Nuclear Operating Company
South Texas Project Electric Generating Station P.O. Box 289 Wadsworth, Texas 77483

June 29, 2006
NOC-AE-06002035

U. S. Nuclear Regulatory Commission
Attention: Document Control Desk
One White Flint North
11555 Rockville Pike
Rockville, MD 20852-2738

South Texas Project
Units 1 and 2
Docket No. STN 50-498 and STN 50-499
Core Operating Limits Reports

In accordance with Technical Specification 6.9.1.6.d, STP Nuclear Operating Company submits revised Core Operating Limits Reports for Unit 1 and for Unit 2. These revisions result from implementing the Westinghouse Best Estimate Analyzer for Core Operations – Nuclear (BEACON) power distribution monitoring system as approved by the NRC for use at the South Texas Project (ML06070501).

There are no commitments in this letter.

If there are any questions regarding this request, please contact John Conly at (361) 972-7336 or me at (361) 972-7795.

David J Hoppe
for David A. Leazar
Manager, Fuels & Analysis

jtc

Attachments: Unit 1 Cycle 13 Core Operating Limits Report, Revision 1
Unit 2 Cycle 12 Core Operating Limits Report, Revision 1

A001

STI: 32022440

cc:

(paper copy)

Regional Administrator, Region IV
U. S. Nuclear Regulatory Commission
611 Ryan Plaza Drive, Suite 400
Arlington, Texas 76011-8064

Richard A. Ratliff
Bureau of Radiation Control
Texas Department of State Health Services
1100 West 49th Street
Austin, TX 78756-3189

Senior Resident Inspector
U. S. Nuclear Regulatory Commission
P. O. Box 289, Mail Code: MN116
Wadsworth, TX 77483

C. M. Canady
City of Austin
Electric Utility Department
721 Barton Springs Road
Austin, TX 78704

(electronic copy)

A. H. Gutterman, Esquire
Morgan, Lewis & Bockius LLP

Mohan C. Thadani
U. S. Nuclear Regulatory Commission

Steve Winn
Christine Jacobs
Eddy Daniels
NRG South Texas LP

J. J. Nesrsta
R. K. Temple
E. Alarcon
City Public Service

Jon C. Wood
Cox Smith Matthews

C. Kirksey
City of Austin

SOUTH TEXAS PROJECT

Unit 1 Cycle 13

CORE OPERATING LIMITS REPORT

Revision 1

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report for STPEGS Unit 1 Cycle 13 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

1)	2.1	SAFETY LIMITS
2)	2.2	LIMITING SAFETY SYSTEM SETTINGS
3)	3/4.1.1.1	SHUTDOWN MARGIN
4)	3/4.1.1.3	MODERATOR TEMPERATURE COEFFICIENT LIMITS
5)	3/4.1.3.5	SHUTDOWN ROD INSERTION LIMITS
6)	3/4.1.3.6	CONTROL ROD INSERTION LIMITS
7)	3/4.2.1	AFD LIMITS
8)	3/4.2.2	HEAT FLUX HOT CHANNEL FACTOR
9)	3/4.2.3	NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR
10)	3/4.2.5	DNB PARAMETERS

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

2.1 SAFETY LIMITS (Specification 2.1):

2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature (T_{avg}) shall not exceed the limits shown in Figure 1.

2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.

2.2.2 The Over-temperature ΔT and Over-power ΔT setpoint parameter values are listed below:

Over-temperature ΔT Setpoint Parameter Values

τ_1 measured reactor vessel ΔT lead/lag time constant, τ_1 = 8 sec
τ_2 measured reactor vessel ΔT lead/lag time constant, τ_2 = 3 sec
τ_3 measured reactor vessel ΔT lag time constant, τ_3 = 2 sec
τ_4 measured reactor vessel average temperature lead/lag time constant, τ_4 = 28 sec
τ_5 measured reactor vessel average temperature lead/lag time constant, τ_5 = 4 sec
τ_6 measured reactor vessel average temperature lag time constant, τ_6 = 2 sec
K_1 Overtemperature ΔT reactor trip setpoint, K_1 = 1.14
K_2 Overtemperature ΔT reactor trip setpoint T_{avg} coefficient, K_2 = 0.028/°F
K_3 Overtemperature ΔT reactor trip setpoint pressure coefficient, K_3 = 0.00143/psig
T' Nominal full power T_{avg}, T' ≤ 592.0 °F
P' Nominal RCS pressure, P' = 2235 psig
$f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

(1) For $q_t - q_b$ between -70% and +8%, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;

(2) For each percent that the magnitude of $q_t - q_b$ exceeds -70%, the ΔT Trip Setpoint shall be automatically reduced by 0.0% of its value at RATED THERMAL POWER; and

(3) For each percent that the magnitude of $q_t - q_b$ exceeds +8%, the ΔT Trip Setpoint shall be automatically reduced by 2.65% of its value at RATED THERMAL POWER.

