9.63092    | -15.08341   | -3.42726    |
| 13 | 7 | -9.99767    | -18.70822   | -5.87001    |
| 13 | 8 | -10.28369   | NUMXQ(K)= 8 |             |
|    |   | 8.673E-04   | 0.085       | 1.000       |
|    |   | 6.099E-04   | 0.256       | 3.000       |
|    |   | 5.113E-04   | 0.426       | 5.000       |
|    |   | 3.421E-04   | 0.852       | 10.000      |
|    |   | 2.642E-04   | 1.278       | 15.000      |
|    |   | 2.157E-04   | 1.704       | 20.000      |
|    |   | 1.793E-04   | 2.130       | 25.000      |
|    |   | 1.534E-04   | 2.556       | 30.000      |
|    |   | 1.340E-04   | 2.982       | 35.000      |
|    |   | 1.181E-04   | 3.408       | 40.000      |
|    |   | 1.052E-04   | 3.834       | 45.000      |
|    |   | 9.465E-05   | 4.260       | 50.000      |
|    |   | 8.435E-05   | 4.686       | 55.000      |
|    |   | 7.459E-05   | 5.111       | 60.000      |
|    |   | 6.649E-05   | 5.537       | 65.000      |
|    |   | 5.870E-05   | 5.963       | 70.000      |
|    |   | 5.207E-05   | 6.389       | 75.000      |
|    |   | 4.646E-05   | 6.815       | 80.000      |
|    |   | 3.916E-05   | 7.241       | 85.000      |
|    |   | 4.715E-04   | 0.5         | 5.87        |

ANNUAL AVERAGE = 7.70E-06

K= 13 FIVEXQ(K)= 4.715E-04 FIVEPR(K)= 5.869

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ESE SECTOR.

| STABILITY | WINDSPEED      | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------|----------------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS     | METER/SEC      | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
|           | AT 10.0 METERS |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A         | 2.0            | 0.08      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A         | 3.0            | 0.55      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A         | 4.0            | 0.90      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A         | 5.0            | 0.83      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A         | 6.0            | 0.93      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A         | 8.0            | 0.75      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
| A         | 9.9            | 0.03      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 2.814E-06                         | 2.704E-06 | 2.704E-06 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| B         | 1.5            | 0.03      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B         | 2.0            | 0.15      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B         | 3.0            | 0.70      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B         | 4.0            | 1.08      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B         | 5.0            | 0.98      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B         | 6.0            | 0.60      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B         | 8.0            | 0.45      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| B         | 9.9            | 0.08      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.786E-06                         | 7.796E-06 | 7.796E-06 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| C         | 1.5            | 0.03      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C         | 2.0            | 0.30      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C         | 3.0            | 1.23      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C         | 4.0            | 1.45      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C         | 5.0            | 1.18      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C         | 6.0            | 0.53      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C         | 8.0            | 0.60      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C         | 9.9            | 0.13      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
| C         | 24.3           | 0.08      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 7.433E-06                         | 5.881E-06 | 5.881E-06 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| D         | 1.0            | 0.28      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D         | 1.5            | 1.76      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D         | 2.0            | 2.03      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D         | 3.0            | 7.67      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D         | 4.0            | 7.57      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D         | 5.0            | 7.17      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D         | 6.0            | 5.69      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D         | 8.0            | 4.96      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D         | 9.9            | 1.25      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
| D         | 24.3           | 0.08      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 1.858E-05                         | 1.119E-05 | 1.119E-05 |

|  |                   |               |                    |
|--|-------------------|---------------|--------------------|
| CALCULATION NO. BYR04-050, BRW-04-0044-M | MINOR REV. NO. 1B | APPENDIX BB-7 | PAGE NO. 64 of 160 |
|--|-------------------|---------------|--------------------|

|   |      |      |      |    |    |      |      |      |           |           |           |
|---|------|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 0.4  | 0.01 | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 8.570E-04 | 1.111E-03 | 8.570E-04 |
| E | 1.0  | 1.28 | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 2.917E-04 | 3.781E-04 | 2.917E-04 |
| E | 1.5  | 4.29 | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.976E-04 | 2.560E-04 | 1.976E-04 |
| E | 2.0  | 4.14 | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 7.77 | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 6.12 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 4.14 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 2.21 | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 2.11 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 0.40 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.08 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
| F | 0.4  | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 2.06 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 4.99 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 2.33 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 0.93 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 0.08 | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| F | 7.9  | 0.03 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.619E-04 | 8.729E-05 | 8.729E-05 |
| G | 0.4  | 0.05 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 2.03 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 2.28 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.53 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.03 | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

ESE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED  
AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.052     | 0.097     | 0.102     | 2.133     | 4.415     | 4.440     | 6.496     | 7.023     | 12.013    | 13.291    |
| 0.00476   | 0.00883   | 0.00932   | 0.19455   | 0.40264   | 0.40493   | 0.59244   | 0.64046   | 1.09553   | 1.21215   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 15.623    | 16.551    | 16.827    | 21.115    | 21.190    | 25.327    | 27.083    | 34.856    | 36.887    | 43.005    |
| 1.42482   | 1.50943   | 1.53459   | 1.92562   | 1.93248   | 2.30980   | 2.46987   | 3.17877   | 3.36399   | 3.92196   |
| 9.321E-05 | 9.028E-05 | 8.729E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 |
| 43.030    | 50.703    | 50.728    | 54.865    | 55.166    | 62.739    | 64.945    | 72.117    | 72.142    | 74.248    |
| 3.92425   | 4.62400   | 4.62629   | 5.00360   | 5.03104   | 5.72164   | 5.92288   | 6.57689   | 6.57918   | 6.77127   |
| 4.743E-05 | 4.551E-05 | 3.966E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 |
| 75.477    | 81.169    | 81.570    | 81.720    | 83.175    | 88.140    | 89.318    | 90.572    | 91.274    | 91.801    |
| 6.88332   | 7.40241   | 7.43900   | 7.45272   | 7.58535   | 8.03813   | 8.14561   | 8.25995   | 8.32398   | 8.37200   |
| 1.927E-05 | 1.796E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 |
| 92.879    | 93.481    | 93.556    | 94.534    | 94.659    | 94.734    | 95.336    | 95.411    | 95.863    | 96.414    |
| 8.47033   | 8.52521   | 8.53207   | 8.62126   | 8.63269   | 8.63955   | 8.69443   | 8.70129   | 8.74245   | 8.79276   |
| 7.796E-06 | 6.686E-06 | 5.881E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 | 2.704E-06 |           |           |           |
| 96.490    | 97.392    | 97.467    | 98.295    | 99.223    | 99.975    | 100.000   |           |           |           |
| 8.79962   | 8.88195   | 8.88881   | 8.96427   | 9.04888   | 9.11748   | 9.11977   |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.194  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.592  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 1.094  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 3.176  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.620  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.919  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 7.399  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 8.034

| K           | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|-------------|---|--------------|-------------|--------------|
| 14          | 1 | -6.09537     | -10.23640   | -1.06105     |
| 14          | 2 | -7.17293     | -10.48342   | -1.14660     |
| 14          | 3 | -7.59738     | -11.96360   | -1.73467     |
| 14          | 4 | -7.98712     | -13.01877   | -2.19497     |
| 14          | 5 | -8.94587     | -12.88565   | -2.12323     |
| 14          | 6 | -9.31262     | -13.73133   | -2.62577     |
| 14          | 7 | -9.63092     | -14.61653   | -3.19261     |
| 14          | 8 | -9.99767     | -19.40802   | -6.50455     |
| 14          | 9 | -10.28369    |             |              |
| NUMXQ(K)= 9 |   |              |             |              |
|             |   | 9.797E-04    | 0.091       | 1.000        |
|             |   | 6.770E-04    | 0.274       | 3.000        |
|             |   | 5.569E-04    | 0.456       | 5.000        |
|             |   | 3.829E-04    | 0.912       | 10.000       |
|             |   | 2.816E-04    | 1.368       | 15.000       |
|             |   | 2.189E-04    | 1.824       | 20.000       |
|             |   | 1.787E-04    | 2.280       | 25.000       |
|             |   | 1.506E-04    | 2.736       | 30.000       |
|             |   | 1.298E-04    | 3.192       | 35.000       |
|             |   | 1.142E-04    | 3.648       | 40.000       |
|             |   | 1.017E-04    | 4.104       | 45.000       |
|             |   | 9.156E-05    | 4.560       | 50.000       |
|             |   | 8.146E-05    | 5.016       | 55.000       |
|             |   | 7.284E-05    | 5.472       | 60.000       |
|             |   | 6.558E-05    | 5.928       | 65.000       |
|             |   | 5.817E-05    | 6.384       | 70.000       |
|             |   | 5.193E-05    | 6.840       | 75.000       |
|             |   | 4.663E-05    | 7.296       | 80.000       |
|             |   | 3.880E-05    | 7.752       | 85.000       |
|             |   |              |             |              |
|             |   | 5.370E-04    | 0.5         | 5.48         |

ANNUAL AVERAGE = 8.96E-06

K= 14 FIVEXQ(K)= 5.370E-04 FIVEPR(K)= 5.483

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SE SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            |                                   |           |           |
|                |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 3.0       | 1.05      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.49      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 2.25      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.69      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.54      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.18      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.02      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 1.56      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 1.02      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.73      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.15      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.07      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.18      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.74      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.85      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 1.82      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.80      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.25      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.54      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D              | 1.5       | 2.62      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D              | 2.0       | 4.83      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D              | 3.0       | 11.73     | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 10.13     | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D              | 5.0       | 7.01      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D              | 6.0       | 2.47      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D              | 8.0       | 1.74      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D              | 9.9       | 0.07      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| E              | 0.4       | 0.01      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E              | 1.0       | 1.71      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E              | 1.5       | 4.72      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |
| E              | 2.0       | 6.25      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.504E-04                         | 1.948E-04 | 1.504E-04 |
| E              | 3.0       | 6.65      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 55.9       | 1.503E-04                         | 1.303E-04 | 1.303E-04 |

|   |     |      |      |    |    |      |      |      |           |           |           |
|---|-----|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 4.0 | 4.72 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0 | 2.22 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9 | 0.84 | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9 | 0.69 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| F | 0.4 | 0.06 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0 | 2.87 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5 | 4.14 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0 | 1.60 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0 | 0.36 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0 | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 32.4 | 3.093E-04 | 1.735E-04 | 1.735E-04 |
| G | 0.4 | 0.07 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0 | 2.80 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5 | 1.42 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0 | 0.18 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0 | 0.07 | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

SE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.072     | 0.134     | 0.141     | 2.938     | 4.355     | 4.428     | 7.297     | 7.479     | 11.620    | 13.327    |
| 0.00452   | 0.00845   | 0.00890   | 0.18498   | 0.27416   | 0.27873   | 0.45939   | 0.47082   | 0.73151   | 0.83899   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 14.926    | 15.289    | 15.834    | 20.556    | 20.593    | 26.841    | 29.456    | 36.104    | 40.935    | 45.657    |
| 0.93961   | 0.96247   | 0.99678   | 1.29406   | 1.29634   | 1.68966   | 1.85431   | 2.27279   | 2.57693   | 2.87421   |
| 9.321E-05 | 9.028E-05 | 7.863E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 |
| 45.730    | 57.463    | 59.679    | 59.860    | 69.995    | 70.831    | 77.841    | 77.878    | 78.568    | 80.312    |
| 2.87878   | 3.61740   | 3.75690   | 3.76833   | 4.40634   | 4.45893   | 4.90028   | 4.90256   | 4.94601   | 5.05578   |
| 4.551E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 |
| 82.782    | 82.963    | 84.816    | 86.560    | 88.376    | 88.448    | 89.466    | 90.265    | 91.827    | 92.081    |
| 5.21127   | 5.22271   | 5.33933   | 5.44910   | 5.56344   | 5.56801   | 5.63204   | 5.68235   | 5.78068   | 5.79668   |
| 1.545E-05 | 1.291E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 |           |           |
| 93.098    | 93.825    | 93.970    | 95.023    | 96.513    | 98.765    | 99.455    | 100.000   |           |           |
| 5.86071   | 5.90645   | 5.91560   | 5.98191   | 6.07567   | 6.21745   | 6.26090   | 6.29520   |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.185  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.459  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.731  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.270  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.614  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.403  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.897

| K  | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|----|---|--------------|-------------|--------------|
| 15 | 1 | -6.09537     | -10.26415   | -1.06482     |
| 15 | 2 | -7.17293     | -11.31265   | -1.42599     |
| 15 | 3 | -7.59738     | -13.80570   | -2.38288     |
| 15 | 4 | -7.98712     | -13.29595   | -2.17412     |
| 15 | 5 | -8.94587     | -12.55138   | -1.80199     |
| 15 | 6 | -9.31262     | -14.88633   | -3.10112     |
| 15 | 7 | -9.59663     | -17.01813   | -4.35089     |
| 15 | 8 | -9.81756     | NUMXQ(K)= 8 |              |
|    |   | 1.081E-03    | 0.063       | 1.000        |
|    |   | 7.600E-04    | 0.189       | 3.000        |
|    |   | 6.014E-04    | 0.315       | 5.000        |
|    |   | 3.862E-04    | 0.630       | 10.000       |
|    |   | 2.772E-04    | 0.944       | 15.000       |
|    |   | 2.187E-04    | 1.259       | 20.000       |
|    |   | 1.807E-04    | 1.574       | 25.000       |
|    |   | 1.540E-04    | 1.889       | 30.000       |
|    |   | 1.340E-04    | 2.203       | 35.000       |
|    |   | 1.204E-04    | 2.518       | 40.000       |
|    |   | 1.099E-04    | 2.833       | 45.000       |
|    |   | 1.011E-04    | 3.148       | 50.000       |
|    |   | 9.357E-05    | 3.462       | 55.000       |
|    |   | 8.491E-05    | 3.777       | 60.000       |
|    |   | 7.569E-05    | 4.092       | 65.000       |
|    |   | 6.795E-05    | 4.407       | 70.000       |
|    |   | 5.890E-05    | 4.721       | 75.000       |
|    |   | 4.681E-04    | 0.5         | 7.94         |

ANNUAL AVERAGE = 6.71E-06

K= 15 FIVEXQ(K)= 4.681E-04 FIVEPR(K)= 7.943

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSE SECTOR.

| STABILITY | WINDSPEED      | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------|----------------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS     | METER/SEC      | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
|           | AT 10.0 METERS |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A         | 2.0            | 0.12      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A         | 3.0            | 0.56      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A         | 4.0            | 1.98      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A         | 5.0            | 2.34      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A         | 6.0            | 0.77      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A         | 8.0            | 0.32      | 485.     | 0.         | 0.           | 97.4    | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| B         | 1.0            | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 8.375E-05                         | 7.431E-05 | 7.431E-05 |
| B         | 1.5            | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B         | 2.0            | 0.04      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B         | 3.0            | 1.09      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B         | 4.0            | 1.25      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B         | 5.0            | 1.33      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B         | 6.0            | 0.69      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B         | 8.0            | 0.28      | 485.     | 0.         | 0.           | 73.3    | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| C         | 2.0            | 0.36      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C         | 3.0            | 1.13      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C         | 4.0            | 1.65      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C         | 5.0            | 1.33      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C         | 6.0            | 0.48      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C         | 8.0            | 0.32      | 485.     | 0.         | 0.           | 55.6    | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| D         | 1.0            | 0.65      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 2.174E-04                         | 2.620E-04 | 2.174E-04 |
| D         | 1.5            | 1.57      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 78.4       | 1.473E-04                         | 1.774E-04 | 1.473E-04 |
| D         | 2.0            | 3.67      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 77.9       | 1.127E-04                         | 1.350E-04 | 1.127E-04 |
| D         | 3.0            | 11.14     | 485.     | 0.         | 0.           | 39.2    | 18.0    | 60.4       | 9.715E-05                         | 9.028E-05 | 9.028E-05 |
| D         | 4.0            | 8.60      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 50.5       | 8.749E-05                         | 6.796E-05 | 6.796E-05 |
| D         | 5.0            | 8.35      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 43.9       | 8.063E-05                         | 5.449E-05 | 5.449E-05 |
| D         | 6.0            | 5.61      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 7.545E-05                         | 4.551E-05 | 4.551E-05 |
| D         | 8.0            | 3.59      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 5.674E-05                         | 3.419E-05 | 3.419E-05 |
| D         | 9.9            | 0.85      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 4.562E-05                         | 2.749E-05 | 2.749E-05 |
| D         | 24.3           | 0.12      | 485.     | 0.         | 0.           | 39.2    | 18.0    | 39.2       | 1.858E-05                         | 1.119E-05 | 1.119E-05 |
|           |                |           |          |            |              |         |         |            |                                   |           |           |
| E         | 0.4            | 0.01      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 8.570E-04                         | 1.111E-03 | 8.570E-04 |
| E         | 1.0            | 1.49      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 2.917E-04                         | 3.781E-04 | 2.917E-04 |
| E         | 1.5            | 3.31      | 485.     | 0.         | 0.           | 27.9    | 12.7    | 83.6       | 1.976E-04                         | 2.560E-04 | 1.976E-04 |

|   |      |      |      |    |    |      |      |      |           |           |           |
|---|------|------|------|----|----|------|------|------|-----------|-----------|-----------|
| E | 2.0  | 3.59 | 485. | 0. | 0. | 27.9 | 12.7 | 83.6 | 1.504E-04 | 1.948E-04 | 1.504E-04 |
| E | 3.0  | 8.68 | 485. | 0. | 0. | 27.9 | 12.7 | 55.9 | 1.503E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 6.17 | 485. | 0. | 0. | 27.9 | 12.7 | 42.1 | 1.503E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 3.43 | 485. | 0. | 0. | 27.9 | 12.7 | 33.8 | 1.503E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 1.21 | 485. | 0. | 0. | 27.9 | 12.7 | 28.2 | 1.503E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 0.93 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 24.1 | 0.08 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
|   |      |      |      |    |    |      |      |      |           |           |           |
| F | 0.4  | 0.05 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 1.474E-03 | 1.965E-03 | 1.474E-03 |
| F | 1.0  | 2.10 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 5.018E-04 | 6.690E-04 | 5.018E-04 |
| F | 1.5  | 2.74 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 3.398E-04 | 4.530E-04 | 3.398E-04 |
| F | 2.0  | 1.13 | 485. | 0. | 0. | 19.2 | 8.0  | 76.9 | 2.586E-04 | 3.447E-04 | 2.586E-04 |
| F | 3.0  | 0.48 | 485. | 0. | 0. | 19.2 | 8.0  | 46.3 | 2.871E-04 | 2.305E-04 | 2.305E-04 |
| F | 5.0  | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 24.5 | 3.277E-04 | 1.391E-04 | 1.391E-04 |
|   |      |      |      |    |    |      |      |      |           |           |           |
| G | 0.4  | 0.07 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 2.253E-03 | 4.506E-03 | 2.253E-03 |
| G | 1.0  | 2.66 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 7.671E-04 | 1.534E-03 | 7.671E-04 |
| G | 1.5  | 1.13 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 5.195E-04 | 1.039E-03 | 5.195E-04 |
| G | 2.0  | 0.36 | 485. | 0. | 0. | 13.3 | 5.1  | 79.7 | 3.953E-04 | 7.905E-04 | 3.953E-04 |
| G | 3.0  | 0.04 | 485. | 0. | 0. | 13.3 | 5.1  | 41.3 | 5.092E-04 | 5.286E-04 | 5.092E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### SITE EXCLUSION BOUNDARY CALCULATIONS:

SSE SECTOR BOUNDARY DISTANCE = 485.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.953E-04 | 3.398E-04 | 2.917E-04 |
| 0.068     | 0.114     | 0.120     | 2.784     | 3.914     | 3.954     | 6.052     | 6.416     | 9.160     | 10.653    |
| 0.00388   | 0.00646   | 0.00681   | 0.15774   | 0.22177   | 0.22405   | 0.34297   | 0.36355   | 0.51905   | 0.60366   |
| 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 | 1.303E-04 | 1.127E-04 | 9.806E-05 |
| 11.783    | 12.267    | 12.913    | 16.222    | 19.814    | 21.388    | 21.428    | 30.104    | 33.777    | 39.951    |
| 0.66769   | 0.69513   | 0.73172   | 0.91923   | 1.12275   | 1.21194   | 1.21422   | 1.70588   | 1.91397   | 2.26384   |
| 9.028E-05 | 7.863E-05 | 7.431E-05 | 7.093E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 |
| 51.089    | 54.519    | 54.560    | 54.923    | 63.519    | 64.729    | 73.083    | 73.123    | 74.051    | 75.181    |
| 2.89499   | 3.08936   | 3.09165   | 3.11223   | 3.59931   | 3.66791   | 4.14127   | 4.14356   | 4.19616   | 4.26019   |
| 4.551E-05 | 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 |
| 80.791    | 80.831    | 82.486    | 86.077    | 87.409    | 88.257    | 89.346    | 89.830    | 91.081    | 91.404    |
| 4.57804   | 4.58033   | 4.67409   | 4.87761   | 4.95307   | 5.00110   | 5.06284   | 5.09028   | 5.16117   | 5.17946   |
| 1.615E-05 | 1.545E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 | 6.686E-06 | 5.361E-06 | 4.477E-06 |
| 91.485    | 92.817    | 92.938    | 93.624    | 93.745    | 94.027    | 94.592    | 96.570    | 98.910    | 99.677    |
| 5.18404   | 5.25950   | 5.26636   | 5.30523   | 5.31210   | 5.32810   | 5.36012   | 5.47217   | 5.60480   | 5.64825   |
| 3.363E-06 |           |           |           |           |           |           |           |           |           |
| 100.000   |           |           |           |           |           |           |           |           |           |
| 5.66654   |           |           |           |           |           |           |           |           |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.158  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.343  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.918  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.892  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.596  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.138  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.574

| K  | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|----|---|-------------|-------------|-------------|
| 16 | 1 | -6.09537    | -10.35618   | -1.07813    |
| 16 | 2 | -7.17293    | -12.21438   | -1.70748    |
| 16 | 3 | -7.59738    | -14.88569   | -2.69540    |
| 16 | 4 | -8.52936    | -12.53315   | -1.69780    |
| 16 | 5 | -9.31262    | -14.85114   | -2.91981    |
| 16 | 6 | -9.59663    | -15.74186   | -3.41476    |
| 16 | 7 | -9.81756    | -16.42147   | -3.80649    |
| 16 | 8 | -9.99767    | NUMXQ(K)= 8 |             |
|    |   | 1.063E-03   | 0.057       | 1.000       |
|    |   | 7.373E-04   | 0.170       | 3.000       |
|    |   | 5.586E-04   | 0.283       | 5.000       |
|    |   | 3.162E-04   | 0.567       | 10.000      |
|    |   | 2.136E-04   | 0.850       | 15.000      |
|    |   | 1.729E-04   | 1.133       | 20.000      |
|    |   | 1.493E-04   | 1.417       | 25.000      |
|    |   | 1.320E-04   | 1.700       | 30.000      |
|    |   | 1.186E-04   | 1.983       | 35.000      |
|    |   | 1.079E-04   | 2.267       | 40.000      |
|    |   | 9.912E-05   | 2.550       | 45.000      |
|    |   | 9.173E-05   | 2.833       | 50.000      |
|    |   | 8.210E-05   | 3.117       | 55.000      |
|    |   | 7.328E-05   | 3.400       | 60.000      |
|    |   | 6.556E-05   | 3.683       | 65.000      |
|    |   | 5.835E-05   | 3.967       | 70.000      |
|    |   | 5.203E-05   | 4.250       | 75.000      |
|    |   | 4.632E-05   | 4.533       | 80.000      |
|    |   | 3.556E-04   | 0.5         | 8.82        |

ANNUAL AVERAGE = 5.29E-06

K= 16 FIVEXQ(K)= 3.556E-04 FIVEPR(K)= 8.824

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ALL SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y           | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|-------------------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS            | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              | CA=1459.SQ.METERS |         |            |                                   |           |           |
| A              | 1.5       | 0.03      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 1.817E-05                         | 1.746E-05 | 1.746E-05 |
| A              | 2.0       | 0.26      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 1.382E-05                         | 1.328E-05 | 1.328E-05 |
| A              | 3.0       | 1.20      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 9.244E-06                         | 8.882E-06 | 8.882E-06 |
| A              | 4.0       | 1.24      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 6.958E-06                         | 6.686E-06 | 6.686E-06 |
| A              | 5.0       | 1.06      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 5.579E-06                         | 5.361E-06 | 5.361E-06 |
| A              | 6.0       | 0.51      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 4.659E-06                         | 4.477E-06 | 4.477E-06 |
| A              | 8.0       | 0.34      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 3.500E-06                         | 3.363E-06 | 3.363E-06 |
| A              | 9.9       | 0.03      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 2.814E-06                         | 2.704E-06 | 2.704E-06 |
| A              | 24.3      | 0.03      | 485.     | 0.         | 0.           | 97.4              | 117.1   | 97.4       | 1.146E-06                         | 1.101E-06 | 1.101E-06 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| B              | 1.0       | 0.00      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 8.375E-05                         | 7.431E-05 | 7.431E-05 |
| B              | 1.5       | 0.07      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 5.672E-05                         | 5.032E-05 | 5.032E-05 |
| B              | 2.0       | 0.27      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 4.316E-05                         | 3.829E-05 | 3.829E-05 |
| B              | 3.0       | 1.00      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 2.886E-05                         | 2.560E-05 | 2.560E-05 |
| B              | 4.0       | 0.87      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 2.172E-05                         | 1.927E-05 | 1.927E-05 |
| B              | 5.0       | 0.70      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 1.742E-05                         | 1.545E-05 | 1.545E-05 |
| B              | 6.0       | 0.40      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 1.455E-05                         | 1.291E-05 | 1.291E-05 |
| B              | 8.0       | 0.25      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 1.093E-05                         | 9.696E-06 | 9.696E-06 |
| B              | 9.9       | 0.04      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 8.786E-06                         | 7.796E-06 | 7.796E-06 |
| B              | 24.3      | 0.01      | 485.     | 0.         | 0.           | 73.3              | 49.9    | 73.3       | 3.578E-06                         | 3.175E-06 | 3.175E-06 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| C              | 1.0       | 0.01      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 1.740E-04                         | 1.376E-04 | 1.376E-04 |
| C              | 1.5       | 0.13      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 1.178E-04                         | 9.321E-05 | 9.321E-05 |
| C              | 2.0       | 0.50      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 8.966E-05                         | 7.093E-05 | 7.093E-05 |
| C              | 3.0       | 1.29      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 5.995E-05                         | 4.743E-05 | 4.743E-05 |
| C              | 4.0       | 1.19      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 4.512E-05                         | 3.570E-05 | 3.570E-05 |
| C              | 5.0       | 0.88      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 3.618E-05                         | 2.862E-05 | 2.862E-05 |
| C              | 6.0       | 0.49      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 3.022E-05                         | 2.391E-05 | 2.391E-05 |
| C              | 8.0       | 0.35      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 2.270E-05                         | 1.796E-05 | 1.796E-05 |
| C              | 9.9       | 0.05      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 1.825E-05                         | 1.444E-05 | 1.444E-05 |
| C              | 24.3      | 0.02      | 485.     | 0.         | 0.           | 55.6              | 31.6    | 55.6       | 7.433E-06                         | 5.881E-06 | 5.881E-06 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| D              | 1.0       | 0.42      | 485.     | 0.         | 0.           | 39.2              | 18.0    | 39.2       | 4.349E-04                         | 2.620E-04 | 2.620E-04 |
| D              | 1.5       | 1.85      | 485.     | 0.         | 0.           | 39.2              | 18.0    | 39.2       | 2.945E-04                         | 1.774E-04 | 1.774E-04 |
| D              | 2.0       | 3.20      | 485.     | 0.         | 0.           | 39.2              | 18.0    | 39.2       | 2.241E-04                         | 1.350E-04 | 1.350E-04 |
| D              | 3.0       | 8.25      | 485.     | 0.         | 0.           | 39.2              | 18.0    | 39.2       | 1.498E-04                         | 9.028E-05 | 9.028E-05 |
| D              | 4.0       | 7.24      | 485.     | 0.         | 0.           | 39.2              | 18.0    | 39.2       | 1.128E-04                         | 6.796E-05 | 6.796E-05 |

|   |      |      |      |    |    |      |      |      |           |           |           |
|---|------|------|------|----|----|------|------|------|-----------|-----------|-----------|
| D | 5.0  | 6.01 | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 9.044E-05 | 5.449E-05 | 5.449E-05 |
| D | 6.0  | 4.15 | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 7.553E-05 | 4.551E-05 | 4.551E-05 |
| D | 8.0  | 3.43 | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 5.674E-05 | 3.419E-05 | 3.419E-05 |
| D | 9.9  | 0.87 | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 4.562E-05 | 2.749E-05 | 2.749E-05 |
| D | 24.3 | 0.15 | 485. | 0. | 0. | 39.2 | 18.0 | 39.2 | 1.858E-05 | 1.119E-05 | 1.119E-05 |
| E | 0.4  | 0.01 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 2.571E-03 | 1.111E-03 | 1.111E-03 |
| E | 1.0  | 1.65 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 8.752E-04 | 3.781E-04 | 3.781E-04 |
| E | 1.5  | 3.96 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 5.927E-04 | 2.560E-04 | 2.560E-04 |
| E | 2.0  | 4.85 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 4.511E-04 | 1.948E-04 | 1.948E-04 |
| E | 3.0  | 9.56 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.016E-04 | 1.303E-04 | 1.303E-04 |
| E | 4.0  | 7.23 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 2.270E-04 | 9.806E-05 | 9.806E-05 |
| E | 5.0  | 4.72 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.820E-04 | 7.863E-05 | 7.863E-05 |
| E | 5.9  | 2.72 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.520E-04 | 6.567E-05 | 6.567E-05 |
| E | 7.9  | 2.33 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 1.142E-04 | 4.933E-05 | 4.933E-05 |
| E | 9.8  | 0.61 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 9.182E-05 | 3.966E-05 | 3.966E-05 |
| E | 24.1 | 0.20 | 485. | 0. | 0. | 27.9 | 12.7 | 27.9 | 3.740E-05 | 1.615E-05 | 1.615E-05 |
| F | 0.4  | 0.05 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 5.896E-03 | 1.965E-03 | 1.965E-03 |
| F | 1.0  | 2.10 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.007E-03 | 6.690E-04 | 6.690E-04 |
| F | 1.5  | 2.76 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 1.359E-03 | 4.530E-04 | 4.530E-04 |
| F | 2.0  | 2.07 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 1.034E-03 | 3.447E-04 | 3.447E-04 |
| F | 3.0  | 1.90 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 6.916E-04 | 2.305E-04 | 2.305E-04 |
| F | 4.0  | 0.49 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 5.206E-04 | 1.735E-04 | 1.735E-04 |
| F | 5.0  | 0.16 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 4.174E-04 | 1.391E-04 | 1.391E-04 |
| F | 5.9  | 0.02 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 3.486E-04 | 1.162E-04 | 1.162E-04 |
| F | 7.9  | 0.01 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.619E-04 | 8.729E-05 | 8.729E-05 |
| F | 9.8  | 0.03 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 2.106E-04 | 7.018E-05 | 7.018E-05 |
| F | 24.1 | 0.04 | 485. | 0. | 0. | 19.2 | 8.0  | 19.2 | 8.576E-05 | 2.858E-05 | 2.858E-05 |
| G | 0.4  | 0.04 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 1.352E-02 | 4.506E-03 | 4.506E-03 |
| G | 1.0  | 1.69 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 4.602E-03 | 1.534E-03 | 1.534E-03 |
| G | 1.5  | 1.11 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 3.117E-03 | 1.039E-03 | 1.039E-03 |
| G | 2.0  | 0.48 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 2.372E-03 | 7.905E-04 | 7.905E-04 |
| G | 3.0  | 0.37 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 1.586E-03 | 5.286E-04 | 5.286E-04 |
| G | 4.0  | 0.03 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 1.194E-03 | 3.979E-04 | 3.979E-04 |
| G | 5.0  | 0.01 | 485. | 0. | 0. | 13.3 | 5.1  | 13.3 | 9.571E-04 | 3.190E-04 | 3.190E-04 |



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

SITE EXCLUSION BOUNDARY CALCULATIONS:

DIRECTION-INDEPENDENT (S.R.P 2.3.4) MODEL.

MINIMUM BOUNDARY DISTANCE = 485.0 METERS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.506E-03 | 1.965E-03 | 1.534E-03 | 1.111E-03 | 1.039E-03 | 7.905E-04 | 6.690E-04 | 5.286E-04 | 4.530E-04 | 3.979E-04 |
| 0.043     | 0.089     | 1.781     | 1.788     | 2.897     | 3.380     | 5.484     | 5.856     | 8.619     | 8.649     |
| 0.04345   | 0.08918   | 1.78139   | 1.78825   | 2.89732   | 3.37983   | 5.48365   | 5.85639   | 8.61880   | 8.64853   |
| 3.781E-04 | 3.447E-04 | 3.190E-04 | 2.620E-04 | 2.560E-04 | 2.305E-04 | 1.948E-04 | 1.774E-04 | 1.735E-04 | 1.391E-04 |
| 10.295    | 12.367    | 12.374    | 12.792    | 16.751    | 18.649    | 23.499    | 25.351    | 25.840    | 25.996    |
| 10.29499  | 12.36680  | 12.37366  | 12.79213  | 16.75051  | 18.64853  | 23.49874  | 25.35102  | 25.84038  | 25.99588  |
| 1.376E-04 | 1.350E-04 | 1.303E-04 | 1.162E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 8.729E-05 | 7.863E-05 | 7.431E-05 |
| 26.005    | 29.202    | 38.765    | 38.788    | 46.021    | 46.149    | 54.397    | 54.404    | 59.120    | 59.124    |
| 26.00503  | 29.20192  | 38.76515  | 38.78802  | 46.02104  | 46.14910  | 54.39744  | 54.40430  | 59.11960  | 59.12417  |
| 7.093E-05 | 7.018E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 | 4.551E-05 | 3.966E-05 |
| 59.627    | 59.655    | 66.892    | 69.611    | 75.625    | 75.694    | 78.024    | 79.319    | 83.471    | 84.084    |
| 59.62726  | 59.65470  | 66.89230  | 69.61125  | 75.62543  | 75.69403  | 78.02424  | 79.31854  | 83.47129  | 84.08414  |
| 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.858E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 |
| 84.349    | 85.541    | 88.976    | 89.858    | 89.899    | 90.766    | 91.768    | 92.262    | 93.135    | 93.490    |
| 84.34941  | 85.54081  | 88.97552  | 89.85822  | 89.89938  | 90.76606  | 91.76766  | 92.26160  | 93.13515  | 93.48959  |
| 1.746E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 | 7.796E-06 |
| 93.524    | 93.727    | 94.423    | 94.471    | 94.729    | 95.134    | 95.280    | 95.534    | 96.730    | 96.767    |
| 93.52390  | 93.72742  | 94.42259  | 94.47061  | 94.72902  | 95.13377  | 95.28013  | 95.53396  | 96.72993  | 96.76653  |
| 6.686E-06 | 5.881E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 | 3.175E-06 | 2.704E-06 | 1.101E-06 |           |           |
| 98.006    | 98.029    | 99.088    | 99.598    | 99.936    | 99.945    | 99.973    | 100.000   |           |           |
| 98.00595  | 98.02882  | 99.08759  | 99.59753  | 99.93597  | 99.94512  | 99.97256  | 100.00000 |           |           |

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

ERROR IN NORMAL TRANSFORMATION FOR A( 68)= 100.00000  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 12.365

|           |        |        |
|-----------|--------|--------|
| 1.869E-03 | 1.000  | 1.000  |
| 1.083E-03 | 3.000  | 3.000  |
| 7.458E-04 | 5.000  | 5.000  |
| 4.199E-04 | 10.000 | 10.000 |
| 2.943E-04 | 15.000 | 15.000 |
| 2.278E-04 | 20.000 | 20.000 |
| 1.864E-04 | 25.000 | 25.000 |
| 1.623E-04 | 30.000 | 30.000 |
| 1.428E-04 | 35.000 | 35.000 |
| 1.265E-04 | 40.000 | 40.000 |
| 1.123E-04 | 45.000 | 45.000 |
| 1.000E-04 | 50.000 | 50.000 |
| 8.920E-05 | 55.000 | 55.000 |
| 8.064E-05 | 60.000 | 60.000 |
| 7.266E-05 | 65.000 | 65.000 |
| 6.509E-05 | 70.000 | 70.000 |
| 5.774E-05 | 75.000 | 75.000 |
| 5.053E-05 | 80.000 | 80.000 |
| 4.235E-05 | 85.000 | 85.000 |
| 7.458E-04 | 5.0    | 5.00   |

K= 17 FIVEXQ(K)= 7.458E-04 FIVEPR(K)= 5.000

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# SITE EXCLUSION BOUNDARY CALCULATIONS:

## FIVE PERCENT OVERALL SITE LIMIT

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.253E-03 | 1.474E-03 | 8.570E-04 | 7.671E-04 | 5.195E-04 | 5.092E-04 | 5.018E-04 | 3.979E-04 | 3.953E-04 | 3.398E-04 |
| 0.043     | 0.089     | 0.096     | 1.788     | 2.897     | 3.270     | 5.374     | 5.404     | 5.886     | 8.649     |
| 0.04345   | 0.08918   | 0.09604   | 1.78825   | 2.89732   | 3.27007   | 5.37388   | 5.40361   | 5.88612   | 8.64852   |
| 3.190E-04 | 2.917E-04 | 2.586E-04 | 2.305E-04 | 2.174E-04 | 1.976E-04 | 1.735E-04 | 1.504E-04 | 1.473E-04 | 1.391E-04 |
| 8.655     | 10.302    | 12.374    | 14.272    | 14.690    | 18.649    | 19.138    | 23.988    | 25.840    | 25.996    |
| 8.65538   | 10.30185  | 12.37366  | 14.27167  | 14.69014  | 18.64852  | 19.13789  | 23.98811  | 25.84038  | 25.99588  |
| 1.376E-04 | 1.303E-04 | 1.162E-04 | 1.127E-04 | 9.806E-05 | 9.321E-05 | 9.028E-05 | 8.729E-05 | 7.863E-05 | 7.431E-05 |
| 26.005    | 35.568    | 35.591    | 38.788    | 46.021    | 46.149    | 54.397    | 54.404    | 59.120    | 59.124    |
| 26.00503  | 35.56825  | 35.59112  | 38.78801  | 46.02103  | 46.14908  | 54.39742  | 54.40428  | 59.11958  | 59.12415  |
| 7.093E-05 | 7.018E-05 | 6.796E-05 | 6.567E-05 | 5.449E-05 | 5.032E-05 | 4.933E-05 | 4.743E-05 | 4.551E-05 | 3.966E-05 |
| 59.627    | 59.655    | 66.892    | 69.611    | 75.625    | 75.694    | 78.024    | 79.319    | 83.471    | 84.084    |
| 59.62723  | 59.65467  | 66.89227  | 69.61122  | 75.62541  | 75.69402  | 78.02424  | 79.31854  | 83.47129  | 84.08414  |
| 3.829E-05 | 3.570E-05 | 3.419E-05 | 2.862E-05 | 2.858E-05 | 2.749E-05 | 2.560E-05 | 2.391E-05 | 1.927E-05 | 1.796E-05 |
| 84.349    | 85.541    | 88.976    | 89.858    | 89.899    | 90.766    | 91.768    | 92.262    | 93.135    | 93.490    |
| 84.34940  | 85.54082  | 88.97552  | 89.85822  | 89.89938  | 90.76606  | 91.76765  | 92.26160  | 93.13514  | 93.48959  |
| 1.746E-05 | 1.615E-05 | 1.545E-05 | 1.444E-05 | 1.328E-05 | 1.291E-05 | 1.119E-05 | 9.696E-06 | 8.882E-06 | 7.796E-06 |
| 93.524    | 93.727    | 94.423    | 94.471    | 94.729    | 95.134    | 95.280    | 95.534    | 96.730    | 96.767    |
| 93.52389  | 93.72740  | 94.42257  | 94.47060  | 94.72899  | 95.13375  | 95.28010  | 95.53393  | 96.72990  | 96.76649  |
| 6.686E-06 | 5.881E-06 | 5.361E-06 | 4.477E-06 | 3.363E-06 | 3.175E-06 | 2.704E-06 | 1.101E-06 |           |           |
| 98.006    | 98.029    | 99.088    | 99.598    | 99.936    | 99.945    | 99.973    | 100.000   |           |           |
| 98.00592  | 98.02879  | 99.08754  | 99.59749  | 99.93593  | 99.94508  | 99.97251  | 99.99995  |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 18.652

| K  | I | XQSAVE(K, I) | XQINT(K, I)  | XQSLOP(K, I) |
|----|---|--------------|--------------|--------------|
| 18 | 1 | -6.09537     | -9.00325     | -0.87322     |
| 18 | 2 | -7.59738     | -9.68374     | -1.29589     |
| 18 | 3 | -8.52936     | -9.24120     | -0.79911     |
| 18 | 4 | -8.94587     | -9.22838     | -0.76442     |
| 18 | 5 | -9.31262     | -9.22551     | -0.79051     |
| 18 | 6 | -9.63092     | -9.22209     | -0.79718     |
| 18 | 7 | -9.99767     | -8.89545     | -1.13291     |
| 18 | 8 | -10.28369    | NUMXQ(K) = 8 |              |
|    |   | 9.383E-04    | 1.000        | 1.000        |
|    |   | 6.359E-04    | 3.000        | 3.000        |
|    |   | 5.174E-04    | 5.000        | 5.000        |
|    |   | 3.279E-04    | 10.000       | 10.000       |
|    |   | 2.386E-04    | 15.000       | 15.000       |
|    |   | 1.899E-04    | 20.000       | 20.000       |
|    |   | 1.662E-04    | 25.000       | 25.000       |
|    |   | 1.474E-04    | 30.000       | 30.000       |
|    |   | 1.319E-04    | 35.000       | 35.000       |
|    |   | 1.192E-04    | 40.000       | 40.000       |
|    |   | 1.081E-04    | 45.000       | 45.000       |
|    |   | 9.821E-05    | 50.000       | 50.000       |
|    |   | 8.920E-05    | 55.000       | 55.000       |
|    |   | 8.064E-05    | 60.000       | 60.000       |
|    |   | 7.266E-05    | 65.000       | 65.000       |
|    |   | 6.509E-05    | 70.000       | 70.000       |
|    |   | 5.774E-05    | 75.000       | 75.000       |
|    |   | 5.053E-05    | 80.000       | 80.000       |
|    |   | 4.235E-05    | 85.000       | 85.000       |
|    |   | 5.174E-04    | 5.0          | 5.00         |