Over-power ΔT Setpoint Parameter Values

τ_1 measured reactor vessel ΔT lead/lag time constant, τ_1 = 8 sec
τ_2 measured reactor vessel ΔT lead/lag time constant, τ_2 = 3 sec
τ_3 measured reactor vessel ΔT lag time constant, τ_3 = 2 sec
τ_6 measured reactor vessel average temperature lag time constant, τ_6 = 2 sec
τ_7 Time constant utilized in the rate-lag compensator for T_{avg}, τ_7 = 10 sec
K_4 Overpower ΔT reactor trip setpoint, K_4 = 1.08
K_5 Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient, K_5 = 0.02/°F for increasing average temperature, and K_5 = 0 for decreasing average temperature
K_6 Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 = 0.002/°F for T > T'', and K_6 = 0 for T ≤ T''
T'' Indicated full power T_{avg}, T'' ≤ 592.0 °F
$f_2(\Delta I)$ = 0 for all (ΔI)

2.3 SHUTDOWN MARGIN (Specification 3.1.1.1):

The SHUTDOWN MARGIN shall be:

2.3.1 Greater than 1.3% $\Delta\rho$ for MODES 1 and 2*
*See Special Test Exception 3.10.1

2.3.2 Greater than the limits in Figure 2 for MODES 3 and 4.

2.3.3 Greater than the limits in Figure 3 for MODE 5.

2.4 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):

2.4.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 4.

2.4.2 The EOL, ARO, HFP, MTC shall be less negative than –62.6 pcm/°F.

2.4.3 The 300 ppm, ARO, HFP, MTC shall be less negative than –53.6 pcm/°F (300 ppm Surveillance Limit).

Where: BOL stands for Beginning-of-Cycle Life,
EOL stands for End-of-Cycle Life,
ARO stands for All Rods Out,
HFP stands for Hot Full Power (100% RATED THERMAL POWER),
HFP vessel average temperature is 592 °F.

2.4.4 The Revised Predicted near-EOL 300 ppm MTC shall be calculated using the algorithm from T.S. 6.9.1.6.b.10:

Revised Predicted MTC = Predicted MTC + AFD Correction - 3 pcm/°F

If the Revised Predicted MTC is less negative than the S.R. 4.1.1.3b limit and all of the benchmark data contained in the surveillance procedure are met, then an MTC measurement in accordance with S.R. 4.1.1.3b is not required.

2.5 ROD INSERTION LIMITS (Specification 3.1.3.5 and 3.1.3.6):

2.5.1 All banks shall have the same Full Out Position (FOP) of at least 250 steps withdrawn but not exceeding 259 steps withdrawn.

2.5.2 The Control Banks shall be limited in physical insertion as specified in Figure 5.

2.5.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

2.6 AXIAL FLUX DIFFERENCE (Specification 3.2.1):

2.6.1 AFD limits as required by Technical Specification 3.2.1 are determined by CAOC Operations with an AFD target band of +5, -10%.

2.6.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 6, as required by Technical Specifications.

2.7 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):

2.7.1 $F_Q^{RTP} = 2.55$.

2.7.2 K(Z) is provided in Figure 7.

2.7.3 The F_{xy} limits for RATED THERMAL POWER (F_{xy}^{RTP}) within specific core planes shall be:

2.7.3.1 Less than or equal to 2.102 for all cycle burnups for all core planes containing Bank "D" control rods, and

2.7.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.

2.7.3.3 $PF_{xy} = 0.2$.

These F_{xy} limits were used to confirm that the heat flux hot channel factor $F_Q(Z)$ will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these F_{xy} limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

2.7.4 Core Power Distribution Measurement Uncertainty for the Heat Flux Hot Channel Factor

2.7.4.1 If the Power Distribution Monitoring System(PDMS) is operable, as defined in the Technical Requirements Manual, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ using the PDMS shall be calculated by:

$$U_{FQ} = (1.0 + (U_Q/100))*U_E$$

Where:

$U_Q =$ Uncertainty for power peaking factor as defined in Equation 5-19 of Reference 3.6

$U_E =$ Engineering uncertainty factor of 1.03.

This uncertainty is calculated and applied automatically by the BEACON computer code.

2.7.4.2 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ shall be calculated by:

$$U_{FQ} = U_{QU} * U_E$$

Where:

U_{QU} = Base F_Q measurement uncertainty of 1.05.
U_E = Engineering uncertainty factor of 1.03.

2.8 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.8.1 $F_{\Delta H}^{RTP} = 1.62$ [1]

2.8.2 $PF_{\Delta H} = 0.3$

2.8.3 Core Power Distribution Measurement Uncertainty for the Enthalpy Rise Hot Channel Factor

2.8.3.1 If the Power Distribution Monitoring System(PDMS) is operable, as defined in the Technical Requirements Manual, the core power distribution measurement uncertainty ($U_{F\Delta H}$) to be applied to the $F_{\Delta H}^{N}$ using the PDMS shall be calculated by:

$$U_{F\Delta H} = 1.0 + (U_{\Delta H}/100)$$

Where:

$U_{\Delta H}$ = Uncertainty for power peaking factor as defined in Equation 5-19 of Reference 3.6

This uncertainty is calculated and applied automatically by the BEACON computer code.

2.8.3.2 If the moveable detector system is used, the core power distribution measurement uncertainty ($U_{F\Delta H}$) shall be:

$$U_{F\Delta H} = 1.04$$

[1] Applies to all fuel in the Unit 1 Cycle 13 Core.

2.9 **DNB PARAMETERS (Specification 3.2.5):**

2.9.1 The following DNB-related parameters shall be maintained within the following limits:[1]

2.9.1.1 Reactor Coolant System T_{avg}, ≤ 595 °F[2],

2.9.1.2 Pressurizer Pressure, > 2200 psig[3],

2.9.1.3 Minimum Measured Reactor Coolant System Flow[4] > 403,000 gpm.

3.0 REFERENCES

3.1 Letter from D. E. Robinson (Westinghouse) to D. F. Hoppes (STPNOC), "Unit 1 Cycle 13 Final Reload Evaluation (RE) Revision 1," ST-UB-NOC-05002532, Rev. 1, March 29 2005.

3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.

3.3 STPNOC Calculation ZC-7035, Rev. 2, "Loop Uncertainty Calculation for RCS Tavg Instrumentation," Section 10.1, effective July 22, 2003.

3.4 STPNOC Calculation ZC-7032, Rev. 4, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," Section 2.3, Page 9, effective July 22, 2003.

3.5 Condition Report Engineering Evaluation 03-6461-9, Revision 0, "Reload Safety Evaluation and Core Operating Limits Report for South Texas Unit 1 Cycle 13 Modes 1, 2, 3, 4, and 5."

3.6 WCAP-12472-P-A, BEACON Core Monitoring and Operations Support System, August 1994.

---

1 A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

2 Includes a 1.9 °F measurement uncertainty per Reference 3.3.

3 Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Includes a 9.6 PSI measurement uncertainty as read on QDPS display per Reference 3.4.