K= 18 FIVEXQ(K)= 5.174E-04 FIVEPR(K)= 5.000

| K  | HIGHPR   | PR      | GRNDVT(K) |
|----|----------|---------|-----------|
| 1  | -2.81988 | 0.24021 | 4.22800   |
| 2  | -1.75742 | 3.94233 | 5.26942   |
| 3  | -2.79697 | 0.25793 | 6.10231   |
| 4  | -2.67341 | 0.37542 | 5.98233   |
| 5  | -2.57624 | 0.49942 | 5.25961   |
| 6  | -2.79281 | 0.26127 | 4.65728   |
| 7  | -2.99900 | 0.13544 | 4.98165   |
| 8  | -3.13939 | 0.08466 | 6.51959   |
| 9  | -3.19979 | 0.06877 | 6.53955   |
| 10 | -3.17950 | 0.07377 | 7.74017   |

|    |          |         |         |
|----|----------|---------|---------|
| 11 | -3.12734 | 0.08820 | 5.87912 |
| 12 | -2.76312 | 0.28626 | 7.24032 |
| 13 | -2.73655 | 0.31044 | 8.51913 |
| 14 | -2.62932 | 0.42779 | 9.11977 |
| 15 | -2.69567 | 0.35124 | 6.29520 |
| 16 | -2.77938 | 0.27232 | 5.66654 |

|    |           |           |
|----|-----------|-----------|
| K  | HOURS (K) | TOTHR     |
| 1  | 21.04263  | 21.04263  |
| 2  | 345.34800 | 366.39060 |
| 3  | 22.59442  | 388.98500 |
| 4  | 32.88678  | 421.87180 |
| 5  | 43.74879  | 465.62060 |
| 6  | 22.88734  | 488.50790 |
| 7  | 11.86451  | 500.37240 |
| 8  | 7.41591   | 507.78830 |
| 9  | 6.02441   | 513.81270 |
| 10 | 6.46249   | 520.27520 |
| 11 | 7.72658   | 528.00180 |
| 12 | 25.07666  | 553.07840 |
| 13 | 27.19497  | 580.27340 |
| 14 | 37.47427  | 617.74760 |
| 15 | 30.76847  | 648.51610 |
| 16 | 23.85486  | 672.37100 |

| K | FIVEXQ    | SVANN     | SLTIME  | TIMINT  | I | TIME  | XQT       |
|---|-----------|-----------|---------|---------|---|-------|-----------|
| 1 | 3.377E-04 | 4.555E-06 | -0.5135 | -7.6374 | 1 | 8.0   | -8.70527  |
|   |           |           |         |         | 2 | 16.0  | -9.06123  |
|   |           |           |         |         | 3 | 72.0  | -9.83362  |
|   |           |           |         |         | 4 | 624.0 | -10.94259 |
| 2 | 3.020E-04 | 4.650E-06 | -0.4977 | -7.7601 | 1 | 8.0   | -8.79515  |
|   |           |           |         |         | 2 | 16.0  | -9.14016  |
|   |           |           |         |         | 3 | 72.0  | -9.88881  |
|   |           |           |         |         | 4 | 624.0 | -10.96367 |
| 3 | 3.794E-04 | 5.897E-06 | -0.4966 | -7.5326 | 1 | 8.0   | -8.56532  |
|   |           |           |         |         | 2 | 16.0  | -8.90955  |
|   |           |           |         |         | 3 | 72.0  | -9.65651  |
|   |           |           |         |         | 4 | 624.0 | -10.72895 |
| 4 | 4.962E-04 | 7.880E-06 | -0.4941 | -7.2661 | 1 | 8.0   | -8.29349  |
|   |           |           |         |         | 2 | 16.0  | -8.63594  |
|   |           |           |         |         | 3 | 72.0  | -9.37903  |
|   |           |           |         |         | 4 | 624.0 | -10.44592 |
| 5 | 5.707E-04 | 8.804E-06 | -0.4975 | -7.1238 | 1 | 8.0   | -8.15833  |
|   |           |           |         |         | 2 | 16.0  | -8.50318  |
|   |           |           |         |         | 3 | 72.0  | -9.25147  |
|   |           |           |         |         | 4 | 624.0 | -10.32583 |

|    |           |           |         |         |   |                 |
|----|-----------|-----------|---------|---------|---|-----------------|
| 6  | 4.306E-04 | 6.280E-06 | -0.5042 | -7.4007 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.44923    |
|    |           |           |         |         | 2 | 16.0 -8.79873   |
|    |           |           |         |         | 3 | 72.0 -9.55711   |
|    |           |           |         |         | 4 | 624.0 -10.64596 |
| 7  | 2.922E-04 | 4.500E-06 | -0.4977 | -7.7932 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.82813    |
|    |           |           |         |         | 2 | 16.0 -9.17311   |
|    |           |           |         |         | 3 | 72.0 -9.92171   |
|    |           |           |         |         | 4 | 624.0 -10.99650 |
| 8  | 2.294E-04 | 4.280E-06 | -0.4748 | -8.0508 |   |                 |
|    |           |           |         |         | 1 | 8.0 -9.03825    |
|    |           |           |         |         | 2 | 16.0 -9.36739   |
|    |           |           |         |         | 3 | 72.0 -10.08160  |
|    |           |           |         |         | 4 | 624.0 -11.10703 |
| 9  | 1.886E-04 | 3.427E-06 | -0.4780 | -8.2445 |   |                 |
|    |           |           |         |         | 1 | 8.0 -9.23849    |
|    |           |           |         |         | 2 | 16.0 -9.56981   |
|    |           |           |         |         | 3 | 72.0 -10.28875  |
|    |           |           |         |         | 4 | 624.0 -11.32097 |
| 10 | 2.142E-04 | 3.939E-06 | -0.4766 | -8.1181 |   |                 |
|    |           |           |         |         | 1 | 8.0 -9.10917    |
|    |           |           |         |         | 2 | 16.0 -9.43952   |
|    |           |           |         |         | 3 | 72.0 -10.15633  |
|    |           |           |         |         | 4 | 624.0 -11.18551 |
| 11 | 2.046E-04 | 3.502E-06 | -0.4851 | -8.1580 |   |                 |
|    |           |           |         |         | 1 | 8.0 -9.16683    |
|    |           |           |         |         | 2 | 16.0 -9.50309   |
|    |           |           |         |         | 3 | 72.0 -10.23276  |
|    |           |           |         |         | 4 | 624.0 -11.28038 |
| 12 | 4.637E-04 | 6.082E-06 | -0.5169 | -7.3180 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.39277    |
|    |           |           |         |         | 2 | 16.0 -8.75104   |
|    |           |           |         |         | 3 | 72.0 -9.52845   |
|    |           |           |         |         | 4 | 624.0 -10.64462 |
| 13 | 4.715E-04 | 7.700E-06 | -0.4907 | -7.3195 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.33990    |
|    |           |           |         |         | 2 | 16.0 -8.68004   |
|    |           |           |         |         | 3 | 72.0 -9.41811   |
|    |           |           |         |         | 4 | 624.0 -10.47780 |
| 14 | 5.370E-04 | 8.960E-06 | -0.4882 | -7.1911 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.20623    |
|    |           |           |         |         | 2 | 16.0 -8.54460   |
|    |           |           |         |         | 3 | 72.0 -9.27884   |
|    |           |           |         |         | 4 | 624.0 -10.33302 |
| 15 | 4.681E-04 | 6.713E-06 | -0.5062 | -7.3160 |   |                 |
|    |           |           |         |         | 1 | 8.0 -8.36861    |
|    |           |           |         |         | 2 | 16.0 -8.71949   |
|    |           |           |         |         | 3 | 72.0 -9.48087   |
|    |           |           |         |         | 4 | 624.0 -10.57402 |
| 16 | 3.556E-04 | 5.289E-06 | -0.5019 | -7.5938 |   |                 |

|    |           |           |         |         |   |       |           |
|----|-----------|-----------|---------|---------|---|-------|-----------|
| 17 | 7.458E-04 | 8.960E-06 | -0.5273 | -6.8356 | 1 | 8.0   | -8.63744  |
|    |           |           |         |         | 2 | 16.0  | -8.98531  |
|    |           |           |         |         | 3 | 72.0  | -9.74016  |
|    |           |           |         |         | 4 | 624.0 | -10.82395 |
| 18 | 5.174E-04 | 8.960E-06 | -0.4837 | -7.2313 | 1 | 8.0   | -7.93213  |
|    |           |           |         |         | 2 | 16.0  | -8.29764  |
|    |           |           |         |         | 3 | 72.0  | -9.09078  |
|    |           |           |         |         | 4 | 624.0 | -10.22954 |
|    |           |           |         |         | 1 | 8.0   | -8.23722  |
|    |           |           |         |         | 2 | 16.0  | -8.57252  |
|    |           |           |         |         | 3 | 72.0  | -9.30009  |
|    |           |           |         |         | 4 | 624.0 | -10.34471 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

RELATIVE CONCENTRATION (X/Q) VALUES (SEC/CUBIC METER)  
VERSUS  
AVERAGING TIME

| DOWNWIND DISTANCE |      |           |           |            |          |           |                | HOURS PER YEAR MAX               | DOWNWIND |
|-------------------|------|-----------|-----------|------------|----------|-----------|----------------|----------------------------------|----------|
| SECTOR (METERS)   |      | 0-2 HOURS | 0-8 HOURS | 8-24 HOURS | 1-4 DAYS | 4-30 DAYS | ANNUAL AVERAGE | 0-2 HR X/Q IS EXCEEDED IN SECTOR |          |
| S                 | 485. | 3.38E-04  | 1.66E-04  | 1.16E-04   | 5.36E-05 | 1.77E-05  | 4.55E-06       | 21.0                             | S        |
| SSW               | 485. | 3.02E-04  | 1.51E-04  | 1.07E-04   | 5.07E-05 | 1.73E-05  | 4.65E-06       | 345.3                            | SSW      |
| SW                | 485. | 3.79E-04  | 1.91E-04  | 1.35E-04   | 6.40E-05 | 2.19E-05  | 5.90E-06       | 22.6                             | SW       |
| WSW               | 485. | 4.96E-04  | 2.50E-04  | 1.78E-04   | 8.45E-05 | 2.91E-05  | 7.88E-06       | 32.9                             | WSW      |
| W                 | 485. | 5.71E-04  | 2.86E-04  | 2.03E-04   | 9.60E-05 | 3.28E-05  | 8.80E-06       | 43.7                             | W        |
| WNW               | 485. | 4.31E-04  | 2.14E-04  | 1.51E-04   | 7.07E-05 | 2.38E-05  | 6.28E-06       | 22.9                             | WNW      |
| NW                | 485. | 2.92E-04  | 1.47E-04  | 1.04E-04   | 4.91E-05 | 1.68E-05  | 4.50E-06       | 11.9                             | NW       |
| NNW               | 485. | 2.29E-04  | 1.19E-04  | 8.55E-05   | 4.18E-05 | 1.50E-05  | 4.28E-06       | 7.4                              | NNW      |
| N                 | 485. | 1.89E-04  | 9.72E-05  | 6.98E-05   | 3.40E-05 | 1.21E-05  | 3.43E-06       | 6.0                              | N        |
| NNE               | 485. | 2.14E-04  | 1.11E-04  | 7.95E-05   | 3.88E-05 | 1.39E-05  | 3.94E-06       | 6.5                              | NNE      |
| NE                | 485. | 2.05E-04  | 1.04E-04  | 7.46E-05   | 3.60E-05 | 1.26E-05  | 3.50E-06       | 7.7                              | NE       |
| ENE               | 485. | 4.64E-04  | 2.26E-04  | 1.58E-04   | 7.28E-05 | 2.38E-05  | 6.08E-06       | 25.1                             | ENE      |
| E                 | 485. | 4.71E-04  | 2.39E-04  | 1.70E-04   | 8.12E-05 | 2.82E-05  | 7.70E-06       | 27.2                             | E        |
| ESE               | 485. | 5.37E-04  | 2.73E-04  | 1.95E-04   | 9.34E-05 | 3.25E-05  | 8.96E-06       | 37.5                             | ESE      |
| SE                | 485. | 4.68E-04  | 2.32E-04  | 1.63E-04   | 7.63E-05 | 2.56E-05  | 6.71E-06       | 30.8                             | SE       |
| SSE               | 485. | 3.56E-04  | 1.77E-04  | 1.25E-04   | 5.89E-05 | 1.99E-05  | 5.29E-06       | 23.9                             | SSE      |
| MAX X/Q           |      | 5.71E-04  |           |            |          |           |                | TOTAL HOURS AROUND SITE: 672.4   |          |
| SRP 2.3.4         | 485. | 7.46E-04  | 3.59E-04  | 2.49E-04   | 1.13E-04 | 3.61E-05  | 8.96E-06       |                                  |          |
| SITE LIMIT        |      | 5.17E-04  | 2.65E-04  | 1.89E-04   | 9.14E-05 | 3.22E-05  | 8.96E-06       |                                  |          |

THE FIVE-PERCENT-FOR-THE-ENTIRE-SITE X/Q IS LIMITING.

\*\*NOTE\*\*: VALUES ON THIS PAGE ARE APPROXIMATIONS ONLY.  
CHECK THE REASONABLENESS OF THE ENVELOPES  
COMPUTED FOR THE 0-2 HOUR VALUES. FOR ANY  
FAULTY ENVELOPES, ADJUST THE ABOVE VALUES.



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE S SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 3.0       | 1.46      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 1.78      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 1.68      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.65      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.11      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| B              | 2.0       | 0.16      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 1.14      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 1.24      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.54      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 6.0       | 0.49      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B              | 8.0       | 0.11      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| C              | 1.5       | 0.05      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.59      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 1.14      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 1.46      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 1.03      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.54      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 0.22      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C              | 9.9       | 0.05      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
| D              | 1.0       | 0.49      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D              | 1.5       | 1.68      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D              | 2.0       | 3.84      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 189.6      | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D              | 3.0       | 9.03      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 162.1      | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D              | 4.0       | 8.98      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 146.5      | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D              | 5.0       | 5.41      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 136.2      | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D              | 6.0       | 3.84      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.8      | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D              | 8.0       | 1.78      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D              | 9.9       | 0.54      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 5.257E-06                         | 4.886E-06 | 4.886E-06 |
| E              | 0.4       | 0.01      | 1810.    | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 1.568E-04                         | 2.653E-04 | 1.568E-04 |
| E              | 1.0       | 2.33      | 1810.    | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 5.339E-05                         | 9.030E-05 | 5.339E-05 |
| E              | 1.5       | 4.54      | 1810.    | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 3.616E-05                         | 6.115E-05 | 3.616E-05 |
| E              | 2.0       | 5.35      | 1810.    | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 2.752E-05                         | 4.654E-05 | 2.752E-05 |
| E              | 3.0       | 10.17     | 1810.    | 0.         | 0.           | 91.5    | 32.3    | 135.6      | 2.430E-05                         | 3.112E-05 | 2.430E-05 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B | APPENDIX BB-7 |  |  |  | PAGE NO. 86 of 160 |
|--|--|--|--|--|--|-------------------|---------------|--|--|--|--------------------|
|--|--|--|--|--|--|-------------------|---------------|--|--|--|--------------------|

|   |      |      |       |    |    |      |      |       |           |           |           |
|---|------|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 4.0  | 6.76 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 2.49 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 2.11 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 1.46 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.76 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.05 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| F | 0.4  | 0.08 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 3.46 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 2.43 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 2.43 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 1.14 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| G | 0.4  | 0.07 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 2.81 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.97 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.43 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.05 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.05 | 1810. | 0. | 0. | 43.6 | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

S SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.072     | 0.147     | 0.157     | 2.970     | 3.943     | 7.405     | 7.459     | 7.891     | 7.946     | 10.379    |
| 0.00305   | 0.00623   | 0.00664   | 0.12556   | 0.16672   | 0.31307   | 0.31536   | 0.33365   | 0.33594   | 0.43884   |
| 5.339E-05 | 4.920E-05 | 4.786E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 |
| 12.705    | 15.139    | 16.275    | 20.818    | 21.305    | 26.659    | 36.827    | 38.504    | 45.265    | 47.753    |
| 0.53717   | 0.64008   | 0.68810   | 0.88019   | 0.90077   | 1.12716   | 1.55707   | 1.62796   | 1.91380   | 2.01899   |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 |
| 51.593    | 53.702    | 62.735    | 64.195    | 73.173    | 73.227    | 78.636    | 79.393    | 83.233    | 83.828    |
| 2.18135   | 2.27054   | 2.65243   | 2.71417   | 3.09377   | 3.09606   | 3.32473   | 3.35675   | 3.51911   | 3.54426   |
| 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 |
| 85.613    | 86.749    | 87.290    | 88.750    | 88.804    | 89.832    | 89.994    | 90.535    | 91.671    | 91.887    |
| 3.61972   | 3.66775   | 3.69061   | 3.75236   | 3.75464   | 3.79809   | 3.80495   | 3.82782   | 3.87584   | 3.88499   |
| 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 |
| 91.941    | 93.185    | 93.726    | 94.213    | 94.321    | 95.781    | 97.566    | 99.243    | 99.892    | 100.000   |
| 3.88727   | 3.93987   | 3.96274   | 3.98332   | 3.98789   | 4.04963   | 4.12510   | 4.19599   | 4.22343   | 4.22800   |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.125  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.313  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.687  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 1.912  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.091  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 3.354  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 3.541

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 1 | 1 | -7.71082     | -12.09005   | -1.09243     |
| 1 | 2 | -8.78838     | -13.70105   | -1.62547     |
| 1 | 3 | -9.25677     | -16.24183   | -2.55475     |
| 1 | 4 | -9.94734     | -14.90189   | -2.01091     |
| 1 | 5 | -10.73463    | -17.27135   | -3.15429     |
| 1 | 6 | -11.38039    | -20.94877   | -5.12335     |
| 1 | 7 | -11.56701    | -23.90543   | -6.73796     |
| 1 | 8 | -11.73251    | NUMXQ(K)= 8 |              |
|   |   | 2.152E-04    | 0.042       | 1.000        |
|   |   | 1.517E-04    | 0.127       | 3.000        |
|   |   | 1.173E-04    | 0.211       | 5.000        |
|   |   | 7.386E-05    | 0.423       | 10.000       |
|   |   | 5.155E-05    | 0.634       | 15.000       |
|   |   | 4.117E-05    | 0.846       | 20.000       |
|   |   | 3.483E-05    | 1.057       | 25.000       |
|   |   | 3.028E-05    | 1.268       | 30.000       |
|   |   | 2.682E-05    | 1.480       | 35.000       |
|   |   | 2.409E-05    | 1.691       | 40.000       |
|   |   | 2.188E-05    | 1.903       | 45.000       |
|   |   | 1.913E-05    | 2.114       | 50.000       |
|   |   | 1.686E-05    | 2.325       | 55.000       |
|   |   | 1.500E-05    | 2.537       | 60.000       |
|   |   | 1.345E-05    | 2.748       | 65.000       |
|   |   | 1.214E-05    | 2.960       | 70.000       |
|   |   | 1.079E-05    | 3.171       | 75.000       |
|   |   | 9.257E-06    | 3.382       | 80.000       |
|   |   | 6.377E-05    | 0.5         | 11.83        |

ANNUAL AVERAGE = 5.72E-07

K= 1 FIVEXQ(K)= 6.377E-05 FIVEPR(K)=11.826

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSW SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT<br>METERS | EFF<br>METERS | PLUME<br>METERS | HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) |           |      |
|-----------------|--|----------------------|--------------------|-------------------|--------------|---------------|-----------------|--------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|------|
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      | MEANDER                           | BLDG WAKE | USED |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      | CA=1459.SQ.METERS                 |           |      |
| A               | 2.0                                      | 0.22                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 4.927E-07         | 4.919E-07            | 4.919E-07                         |           |      |
| A               | 3.0                                      | 0.65                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 3.294E-07         | 3.289E-07            | 3.289E-07                         |           |      |
| A               | 4.0                                      | 1.78                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 2.480E-07         | 2.476E-07            | 2.476E-07                         |           |      |
| A               | 5.0                                      | 1.74                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 1.988E-07         | 1.985E-07            | 1.985E-07                         |           |      |
| A               | 6.0                                      | 0.43                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 1.660E-07         | 1.658E-07            | 1.658E-07                         |           |      |
| A               | 8.0                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 1.247E-07         | 1.246E-07            | 1.246E-07                         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |           |      |
| B               | 1.5                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 4.107E-06         | 4.069E-06            | 4.069E-06                         |           |      |
| B               | 2.0                                      | 0.13                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 3.125E-06         | 3.096E-06            | 3.096E-06                         |           |      |
| B               | 3.0                                      | 0.74                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 2.089E-06         | 2.070E-06            | 2.070E-06                         |           |      |
| B               | 4.0                                      | 1.13                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 1.573E-06         | 1.558E-06            | 1.558E-06                         |           |      |
| B               | 5.0                                      | 0.87                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 1.261E-06         | 1.250E-06            | 1.250E-06                         |           |      |
| B               | 6.0                                      | 0.52                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 1.053E-06         | 1.044E-06            | 1.044E-06                         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |           |      |
| C               | 1.5                                      | 0.13                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 1.081E-05         | 1.055E-05            | 1.055E-05                         |           |      |
| C               | 2.0                                      | 0.56                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 8.223E-06         | 8.029E-06            | 8.029E-06                         |           |      |
| C               | 3.0                                      | 1.08                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 5.498E-06         | 5.368E-06            | 5.368E-06                         |           |      |
| C               | 4.0                                      | 1.17                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 4.139E-06         | 4.041E-06            | 4.041E-06                         |           |      |
| C               | 5.0                                      | 0.78                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 3.318E-06         | 3.240E-06            | 3.240E-06                         |           |      |
| C               | 6.0                                      | 0.52                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 2.771E-06         | 2.706E-06            | 2.706E-06                         |           |      |
| C               | 8.0                                      | 0.17                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 2.082E-06         | 2.033E-06            | 2.033E-06                         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |           |      |
| D               | 1.0                                      | 0.91                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 190.3             | 3.389E-05         | 4.657E-05            | 3.389E-05                         |           |      |
| D               | 1.5                                      | 2.21                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 190.3             | 2.295E-05         | 3.154E-05            | 2.295E-05                         |           |      |
| D               | 2.0                                      | 3.04                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 189.6             | 1.753E-05         | 2.400E-05            | 1.753E-05                         |           |      |
| D               | 3.0                                      | 9.63                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 162.1             | 1.371E-05         | 1.605E-05            | 1.371E-05                         |           |      |
| D               | 4.0                                      | 8.51                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 146.5             | 1.142E-05         | 1.208E-05            | 1.142E-05                         |           |      |
| D               | 5.0                                      | 8.42                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 136.2             | 9.848E-06         | 9.685E-06            | 9.685E-06                         |           |      |
| D               | 6.0                                      | 6.42                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 128.8             | 8.699E-06         | 8.088E-06            | 8.088E-06                         |           |      |
| D               | 8.0                                      | 2.86                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 128.7             | 6.538E-06         | 6.076E-06            | 6.076E-06                         |           |      |
| D               | 9.9                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 128.7             | 5.257E-06         | 4.886E-06            | 4.886E-06                         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |           |      |
| E               | 0.4                                      | 0.01                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 1.568E-04         | 2.653E-04            | 1.568E-04                         |           |      |
| E               | 1.0                                      | 2.17                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 5.339E-05         | 9.030E-05            | 5.339E-05                         |           |      |
| E               | 1.5                                      | 4.08                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 3.616E-05         | 6.115E-05            | 3.616E-05                         |           |      |
| E               | 2.0                                      | 5.42                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 2.752E-05         | 4.654E-05            | 2.752E-05                         |           |      |
| E               | 3.0                                      | 10.33                | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 135.6             | 2.430E-05         | 3.112E-05            | 2.430E-05                         |           |      |

|   |     |      |       |    |    |      |      |       |           |           |           |
|---|-----|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 4.0 | 5.60 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0 | 3.78 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9 | 2.26 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9 | 3.08 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8 | 0.61 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| F | 0.4 | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0 | 1.95 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5 | 1.30 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0 | 1.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0 | 0.39 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 9.8 | 0.17 | 1810. | 0. | 0. | 63.2 | 21.0 | 63.2  | 2.439E-05 | 1.807E-05 | 1.807E-05 |
| G | 0.4 | 0.05 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0 | 1.91 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5 | 0.87 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0 | 0.13 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0 | 0.04 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SSW SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.049     | 0.091     | 0.101     | 2.010     | 2.878     | 4.831     | 4.874     | 5.004     | 6.306     | 8.476     |
| 0.00258   | 0.00482   | 0.00530   | 0.10591   | 0.15165   | 0.25455   | 0.25684   | 0.26370   | 0.33230   | 0.44664   |
| 4.920E-05 | 4.786E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 | 1.807E-05 |
| 9.518     | 9.908     | 13.988    | 14.899    | 20.323    | 30.652    | 32.865    | 38.463    | 42.239    | 42.412    |
| 0.50152   | 0.52210   | 0.73706   | 0.78508   | 1.07093   | 1.61518   | 1.73180   | 2.02679   | 2.22574   | 2.23489   |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 |
| 45.450    | 47.707    | 57.341    | 60.422    | 68.928    | 69.058    | 77.477    | 78.085    | 84.507    | 85.071    |
| 2.39496   | 2.51387   | 3.02153   | 3.18389   | 3.63210   | 3.63896   | 4.08259   | 4.11460   | 4.45304   | 4.48277   |
| 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 |
| 87.936    | 89.021    | 89.064    | 89.107    | 90.279    | 91.060    | 91.190    | 91.711    | 92.449    | 92.623    |
| 4.63370   | 4.69087   | 4.69315   | 4.69544   | 4.75718   | 4.79835   | 4.80521   | 4.83265   | 4.87152   | 4.88067   |
| 1.558E-06 | 1.250E-06 | 1.044E-06 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 |           |
| 93.751    | 94.619    | 95.140    | 95.357    | 96.007    | 97.787    | 99.523    | 99.957    | 100.000   |           |
| 4.94012   | 4.98586   | 5.01330   | 5.02473   | 5.05904   | 5.15279   | 5.24426   | 5.26713   | 5.26942   |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2) = 0.106  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3) = 0.254  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4) = 1.070  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6) = 2.025  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7) = 3.629  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8) = 4.079

| K | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|---|---|-------------|-------------|-------------|
| 2 | 1 | -7.71082    | -12.18668   | -1.10571    |
| 2 | 2 | -8.78838    | -14.08399   | -1.72304    |
| 2 | 3 | -9.25677    | -16.21843   | -2.48491    |
| 2 | 4 | -10.50075   | -12.29200   | -0.77848    |
| 2 | 5 | -10.62522   | -13.16077   | -1.18424    |
| 2 | 6 | -10.73463   | -15.95933   | -2.55027    |
| 2 | 7 | -11.38039   | -16.86238   | -3.05323    |
| 2 | 8 | -11.54497   | NUMXQ(K)= 8 |             |
|   |   | 1.908E-04   | 0.053       | 1.000       |
|   |   | 1.237E-04   | 0.158       | 3.000       |
|   |   | 9.286E-05   | 0.263       | 5.000       |
|   |   | 5.212E-05   | 0.527       | 10.000      |
|   |   | 3.642E-05   | 0.790       | 15.000      |
|   |   | 2.793E-05   | 1.054       | 20.000      |
|   |   | 2.587E-05   | 1.317       | 25.000      |
|   |   | 2.446E-05   | 1.581       | 30.000      |
|   |   | 2.280E-05   | 1.844       | 35.000      |
|   |   | 2.089E-05   | 2.108       | 40.000      |
|   |   | 1.841E-05   | 2.371       | 45.000      |
|   |   | 1.642E-05   | 2.635       | 50.000      |
|   |   | 1.477E-05   | 2.898       | 55.000      |
|   |   | 1.339E-05   | 3.162       | 60.000      |
|   |   | 1.222E-05   | 3.425       | 65.000      |
|   |   | 1.117E-05   | 3.689       | 70.000      |
|   |   | 1.014E-05   | 3.952       | 75.000      |
|   |   | 5.453E-05   | 0.5         | 9.49        |

ANNUAL AVERAGE = 6.06E-07

K= 2 FIVEXQ(K)= 5.453E-05 FIVEPR(K)= 9.489



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SW SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |           |      |
| A               | 1.5                                      | 0.07                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 6.474E-07                         | 6.465E-07 | 6.465E-07 |      |
| A               | 2.0                                      | 0.52                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 4.927E-07                         | 4.919E-07 | 4.919E-07 |      |
| A               | 3.0                                      | 2.51                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |      |
| A               | 4.0                                      | 2.06                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |      |
| A               | 5.0                                      | 0.94                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |      |
| A               | 6.0                                      | 0.19                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| B               | 1.0                                      | 0.04                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 6.064E-06                         | 6.008E-06 | 6.008E-06 |      |
| B               | 1.5                                      | 0.15                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06 | 4.069E-06 |      |
| B               | 2.0                                      | 0.34                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |      |
| B               | 3.0                                      | 1.16                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |      |
| B               | 4.0                                      | 1.27                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |      |
| B               | 5.0                                      | 0.49                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |      |
| B               | 6.0                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |      |
| B               | 8.0                                      | 0.04                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07 | 7.840E-07 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| C               | 1.5                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05 | 1.055E-05 |      |
| C               | 2.0                                      | 0.86                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |      |
| C               | 3.0                                      | 1.50                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |      |
| C               | 4.0                                      | 1.35                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |      |
| C               | 5.0                                      | 0.86                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |      |
| C               | 6.0                                      | 0.15                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06 | 2.706E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| D               | 1.0                                      | 0.56                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |      |
| D               | 1.5                                      | 3.37                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |      |
| D               | 2.0                                      | 4.83                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |      |
| D               | 3.0                                      | 11.80                | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |      |
| D               | 4.0                                      | 9.82                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |      |
| D               | 5.0                                      | 7.34                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |      |
| D               | 6.0                                      | 4.16                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |      |
| D               | 8.0                                      | 0.49                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06 | 6.076E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| E               | 0.4                                      | 0.01                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 1.568E-04                         | 2.653E-04 | 1.568E-04 |      |
| E               | 1.0                                      | 3.19                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 5.339E-05                         | 9.030E-05 | 5.339E-05 |      |
| E               | 1.5                                      | 5.47                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 3.616E-05                         | 6.115E-05 | 3.616E-05 |      |
| E               | 2.0                                      | 5.85                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 2.752E-05                         | 4.654E-05 | 2.752E-05 |      |
| E               | 3.0                                      | 7.57                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 135.6                | 2.430E-05                         | 3.112E-05 | 2.430E-05 |      |

|   |     |      |       |    |    |      |      |       |           |           |           |
|---|-----|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 4.0 | 5.73 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0 | 2.47 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9 | 1.76 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9 | 2.81 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8 | 0.11 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| F | 0.4 | 0.07 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0 | 3.15 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5 | 1.39 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0 | 0.37 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0 | 0.15 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0 | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 7.9 | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 63.2  | 3.033E-05 | 2.248E-05 | 2.248E-05 |
| F | 9.8 | 0.30 | 1810. | 0. | 0. | 63.2 | 21.0 | 63.2  | 2.439E-05 | 1.807E-05 | 1.807E-05 |
| G | 0.4 | 0.05 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0 | 1.99 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5 | 0.37 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

SW SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 6.465E-05 | 5.339E-05 | 4.920E-05 | 4.786E-05 |
| 0.051     | 0.119     | 0.133     | 2.119     | 2.494     | 5.641     | 7.028     | 10.213    | 10.588    | 10.738    |
| 0.00311   | 0.00729   | 0.00810   | 0.12930   | 0.15216   | 0.34425   | 0.42886   | 0.62324   | 0.64610   | 0.65525   |
| 4.469E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.248E-05 | 2.178E-05 | 1.878E-05 | 1.807E-05 |
| 10.775    | 16.246    | 16.808    | 22.654    | 30.224    | 33.597    | 33.634    | 39.368    | 41.841    | 42.141    |
| 0.65754   | 0.99140   | 1.02571   | 1.38244   | 1.84437   | 2.05017   | 2.05246   | 2.40234   | 2.55326   | 2.57156   |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 |
| 46.975    | 48.736    | 60.540    | 63.351    | 73.169    | 73.281    | 80.626    | 80.739    | 84.898    | 85.760    |
| 2.86655   | 2.97403   | 3.69435   | 3.86586   | 4.46499   | 4.47185   | 4.92006   | 4.92692   | 5.18075   | 5.23334   |
| 6.076E-06 | 6.008E-06 | 5.368E-06 | 4.069E-06 | 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 1.558E-06 |
| 86.247    | 86.285    | 87.784    | 87.933    | 89.283    | 90.144    | 90.482    | 90.632    | 91.793    | 93.067    |
| 5.26307   | 5.26536   | 5.35683   | 5.36598   | 5.44830   | 5.50089   | 5.52148   | 5.53062   | 5.60151   | 5.67926   |
| 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.465E-07 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |           |
| 93.555    | 93.667    | 93.704    | 93.779    | 94.304    | 96.815    | 98.876    | 99.813    | 100.000   |           |
| 5.70899   | 5.71585   | 5.71814   | 5.72271   | 5.75472   | 5.90794   | 6.03371   | 6.09088   | 6.10231   |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.129  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.344  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 1.842  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 4.461  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 4.916

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 3 | 1 | -7.71082     | -12.06573   | -1.08759     |
| 3 | 2 | -8.78838     | -13.33164   | -1.50768     |
| 3 | 3 | -9.25677     | -15.26786   | -2.22407     |
| 3 | 4 | -10.62522    | -12.70037   | -0.99411     |
| 3 | 5 | -10.73463    | -15.32931   | -2.32361     |
| 3 | 6 | -11.38039    | -17.40055   | -3.54236     |
| 3 | 7 | -11.54497    | NUMXQ(K)= 7 |              |
|   |   | 1.939E-04    | 0.061       | 1.000        |
|   |   | 1.298E-04    | 0.183       | 3.000        |
|   |   | 1.014E-04    | 0.305       | 5.000        |
|   |   | 6.171E-05    | 0.610       | 10.000       |
|   |   | 4.452E-05    | 0.915       | 15.000       |
|   |   | 3.496E-05    | 1.220       | 20.000       |
|   |   | 2.879E-05    | 1.526       | 25.000       |
|   |   | 2.446E-05    | 1.831       | 30.000       |
|   |   | 2.288E-05    | 2.136       | 35.000       |
|   |   | 2.144E-05    | 2.441       | 40.000       |
|   |   | 1.906E-05    | 2.746       | 45.000       |
|   |   | 1.712E-05    | 3.051       | 50.000       |
|   |   | 1.551E-05    | 3.356       | 55.000       |
|   |   | 1.415E-05    | 3.661       | 60.000       |
|   |   | 1.299E-05    | 3.967       | 65.000       |
|   |   | 1.199E-05    | 4.272       | 70.000       |
|   |   | 1.095E-05    | 4.577       | 75.000       |
|   |   | 9.815E-06    | 4.882       | 80.000       |
|   |   | 7.205E-05    | 0.5         | 8.19         |

ANNUAL AVERAGE = 7.70E-07

K= 3 FIVEXQ(K)= 7.205E-05 FIVEPR(K)= 8.194

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WSW SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |           |      |
| A               | 1.5                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 6.474E-07                         | 6.465E-07 | 6.465E-07 |      |
| A               | 2.0                                      | 0.61                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 4.927E-07                         | 4.919E-07 | 4.919E-07 |      |
| A               | 3.0                                      | 1.68                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |      |
| A               | 4.0                                      | 0.73                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |      |
| A               | 5.0                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |      |
| A               | 6.0                                      | 0.04                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| B               | 1.5                                      | 0.23                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06 | 4.069E-06 |      |
| B               | 2.0                                      | 0.57                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |      |
| B               | 3.0                                      | 1.34                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |      |
| B               | 4.0                                      | 0.54                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |      |
| B               | 5.0                                      | 0.15                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |      |
| B               | 6.0                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| C               | 1.0                                      | 0.08                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 1.596E-05                         | 1.558E-05 | 1.558E-05 |      |
| C               | 1.5                                      | 0.38                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05 | 1.055E-05 |      |
| C               | 2.0                                      | 0.76                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |      |
| C               | 3.0                                      | 1.57                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |      |
| C               | 4.0                                      | 0.54                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |      |
| C               | 5.0                                      | 0.08                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| D               | 1.0                                      | 1.38                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |      |
| D               | 1.5                                      | 5.01                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |      |
| D               | 2.0                                      | 7.45                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |      |
| D               | 3.0                                      | 13.11                | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |      |
| D               | 4.0                                      | 7.76                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |      |
| D               | 5.0                                      | 3.52                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |      |
| D               | 6.0                                      | 0.76                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |      |
| E               | 0.4                                      | 0.02                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 1.568E-04                         | 2.653E-04 | 1.568E-04 |      |
| E               | 1.0                                      | 4.74                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 5.339E-05                         | 9.030E-05 | 5.339E-05 |      |
| E               | 1.5                                      | 10.05                | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 3.616E-05                         | 6.115E-05 | 3.616E-05 |      |
| E               | 2.0                                      | 8.98                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 179.1                | 2.752E-05                         | 4.654E-05 | 2.752E-05 |      |
| E               | 3.0                                      | 10.02                | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 135.6                | 2.430E-05                         | 3.112E-05 | 2.430E-05 |      |
| E               | 4.0                                      | 3.71                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 113.9                | 2.178E-05                         | 2.342E-05 | 2.178E-05 |      |
| E               | 5.0                                      | 1.30                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 100.8                | 1.973E-05                         | 1.878E-05 | 1.878E-05 |      |
| E               | 5.9                                      | 0.57                 | 1810.              | 0.                | 0.               | 0.                 | 91.5              | 32.3              | 92.0                 | 1.805E-05                         | 1.568E-05 | 1.568E-05 |      |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |     |      |       |    |    | MINOR REV. NO. 1B |      | APPENDIX BB-7 |           |           | PAGE NO. 98 of 160 |  |
|--|-----|------|-------|----|----|-------------------|------|---------------|-----------|-----------|--------------------|--|
| E  | 7.9 | 0.23 | 1810. | 0. | 0. | 91.5              | 32.3 | 91.5          | 1.363E-05 | 1.178E-05 | 1.178E-05          |  |
| F  | 0.4 | 0.09 | 1810. | 0. | 0. | 63.2              | 21.0 | 153.8         | 2.804E-04 | 5.061E-04 | 2.804E-04          |  |
| F  | 1.0 | 4.36 | 1810. | 0. | 0. | 63.2              | 21.0 | 153.8         | 9.546E-05 | 1.723E-04 | 9.546E-05          |  |
| F  | 1.5 | 2.87 | 1810. | 0. | 0. | 63.2              | 21.0 | 153.8         | 6.465E-05 | 1.167E-04 | 6.465E-05          |  |
| F  | 2.0 | 0.42 | 1810. | 0. | 0. | 63.2              | 21.0 | 153.8         | 4.920E-05 | 8.879E-05 | 4.920E-05          |  |
| F  | 3.0 | 0.15 | 1810. | 0. | 0. | 63.2              | 21.0 | 105.7         | 4.786E-05 | 5.937E-05 | 4.786E-05          |  |
| G  | 0.4 | 0.08 | 1810. | 0. | 0. | 43.6              | 13.7 | 147.9         | 4.480E-04 | 8.550E-04 | 4.480E-04          |  |
| G  | 1.0 | 3.10 | 1810. | 0. | 0. | 43.6              | 13.7 | 147.9         | 1.525E-04 | 2.911E-04 | 1.525E-04          |  |
| G  | 1.5 | 0.54 | 1810. | 0. | 0. | 43.6              | 13.7 | 147.9         | 1.033E-04 | 1.971E-04 | 1.033E-04          |  |
| G  | 2.0 | 0.11 | 1810. | 0. | 0. | 43.6              | 13.7 | 147.9         | 7.859E-05 | 1.500E-04 | 7.859E-05          |  |
| G  | 3.0 | 0.04 | 1810. | 0. | 0. | 43.6              | 13.7 | 87.7          | 8.860E-05 | 1.003E-04 | 8.860E-05          |  |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

WSW SECTOR      BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.079     | 0.174     | 0.194     | 3.290     | 3.825     | 8.183     | 8.221     | 8.336     | 11.203    | 15.943    |
| 0.00476   | 0.01042   | 0.01160   | 0.19683   | 0.22885   | 0.48954   | 0.49182   | 0.49868   | 0.67019   | 0.95375   |
|           |           |           |           |           |           |           |           |           |           |
| 4.920E-05 | 4.786E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 | 1.753E-05 |
| 16.363    | 16.516    | 26.569    | 27.945    | 36.928    | 46.943    | 51.951    | 55.659    | 56.958    | 64.412    |
| 0.97890   | 0.98805   | 1.58947   | 1.67179   | 2.20918   | 2.80831   | 3.10788   | 3.32969   | 3.40744   | 3.85336   |
|           |           |           |           |           |           |           |           |           |           |
| 1.568E-05 | 1.558E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 8.088E-06 | 8.029E-06 | 5.368E-06 |
| 64.986    | 65.062    | 78.173    | 78.403    | 86.162    | 86.545    | 90.061    | 90.826    | 91.590    | 93.158    |
| 3.88766   | 3.89224   | 4.67659   | 4.69032   | 5.15453   | 5.17740   | 5.38778   | 5.43351   | 5.47925   | 5.57300   |
|           |           |           |           |           |           |           |           |           |           |
| 4.069E-06 | 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.070E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 6.465E-07 | 4.919E-07 |
| 93.387    | 93.922    | 93.999    | 94.572    | 95.910    | 96.445    | 96.598    | 96.713    | 96.827    | 97.439    |
| 5.58673   | 5.61874   | 5.62331   | 5.65762   | 5.73765   | 5.76967   | 5.77881   | 5.78567   | 5.79253   | 5.82912   |
|           |           |           |           |           |           |           |           |           |           |
| 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |           |           |           |           |           |           |
| 99.121    | 99.847    | 99.962    | 100.000   |           |           |           |           |           |           |
| 5.92974   | 5.97319   | 5.98005   | 5.98234   |           |           |           |           |           |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.197  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.489  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 2.207  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.806  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.105  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.327  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.673  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.151

| K | I | XQSAVE(K,I) | XQINT(K,I)   | XQSLOP(K,I) |
|---|---|-------------|--------------|-------------|
| 4 | 1 | -7.71082    | -11.83691    | -1.05722    |
| 4 | 2 | -8.78838    | -13.29054    | -1.56133    |
| 4 | 3 | -9.25677    | -14.88764    | -2.17952    |
| 4 | 4 | -10.50075   | -12.94221    | -1.21298    |
| 4 | 5 | -10.62522   | -13.05795    | -1.27357    |
| 4 | 6 | -10.68199   | -13.87328    | -1.71061    |
| 4 | 7 | -10.73463   | -16.12957    | -2.94031    |
| 4 | 8 | -11.19742   | -17.72502    | -3.89145    |
| 4 | 9 | -11.38039   | NUMXQ(K) = 9 |             |
|   |   | 2.223E-04   | 0.060        | 1.000       |
|   |   | 1.572E-04   | 0.179        | 3.000       |
|   |   | 1.236E-04   | 0.299        | 5.000       |
|   |   | 8.197E-05   | 0.598        | 10.000      |
|   |   | 5.957E-05   | 0.897        | 15.000      |
|   |   | 4.703E-05   | 1.196        | 20.000      |
|   |   | 3.891E-05   | 1.496        | 25.000      |
|   |   | 3.317E-05   | 1.795        | 30.000      |
|   |   | 2.889E-05   | 2.094        | 35.000      |
|   |   | 2.641E-05   | 2.393        | 40.000      |
|   |   | 2.484E-05   | 2.692        | 45.000      |
|   |   | 2.345E-05   | 2.991        | 50.000      |
|   |   | 2.198E-05   | 3.290        | 55.000      |
|   |   | 1.971E-05   | 3.589        | 60.000      |
|   |   | 1.769E-05   | 3.889        | 65.000      |
|   |   | 1.599E-05   | 4.188        | 70.000      |
|   |   | 1.453E-05   | 4.487        | 75.000      |
|   |   | 1.313E-05   | 4.786        | 80.000      |
|   |   | 1.172E-05   | 5.085        | 85.000      |
|   |   | 9.396E-05   | 0.5          | 8.36        |

ANNUAL AVERAGE = 1.02E-06

K= 4 FIVEXQ(K) = 9.396E-05 FIVEPR(K) = 8.358



RUN DATE: 04/05/09

METEOROLOGICAL INSTRUMENTATION

WIND SENSORS HEIGHT: 10.4 meters

DELTA-T HEIGHTS: 61.9-10.4 meters

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE W SECTOR.

STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT SIGMA-Y SIGMA-Z MEANDER-SY \*\* CHI/O VALUES (SEC/CUBIC METER)

| CLASS | METER/SEC<br>AT 10.0 METERS | PERCENT | METERS | METERS | METERS | METERS | METERS | METERS | MEANDER | BLDG WAKE         | USED |
|-------|-----------------------------|---------|--------|--------|--------|--------|--------|--------|---------|-------------------|------|
|       |                             |         |        |        |        |        |        |        |         | CA=1459.SQ.METERS |      |

|   |     |       |       |    |    |       |        |       |           |           |           |
|---|-----|-------|-------|----|----|-------|--------|-------|-----------|-----------|-----------|
| A | 2.0 | 0.91  | 1810. | 0. | 0. | 320.1 | 1000.0 | 320.1 | 4.927E-07 | 4.919E-07 | 4.919E-07 |
| A | 3.0 | 1.96  | 1810. | 0. | 0. | 320.1 | 1000.0 | 320.1 | 3.294E-07 | 3.289E-07 | 3.289E-07 |
| A | 4.0 | 0.87  | 1810. | 0. | 0. | 320.1 | 1000.0 | 320.1 | 2.480E-07 | 2.476E-07 | 2.476E-07 |
| A | 5.0 | 0.35  | 1810. | 0. | 0. | 320.1 | 1000.0 | 320.1 | 1.988E-07 | 1.985E-07 | 1.985E-07 |
| B | 1.5 | 0.26  | 1810. | 0. | 0. | 240.7 | 209.6  | 240.7 | 4.107E-06 | 4.069E-06 | 4.069E-06 |
| B | 2.0 | 0.87  | 1810. | 0. | 0. | 240.7 | 209.6  | 240.7 | 3.125E-06 | 3.096E-06 | 3.096E-06 |
| B | 3.0 | 1.26  | 1810. | 0. | 0. | 240.7 | 209.6  | 240.7 | 2.089E-06 | 2.070E-06 | 2.070E-06 |
| B | 4.0 | 0.65  | 1810. | 0. | 0. | 240.7 | 209.6  | 240.7 | 1.573E-06 | 1.558E-06 | 1.558E-06 |
| B | 5.0 | 0.17  | 1810. | 0. | 0. | 240.7 | 209.6  | 240.7 | 1.261E-06 | 1.250E-06 | 1.250E-06 |
| C | 1.0 | 0.04  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 1.596E-05 | 1.558E-05 | 1.558E-05 |
| C | 1.5 | 0.43  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 1.081E-05 | 1.055E-05 | 1.055E-05 |
| C | 2.0 | 1.04  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 8.223E-06 | 8.029E-06 | 8.029E-06 |
| C | 3.0 | 2.13  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 5.498E-06 | 5.368E-06 | 5.368E-06 |
| C | 4.0 | 0.70  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 4.139E-06 | 4.041E-06 | 4.041E-06 |
| C | 5.0 | 0.17  | 1810. | 0. | 0. | 182.8 | 104.9  | 182.8 | 3.318E-06 | 3.240E-06 | 3.240E-06 |
| D | 1.0 | 1.00  | 1810. | 0. | 0. | 128.7 | 47.4   | 190.3 | 3.389E-05 | 4.657E-05 | 3.389E-05 |
| D | 1.5 | 5.57  | 1810. | 0. | 0. | 128.7 | 47.4   | 190.3 | 2.295E-05 | 3.154E-05 | 2.295E-05 |
| D | 2.0 | 7.13  | 1810. | 0. | 0. | 128.7 | 47.4   | 189.6 | 1.753E-05 | 2.400E-05 | 1.753E-05 |
| D | 3.0 | 8.57  | 1810. | 0. | 0. | 128.7 | 47.4   | 162.1 | 1.371E-05 | 1.605E-05 | 1.371E-05 |
| D | 4.0 | 4.61  | 1810. | 0. | 0. | 128.7 | 47.4   | 146.5 | 1.142E-05 | 1.208E-05 | 1.142E-05 |
| D | 5.0 | 1.13  | 1810. | 0. | 0. | 128.7 | 47.4   | 136.2 | 9.848E-06 | 9.685E-06 | 9.685E-06 |
| D | 6.0 | 0.13  | 1810. | 0. | 0. | 128.7 | 47.4   | 128.8 | 8.699E-06 | 8.088E-06 | 8.088E-06 |
| D | 8.0 | 0.04  | 1810. | 0. | 0. | 128.7 | 47.4   | 128.7 | 6.538E-06 | 6.076E-06 | 6.076E-06 |
| E | 0.4 | 0.03  | 1810. | 0. | 0. | 91.5  | 32.3   | 179.1 | 1.568E-04 | 2.653E-04 | 1.568E-04 |
| E | 1.0 | 6.09  | 1810. | 0. | 0. | 91.5  | 32.3   | 179.1 | 5.339E-05 | 9.030E-05 | 5.339E-05 |
| E | 1.5 | 12.39 | 1810. | 0. | 0. | 91.5  | 32.3   | 179.1 | 3.616E-05 | 6.115E-05 | 3.616E-05 |
| E | 2.0 | 8.74  | 1810. | 0. | 0. | 91.5  | 32.3   | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0 | 7.61  | 1810. | 0. | 0. | 91.5  | 32.3   | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0 | 2.43  | 1810. | 0. | 0. | 91.5  | 32.3   | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0 | 0.57  | 1810. | 0. | 0. | 91.5  | 32.3   | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9 | 0.09  | 1810. | 0. | 0. | 91.5  | 32.3   | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| F | 0.4 | 0.14  | 1810. | 0. | 0. | 63.2  | 21.0   | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |     |      |       | MINOR REV. NO. 1B |    | APPENDIX BB-7 |      |       |           | PAGE NO. 102 of 160 |           |  |
|--|-----|------|-------|-------------------|----|---------------|------|-------|-----------|---------------------|-----------|--|
| F  | 1.0 | 6.22 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 9.546E-05 | 1.723E-04           | 9.546E-05 |  |
| F  | 1.5 | 6.26 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 6.465E-05 | 1.167E-04           | 6.465E-05 |  |
| F  | 2.0 | 1.22 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 4.920E-05 | 8.879E-05           | 4.920E-05 |  |
| F  | 3.0 | 0.26 | 1810. | 0.                | 0. | 63.2          | 21.0 | 105.7 | 4.786E-05 | 5.937E-05           | 4.786E-05 |  |
| G  | 0.4 | 0.10 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 4.480E-04 | 8.550E-04           | 4.480E-04 |  |
| G  | 1.0 | 3.96 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 1.525E-04 | 2.911E-04           | 1.525E-04 |  |
| G  | 1.5 | 2.83 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 1.033E-04 | 1.971E-04           | 1.033E-04 |  |
| G  | 2.0 | 1.09 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 7.859E-05 | 1.500E-04           | 7.859E-05 |  |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

W SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 | 4.920E-05 |
| 0.102     | 0.237     | 0.262     | 4.219     | 7.045     | 13.262    | 14.349    | 20.610    | 26.697    | 27.914    |
| 0.00534   | 0.01245   | 0.01379   | 0.22188   | 0.37052   | 0.69753   | 0.75470   | 1.08399   | 1.40414   | 1.46817   |
| 4.786E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 | 1.753E-05 | 1.568E-05 |
| 28.175    | 40.566    | 41.566    | 50.305    | 57.914    | 63.479    | 65.913    | 66.479    | 73.609    | 73.696    |
| 1.48189   | 2.13361   | 2.18621   | 2.64585   | 3.04603   | 3.33873   | 3.46679   | 3.49652   | 3.87155   | 3.87612   |
| 1.558E-05 | 1.371E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 8.088E-06 | 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.069E-06 |
| 73.739    | 82.305    | 86.913    | 87.348    | 88.478    | 88.609    | 89.652    | 89.696    | 91.826    | 92.087    |
| 3.87841   | 4.32890   | 4.57130   | 4.59417   | 4.65362   | 4.66048   | 4.71536   | 4.71765   | 4.82970   | 4.84342   |
| 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.070E-06 | 1.558E-06 | 1.250E-06 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 |
| 92.783    | 92.957    | 93.826    | 95.087    | 95.739    | 95.913    | 96.826    | 98.783    | 99.652    | 100.000   |
| 4.88001   | 4.88916   | 4.93489   | 5.00121   | 5.03551   | 5.04466   | 5.09268   | 5.19558   | 5.24132   | 5.25961   |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

|                  |                                    |            |       |
|------------------|------------------------------------|------------|-------|
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 2)= | 0.222 |
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 3)= | 0.697 |
| HANDCHECK GRAPH: | SLOPE LT -1.0 FOR LOW PERCENTAGES. | XSAVE( 4)= | 1.403 |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.131  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.336  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.464  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.868  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.325  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 4.568

| K | I  | XQSAVE (K, I) | XQINT (K, I)   | XQSLOP (K, I) |
|---|----|---------------|----------------|---------------|
| 5 | 1  | -7.71082      | -11.76849      | -1.04727      |
| 5 | 2  | -8.78838      | -12.23565      | -1.21144      |
| 5 | 3  | -9.25677      | -14.70226      | -2.21455      |
| 5 | 4  | -9.83784      | -14.89658      | -2.30301      |
| 5 | 5  | -10.22758     | -14.98256      | -2.34543      |
| 5 | 6  | -10.68199     | -16.37066      | -3.10246      |
| 5 | 7  | -10.73463     | -18.53890      | -4.29601      |
| 5 | 8  | -10.95135     | -19.29725      | -4.72538      |
| 5 | 9  | -11.19742     | -23.34609      | -7.08744      |
| 5 | 10 | -11.38039     | NUMXQ (K) = 10 |               |
|   |    | 2.395E-04     | 0.053          | 1.000         |
|   |    | 1.706E-04     | 0.158          | 3.000         |
|   |    | 1.427E-04     | 0.263          | 5.000         |
|   |    | 1.077E-04     | 0.526          | 10.000        |
|   |    | 8.650E-05     | 0.789          | 15.000        |
|   |    | 6.830E-05     | 1.052          | 20.000        |
|   |    | 5.651E-05     | 1.315          | 25.000        |
|   |    | 4.801E-05     | 1.578          | 30.000        |
|   |    | 4.160E-05     | 1.841          | 35.000        |
|   |    | 3.665E-05     | 2.104          | 40.000        |
|   |    | 3.264E-05     | 2.367          | 45.000        |
|   |    | 2.937E-05     | 2.630          | 50.000        |
|   |    | 2.665E-05     | 2.893          | 55.000        |
|   |    | 2.435E-05     | 3.156          | 60.000        |
|   |    | 2.221E-05     | 3.419          | 65.000        |
|   |    | 1.936E-05     | 3.682          | 70.000        |
|   |    | 1.683E-05     | 3.945          | 75.000        |
|   |    | 1.460E-05     | 4.208          | 80.000        |
|   |    | 1.231E-05     | 4.471          | 85.000        |
|   |    | 1.100E-04     | 0.5            | 9.51          |

ANNUAL AVERAGE = 1.09E-06

K= 5 FIVEXQ (K) = 1.100E-04 FIVEPR (K) = 9.506

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE WNW SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT<br>METERS | EFF<br>METERS | PLUME<br>METERS | HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER | BLDG WAKE | USED |
|-----------------|--|----------------------|--------------------|-------------------|--------------|---------------|-----------------|--------------|-------------------|-------------------|----------------------|-----------------------------------|---------|-----------|------|
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      | CA=1459.SQ.METERS                 |         |           |      |
| A               | 1.5                                      | 0.05                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 6.474E-07         | 6.465E-07            | 6.465E-07                         |         |           |      |
| A               | 2.0                                      | 0.29                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 4.927E-07         | 4.919E-07            | 4.919E-07                         |         |           |      |
| A               | 3.0                                      | 1.37                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 3.294E-07         | 3.289E-07            | 3.289E-07                         |         |           |      |
| A               | 4.0                                      | 0.69                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 2.480E-07         | 2.476E-07            | 2.476E-07                         |         |           |      |
| A               | 5.0                                      | 0.34                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 1.988E-07         | 1.985E-07            | 1.985E-07                         |         |           |      |
| A               | 6.0                                      | 0.15                 | 1810.              | 0.                | 0.           | 0.            | 320.1           | 1000.0       | 320.1             | 1.660E-07         | 1.658E-07            | 1.658E-07                         |         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |         |           |      |
| B               | 1.5                                      | 0.05                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 4.107E-06         | 4.069E-06            | 4.069E-06                         |         |           |      |
| B               | 2.0                                      | 0.59                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 3.125E-06         | 3.096E-06            | 3.096E-06                         |         |           |      |
| B               | 3.0                                      | 1.33                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 2.089E-06         | 2.070E-06            | 2.070E-06                         |         |           |      |
| B               | 4.0                                      | 0.49                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 1.573E-06         | 1.558E-06            | 1.558E-06                         |         |           |      |
| B               | 5.0                                      | 0.05                 | 1810.              | 0.                | 0.           | 0.            | 240.7           | 209.6        | 240.7             | 1.261E-06         | 1.250E-06            | 1.250E-06                         |         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |         |           |      |
| C               | 1.5                                      | 0.29                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 1.081E-05         | 1.055E-05            | 1.055E-05                         |         |           |      |
| C               | 2.0                                      | 0.88                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 8.223E-06         | 8.029E-06            | 8.029E-06                         |         |           |      |
| C               | 3.0                                      | 1.72                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 5.498E-06         | 5.368E-06            | 5.368E-06                         |         |           |      |
| C               | 4.0                                      | 0.49                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 4.139E-06         | 4.041E-06            | 4.041E-06                         |         |           |      |
| C               | 6.0                                      | 0.20                 | 1810.              | 0.                | 0.           | 0.            | 182.8           | 104.9        | 182.8             | 2.771E-06         | 2.706E-06            | 2.706E-06                         |         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |         |           |      |
| D               | 1.0                                      | 0.34                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 190.3             | 3.389E-05         | 4.657E-05            | 3.389E-05                         |         |           |      |
| D               | 1.5                                      | 2.11                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 190.3             | 2.295E-05         | 3.154E-05            | 2.295E-05                         |         |           |      |
| D               | 2.0                                      | 4.57                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 189.6             | 1.753E-05         | 2.400E-05            | 1.753E-05                         |         |           |      |
| D               | 3.0                                      | 8.15                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 162.1             | 1.371E-05         | 1.605E-05            | 1.371E-05                         |         |           |      |
| D               | 4.0                                      | 4.37                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 146.5             | 1.142E-05         | 1.208E-05            | 1.142E-05                         |         |           |      |
| D               | 5.0                                      | 2.80                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 136.2             | 9.848E-06         | 9.685E-06            | 9.685E-06                         |         |           |      |
| D               | 6.0                                      | 1.57                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 128.8             | 8.699E-06         | 8.088E-06            | 8.088E-06                         |         |           |      |
| D               | 8.0                                      | 0.34                 | 1810.              | 0.                | 0.           | 0.            | 128.7           | 47.4         | 128.7             | 6.538E-06         | 6.076E-06            | 6.076E-06                         |         |           |      |
|                 |  |                      |                    |                   |              |               |                 |              |                   |                   |                      |                                   |         |           |      |
| E               | 0.4                                      | 0.01                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 1.568E-04         | 2.653E-04            | 1.568E-04                         |         |           |      |
| E               | 1.0                                      | 1.67                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 5.339E-05         | 9.030E-05            | 5.339E-05                         |         |           |      |
| E               | 1.5                                      | 7.81                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 3.616E-05         | 6.115E-05            | 3.616E-05                         |         |           |      |
| E               | 2.0                                      | 9.43                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 179.1             | 2.752E-05         | 4.654E-05            | 2.752E-05                         |         |           |      |
| E               | 3.0                                      | 13.21                | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 135.6             | 2.430E-05         | 3.112E-05            | 2.430E-05                         |         |           |      |
| E               | 4.0                                      | 4.32                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 113.9             | 2.178E-05         | 2.342E-05            | 2.178E-05                         |         |           |      |
| E               | 5.0                                      | 2.46                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 100.8             | 1.973E-05         | 1.878E-05            | 1.878E-05                         |         |           |      |
| E               | 5.9                                      | 1.23                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 92.0              | 1.805E-05         | 1.568E-05            | 1.568E-05                         |         |           |      |
| E               | 7.9                                      | 0.15                 | 1810.              | 0.                | 0.           | 0.            | 91.5            | 32.3         | 91.5              | 1.363E-05         | 1.178E-05            | 1.178E-05                         |         |           |      |

|   |     |      |       |    |    |      |      |       |           |           |           |
|---|-----|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| F | 0.4 | 0.06 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0 | 2.95 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5 | 7.22 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0 | 7.37 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0 | 2.41 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0 | 0.05 | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| G | 0.4 | 0.06 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0 | 2.26 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5 | 2.36 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0 | 1.47 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0 | 0.29 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

WNW SECTOR      BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.058     | 0.122     | 0.129     | 2.388     | 4.744     | 7.691     | 7.985     | 9.458     | 16.676    | 18.345    |
| 0.00270   | 0.00568   | 0.00601   | 0.11120   | 0.22096   | 0.35817   | 0.37189   | 0.44049   | 0.77665   | 0.85440   |
|           |           |           |           |           |           |           |           |           |           |
| 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 |
| 25.710    | 28.116    | 28.166    | 35.973    | 36.316    | 45.744    | 58.952    | 61.063    | 65.384    | 67.839    |
| 1.19741   | 1.30946   | 1.31175   | 1.67534   | 1.69135   | 2.13041   | 2.74555   | 2.84388   | 3.04511   | 3.15945   |
|           |           |           |           |           |           |           |           |           |           |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 8.088E-06 | 8.029E-06 | 6.076E-06 |
| 72.405    | 73.633    | 81.784    | 81.931    | 86.301    | 86.595    | 89.394    | 90.965    | 91.849    | 92.193    |
| 3.37212   | 3.42929   | 3.80889   | 3.81575   | 4.01927   | 4.03299   | 4.16334   | 4.23651   | 4.27767   | 4.29368   |
|           |           |           |           |           |           |           |           |           |           |
| 5.368E-06 | 4.069E-06 | 4.041E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 1.558E-06 | 1.250E-06 | 6.465E-07 | 4.919E-07 |
| 93.911    | 93.961    | 94.452    | 95.041    | 95.237    | 96.563    | 97.054    | 97.103    | 97.152    | 97.447    |
| 4.37372   | 4.37600   | 4.39887   | 4.42631   | 4.43546   | 4.49720   | 4.52007   | 4.52236   | 4.52464   | 4.53836   |
|           |           |           |           |           |           |           |           |           |           |
| 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |           |           |           |           |           |           |
| 98.822    | 99.509    | 99.853    | 100.000   |           |           |           |           |           |           |
| 4.60239   | 4.63441   | 4.65042   | 4.65728   |           |           |           |           |           |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.111  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.358  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.776  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.308  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.743  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.042  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 3.806  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.016

| K | I | XQSAVE(K, I) | XQINT(K, I)  | XQSLOP(K, I) |
|---|---|--------------|--------------|--------------|
| 6 | 1 | -7.71082     | -12.15629    | -1.10103     |
| 6 | 2 | -8.78838     | -12.66776    | -1.26824     |
| 6 | 3 | -9.25677     | -13.14771    | -1.44669     |
| 6 | 4 | -9.64651     | -13.35526    | -1.53245     |
| 6 | 5 | -9.94734     | -14.90897    | -2.23111     |
| 6 | 6 | -10.62522    | -15.25415    | -2.41089     |
| 6 | 7 | -10.73463    | -19.33111    | -4.58571     |
| 6 | 8 | -11.19742    | -24.25202    | -7.36008     |
| 6 | 9 | -11.38039    | NUMXQ(K) = 9 |              |
|   |   | 2.012E-04    | 0.047        | 1.000        |
|   |   | 1.397E-04    | 0.140        | 3.000        |
|   |   | 1.141E-04    | 0.233        | 5.000        |
|   |   | 8.395E-05    | 0.466        | 10.000       |
|   |   | 6.833E-05    | 0.699        | 15.000       |
|   |   | 5.836E-05    | 0.931        | 20.000       |
|   |   | 5.130E-05    | 1.164        | 25.000       |
|   |   | 4.523E-05    | 1.397        | 30.000       |
|   |   | 3.946E-05    | 1.630        | 35.000       |
|   |   | 3.498E-05    | 1.863        | 40.000       |
|   |   | 3.139E-05    | 2.096        | 45.000       |
|   |   | 2.844E-05    | 2.329        | 50.000       |
|   |   | 2.598E-05    | 2.562        | 55.000       |
|   |   | 2.385E-05    | 2.794        | 60.000       |
|   |   | 2.191E-05    | 3.027        | 65.000       |
|   |   | 1.895E-05    | 3.260        | 70.000       |
|   |   | 1.643E-05    | 3.493        | 75.000       |
|   |   | 1.436E-05    | 3.726        | 80.000       |
|   |   | 1.203E-05    | 3.959        | 85.000       |
|   |   | 8.103E-05    | 0.5          | 10.74        |

ANNUAL AVERAGE = 7.79E-07

K= 6 FIVEXQ(K) = 8.103E-05 FIVEPR(K) = 10.736



USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NW SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y           | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|-------------------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS            | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              | CA=1459.SQ.METERS |         |            |                                   |           |           |
| A              | 1.5       | 0.14      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 6.474E-07                         | 6.465E-07 | 6.465E-07 |
| A              | 2.0       | 0.64      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A              | 3.0       | 1.47      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 0.87      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 0.28      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.09      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.32      | 1810.    | 0.         | 0.           | 320.1             | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| B              | 1.5       | 0.05      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 4.107E-06                         | 4.069E-06 | 4.069E-06 |
| B              | 2.0       | 0.46      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 1.47      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 0.55      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.32      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 8.0       | 0.23      | 1810.    | 0.         | 0.           | 240.7             | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| C              | 1.0       | 0.05      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 1.596E-05                         | 1.558E-05 | 1.558E-05 |
| C              | 1.5       | 0.23      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.60      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 1.79      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 0.73      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 0.41      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.23      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 0.23      | 1810.    | 0.         | 0.           | 182.8             | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| D              | 1.0       | 0.18      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 190.3      | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D              | 1.5       | 1.10      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 190.3      | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D              | 2.0       | 3.03      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 189.6      | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D              | 3.0       | 8.72      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 162.1      | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D              | 4.0       | 6.06      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 146.5      | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D              | 5.0       | 4.45      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 136.2      | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D              | 6.0       | 3.72      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 128.8      | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D              | 8.0       | 1.79      | 1810.    | 0.         | 0.           | 128.7             | 47.4    | 128.7      | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
|                |           |           |          |            |              |                   |         |            |                                   |           |           |
| E              | 0.4       | 0.00      | 1810.    | 0.         | 0.           | 91.5              | 32.3    | 179.1      | 1.568E-04                         | 2.653E-04 | 1.568E-04 |
| E              | 1.0       | 0.96      | 1810.    | 0.         | 0.           | 91.5              | 32.3    | 179.1      | 5.339E-05                         | 9.030E-05 | 5.339E-05 |
| E              | 1.5       | 2.75      | 1810.    | 0.         | 0.           | 91.5              | 32.3    | 179.1      | 3.616E-05                         | 6.115E-05 | 3.616E-05 |
| E              | 2.0       | 5.74      | 1810.    | 0.         | 0.           | 91.5              | 32.3    | 179.1      | 2.752E-05                         | 4.654E-05 | 2.752E-05 |

|  |  |  |  |  |  |                   |  |  |               |  |  |                     |
|--|--|--|--|--|--|-------------------|--|--|---------------|--|--|---------------------|
| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B |  |  | APPENDIX BB-7 |  |  | PAGE NO. 110 of 160 |
|--|--|--|--|--|--|-------------------|--|--|---------------|--|--|---------------------|

|   |     |       |       |    |    |      |      |       |           |           |           |
|---|-----|-------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 3.0 | 16.30 | 1810. | 0. | 0. | 91.5 | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0 | 11.66 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0 | 4.59  | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9 | 1.70  | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9 | 1.61  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8 | 0.09  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
|   |     |       |       |    |    |      |      |       |           |           |           |
| F | 0.4 | 0.03  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0 | 1.47  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5 | 3.12  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0 | 3.53  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0 | 3.26  | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0 | 0.23  | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0 | 0.05  | 1810. | 0. | 0. | 63.2 | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
|   |     |       |       |    |    |      |      |       |           |           |           |
| G | 0.4 | 0.03  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0 | 1.24  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5 | 0.69  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0 | 0.50  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0 | 0.23  | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

NW SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.032     | 0.064     | 0.068     | 1.307     | 1.996     | 3.465     | 3.694     | 4.199     | 7.321     | 8.285     |
| 0.00159   | 0.00318   | 0.00338   | 0.06512   | 0.09942   | 0.17260   | 0.18403   | 0.20918   | 0.36468   | 0.41271   |
|           |           |           |           |           |           |           |           |           |           |
| 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 |
| 11.819    | 15.078    | 15.308    | 18.062    | 18.108    | 18.292    | 24.029    | 40.325    | 41.427    | 53.086    |
| 0.58879   | 0.75115   | 0.76258   | 0.89979   | 0.90207   | 0.91122   | 1.19706   | 2.00886   | 2.06375   | 2.64458   |
|           |           |           |           |           |           |           |           |           |           |
| 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.558E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 |
| 57.677    | 60.707    | 62.405    | 62.451    | 71.173    | 72.779    | 78.838    | 79.068    | 83.521    | 83.612    |
| 2.87326   | 3.02419   | 3.10880   | 3.11108   | 3.54557   | 3.62560   | 3.92746   | 3.93889   | 4.16071   | 4.16528   |
|           |           |           |           |           |           |           |           |           |           |
| 8.088E-06 | 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.069E-06 | 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 |
| 87.331    | 87.927    | 89.718    | 91.508    | 91.554    | 92.288    | 92.701    | 93.160    | 93.390    | 94.859    |
| 4.35051   | 4.38023   | 4.46942   | 4.55860   | 4.56089   | 4.59748   | 4.61806   | 4.64092   | 4.65236   | 4.72553   |
|           |           |           |           |           |           |           |           |           |           |
| 2.033E-06 | 1.558E-06 | 1.250E-06 | 7.840E-07 | 6.465E-07 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |
| 95.088    | 95.639    | 95.960    | 96.190    | 96.328    | 96.970    | 98.439    | 99.311    | 99.587    | 99.679    |
| 4.73697   | 4.76441   | 4.78042   | 4.79185   | 4.79871   | 4.83073   | 4.90390   | 4.94735   | 4.96107   | 4.96564   |
|           |           |           |           |           |           |           |           |           |           |
| 1.246E-07 |           |           |           |           |           |           |           |           |           |
| 100.000   |           |           |           |           |           |           |           |           |           |
| 4.98165   |           |           |           |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.065  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.750  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 2.642  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 3.542  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.924  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 4.157

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 7 | 1 | -7.71082     | -12.45468   | -1.14012     |
| 7 | 2 | -8.78838     | -13.54533   | -1.47929     |
| 7 | 3 | -9.94734     | -13.80787   | -1.58722     |
| 7 | 4 | -10.73463    | -17.63891   | -3.56583     |
| 7 | 5 | -11.19742    | -18.24652   | -3.90219     |
| 7 | 6 | -11.38039    | -22.17016   | -6.13209     |
| 7 | 7 | -11.54497    | NUMXQ(K)= 7 |              |
|   |   | 1.663E-04    | 0.050       | 1.000        |
|   |   | 1.059E-04    | 0.149       | 3.000        |
|   |   | 8.350E-05    | 0.249       | 5.000        |
|   |   | 5.933E-05    | 0.498       | 10.000       |
|   |   | 4.799E-05    | 0.747       | 15.000       |
|   |   | 4.057E-05    | 0.996       | 20.000       |
|   |   | 3.545E-05    | 1.245       | 25.000       |
|   |   | 3.166E-05    | 1.494       | 30.000       |
|   |   | 2.871E-05    | 1.744       | 35.000       |
|   |   | 2.632E-05    | 1.993       | 40.000       |
|   |   | 2.435E-05    | 2.242       | 45.000       |
|   |   | 2.269E-05    | 2.491       | 50.000       |
|   |   | 2.062E-05    | 2.740       | 55.000       |
|   |   | 1.800E-05    | 2.989       | 60.000       |
|   |   | 1.586E-05    | 3.238       | 65.000       |
|   |   | 1.408E-05    | 3.487       | 70.000       |
|   |   | 1.249E-05    | 3.736       | 75.000       |
|   |   | 1.095E-05    | 3.985       | 80.000       |
|   |   | 5.921E-05    | 0.5         | 10.04        |

ANNUAL AVERAGE = 5.81E-07

K= 7 FIVEXQ(K)= 5.921E-05 FIVEPR(K)=10.037

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNW SECTOR.

| STABILITY WINDSPEED FREQUENCY DISTANCE TERRAIN HT EFF PLUME HT |           |         |        |        |        | SIGMA-Y SIGMA-Z MEANDER-SY ** CHI/Q VALUES (SEC/CUBIC METER) |        |        |           |           |           |      |
|--|-----------|---------|--------|--------|--------|--|--------|--------|-----------|-----------|-----------|------|
| CLASS  | METER/SEC | PERCENT | METERS | METERS | METERS | METERS   | METERS | METERS | METERS    | MEANDER   | BLDG WAKE | USED |
| AT 10.0 METERS   |           |         |        |        |        | CA=1459.SQ.METERS  |        |        |           |           |           |      |
| A  | 1.5       | 0.07    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 6.474E-07 | 6.465E-07 | 6.465E-07 |      |
| A  | 2.0       | 0.25    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 4.927E-07 | 4.919E-07 | 4.919E-07 |      |
| A  | 3.0       | 1.79    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 3.294E-07 | 3.289E-07 | 3.289E-07 |      |
| A  | 4.0       | 1.33    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 2.480E-07 | 2.476E-07 | 2.476E-07 |      |
| A  | 5.0       | 0.35    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 1.988E-07 | 1.985E-07 | 1.985E-07 |      |
| A  | 6.0       | 0.25    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 1.660E-07 | 1.658E-07 | 1.658E-07 |      |
| A  | 8.0       | 0.42    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 1.247E-07 | 1.246E-07 | 1.246E-07 |      |
| A  | 9.9       | 0.11    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 1.003E-07 | 1.001E-07 | 1.001E-07 |      |
| A  | 24.3      | 0.04    | 1810.  | 0.     | 0.     | 320.1  | 1000.0 | 320.1  | 4.085E-08 | 4.079E-08 | 4.079E-08 |      |
|  |           |         |        |        |        |  |        |        |           |           |           |      |
| B  | 1.5       | 0.11    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 4.107E-06 | 4.069E-06 | 4.069E-06 |      |
| B  | 2.0       | 0.39    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 3.125E-06 | 3.096E-06 | 3.096E-06 |      |
| B  | 3.0       | 1.02    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 2.089E-06 | 2.070E-06 | 2.070E-06 |      |
| B  | 4.0       | 0.67    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 1.573E-06 | 1.558E-06 | 1.558E-06 |      |
| B  | 5.0       | 0.53    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 1.261E-06 | 1.250E-06 | 1.250E-06 |      |
| B  | 6.0       | 0.28    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 1.053E-06 | 1.044E-06 | 1.044E-06 |      |
| B  | 8.0       | 0.39    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 7.912E-07 | 7.840E-07 | 7.840E-07 |      |
| B  | 9.9       | 0.04    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 6.361E-07 | 6.303E-07 | 6.303E-07 |      |
| B  | 24.3      | 0.04    | 1810.  | 0.     | 0.     | 240.7  | 209.6  | 240.7  | 2.591E-07 | 2.567E-07 | 2.567E-07 |      |
|  |           |         |        |        |        |  |        |        |           |           |           |      |
| C  | 1.5       | 0.07    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 1.081E-05 | 1.055E-05 | 1.055E-05 |      |
| C  | 2.0       | 0.49    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 8.223E-06 | 8.029E-06 | 8.029E-06 |      |
| C  | 3.0       | 1.44    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 5.498E-06 | 5.368E-06 | 5.368E-06 |      |
| C  | 4.0       | 1.23    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 4.139E-06 | 4.041E-06 | 4.041E-06 |      |
| C  | 5.0       | 0.46    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 3.318E-06 | 3.240E-06 | 3.240E-06 |      |
| C  | 6.0       | 0.67    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 2.771E-06 | 2.706E-06 | 2.706E-06 |      |
| C  | 8.0       | 0.49    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 2.082E-06 | 2.033E-06 | 2.033E-06 |      |
| C  | 9.9       | 0.04    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 1.674E-06 | 1.634E-06 | 1.634E-06 |      |
| C  | 24.3      | 0.04    | 1810.  | 0.     | 0.     | 182.8  | 104.9  | 182.8  | 6.818E-07 | 6.656E-07 | 6.656E-07 |      |
|  |           |         |        |        |        |  |        |        |           |           |           |      |
| D  | 1.0       | 0.14    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 190.3  | 3.389E-05 | 4.657E-05 | 3.389E-05 |      |
| D  | 1.5       | 0.67    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 190.3  | 2.295E-05 | 3.154E-05 | 2.295E-05 |      |
| D  | 2.0       | 1.89    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 189.6  | 1.753E-05 | 2.400E-05 | 1.753E-05 |      |
| D  | 3.0       | 7.12    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 162.1  | 1.371E-05 | 1.605E-05 | 1.371E-05 |      |
| D  | 4.0       | 7.61    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 146.5  | 1.142E-05 | 1.208E-05 | 1.142E-05 |      |
| D  | 5.0       | 5.16    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 136.2  | 9.848E-06 | 9.685E-06 | 9.685E-06 |      |
| D  | 6.0       | 4.67    | 1810.  | 0.     | 0.     | 128.7  | 47.4   | 128.8  | 8.699E-06 | 8.088E-06 | 8.088E-06 |      |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  | PAGE NO. 114 of 160 |  |
|--|--|--|--|--|--|-------------------|--|---------------|--|--|---------------------|--|
|--|--|--|--|--|--|-------------------|--|---------------|--|--|---------------------|--|

|   |      |       |       |    |    |       |      |       |           |           |           |
|---|------|-------|-------|----|----|-------|------|-------|-----------|-----------|-----------|
| D | 8.0  | 3.75  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 6.538E-06 | 6.076E-06 | 6.076E-06 |
| D | 9.9  | 0.63  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 5.257E-06 | 4.886E-06 | 4.886E-06 |
| D | 24.3 | 0.11  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 2.141E-06 | 1.990E-06 | 1.990E-06 |
| E | 0.4  | 0.00  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 1.568E-04 | 2.653E-04 | 1.568E-04 |
| E | 1.0  | 0.46  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 5.339E-05 | 9.030E-05 | 5.339E-05 |
| E | 1.5  | 1.33  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 3.616E-05 | 6.115E-05 | 3.616E-05 |
| E | 2.0  | 3.68  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 14.80 | 1810. | 0. | 0. | 91.5  | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 11.12 | 1810. | 0. | 0. | 91.5  | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 7.82  | 1810. | 0. | 0. | 91.5  | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 4.77  | 1810. | 0. | 0. | 91.5  | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 2.70  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.18  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.35  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
| F | 0.4  | 0.02  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 0.81  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 1.26  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 1.54  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 2.53  | 1810. | 0. | 0. | 63.2  | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 0.95  | 1810. | 0. | 0. | 63.2  | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0  | 0.04  | 1810. | 0. | 0. | 63.2  | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
| G | 0.4  | 0.02  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 0.63  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.14  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.04  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.11  | 1810. | 0. | 0. | 43.6  | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.04  | 1810. | 0. | 0. | 43.6  | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |

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4.079E-08
100.000
6.51959

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## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.043  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.493  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 2.625  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 3.135  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 4.705  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 5.045  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 5.393  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.638

| K | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|---|---|--------------|-------------|--------------|
| 8 | 1 | -7.71082     | -12.67720   | -1.16788     |
| 8 | 2 | -8.78838     | -13.93802   | -1.54652     |
| 8 | 3 | -9.94734     | -13.11472   | -1.22747     |
| 8 | 4 | -10.73463    | -14.43346   | -1.90757     |
| 8 | 5 | -10.88275    | -15.83067   | -2.65820     |
| 8 | 6 | -11.38039    | -19.55400   | -4.88219     |
| 8 | 7 | -11.54497    | -20.98979   | -5.75743     |
| 8 | 8 | -11.73251    | -32.14287   | -12.69392    |
| 8 | 9 | -12.01110    | NUMXQ(K)= 9 |              |
|   |   | 1.278E-04    | 0.065       | 1.000        |
|   |   | 7.671E-05    | 0.196       | 3.000        |
|   |   | 5.946E-05    | 0.326       | 5.000        |
|   |   | 4.247E-05    | 0.652       | 10.000       |
|   |   | 3.541E-05    | 0.978       | 15.000       |
|   |   | 3.095E-05    | 1.304       | 20.000       |
|   |   | 2.778E-05    | 1.630       | 25.000       |
|   |   | 2.537E-05    | 1.956       | 30.000       |
|   |   | 2.345E-05    | 2.282       | 35.000       |
|   |   | 2.186E-05    | 2.608       | 40.000       |
|   |   | 1.987E-05    | 2.934       | 45.000       |
|   |   | 1.795E-05    | 3.260       | 50.000       |
|   |   | 1.601E-05    | 3.586       | 55.000       |
|   |   | 1.440E-05    | 3.912       | 60.000       |
|   |   | 1.304E-05    | 4.238       | 65.000       |
|   |   | 1.188E-05    | 4.564       | 70.000       |
|   |   | 1.045E-05    | 4.890       | 75.000       |
|   |   | 8.842E-06    | 5.216       | 80.000       |
|   |   | 6.800E-06    | 5.542       | 85.000       |
|   |   | 4.761E-05    | 0.5         | 7.67         |

ANNUAL AVERAGE = 5.72E-07



K= 8      FIVEXQ (K) = 4.761E-05      FIVEPR (K) = 7.669

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE N SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 2.0       | 0.24      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A              | 3.0       | 1.61      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 1.12      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 1.08      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.73      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.63      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| A              | 9.9       | 0.21      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.003E-07                         | 1.001E-07 | 1.001E-07 |
| A              | 24.3      | 0.10      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.085E-08                         | 4.079E-08 | 4.079E-08 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 1.5       | 0.14      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 4.107E-06                         | 4.069E-06 | 4.069E-06 |
| B              | 2.0       | 0.17      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 0.73      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 0.66      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.70      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 6.0       | 0.77      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B              | 8.0       | 0.31      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| B              | 9.9       | 0.21      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 6.361E-07                         | 6.303E-07 | 6.303E-07 |
| B              | 24.3      | 0.03      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.591E-07                         | 2.567E-07 | 2.567E-07 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.14      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.45      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 0.70      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 0.94      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 0.94      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.59      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 0.63      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C              | 9.9       | 0.07      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.10      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D              | 1.5       | 0.42      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D              | 2.0       | 1.22      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 189.6      | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D              | 3.0       | 4.02      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 162.1      | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D              | 4.0       | 4.48      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 146.5      | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D              | 5.0       | 5.42      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 136.2      | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D              | 6.0       | 5.00      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.8      | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D              | 8.0       | 7.17      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D              | 9.9       | 2.10      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 5.257E-06                         | 4.886E-06 | 4.886E-06 |

|  |  |  |  |                   |  |               |  |  |  |                     |  |
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|
| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  |  | PAGE NO. 119 of 160 |  |
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|

|   |      |       |       |    |    |       |      |       |           |           |           |
|---|------|-------|-------|----|----|-------|------|-------|-----------|-----------|-----------|
| D | 24.3 | 0.45  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 2.141E-06 | 1.990E-06 | 1.990E-06 |
| E | 0.4  | 0.00  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 1.568E-04 | 2.653E-04 | 1.568E-04 |
| E | 1.0  | 0.35  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 5.339E-05 | 9.030E-05 | 5.339E-05 |
| E | 1.5  | 0.66  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 3.616E-05 | 6.115E-05 | 3.616E-05 |
| E | 2.0  | 1.92  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 8.15  | 1810. | 0. | 0. | 91.5  | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 11.15 | 1810. | 0. | 0. | 91.5  | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 10.84 | 1810. | 0. | 0. | 91.5  | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 7.55  | 1810. | 0. | 0. | 91.5  | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 6.47  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 2.83  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.42  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
| F | 0.4  | 0.01  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 0.59  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 0.56  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 0.73  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 1.50  | 1810. | 0. | 0. | 63.2  | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 0.59  | 1810. | 0. | 0. | 63.2  | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0  | 0.24  | 1810. | 0. | 0. | 63.2  | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
| G | 0.4  | 0.01  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 0.45  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.31  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.14  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.07  | 1810. | 0. | 0. | 43.6  | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.07  | 1810. | 0. | 0. | 43.6  | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

N SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.012     | 0.025     | 0.026     | 0.481     | 0.795     | 1.390     | 1.460     | 1.600     | 1.670     | 2.229     |
| 0.00076   | 0.00161   | 0.00170   | 0.03143   | 0.05201   | 0.09089   | 0.09546   | 0.10461   | 0.10918   | 0.14577   |
| 5.339E-05 | 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 |
| 2.579     | 3.313     | 4.817     | 5.411     | 6.076     | 6.320     | 6.425     | 8.348     | 16.496    | 16.916    |
| 0.16864   | 0.21666   | 0.31499   | 0.35386   | 0.39731   | 0.41332   | 0.42018   | 0.54595   | 1.07877   | 1.10621   |
| 2.178E-05 | 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 |
| 28.071    | 38.911    | 40.135    | 47.688    | 51.709    | 58.178    | 62.654    | 62.794    | 68.214    | 71.046    |
| 1.83568   | 2.54458   | 2.62462   | 3.11856   | 3.38153   | 3.80458   | 4.09729   | 4.10644   | 4.46089   | 4.64611   |
| 8.088E-06 | 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 |
| 76.047    | 76.501    | 83.670    | 84.369    | 86.467    | 86.607    | 87.551    | 87.971    | 88.915    | 89.090    |
| 4.97312   | 5.00285   | 5.47163   | 5.51737   | 5.65457   | 5.66372   | 5.72546   | 5.75290   | 5.81465   | 5.82608   |
| 2.706E-06 | 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.303E-07 |
| 89.684    | 90.419    | 91.048    | 91.503    | 91.573    | 92.237    | 92.936    | 93.706    | 94.020    | 94.230    |
| 5.86496   | 5.91298   | 5.95414   | 5.98387   | 5.98844   | 6.03189   | 6.07762   | 6.12793   | 6.14851   | 6.16223   |
| 4.919E-07 | 3.289E-07 | 2.567E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 | 1.001E-07 | 4.079E-08 |           |
| 94.475    | 96.084    | 96.119    | 97.238    | 98.322    | 99.056    | 99.685    | 99.895    | 100.000   |           |
| 6.17824   | 6.28343   | 6.28572   | 6.35890   | 6.42979   | 6.47781   | 6.51897   | 6.53269   | 6.53955   |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.031  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.091  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.353  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.542  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 3.116  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.094  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.643  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 4.999

K I XQSAVE(K,I) XQINT(K,I) XQSLOP(K,I)

9 1 -7.71082 -12.85672 -1.18987  
 9 2 -8.78838 -14.12028 -1.55943  
 9 3 -9.25677 -14.82390 -1.78503  
 9 4 -10.01579 -13.16830 -1.17038  
 9 5 -10.88275 -14.84538 -2.02918  
 9 6 -11.06285 -15.82967 -2.55722  
 9 7 -11.38039 -16.85190 -3.14474  
 9 8 -11.56701 -19.37663 -4.64707  
 9 9 -11.73251 NUMXQ(K)= 9

|           |       |        |
|-----------|-------|--------|
| 1.108E-04 | 0.065 | 1.000  |
| 6.284E-05 | 0.196 | 3.000  |
| 4.683E-05 | 0.327 | 5.000  |
| 3.489E-05 | 0.654 | 10.000 |
| 2.934E-05 | 0.981 | 15.000 |
| 2.580E-05 | 1.308 | 20.000 |
| 2.328E-05 | 1.635 | 25.000 |
| 2.134E-05 | 1.962 | 30.000 |
| 1.980E-05 | 2.289 | 35.000 |
| 1.833E-05 | 2.616 | 40.000 |
| 1.652E-05 | 2.943 | 45.000 |
| 1.486E-05 | 3.270 | 50.000 |
| 1.331E-05 | 3.597 | 55.000 |
| 1.202E-05 | 3.924 | 60.000 |
| 1.082E-05 | 4.251 | 65.000 |
| 9.687E-06 | 4.578 | 70.000 |
| 8.395E-06 | 4.905 | 75.000 |

|           |     |      |
|-----------|-----|------|
| 3.895E-05 | 0.5 | 7.65 |
|-----------|-----|------|

ANNUAL AVERAGE = 4.59E-07

K= 9 FIVEXQ(K)= 3.895E-05 FIVEPR(K)= 7.646

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NNE SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
|                |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| AT 10.0 METERS |           |           |          |            |              |         |         |            |                                   |           |           |
| A              | 1.5       | 0.09      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 6.474E-07                         | 6.465E-07 | 6.465E-07 |
| A              | 2.0       | 0.24      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A              | 3.0       | 0.71      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 0.92      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 1.83      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.80      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.95      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| A              | 9.9       | 0.06      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.003E-07                         | 1.001E-07 | 1.001E-07 |
| A              | 24.3      | 0.21      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.085E-08                         | 4.079E-08 | 4.079E-08 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 2.0       | 0.12      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 0.62      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 0.80      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.83      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 6.0       | 0.59      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B              | 8.0       | 0.50      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| B              | 9.9       | 0.06      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 6.361E-07                         | 6.303E-07 | 6.303E-07 |
| B              | 24.3      | 0.06      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.591E-07                         | 2.567E-07 | 2.567E-07 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.06      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.32      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 0.68      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 1.03      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 0.92      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.86      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 1.03      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C              | 9.9       | 0.30      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
| C              | 24.3      | 0.18      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 6.818E-07                         | 6.656E-07 | 6.656E-07 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.03      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D              | 1.5       | 0.35      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D              | 2.0       | 1.18      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 189.6      | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D              | 3.0       | 2.87      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 162.1      | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D              | 4.0       | 4.43      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 146.5      | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D              | 5.0       | 5.29      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 136.2      | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D              | 6.0       | 5.29      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.8      | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D              | 8.0       | 7.47      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 6.538E-06                         | 6.076E-06 | 6.076E-06 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  |  | PAGE NO. 123 of 160 |  |
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|

|   |      |       |       |    |    |       |      |       |           |           |           |
|---|------|-------|-------|----|----|-------|------|-------|-----------|-----------|-----------|
| D | 9.9  | 3.28  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 5.257E-06 | 4.886E-06 | 4.886E-06 |
| D | 24.3 | 0.47  | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 2.141E-06 | 1.990E-06 | 1.990E-06 |
| E | 0.4  | 0.00  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 1.568E-04 | 2.653E-04 | 1.568E-04 |
| E | 1.0  | 0.38  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 5.339E-05 | 9.030E-05 | 5.339E-05 |
| E | 1.5  | 0.50  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 3.616E-05 | 6.115E-05 | 3.616E-05 |
| E | 2.0  | 0.95  | 1810. | 0. | 0. | 91.5  | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 5.52  | 1810. | 0. | 0. | 91.5  | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 10.34 | 1810. | 0. | 0. | 91.5  | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 11.46 | 1810. | 0. | 0. | 91.5  | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 7.80  | 1810. | 0. | 0. | 91.5  | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 6.97  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 1.30  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.30  | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
| F | 0.4  | 0.01  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 0.56  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 0.74  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 0.80  | 1810. | 0. | 0. | 63.2  | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 1.83  | 1810. | 0. | 0. | 63.2  | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 2.16  | 1810. | 0. | 0. | 63.2  | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0  | 1.39  | 1810. | 0. | 0. | 63.2  | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
| F | 5.9  | 0.30  | 1810. | 0. | 0. | 63.2  | 21.0 | 63.6  | 4.009E-05 | 2.992E-05 | 2.992E-05 |
| F | 7.9  | 0.03  | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 3.033E-05 | 2.248E-05 | 2.248E-05 |
| G | 0.4  | 0.01  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 0.35  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.27  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.24  | 1810. | 0. | 0. | 43.6  | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.18  | 1810. | 0. | 0. | 43.6  | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.12  | 1810. | 0. | 0. | 43.6  | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |
| G | 5.0  | 0.09  | 1810. | 0. | 0. | 43.6  | 13.7 | 51.3  | 9.150E-05 | 6.053E-05 | 6.053E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