4 Includes a 2.8% flow measurement uncertainty.

Figure 1

Reactor Core Safety Limits - Four Loops in Operation

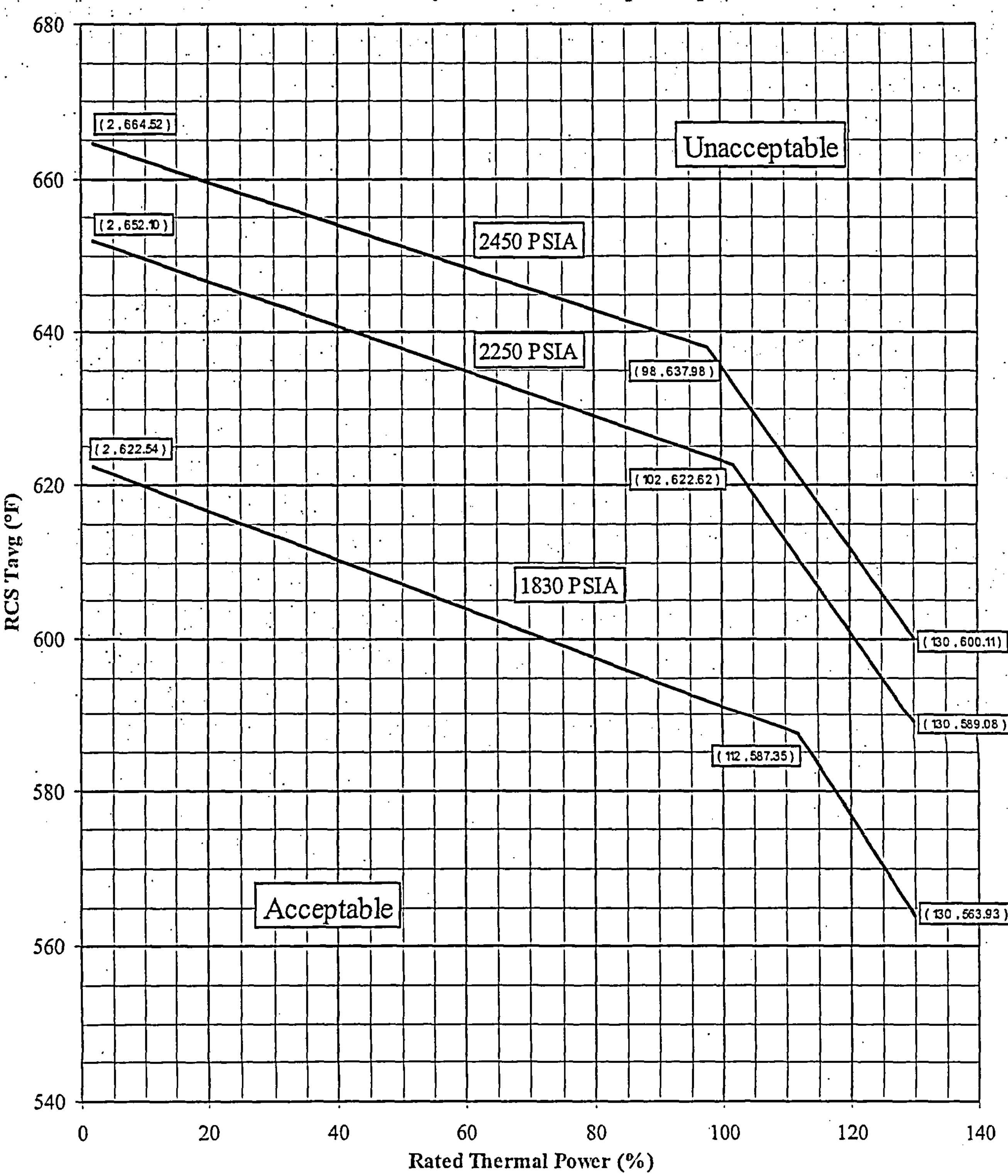


Figure 2

Required Shutdown Margin for Modes 3 & 4

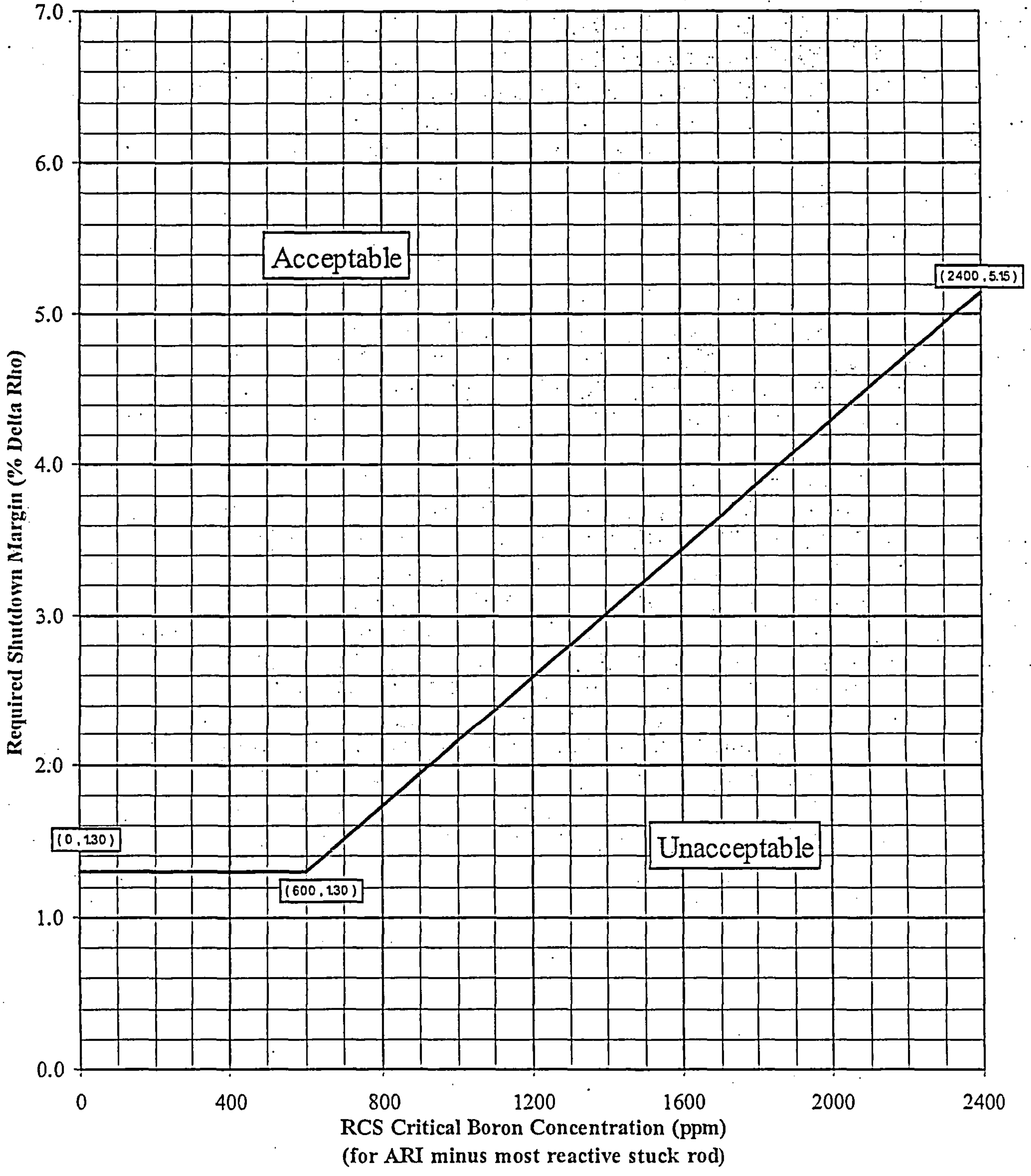
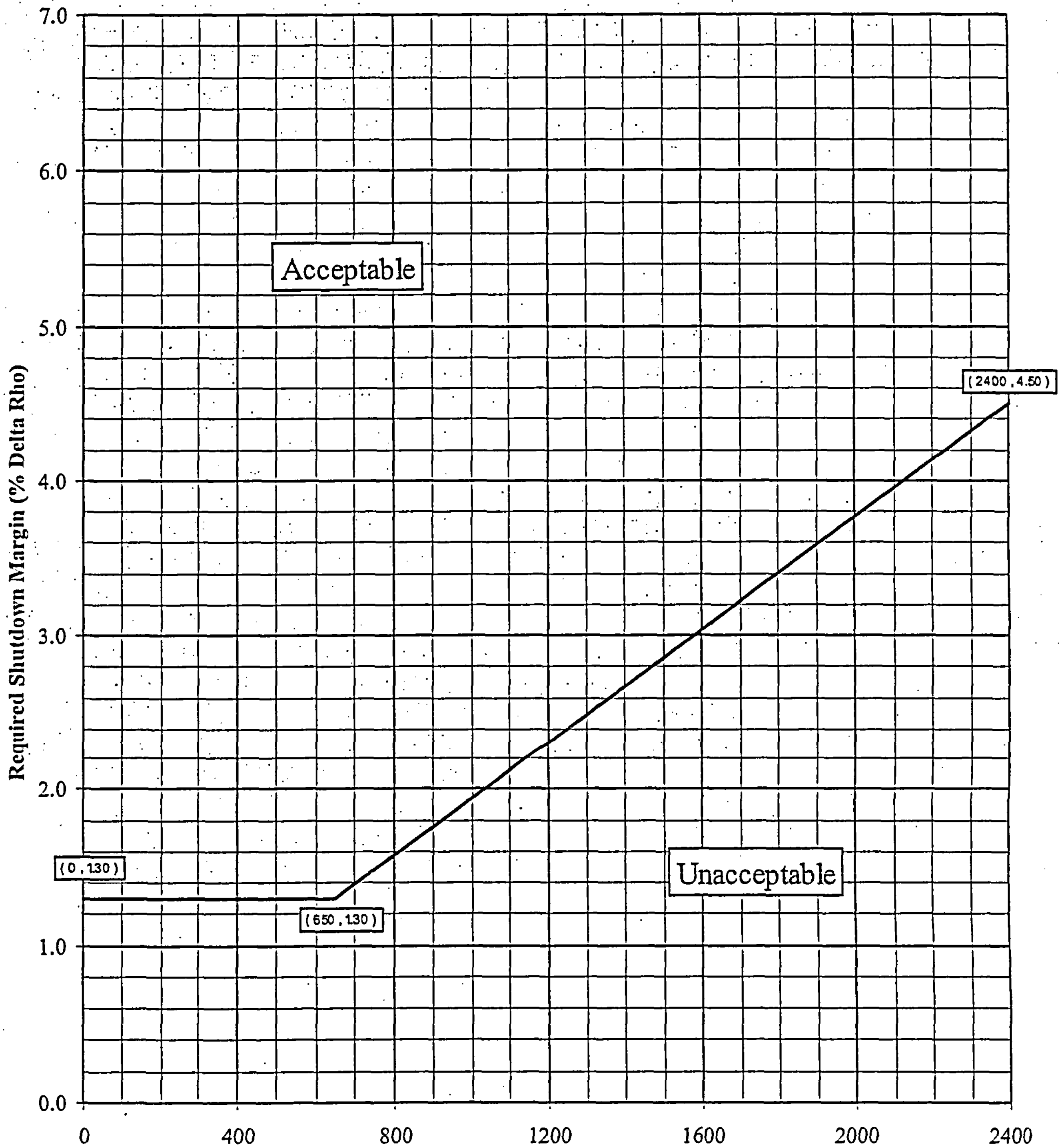