NNE SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.009     | 0.021     | 0.023     | 0.377     | 0.643     | 1.205     | 1.382     | 1.618     | 1.736     | 2.475     |
| 0.00070   | 0.00165   | 0.00177   | 0.02921   | 0.04979   | 0.09324   | 0.10696   | 0.12526   | 0.13441   | 0.19157   |
| 6.053E-05 | 5.339E-05 | 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.992E-05 | 2.752E-05 |
| 2.564     | 2.948     | 3.745     | 5.577     | 7.734     | 8.236     | 9.625     | 9.654     | 9.950     | 10.895    |
| 0.19843   | 0.22816   | 0.28990   | 0.43168   | 0.59862   | 0.63749   | 0.74497   | 0.74726   | 0.77012   | 0.84330   |
| 2.430E-05 | 2.295E-05 | 2.248E-05 | 2.178E-05 | 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 |
| 16.420    | 16.774    | 16.804    | 27.144    | 38.607    | 39.789    | 47.589    | 50.455    | 57.427    | 61.859    |
| 1.27092   | 1.29837   | 1.30065   | 2.10102   | 2.98828   | 3.07975   | 3.68346   | 3.90527   | 4.44495   | 4.78796   |
| 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.041E-06 | 3.858E-06 |
| 61.918    | 67.206    | 68.506    | 73.794    | 74.119    | 81.594    | 82.274    | 85.553    | 86.587    | 86.882    |
| 4.79253   | 5.20186   | 5.30248   | 5.71181   | 5.73697   | 6.31552   | 6.36811   | 6.62194   | 6.70198   | 6.72485   |
| 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 |
| 87.798    | 87.916    | 88.773    | 89.394    | 90.428    | 90.900    | 91.196    | 91.994    | 92.821    | 93.412    |
| 6.79573   | 6.80488   | 6.87120   | 6.91922   | 6.99926   | 7.03584   | 7.05871   | 7.12046   | 7.18448   | 7.23022   |
| 7.840E-07 | 6.656E-07 | 6.465E-07 | 6.303E-07 | 4.919E-07 | 3.289E-07 | 2.567E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |
| 93.914    | 94.091    | 94.180    | 94.239    | 94.475    | 95.184    | 95.243    | 96.159    | 97.991    | 98.789    |
| 7.26909   | 7.28281   | 7.28968   | 7.29425   | 7.31254   | 7.36743   | 7.37200   | 7.44289   | 7.58467   | 7.64641   |
| 1.246E-07 | 1.001E-07 | 4.079E-08 |           |           |           |           |           |           |           |
| 99.734    | 99.793    | 100.000   |           |           |           |           |           |           |           |
| 7.71959   | 7.72416   | 7.74017   |           |           |           |           |           |           |           |



X/Q PERCENTILES  
(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.029  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.093  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.598  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.099  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 3.680  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.784  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 9)= 5.299  
HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE (10)= 5.733

| K  | I  | XQSAVE(K, I) | XQINT(K, I)   | XQSLOP(K, I) |
|----|----|--------------|---------------|--------------|
| 10 | 1  | -7.71082     | -12.89050     | -1.19282     |
| 10 | 2  | -8.78838     | -13.70294     | -1.42907     |
| 10 | 3  | -9.25677     | -13.20666     | -1.26956     |
| 10 | 4  | -10.01579    | -13.78278     | -1.49878     |
| 10 | 5  | -10.73463    | -12.73195     | -0.98208     |
| 10 | 6  | -10.88275    | -14.49532     | -1.91858     |
| 10 | 7  | -11.06285    | -15.68413     | -2.58307     |
| 10 | 8  | -11.38039    | -17.65162     | -3.76394     |
| 10 | 9  | -11.56701    | -18.43112     | -4.24614     |
| 10 | 10 | -11.73251    | NUMXQ(K) = 10 |              |
|    |    | 1.032E-04    | 0.077         | 1.000        |
|    |    | 6.689E-05    | 0.232         | 3.000        |
|    |    | 5.408E-05    | 0.387         | 5.000        |
|    |    | 3.893E-05    | 0.774         | 10.000       |
|    |    | 3.104E-05    | 1.161         | 15.000       |
|    |    | 2.624E-05    | 1.548         | 20.000       |
|    |    | 2.292E-05    | 1.935         | 25.000       |
|    |    | 2.090E-05    | 2.322         | 30.000       |
|    |    | 1.959E-05    | 2.709         | 35.000       |
|    |    | 1.822E-05    | 3.096         | 40.000       |
|    |    | 1.647E-05    | 3.483         | 45.000       |
|    |    | 1.479E-05    | 3.870         | 50.000       |
|    |    | 1.319E-05    | 4.257         | 55.000       |
|    |    | 1.186E-05    | 4.644         | 60.000       |
|    |    | 1.043E-05    | 5.031         | 65.000       |
|    |    | 9.056E-06    | 5.418         | 70.000       |
|    |    | 4.840E-05    | 0.5           | 6.46         |

ANNUAL AVERAGE = 5.21E-07

K= 10 FIVEXQ(K)= 4.840E-05 FIVEPR(K)= 6.460

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE NE SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | MEANDER                           | BLDG WAKE | USED      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |           |
| A               | 3.0                                      | 0.74                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A               | 4.0                                      | 1.17                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A               | 5.0                                      | 1.28                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A               | 6.0                                      | 0.78                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A               | 8.0                                      | 0.27                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| A               | 24.3                                     | 0.04                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 4.085E-08                         | 4.079E-08 | 4.079E-08 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| B               | 2.0                                      | 0.16                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B               | 3.0                                      | 0.78                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B               | 4.0                                      | 0.70                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B               | 5.0                                      | 1.09                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B               | 6.0                                      | 0.70                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B               | 8.0                                      | 0.70                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| C               | 1.5                                      | 0.04                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C               | 2.0                                      | 0.27                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C               | 3.0                                      | 1.01                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C               | 4.0                                      | 1.36                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C               | 5.0                                      | 1.44                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C               | 6.0                                      | 1.21                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C               | 8.0                                      | 0.43                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| D               | 1.0                                      | 0.23                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D               | 1.5                                      | 0.74                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D               | 2.0                                      | 1.28                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D               | 3.0                                      | 5.64                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D               | 4.0                                      | 8.87                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D               | 5.0                                      | 9.30                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D               | 6.0                                      | 5.99                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D               | 8.0                                      | 6.46                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D               | 9.9                                      | 1.28                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 5.257E-06                         | 4.886E-06 | 4.886E-06 |
| D               | 24.3                                     | 0.58                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 2.141E-06                         | 1.990E-06 | 1.990E-06 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| E               | 0.4                                      | 0.00                 | 1810.              | 0.                | 0.               |                    | 91.5              | 32.3              | 179.1                | 1.568E-04                         | 2.653E-04 | 1.568E-04 |
| E               | 1.0                                      | 0.35                 | 1810.              | 0.                | 0.               |                    | 91.5              | 32.3              | 179.1                | 5.339E-05                         | 9.030E-05 | 5.339E-05 |
| E               | 1.5                                      | 0.78                 | 1810.              | 0.                | 0.               |                    | 91.5              | 32.3              | 179.1                | 3.616E-05                         | 6.115E-05 | 3.616E-05 |
| E               | 2.0                                      | 1.94                 | 1810.              | 0.                | 0.               |                    | 91.5              | 32.3              | 179.1                | 2.752E-05                         | 4.654E-05 | 2.752E-05 |

|   |      |       |       |    |    |      |      |       |           |           |           |
|---|------|-------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 3.0  | 8.71  | 1810. | 0. | 0. | 91.5 | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 11.63 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 7.23  | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 3.07  | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 2.37  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.74  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.58  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
| F | 0.4  | 0.02  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 0.74  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 0.86  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 1.44  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 1.67  | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 1.40  | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0  | 0.39  | 1810. | 0. | 0. | 63.2 | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
| G | 0.4  | 0.02  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 0.74  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.43  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.23  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.04  | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.08  | 1810. | 0. | 0. | 43.6 | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

NE SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.019     | 0.035     | 0.036     | 0.776     | 1.203     | 1.942     | 1.981     | 2.215     | 2.292     | 3.148     |
| 0.00112   | 0.00206   | 0.00215   | 0.04559   | 0.07075   | 0.11420   | 0.11648   | 0.13020   | 0.13478   | 0.18509   |
| 5.339E-05 | 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 |
| 3.498     | 4.937     | 6.610     | 8.010     | 8.788     | 9.177     | 9.411     | 11.355    | 20.068    | 20.807    |
| 0.20567   | 0.29028   | 0.38861   | 0.47093   | 0.51667   | 0.53953   | 0.55325   | 0.66759   | 1.17983   | 1.22328   |
| 2.178E-05 | 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 |
| 32.437    | 39.672    | 40.955    | 44.028    | 49.668    | 52.041    | 60.909    | 60.948    | 70.244    | 70.983    |
| 1.90702   | 2.33235   | 2.40782   | 2.58847   | 2.92005   | 3.05954   | 3.58092   | 3.58321   | 4.12975   | 4.17320   |
| 8.088E-06 | 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 |
| 76.973    | 77.246    | 83.702    | 84.714    | 85.997    | 87.359    | 87.942    | 89.381    | 89.537    | 90.743    |
| 4.52536   | 4.54136   | 4.92097   | 4.98042   | 5.05588   | 5.13592   | 5.17022   | 5.25483   | 5.26398   | 5.33487   |
| 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 |
| 91.521    | 91.948    | 92.532    | 93.232    | 94.321    | 95.021    | 95.721    | 96.460    | 97.627    | 98.911    |
| 5.38060   | 5.40576   | 5.44006   | 5.48122   | 5.54525   | 5.58641   | 5.62757   | 5.67102   | 5.73963   | 5.81509   |
| 1.658E-07 | 1.246E-07 | 4.079E-08 |           |           |           |           |           |           |           |
| 99.689    | 99.961    | 100.000   |           |           |           |           |           |           |           |
| 5.86082   | 5.87683   | 5.87912   |           |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.046  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.114  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.470  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 1.905  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.330  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.126  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.522

| K  | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|----|---|--------------|-------------|--------------|
| 11 | 1 | -7.71082     | -12.65721   | -1.16650     |
| 11 | 2 | -8.78838     | -14.63457   | -1.76270     |
| 11 | 3 | -9.25677     | -14.35723   | -1.67180     |
| 11 | 4 | -10.01579    | -13.58447   | -1.37422     |
| 11 | 5 | -10.73463    | -14.39743   | -1.76624     |
| 11 | 6 | -10.88275    | -16.07671   | -2.61013     |
| 11 | 7 | -11.54497    | -18.79886   | -4.17800     |
| 11 | 8 | -11.72508    | NUMXQ(K)= 8 |              |
|    |   | 1.344E-04    | 0.059       | 1.000        |
|    |   | 7.644E-05    | 0.176       | 3.000        |
|    |   | 5.819E-05    | 0.294       | 5.000        |
|    |   | 4.019E-05    | 0.588       | 10.000       |
|    |   | 3.288E-05    | 0.882       | 15.000       |
|    |   | 2.834E-05    | 1.176       | 20.000       |
|    |   | 2.515E-05    | 1.470       | 25.000       |
|    |   | 2.275E-05    | 1.764       | 30.000       |
|    |   | 2.060E-05    | 2.058       | 35.000       |
|    |   | 1.861E-05    | 2.352       | 40.000       |
|    |   | 1.632E-05    | 2.646       | 45.000       |
|    |   | 1.447E-05    | 2.940       | 50.000       |
|    |   | 1.296E-05    | 3.234       | 55.000       |
|    |   | 1.170E-05    | 3.527       | 60.000       |
|    |   | 1.064E-05    | 3.821       | 65.000       |
|    |   | 9.726E-06    | 4.115       | 70.000       |
|    |   | 8.515E-06    | 4.409       | 75.000       |
|    |   | 4.344E-05    | 0.5         | 8.50         |

ANNUAL AVERAGE = 4.62E-07

K= 11 FIVEXQ(K)= 4.344E-05 FIVEPR(K)= 8.505

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ENE SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE          | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|-------------------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS            | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           | CA=1459.SQ.METERS |            |              |         |         |            |                                   |           |           |
| A              | 2.0       | 0.22      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A              | 3.0       | 0.82      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 1.20      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 0.79      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.60      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.16      | 1810.             | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| B              | 2.0       | 0.19      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 0.60      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 0.85      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.76      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 6.0       | 0.41      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B              | 8.0       | 0.22      | 1810.             | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| C              | 1.5       | 0.09      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.35      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 1.04      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 1.17      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 1.20      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.57      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 0.41      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C              | 9.9       | 0.03      | 1810.             | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.13      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D              | 1.5       | 0.88      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 190.3      | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D              | 2.0       | 1.83      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 189.6      | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D              | 3.0       | 7.07      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 162.1      | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D              | 4.0       | 7.20      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 146.5      | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D              | 5.0       | 6.35      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 136.2      | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D              | 6.0       | 3.63      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 128.8      | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D              | 8.0       | 2.68      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D              | 9.9       | 0.69      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 5.257E-06                         | 4.886E-06 | 4.886E-06 |
| D              | 24.3      | 0.03      | 1810.             | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 2.141E-06                         | 1.990E-06 | 1.990E-06 |
|                |           |           |                   |            |              |         |         |            |                                   |           |           |
| E              | 0.4       | 0.00      | 1810.             | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 1.568E-04                         | 2.653E-04 | 1.568E-04 |
| E              | 1.0       | 0.63      | 1810.             | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 5.339E-05                         | 9.030E-05 | 5.339E-05 |
| E              | 1.5       | 1.42      | 1810.             | 0.         | 0.           | 91.5    | 32.3    | 179.1      | 3.616E-05                         | 6.115E-05 | 3.616E-05 |

|   |      |       |       |    |    |      |      |       |           |           |           |
|---|------|-------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 2.0  | 4.42  | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 13.30 | 1810. | 0. | 0. | 91.5 | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 7.86  | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 3.60  | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 1.93  | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 1.45  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.85  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.41  | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
|   |      |       |       |    |    |      |      |       |           |           |           |
| F | 0.4  | 0.02  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 0.98  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 1.71  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 3.25  | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 8.18  | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 1.17  | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 24.1 | 0.54  | 1810. | 0. | 0. | 63.2 | 21.0 | 63.2  | 9.933E-06 | 7.361E-06 | 7.361E-06 |
|   |      |       |       |    |    |      |      |       |           |           |           |
| G | 0.4  | 0.01  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 0.54  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 0.98  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.95  | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 3.51  | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |
| G | 4.0  | 0.09  | 1810. | 0. | 0. | 43.6 | 13.7 | 63.6  | 9.194E-05 | 7.549E-05 | 7.549E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

ENE SECTOR      BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5      A= 2917.      D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.014     | 0.035     | 0.038     | 0.575     | 1.554     | 2.533     | 6.039     | 6.986     | 7.081     | 8.786     |
| 0.00100   | 0.00254   | 0.00273   | 0.04160   | 0.11249   | 0.18338   | 0.43721   | 0.50582   | 0.51268   | 0.63616   |
|           |           |           |           |           |           |           |           |           |           |
| 5.339E-05 | 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 |
| 9.418     | 12.671    | 20.851    | 22.020    | 23.441    | 23.568    | 27.989    | 41.286    | 42.170    | 50.035    |
| 0.68190   | 0.91743   | 1.50970   | 1.59431   | 1.69722   | 1.70637   | 2.02651   | 2.98924   | 3.05327   | 3.62267   |
|           |           |           |           |           |           |           |           |           |           |
| 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 |
| 53.635    | 55.467    | 57.394    | 64.468    | 65.921    | 73.122    | 73.217    | 79.565    | 80.418    | 84.050    |
| 3.88336   | 4.01599   | 4.15549   | 4.66772   | 4.77291   | 5.29429   | 5.30115   | 5.76079   | 5.82253   | 6.08551   |
|           |           |           |           |           |           |           |           |           |           |
| 8.029E-06 | 7.361E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 |
| 84.398    | 84.935    | 87.619    | 88.661    | 89.356    | 90.525    | 90.935    | 92.136    | 92.325    | 92.894    |
| 6.11066   | 6.14954   | 6.34391   | 6.41938   | 6.46969   | 6.55430   | 6.58402   | 6.67092   | 6.68464   | 6.72580   |
|           |           |           |           |           |           |           |           |           |           |
| 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 4.919E-07 | 3.289E-07 |
| 93.494    | 93.904    | 93.936    | 93.968    | 94.820    | 95.578    | 95.989    | 96.210    | 96.431    | 97.252    |
| 6.76925   | 6.79898   | 6.80127   | 6.80355   | 6.86529   | 6.92018   | 6.94991   | 6.96591   | 6.98192   | 7.04138   |
|           |           |           |           |           |           |           |           |           |           |
| 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 |           |           |           |           |           |           |
| 98.452    | 99.242    | 99.842    | 100.000   |           |           |           |           |           |           |
| 7.12827   | 7.18544   | 7.22889   | 7.24032   |           |           |           |           |           |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 1.508  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 3.619  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 5.291  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 5.757  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 5.819

| K  | I | XQSAVE(K,I) | XQINT(K,I)  | XQSLOP(K,I) |
|----|---|-------------|-------------|-------------|
| 12 | 1 | -7.71082    | -11.91790   | -0.98636    |
| 12 | 2 | -9.33138    | -12.88668   | -1.35580    |
| 12 | 3 | -9.94734    | -14.54404   | -2.12027    |
| 12 | 4 | -10.73463   | -17.20365   | -3.60058    |
| 12 | 5 | -11.38039   | -17.74777   | -3.93702    |
| 12 | 6 | -11.54497   | -18.05599   | -4.13264    |
| 12 | 7 | -11.56701   | NUMXQ(K)= 7 |             |
|    |   | 1.544E-04   | 0.072       | 1.000       |
|    |   | 1.112E-04   | 0.217       | 3.000       |
|    |   | 9.434E-05   | 0.362       | 5.000       |
|    |   | 6.972E-05   | 0.724       | 10.000      |
|    |   | 5.690E-05   | 1.086       | 15.000      |
|    |   | 4.894E-05   | 1.448       | 20.000      |
|    |   | 4.100E-05   | 1.810       | 25.000      |
|    |   | 3.496E-05   | 2.172       | 30.000      |
|    |   | 3.044E-05   | 2.534       | 35.000      |
|    |   | 2.692E-05   | 2.896       | 40.000      |
|    |   | 2.411E-05   | 3.258       | 45.000      |
|    |   | 2.179E-05   | 3.620       | 50.000      |
|    |   | 1.862E-05   | 3.982       | 55.000      |
|    |   | 1.608E-05   | 4.344       | 60.000      |
|    |   | 1.402E-05   | 4.706       | 65.000      |
|    |   | 1.233E-05   | 5.068       | 70.000      |
|    |   | 1.087E-05   | 5.430       | 75.000      |
|    |   | 9.576E-06   | 5.792       | 80.000      |
|    |   | 8.324E-05   | 0.5         | 6.91        |

ANNUAL AVERAGE = 7.67E-07

K= 12 FIVEXQ(K)= 8.324E-05 FIVEPR(K)= 6.906

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE E SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | MEANDER                           | BLDG WAKE | USED      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |           |
| A               | 1.5                                      | 0.03                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 6.474E-07                         | 6.465E-07 | 6.465E-07 |
| A               | 2.0                                      | 0.05                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A               | 3.0                                      | 0.91                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A               | 4.0                                      | 1.23                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A               | 5.0                                      | 0.78                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A               | 6.0                                      | 0.56                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A               | 8.0                                      | 0.30                 | 1810.              | 0.                | 0.               | 0.                 | 320.1             | 1000.0            | 320.1                | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| B               | 1.5                                      | 0.03                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06 | 4.069E-06 |
| B               | 2.0                                      | 0.05                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B               | 3.0                                      | 1.42                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B               | 4.0                                      | 0.56                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B               | 5.0                                      | 0.81                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B               | 6.0                                      | 0.21                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B               | 8.0                                      | 0.32                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| B               | 9.9                                      | 0.11                 | 1810.              | 0.                | 0.               | 0.                 | 240.7             | 209.6             | 240.7                | 6.361E-07                         | 6.303E-07 | 6.303E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| C               | 1.5                                      | 0.08                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C               | 2.0                                      | 0.43                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C               | 3.0                                      | 1.29                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C               | 4.0                                      | 1.50                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C               | 5.0                                      | 0.94                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C               | 6.0                                      | 0.32                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C               | 8.0                                      | 0.32                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C               | 9.9                                      | 0.03                 | 1810.              | 0.                | 0.               | 0.                 | 182.8             | 104.9             | 182.8                | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| D               | 1.0                                      | 0.21                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D               | 1.5                                      | 1.10                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D               | 2.0                                      | 2.28                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D               | 3.0                                      | 8.54                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D               | 4.0                                      | 7.14                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D               | 5.0                                      | 7.01                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D               | 6.0                                      | 5.15                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D               | 8.0                                      | 5.15                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D               | 9.9                                      | 1.37                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.7                | 5.257E-06                         | 4.886E-06 | 4.886E-06 |
| D               | 24.3                                     | 0.27                 | 1810.              | 0.                | 0.               | 0.                 | 128.7             | 47.4              | 128.7                | 2.141E-06                         | 1.990E-06 | 1.990E-06 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |      |      |       | MINOR REV. NO. 1B |    | APPENDIX BB-7 |      |       |           | PAGE NO. 135 of 160 |           |  |
|--|------|------|-------|-------------------|----|---------------|------|-------|-----------|---------------------|-----------|--|
| E  | 0.4  | 0.00 | 1810. | 0.                | 0. | 91.5          | 32.3 | 179.1 | 1.568E-04 | 2.653E-04           | 1.568E-04 |  |
| E  | 1.0  | 0.62 | 1810. | 0.                | 0. | 91.5          | 32.3 | 179.1 | 5.339E-05 | 9.030E-05           | 5.339E-05 |  |
| E  | 1.5  | 3.17 | 1810. | 0.                | 0. | 91.5          | 32.3 | 179.1 | 3.616E-05 | 6.115E-05           | 3.616E-05 |  |
| E  | 2.0  | 4.83 | 1810. | 0.                | 0. | 91.5          | 32.3 | 179.1 | 2.752E-05 | 4.654E-05           | 2.752E-05 |  |
| E  | 3.0  | 8.00 | 1810. | 0.                | 0. | 91.5          | 32.3 | 135.6 | 2.430E-05 | 3.112E-05           | 2.430E-05 |  |
| E  | 4.0  | 5.37 | 1810. | 0.                | 0. | 91.5          | 32.3 | 113.9 | 2.178E-05 | 2.342E-05           | 2.178E-05 |  |
| E  | 5.0  | 3.60 | 1810. | 0.                | 0. | 91.5          | 32.3 | 100.8 | 1.973E-05 | 1.878E-05           | 1.878E-05 |  |
| E  | 5.9  | 2.01 | 1810. | 0.                | 0. | 91.5          | 32.3 | 92.0  | 1.805E-05 | 1.568E-05           | 1.568E-05 |  |
| E  | 7.9  | 1.91 | 1810. | 0.                | 0. | 91.5          | 32.3 | 91.5  | 1.363E-05 | 1.178E-05           | 1.178E-05 |  |
| E  | 9.8  | 1.15 | 1810. | 0.                | 0. | 91.5          | 32.3 | 91.5  | 1.096E-05 | 9.474E-06           | 9.474E-06 |  |
| E  | 24.1 | 0.62 | 1810. | 0.                | 0. | 91.5          | 32.3 | 91.5  | 4.464E-06 | 3.858E-06           | 3.858E-06 |  |
|  |      |      |       |                   |    |               |      |       |           |                     |           |  |
| F  | 0.4  | 0.03 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 2.804E-04 | 5.061E-04           | 2.804E-04 |  |
| F  | 1.0  | 1.50 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 9.546E-05 | 1.723E-04           | 9.546E-05 |  |
| F  | 1.5  | 3.44 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 6.465E-05 | 1.167E-04           | 6.465E-05 |  |
| F  | 2.0  | 4.40 | 1810. | 0.                | 0. | 63.2          | 21.0 | 153.8 | 4.920E-05 | 8.879E-05           | 4.920E-05 |  |
| F  | 3.0  | 3.44 | 1810. | 0.                | 0. | 63.2          | 21.0 | 105.7 | 4.786E-05 | 5.937E-05           | 4.786E-05 |  |
| F  | 4.0  | 0.35 | 1810. | 0.                | 0. | 63.2          | 21.0 | 83.8  | 4.545E-05 | 4.469E-05           | 4.469E-05 |  |
| F  | 5.0  | 0.03 | 1810. | 0.                | 0. | 63.2          | 21.0 | 71.4  | 4.275E-05 | 3.583E-05           | 3.583E-05 |  |
| F  | 24.1 | 0.03 | 1810. | 0.                | 0. | 63.2          | 21.0 | 63.2  | 9.933E-06 | 7.361E-06           | 7.361E-06 |  |
|  |      |      |       |                   |    |               |      |       |           |                     |           |  |
| G  | 0.4  | 0.03 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 4.480E-04 | 8.550E-04           | 4.480E-04 |  |
| G  | 1.0  | 1.15 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 1.525E-04 | 2.911E-04           | 1.525E-04 |  |
| G  | 1.5  | 1.96 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 1.033E-04 | 1.971E-04           | 1.033E-04 |  |
| G  | 2.0  | 1.26 | 1810. | 0.                | 0. | 43.6          | 13.7 | 147.9 | 7.859E-05 | 1.500E-04           | 7.859E-05 |  |
| G  | 3.0  | 0.59 | 1810. | 0.                | 0. | 43.6          | 13.7 | 87.7  | 8.860E-05 | 1.003E-04           | 8.860E-05 |  |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

E SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.030     | 0.062     | 0.065     | 1.219     | 3.179     | 4.682     | 5.272     | 6.534     | 9.970     | 10.587    |
| 0.00252   | 0.00531   | 0.00553   | 0.10386   | 0.27079   | 0.39885   | 0.44916   | 0.55664   | 0.84934   | 0.90194   |
| 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 |
| 14.989    | 18.425    | 18.774    | 21.942    | 21.968    | 22.183    | 27.015    | 35.014    | 36.115    | 41.483    |
| 1.27697   | 1.56967   | 1.59940   | 1.86924   | 1.87152   | 1.88982   | 2.30143   | 2.98289   | 3.07665   | 3.53400   |
| 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 |
| 45.080    | 47.362    | 49.375    | 57.911    | 59.817    | 66.957    | 67.037    | 74.043    | 75.197    | 80.351    |
| 3.84042   | 4.03480   | 4.20631   | 4.93349   | 5.09585   | 5.70413   | 5.71099   | 6.30784   | 6.40617   | 6.84523   |
| 8.029E-06 | 7.361E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 |
| 80.781    | 80.808    | 85.961    | 87.250    | 88.619    | 88.646    | 90.149    | 90.766    | 91.706    | 91.759    |
| 6.88181   | 6.88410   | 7.32316   | 7.43292   | 7.54955   | 7.55183   | 7.67989   | 7.73249   | 7.81252   | 7.81710   |
| 2.706E-06 | 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.465E-07 |
| 92.081    | 93.504    | 93.826    | 94.095    | 94.121    | 94.685    | 95.490    | 95.705    | 96.027    | 96.054    |
| 7.84454   | 7.96574   | 7.99318   | 8.01605   | 8.01833   | 8.06636   | 8.13496   | 8.15325   | 8.18069   | 8.18298   |
| 6.303E-07 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 |           |           |           |
| 96.162    | 96.215    | 97.128    | 98.363    | 99.141    | 99.705    | 100.000   |           |           |           |
| 8.19213   | 8.19670   | 8.27445   | 8.37964   | 8.44596   | 8.49398   | 8.51913   |           |           |           |

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.398  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 1.568  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 3.531  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 5.700  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 6.402  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 6.878

| K           | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|-------------|---|--------------|-------------|--------------|
| 13          | 1 | -7.71082     | -12.18704   | -1.10433     |
| 13          | 2 | -9.25677     | -12.91461   | -1.37853     |
| 13          | 3 | -9.94734     | -14.86563   | -2.28493     |
| 13          | 4 | -10.73463    | -15.86656   | -2.83856     |
| 13          | 5 | -11.38039    | -16.41466   | -3.18537     |
| 13          | 6 | -11.56701    | -18.39092   | -4.48395     |
| 13          | 7 | -11.73251    |             |              |
| NUMXQ(K)= 7 |   |              |             |              |
|             |   | 1.630E-04    | 0.085       | 1.000        |
|             |   | 1.123E-04    | 0.256       | 3.000        |
|             |   | 9.258E-05    | 0.426       | 5.000        |
|             |   | 6.606E-05    | 0.852       | 10.000       |
|             |   | 5.350E-05    | 1.278       | 15.000       |
|             |   | 4.439E-05    | 1.704       | 20.000       |
|             |   | 3.601E-05    | 2.130       | 25.000       |
|             |   | 3.019E-05    | 2.556       | 30.000       |
|             |   | 2.591E-05    | 2.982       | 35.000       |
|             |   | 2.261E-05    | 3.408       | 40.000       |
|             |   | 1.959E-05    | 3.834       | 45.000       |
|             |   | 1.705E-05    | 4.260       | 50.000       |
|             |   | 1.500E-05    | 4.686       | 55.000       |
|             |   | 1.331E-05    | 5.111       | 60.000       |
|             |   | 1.190E-05    | 5.537       | 65.000       |
|             |   | 1.064E-05    | 5.963       | 70.000       |
|             |   | 9.514E-06    | 6.389       | 75.000       |
|             |   | 8.212E-06    | 6.815       | 80.000       |
|             |   | 8.583E-05    | 0.5         | 5.87         |

ANNUAL AVERAGE = 9.62E-07

K= 13 FIVEXQ(K)= 8.583E-05 FIVEPR(K)= 5.869

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ESE SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|-----------------|--|----------------------|--------------------|-------------------|------------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | MEANDER                           | BLDG WAKE | USED      |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      | CA=1459.SQ.METERS                 |           |           |
| A               | 2.0                                      | 0.08                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A               | 3.0                                      | 0.55                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A               | 4.0                                      | 0.90                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A               | 5.0                                      | 0.83                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A               | 6.0                                      | 0.93                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A               | 8.0                                      | 0.75                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| A               | 9.9                                      | 0.03                 | 1810.              | 0.                | 0.               |                    | 320.1             | 1000.0            | 320.1                | 1.003E-07                         | 1.001E-07 | 1.001E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| B               | 1.5                                      | 0.03                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06 | 4.069E-06 |
| B               | 2.0                                      | 0.15                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B               | 3.0                                      | 0.70                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B               | 4.0                                      | 1.08                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B               | 5.0                                      | 0.98                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B               | 6.0                                      | 0.60                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B               | 8.0                                      | 0.45                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| B               | 9.9                                      | 0.08                 | 1810.              | 0.                | 0.               |                    | 240.7             | 209.6             | 240.7                | 6.361E-07                         | 6.303E-07 | 6.303E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| C               | 1.5                                      | 0.03                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C               | 2.0                                      | 0.30                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C               | 3.0                                      | 1.23                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C               | 4.0                                      | 1.45                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C               | 5.0                                      | 1.18                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C               | 6.0                                      | 0.53                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C               | 8.0                                      | 0.60                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C               | 9.9                                      | 0.13                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
| C               | 24.3                                     | 0.08                 | 1810.              | 0.                | 0.               |                    | 182.8             | 104.9             | 182.8                | 6.818E-07                         | 6.656E-07 | 6.656E-07 |
|                 |  |                      |                    |                   |                  |                    |                   |                   |                      |                                   |           |           |
| D               | 1.0                                      | 0.28                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |
| D               | 1.5                                      | 1.76                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |
| D               | 2.0                                      | 2.03                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |
| D               | 3.0                                      | 7.67                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |
| D               | 4.0                                      | 7.57                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |
| D               | 5.0                                      | 7.17                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |
| D               | 6.0                                      | 5.69                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |
| D               | 8.0                                      | 4.96                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06 | 6.076E-06 |
| D               | 9.9                                      | 1.25                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 5.257E-06                         | 4.886E-06 | 4.886E-06 |
| D               | 24.3                                     | 0.08                 | 1810.              | 0.                | 0.               |                    | 128.7             | 47.4              | 128.7                | 2.141E-06                         | 1.990E-06 | 1.990E-06 |

|   |      |      |       |    |    |      |      |       |           |           |           |
|---|------|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 0.4  | 0.01 | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 1.568E-04 | 2.653E-04 | 1.568E-04 |
| E | 1.0  | 1.28 | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 5.339E-05 | 9.030E-05 | 5.339E-05 |
| E | 1.5  | 4.29 | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 3.616E-05 | 6.115E-05 | 3.616E-05 |
| E | 2.0  | 4.14 | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 7.77 | 1810. | 0. | 0. | 91.5 | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 6.12 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 4.14 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 2.21 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 2.11 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.40 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.08 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| F | 0.4  | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 2.06 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 4.99 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 2.33 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 0.93 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0  | 0.08 | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| F | 7.9  | 0.03 | 1810. | 0. | 0. | 63.2 | 21.0 | 63.2  | 3.033E-05 | 2.248E-05 | 2.248E-05 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| G | 0.4  | 0.05 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 2.03 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 2.28 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.53 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.03 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

#### LOW POPULATION ZONE CALCULATIONS:

ESE SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.052     | 0.097     | 0.102     | 2.133     | 4.415     | 6.471     | 6.496     | 7.023     | 12.013    | 13.291    |
| 0.00476   | 0.00883   | 0.00932   | 0.19455   | 0.40264   | 0.59016   | 0.59244   | 0.64046   | 1.09553   | 1.21215   |
| 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.248E-05 | 2.178E-05 |
| 15.623    | 16.551    | 16.626    | 20.914    | 21.190    | 25.327    | 33.101    | 34.856    | 34.881    | 40.999    |
| 1.42482   | 1.50943   | 1.51629   | 1.90733   | 1.93248   | 2.30980   | 3.01869   | 3.17877   | 3.18105   | 3.73902   |
| 1.878E-05 | 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 |
| 45.136    | 47.167    | 49.374    | 57.047    | 59.153    | 66.726    | 66.751    | 73.922    | 74.323    | 80.015    |
| 4.11634   | 4.30157   | 4.50280   | 5.20255   | 5.39464   | 6.08524   | 6.08753   | 6.74154   | 6.77813   | 7.29722   |
| 8.029E-06 | 6.076E-06 | 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 |
| 80.316    | 85.281    | 86.510    | 87.764    | 87.789    | 89.243    | 89.318    | 90.497    | 90.647    | 91.174    |
| 7.32466   | 7.77744   | 7.88949   | 8.00383   | 8.00612   | 8.13875   | 8.14561   | 8.25309   | 8.26681   | 8.31483   |
| 2.070E-06 | 2.033E-06 | 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.656E-07 | 6.303E-07 |
| 91.876    | 92.478    | 92.553    | 92.678    | 93.756    | 94.734    | 95.336    | 95.787    | 95.863    | 95.938    |
| 8.37886   | 8.43374   | 8.44060   | 8.45204   | 8.55037   | 8.63955   | 8.69443   | 8.73559   | 8.74246   | 8.74932   |
| 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 | 1.001E-07 |           |           |           |
| 96.013    | 96.565    | 97.467    | 98.295    | 99.223    | 99.975    | 100.000   |           |           |           |
| 8.75618   | 8.80648   | 8.88881   | 8.96427   | 9.04888   | 9.11748   | 9.11977   |           |           |           |

#### X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.194  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.589  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 1.094  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 3.016  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 3.736  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 6.081  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 6.738  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 9)= 7.321  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE(10)= 7.774

| K  | I  | XQSAVE(K,I) | XQINT(K,I)   | XQSLOP(K,I) |
|----|----|-------------|--------------|-------------|
| 14 | 1  | -7.71082    | -11.85185    | -1.06105    |
| 14 | 2  | -8.78838    | -12.45509    | -1.26998    |
| 14 | 3  | -9.25677    | -13.59902    | -1.72421    |
| 14 | 4  | -9.64651    | -15.06723    | -2.36469    |
| 14 | 5  | -10.62522   | -12.76027    | -1.13659    |
| 14 | 6  | -10.73463   | -15.64805    | -2.75693    |
| 14 | 7  | -11.38039   | -16.24626    | -3.14337    |
| 14 | 8  | -11.54497   | -18.02086    | -4.32991    |
| 14 | 9  | -11.73251   | -24.43790    | -8.74843    |
| 14 | 10 | -12.01110   | NUMXQ(K)= 10 |             |
|    |    | 1.948E-04   | 0.091        | 1.000       |
|    |    | 1.328E-04   | 0.274        | 3.000       |
|    |    | 1.070E-04   | 0.456        | 5.000       |
|    |    | 7.279E-05   | 0.912        | 10.000      |
|    |    | 5.281E-05   | 1.368        | 15.000      |
|    |    | 4.025E-05   | 1.824        | 20.000      |
|    |    | 3.235E-05   | 2.280        | 25.000      |
|    |    | 2.690E-05   | 2.736        | 30.000      |
|    |    | 2.362E-05   | 3.192        | 35.000      |
|    |    | 2.206E-05   | 3.648        | 40.000      |
|    |    | 1.934E-05   | 4.104        | 45.000      |
|    |    | 1.687E-05   | 4.560        | 50.000      |
|    |    | 1.486E-05   | 5.016        | 55.000      |
|    |    | 1.322E-05   | 5.472        | 60.000      |
|    |    | 1.184E-05   | 5.928        | 65.000      |
|    |    | 1.058E-05   | 6.384        | 70.000      |
|    |    | 9.375E-06   | 6.840        | 75.000      |
|    |    | 8.101E-06   | 7.296        | 80.000      |
|    |    | 6.171E-06   | 7.752        | 85.000      |
|    |    | 1.027E-04   | 0.5          | 5.48        |

ANNUAL AVERAGE = 1.12E-06

K= 14 FIVEXQ(K)= 1.027E-04 FIVEPR(K)= 5.483

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SE SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT<br>METERS | EFF PLUME<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER           | BLDG WAKE | USED |
|-----------------|--|----------------------|--------------------|-------------------|--------------|---------------------|-------------------|-------------------|----------------------|-----------------------------------|-------------------|-----------|------|
|                 |  |                      |                    |                   |              |                     |                   |                   |                      |                                   | CA=1459.SQ.METERS |           |      |
| A               | 3.0                                      | 1.05                 | 1810.              | 0.                | 0.           | 0.                  | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07         | 3.289E-07 |      |
| A               | 4.0                                      | 1.49                 | 1810.              | 0.                | 0.           | 0.                  | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07         | 2.476E-07 |      |
| A               | 5.0                                      | 2.25                 | 1810.              | 0.                | 0.           | 0.                  | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07         | 1.985E-07 |      |
| A               | 6.0                                      | 0.69                 | 1810.              | 0.                | 0.           | 0.                  | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07         | 1.658E-07 |      |
| A               | 8.0                                      | 0.54                 | 1810.              | 0.                | 0.           | 0.                  | 320.1             | 1000.0            | 320.1                | 1.247E-07                         | 1.246E-07         | 1.246E-07 |      |
|                 |  |                      |                    |                   |              |                     |                   |                   |                      |                                   |                   |           |      |
| B               | 1.5                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06         | 4.069E-06 |      |
| B               | 2.0                                      | 0.18                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06         | 3.096E-06 |      |
| B               | 3.0                                      | 1.02                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06         | 2.070E-06 |      |
| B               | 4.0                                      | 1.56                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06         | 1.558E-06 |      |
| B               | 5.0                                      | 1.02                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06         | 1.250E-06 |      |
| B               | 6.0                                      | 0.73                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06         | 1.044E-06 |      |
| B               | 8.0                                      | 0.15                 | 1810.              | 0.                | 0.           | 0.                  | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07         | 7.840E-07 |      |
|                 |  |                      |                    |                   |              |                     |                   |                   |                      |                                   |                   |           |      |
| C               | 1.5                                      | 0.07                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 1.081E-05                         | 1.055E-05         | 1.055E-05 |      |
| C               | 2.0                                      | 0.18                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06         | 8.029E-06 |      |
| C               | 3.0                                      | 1.74                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06         | 5.368E-06 |      |
| C               | 4.0                                      | 1.85                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06         | 4.041E-06 |      |
| C               | 5.0                                      | 1.82                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06         | 3.240E-06 |      |
| C               | 6.0                                      | 0.80                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06         | 2.706E-06 |      |
| C               | 8.0                                      | 0.25                 | 1810.              | 0.                | 0.           | 0.                  | 182.8             | 104.9             | 182.8                | 2.082E-06                         | 2.033E-06         | 2.033E-06 |      |
|                 |  |                      |                    |                   |              |                     |                   |                   |                      |                                   |                   |           |      |
| D               | 1.0                                      | 0.54                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05         | 3.389E-05 |      |
| D               | 1.5                                      | 2.62                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05         | 2.295E-05 |      |
| D               | 2.0                                      | 4.83                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05         | 1.753E-05 |      |
| D               | 3.0                                      | 11.73                | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05         | 1.371E-05 |      |
| D               | 4.0                                      | 10.13                | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05         | 1.142E-05 |      |
| D               | 5.0                                      | 7.01                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06         | 9.685E-06 |      |
| D               | 6.0                                      | 2.47                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06         | 8.088E-06 |      |
| D               | 8.0                                      | 1.74                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06         | 6.076E-06 |      |
| D               | 9.9                                      | 0.07                 | 1810.              | 0.                | 0.           | 0.                  | 128.7             | 47.4              | 128.7                | 5.257E-06                         | 4.886E-06         | 4.886E-06 |      |
|                 |  |                      |                    |                   |              |                     |                   |                   |                      |                                   |                   |           |      |
| E               | 0.4                                      | 0.01                 | 1810.              | 0.                | 0.           | 0.                  | 91.5              | 32.3              | 179.1                | 1.568E-04                         | 2.653E-04         | 1.568E-04 |      |
| E               | 1.0                                      | 1.71                 | 1810.              | 0.                | 0.           | 0.                  | 91.5              | 32.3              | 179.1                | 5.339E-05                         | 9.030E-05         | 5.339E-05 |      |
| E               | 1.5                                      | 4.72                 | 1810.              | 0.                | 0.           | 0.                  | 91.5              | 32.3              | 179.1                | 3.616E-05                         | 6.115E-05         | 3.616E-05 |      |
| E               | 2.0                                      | 6.25                 | 1810.              | 0.                | 0.           | 0.                  | 91.5              | 32.3              | 179.1                | 2.752E-05                         | 4.654E-05         | 2.752E-05 |      |
| E               | 3.0                                      | 6.65                 | 1810.              | 0.                | 0.           | 0.                  | 91.5              | 32.3              | 135.6                | 2.430E-05                         | 3.112E-05         | 2.430E-05 |      |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  |  | PAGE NO. 143 of 160 |  |
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|
|--|--|--|--|-------------------|--|---------------|--|--|--|---------------------|--|

|   |     |      |       |    |    |      |      |       |           |           |           |
|---|-----|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 4.0 | 4.72 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0 | 2.22 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9 | 0.84 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9 | 0.69 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| F | 0.4 | 0.06 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0 | 2.87 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5 | 4.14 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0 | 1.60 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0 | 0.36 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 4.0 | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 83.8  | 4.545E-05 | 4.469E-05 | 4.469E-05 |
| G | 0.4 | 0.07 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0 | 2.80 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5 | 1.42 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0 | 0.18 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0 | 0.07 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SE SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.072     | 0.134     | 0.141     | 2.938     | 4.355     | 7.225     | 7.297     | 7.479     | 11.620    | 13.327    |
| 0.00452   | 0.00845   | 0.00890   | 0.18498   | 0.27416   | 0.45481   | 0.45939   | 0.47082   | 0.73151   | 0.83899   |
| 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 |
| 14.926    | 15.289    | 15.325    | 20.048    | 20.593    | 26.841    | 33.488    | 36.104    | 40.826    | 43.042    |
| 0.93961   | 0.96247   | 0.96476   | 1.26204   | 1.29634   | 1.68966   | 2.10814   | 2.27279   | 2.57007   | 2.70956   |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 8.088E-06 | 8.029E-06 | 6.076E-06 |
| 47.873    | 48.708    | 60.442    | 61.132    | 71.267    | 71.339    | 78.350    | 80.820    | 81.002    | 82.745    |
| 3.01370   | 3.06629   | 3.80492   | 3.84837   | 4.48637   | 4.49095   | 4.93229   | 5.08779   | 5.09922   | 5.20899   |
| 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 | 1.558E-06 |
| 84.489    | 84.562    | 84.598    | 86.451    | 88.267    | 88.448    | 89.248    | 90.265    | 90.519    | 92.081    |
| 5.31875   | 5.32333   | 5.32561   | 5.44224   | 5.55657   | 5.56801   | 5.61832   | 5.68235   | 5.69835   | 5.79668   |
| 1.250E-06 | 1.044E-06 | 7.840E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 |           |           |
| 93.098    | 93.825    | 93.970    | 95.023    | 96.513    | 98.765    | 99.455    | 100.000   |           |           |
| 5.86071   | 5.90645   | 5.91560   | 5.98191   | 6.07567   | 6.21745   | 6.26090   | 6.29520   |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

|                 |                 |                       |
|-----------------|-----------------|-----------------------|
| CHI/Q           | WITH RESPECT TO | WHEN THE WIND BLOWS   |
| SEC/CUBIC METER | THE TOTAL TIME  | INTO THIS SECTOR ONLY |