Figure 3

Required Shutdown Margin for Mode 5



RCS Critical Boron Concentration (ppm)
(for ARI minus most reactive stuck rod)

Figure 4

MTC versus Power Level

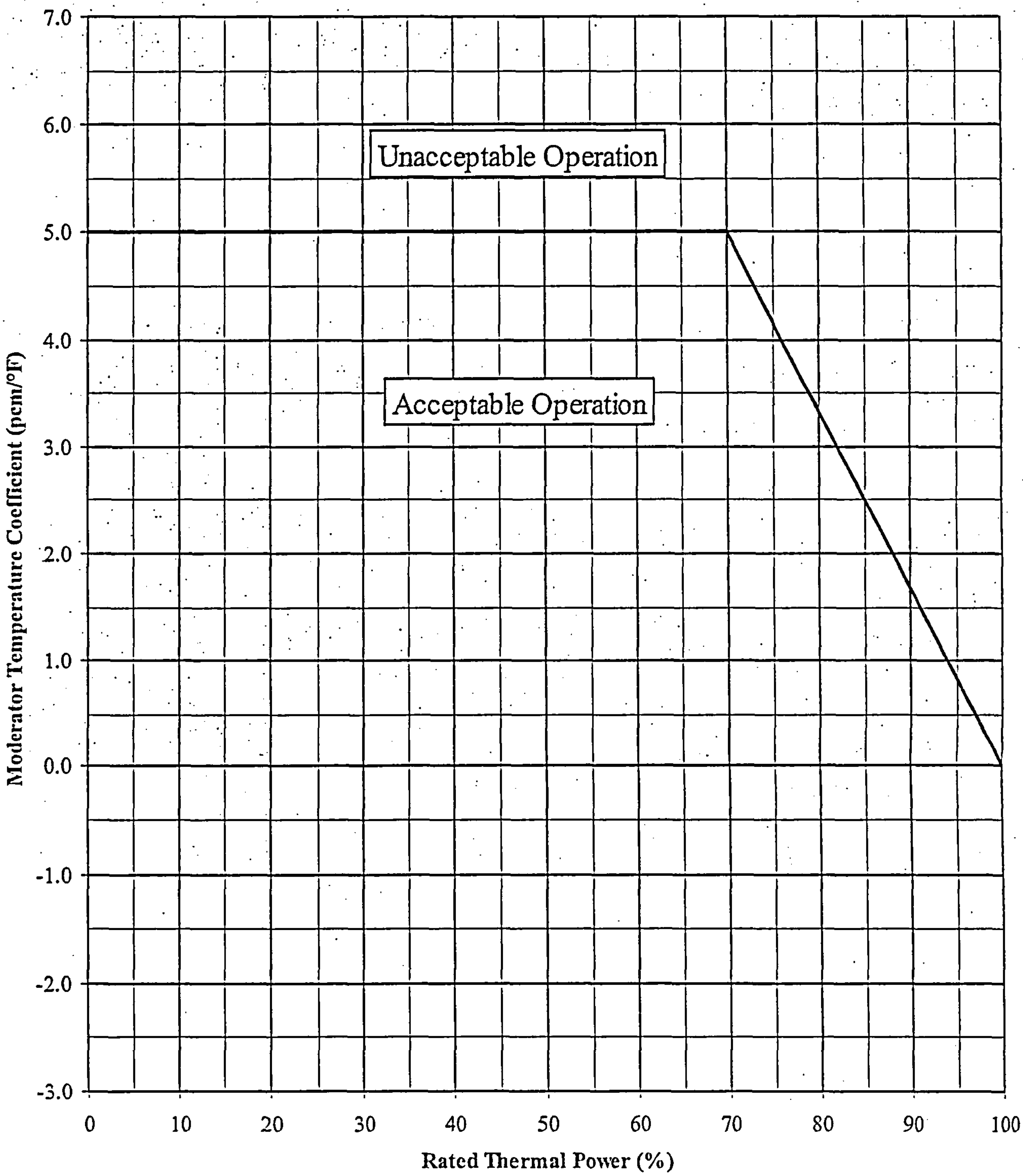


Figure 5

Control Rod Insertion Limits* versus Power Level

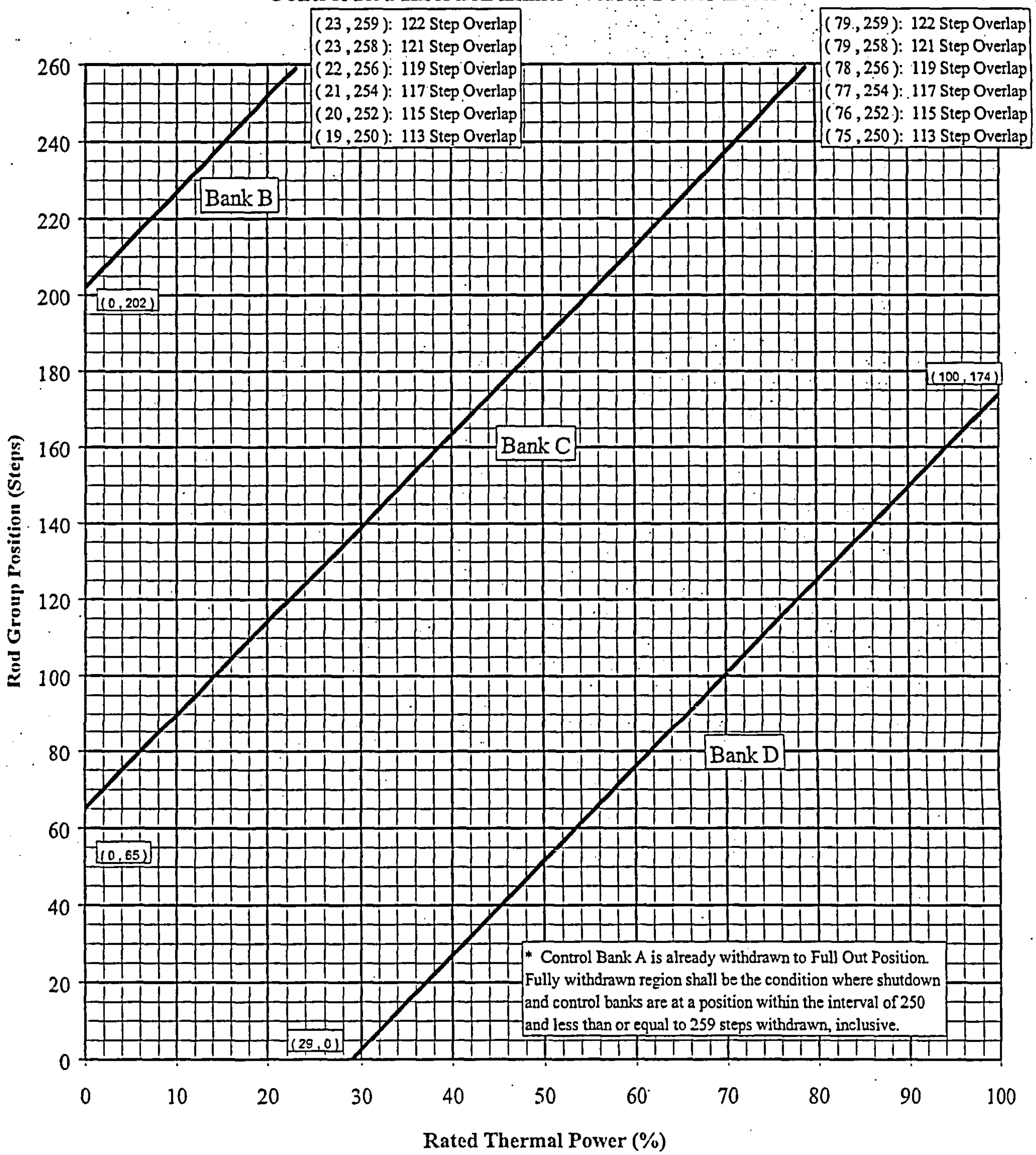


Figure 6

AFD Limits versus Power Level

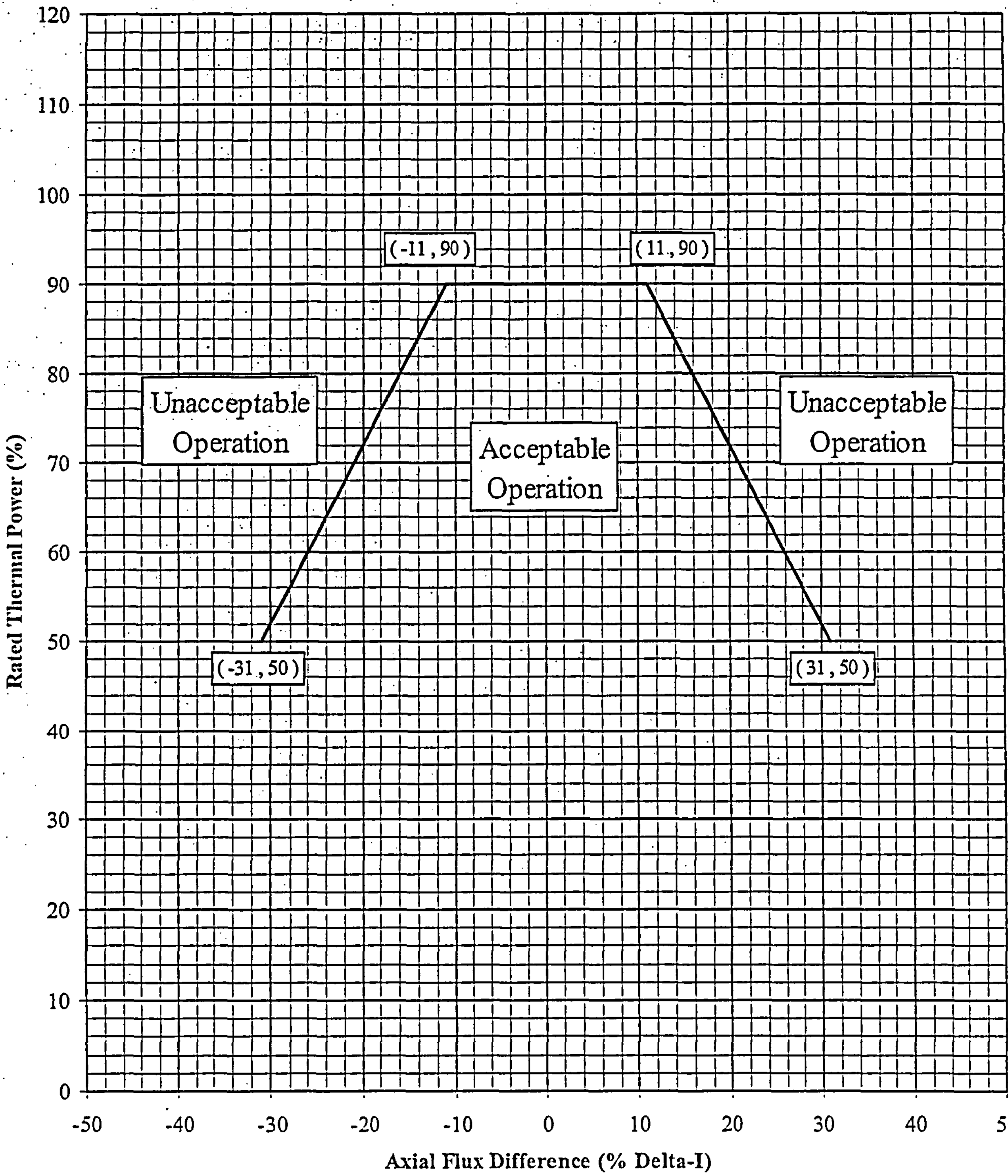
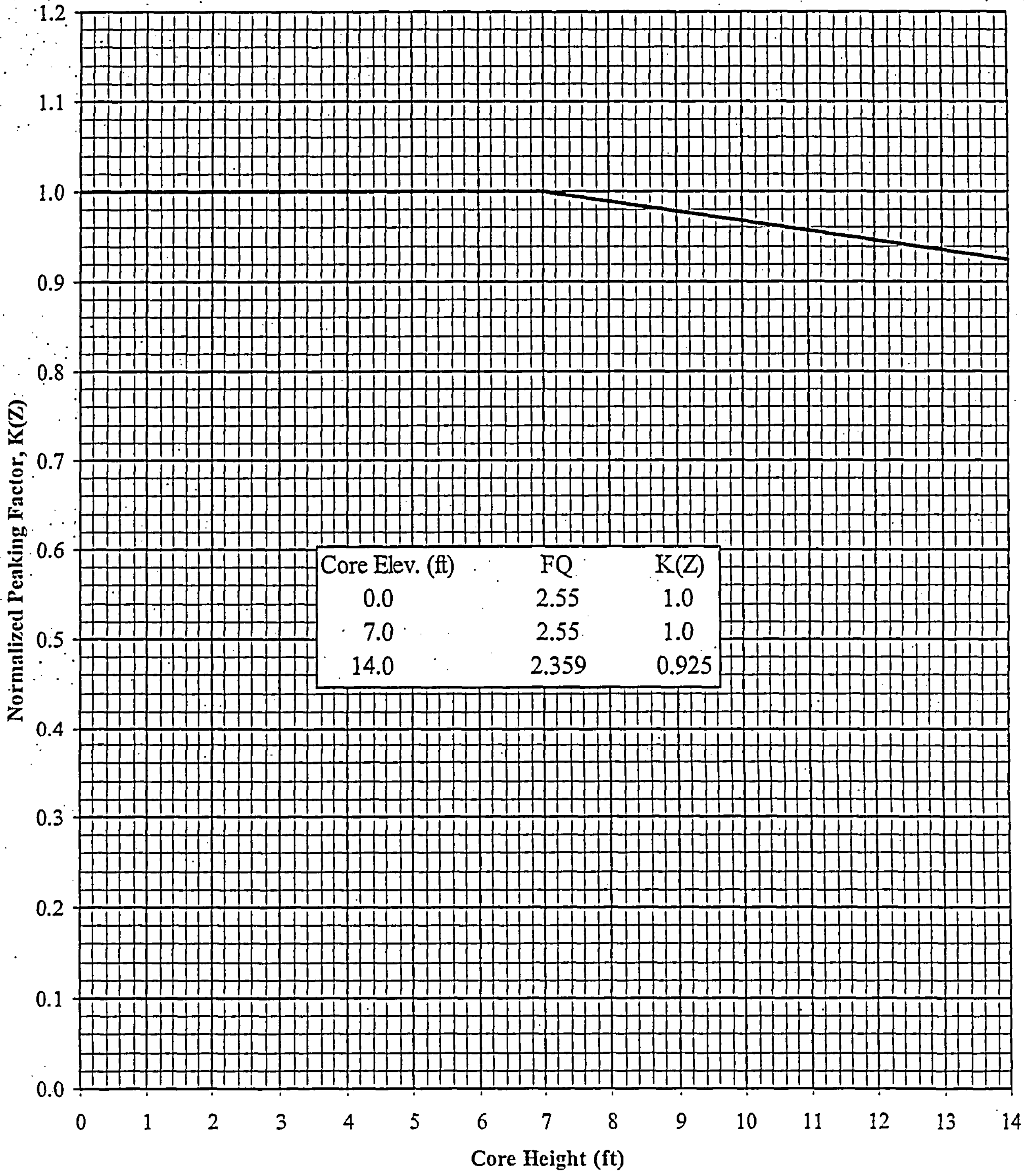