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 2)= 0.185  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 3)= 0.454  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 4)= 0.731  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 5)= 2.270  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 6)= 2.567  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 7)= 4.483  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE ( 8)= 4.929

| K  | I | XQSAVE(K, I) | XQINT(K, I) | XQSLOP(K, I) |
|----|---|--------------|-------------|--------------|
| 15 | 1 | -7.71082     | -11.87959   | -1.06482     |
| 15 | 2 | -8.78838     | -13.40987   | -1.59195     |
| 15 | 3 | -9.25677     | -15.34572   | -2.33399     |
| 15 | 4 | -9.64651     | -15.38022   | -2.34812     |
| 15 | 5 | -10.68199    | -12.69557   | -1.00636     |
| 15 | 6 | -10.73463    | -15.74110   | -2.56934     |
| 15 | 7 | -11.38039    | -17.53360   | -3.62548     |
| 15 | 8 | -11.54497    |             |              |

NUMXQ(K)= 8

|           |       |        |
|-----------|-------|--------|
| 2.149E-04 | 0.063 | 1.000  |
| 1.509E-04 | 0.189 | 3.000  |
| 1.162E-04 | 0.315 | 5.000  |
| 7.329E-05 | 0.630 | 10.000 |
| 5.189E-05 | 0.944 | 15.000 |
| 4.016E-05 | 1.259 | 20.000 |
| 3.269E-05 | 1.574 | 25.000 |
| 2.750E-05 | 1.889 | 30.000 |
| 2.367E-05 | 2.203 | 35.000 |
| 2.197E-05 | 2.518 | 40.000 |
| 1.954E-05 | 2.833 | 45.000 |
| 1.734E-05 | 3.148 | 50.000 |
| 1.554E-05 | 3.462 | 55.000 |
| 1.403E-05 | 3.777 | 60.000 |
| 1.276E-05 | 4.092 | 65.000 |
| 1.167E-05 | 4.407 | 70.000 |
| 1.045E-05 | 4.721 | 75.000 |

|           |     |      |
|-----------|-----|------|
| 8.847E-05 | 0.5 | 7.94 |
|-----------|-----|------|

ANNUAL AVERAGE = 8.41E-07

K= 15 FIVEXQ(K)= 8.847E-05 FIVEPR(K)= 7.943

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE SSE SECTOR.

| STABILITY CLASS | WINDSPEED<br>METER/SEC<br>AT 10.0 METERS | FREQUENCY<br>PERCENT | DISTANCE<br>METERS | TERRAIN<br>METERS | HT<br>METERS | EFF<br>METERS | PLUME HT<br>METERS | SIGMA-Y<br>METERS | SIGMA-Z<br>METERS | MEANDER-SY<br>METERS | ** CHI/Q VALUES (SEC/CUBIC METER) | MEANDER   | BLDG WAKE | USED |
|-----------------|--|----------------------|--------------------|-------------------|--------------|---------------|--------------------|-------------------|-------------------|----------------------|-----------------------------------|-----------|-----------|------|
|                 |  |                      |                    |                   |              |               |                    |                   |                   |                      |                                   |           |           |      |
| A               | 2.0                                      | 0.12                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 4.927E-07                         | 4.919E-07 | 4.919E-07 |      |
| A               | 3.0                                      | 0.56                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 3.294E-07                         | 3.289E-07 | 3.289E-07 |      |
| A               | 4.0                                      | 1.98                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 2.480E-07                         | 2.476E-07 | 2.476E-07 |      |
| A               | 5.0                                      | 2.34                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 1.988E-07                         | 1.985E-07 | 1.985E-07 |      |
| A               | 6.0                                      | 0.77                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 1.660E-07                         | 1.658E-07 | 1.658E-07 |      |
| A               | 8.0                                      | 0.32                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 320.1             | 1000.0            | 320.1                | 1.247E-07                         | 1.246E-07 | 1.246E-07 |      |
| B               | 1.0                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 6.064E-06                         | 6.008E-06 | 6.008E-06 |      |
| B               | 1.5                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 4.107E-06                         | 4.069E-06 | 4.069E-06 |      |
| B               | 2.0                                      | 0.04                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 3.125E-06                         | 3.096E-06 | 3.096E-06 |      |
| B               | 3.0                                      | 1.09                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 2.089E-06                         | 2.070E-06 | 2.070E-06 |      |
| B               | 4.0                                      | 1.25                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 1.573E-06                         | 1.558E-06 | 1.558E-06 |      |
| B               | 5.0                                      | 1.33                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 1.261E-06                         | 1.250E-06 | 1.250E-06 |      |
| B               | 6.0                                      | 0.69                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 1.053E-06                         | 1.044E-06 | 1.044E-06 |      |
| B               | 8.0                                      | 0.28                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 240.7             | 209.6             | 240.7                | 7.912E-07                         | 7.840E-07 | 7.840E-07 |      |
| C               | 2.0                                      | 0.36                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 8.223E-06                         | 8.029E-06 | 8.029E-06 |      |
| C               | 3.0                                      | 1.13                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 5.498E-06                         | 5.368E-06 | 5.368E-06 |      |
| C               | 4.0                                      | 1.65                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 4.139E-06                         | 4.041E-06 | 4.041E-06 |      |
| C               | 5.0                                      | 1.33                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 3.318E-06                         | 3.240E-06 | 3.240E-06 |      |
| C               | 6.0                                      | 0.48                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 2.771E-06                         | 2.706E-06 | 2.706E-06 |      |
| C               | 8.0                                      | 0.32                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 182.8             | 104.9             | 182.8                | 2.082E-06                         | 2.033E-06 | 2.033E-06 |      |
| D               | 1.0                                      | 0.65                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 190.3                | 3.389E-05                         | 4.657E-05 | 3.389E-05 |      |
| D               | 1.5                                      | 1.57                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 190.3                | 2.295E-05                         | 3.154E-05 | 2.295E-05 |      |
| D               | 2.0                                      | 3.67                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 189.6                | 1.753E-05                         | 2.400E-05 | 1.753E-05 |      |
| D               | 3.0                                      | 11.14                | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 162.1                | 1.371E-05                         | 1.605E-05 | 1.371E-05 |      |
| D               | 4.0                                      | 8.60                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 146.5                | 1.142E-05                         | 1.208E-05 | 1.142E-05 |      |
| D               | 5.0                                      | 8.35                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 136.2                | 9.848E-06                         | 9.685E-06 | 9.685E-06 |      |
| D               | 6.0                                      | 5.61                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 128.8                | 8.699E-06                         | 8.088E-06 | 8.088E-06 |      |
| D               | 8.0                                      | 3.59                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 128.7                | 6.538E-06                         | 6.076E-06 | 6.076E-06 |      |
| D               | 9.9                                      | 0.85                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 128.7                | 5.257E-06                         | 4.886E-06 | 4.886E-06 |      |
| D               | 24.3                                     | 0.12                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 128.7             | 47.4              | 128.7                | 2.141E-06                         | 1.990E-06 | 1.990E-06 |      |
| E               | 0.4                                      | 0.01                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 91.5              | 32.3              | 179.1                | 1.568E-04                         | 2.653E-04 | 1.568E-04 |      |
| E               | 1.0                                      | 1.49                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 91.5              | 32.3              | 179.1                | 5.339E-05                         | 9.030E-05 | 5.339E-05 |      |
| E               | 1.5                                      | 3.31                 | 1810.              | 0.                | 0.           | 0.            | 0.                 | 91.5              | 32.3              | 179.1                | 3.616E-05                         | 6.115E-05 | 3.616E-05 |      |

CA=1459.SQ.METERS

|   |      |      |       |    |    |      |      |       |           |           |           |
|---|------|------|-------|----|----|------|------|-------|-----------|-----------|-----------|
| E | 2.0  | 3.59 | 1810. | 0. | 0. | 91.5 | 32.3 | 179.1 | 2.752E-05 | 4.654E-05 | 2.752E-05 |
| E | 3.0  | 8.68 | 1810. | 0. | 0. | 91.5 | 32.3 | 135.6 | 2.430E-05 | 3.112E-05 | 2.430E-05 |
| E | 4.0  | 6.17 | 1810. | 0. | 0. | 91.5 | 32.3 | 113.9 | 2.178E-05 | 2.342E-05 | 2.178E-05 |
| E | 5.0  | 3.43 | 1810. | 0. | 0. | 91.5 | 32.3 | 100.8 | 1.973E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 1.21 | 1810. | 0. | 0. | 91.5 | 32.3 | 92.0  | 1.805E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 0.93 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 24.1 | 0.08 | 1810. | 0. | 0. | 91.5 | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| F | 0.4  | 0.05 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 2.804E-04 | 5.061E-04 | 2.804E-04 |
| F | 1.0  | 2.10 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 9.546E-05 | 1.723E-04 | 9.546E-05 |
| F | 1.5  | 2.74 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 6.465E-05 | 1.167E-04 | 6.465E-05 |
| F | 2.0  | 1.13 | 1810. | 0. | 0. | 63.2 | 21.0 | 153.8 | 4.920E-05 | 8.879E-05 | 4.920E-05 |
| F | 3.0  | 0.48 | 1810. | 0. | 0. | 63.2 | 21.0 | 105.7 | 4.786E-05 | 5.937E-05 | 4.786E-05 |
| F | 5.0  | 0.04 | 1810. | 0. | 0. | 63.2 | 21.0 | 71.4  | 4.275E-05 | 3.583E-05 | 3.583E-05 |
|   |      |      |       |    |    |      |      |       |           |           |           |
| G | 0.4  | 0.07 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 4.480E-04 | 8.550E-04 | 4.480E-04 |
| G | 1.0  | 2.66 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.525E-04 | 2.911E-04 | 1.525E-04 |
| G | 1.5  | 1.13 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 1.033E-04 | 1.971E-04 | 1.033E-04 |
| G | 2.0  | 0.36 | 1810. | 0. | 0. | 43.6 | 13.7 | 147.9 | 7.859E-05 | 1.500E-04 | 7.859E-05 |
| G | 3.0  | 0.04 | 1810. | 0. | 0. | 43.6 | 13.7 | 87.7  | 8.860E-05 | 1.003E-04 | 8.860E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

SSE SECTOR BOUNDARY DISTANCE = 1810.0 METERS

LATERAL PLUME MEANDER/BUILDING WAKE CREDIT ALLOWED

AS A FUNCTION OF DOWNWIND DISTANCE.

MEANDER CREDIT IS FOR WINDSPEEDS LESS THAN 6 MPS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.

THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.

THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 6.465E-05 | 5.339E-05 |
| 0.068     | 0.114     | 0.120     | 2.784     | 3.914     | 6.012     | 6.052     | 6.416     | 9.160     | 10.653    |
| 0.00388   | 0.00646   | 0.00681   | 0.15774   | 0.22177   | 0.34068   | 0.34297   | 0.36355   | 0.51905   | 0.60366   |
| 4.920E-05 | 4.786E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.752E-05 | 2.430E-05 | 2.295E-05 | 2.178E-05 | 1.878E-05 |
| 11.783    | 12.267    | 15.576    | 15.617    | 16.262    | 19.854    | 28.530    | 30.104    | 36.279    | 39.709    |
| 0.66769   | 0.69513   | 0.88264   | 0.88493   | 0.92152   | 1.12504   | 1.61669   | 1.70588   | 2.05575   | 2.25012   |
| 1.753E-05 | 1.568E-05 | 1.371E-05 | 1.178E-05 | 1.142E-05 | 9.685E-06 | 8.088E-06 | 8.029E-06 | 6.076E-06 | 6.008E-06 |
| 43.381    | 44.592    | 55.730    | 56.658    | 65.254    | 73.608    | 79.217    | 79.580    | 83.172    | 83.212    |
| 2.45822   | 2.52682   | 3.15797   | 3.21056   | 3.69764   | 4.17100   | 4.48886   | 4.50944   | 4.71296   | 4.71525   |
| 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 |
| 84.342    | 85.190    | 85.230    | 86.884    | 86.965    | 88.297    | 88.337    | 88.822    | 89.911    | 90.234    |
| 4.77928   | 4.82730   | 4.82959   | 4.92335   | 4.92792   | 5.00338   | 5.00567   | 5.03311   | 5.09485   | 5.11315   |
| 1.990E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 4.919E-07 | 3.289E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 |
| 90.355    | 91.606    | 92.938    | 93.624    | 93.906    | 94.027    | 94.592    | 96.570    | 98.910    | 99.677    |
| 5.12001   | 5.19090   | 5.26636   | 5.30523   | 5.32124   | 5.32810   | 5.36012   | 5.47217   | 5.60480   | 5.64825   |
| 1.246E-07 |           |           |           |           |           |           |           |           |           |
| 100.000   |           |           |           |           |           |           |           |           |           |
| 5.66654   |           |           |           |           |           |           |           |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE ORDERED X/Q-FREQUENCY VALUES, AND AS PLOTTED ON A LOG-NORMAL GRAPH.)



PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 2)= 0.158  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 0.340  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 0.518  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 5)= 1.615  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 6)= 2.054  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 7)= 3.155  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 8)= 3.694  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 9)= 4.168  
 HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE(10)= 4.506

| K  | I  | XQSAVE(K, I) | XQINT(K, I)  | XQSLOP(K, I) |
|----|----|--------------|--------------|--------------|
| 16 | 1  | -7.71082     | -11.97163    | -1.07813     |
| 16 | 2  | -8.78838     | -14.40194    | -1.90125     |
| 16 | 3  | -9.25677     | -16.63657    | -2.72699     |
| 16 | 4  | -9.64651     | -15.58311    | -2.31601     |
| 16 | 5  | -10.62522    | -13.01781    | -1.11767     |
| 16 | 6  | -10.73463    | -15.86353    | -2.51071     |
| 16 | 7  | -11.19742    | -15.97478    | -2.57057     |
| 16 | 8  | -11.38039    | -16.65777    | -2.95270     |
| 16 | 9  | -11.54497    | -20.37233    | -5.09791     |
| 16 | 10 | -11.73251    | NUMXQ(K)= 10 |              |
|    |    | 2.114E-04    | 0.057        | 1.000        |
|    |    | 1.459E-04    | 0.170        | 3.000        |
|    |    | 1.071E-04    | 0.283        | 5.000        |
|    |    | 6.023E-05    | 0.567        | 10.000       |
|    |    | 4.299E-05    | 0.850        | 15.000       |
|    |    | 3.350E-05    | 1.133        | 20.000       |
|    |    | 2.743E-05    | 1.417        | 25.000       |
|    |    | 2.375E-05    | 1.700        | 30.000       |
|    |    | 2.214E-05    | 1.983        | 35.000       |
|    |    | 1.966E-05    | 2.267        | 40.000       |
|    |    | 1.733E-05    | 2.550        | 45.000       |
|    |    | 1.546E-05    | 2.833        | 50.000       |
|    |    | 1.391E-05    | 3.117        | 55.000       |
|    |    | 1.259E-05    | 3.400        | 60.000       |
|    |    | 1.147E-05    | 3.683        | 65.000       |
|    |    | 1.038E-05    | 3.967        | 70.000       |
|    |    | 9.260E-06    | 4.250        | 75.000       |
|    |    | 6.697E-05    | 0.5          | 8.82         |

ANNUAL AVERAGE = 6.65E-07

K= 16 FIVEXQ(K)= 6.697E-05 FIVEPR(K)= 8.824

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

PARAMETER VALUES FOR THE CHI/Q CALCULATIONS FOR THE ALL SECTOR.

| STABILITY      | WINDSPEED | FREQUENCY | DISTANCE | TERRAIN HT | EFF PLUME HT | SIGMA-Y | SIGMA-Z | MEANDER-SY | ** CHI/Q VALUES (SEC/CUBIC METER) |           |           |
|----------------|-----------|-----------|----------|------------|--------------|---------|---------|------------|-----------------------------------|-----------|-----------|
| CLASS          | METER/SEC | PERCENT   | METERS   | METERS     | METERS       | METERS  | METERS  | METERS     | MEANDER                           | BLDG WAKE | USED      |
| AT 10.0 METERS |           |           |          |            |              |         |         |            | CA=1459.SQ.METERS                 |           |           |
| A              | 1.5       | 0.03      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 6.474E-07                         | 6.465E-07 | 6.465E-07 |
| A              | 2.0       | 0.26      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.927E-07                         | 4.919E-07 | 4.919E-07 |
| A              | 3.0       | 1.20      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 3.294E-07                         | 3.289E-07 | 3.289E-07 |
| A              | 4.0       | 1.24      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 2.480E-07                         | 2.476E-07 | 2.476E-07 |
| A              | 5.0       | 1.06      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.988E-07                         | 1.985E-07 | 1.985E-07 |
| A              | 6.0       | 0.51      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.660E-07                         | 1.658E-07 | 1.658E-07 |
| A              | 8.0       | 0.34      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.247E-07                         | 1.246E-07 | 1.246E-07 |
| A              | 9.9       | 0.03      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 1.003E-07                         | 1.001E-07 | 1.001E-07 |
| A              | 24.3      | 0.03      | 1810.    | 0.         | 0.           | 320.1   | 1000.0  | 320.1      | 4.085E-08                         | 4.079E-08 | 4.079E-08 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| B              | 1.0       | 0.00      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 6.064E-06                         | 6.008E-06 | 6.008E-06 |
| B              | 1.5       | 0.07      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 4.107E-06                         | 4.069E-06 | 4.069E-06 |
| B              | 2.0       | 0.27      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 3.125E-06                         | 3.096E-06 | 3.096E-06 |
| B              | 3.0       | 1.00      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.089E-06                         | 2.070E-06 | 2.070E-06 |
| B              | 4.0       | 0.87      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.573E-06                         | 1.558E-06 | 1.558E-06 |
| B              | 5.0       | 0.70      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.261E-06                         | 1.250E-06 | 1.250E-06 |
| B              | 6.0       | 0.40      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 1.053E-06                         | 1.044E-06 | 1.044E-06 |
| B              | 8.0       | 0.25      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 7.912E-07                         | 7.840E-07 | 7.840E-07 |
| B              | 9.9       | 0.04      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 6.361E-07                         | 6.303E-07 | 6.303E-07 |
| B              | 24.3      | 0.01      | 1810.    | 0.         | 0.           | 240.7   | 209.6   | 240.7      | 2.591E-07                         | 2.567E-07 | 2.567E-07 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| C              | 1.0       | 0.01      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.596E-05                         | 1.558E-05 | 1.558E-05 |
| C              | 1.5       | 0.13      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.081E-05                         | 1.055E-05 | 1.055E-05 |
| C              | 2.0       | 0.50      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 8.223E-06                         | 8.029E-06 | 8.029E-06 |
| C              | 3.0       | 1.29      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 5.498E-06                         | 5.368E-06 | 5.368E-06 |
| C              | 4.0       | 1.19      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 4.139E-06                         | 4.041E-06 | 4.041E-06 |
| C              | 5.0       | 0.88      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 3.318E-06                         | 3.240E-06 | 3.240E-06 |
| C              | 6.0       | 0.49      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.771E-06                         | 2.706E-06 | 2.706E-06 |
| C              | 8.0       | 0.35      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 2.082E-06                         | 2.033E-06 | 2.033E-06 |
| C              | 9.9       | 0.05      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 1.674E-06                         | 1.634E-06 | 1.634E-06 |
| C              | 24.3      | 0.02      | 1810.    | 0.         | 0.           | 182.8   | 104.9   | 182.8      | 6.818E-07                         | 6.656E-07 | 6.656E-07 |
|                |           |           |          |            |              |         |         |            |                                   |           |           |
| D              | 1.0       | 0.42      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 5.011E-05                         | 4.657E-05 | 4.657E-05 |
| D              | 1.5       | 1.85      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 3.394E-05                         | 3.154E-05 | 3.154E-05 |
| D              | 2.0       | 3.20      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 2.582E-05                         | 2.400E-05 | 2.400E-05 |
| D              | 3.0       | 8.25      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 1.727E-05                         | 1.605E-05 | 1.605E-05 |
| D              | 4.0       | 7.24      | 1810.    | 0.         | 0.           | 128.7   | 47.4    | 128.7      | 1.300E-05                         | 1.208E-05 | 1.208E-05 |

| CALCULATION NO. BYR04-050, BRW-04-0044-M |  |  |  |  |  | MINOR REV. NO. 1B |  | APPENDIX BB-7 |  |  | PAGE NO. 151 of 160 |  |
|--|--|--|--|--|--|-------------------|--|---------------|--|--|---------------------|--|
|--|--|--|--|--|--|-------------------|--|---------------|--|--|---------------------|--|

|   |      |      |       |    |    |       |      |       |           |           |           |
|---|------|------|-------|----|----|-------|------|-------|-----------|-----------|-----------|
| D | 5.0  | 6.01 | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 1.042E-05 | 9.685E-06 | 9.685E-06 |
| D | 6.0  | 4.15 | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 8.703E-06 | 8.088E-06 | 8.088E-06 |
| D | 8.0  | 3.43 | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 6.538E-06 | 6.076E-06 | 6.076E-06 |
| D | 9.9  | 0.87 | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 5.257E-06 | 4.886E-06 | 4.886E-06 |
| D | 24.3 | 0.15 | 1810. | 0. | 0. | 128.7 | 47.4 | 128.7 | 2.141E-06 | 1.990E-06 | 1.990E-06 |
| E | 0.4  | 0.01 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 3.069E-04 | 2.653E-04 | 2.653E-04 |
| E | 1.0  | 1.65 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.045E-04 | 9.030E-05 | 9.030E-05 |
| E | 1.5  | 3.96 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 7.075E-05 | 6.115E-05 | 6.115E-05 |
| E | 2.0  | 4.85 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 5.384E-05 | 4.654E-05 | 4.654E-05 |
| E | 3.0  | 9.56 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 3.600E-05 | 3.112E-05 | 3.112E-05 |
| E | 4.0  | 7.23 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 2.710E-05 | 2.342E-05 | 2.342E-05 |
| E | 5.0  | 4.72 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 2.173E-05 | 1.878E-05 | 1.878E-05 |
| E | 5.9  | 2.72 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.815E-05 | 1.568E-05 | 1.568E-05 |
| E | 7.9  | 2.33 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.363E-05 | 1.178E-05 | 1.178E-05 |
| E | 9.8  | 0.61 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 1.096E-05 | 9.474E-06 | 9.474E-06 |
| E | 24.1 | 0.20 | 1810. | 0. | 0. | 91.5  | 32.3 | 91.5  | 4.464E-06 | 3.858E-06 | 3.858E-06 |
| F | 0.4  | 0.05 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 6.829E-04 | 5.061E-04 | 5.061E-04 |
| F | 1.0  | 2.10 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 2.325E-04 | 1.723E-04 | 1.723E-04 |
| F | 1.5  | 2.76 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 1.574E-04 | 1.167E-04 | 1.167E-04 |
| F | 2.0  | 2.07 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 1.198E-04 | 8.879E-05 | 8.879E-05 |
| F | 3.0  | 1.90 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 8.010E-05 | 5.937E-05 | 5.937E-05 |
| F | 4.0  | 0.49 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 6.030E-05 | 4.469E-05 | 4.469E-05 |
| F | 5.0  | 0.16 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 4.834E-05 | 3.583E-05 | 3.583E-05 |
| F | 5.9  | 0.02 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 4.038E-05 | 2.992E-05 | 2.992E-05 |
| F | 7.9  | 0.01 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 3.033E-05 | 2.248E-05 | 2.248E-05 |
| F | 9.8  | 0.03 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 2.439E-05 | 1.807E-05 | 1.807E-05 |
| F | 24.1 | 0.04 | 1810. | 0. | 0. | 63.2  | 21.0 | 63.2  | 9.933E-06 | 7.361E-06 | 7.361E-06 |
| G | 0.4  | 0.04 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 1.519E-03 | 8.550E-04 | 8.550E-04 |
| G | 1.0  | 1.69 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 5.172E-04 | 2.911E-04 | 2.911E-04 |
| G | 1.5  | 1.11 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 3.503E-04 | 1.971E-04 | 1.971E-04 |
| G | 2.0  | 0.48 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 2.666E-04 | 1.500E-04 | 1.500E-04 |
| G | 3.0  | 0.37 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 1.782E-04 | 1.003E-04 | 1.003E-04 |
| G | 4.0  | 0.03 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 1.342E-04 | 7.549E-05 | 7.549E-05 |
| G | 5.0  | 0.01 | 1810. | 0. | 0. | 43.6  | 13.7 | 43.6  | 1.076E-04 | 6.053E-05 | 6.053E-05 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

LOW POPULATION ZONE CALCULATIONS:

DIRECTION-INDEPENDENT (S.R.P 2.3.4) MODEL.

MINIMUM BOUNDARY DISTANCE = 1810.0 METERS.

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 8.550E-04 | 5.061E-04 | 2.911E-04 | 2.653E-04 | 1.971E-04 | 1.723E-04 | 1.500E-04 | 1.167E-04 | 1.003E-04 | 9.030E-05 |
| 0.043     | 0.089     | 1.781     | 1.788     | 2.897     | 5.001     | 5.484     | 8.246     | 8.619     | 10.265    |
| 0.04345   | 0.08918   | 1.78139   | 1.78825   | 2.89732   | 5.00114   | 5.48365   | 8.24606   | 8.61880   | 10.26526  |
| 8.879E-05 | 7.549E-05 | 6.115E-05 | 6.053E-05 | 5.937E-05 | 4.657E-05 | 4.654E-05 | 4.469E-05 | 3.583E-05 | 3.154E-05 |
| 12.337    | 12.367    | 16.325    | 16.332    | 18.230    | 18.649    | 23.499    | 23.988    | 24.144    | 25.996    |
| 12.33707  | 12.36680  | 16.32518  | 16.33204  | 18.23005  | 18.64853  | 23.49874  | 23.98811  | 24.14361  | 25.99589  |
| 3.112E-05 | 2.992E-05 | 2.400E-05 | 2.342E-05 | 2.248E-05 | 1.878E-05 | 1.807E-05 | 1.605E-05 | 1.568E-05 | 1.558E-05 |
| 35.559    | 35.582    | 38.779    | 46.012    | 46.019    | 50.734    | 50.762    | 59.010    | 61.729    | 61.738    |
| 35.55911  | 35.58198  | 38.77887  | 46.01189  | 46.01875  | 50.73405  | 50.76149  | 59.00983  | 61.72879  | 61.73794  |
| 1.208E-05 | 1.178E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 | 7.361E-06 | 6.076E-06 | 6.008E-06 |
| 68.976    | 71.306    | 71.434    | 77.448    | 78.061    | 82.214    | 82.717    | 82.758    | 86.193    | 86.197    |
| 68.97553  | 71.30574  | 71.43380  | 77.44798  | 78.06084  | 82.21358  | 82.71667  | 82.75784  | 86.19255  | 86.19712  |
| 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 |
| 87.491    | 88.358    | 88.427    | 89.618    | 89.822    | 90.704    | 90.970    | 91.464    | 92.465    | 92.820    |
| 87.49142  | 88.35811  | 88.42671  | 89.61811  | 89.82163  | 90.70432  | 90.96959  | 91.46353  | 92.46513  | 92.81958  |
| 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.656E-07 | 6.465E-07 | 6.303E-07 | 4.919E-07 |
| 92.966    | 93.014    | 93.888    | 94.583    | 94.987    | 95.241    | 95.264    | 95.298    | 95.335    | 95.593    |
| 92.96593  | 93.01395  | 93.88750  | 94.58267  | 94.98743  | 95.24126  | 95.26412  | 95.29842  | 95.33501  | 95.59342  |
| 3.289E-07 | 2.567E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 | 1.001E-07 | 4.079E-08 |           |           |
| 96.789    | 96.799    | 98.038    | 99.097    | 99.607    | 99.945    | 99.973    | 100.000   |           |           |
| 96.78940  | 96.79855  | 98.03797  | 99.09674  | 99.60669  | 99.94513  | 99.97257  | 100.00000 |           |           |

X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED  
 CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
 SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

ERROR IN NORMAL TRANSFORMATION FOR A( 68)= 100.00000

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 4.997

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 12.335

|           |        |        |
|-----------|--------|--------|
| 3.546E-04 | 1.000  | 1.000  |
| 2.260E-04 | 3.000  | 3.000  |
| 1.723E-04 | 5.000  | 5.000  |
| 1.050E-04 | 10.000 | 10.000 |
| 7.411E-05 | 15.000 | 15.000 |
| 5.552E-05 | 20.000 | 20.000 |
| 4.413E-05 | 25.000 | 25.000 |
| 3.740E-05 | 30.000 | 30.000 |
| 3.207E-05 | 35.000 | 35.000 |
| 2.773E-05 | 40.000 | 40.000 |
| 2.409E-05 | 45.000 | 45.000 |
| 2.118E-05 | 50.000 | 50.000 |
| 1.866E-05 | 55.000 | 55.000 |
| 1.641E-05 | 60.000 | 60.000 |
| 1.433E-05 | 65.000 | 65.000 |
| 1.240E-05 | 70.000 | 70.000 |
| 1.061E-05 | 75.000 | 75.000 |
| 8.921E-06 | 80.000 | 80.000 |
| 6.820E-06 | 85.000 | 85.000 |
| 4.446E-06 | 90.000 | 90.000 |
| 1.723E-04 | 5.0    | 5.00   |

K= 17 FIVEXQ(K)= 1.723E-04 FIVEPR(K)= 5.000

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

# LOW POPULATION ZONE CALCULATIONS:

## FIVE PERCENT OVERALL SITE LIMIT

BUILDING WAKE CREDIT ALLOWED: C= 0.5 A= 2917. D= 60.7

CORRECTION FACTORS USED IN THE ANNUAL AVERAGE CALCULATIONS.

BELOW ARE PRINTED THE ORDERED VALUES OF CHI/Q AND THE FREQUENCY WITH WHICH THAT VALUE IS REACHED OR EXCEEDED.  
THE TOP NUMBER IS THE CHI/Q. THE MIDDLE NUMBER IS THE FREQUENCY NORMALIZED TO THIS SECTOR.  
THE THIRD NUMBER IS THE FREQUENCY WITH RESPECT TO ALL TIME.

|           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 4.480E-04 | 2.804E-04 | 1.568E-04 | 1.525E-04 | 1.033E-04 | 9.546E-05 | 8.860E-05 | 7.859E-05 | 7.549E-05 | 6.465E-05 |
| 0.043     | 0.089     | 0.096     | 1.788     | 2.897     | 5.001     | 5.374     | 5.856     | 5.886     | 8.649     |
| 0.04345   | 0.08918   | 0.09604   | 1.78825   | 2.89732   | 5.00114   | 5.37389   | 5.85639   | 5.88612   | 8.64852   |
| 6.053E-05 | 5.339E-05 | 4.920E-05 | 4.786E-05 | 4.469E-05 | 3.616E-05 | 3.583E-05 | 3.389E-05 | 2.992E-05 | 2.752E-05 |
| 8.655     | 10.302    | 12.374    | 14.272    | 14.761    | 18.719    | 18.875    | 19.293    | 19.316    | 24.166    |
| 8.65538   | 10.30185  | 12.37366  | 14.27167  | 14.76103  | 18.71941  | 18.87491  | 19.29338  | 19.31625  | 24.16647  |
| 2.430E-05 | 2.295E-05 | 2.248E-05 | 2.178E-05 | 1.878E-05 | 1.807E-05 | 1.753E-05 | 1.568E-05 | 1.558E-05 | 1.371E-05 |
| 33.730    | 35.582    | 35.589    | 42.822    | 47.537    | 47.565    | 50.761    | 53.480    | 53.490    | 61.738    |
| 33.72970  | 35.58197  | 35.58883  | 42.82185  | 47.53716  | 47.56460  | 50.76148  | 53.48045  | 53.48959  | 61.73793  |
| 1.178E-05 | 1.142E-05 | 1.055E-05 | 9.685E-06 | 9.474E-06 | 8.088E-06 | 8.029E-06 | 7.361E-06 | 6.076E-06 | 6.008E-06 |
| 64.068    | 71.306    | 71.434    | 77.448    | 78.061    | 82.214    | 82.717    | 82.758    | 86.193    | 86.197    |
| 64.06815  | 71.30573  | 71.43377  | 77.44796  | 78.06081  | 82.21355  | 82.71664  | 82.75780  | 86.19251  | 86.19709  |
| 5.368E-06 | 4.886E-06 | 4.069E-06 | 4.041E-06 | 3.858E-06 | 3.240E-06 | 3.096E-06 | 2.706E-06 | 2.070E-06 | 2.033E-06 |
| 87.491    | 88.358    | 88.427    | 89.618    | 89.822    | 90.704    | 90.970    | 91.464    | 92.465    | 92.820    |
| 87.49139  | 88.35807  | 88.42668  | 89.61810  | 89.82161  | 90.70431  | 90.96957  | 91.46352  | 92.46511  | 92.81956  |
| 1.990E-06 | 1.634E-06 | 1.558E-06 | 1.250E-06 | 1.044E-06 | 7.840E-07 | 6.656E-07 | 6.465E-07 | 6.303E-07 | 4.919E-07 |
| 92.966    | 93.014    | 93.888    | 94.583    | 94.987    | 95.241    | 95.264    | 95.298    | 95.335    | 95.593    |
| 92.96591  | 93.01394  | 93.88748  | 94.58265  | 94.98741  | 95.24124  | 95.26411  | 95.29840  | 95.33498  | 95.59338  |
| 3.289E-07 | 2.567E-07 | 2.476E-07 | 1.985E-07 | 1.658E-07 | 1.246E-07 | 1.001E-07 | 4.079E-08 |           |           |
| 96.789    | 96.799    | 98.038    | 99.097    | 99.607    | 99.945    | 99.973    | 100.000   |           |           |
| 96.78935  | 96.79850  | 98.03793  | 99.09669  | 99.60664  | 99.94508  | 99.97251  | 99.99995  |           |           |

## X/Q PERCENTILES

(BASED ON THE UPPER ENVELOPE OF THE  
ORDERED X/Q-FREQUENCY VALUES, AND AS  
PLOTTED ON A LOG-NORMAL GRAPH.)

PERCENT OF TIME CHI/Q IS EQUALED OR EXCEEDED

CHI/Q WITH RESPECT TO WHEN THE WIND BLOWS  
SEC/CUBIC METER THE TOTAL TIME INTO THIS SECTOR ONLY

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 3)= 4.997

HANDCHECK GRAPH: SLOPE LT -1.0 FOR LOW PERCENTAGES. XSAVE( 4)= 14.271

| K  | I  | XQSAVE(K,I) | XQINT(K,I)   | XQSLOP(K,I) |
|----|----|-------------|--------------|-------------|
| 18 | 1  | -7.71082    | -10.62810    | -0.87604    |
| 18 | 2  | -8.78838    | -10.95057    | -1.02960    |
| 18 | 3  | -9.25677    | -11.22605    | -1.19705    |
| 18 | 4  | -9.94734    | -11.06343    | -1.04482    |
| 18 | 5  | -10.62522   | -10.81734    | -0.45808    |
| 18 | 6  | -10.73463   | -10.89166    | -0.86968    |
| 18 | 7  | -11.38039   | -10.89735    | -0.85955    |
| 18 | 8  | -11.54497   | -10.79936    | -0.98961    |
| 18 | 9  | -11.73251   | -10.08712    | -1.74494    |
| 18 | 10 | -16.11664   | NUMXQ(K)= 10 |             |
|    |    | 1.860E-04   | 1.000        | 1.000       |
|    |    | 1.217E-04   | 3.000        | 3.000       |
|    |    | 9.547E-05   | 5.000        | 5.000       |
|    |    | 6.179E-05   | 10.000       | 10.000      |
|    |    | 4.629E-05   | 15.000       | 15.000      |
|    |    | 3.776E-05   | 20.000       | 20.000      |
|    |    | 3.171E-05   | 25.000       | 25.000      |
|    |    | 2.710E-05   | 30.000       | 30.000      |
|    |    | 2.391E-05   | 35.000       | 35.000      |
|    |    | 2.251E-05   | 40.000       | 40.000      |
|    |    | 2.076E-05   | 45.000       | 45.000      |
|    |    | 1.861E-05   | 50.000       | 50.000      |
|    |    | 1.669E-05   | 55.000       | 55.000      |
|    |    | 1.494E-05   | 60.000       | 60.000      |
|    |    | 1.332E-05   | 65.000       | 65.000      |
|    |    | 1.180E-05   | 70.000       | 70.000      |
|    |    | 1.037E-05   | 75.000       | 75.000      |
|    |    | 8.877E-06   | 80.000       | 80.000      |
|    |    | 6.820E-06   | 85.000       | 85.000      |
|    |    | 4.445E-06   | 90.000       | 90.000      |
|    |    | 9.547E-05   | 5.0          | 5.00        |

K= 18 FIVEXQ(K)= 9.547E-05 FIVEPR(K)= 5.000

| K | HIGHPR   | PR      | GRNDVT(K) |
|---|----------|---------|-----------|
| 1 | -2.82155 | 0.23897 | 4.22800   |
| 2 | -1.78309 | 3.72857 | 5.26942   |
| 3 | -2.79697 | 0.25793 | 6.10231   |
| 4 | -2.67453 | 0.37417 | 5.98233   |
| 5 | -2.57624 | 0.49942 | 5.25961   |
| 6 | -2.80156 | 0.25429 | 4.65728   |

|    |          |         |         |
|----|----------|---------|---------|
| 7  | -2.99512 | 0.13717 | 4.98165 |
| 8  | -3.11882 | 0.09080 | 6.51959 |
| 9  | -3.20989 | 0.06640 | 6.53955 |
| 10 | -3.21065 | 0.06622 | 7.74017 |
| 11 | -3.13149 | 0.08697 | 5.87912 |
| 12 | -2.84197 | 0.22418 | 7.24032 |
| 13 | -2.78209 | 0.27006 | 8.51913 |
| 14 | -2.63026 | 0.42660 | 9.11977 |
| 15 | -2.69806 | 0.34873 | 6.29520 |
| 16 | -2.78093 | 0.27102 | 5.66654 |

|    |           |           |
|----|-----------|-----------|
| K  | HOURS (K) | TOTHR     |
| 1  | 20.93350  | 20.93350  |
| 2  | 326.62310 | 347.55660 |
| 3  | 22.59442  | 370.15100 |
| 4  | 32.77713  | 402.92820 |
| 5  | 43.74879  | 446.67690 |
| 6  | 22.27539  | 468.95230 |
| 7  | 12.01645  | 480.96880 |
| 8  | 7.95371   | 488.92250 |
| 9  | 5.81660   | 494.73910 |
| 10 | 5.80094   | 500.54000 |
| 11 | 7.61850   | 508.15850 |
| 12 | 19.63861  | 527.79710 |
| 13 | 23.65697  | 551.45410 |
| 14 | 37.36984  | 588.82400 |
| 15 | 30.54865  | 619.37260 |
| 16 | 23.74155  | 643.11420 |

| K | FIVEXQ    | SVANN     | SLTIME  | TIMINT  | I | TIME  | XQT       |
|---|-----------|-----------|---------|---------|---|-------|-----------|
| 1 | 6.377E-05 | 5.718E-07 | -0.5622 | -9.2705 | 1 | 8.0   | -10.43961 |
|   |           |           |         |         | 2 | 16.0  | -10.82932 |
|   |           |           |         |         | 3 | 72.0  | -11.67496 |
|   |           |           |         |         | 4 | 624.0 | -12.88909 |
| 2 | 5.453E-05 | 6.058E-07 | -0.5367 | -9.4447 | 1 | 8.0   | -10.56070 |
|   |           |           |         |         | 2 | 16.0  | -10.93269 |
|   |           |           |         |         | 3 | 72.0  | -11.73988 |
|   |           |           |         |         | 4 | 624.0 | -12.89880 |
| 3 | 7.205E-05 | 7.697E-07 | -0.5413 | -9.1629 | 1 | 8.0   | -10.28857 |
|   |           |           |         |         | 2 | 16.0  | -10.66380 |
|   |           |           |         |         | 3 | 72.0  | -11.47801 |
|   |           |           |         |         | 4 | 624.0 | -12.64702 |
| 4 | 9.396E-05 | 1.021E-06 | -0.5393 | -8.8989 | 1 | 8.0   | -10.02028 |
|   |           |           |         |         | 2 | 16.0  | -10.39408 |
|   |           |           |         |         | 3 | 72.0  | -11.20518 |
|   |           |           |         |         | 4 | 624.0 | -12.36974 |
| 5 | 1.100E-04 | 1.095E-06 | -0.5498 | -8.7336 |   |       |           |



|    |           |           |         |         |   |       |           |
|----|-----------|-----------|---------|---------|---|-------|-----------|
| 6  | 8.103E-05 | 7.787E-07 | -0.5540 | -9.0367 | 1 | 8.0   | -9.87689  |
|    |           |           |         |         | 2 | 16.0  | -10.25798 |
|    |           |           |         |         | 3 | 72.0  | -11.08493 |
|    |           |           |         |         | 4 | 624.0 | -12.27222 |
| 7  | 5.921E-05 | 5.805E-07 | -0.5516 | -9.3520 | 1 | 8.0   | -10.18863 |
|    |           |           |         |         | 2 | 16.0  | -10.57260 |
|    |           |           |         |         | 3 | 72.0  | -11.40579 |
|    |           |           |         |         | 4 | 624.0 | -12.60205 |
| 8  | 4.761E-05 | 5.721E-07 | -0.5273 | -9.5870 | 1 | 8.0   | -10.49898 |
|    |           |           |         |         | 2 | 16.0  | -10.88130 |
|    |           |           |         |         | 3 | 72.0  | -11.71091 |
|    |           |           |         |         | 4 | 624.0 | -12.90202 |
| 9  | 3.895E-05 | 4.593E-07 | -0.5296 | -9.7861 | 1 | 8.0   | -10.68347 |
|    |           |           |         |         | 2 | 16.0  | -11.04896 |
|    |           |           |         |         | 3 | 72.0  | -11.84206 |
|    |           |           |         |         | 4 | 624.0 | -12.98076 |
| 10 | 4.840E-05 | 5.213E-07 | -0.5404 | -9.5614 | 1 | 8.0   | -10.88724 |
|    |           |           |         |         | 2 | 16.0  | -11.25430 |
|    |           |           |         |         | 3 | 72.0  | -12.05079 |
|    |           |           |         |         | 4 | 624.0 | -13.19437 |
| 11 | 4.344E-05 | 4.623E-07 | -0.5418 | -9.6686 | 1 | 8.0   | -10.68508 |
|    |           |           |         |         | 2 | 16.0  | -11.05963 |
|    |           |           |         |         | 3 | 72.0  | -11.87238 |
|    |           |           |         |         | 4 | 624.0 | -13.03928 |
| 12 | 8.324E-05 | 7.667E-07 | -0.5590 | -9.0063 | 1 | 8.0   | -10.79522 |
|    |           |           |         |         | 2 | 16.0  | -11.17075 |
|    |           |           |         |         | 3 | 72.0  | -11.98563 |
|    |           |           |         |         | 4 | 624.0 | -13.15560 |
| 13 | 8.583E-05 | 9.623E-07 | -0.5356 | -8.9920 | 1 | 8.0   | -10.16877 |
|    |           |           |         |         | 2 | 16.0  | -10.55625 |
|    |           |           |         |         | 3 | 72.0  | -11.39705 |
|    |           |           |         |         | 4 | 624.0 | -12.60422 |
| 14 | 1.027E-04 | 1.116E-06 | -0.5394 | -8.8095 | 1 | 8.0   | -10.10565 |
|    |           |           |         |         | 2 | 16.0  | -10.47687 |
|    |           |           |         |         | 3 | 72.0  | -11.28241 |
|    |           |           |         |         | 4 | 624.0 | -12.43896 |
| 15 | 8.847E-05 | 8.407E-07 | -0.5553 | -8.9479 | 1 | 8.0   | -9.93102  |
|    |           |           |         |         | 2 | 16.0  | -10.30487 |
|    |           |           |         |         | 3 | 72.0  | -11.11610 |
|    |           |           |         |         | 4 | 624.0 | -12.28083 |
|    |           |           |         |         | 1 | 8.0   | -10.10263 |

|    |           |           |         |         |   |       |           |
|----|-----------|-----------|---------|---------|---|-------|-----------|
|    |           |           |         |         | 2 | 16.0  | -10.48754 |
|    |           |           |         |         | 3 | 72.0  | -11.32276 |
|    |           |           |         |         | 4 | 624.0 | -12.52193 |
| 16 | 6.697E-05 | 6.650E-07 | -0.5501 | -9.2299 |   |       |           |
|    |           |           |         |         | 1 | 8.0   | -10.37375 |
|    |           |           |         |         | 2 | 16.0  | -10.75502 |
|    |           |           |         |         | 3 | 72.0  | -11.58237 |
|    |           |           |         |         | 4 | 624.0 | -12.77023 |
| 17 | 1.723E-04 | 1.116E-06 | -0.6010 | -8.2496 |   |       |           |
|    |           |           |         |         | 1 | 8.0   | -9.49940  |
|    |           |           |         |         | 2 | 16.0  | -9.91600  |
|    |           |           |         |         | 3 | 72.0  | -10.81999 |
|    |           |           |         |         | 4 | 624.0 | -12.11790 |
| 18 | 9.547E-05 | 1.116E-06 | -0.5306 | -8.8889 |   |       |           |
|    |           |           |         |         | 1 | 8.0   | -9.99224  |
|    |           |           |         |         | 2 | 16.0  | -10.36003 |
|    |           |           |         |         | 3 | 72.0  | -11.15810 |
|    |           |           |         |         | 4 | 624.0 | -12.30394 |

USNRC COMPUTER CODE-PAVAN, VERSION 2.0

RUN DATE: 04/05/09

PLANT NAME: Braidwood

METEOROLOGICAL INSTRUMENTATION

DATA PERIOD:

WIND SENSORS HEIGHT: 10.4 meters

TYPE OF RELEASE: Ground Release

DELTA-T HEIGHTS: 61.9-10.4 meters

SOURCE OF DATA:

COMMENTS: Braidwood, 94-98 met (r3), 11 ws cats, 34' wind, 30'-199' Delta T

PROGRAM: PAVAN, 10/76, 8/79 REVISION, IMPLEMENTATION OF REGULATORY GUIDE 1.145

RELATIVE CONCENTRATION (X/Q) VALUES (SEC/CUBIC METER)  
VERSUS  
AVERAGING TIME

| DOWNWIND DISTANCE |          |           |           |            |          |           |                | HOURS PER YEAR MAX               | DOWNWIND |
|-------------------|----------|-----------|-----------|------------|----------|-----------|----------------|----------------------------------|----------|
| SECTOR            | (METERS) | 0-2 HOURS | 0-8 HOURS | 8-24 HOURS | 1-4 DAYS | 4-30 DAYS | ANNUAL AVERAGE | 0-2 HR X/Q IS EXCEEDED IN SECTOR |          |
| S                 | 1810.    | 6.38E-05  | 2.93E-05  | 1.98E-05   | 8.50E-06 | 2.53E-06  | 5.72E-07       | 20.9                             | S        |
| SSW               | 1810.    | 5.45E-05  | 2.59E-05  | 1.79E-05   | 7.97E-06 | 2.50E-06  | 6.06E-07       | 326.6                            | SSW      |
| SW                | 1810.    | 7.21E-05  | 3.40E-05  | 2.34E-05   | 1.04E-05 | 3.22E-06  | 7.70E-07       | 22.6                             | SW       |
| WSW               | 1810.    | 9.40E-05  | 4.45E-05  | 3.06E-05   | 1.36E-05 | 4.25E-06  | 1.02E-06       | 32.8                             | WSW      |
| W                 | 1810.    | 1.10E-04  | 5.13E-05  | 3.51E-05   | 1.53E-05 | 4.68E-06  | 1.09E-06       | 43.7                             | W        |
| WNW               | 1810.    | 8.10E-05  | 3.76E-05  | 2.56E-05   | 1.11E-05 | 3.37E-06  | 7.79E-07       | 22.3                             | WNW      |
| NW                | 1810.    | 5.92E-05  | 2.76E-05  | 1.88E-05   | 8.20E-06 | 2.49E-06  | 5.81E-07       | 12.0                             | NW       |
| NNW               | 1810.    | 4.76E-05  | 2.29E-05  | 1.59E-05   | 7.20E-06 | 2.30E-06  | 5.72E-07       | 8.0                              | NNW      |
| N                 | 1810.    | 3.90E-05  | 1.87E-05  | 1.30E-05   | 5.84E-06 | 1.86E-06  | 4.59E-07       | 5.8                              | N        |
| NNE               | 1810.    | 4.84E-05  | 2.29E-05  | 1.57E-05   | 6.98E-06 | 2.17E-06  | 5.21E-07       | 5.8                              | NNE      |
| NE                | 1810.    | 4.34E-05  | 2.05E-05  | 1.41E-05   | 6.23E-06 | 1.93E-06  | 4.62E-07       | 7.6                              | NE       |
| ENE               | 1810.    | 8.32E-05  | 3.83E-05  | 2.60E-05   | 1.12E-05 | 3.36E-06  | 7.67E-07       | 19.6                             | ENE      |
| E                 | 1810.    | 8.58E-05  | 4.08E-05  | 2.82E-05   | 1.26E-05 | 3.96E-06  | 9.62E-07       | 23.7                             | E        |
| ESE               | 1810.    | 1.03E-04  | 4.86E-05  | 3.35E-05   | 1.49E-05 | 4.64E-06  | 1.12E-06       | 37.4                             | ESE      |
| SE                | 1810.    | 8.85E-05  | 4.10E-05  | 2.79E-05   | 1.21E-05 | 3.65E-06  | 8.41E-07       | 30.5                             | SE       |
| SSE               | 1810.    | 6.70E-05  | 3.12E-05  | 2.13E-05   | 9.33E-06 | 2.84E-06  | 6.65E-07       | 23.7                             | SSE      |
| MAX X/Q           |          | 1.10E-04  |           |            |          |           |                | TOTAL HOURS AROUND SITE: 643.1   |          |
| SRP 2.3.4         | 1810.    | 1.72E-04  | 7.49E-05  | 4.94E-05   | 2.00E-05 | 5.46E-06  | 1.12E-06       |                                  |          |
| SITE LIMIT        |          | 9.55E-05  | 4.58E-05  | 3.17E-05   | 1.43E-05 | 4.53E-06  | 1.12E-06       |                                  |          |

THE FIVE-PERCENT-FOR-THE-ENTIRE-SITE X/Q IS LIMITING.

\*\*NOTE\*\*: VALUES ON THIS PAGE ARE APPROXIMATIONS ONLY.  
CHECK THE REASONABLENESS OF THE ENVELOPES  
COMPUTED FOR THE 0-2 HOUR VALUES. FOR ANY  
FAULTY ENVELOPES, ADJUST THE ABOVE VALUES.



**ATTACHMENT 4**

**Braidwood and Byron Stations  
Measurement Uncertainty Recapture Technical Evaluation**

**Response to NRC Acceptance Review Questions**

**Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B,  
Appendix BB-1: "Byron Joint Frequency Distribution"**

## Byron

## Joint Frequency Distribution

1994-1998 (Rev. 4)

30 ft wind

250-30 ft Delta T

|       | Wind Speed<br>Category <sup>(1)</sup> | Wind Direction Category |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | Total | Calms | Total |
|-------|---------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|
|       |                                       | N                       | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW |       |       |       |
| 1 (A) | 2                                     | 1                       | 2   | 0   | 2   | 2   | 0   | 0   | 0   | 0   | 1   | 0   | 0   | 0   | 1   | 1   | 1   | 10    | 1485  |       |
|       | 3                                     | 0                       | 0   | 0   | 0   | 0   | 3   | 3   | 1   | 1   | 3   | 2   | 6   | 1   | 1   | 2   | 0   | 23    |       |       |
|       | 4                                     | 2                       | 2   | 1   | 2   | 3   | 2   | 2   | 1   | 0   | 1   | 5   | 4   | 4   | 3   | 3   | 1   | 36    |       |       |
|       | 5                                     | 18                      | 9   | 10  | 7   | 14  | 8   | 4   | 15  | 7   | 11  | 19  | 10  | 10  | 16  | 8   | 13  | 177   |       |       |
|       | 6                                     | 39                      | 21  | 11  | 9   | 25  | 14  | 7   | 21  | 8   | 12  | 20  | 9   | 14  | 30  | 28  | 18  | 286   |       |       |
|       | 7                                     | 19                      | 21  | 7   | 12  | 18  | 9   | 10  | 21  | 17  | 19  | 28  | 23  | 18  | 32  | 49  | 18  | 321   |       |       |
|       | 8                                     | 10                      | 18  | 5   | 8   | 1   | 4   | 9   | 10  | 9   | 20  | 19  | 15  | 27  | 19  | 45  | 20  | 239   |       |       |
|       | 9                                     | 14                      | 7   | 3   | 16  | 2   | 6   | 7   | 25  | 32  | 33  | 29  | 25  | 26  | 46  | 34  | 14  | 319   |       |       |
|       | 10                                    | 0                       | 2   | 0   | 6   | 0   | 0   | 0   | 5   | 10  | 13  | 7   | 3   | 10  | 4   | 2   | 1   | 63    |       |       |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 2   | 4   | 2   | 1   | 1   | 0   | 0   | 0   | 11    |       |       |
| 2 (B) | 2                                     | 0                       | 2   | 0   | 2   | 2   | 0   | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 1   | 1   | 0   | 9     | 1430  |       |
|       | 3                                     | 3                       | 3   | 0   | 1   | 3   | 3   | 2   | 1   | 2   | 1   | 0   | 1   | 1   | 1   | 2   | 4   | 28    |       |       |
|       | 4                                     | 5                       | 5   | 1   | 0   | 3   | 5   | 3   | 1   | 0   | 3   | 2   | 5   | 4   | 1   | 3   | 5   | 46    |       |       |
|       | 5                                     | 19                      | 8   | 5   | 9   | 14  | 16  | 9   | 12  | 9   | 13  | 22  | 6   | 11  | 7   | 18  | 16  | 194   |       |       |
|       | 6                                     | 22                      | 20  | 8   | 7   | 21  | 12  | 22  | 12  | 20  | 23  | 29  | 13  | 16  | 20  | 34  | 16  | 295   |       |       |
|       | 7                                     | 39                      | 20  | 9   | 4   | 15  | 13  | 15  | 20  | 12  | 21  | 31  | 25  | 28  | 27  | 42  | 22  | 343   |       |       |
|       | 8                                     | 13                      | 16  | 3   | 5   | 4   | 7   | 10  | 9   | 14  | 27  | 22  | 13  | 21  | 32  | 27  | 16  | 239   |       |       |
|       | 9                                     | 10                      | 3   | 8   | 14  | 2   | 1   | 4   | 13  | 17  | 24  | 14  | 10  | 19  | 26  | 23  | 9   | 197   |       |       |
|       | 10                                    | 2                       | 1   | 0   | 4   | 0   | 1   | 5   | 6   | 5   | 6   | 4   | 6   | 10  | 9   | 3   | 1   | 63    |       |       |
|       | 11                                    | 3                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 3   | 2   | 3   | 2   | 0   | 2   | 0   | 0   | 16    |       |       |
| 3 (C) | 2                                     | 2                       | 1   | 0   | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 5     | 2229  |       |
|       | 3                                     | 2                       | 1   | 1   | 1   | 4   | 2   | 2   | 1   | 2   | 2   | 10  | 2   | 3   | 3   | 4   | 4   | 44    |       |       |
|       | 4                                     | 6                       | 14  | 9   | 4   | 10  | 9   | 13  | 7   | 8   | 7   | 6   | 8   | 5   | 5   | 4   | 10  | 125   |       |       |
|       | 5                                     | 21                      | 10  | 13  | 12  | 49  | 25  | 33  | 12  | 23  | 41  | 36  | 19  | 25  | 29  | 44  | 25  | 417   |       |       |
|       | 6                                     | 36                      | 26  | 16  | 9   | 29  | 14  | 20  | 26  | 41  | 36  | 45  | 22  | 40  | 40  | 58  | 35  | 493   |       |       |
|       | 7                                     | 35                      | 17  | 13  | 17  | 11  | 12  | 23  | 31  | 33  | 38  | 48  | 33  | 27  | 45  | 47  | 34  | 464   |       |       |
|       | 8                                     | 18                      | 12  | 10  | 7   | 5   | 2   | 10  | 25  | 22  | 28  | 28  | 13  | 27  | 41  | 44  | 16  | 308   |       |       |
|       | 9                                     | 12                      | 9   | 4   | 10  | 2   | 3   | 5   | 8   | 28  | 30  | 19  | 23  | 33  | 43  | 33  | 14  | 276   |       |       |
|       | 10                                    | 2                       | 2   | 2   | 1   | 0   | 2   | 5   | 2   | 7   | 7   | 4   | 7   | 10  | 17  | 5   | 0   | 73    |       |       |
|       | 11                                    | 2                       | 0   | 0   | 0   | 0   | 0   | 0   | 5   | 0   | 3   | 4   | 4   | 3   | 2   | 0   | 1   | 24    |       |       |
| 4 (D) | 2                                     | 18                      | 25  | 16  | 17  | 22  | 13  | 18  | 6   | 10  | 16  | 21  | 29  | 26  | 32  | 26  | 15  | 310   | 20380 |       |
|       | 3                                     | 32                      | 40  | 52  | 45  | 59  | 49  | 38  | 34  | 33  | 33  | 49  | 50  | 46  | 64  | 58  | 65  | 747   |       |       |
|       | 4                                     | 109                     | 85  | 72  | 53  | 107 | 79  | 47  | 48  | 64  | 68  | 74  | 75  | 82  | 107 | 98  | 95  | 1263  |       |       |
|       | 5                                     | 271                     | 186 | 165 | 158 | 294 | 162 | 164 | 184 | 227 | 225 | 264 | 212 | 241 | 312 | 364 | 303 | 3732  |       |       |
|       | 6                                     | 327                     | 175 | 136 | 188 | 223 | 120 | 159 | 225 | 255 | 205 | 242 | 221 | 285 | 359 | 388 | 287 | 3795  |       |       |
|       | 7                                     | 372                     | 211 | 141 | 272 | 171 | 115 | 152 | 227 | 215 | 190 | 243 | 227 | 328 | 371 | 299 | 272 | 3806  |       |       |
|       | 8                                     | 220                     | 133 | 121 | 191 | 71  | 62  | 77  | 164 | 196 | 156 | 164 | 154 | 253 | 314 | 205 | 127 | 2608  |       |       |
|       | 9                                     | 197                     | 185 | 217 | 232 | 35  | 79  | 84  | 202 | 188 | 221 | 153 | 191 | 403 | 318 | 142 | 103 | 2950  |       |       |
|       | 10                                    | 40                      | 36  | 85  | 37  | 1   | 30  | 27  | 56  | 58  | 76  | 39  | 81  | 142 | 136 | 22  | 17  | 883   |       |       |
|       | 11                                    | 16                      | 4   | 16  | 0   | 0   | 7   | 1   | 21  | 2   | 14  | 27  | 44  | 98  | 32  | 0   | 0   | 282   |       |       |
| 5 (E) | 2                                     | 30                      | 27  | 30  | 27  | 37  | 20  | 27  | 27  | 28  | 35  | 43  | 44  | 62  | 65  | 73  | 44  | 619   | 11763 |       |
|       | 3                                     | 50                      | 34  | 31  | 43  | 94  | 47  | 44  | 42  | 60  | 71  | 95  | 75  | 104 | 103 | 105 | 57  | 1055  |       |       |
|       | 4                                     | 45                      | 50  | 30  | 43  | 154 | 81  | 50  | 55  | 90  | 90  | 123 | 108 | 98  | 116 | 185 | 87  | 1405  |       |       |
|       | 5                                     | 152                     | 122 | 86  | 128 | 329 | 171 | 201 | 221 | 257 | 208 | 216 | 180 | 251 | 218 | 192 | 199 | 3131  |       |       |
|       | 6                                     | 120                     | 87  | 91  | 137 | 149 | 109 | 169 | 245 | 242 | 172 | 174 | 147 | 189 | 128 | 130 | 99  | 2388  |       |       |
|       | 7                                     | 46                      | 28  | 51  | 110 | 40  | 71  | 113 | 190 | 219 | 159 | 132 | 103 | 154 | 65  | 44  | 30  | 1555  |       |       |
|       | 8                                     | 14                      | 10  | 37  | 62  | 16  | 35  | 51  | 134 | 138 | 148 | 54  | 31  | 51  | 20  | 11  | 9   | 821   |       |       |
|       | 9                                     | 6                       | 4   | 8   | 36  | 7   | 39  | 24  | 105 | 143 | 142 | 44  | 21  | 38  | 8   | 3   | 5   | 633   |       |       |
|       | 10                                    | 0                       | 0   | 0   | 1   | 0   | 16  | 10  | 17  | 20  | 49  | 6   | 2   | 8   | 1   | 0   | 0   | 130   |       |       |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 6   | 1   | 6   | 1   | 1   | 0   | 0   | 0   | 4   | 0   | 0   | 19    |       |       |
| 6 (F) | 2                                     | 24                      | 21  | 18  | 9   | 15  | 14  | 10  | 21  | 21  | 30  | 46  | 54  | 70  | 89  | 95  | 39  | 576   | 4539  |       |
|       | 3                                     | 31                      | 12  | 7   | 11  | 54  | 34  | 30  | 42  | 66  | 73  | 66  | 69  | 113 | 78  | 126 | 64  | 876   |       |       |
|       | 4                                     | 20                      | 19  | 9   | 13  | 102 | 63  | 44  | 53  | 96  | 102 | 51  | 50  | 63  | 25  | 66  | 64  | 840   |       |       |
|       | 5                                     | 39                      | 32  | 14  | 26  | 116 | 160 | 212 | 275 | 234 | 86  | 43  | 16  | 37  | 18  | 15  | 42  | 1365  |       |       |
|       | 6                                     | 15                      | 6   | 4   | 22  | 22  | 97  | 107 | 200 | 116 | 38  | 3   | 6   | 3   | 1   | 0   | 0   | 640   |       |       |
|       | 7                                     | 1                       | 1   | 0   | 8   | 1   | 20  | 20  | 100 | 41  | 4   | 2   | 2   | 2   | 0   | 0   | 0   | 202   |       |       |
|       | 8                                     | 0                       | 0   | 0   | 0   | 0   | 2   | 1   | 12  | 12  | 1   | 0   | 1   | 0   | 0   | 0   | 0   | 29    |       |       |
|       | 9                                     | 0                       | 0   | 0   | 1   | 0   | 0   | 0   | 4   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 6     |       |       |
|       | 10                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0     |       |       |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0     |       |       |

|       |    |    |   |   |    |    |    |    |    |    |    |    |    |    |    |     |    |     |
|-------|----|----|---|---|----|----|----|----|----|----|----|----|----|----|----|-----|----|-----|
| 7 (G) | 2  | 25 | 9 | 8 | 15 | 17 | 10 | 11 | 15 | 25 | 43 | 50 | 52 | 73 | 94 | 110 | 68 | 625 |
|       | 3  | 7  | 3 | 2 | 8  | 29 | 30 | 14 | 35 | 54 | 42 | 27 | 30 | 39 | 23 | 78  | 48 | 469 |
|       | 4  | 5  | 1 | 1 | 3  | 35 | 28 | 17 | 19 | 69 | 34 | 6  | 4  | 9  | 6  | 13  | 10 | 260 |
|       | 5  | 9  | 1 | 0 | 2  | 30 | 54 | 62 | 60 | 83 | 7  | 1  | 2  | 2  | 1  | 0   | 0  | 314 |
|       | 6  | 1  | 0 | 0 | 3  | 6  | 31 | 30 | 32 | 18 | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 121 |
|       | 7  | 0  | 0 | 0 | 2  | 0  | 3  | 5  | 14 | 3  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 27  |
|       | 8  | 0  | 0 | 0 | 0  | 1  | 0  | 0  | 1  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 2   |
|       | 9  | 0  | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0   |
|       | 10 | 0  | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0   |
|       | 11 | 0  | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0   |

11

1829  
43655

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

## Byron

## Joint Frequency Distribution

1994-1998 (Rev. 4)

30 ft wind

250-30 ft Delta T

|                                    |       | Wind Direction Category |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | Total   | Calms    | Total   |
|------------------------------------|-------|-------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|
| Wind Speed Category <sup>(1)</sup> |       | 1                       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10      | 11      | 12      | 13      | 14      | 15      | 16      |         |          |         |
| 1 (A)                              | 2     | 0.00229                 | 0.00458 | 0.00000 | 0.00458 | 0.00458 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00229 | 0.00229 | 0.00229  | 0.00000 |
|                                    | 3     | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00687 | 0.00687 | 0.00229 | 0.00229 | 0.00687 | 0.00458 | 0.01374 | 0.00229 | 0.00229 | 0.00458 | 0.00000 | 0.05269 |          |         |
|                                    | 4     | 0.00458                 | 0.00458 | 0.00229 | 0.00458 | 0.00687 | 0.00458 | 0.00458 | 0.00229 | 0.00000 | 0.00229 | 0.01145 | 0.00916 | 0.00916 | 0.00687 | 0.00687 | 0.00229 | 0.08246 |          |         |
|                                    | 5     | 0.03665                 | 0.02062 | 0.02291 | 0.01603 | 0.03207 | 0.01833 | 0.00916 | 0.03436 | 0.01603 | 0.02520 | 0.04352 | 0.02291 | 0.02291 | 0.03665 | 0.01833 | 0.02978 | 0.40545 |          |         |
|                                    | 6     | 0.08934                 | 0.04810 | 0.02520 | 0.02062 | 0.05727 | 0.03207 | 0.01603 | 0.04810 | 0.01833 | 0.02749 | 0.04581 | 0.02062 | 0.03207 | 0.06872 | 0.06414 | 0.04123 | 0.65514 |          |         |
|                                    | 7     | 0.04352                 | 0.04810 | 0.01603 | 0.02749 | 0.04123 | 0.02062 | 0.02291 | 0.04810 | 0.03894 | 0.04352 | 0.06414 | 0.05269 | 0.04123 | 0.07330 | 0.11224 | 0.04123 | 0.73531 |          |         |
|                                    | 8     | 0.02291                 | 0.04123 | 0.01145 | 0.01833 | 0.00229 | 0.00916 | 0.02062 | 0.02291 | 0.02062 | 0.04581 | 0.04352 | 0.03436 | 0.06185 | 0.04352 | 0.10308 | 0.04581 | 0.54747 |          |         |
|                                    | 9     | 0.03207                 | 0.01603 | 0.00687 | 0.03665 | 0.00458 | 0.01374 | 0.01603 | 0.05727 | 0.07330 | 0.07559 | 0.06643 | 0.05727 | 0.05956 | 0.10537 | 0.07788 | 0.03207 | 0.73073 |          |         |
|                                    | 10    | 0.00000                 | 0.00458 | 0.00000 | 0.01374 | 0.00000 | 0.00000 | 0.00000 | 0.01145 | 0.02291 | 0.02978 | 0.01603 | 0.00687 | 0.02291 | 0.00916 | 0.00458 | 0.00229 | 0.14431 |          |         |
|                                    | 11    | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00458 | 0.00916 | 0.00458 | 0.00229 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.02520 | 3.401672 |         |
|                                    | 2 (B) | 2                       | 0.00000 | 0.00458 | 0.00000 | 0.00458 | 0.00458 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00229 | 0.00000 | 0.02062  | 0.00000 |
| 3                                  |       | 0.00687                 | 0.00687 | 0.00000 | 0.00229 | 0.00687 | 0.00687 | 0.00458 | 0.00229 | 0.00458 | 0.00229 | 0.00000 | 0.00229 | 0.00229 | 0.00229 | 0.00458 | 0.00916 | 0.06414 |          |         |
| 4                                  |       | 0.01145                 | 0.01145 | 0.00229 | 0.00000 | 0.00687 | 0.01145 | 0.00687 | 0.00229 | 0.00000 | 0.00687 | 0.00458 | 0.01145 | 0.00916 | 0.00229 | 0.00687 | 0.01145 | 0.10537 |          |         |
| 5                                  |       | 0.04352                 | 0.01833 | 0.01145 | 0.02062 | 0.03207 | 0.03665 | 0.02062 | 0.02749 | 0.02062 | 0.02978 | 0.05040 | 0.01374 | 0.02520 | 0.01603 | 0.04123 | 0.03665 | 0.44439 |          |         |
| 6                                  |       | 0.05040                 | 0.04581 | 0.01833 | 0.01603 | 0.04810 | 0.02749 | 0.05040 | 0.02749 | 0.04581 | 0.05269 | 0.06643 | 0.02978 | 0.03665 | 0.04581 | 0.07788 | 0.03665 | 0.67575 |          |         |
| 7                                  |       | 0.08934                 | 0.04581 | 0.02062 | 0.00916 | 0.03436 | 0.02978 | 0.03436 | 0.04581 | 0.02749 | 0.04810 | 0.07101 | 0.05727 | 0.06414 | 0.06185 | 0.09621 | 0.05040 | 0.78571 |          |         |
| 8                                  |       | 0.02978                 | 0.03665 | 0.00687 | 0.01145 | 0.00916 | 0.01603 | 0.02291 | 0.02062 | 0.03207 | 0.06185 | 0.05040 | 0.02978 | 0.04810 | 0.07330 | 0.06185 | 0.03665 | 0.54747 |          |         |
| 9                                  |       | 0.02291                 | 0.00687 | 0.01833 | 0.03207 | 0.00458 | 0.00229 | 0.00916 | 0.02978 | 0.03894 | 0.05498 | 0.03207 | 0.02291 | 0.04352 | 0.05956 | 0.05269 | 0.02062 | 0.45127 |          |         |
| 10                                 |       | 0.00458                 | 0.00229 | 0.00000 | 0.00916 | 0.00000 | 0.00229 | 0.01145 | 0.01374 | 0.01145 | 0.01374 | 0.00916 | 0.01374 | 0.02291 | 0.02062 | 0.00687 | 0.00229 | 0.14431 |          |         |
| 11                                 |       | 0.00687                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00687 | 0.00458 | 0.00687 | 0.00458 | 0.00000 | 0.00458 | 0.00000 | 0.00000 | 0.03665 | 3.275684 |         |
| 3 (C)                              |       | 2                       | 0.00458 | 0.00229 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.01145  | 0.00000 |
|                                    | 3     | 0.00458                 | 0.00229 | 0.00229 | 0.00229 | 0.00916 | 0.00458 | 0.00458 | 0.00229 | 0.00458 | 0.00229 | 0.00229 | 0.00458 | 0.00687 | 0.00687 | 0.00916 | 0.00916 | 0.10079 |          |         |
|                                    | 4     | 0.01374                 | 0.03207 | 0.02062 | 0.00916 | 0.02291 | 0.02062 | 0.02978 | 0.01603 | 0.01833 | 0.01603 | 0.01374 | 0.01833 | 0.01145 | 0.01145 | 0.00916 | 0.02291 | 0.28634 |          |         |
|                                    | 5     | 0.04810                 | 0.02291 | 0.02978 | 0.02749 | 0.05727 | 0.07559 | 0.02749 | 0.05269 | 0.09392 | 0.08246 | 0.04352 | 0.05727 | 0.06643 | 0.05727 | 0.06643 | 0.10079 | 0.05727 | 0.95522  |         |
|                                    | 6     | 0.08246                 | 0.05956 | 0.03665 | 0.02062 | 0.06643 | 0.03207 | 0.04581 | 0.05956 | 0.09392 | 0.08246 | 0.10308 | 0.05040 | 0.09163 | 0.09163 | 0.13286 | 0.08017 | 1.12931 |          |         |
|                                    | 7     | 0.08017                 | 0.03894 | 0.02978 | 0.03894 | 0.02520 | 0.02749 | 0.05269 | 0.07101 | 0.07559 | 0.08705 | 0.10995 | 0.07559 | 0.06185 | 0.10308 | 0.10766 | 0.07788 | 1.06288 |          |         |
|                                    | 8     | 0.04123                 | 0.02749 | 0.02291 | 0.01603 | 0.01145 | 0.00458 | 0.02291 | 0.05727 | 0.05040 | 0.06414 | 0.06414 | 0.02978 | 0.06185 | 0.09392 | 0.10079 | 0.03665 | 0.70553 |          |         |
|                                    | 9     | 0.02749                 | 0.02062 | 0.00916 | 0.02291 | 0.00458 | 0.00687 | 0.01145 | 0.01833 | 0.06414 | 0.06872 | 0.04352 | 0.05269 | 0.07559 | 0.09850 | 0.07559 | 0.03207 | 0.63223 |          |         |
|                                    | 10    | 0.00458                 | 0.00458 | 0.00458 | 0.00229 | 0.00000 | 0.00458 | 0.01145 | 0.00458 | 0.01603 | 0.01603 | 0.00916 | 0.01803 | 0.02291 | 0.03894 | 0.01145 | 0.00000 | 0.16722 |          |         |
|                                    | 11    | 0.00458                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.01145 | 0.00000 | 0.00687 | 0.00916 | 0.00916 | 0.00687 | 0.00458 | 0.00000 | 0.00229 | 0.05498 | 5.105944 |         |
|                                    | 4 (D) | 2                       | 0.04123 | 0.05727 | 0.03665 | 0.03894 | 0.05040 | 0.02978 | 0.04123 | 0.01374 | 0.02291 | 0.03665 | 0.04810 | 0.06643 | 0.05956 | 0.07330 | 0.05956 | 0.03436 | 0.71011  | 0.00916 |
| 3                                  |       | 0.07330                 | 0.09163 | 0.11912 | 0.10308 | 0.13515 | 0.11224 | 0.08705 | 0.07788 | 0.07559 | 0.07559 | 0.11224 | 0.11453 | 0.10537 | 0.14660 | 0.13286 | 0.14889 | 1.71114 |          |         |
| 4                                  |       | 0.24969                 | 0.19471 | 0.16493 | 0.12141 | 0.24510 | 0.18096 | 0.10766 | 0.10995 | 0.14660 | 0.15577 | 0.16951 | 0.17180 | 0.18784 | 0.24510 | 0.22449 | 0.21762 | 2.89314 |          |         |
| 5                                  |       | 0.62078                 | 0.42607 | 0.37796 | 0.36193 | 0.67346 | 0.37109 | 0.37567 | 0.42149 | 0.51999 | 0.51540 | 0.60474 | 0.48563 | 0.55206 | 0.71469 | 0.83381 | 0.69408 | 8.54885 |          |         |
| 6                                  |       | 0.74906                 | 0.40087 | 0.31153 | 0.43065 | 0.51082 | 0.27488 | 0.36422 | 0.51540 | 0.58413 | 0.46959 | 0.55435 | 0.50624 | 0.65285 | 0.82236 | 0.88879 | 0.65743 | 8.69316 |          |         |
| 7                                  |       | 0.85214                 | 0.48334 | 0.32299 | 0.62307 | 0.39171 | 0.28343 | 0.34818 | 0.51999 | 0.49250 | 0.43523 | 0.55664 | 0.51999 | 0.75135 | 0.84985 | 0.68492 | 0.62307 | 8.71836 |          |         |
| 8                                  |       | 0.50395                 | 0.30466 | 0.27717 | 0.43752 | 0.16264 | 0.14202 | 0.17638 | 0.37567 | 0.44897 | 0.35735 | 0.37567 | 0.35277 | 0.57954 | 0.71928 | 0.46959 | 0.29092 | 5.97412 |          |         |
| 9                                  |       | 0.45127                 | 0.42378 | 0.49708 | 0.53144 | 0.08017 | 0.18096 | 0.19242 | 0.46272 | 0.43065 | 0.50624 | 0.35048 | 0.43752 | 0.92315 | 0.72844 | 0.32528 | 0.23594 | 6.75753 |          |         |
| 10                                 |       | 0.09163                 | 0.08246 | 0.19471 | 0.08476 | 0.00229 | 0.06872 | 0.06185 | 0.12828 | 0.13286 | 0.17409 | 0.08934 | 0.18555 | 0.32528 | 0.31153 | 0.05040 | 0.03894 | 2.02268 |          |         |
| 11                                 |       | 0.03665                 | 0.00916 | 0.03665 | 0.00000 | 0.00000 | 0.01603 | 0.00229 | 0.04810 | 0.00458 | 0.03207 | 0.06185 | 0.10079 | 0.22449 | 0.07330 | 0.00000 | 0.00000 | 0.64597 | 46.68423 |         |
| 5 (E)                              |       | 2                       | 0.06872 | 0.06185 | 0.06872 | 0.06185 | 0.08476 | 0.04581 | 0.06185 | 0.06185 | 0.06414 | 0.08017 | 0.09850 | 0.10079 | 0.14202 | 0.14889 | 0.16722 | 0.10079 | 1.41794  | 0.01603 |
|                                    | 3     | 0.11453                 | 0.07788 | 0.07101 | 0.09850 | 0.21532 | 0.10766 | 0.10079 | 0.09621 | 0.13744 | 0.16264 | 0.21762 | 0.17180 | 0.23823 | 0.23594 | 0.24052 | 0.13057 | 2.41668 |          |         |
|                                    | 4     | 0.10308                 | 0.11453 | 0.06872 | 0.09850 | 0.35277 | 0.18555 | 0.11453 | 0.12599 | 0.20616 | 0.20616 | 0.28175 | 0.24739 | 0.22449 | 0.26572 | 0.42378 | 0.19929 | 3.21842 |          |         |
|                                    | 5     | 0.34818                 | 0.27946 | 0.19700 | 0.29321 | 0.75364 | 0.39171 | 0.46043 | 0.50624 | 0.58871 | 0.47648 | 0.49479 | 0.41232 | 0.57496 | 0.49937 | 0.43981 | 0.45585 | 7.17215 |          |         |
|                                    | 6     | 0.27488                 | 0.19929 | 0.20845 | 0.31382 | 0.34131 | 0.24969 | 0.38713 | 0.56122 | 0.55435 | 0.39400 | 0.39858 | 0.33673 | 0.43294 | 0.29321 | 0.29779 | 0.22678 | 5.47016 |          |         |
|                                    | 7     | 0.10537                 | 0.06414 | 0.11683 | 0.25198 | 0.09163 | 0.16264 | 0.25885 | 0.43523 | 0.50166 | 0.36422 | 0.30237 | 0.23594 | 0.35277 | 0.14889 | 0.10079 | 0.06872 | 3.56202 |          |         |
|                                    | 8     | 0.03207                 | 0.02291 | 0.08476 | 0.14202 | 0.03665 | 0.08017 | 0.11683 | 0.30695 | 0.31611 | 0.33902 | 0.12370 | 0.07101 | 0.11683 | 0.04581 | 0.02520 | 0.02062 | 1.88066 |          |         |
|                                    | 9     | 0.01374                 | 0.00916 | 0.01833 | 0.08246 | 0.01603 | 0.08934 | 0.05498 | 0.24052 | 0.32757 | 0.32528 | 0.10079 | 0.04810 | 0.08705 | 0.01833 | 0.00687 | 0.01145 | 1.45001 |          |         |
|                                    | 10    | 0.00000                 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.03665 | 0.02291 | 0.03894 | 0.04581 | 0.11224 | 0.01374 | 0.00    |         |         |         |         |         |          |         |



|          |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
|----------|----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 7 (G)    | 2  | 0.05727 | 0.02062 | 0.01833 | 0.03436 | 0.03894 | 0.02291 | 0.02520 | 0.03436 | 0.05727 | 0.09850 | 0.11453 | 0.11912 | 0.16722 | 0.21532 | 0.25198 | 0.15577 | 1.43168 | 0.02520 |
|          | 3  | 0.01603 | 0.00687 | 0.00458 | 0.01833 | 0.06643 | 0.06872 | 0.03207 | 0.08017 | 0.12370 | 0.09621 | 0.06185 | 0.06872 | 0.08934 | 0.05269 | 0.17867 | 0.10995 | 1.07433 |         |
|          | 4  | 0.01145 | 0.00229 | 0.00229 | 0.00687 | 0.08017 | 0.06414 | 0.03894 | 0.04352 | 0.15806 | 0.07788 | 0.01374 | 0.00916 | 0.02062 | 0.01374 | 0.02978 | 0.02291 | 0.59558 |         |
|          | 5  | 0.02062 | 0.00229 | 0.00000 | 0.00458 | 0.06872 | 0.12370 | 0.14202 | 0.13744 | 0.19013 | 0.01603 | 0.00229 | 0.00458 | 0.00458 | 0.00229 | 0.00000 | 0.00000 | 0.71928 |         |
|          | 6  | 0.00229 | 0.00000 | 0.00000 | 0.00687 | 0.01374 | 0.07101 | 0.06872 | 0.07330 | 0.04123 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.27717 |         |
|          | 7  | 0.00000 | 0.00000 | 0.00000 | 0.00458 | 0.00000 | 0.00687 | 0.01145 | 0.03207 | 0.00687 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.06185 |         |
|          | 8  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00458 |         |
|          | 9  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |         |
|          | 10 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |         |
|          | 11 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |         |
| 99.93815 |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |

4.189669

100

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

## Byron

## Joint Frequency Distribution

1994-1998 (Rev. 4)

250 ft wind

250-30 ft Delta T

|       | Wind Speed Category <sup>(1)</sup> | Wind Direction Category |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | Total | Calms | Total |
|-------|------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|
|       |                                    | N                       | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW |       |       |       |
| 1 (A) | 2                                  | 0                       | 0   | 1   | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 1   | 1   | 0   | 0   | 0   | 2   | 6     | 0     |       |
|       | 3                                  | 1                       | 1   | 1   | 0   | 1   | 1   | 2   | 1   | 1   | 0   | 1   | 3   | 1   | 0   | 0   | 1   | 15    |       |       |
|       | 4                                  | 2                       | 2   | 0   | 0   | 1   | 2   | 2   | 1   | 0   | 3   | 7   | 3   | 2   | 0   | 3   | 0   | 28    |       |       |
|       | 5                                  | 2                       | 2   | 4   | 6   | 6   | 2   | 2   | 3   | 6   | 3   | 9   | 8   | 8   | 4   | 7   | 5   | 77    |       |       |
|       | 6                                  | 22                      | 13  | 3   | 8   | 14  | 7   | 7   | 8   | 7   | 13  | 16  | 6   | 5   | 17  | 10  | 12  | 168   |       |       |
|       | 7                                  | 26                      | 19  | 13  | 4   | 20  | 4   | 6   | 20  | 7   | 13  | 12  | 14  | 11  | 23  | 20  | 14  | 226   |       |       |
|       | 8                                  | 15                      | 16  | 5   | 3   | 15  | 13  | 5   | 13  | 12  | 12  | 20  | 16  | 18  | 16  | 25  | 13  | 217   |       |       |
|       | 9                                  | 19                      | 17  | 11  | 9   | 14  | 8   | 14  | 19  | 21  | 31  | 36  | 19  | 31  | 36  | 71  | 28  | 384   |       |       |
|       | 10                                 | 7                       | 5   | 1   | 12  | 2   | 8   | 7   | 16  | 20  | 21  | 15  | 17  | 19  | 38  | 38  | 12  | 238   |       |       |
|       | 11                                 | 0                       | 2   | 0   | 8   | 2   | 2   | 2   | 11  | 21  | 18  | 17  | 7   | 13  | 11  | 11  | 1   | 126   |       | 1485  |
|       | 2 (B)                              | 2                       | 0   | 0   | 1   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 0     | 3     | 0     |
| 3     |                                    | 2                       | 1   | 1   | 0   | 2   | 3   | 3   | 2   | 1   | 0   | 0   | 1   | 2   | 1   | 0   | 1   | 20    |       |       |
| 4     |                                    | 2                       | 2   | 0   | 0   | 3   | 3   | 2   | 2   | 0   | 0   | 2   | 0   | 2   | 3   | 3   | 2   | 26    |       |       |
| 5     |                                    | 11                      | 7   | 5   | 5   | 7   | 5   | 2   | 5   | 3   | 5   | 13  | 6   | 5   | 3   | 6   | 12  | 100   |       |       |
| 6     |                                    | 16                      | 6   | 4   | 6   | 17  | 10  | 9   | 11  | 14  | 21  | 18  | 5   | 8   | 9   | 14  | 13  | 181   |       |       |
| 7     |                                    | 18                      | 16  | 8   | 2   | 14  | 10  | 18  | 15  | 8   | 13  | 16  | 11  | 14  | 13  | 25  | 12  | 213   |       |       |
| 8     |                                    | 18                      | 21  | 8   | 4   | 10  | 11  | 9   | 14  | 13  | 16  | 23  | 25  | 23  | 27  | 23  | 18  | 263   |       |       |
| 9     |                                    | 25                      | 19  | 8   | 4   | 11  | 11  | 14  | 14  | 22  | 32  | 33  | 18  | 26  | 41  | 51  | 23  | 352   |       |       |
| 10    |                                    | 7                       | 3   | 8   | 10  | 3   | 3   | 7   | 7   | 16  | 15  | 9   | 10  | 19  | 16  | 17  | 12  | 162   |       |       |
| 11    |                                    | 4                       | 1   | 0   | 9   | 0   | 4   | 5   | 7   | 13  | 9   | 8   | 9   | 16  | 15  | 8   | 2   | 110   |       | 1430  |
| 3 (C) |                                    | 2                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 0     | 1     | 0     |
|       | 3                                  | 2                       | 1   | 1   | 0   | 0   | 0   | 1   | 0   | 1   | 2   | 3   | 1   | 1   | 1   | 1   | 3   | 18    |       |       |
|       | 4                                  | 8                       | 3   | 2   | 2   | 3   | 4   | 5   | 5   | 6   | 2   | 8   | 7   | 4   | 3   | 5   | 3   | 70    |       |       |
|       | 5                                  | 13                      | 4   | 17  | 9   | 20  | 28  | 25  | 12  | 14  | 22  | 17  | 12  | 8   | 15  | 18  | 15  | 249   |       |       |
|       | 6                                  | 17                      | 11  | 8   | 9   | 33  | 14  | 7   | 15  | 23  | 29  | 26  | 11  | 32  | 33  | 29  | 22  | 319   |       |       |
|       | 7                                  | 27                      | 27  | 11  | 6   | 19  | 8   | 16  | 23  | 25  | 30  | 40  | 19  | 18  | 34  | 42  | 26  | 371   |       |       |
|       | 8                                  | 21                      | 16  | 5   | 8   | 15  | 5   | 19  | 14  | 30  | 22  | 26  | 29  | 19  | 32  | 42  | 22  | 325   |       |       |
|       | 9                                  | 23                      | 20  | 14  | 13  | 12  | 12  | 20  | 33  | 28  | 42  | 46  | 24  | 39  | 66  | 62  | 34  | 488   |       |       |
|       | 10                                 | 11                      | 8   | 7   | 8   | 4   | 3   | 3   | 10  | 22  | 24  | 20  | 19  | 17  | 30  | 22  | 9   | 217   |       |       |
|       | 11                                 | 3                       | 2   | 3   | 2   | 1   | 5   | 9   | 10  | 14  | 12  | 14  | 16  | 17  | 31  | 16  | 7   | 162   |       | 2220  |
|       | 4 (D)                              | 2                       | 6   | 10  | 9   | 9   | 4   | 3   | 3   | 6   | 9   | 6   | 6   | 9   | 7   | 12  | 10  | 2     | 111   | 2     |
| 3     |                                    | 25                      | 16  | 22  | 26  | 29  | 17  | 20  | 9   | 20  | 21  | 16  | 19  | 25  | 29  | 19  | 27  | 340   |       |       |
| 4     |                                    | 38                      | 32  | 33  | 31  | 44  | 30  | 34  | 21  | 24  | 31  | 34  | 47  | 43  | 30  | 48  | 51  | 571   |       |       |
| 5     |                                    | 136                     | 104 | 87  | 101 | 137 | 92  | 76  | 80  | 103 | 107 | 122 | 108 | 128 | 146 | 143 | 142 | 1812  |       |       |
| 6     |                                    | 166                     | 133 | 99  | 84  | 178 | 99  | 87  | 110 | 119 | 128 | 148 | 158 | 168 | 174 | 210 | 152 | 2213  |       |       |
| 7     |                                    | 206                     | 163 | 82  | 119 | 175 | 98  | 75  | 127 | 155 | 168 | 167 | 150 | 189 | 233 | 278 | 236 | 2621  |       |       |
| 8     |                                    | 192                     | 182 | 91  | 120 | 169 | 74  | 64  | 100 | 131 | 133 | 141 | 186 | 232 | 273 | 265 | 195 | 2548  |       |       |
| 9     |                                    | 408                     | 286 | 166 | 283 | 269 | 135 | 151 | 244 | 283 | 248 | 289 | 301 | 459 | 523 | 417 | 299 | 4741  |       |       |
| 10    |                                    | 180                     | 157 | 160 | 173 | 108 | 85  | 129 | 171 | 199 | 202 | 194 | 174 | 324 | 304 | 184 | 130 | 2874  |       |       |
| 11    |                                    | 99                      | 134 | 192 | 154 | 57  | 94  | 122 | 239 | 178 | 197 | 173 | 147 | 310 | 251 | 73  | 28  | 2448  |       | 20281 |
| 5 (E) |                                    | 2                       | 5   | 3   | 6   | 5   | 7   | 5   | 1   | 3   | 2   | 3   | 7   | 10  | 8   | 12  | 10  | 1     | 88    | 2     |
|       | 3                                  | 6                       | 14  | 25  | 15  | 21  | 8   | 8   | 5   | 8   | 8   | 9   | 3   | 7   | 8   | 13  | 14  | 172   |       |       |
|       | 4                                  | 19                      | 15  | 15  | 9   | 26  | 10  | 16  | 10  | 14  | 8   | 6   | 9   | 7   | 11  | 20  | 18  | 213   |       |       |
|       | 5                                  | 43                      | 35  | 37  | 54  | 89  | 37  | 27  | 33  | 19  | 28  | 39  | 43  | 41  | 37  | 38  | 52  | 652   |       |       |
|       | 6                                  | 55                      | 40  | 53  | 66  | 125 | 54  | 46  | 34  | 37  | 67  | 75  | 60  | 67  | 96  | 83  | 67  | 1025  |       |       |
|       | 7                                  | 71                      | 55  | 61  | 56  | 166 | 58  | 52  | 42  | 86  | 80  | 111 | 108 | 118 | 162 | 169 | 105 | 1500  |       |       |
|       | 8                                  | 107                     | 59  | 52  | 73  | 140 | 68  | 71  | 58  | 86  | 107 | 131 | 145 | 169 | 158 | 191 | 125 | 1740  |       |       |
|       | 9                                  | 126                     | 147 | 105 | 153 | 167 | 143 | 163 | 186 | 266 | 338 | 313 | 241 | 363 | 247 | 254 | 168 | 3380  |       |       |
|       | 10                                 | 31                      | 28  | 34  | 90  | 57  | 119 | 152 | 199 | 260 | 319 | 223 | 99  | 85  | 59  | 32  | 23  | 1810  |       |       |
|       | 11                                 | 1                       | 2   | 6   | 20  | 11  | 95  | 91  | 228 | 239 | 275 | 95  | 16  | 32  | 8   | 4   | 1   | 1124  |       | 11706 |
|       | 6 (F)                              | 2                       | 1   | 1   | 1   | 5   | 4   | 5   | 3   | 4   | 0   | 0   | 2   | 2   | 5   | 2   | 2   | 3     | 40    | 1     |
| 3     |                                    | 4                       | 4   | 6   | 7   | 9   | 4   | 1   | 4   | 2   | 3   | 3   | 8   | 1   | 6   | 2   | 9   | 73    |       |       |
| 4     |                                    | 6                       | 3   | 8   | 6   | 7   | 6   | 1   | 8   | 6   | 5   | 5   | 4   | 11  | 4   | 5   | 7   | 92    |       |       |
| 5     |                                    | 19                      | 16  | 19  | 22  | 26  | 14  | 16  | 12  | 19  | 14  | 8   | 15  | 17  | 22  | 20  | 20  | 279   |       |       |
| 6     |                                    | 40                      | 24  | 20  | 13  | 31  | 26  | 23  | 24  | 31  | 21  | 23  | 27  | 18  | 31  | 28  | 28  | 408   |       |       |
| 7     |                                    | 36                      | 18  | 11  | 17  | 49  | 20  | 24  | 35  | 38  | 40  | 37  | 35  | 46  | 75  | 68  | 49  | 598   |       |       |
| 8     |                                    | 29                      | 29  | 30  | 10  | 44  | 23  | 41  | 36  | 52  | 52  | 71  | 44  | 58  | 80  | 63  | 60  | 722   |       |       |
| 9     |                                    | 53                      | 49  | 28  | 15  | 37  | 82  | 133 | 90  | 173 | 163 | 145 | 75  | 61  | 63  | 68  | 72  | 1307  |       |       |
| 10    |                                    | 5                       | 7   | 1   | 5   | 11  | 94  | 113 | 132 | 181 | 154 | 37  | 10  | 3   | 2   | 2   | 3   | 760   |       |       |
| 11    |                                    | 0                       | 0   | 0   | 0   | 0   | 25  | 33  | 74  | 90  | 17  | 1   | 2   | 0   | 0   | 0   | 0   | 242   |       | 4522  |

|       |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |     |
|-------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 7 (G) | 2  | 4  | 5  | 1  | 3  | 2  | 3  | 1  | 0  | 5  | 1  | 4  | 5  | 7  | 4  | 3  | 4  | 52  |
|       | 3  | 7  | 6  | 4  | 3  | 4  | 2  | 3  | 1  | 3  | 1  | 4  | 3  | 3  | 3  | 2  | 8  | 57  |
|       | 4  | 3  | 3  | 8  | 7  | 8  | 2  | 2  | 1  | 2  | 6  | 3  | 2  | 3  | 3  | 5  | 5  | 63  |
|       | 5  | 10 | 13 | 25 | 32 | 18 | 7  | 5  | 3  | 7  | 11 | 8  | 6  | 12 | 17 | 25 | 19 | 218 |
|       | 6  | 22 | 15 | 19 | 11 | 10 | 11 | 10 | 10 | 13 | 15 | 10 | 12 | 24 | 9  | 15 | 31 | 237 |
|       | 7  | 25 | 18 | 10 | 1  | 9  | 7  | 18 | 11 | 25 | 10 | 15 | 10 | 17 | 18 | 20 | 31 | 245 |
|       | 8  | 12 | 11 | 7  | 1  | 8  | 11 | 13 | 19 | 22 | 18 | 25 | 15 | 21 | 21 | 27 | 27 | 256 |
|       | 9  | 23 | 15 | 6  | 1  | 3  | 28 | 58 | 58 | 51 | 51 | 52 | 19 | 21 | 12 | 38 | 24 | 458 |
|       | 10 | 1  | 4  | 0  | 1  | 5  | 29 | 44 | 33 | 32 | 25 | 9  | 0  | 1  | 0  | 0  | 0  | 184 |
|       | 11 | 0  | 0  | 0  | 0  | 1  | 13 | 13 | 17 | 9  | 5  | 1  | 0  | 0  | 0  | 0  | 0  | 59  |

1

1830  
43474

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

## Byron

## Joint Frequency Distribution

1994-1998 (Rev. 4)

250 ft wind

250-30 ft Delta T

|       | Wind Speed<br>Category <sup>(1)</sup> | Wind Direction Category |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | Total    | Calms   | Total   |
|-------|---------------------------------------|-------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|---------|
|       |                                       | 1                       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10      | 11      | 12      | 13      | 14      | 15      | 16      |          |         |         |
| 1 (A) | 2                                     | 0.00000                 | 0.00000 | 0.00230 | 0.00000 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00230 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.00460 | 0.01380  | 0.00000 | 0.00000 |
|       | 3                                     | 0.00230                 | 0.00230 | 0.00230 | 0.00000 | 0.00230 | 0.00230 | 0.00460 | 0.00230 | 0.00230 | 0.00000 | 0.00000 | 0.00230 | 0.00690 | 0.00230 | 0.00000 | 0.00000 | 0.00230  | 0.03450 | 0.00000 |
|       | 4                                     | 0.00460                 | 0.00460 | 0.00000 | 0.00000 | 0.00230 | 0.00460 | 0.00460 | 0.00230 | 0.00000 | 0.00690 | 0.01610 | 0.00690 | 0.00460 | 0.00000 | 0.00690 | 0.00000 | 0.00000  | 0.06441 | 0.00000 |
|       | 5                                     | 0.00460                 | 0.00460 | 0.00920 | 0.01380 | 0.01380 | 0.00460 | 0.00460 | 0.00690 | 0.01380 | 0.00690 | 0.02070 | 0.01840 | 0.01840 | 0.00920 | 0.01610 | 0.01150 | 0.17712  | 0.00000 | 0.00000 |
|       | 6                                     | 0.05060                 | 0.02990 | 0.00690 | 0.01840 | 0.03220 | 0.01610 | 0.01610 | 0.01840 | 0.01610 | 0.02990 | 0.03680 | 0.01380 | 0.01150 | 0.03910 | 0.02300 | 0.02760 | 0.38644  | 0.00000 | 0.00000 |
|       | 7                                     | 0.05981                 | 0.04370 | 0.02990 | 0.00920 | 0.04600 | 0.00920 | 0.01380 | 0.04600 | 0.01610 | 0.02990 | 0.02760 | 0.03220 | 0.02530 | 0.05291 | 0.04600 | 0.03220 | 0.51985  | 0.00000 | 0.00000 |
|       | 8                                     | 0.03450                 | 0.03680 | 0.01150 | 0.00690 | 0.03450 | 0.02990 | 0.01150 | 0.02990 | 0.02760 | 0.02760 | 0.04600 | 0.03680 | 0.04140 | 0.03680 | 0.05751 | 0.02990 | 0.49915  | 0.00000 | 0.00000 |
|       | 9                                     | 0.04370                 | 0.03910 | 0.02530 | 0.02070 | 0.03220 | 0.01840 | 0.03220 | 0.04370 | 0.04830 | 0.07131 | 0.08281 | 0.04370 | 0.07131 | 0.08281 | 0.16332 | 0.06441 | 0.88329  | 0.00000 | 0.00000 |
|       | 10                                    | 0.01610                 | 0.01150 | 0.00230 | 0.02760 | 0.00460 | 0.01840 | 0.01610 | 0.03680 | 0.04600 | 0.04830 | 0.03450 | 0.03910 | 0.04370 | 0.08741 | 0.08741 | 0.02760 | 0.54745  | 0.00000 | 0.00000 |
|       | 11                                    | 0.00000                 | 0.00460 | 0.00000 | 0.01840 | 0.00460 | 0.00460 | 0.00460 | 0.02530 | 0.04830 | 0.04140 | 0.03910 | 0.01610 | 0.02990 | 0.02530 | 0.02530 | 0.00230 | 0.28983  | 0.00000 | 0.00000 |
|       | 2 (B)                                 | 2                       | 0.00000 | 0.00000 | 0.00230 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00230 | 0.00000  | 0.00690 | 0.00000 |
| 3     |                                       | 0.00460                 | 0.00230 | 0.00230 | 0.00000 | 0.00460 | 0.00690 | 0.00690 | 0.00460 | 0.00230 | 0.00000 | 0.00000 | 0.00230 | 0.00460 | 0.00230 | 0.00000 | 0.00230 | 0.04600  | 0.00591 | 0.00000 |
| 4     |                                       | 0.00460                 | 0.00460 | 0.00000 | 0.00000 | 0.00690 | 0.00690 | 0.00460 | 0.00460 | 0.00000 | 0.00000 | 0.00460 | 0.00000 | 0.00690 | 0.00690 | 0.00460 | 0.00690 | 0.05981  | 0.00000 | 0.00000 |
| 5     |                                       | 0.02530                 | 0.01610 | 0.01150 | 0.01150 | 0.01610 | 0.01150 | 0.00460 | 0.01150 | 0.00690 | 0.01150 | 0.02990 | 0.01380 | 0.01150 | 0.00690 | 0.01380 | 0.02760 | 0.23002  | 0.00000 | 0.00000 |
| 6     |                                       | 0.03680                 | 0.01380 | 0.00920 | 0.01380 | 0.03910 | 0.02300 | 0.02070 | 0.02530 | 0.03220 | 0.04830 | 0.04140 | 0.01150 | 0.01840 | 0.02070 | 0.03220 | 0.02990 | 0.41634  | 0.00000 | 0.00000 |
| 7     |                                       | 0.04140                 | 0.03680 | 0.01840 | 0.00460 | 0.03220 | 0.02300 | 0.04140 | 0.03450 | 0.01840 | 0.02990 | 0.03680 | 0.02530 | 0.03220 | 0.02990 | 0.05751 | 0.02760 | 0.48995  | 0.00000 | 0.00000 |
| 8     |                                       | 0.04140                 | 0.04830 | 0.01840 | 0.00920 | 0.02300 | 0.02530 | 0.02070 | 0.03220 | 0.02990 | 0.03680 | 0.05291 | 0.05751 | 0.05291 | 0.06211 | 0.05291 | 0.04140 | 0.60496  | 0.00000 | 0.00000 |
| 9     |                                       | 0.05751                 | 0.04370 | 0.01840 | 0.00920 | 0.02530 | 0.02530 | 0.03220 | 0.03220 | 0.05060 | 0.07381 | 0.07591 | 0.04140 | 0.05981 | 0.09431 | 0.11731 | 0.05291 | 0.80968  | 0.00000 | 0.00000 |
| 10    |                                       | 0.01610                 | 0.00690 | 0.01840 | 0.02300 | 0.00690 | 0.00690 | 0.01610 | 0.01610 | 0.03680 | 0.03450 | 0.02070 | 0.02300 | 0.04370 | 0.03680 | 0.03910 | 0.02760 | 0.37264  | 0.00000 | 0.00000 |
| 11    |                                       | 0.00920                 | 0.00230 | 0.00000 | 0.02070 | 0.00000 | 0.00920 | 0.01150 | 0.01610 | 0.02990 | 0.02070 | 0.01840 | 0.02070 | 0.03680 | 0.03450 | 0.01840 | 0.00460 | 0.25302  | 0.00000 | 0.00000 |
| 3 (C) |                                       | 2                       | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00230 | 0.00000  | 0.00230 | 0.00000 |
|       | 3                                     | 0.00460                 | 0.00230 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.00230 | 0.00000 | 0.00230 | 0.00460 | 0.00690 | 0.00230 | 0.00230 | 0.00230 | 0.00230 | 0.00690 | 0.04140  | 0.00000 | 0.00000 |
|       | 4                                     | 0.01840                 | 0.00690 | 0.00460 | 0.00460 | 0.00690 | 0.00920 | 0.01150 | 0.01150 | 0.01380 | 0.00460 | 0.01840 | 0.01610 | 0.00920 | 0.00690 | 0.01150 | 0.00690 | 0.16102  | 0.00000 | 0.00000 |
|       | 5                                     | 0.02990                 | 0.00920 | 0.03910 | 0.02070 | 0.04600 | 0.06441 | 0.05751 | 0.02760 | 0.03220 | 0.05060 | 0.03910 | 0.02760 | 0.01840 | 0.03450 | 0.04140 | 0.03450 | 0.57276  | 0.00000 | 0.00000 |
|       | 6                                     | 0.03910                 | 0.02530 | 0.01840 | 0.02070 | 0.07591 | 0.03220 | 0.01810 | 0.03450 | 0.05291 | 0.06671 | 0.05981 | 0.02530 | 0.07361 | 0.07591 | 0.06671 | 0.05060 | 0.73377  | 0.00000 | 0.00000 |
|       | 7                                     | 0.06211                 | 0.06211 | 0.02530 | 0.01380 | 0.04370 | 0.01840 | 0.03680 | 0.05291 | 0.05751 | 0.06901 | 0.08201 | 0.04370 | 0.04140 | 0.07821 | 0.09661 | 0.05981 | 0.85338  | 0.00000 | 0.00000 |
|       | 8                                     | 0.04830                 | 0.03680 | 0.01150 | 0.01840 | 0.03450 | 0.01150 | 0.04370 | 0.03220 | 0.06901 | 0.05060 | 0.05981 | 0.06671 | 0.04370 | 0.07381 | 0.09661 | 0.05060 | 0.74757  | 0.00000 | 0.00000 |
|       | 9                                     | 0.05291                 | 0.04600 | 0.03220 | 0.02990 | 0.02760 | 0.02760 | 0.04800 | 0.07591 | 0.06441 | 0.09661 | 0.10581 | 0.05521 | 0.08971 | 0.15181 | 0.14281 | 0.07821 | 1.12251  | 0.00000 | 0.00000 |
|       | 10                                    | 0.02530                 | 0.01840 | 0.01610 | 0.01840 | 0.00920 | 0.00690 | 0.00690 | 0.02300 | 0.05060 | 0.05521 | 0.04600 | 0.04370 | 0.03910 | 0.06901 | 0.05060 | 0.02070 | 0.49915  | 0.00000 | 0.00000 |
|       | 11                                    | 0.00690                 | 0.00460 | 0.00690 | 0.00460 | 0.00230 | 0.01150 | 0.02070 | 0.02300 | 0.03220 | 0.02760 | 0.03220 | 0.03680 | 0.03910 | 0.07131 | 0.03680 | 0.01610 | 0.37264  | 0.00000 | 0.00000 |
|       | 4 (D)                                 | 2                       | 0.01380 | 0.02300 | 0.02070 | 0.02070 | 0.00920 | 0.00690 | 0.00690 | 0.01380 | 0.02070 | 0.01380 | 0.01380 | 0.02070 | 0.01610 | 0.02760 | 0.02300 | 0.00460  | 0.25533 | 0.00460 |
| 3     |                                       | 0.05751                 | 0.03680 | 0.05060 | 0.05981 | 0.06871 | 0.03910 | 0.04600 | 0.02070 | 0.04600 | 0.04830 | 0.03680 | 0.04370 | 0.05751 | 0.06671 | 0.04370 | 0.06211 | 0.78208  | 0.00000 | 0.00000 |
| 4     |                                       | 0.08741                 | 0.07361 | 0.07591 | 0.07131 | 0.10121 | 0.06901 | 0.07821 | 0.04830 | 0.05521 | 0.07131 | 0.07821 | 0.10811 | 0.09891 | 0.06901 | 0.11041 | 0.11731 | 1.31343  | 0.00000 | 0.00000 |
| 5     |                                       | 0.31283                 | 0.23922 | 0.20012 | 0.23232 | 0.31513 | 0.21162 | 0.17482 | 0.18402 | 0.23692 | 0.24612 | 0.28063 | 0.24842 | 0.29443 | 0.33583 | 0.32893 | 0.32663 | 4.16801  | 0.00000 | 0.00000 |
| 6     |                                       | 0.38184                 | 0.30593 | 0.22772 | 0.19322 | 0.40944 | 0.22772 | 0.20012 | 0.25302 | 0.27373 | 0.29443 | 0.34043 | 0.36344 | 0.38644 | 0.40024 | 0.48305 | 0.34963 | 5.09040  | 0.00000 | 0.00000 |
| 7     |                                       | 0.47385                 | 0.37494 | 0.18862 | 0.27373 | 0.40254 | 0.22542 | 0.17252 | 0.29213 | 0.35653 | 0.38644 | 0.38414 | 0.34503 | 0.43474 | 0.53595 | 0.63946 | 0.54285 | 6.02889  | 0.00000 | 0.00000 |
| 8     |                                       | 0.44164                 | 0.41864 | 0.20932 | 0.27603 | 0.38874 | 0.17022 | 0.14721 | 0.23002 | 0.30133 | 0.30593 | 0.32433 | 0.42784 | 0.53365 | 0.62796 | 0.60956 | 0.44854 | 5.86097  | 0.00000 | 0.00000 |
| 9     |                                       | 0.93849                 | 0.65786 | 0.38184 | 0.65096 | 0.61876 | 0.31053 | 0.34733 | 0.56126 | 0.60496 | 0.57046 | 0.66477 | 0.69237 | 1.05580 | 1.20302 | 0.95919 | 0.68777 | 10.90537 | 0.00000 | 0.00000 |
| 10    |                                       | 0.41404                 | 0.36114 | 0.36804 | 0.39794 | 0.24842 | 0.19552 | 0.29673 | 0.39334 | 0.45774 | 0.48465 | 0.44624 | 0.40024 | 0.74527 | 0.69927 | 0.42324 | 0.29903 | 6.61085  | 0.00000 | 0.00000 |
| 11    |                                       | 0.22772                 | 0.30823 | 0.44164 | 0.35423 | 0.13111 | 0.21622 | 0.28063 | 0.54975 | 0.40944 | 0.45314 | 0.39794 | 0.33813 | 0.71307 | 0.57736 | 0.16792 | 0.06441 | 5.63095  | 0.00000 | 0.00000 |
| 5 (E) |                                       | 2                       | 0.01150 | 0.00690 | 0.01380 | 0.01150 | 0.01610 | 0.01150 | 0.00230 | 0.00690 | 0.00460 | 0.00690 | 0.01610 | 0.02300 | 0.01840 | 0.02760 | 0.02300 | 0.00230  | 0.20242 | 0.00460 |
|       | 3                                     | 0.01380                 | 0.03220 | 0.05751 | 0.03450 | 0.04830 | 0.01840 | 0.01840 | 0.01150 | 0.01840 | 0.01840 | 0.02070 | 0.00690 | 0.01610 | 0.01840 | 0.02990 | 0.03220 | 0.39564  | 0.00000 | 0.00000 |
|       | 4                                     | 0.04370                 | 0.03450 | 0.03450 | 0.02070 | 0.05981 | 0.02300 | 0.03680 | 0.02300 | 0.03220 | 0.01840 | 0.01380 | 0.02070 | 0.01610 | 0.02530 | 0.04600 | 0.04140 | 0.48995  | 0.00000 | 0.00000 |
|       | 5                                     | 0.09891                 | 0.08051 | 0.08511 | 0.12421 | 0.20472 | 0.08511 | 0.06211 | 0.07591 | 0.04370 | 0.06441 | 0.08971 | 0.09891 | 0.09431 | 0.08511 | 0.08741 | 0.11961 | 1.49975  | 0.00000 | 0.00000 |
|       | 6                                     | 0.12651                 | 0.09201 | 0.12191 | 0.15181 | 0.28753 | 0.12421 | 0.10581 | 0.07821 | 0.08511 | 0.15412 | 0.17252 | 0.13801 | 0.15412 | 0.22082 | 0.19092 | 0.15412 | 2.35773  | 0.00000 | 0.00000 |
|       | 7                                     | 0.16332                 | 0.12651 | 0.14031 | 0.12881 | 0.38184 | 0.13341 | 0.11981 | 0.09661 | 0.19782 | 0.18402 | 0.25533 | 0.24842 | 0.27143 | 0.37264 | 0.38874 | 0.24152 | 3.45034  | 0.00000 | 0.00000 |
|       | 8                                     | 0.24612                 | 0.13571 | 0.11961 | 0.16792 | 0.32203 | 0.15642 | 0.16332 | 0.13341 | 0.19782 | 0.24612 | 0.30133 | 0.33353 | 0.38874 | 0.36344 | 0.43934 | 0.28753 | 4.00239  | 0.00000 | 0.00000 |
|       | 9                                     | 0.28983                 | 0.33813 | 0.24152 | 0.35193 | 0.38414 | 0.32893 | 0.37494 | 0.42784 | 0.61186 |         |         |         |         |         |         |         |          |         |         |

|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
|-------|----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 7 (G) | 2  | 0.00920 | 0.01150 | 0.00230 | 0.00690 | 0.00460 | 0.00690 | 0.00230 | 0.00000 | 0.01150 | 0.00230 | 0.00920 | 0.01150 | 0.01610 | 0.00920 | 0.00690 | 0.00920 | 0.11961 | 0.00230 |
|       | 3  | 0.01610 | 0.01380 | 0.00920 | 0.00690 | 0.00920 | 0.00460 | 0.00690 | 0.00230 | 0.00690 | 0.00230 | 0.00920 | 0.00690 | 0.00690 | 0.00690 | 0.00460 | 0.01840 | 0.13111 |         |
|       | 4  | 0.00690 | 0.00690 | 0.01840 | 0.01610 | 0.01840 | 0.00460 | 0.00460 | 0.00230 | 0.00460 | 0.01380 | 0.00690 | 0.00460 | 0.00690 | 0.00690 | 0.01150 | 0.01150 | 0.14491 |         |
|       | 5  | 0.02300 | 0.02990 | 0.05751 | 0.07361 | 0.04140 | 0.01610 | 0.01150 | 0.00690 | 0.01610 | 0.02530 | 0.01840 | 0.01380 | 0.02760 | 0.03910 | 0.05751 | 0.04370 | 0.50145 |         |
|       | 6  | 0.05060 | 0.03450 | 0.04370 | 0.02530 | 0.02300 | 0.02530 | 0.02300 | 0.02300 | 0.02990 | 0.03450 | 0.02300 | 0.02760 | 0.05521 | 0.02070 | 0.03450 | 0.07131 | 0.54515 |         |
|       | 7  | 0.05751 | 0.04140 | 0.02300 | 0.00230 | 0.02070 | 0.01610 | 0.04140 | 0.02530 | 0.05751 | 0.02300 | 0.03450 | 0.02300 | 0.03910 | 0.04140 | 0.04600 | 0.07131 | 0.56356 |         |
|       | 8  | 0.02760 | 0.02530 | 0.01610 | 0.00230 | 0.01840 | 0.02530 | 0.02990 | 0.04370 | 0.05060 | 0.03680 | 0.05751 | 0.03450 | 0.04830 | 0.04830 | 0.06211 | 0.06211 | 0.58886 |         |
|       | 9  | 0.05291 | 0.03450 | 0.01380 | 0.00230 | 0.00690 | 0.06441 | 0.13341 | 0.12681 | 0.11731 | 0.11731 | 0.11961 | 0.04370 | 0.04830 | 0.02760 | 0.08741 | 0.05521 | 1.05350 |         |
|       | 10 | 0.00230 | 0.00920 | 0.00000 | 0.00230 | 0.01150 | 0.06671 | 0.10121 | 0.07591 | 0.07361 | 0.05751 | 0.02070 | 0.00000 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.42324 |         |
|       | 11 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00230 | 0.02990 | 0.02990 | 0.03910 | 0.02070 | 0.01150 | 0.00230 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.13571 |         |
|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | 99.9862 |

4.209413

100

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

## **ATTACHMENT 5**

### **Braidwood and Byron Stations Measurement Uncertainty Recapture Technical Evaluation**

#### **Response to NRC Acceptance Review Questions**

**Calculation No. BYR04-050, BRW-04-0044-M, Minor Rev. 1B,  
Appendix BB-2: "Braidwood Joint Frequency Distribution"**

**Braidwood****Joint Frequency Distribution**

1994-1998 (Rev. 3)

34 ft wind

199-30 ft Delta T

|       | Wind Speed<br>Category <sup>(1)</sup> | Wind Direction Category |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | Total | Calms | Total |
|-------|---------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|
|       |                                       | N                       | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW |       |       |       |
| 1 (A) | 2                                     | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0     | 0     | 0     |
|       | 3                                     | 0                       | 0   | 2   | 3   | 0   | 1   | 3   | 2   | 0   | 3   | 0   | 0   | 1   | 0   | 0   | 0   | 0     | 15    | 0     |
|       | 4                                     | 0                       | 5   | 14  | 16  | 21  | 6   | 14  | 7   | 7   | 8   | 0   | 7   | 2   | 3   | 0   | 3   | 113   | 0     | 0     |
|       | 5                                     | 27                      | 15  | 67  | 44  | 45  | 28  | 32  | 51  | 46  | 24  | 19  | 26  | 34  | 22  | 29  | 14  | 523   | 0     | 0     |
|       | 6                                     | 33                      | 41  | 55  | 19  | 20  | 14  | 19  | 38  | 32  | 31  | 30  | 38  | 46  | 36  | 41  | 49  | 542   | 0     | 0     |
|       | 7                                     | 31                      | 40  | 25  | 3   | 8   | 7   | 6   | 10  | 31  | 62  | 33  | 25  | 29  | 33  | 62  | 58  | 463   | 0     | 0     |
|       | 8                                     | 12                      | 10  | 5   | 1   | 0   | 3   | 2   | 7   | 21  | 27  | 20  | 19  | 21  | 37  | 19  | 19  | 223   | 0     | 0     |
|       | 9                                     | 2                       | 1   | 0   | 0   | 0   | 0   | 7   | 12  | 18  | 32  | 7   | 5   | 11  | 30  | 15  | 8   | 148   | 0     | 0     |
|       | 10                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 3   | 6   | 2   | 0   | 0   | 0   | 1   | 0   | 0   | 12    | 0     | 0     |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 3   | 7   | 1   | 0   | 0   | 0   | 0   | 0   | 12    | 0     | 2051  |
| 2 (B) | 2                                     | 0                       | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 2     | 0     | 0     |
|       | 3                                     | 0                       | 1   | 4   | 6   | 6   | 1   | 1   | 3   | 4   | 0   | 0   | 0   | 1   | 1   | 1   | 1   | 30    | 0     | 0     |
|       | 4                                     | 3                       | 3   | 9   | 15  | 20  | 12  | 10  | 11  | 5   | 4   | 4   | 6   | 2   | 6   | 5   | 1   | 116   | 0     | 0     |
|       | 5                                     | 21                      | 17  | 31  | 35  | 29  | 27  | 32  | 29  | 21  | 21  | 20  | 19  | 53  | 28  | 28  | 27  | 438   | 0     | 0     |
|       | 6                                     | 23                      | 26  | 34  | 14  | 15  | 10  | 12  | 19  | 19  | 27  | 18  | 27  | 21  | 43  | 43  | 31  | 382   | 0     | 0     |
|       | 7                                     | 10                      | 20  | 13  | 4   | 4   | 1   | 7   | 15  | 20  | 28  | 28  | 24  | 30  | 39  | 28  | 33  | 304   | 0     | 0     |
|       | 8                                     | 9                       | 12  | 3   | 3   | 0   | 0   | 0   | 8   | 22  | 20  | 18  | 13  | 8   | 24  | 20  | 17  | 177   | 0     | 0     |
|       | 9                                     | 2                       | 0   | 1   | 0   | 0   | 0   | 5   | 11  | 9   | 17  | 18  | 7   | 12  | 18  | 4   | 7   | 111   | 0     | 0     |
|       | 10                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 6   | 2   | 0   | 0   | 4   | 3   | 0   | 0   | 16    | 0     | 0     |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 1   | 2   | 0   | 0   | 0   | 0   | 0   | 0   | 4     | 0     | 1580  |
| 3 (C) | 2                                     | 0                       | 0   | 0   | 2   | 1   | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 4     | 0     | 0     |
|       | 3                                     | 1                       | 3   | 3   | 10  | 10  | 6   | 5   | 2   | 4   | 2   | 1   | 3   | 3   | 1   | 2   | 0   | 56    | 0     | 0     |
|       | 4                                     | 11                      | 13  | 23  | 20  | 24  | 18  | 13  | 14  | 13  | 11  | 7   | 11  | 16  | 12  | 5   | 9   | 220   | 0     | 0     |
|       | 5                                     | 21                      | 25  | 40  | 41  | 49  | 35  | 39  | 41  | 20  | 23  | 26  | 33  | 48  | 49  | 48  | 28  | 566   | 0     | 0     |
|       | 6                                     | 27                      | 27  | 36  | 14  | 16  | 10  | 16  | 35  | 27  | 35  | 35  | 37  | 56  | 58  | 51  | 41  | 521   | 0     | 0     |
|       | 7                                     | 19                      | 18  | 23  | 2   | 4   | 0   | 9   | 13  | 27  | 31  | 37  | 38  | 35  | 47  | 50  | 33  | 386   | 0     | 0     |
|       | 8                                     | 10                      | 12  | 4   | 0   | 0   | 4   | 5   | 19  | 17  | 29  | 31  | 18  | 12  | 21  | 22  | 12  | 216   | 0     | 0     |
|       | 9                                     | 4                       | 4   | 0   | 0   | 0   | 0   | 5   | 14  | 18  | 35  | 11  | 13  | 12  | 24  | 7   | 8   | 155   | 0     | 0     |
|       | 10                                    | 1                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 2   | 10  | 0   | 1   | 1   | 5   | 0   | 0   | 21    | 0     | 0     |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 0   | 6   | 0   | 0   | 0   | 3   | 0   | 0   | 10    | 0     | 2155  |
| 4 (D) | 2                                     | 9                       | 21  | 15  | 36  | 23  | 7   | 4   | 4   | 3   | 1   | 6   | 4   | 8   | 11  | 15  | 16  | 183   | 0     | 0     |
|       | 3                                     | 31                      | 51  | 90  | 131 | 128 | 43  | 24  | 19  | 12  | 12  | 19  | 28  | 41  | 70  | 72  | 39  | 810   | 0     | 0     |
|       | 4                                     | 71                      | 70  | 129 | 195 | 164 | 93  | 66  | 54  | 35  | 40  | 33  | 58  | 85  | 81  | 133 | 91  | 1398  | 0     | 0     |
|       | 5                                     | 167                     | 222 | 315 | 343 | 197 | 166 | 190 | 203 | 115 | 97  | 145 | 224 | 318 | 306 | 323 | 276 | 3607  | 0     | 0     |
|       | 6                                     | 166                     | 196 | 262 | 203 | 106 | 89  | 132 | 217 | 128 | 150 | 228 | 228 | 266 | 302 | 279 | 213 | 3165  | 0     | 0     |
|       | 7                                     | 100                     | 194 | 196 | 92  | 26  | 57  | 97  | 147 | 155 | 179 | 239 | 201 | 261 | 286 | 193 | 207 | 2630  | 0     | 0     |
|       | 8                                     | 71                      | 148 | 111 | 20  | 3   | 32  | 81  | 133 | 143 | 179 | 154 | 115 | 192 | 227 | 68  | 139 | 1816  | 0     | 0     |
|       | 9                                     | 33                      | 66  | 13  | 0   | 1   | 7   | 39  | 107 | 205 | 253 | 166 | 85  | 192 | 198 | 48  | 89  | 1502  | 0     | 0     |
|       | 10                                    | 10                      | 1   | 0   | 0   | 0   | 0   | 0   | 18  | 60  | 111 | 33  | 22  | 51  | 50  | 2   | 21  | 379   | 0     | 0     |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 3   | 13  | 16  | 15  | 1   | 10  | 3   | 0   | 3   | 64    | 0     | 15554 |
| 5 (E) | 2                                     | 43                      | 50  | 85  | 124 | 140 | 34  | 21  | 13  | 10  | 13  | 9   | 20  | 23  | 51  | 47  | 37  | 720   | 3     | 0     |
|       | 3                                     | 84                      | 94  | 146 | 263 | 285 | 159 | 60  | 38  | 19  | 17  | 20  | 45  | 118 | 171 | 130 | 82  | 1731  | 0     | 0     |
|       | 4                                     | 99                      | 125 | 156 | 235 | 201 | 192 | 125 | 105 | 55  | 32  | 50  | 140 | 180 | 165 | 172 | 89  | 2121  | 0     | 0     |
|       | 5                                     | 188                     | 238 | 202 | 262 | 175 | 269 | 355 | 422 | 233 | 187 | 224 | 421 | 298 | 310 | 183 | 215 | 4182  | 0     | 0     |
|       | 6                                     | 125                     | 129 | 153 | 97  | 56  | 88  | 254 | 317 | 319 | 350 | 299 | 249 | 200 | 244 | 130 | 153 | 3163  | 0     | 0     |
|       | 7                                     | 46                      | 87  | 66  | 34  | 13  | 50  | 100 | 223 | 310 | 388 | 186 | 114 | 134 | 165 | 61  | 85  | 2062  | 0     | 0     |
|       | 8                                     | 39                      | 52  | 47  | 15  | 2   | 25  | 37  | 136 | 216 | 264 | 79  | 61  | 75  | 88  | 23  | 30  | 1189  | 0     | 0     |
|       | 9                                     | 27                      | 71  | 75  | 6   | 0   | 3   | 35  | 77  | 185 | 236 | 61  | 46  | 71  | 84  | 19  | 23  | 1019  | 0     | 0     |
|       | 10                                    | 14                      | 14  | 3   | 0   | 0   | 0   | 2   | 5   | 81  | 44  | 19  | 27  | 43  | 16  | 0   | 0   | 268   | 0     | 0     |
|       | 11                                    | 1                       | 0   | 0   | 0   | 0   | 0   | 0   | 10  | 12  | 10  | 15  | 13  | 23  | 3   | 0   | 2   | 89    | 0     | 16547 |
| 6 (F) | 2                                     | 64                      | 45  | 84  | 114 | 143 | 60  | 32  | 23  | 17  | 19  | 19  | 31  | 56  | 82  | 79  | 52  | 920   | 20    | 0     |
|       | 3                                     | 45                      | 30  | 37  | 75  | 144 | 147 | 68  | 36  | 16  | 25  | 22  | 54  | 128 | 199 | 114 | 68  | 1208  | 0     | 0     |
|       | 4                                     | 45                      | 24  | 10  | 11  | 28  | 150 | 77  | 44  | 21  | 27  | 37  | 103 | 164 | 93  | 44  | 28  | 906   | 0     | 0     |
|       | 5                                     | 21                      | 9   | 4   | 4   | 6   | 49  | 71  | 72  | 43  | 62  | 43  | 259 | 128 | 37  | 10  | 12  | 830   | 0     | 0     |
|       | 6                                     | 0                       | 0   | 1   | 0   | 0   | 1   | 5   | 27  | 17  | 73  | 36  | 37  | 13  | 3   | 1   | 0   | 214   | 0     | 0     |
|       | 7                                     | 0                       | 0   | 0   | 0   | 0   | 0   | 1   | 1   | 7   | 47  | 10  | 0   | 1   | 0   | 0   | 1   | 68    | 0     | 0     |
|       | 8                                     | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 10  | 0   | 0   | 0   | 0   | 0   | 0   | 10    | 0     | 0     |
|       | 9                                     | 0                       | 0   | 1   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 1   | 0   | 0   | 1   | 0   | 0   | 3     | 0     | 0     |
|       | 10                                    | 0                       | 4   | 8   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 12    | 0     | 0     |
|       | 11                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 18    | 0     | 4209  |

|       |    |    |    |    |    |    |    |    |    |    |    |    |     |    |    |    |    |     |
|-------|----|----|----|----|----|----|----|----|----|----|----|----|-----|----|----|----|----|-----|
| 7 (G) | 2  | 52 | 44 | 53 | 81 | 91 | 46 | 27 | 18 | 13 | 12 | 19 | 17  | 43 | 81 | 77 | 66 | 740 |
|       | 3  | 18 | 20 | 10 | 14 | 65 | 48 | 15 | 4  | 9  | 9  | 11 | 31  | 73 | 91 | 39 | 28 | 485 |
|       | 4  | 8  | 3  | 0  | 3  | 25 | 30 | 11 | 1  | 4  | 8  | 6  | 30  | 47 | 21 | 5  | 9  | 211 |
|       | 5  | 1  | 1  | 0  | 1  | 0  | 6  | 5  | 3  | 2  | 6  | 1  | 111 | 22 | 1  | 2  | 1  | 163 |
|       | 6  | 1  | 0  | 0  | 0  | 0  | 0  | 0  | 1  | 2  | 4  | 2  | 3   | 0  | 0  | 0  | 0  | 13  |
|       | 7  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 3  | 0  | 0   | 0  | 0  | 0  | 0  | 3   |
|       | 8  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0  | 0  | 0  | 0   |
|       | 9  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0  | 0  | 0  | 0   |
|       | 10 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0  | 0  | 0  | 0   |
|       | 11 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0  | 0  | 0  | 0  | 0   |

19

1634  
43730

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |



## Braidwood

## Joint Frequency Distribution

1994-1998 (Rev. 3)

34 ft wind

199-30 ft Delta T

|                                    |       | Wind Direction Category |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | Total   | Calms    | Total   |
|------------------------------------|-------|-------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|
| Wind Speed Category <sup>(1)</sup> |       | 1                       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10      | 11      | 12      | 13      | 14      | 15      | 16      |         |          |         |
| 1 (A)                              | 2     | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 |
|                                    | 3     | 0.00000                 | 0.00000 | 0.00457 | 0.00686 | 0.00000 | 0.00229 | 0.00686 | 0.00457 | 0.00000 | 0.00686 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.03430  |         |
|                                    | 4     | 0.00000                 | 0.01143 | 0.03201 | 0.03659 | 0.04802 | 0.01372 | 0.03201 | 0.01601 | 0.01601 | 0.01829 | 0.00000 | 0.01601 | 0.00457 | 0.00686 | 0.00000 | 0.00686 | 0.25840 |          |         |
|                                    | 5     | 0.06174                 | 0.03430 | 0.15321 | 0.10062 | 0.10290 | 0.06403 | 0.07318 | 0.11662 | 0.10519 | 0.05488 | 0.04345 | 0.05946 | 0.07775 | 0.05031 | 0.06632 | 0.03201 | 1.19598 |          |         |
|                                    | 6     | 0.07546                 | 0.09376 | 0.12577 | 0.04345 | 0.04574 | 0.03201 | 0.04345 | 0.08690 | 0.07318 | 0.07089 | 0.06860 | 0.08690 | 0.10519 | 0.08232 | 0.09376 | 0.11205 | 1.23942 |          |         |
|                                    | 7     | 0.07089                 | 0.09147 | 0.05717 | 0.00686 | 0.01829 | 0.01601 | 0.01372 | 0.02287 | 0.07089 | 0.14178 | 0.07546 | 0.05717 | 0.06632 | 0.07546 | 0.14178 | 0.13263 | 1.05877 |          |         |
|                                    | 8     | 0.02744                 | 0.02287 | 0.01143 | 0.00229 | 0.00000 | 0.00686 | 0.00457 | 0.01601 | 0.04802 | 0.06174 | 0.04574 | 0.04345 | 0.04802 | 0.08461 | 0.04345 | 0.04345 | 0.50995 |          |         |
|                                    | 9     | 0.00457                 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.01601 | 0.02744 | 0.04116 | 0.07318 | 0.01601 | 0.01143 | 0.02515 | 0.06860 | 0.03430 | 0.01829 | 0.33844 |          |         |
|                                    | 10    | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00686 | 0.01372 | 0.00457 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.02744 |          |         |
|                                    | 11    | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00686 | 0.01601 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.02744 | 4.690144 |         |
|                                    | 2 (B) | 2                       | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00457  | 0.00000 |
| 3                                  |       | 0.00000                 | 0.00229 | 0.00915 | 0.01372 | 0.01372 | 0.00229 | 0.00686 | 0.00915 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00229 | 0.00229 | 0.00229 | 0.06860 |          |         |
| 4                                  |       | 0.00686                 | 0.00686 | 0.02058 | 0.03430 | 0.04574 | 0.02744 | 0.02287 | 0.02515 | 0.01143 | 0.00915 | 0.00915 | 0.01372 | 0.00457 | 0.01372 | 0.01143 | 0.00229 | 0.26526 |          |         |
| 5                                  |       | 0.04802                 | 0.03887 | 0.07089 | 0.08004 | 0.06632 | 0.06174 | 0.07318 | 0.06632 | 0.04802 | 0.04802 | 0.04574 | 0.04345 | 0.12120 | 0.06403 | 0.06403 | 0.06174 | 1.00160 |          |         |
| 6                                  |       | 0.05260                 | 0.05946 | 0.07775 | 0.03201 | 0.03430 | 0.02287 | 0.02744 | 0.04345 | 0.04345 | 0.06174 | 0.04116 | 0.06174 | 0.04802 | 0.09833 | 0.09833 | 0.07089 | 0.87354 |          |         |
| 7                                  |       | 0.02287                 | 0.04574 | 0.02973 | 0.00915 | 0.00915 | 0.00229 | 0.01601 | 0.03430 | 0.04574 | 0.06403 | 0.06403 | 0.05488 | 0.06860 | 0.08918 | 0.06403 | 0.07546 | 0.69517 |          |         |
| 8                                  |       | 0.02058                 | 0.02744 | 0.00686 | 0.00686 | 0.00000 | 0.00000 | 0.00000 | 0.01829 | 0.05031 | 0.04574 | 0.04116 | 0.02973 | 0.01829 | 0.05488 | 0.04574 | 0.03887 | 0.40476 |          |         |
| 9                                  |       | 0.00457                 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.01143 | 0.02515 | 0.02058 | 0.03887 | 0.04116 | 0.01601 | 0.02744 | 0.04116 | 0.00915 | 0.01601 | 0.25383 |          |         |
| 10                                 |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.01372 | 0.00457 | 0.00000 | 0.00000 | 0.00915 | 0.00686 | 0.00000 | 0.00000 | 0.03659 |          |         |
| 11                                 |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00229 | 0.00457 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00915 | 3.61308  |         |
| 3 (C)                              |       | 2                       | 0.00000 | 0.00000 | 0.00000 | 0.00457 | 0.00229 | 0.00000 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00915  | 0.00000 |
|                                    | 3     | 0.00229                 | 0.00686 | 0.00686 | 0.02287 | 0.02287 | 0.01372 | 0.01143 | 0.00457 | 0.00915 | 0.00457 | 0.00229 | 0.00686 | 0.00686 | 0.00229 | 0.00457 | 0.00000 | 0.12806 |          |         |
|                                    | 4     | 0.02515                 | 0.02973 | 0.05260 | 0.04574 | 0.05488 | 0.04116 | 0.02973 | 0.03201 | 0.02973 | 0.02515 | 0.01601 | 0.02515 | 0.03659 | 0.02744 | 0.01143 | 0.02058 | 0.50309 |          |         |
|                                    | 5     | 0.04802                 | 0.05717 | 0.09147 | 0.09376 | 0.11205 | 0.08004 | 0.08918 | 0.09376 | 0.04574 | 0.05260 | 0.05946 | 0.07546 | 0.10976 | 0.11205 | 0.10976 | 0.06403 | 1.29431 |          |         |
|                                    | 6     | 0.06174                 | 0.06174 | 0.08232 | 0.03201 | 0.03659 | 0.02287 | 0.03659 | 0.08004 | 0.06174 | 0.08004 | 0.08461 | 0.12806 | 0.13263 | 0.11662 | 0.09376 | 1.19140 |         |          |         |
|                                    | 7     | 0.04345                 | 0.04116 | 0.05260 | 0.00457 | 0.00915 | 0.00000 | 0.02058 | 0.02973 | 0.06174 | 0.07089 | 0.08461 | 0.08690 | 0.08004 | 0.10748 | 0.11434 | 0.07546 | 0.88269 |          |         |
|                                    | 8     | 0.02287                 | 0.02744 | 0.00915 | 0.00000 | 0.00000 | 0.00915 | 0.01143 | 0.04345 | 0.03887 | 0.06632 | 0.07089 | 0.04116 | 0.02744 | 0.04802 | 0.05031 | 0.02744 | 0.49394 |          |         |
|                                    | 9     | 0.00915                 | 0.00915 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.01143 | 0.03201 | 0.04116 | 0.08004 | 0.02515 | 0.02973 | 0.02744 | 0.05488 | 0.01601 | 0.01829 | 0.35445 |          |         |
|                                    | 10    | 0.00229                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00457 | 0.02287 | 0.00000 | 0.00229 | 0.00229 | 0.01143 | 0.00000 | 0.00000 | 0.04802 |          |         |
|                                    | 11    | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00000 | 0.01372 | 0.00000 | 0.00000 | 0.00000 | 0.00686 | 0.00000 | 0.00000 | 0.02287 | 4.927967 |         |
|                                    | 4 (D) | 2                       | 0.02058 | 0.04802 | 0.03430 | 0.08232 | 0.05260 | 0.01601 | 0.00915 | 0.00915 | 0.00686 | 0.00229 | 0.01372 | 0.00915 | 0.01829 | 0.02515 | 0.03430 | 0.03659 | 0.41848  | 0.00000 |
| 3                                  |       | 0.07089                 | 0.11662 | 0.20581 | 0.29957 | 0.29271 | 0.09833 | 0.05488 | 0.04345 | 0.02744 | 0.02744 | 0.04345 | 0.06403 | 0.09376 | 0.16007 | 0.16465 | 0.08918 | 1.85228 |          |         |
| 4                                  |       | 0.16236                 | 0.16007 | 0.29499 | 0.44592 | 0.37503 | 0.21267 | 0.15093 | 0.12349 | 0.08004 | 0.09147 | 0.07546 | 0.13263 | 0.19437 | 0.18523 | 0.30414 | 0.20810 | 3.19689 |          |         |
| 5                                  |       | 0.38189                 | 0.50766 | 0.72033 | 0.78436 | 0.45049 | 0.37960 | 0.43448 | 0.46421 | 0.26298 | 0.22182 | 0.33158 | 0.51223 | 0.72719 | 0.69975 | 0.73862 | 0.63115 | 8.24834 |          |         |
| 6                                  |       | 0.37960                 | 0.44820 | 0.59913 | 0.46421 | 0.24240 | 0.20352 | 0.30185 | 0.49623 | 0.29271 | 0.34301 | 0.52138 | 0.52138 | 0.60828 | 0.69060 | 0.63801 | 0.48708 | 7.23759 |          |         |
| 7                                  |       | 0.22868                 | 0.44363 | 0.44820 | 0.21038 | 0.05946 | 0.13035 | 0.22182 | 0.33615 | 0.35445 | 0.40933 | 0.54654 | 0.59684 | 0.59684 | 0.65401 | 0.44134 | 0.47336 | 6.01418 |          |         |
| 8                                  |       | 0.16236                 | 0.33844 | 0.25383 | 0.04574 | 0.00686 | 0.07318 | 0.18523 | 0.30414 | 0.32701 | 0.40933 | 0.35216 | 0.26298 | 0.43906 | 0.51909 | 0.15550 | 0.31786 | 4.15276 |          |         |
| 9                                  |       | 0.07546                 | 0.15093 | 0.02973 | 0.00000 | 0.00229 | 0.01601 | 0.08918 | 0.24468 | 0.46879 | 0.57855 | 0.37960 | 0.19437 | 0.43906 | 0.45278 | 0.10976 | 0.20352 | 3.43471 |          |         |
| 10                                 |       | 0.02287                 | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.04116 | 0.13721 | 0.25383 | 0.07546 | 0.05031 | 0.11662 | 0.11434 | 0.00457 | 0.04802 | 0.86668 |          |         |
| 11                                 |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00686 | 0.02973 | 0.03659 | 0.03430 | 0.00229 | 0.02287 | 0.00686 | 0.00000 | 0.00686 | 0.14635 |          |         |
| 5 (E)                              |       | 2                       | 0.09833 | 0.11434 | 0.19437 | 0.28356 | 0.32015 | 0.07775 | 0.04802 | 0.02973 | 0.02287 | 0.02973 | 0.02058 | 0.04574 | 0.05260 | 0.11662 | 0.10748 | 0.08461 | 1.64647  | 0.00686 |
|                                    | 3     | 0.19209                 | 0.21496 | 0.33387 | 0.60142 | 0.65173 | 0.36359 | 0.13721 | 0.08690 | 0.04345 | 0.03887 | 0.04574 | 0.10290 | 0.26984 | 0.39104 | 0.29728 | 0.18751 | 3.95838 |          |         |
|                                    | 4     | 0.22639                 | 0.28584 | 0.35673 | 0.53739 | 0.45964 | 0.43906 | 0.28584 | 0.24011 | 0.12577 | 0.07318 | 0.11434 | 0.32015 | 0.41162 | 0.37732 | 0.39332 | 0.20352 | 4.85022 |          |         |
|                                    | 5     | 0.42991                 | 0.54425 | 0.46193 | 0.59913 | 0.40018 | 0.61514 | 0.81180 | 0.96501 | 0.53282 | 0.42762 | 0.51223 | 0.68273 | 0.68145 | 0.70890 | 0.41848 | 0.49165 | 9.56323 |          |         |
|                                    | 6     | 0.28584                 | 0.29499 | 0.34987 | 0.22182 | 0.12806 | 0.20123 | 0.58084 | 0.72490 | 0.72948 | 0.80037 | 0.68374 | 0.56940 | 0.45735 | 0.55797 | 0.29728 | 0.34987 | 7.23302 |          |         |
|                                    | 7     | 0.10519                 | 0.19895 | 0.15093 | 0.07775 | 0.02973 | 0.11434 | 0.22868 | 0.50995 | 0.70890 | 0.88726 | 0.42534 | 0.26069 | 0.30643 | 0.37732 | 0.13949 | 0.19437 | 4.71530 |          |         |
|                                    | 8     | 0.08918                 | 0.11891 | 0.10748 | 0.03430 | 0.00457 | 0.05717 | 0.08461 | 0.31100 | 0.49394 | 0.60370 | 0.18065 | 0.13949 | 0.17151 | 0.20123 | 0.05260 | 0.06860 | 2.71896 |          |         |
|                                    | 9     | 0.06174                 | 0.16236 | 0.17151 | 0.01372 | 0.00000 | 0.00686 | 0.08004 |         |         |         |         |         |         |         |         |         |         |          |         |

|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |          |
|-------|----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| 7 (G) | 2  | 0.11891 | 0.10062 | 0.12120 | 0.18523 | 0.20810 | 0.10519 | 0.06174 | 0.04116 | 0.02973 | 0.02744 | 0.04345 | 0.03887 | 0.09833 | 0.18523 | 0.17608 | 0.15093 | 1.69220 | 0.04345  |
|       | 3  | 0.04116 | 0.04574 | 0.02287 | 0.03201 | 0.14864 | 0.10976 | 0.03430 | 0.00915 | 0.02058 | 0.02058 | 0.02515 | 0.07089 | 0.16693 | 0.20810 | 0.08918 | 0.06403 | 1.10908 |          |
|       | 4  | 0.01829 | 0.00686 | 0.00000 | 0.00686 | 0.05717 | 0.06860 | 0.02515 | 0.00229 | 0.00915 | 0.01829 | 0.01372 | 0.06860 | 0.10748 | 0.04802 | 0.01143 | 0.02058 | 0.48251 |          |
|       | 5  | 0.00229 | 0.00229 | 0.00000 | 0.00229 | 0.00000 | 0.01372 | 0.01143 | 0.00686 | 0.00457 | 0.01372 | 0.00229 | 0.25383 | 0.05031 | 0.00229 | 0.00457 | 0.00229 | 0.37274 |          |
|       | 6  | 0.00229 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00229 | 0.00457 | 0.00915 | 0.00457 | 0.00686 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.02973 |          |
|       | 7  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00686 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00686 |          |
|       | 8  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |          |
|       | 9  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |          |
|       | 10 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |          |
|       | 11 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |          |
|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | 99.90396 |

3.736565

100

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

**Braidwood**  
**Joint Frequency Distribution**  
**1994-1998 (Rev. 3)**  
**203 ft wind**  
**199-30 ft Delta T**

|       | Wind Speed Category <sup>(1)</sup> | Wind Direction Category |     |     |     |     |     |     |     |      |      |     |     |      |      |     |       | Total | Calms | Total |
|-------|------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|-------|-------|-------|-------|
|       |                                    | N                       | NNE | NE  | ENE | E   | ESE | SE  | SSE | S    | SSW  | SW  | WSW | W    | WNW  | NW  | NNW   |       |       |       |
| 1 (A) | 2                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 0     |       |       |
|       | 3                                  | 0                       | 0   | 0   | 1   | 0   | 0   | 0   | 0   | 1    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 0     |       |       |
|       | 4                                  | 0                       | 0   | 3   | 17  | 6   | 4   | 7   | 2   | 2    | 1    | 0   | 1   | 2    | 3    | 0   | 0     | 1     |       |       |
|       | 5                                  | 12                      | 13  | 26  | 16  | 22  | 14  | 12  | 14  | 19   | 16   | 6   | 12  | 14   | 2    | 6   | 7     | 211   |       |       |
|       | 6                                  | 19                      | 9   | 25  | 27  | 18  | 20  | 17  | 40  | 30   | 13   | 17  | 15  | 30   | 21   | 18  | 10    | 329   |       |       |
|       | 7                                  | 30                      | 20  | 33  | 25  | 25  | 14  | 12  | 28  | 25   | 24   | 18  | 26  | 40   | 14   | 29  | 31    | 394   |       |       |
|       | 8                                  | 16                      | 24  | 31  | 12  | 16  | 6   | 11  | 10  | 22   | 21   | 24  | 21  | 20   | 19   | 36  | 31    | 320   |       |       |
|       | 9                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 0     |       |       |
|       | 10                                 | 88                      | 73  | 108 | 61  | 63  | 43  | 36  | 73  | 108  | 154  | 88  | 79  | 120  | 115  | 181 | 123   | 1513  |       |       |
|       | 11                                 | 0                       | 0   | 0   | 0   | 1   | 1   | 6   | 10  | 26   | 28   | 4   | 0   | 0    | 17   | 16  | 0     | 109   |       |       |
|       | 2 (B)                              | 2                       | 0   | 0   | 1   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 1     | 2     |       |
| 3     | 0                                  | 0                       | 1   | 1   | 3   | 1   | 1   | 0   | 1   | 0    | 0    | 0   | 0   | 0    | 1    | 0   | 9     |       |       |       |
| 4     | 5                                  | 1                       | 3   | 5   | 8   | 5   | 4   | 4   | 1   | 3    | 0    | 2   | 5   | 1    | 1    | 1   | 49    |       |       |       |
| 5     | 6                                  | 11                      | 9   | 21  | 19  | 19  | 16  | 13  | 12  | 9    | 4    | 16  | 25  | 11   | 10   | 9   | 210   |       |       |       |
| 6     | 21                                 | 9                       | 15  | 23  | 17  | 15  | 18  | 22  | 14  | 14   | 23   | 10  | 25  | 21   | 22   | 21  | 290   |       |       |       |
| 7     | 19                                 | 19                      | 17  | 11  | 13  | 7   | 12  | 12  | 15  | 17   | 12   | 20  | 12  | 26   | 27   | 23  | 262   |       |       |       |
| 8     | 12                                 | 9                       | 15  | 7   | 9   | 8   | 6   | 5   | 10  | 20   | 11   | 21  | 22  | 25   | 20   | 17  | 217   |       |       |       |
| 9     | 0                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     |       |       |       |
| 10    | 56                                 | 49                      | 62  | 40  | 43  | 30  | 32  | 50  | 74  | 98   | 80   | 66  | 76  | 114  | 122  | 89  | 1081  |       |       |       |
| 11    | 0                                  | 0                       | 0   | 0   | 0   | 0   | 5   | 6   | 10  | 12   | 8    | 0   | 8   | 11   | 5    | 1   | 66    |       |       |       |
| 3 (C) | 2                                  | 0                       | 0   | 0   | 2   | 1   | 0   | 0   | 1   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 4     |       |       |
|       | 3                                  | 0                       | 1   | 1   | 3   | 5   | 2   | 3   | 0   | 1    | 2    | 0   | 0   | 2    | 0    | 1   | 1     | 22    |       |       |
|       | 4                                  | 3                       | 13  | 5   | 10  | 12  | 9   | 10  | 7   | 8    | 6    | 4   | 4   | 4    | 0    | 3   | 104   |       |       |       |
|       | 5                                  | 22                      | 19  | 18  | 17  | 24  | 23  | 26  | 22  | 16   | 14   | 15  | 16  | 37   | 24   | 18  | 329   |       |       |       |
|       | 6                                  | 18                      | 15  | 25  | 24  | 22  | 17  | 20  | 17  | 16   | 12   | 19  | 30  | 28   | 40   | 31  | 351   |       |       |       |
|       | 7                                  | 15                      | 16  | 13  | 18  | 27  | 13  | 15  | 17  | 17   | 23   | 24  | 36  | 34   | 28   | 32  | 360   |       |       |       |
|       | 8                                  | 17                      | 13  | 26  | 5   | 3   | 8   | 6   | 12  | 18   | 17   | 23  | 22  | 24   | 43   | 36  | 27    | 300   |       |       |
|       | 9                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     |       |       |       |
|       | 10                                 | 64                      | 51  | 78  | 47  | 54  | 37  | 42  | 67  | 95   | 111  | 112 | 114 | 107  | 155  | 158 | 102   | 1394  |       |       |
|       | 11                                 | 1                       | 0   | 0   | 0   | 0   | 0   | 9   | 7   | 11   | 38   | 3   | 5   | 6    | 24   | 5   | 3     | 112   |       |       |
|       | 4 (D)                              | 2                       | 1   | 7   | 9   | 6   | 7   | 1   | 4   | 2    | 6    | 1   | 0   | 4    | 1    | 2   | 7     | 2     | 60    |       |
| 3     | 16                                 | 21                      | 31  | 45  | 31  | 16  | 6   | 12  | 7   | 9    | 12   | 13  | 17  | 26   | 24   | 23  | 309   |       |       |       |
| 4     | 34                                 | 39                      | 38  | 43  | 56  | 22  | 27  | 16  | 16  | 17   | 14   | 33  | 22  | 41   | 51   | 48  | 517   |       |       |       |
| 5     | 109                                | 67                      | 121 | 114 | 128 | 68  | 87  | 63  | 65  | 46   | 70   | 85  | 114 | 104  | 165  | 133 | 1539  |       |       |       |
| 6     | 91                                 | 95                      | 145 | 189 | 166 | 81  | 85  | 107 | 56  | 51   | 117  | 119 | 158 | 159  | 174  | 155 | 1948  |       |       |       |
| 7     | 129                                | 114                     | 168 | 197 | 128 | 77  | 82  | 125 | 76  | 59   | 153  | 160 | 207 | 213  | 210  | 163 | 2261  |       |       |       |
| 8     | 92                                 | 107                     | 156 | 134 | 102 | 73  | 81  | 103 | 93  | 86   | 161  | 137 | 154 | 178  | 188  | 122 | 1967  |       |       |       |
| 9     | 0                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     |       |       |       |
| 10    | 440                                | 582                     | 856 | 708 | 481 | 339 | 418 | 548 | 596 | 608  | 784  | 642 | 929 | 1097 | 898  | 698 | 10624 |       |       |       |
| 11    | 13                                 | 14                      | 27  | 9   | 8   | 42  | 71  | 92  | 194 | 371  | 99   | 50  | 142 | 230  | 66   | 70  | 1498  |       |       |       |
| 5 (E) | 2                                  | 3                       | 4   | 8   | 8   | 5   | 1   | 1   | 1   | 2    | 1    | 2   | 1   | 4    | 9    | 5   | 5     | 60    |       |       |
|       | 3                                  | 13                      | 17  | 16  | 16  | 12  | 11  | 7   | 6   | 5    | 4    | 5   | 10  | 11   | 12   | 16  | 16    | 177   |       |       |
|       | 4                                  | 26                      | 17  | 22  | 27  | 24  | 16  | 13  | 16  | 10   | 8    | 10  | 12  | 22   | 9    | 18  | 17    | 267   |       |       |
|       | 5                                  | 83                      | 58  | 100 | 119 | 88  | 48  | 53  | 48  | 44   | 23   | 65  | 65  | 44   | 73   | 82  | 61    | 1054  |       |       |
|       | 6                                  | 112                     | 95  | 134 | 251 | 185 | 77  | 113 | 126 | 81   | 65   | 112 | 107 | 116  | 107  | 155 | 133   | 1969  |       |       |
|       | 7                                  | 144                     | 126 | 207 | 241 | 318 | 125 | 172 | 175 | 132  | 106  | 142 | 208 | 170  | 211  | 175 | 183   | 2835  |       |       |
|       | 8                                  | 114                     | 126 | 181 | 147 | 155 | 149 | 193 | 190 | 196  | 145  | 176 | 223 | 194  | 218  | 154 | 173   | 2734  |       |       |
|       | 9                                  | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 0     |       |       |
|       | 10                                 | 440                     | 497 | 688 | 670 | 716 | 601 | 793 | 932 | 1126 | 1251 | 876 | 817 | 832  | 1004 | 710 | 600   | 12553 |       |       |
|       | 11                                 | 22                      | 51  | 79  | 20  | 6   | 38  | 65  | 95  | 255  | 362  | 85  | 72  | 130  | 117  | 43  | 11    | 1451  |       |       |
|       | 6 (F)                              | 2                       | 3   | 0   | 3   | 6   | 2   | 6   | 1   | 0    | 0    | 3   | 5   | 4    | 5    | 2   | 2     | 1     | 43    |       |
| 3     |                                    | 5                       | 7   | 6   | 5   | 7   | 3   | 6   | 6   | 7    | 8    | 7   | 8   | 4    | 5    | 7   | 3     | 94    |       |       |
| 4     |                                    | 7                       | 5   | 7   | 9   | 8   | 9   | 15  | 10  | 14   | 5    | 11  | 7   | 5    | 9    | 5   | 7     | 133   |       |       |
| 5     |                                    | 38                      | 23  | 21  | 38  | 31  | 16  | 27  | 34  | 24   | 22   | 41  | 23  | 21   | 22   | 32  | 29    | 442   |       |       |
| 6     |                                    | 60                      | 38  | 37  | 51  | 43  | 30  | 34  | 42  | 44   | 37   | 31  | 31  | 40   | 53   | 58  | 64    | 693   |       |       |
| 7     |                                    | 58                      | 30  | 28  | 33  | 61  | 55  | 70  | 61  | 35   | 42   | 32  | 43  | 74   | 105  | 113 | 97    | 937   |       |       |
| 8     |                                    | 43                      | 39  | 24  | 16  | 48  | 76  | 90  | 29  | 35   | 26   | 34  | 45  | 123  | 109  | 69  | 45    | 851   |       |       |
| 9     |                                    | 0                       | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0   | 0   | 0    | 0    | 0   | 0     | 0     |       |       |
| 10    |                                    | 144                     | 101 | 77  | 79  | 158 | 274 | 267 | 150 | 142  | 130  | 206 | 192 | 385  | 351  | 248 | 183   | 3087  |       |       |
| 11    |                                    | 0                       | 1   | 12  | 0   | 0   | 0   | 1   | 0   | 1    | 9    | 9   | 9   | 9    | 1    | 0   | 0     | 52    |       |       |

|       |    |    |    |    |    |    |    |    |    |    |    |    |    |     |     |    |    |     |
|-------|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|-----|----|----|-----|
| 7 (G) | 2  | 5  | 7  | 5  | 7  | 3  | 4  | 4  | 2  | 3  | 6  | 6  | 4  | 4   | 4   | 4  | 4  | 72  |
|       | 3  | 4  | 4  | 7  | 6  | 4  | 3  | 7  | 5  | 7  | 4  | 9  | 8  | 5   | 6   | 5  | 6  | 90  |
|       | 4  | 7  | 6  | 4  | 5  | 4  | 5  | 4  | 17 | 11 | 13 | 7  | 14 | 4   | 3   | 2  | 3  | 109 |
|       | 5  | 27 | 15 | 17 | 11 | 11 | 9  | 18 | 28 | 31 | 24 | 24 | 14 | 13  | 14  | 14 | 14 | 284 |
|       | 6  | 26 | 20 | 18 | 10 | 25 | 13 | 32 | 15 | 10 | 17 | 13 | 13 | 7   | 16  | 25 | 26 | 286 |
|       | 7  | 34 | 15 | 10 | 9  | 24 | 19 | 21 | 18 | 2  | 3  | 13 | 11 | 27  | 38  | 34 | 38 | 316 |
|       | 8  | 22 | 9  | 6  | 4  | 6  | 30 | 22 | 9  | 2  | 1  | 4  | 13 | 20  | 54  | 23 | 20 | 245 |
|       | 9  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   | 0  | 0  | 0   |
|       | 10 | 70 | 40 | 28 | 19 | 46 | 78 | 78 | 38 | 8  | 12 | 31 | 48 | 121 | 161 | 92 | 70 | 940 |
|       | 11 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 1  | 0  | 0   | 0   | 0  | 0  | 1   |

2

2345  
60590

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

**Braidwood****Joint Frequency Distribution**

1994-1998 (Rev. 3)

203 ft wind

199-30 ft Delta T

|                                    |       | Wind Direction Category |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | Total    | Calms   | Total    |
|------------------------------------|-------|-------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|----------|
| Wind Speed Category <sup>(1)</sup> |       | 1                       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10      | 11      | 12      | 13      | 14      | 15      | 16      |          |         |          |
| 1 (A)                              | 2     | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00000  |
|                                    | 3     | 0.00000                 | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00330  |
|                                    | 4     | 0.00000                 | 0.00000 | 0.00495 | 0.02806 | 0.00990 | 0.00660 | 0.01155 | 0.00330 | 0.00330 | 0.00165 | 0.00000 | 0.00165 | 0.00330 | 0.00495 | 0.00000 | 0.00165 | 0.00807  | 0.00000 | 0.08087  |
|                                    | 5     | 0.01981                 | 0.02146 | 0.04291 | 0.02641 | 0.03631 | 0.02311 | 0.01981 | 0.02311 | 0.03136 | 0.02641 | 0.00990 | 0.01981 | 0.02311 | 0.00330 | 0.00990 | 0.01155 | 0.34824  | 0.00000 | 0.34824  |
|                                    | 6     | 0.03136                 | 0.01485 | 0.04126 | 0.04456 | 0.02971 | 0.03301 | 0.02806 | 0.06602 | 0.04951 | 0.02146 | 0.02806 | 0.02476 | 0.04951 | 0.03466 | 0.02971 | 0.01650 | 0.54299  | 0.00000 | 0.54299  |
|                                    | 7     | 0.04951                 | 0.03301 | 0.05446 | 0.04126 | 0.04126 | 0.02311 | 0.01981 | 0.04621 | 0.04126 | 0.03961 | 0.02971 | 0.04291 | 0.06602 | 0.02311 | 0.04786 | 0.05116 | 0.65027  | 0.00000 | 0.65027  |
|                                    | 8     | 0.02641                 | 0.03961 | 0.05116 | 0.01981 | 0.02641 | 0.00990 | 0.01815 | 0.01650 | 0.03631 | 0.03466 | 0.03961 | 0.03466 | 0.03301 | 0.03136 | 0.05942 | 0.05116 | 0.52814  | 0.00000 | 0.52814  |
|                                    | 9     | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00000  |
|                                    | 10    | 0.14524                 | 0.12048 | 0.17825 | 0.10068 | 0.10398 | 0.07097 | 0.05942 | 0.12048 | 0.17825 | 0.25417 | 0.14524 | 0.13038 | 0.19805 | 0.18980 | 0.29873 | 0.20300 | 2.49711  | 0.00000 | 2.49711  |
|                                    | 11    | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00165 | 0.00165 | 0.00990 | 0.01650 | 0.04291 | 0.04621 | 0.00660 | 0.00000 | 0.00000 | 0.00000 | 0.02806 | 0.02641 | 0.00000  | 0.17990 | 0.00000  |
|                                    | 2 (B) | 2                       | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00165  | 0.00330 | 0.00000  |
| 3                                  |       | 0.00000                 | 0.00000 | 0.00165 | 0.00165 | 0.00495 | 0.00165 | 0.00495 | 0.00165 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.01485  | 0.00000 | 0.01485  |
| 4                                  |       | 0.00825                 | 0.00165 | 0.00495 | 0.00825 | 0.01320 | 0.00825 | 0.00660 | 0.00660 | 0.00165 | 0.00495 | 0.00000 | 0.00330 | 0.00825 | 0.00165 | 0.00165 | 0.00165 | 0.08087  | 0.00000 | 0.08087  |
| 5                                  |       | 0.00990                 | 0.01815 | 0.01485 | 0.03466 | 0.03136 | 0.03136 | 0.02641 | 0.02146 | 0.01981 | 0.01485 | 0.00660 | 0.02641 | 0.04126 | 0.01815 | 0.01650 | 0.01485 | 0.34659  | 0.00000 | 0.34659  |
| 6                                  |       | 0.03466                 | 0.01485 | 0.02476 | 0.03796 | 0.02806 | 0.02476 | 0.02971 | 0.03631 | 0.02311 | 0.02311 | 0.03796 | 0.01650 | 0.04126 | 0.03466 | 0.03631 | 0.03466 | 0.47863  | 0.00000 | 0.47863  |
| 7                                  |       | 0.03136                 | 0.03136 | 0.02806 | 0.01815 | 0.02146 | 0.01155 | 0.01981 | 0.01981 | 0.02476 | 0.02806 | 0.01981 | 0.03301 | 0.01981 | 0.04291 | 0.04456 | 0.03796 | 0.43241  | 0.00000 | 0.43241  |
| 8                                  |       | 0.01981                 | 0.01485 | 0.02476 | 0.01155 | 0.01485 | 0.01320 | 0.00990 | 0.00825 | 0.01650 | 0.03301 | 0.01815 | 0.03466 | 0.03631 | 0.04126 | 0.03301 | 0.02806 | 0.35814  | 0.00000 | 0.35814  |
| 9                                  |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00000  |
| 10                                 |       | 0.09242                 | 0.08087 | 0.10233 | 0.06602 | 0.07097 | 0.04951 | 0.05281 | 0.08252 | 0.12213 | 0.16174 | 0.13203 | 0.10893 | 0.12543 | 0.18815 | 0.20135 | 0.14689 | 1.78412  | 0.00000 | 1.78412  |
| 11                                 |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00825 | 0.00990 | 0.01650 | 0.01981 | 0.01320 | 0.00000 | 0.01320 | 0.01815 | 0.00825 | 0.00165 | 0.10893  | 0.00000 | 0.10893  |
| 3 (C)                              |       | 2                       | 0.00000 | 0.00000 | 0.00000 | 0.00330 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00660 | 0.00000  |
|                                    | 3     | 0.00000                 | 0.00165 | 0.00165 | 0.00495 | 0.00825 | 0.00330 | 0.00495 | 0.00000 | 0.00165 | 0.00330 | 0.00000 | 0.00000 | 0.00330 | 0.00000 | 0.00165 | 0.00165 | 0.03631  | 0.00000 | 0.03631  |
|                                    | 4     | 0.00495                 | 0.02146 | 0.00825 | 0.01650 | 0.01981 | 0.01485 | 0.01650 | 0.01155 | 0.01320 | 0.00990 | 0.00990 | 0.00660 | 0.00660 | 0.00660 | 0.00000 | 0.00495 | 0.17165  | 0.00000 | 0.17165  |
|                                    | 5     | 0.03631                 | 0.03136 | 0.02971 | 0.02806 | 0.03961 | 0.03796 | 0.04291 | 0.03631 | 0.02641 | 0.02311 | 0.02476 | 0.02641 | 0.06107 | 0.03961 | 0.02971 | 0.02971 | 0.54299  | 0.00000 | 0.54299  |
|                                    | 6     | 0.02971                 | 0.02476 | 0.04126 | 0.03961 | 0.03631 | 0.02806 | 0.03301 | 0.02806 | 0.02641 | 0.01981 | 0.03136 | 0.04951 | 0.04621 | 0.06602 | 0.05116 | 0.02806 | 0.57930  | 0.00000 | 0.57930  |
|                                    | 7     | 0.02476                 | 0.02641 | 0.02146 | 0.02971 | 0.04456 | 0.02146 | 0.02476 | 0.02806 | 0.02806 | 0.03796 | 0.03961 | 0.05942 | 0.05611 | 0.04621 | 0.05281 | 0.05281 | 0.59416  | 0.00000 | 0.59416  |
|                                    | 8     | 0.02806                 | 0.02146 | 0.04291 | 0.00825 | 0.00495 | 0.01320 | 0.00990 | 0.01981 | 0.02971 | 0.02806 | 0.03796 | 0.03631 | 0.03961 | 0.07097 | 0.05942 | 0.04456 | 0.49513  | 0.00000 | 0.49513  |
|                                    | 9     | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00000  |
|                                    | 10    | 0.10563                 | 0.08417 | 0.12873 | 0.07757 | 0.08912 | 0.06107 | 0.06932 | 0.11058 | 0.15679 | 0.18320 | 0.18485 | 0.18815 | 0.17660 | 0.25582 | 0.26077 | 0.16834 | 2.30071  | 0.00000 | 2.30071  |
|                                    | 11    | 0.00165                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.01485 | 0.01155 | 0.01815 | 0.06272 | 0.00495 | 0.00825 | 0.03961 | 0.00825 | 0.00495 | 0.18485  | 0.00000 | 0.18485  |
|                                    | 4 (D) | 2                       | 0.00165 | 0.01155 | 0.01485 | 0.00990 | 0.01155 | 0.00165 | 0.00660 | 0.00330 | 0.00990 | 0.00165 | 0.00000 | 0.00660 | 0.00165 | 0.00330 | 0.01155 | 0.00330  | 0.09903 | 0.00000  |
| 3                                  |       | 0.02641                 | 0.03466 | 0.05116 | 0.07427 | 0.05116 | 0.02641 | 0.00990 | 0.01981 | 0.01155 | 0.01485 | 0.01981 | 0.02146 | 0.02806 | 0.04291 | 0.03961 | 0.03796 | 0.50999  | 0.00000 | 0.50999  |
| 4                                  |       | 0.05611                 | 0.06437 | 0.06272 | 0.07097 | 0.09242 | 0.03631 | 0.04456 | 0.02641 | 0.02641 | 0.02806 | 0.02311 | 0.05446 | 0.03631 | 0.06767 | 0.08417 | 0.07922 | 0.85328  | 0.00000 | 0.85328  |
| 5                                  |       | 0.17990                 | 0.11058 | 0.19970 | 0.18815 | 0.21126 | 0.11223 | 0.14359 | 0.10398 | 0.10728 | 0.07592 | 0.11553 | 0.14029 | 0.18815 | 0.17165 | 0.27232 | 0.21951 | 2.54002  | 0.00000 | 2.54002  |
| 6                                  |       | 0.15019                 | 0.15679 | 0.23931 | 0.31193 | 0.27397 | 0.13369 | 0.14029 | 0.17660 | 0.09242 | 0.08417 | 0.19310 | 0.19640 | 0.26077 | 0.26242 | 0.28718 | 0.25582 | 3.21505  | 0.00000 | 3.21505  |
| 7                                  |       | 0.21291                 | 0.18815 | 0.27727 | 0.32514 | 0.21126 | 0.12708 | 0.13534 | 0.20630 | 0.12543 | 0.09738 | 0.25252 | 0.26407 | 0.34164 | 0.35154 | 0.34659 | 0.26902 | 3.73164  | 0.00000 | 3.73164  |
| 8                                  |       | 0.15184                 | 0.17660 | 0.25747 | 0.22116 | 0.16834 | 0.12048 | 0.13369 | 0.17000 | 0.15349 | 0.14194 | 0.26572 | 0.22611 | 0.25417 | 0.29378 | 0.31028 | 0.20135 | 3.24641  | 0.00000 | 3.24641  |
| 9                                  |       | 0.00000                 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000  | 0.00000 | 0.00000  |
| 10                                 |       | 0.72619                 | 0.96055 | 1.41277 | 1.16851 | 0.79386 | 0.55950 | 0.68988 | 0.90444 | 0.98366 | 1.00347 | 1.29394 | 1.05958 | 1.53326 | 1.81053 | 1.48209 | 1.15201 | 17.53425 | 0.00000 | 17.53425 |
| 11                                 |       | 0.02146                 | 0.02311 | 0.04456 | 0.01485 | 0.01320 | 0.06932 | 0.11718 | 0.15184 | 0.32018 | 0.61231 | 0.16339 | 0.08252 | 0.23436 | 0.37960 | 0.10893 | 0.11553 | 2.47236  | 0.00000 | 2.47236  |
| 5 (E)                              |       | 2                       | 0.00495 | 0.00660 | 0.01320 | 0.01320 | 0.00825 | 0.00165 | 0.00165 | 0.00165 | 0.00330 | 0.00165 | 0.00330 | 0.00165 | 0.00660 | 0.01485 | 0.00825 | 0.00825  | 0.09903 | 0.00165  |
|                                    | 3     | 0.02146                 | 0.02806 | 0.02641 | 0.02641 | 0.01981 | 0.01815 | 0.01155 | 0.00990 | 0.00825 | 0.00660 | 0.00825 | 0.01650 | 0.01815 | 0.01981 | 0.02641 | 0.02641 | 0.29213  | 0.00000 | 0.29213  |
|                                    | 4     | 0.04291                 | 0.02806 | 0.03631 | 0.04456 | 0.03961 | 0.02641 | 0.02146 | 0.02641 | 0.01650 | 0.01320 | 0.01650 | 0.01981 | 0.03631 | 0.01485 | 0.02971 | 0.02806 | 0.44067  | 0.00000 | 0.44067  |
|                                    | 5     | 0.13699                 | 0.09573 | 0.16504 | 0.19640 | 0.14524 | 0.07922 | 0.08747 | 0.07922 | 0.07262 | 0.03796 | 0.10728 | 0.10728 | 0.07262 | 0.12048 | 0.13534 | 0.10068 | 1.73956  | 0.00000 | 1.73956  |
|                                    | 6     | 0.18485                 | 0.15679 | 0.22116 | 0.41426 | 0.30533 | 0.12708 | 0.18650 | 0.20796 |         |         |         |         |         |         |         |         |          |         |          |

|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |          |
|-------|----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| 7 (G) | 2  | 0.00825 | 0.01155 | 0.00825 | 0.01155 | 0.00495 | 0.00660 | 0.00660 | 0.00330 | 0.00495 | 0.00990 | 0.00990 | 0.00660 | 0.00660 | 0.00660 | 0.00660 | 0.00660 | 0.11883 | 0.00330  |
|       | 3  | 0.00660 | 0.00660 | 0.01155 | 0.00990 | 0.00660 | 0.00495 | 0.01155 | 0.00825 | 0.01155 | 0.00660 | 0.01485 | 0.01320 | 0.00825 | 0.00990 | 0.00825 | 0.00990 | 0.14854 |          |
|       | 4  | 0.01155 | 0.00990 | 0.00660 | 0.00825 | 0.00660 | 0.00825 | 0.00660 | 0.02806 | 0.01815 | 0.02146 | 0.01155 | 0.02311 | 0.00660 | 0.00495 | 0.00330 | 0.00495 | 0.17990 |          |
|       | 5  | 0.04456 | 0.02476 | 0.02806 | 0.01815 | 0.01815 | 0.01485 | 0.02971 | 0.04621 | 0.05116 | 0.03961 | 0.03961 | 0.02311 | 0.02146 | 0.02311 | 0.02311 | 0.02311 | 0.46872 |          |
|       | 6  | 0.04291 | 0.03301 | 0.02971 | 0.01850 | 0.04126 | 0.02146 | 0.05281 | 0.02476 | 0.01650 | 0.02806 | 0.02146 | 0.02146 | 0.01155 | 0.02641 | 0.04126 | 0.04291 | 0.47203 |          |
|       | 7  | 0.05611 | 0.02476 | 0.01650 | 0.01485 | 0.03961 | 0.03136 | 0.03466 | 0.02971 | 0.00330 | 0.00495 | 0.02146 | 0.01815 | 0.04456 | 0.06272 | 0.05611 | 0.06272 | 0.52154 |          |
|       | 8  | 0.03631 | 0.01485 | 0.00990 | 0.00660 | 0.00990 | 0.04951 | 0.03631 | 0.01485 | 0.00330 | 0.00165 | 0.00660 | 0.02146 | 0.03301 | 0.08912 | 0.03796 | 0.03301 | 0.40436 |          |
|       | 9  | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |          |
|       | 10 | 0.11553 | 0.06602 | 0.04621 | 0.03136 | 0.07592 | 0.12873 | 0.12873 | 0.06272 | 0.01320 | 0.01981 | 0.05116 | 0.07922 | 0.19970 | 0.26572 | 0.15184 | 0.11553 | 1.55141 |          |
|       | 11 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00165 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00165 |          |
|       |    |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |         | 99.99505 |

3.870276

100

## Notes:

(1) Wind Speed Categories defined as follows:

| Category | Wind Speed (mph) |
|----------|------------------|
| Calm     | <0.8             |
| 2        | ≥ 0.80 - <2.35   |
| 3        | ≥ 2.35 - <3.47   |
| 4        | ≥ 3.47 - <4.56   |
| 5        | ≥ 4.56 - <6.82   |
| 6        | ≥ 6.82 - <9.06   |
| 7        | ≥ 9.06 - <11.30  |
| 8        | ≥ 11.30 - <13.53 |
| 9        | ≥ 13.53 - <18.01 |
| 10       | ≥ 18.01 - <22.40 |
| 11       | ≥ 22.40          |

## ATTACHMENT 6

### Braidwood and Byron Stations Measurement Uncertainty Recapture Technical Evaluation

#### Response to NRC Acceptance Review Questions

#### CD "Meteorological Data Files"

| File Name   | File Size: |
|-------------|------------|
| BRD94r3.met | 317 KB     |
| BRD95r3.met | 317 KB     |
| BRD96r3.met | 318 KB     |
| BRD97r3.met | 317 KB     |
| BRD98r3.met | 317 KB     |
| BYR94r4.met | 317 KB     |
| BYR95r4.met | 317 KB     |
| BYR96r4.met | 318 KB     |
| BYR97r4.met | 317 KB     |
| BYR98r4.met | 317 KB     |

**Sensitivity Level:** Publically Available

**Media:** CD-R

**Special Information:** Data file format is .met which is used by ARCON96, the data file is to be kept in native-format and the CD-R copy can be submitted to the Public Document Room.

## ATTACHMENT 7

### Braidwood and Byron Stations Measurement Uncertainty Recapture Technical Evaluation

#### Response to NRC Acceptance Review Questions

#### CD "PAVAN Input Files"

| File Name:       | File Size: |
|------------------|------------|
| BRDr2_11.inp.txt | 7 KB       |
| BYRr2_11.inp.txt | 7 KB       |

**Sensitivity Level:** Publically Available

**Media:** CD-R

**Special Information:** Data file format is .txt ASCII text which inputs into PAVAN, the data file is to be kept in native-format and the CD-R copy can be submitted to the Public Document Room.