Figure 7

K(Z) - Normalized FQ(Z) versus Core Height



Core Elev. (ft)	FQ	K(Z)
0.0	2.55	1.0
7.0	2.55	1.0
14.0	2.359	0.925

Table 1 (Part 1 of 2)

Unrodded F_{xy} for Each Core Height

for Cycle Burnups Less Than 10500 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	4.633	6.80	37	1.872
13.80	2	3.954	6.60	38	1.861
13.60	3	3.275	6.40	39	1.853
13.40	4	2.596	6.20	40	1.845
13.20	5	2.276	6.00	41	1.841
13.00	6	2.068	5.80	42	1.840
12.80	7	2.070	5.60	43	1.839
12.60	8	2.046	5.40	44	1.840
12.40	9	2.023	5.20	45	1.844
12.20	10	1.995	5.00	46	1.850
12.00	11	1.979	4.80	47	1.860
11.80	12	1.971	4.60	48	1.870
11.60	13	1.971	4.40	49	1.878
11.40	14	1.975	4.20	50	1.885
11.20	15	1.979	4.00	51	1.890
11.00	16	1.984	3.80	52	1.893
10.80	17	1.984	3.60	53	1.893
10.60	18	1.984	3.40	54	1.895
10.40	19	1.982	3.20	55	1.899
10.20	20	1.985	3.00	56	1.904
10.00	21	1.987	2.80	57	1.903
9.80	22	1.989	2.60	58	1.911
9.60	23	1.997	2.40	59	1.921
9.40	24	2.003	2.20	60	1.932
9.20	25	2.011	2.00	61	1.929
9.00	26	2.017	1.80	62	1.920
8.80	27	2.023	1.60	63	1.905
8.60	28	2.027	1.40	64	1.907
8.40	29	2.032	1.20	65	1.909
8.20	30	2.037	1.00	66	1.920
8.00	31	2.033	0.80	67	1.994
7.80	32	2.016	0.60	68	2.124
7.60	33	1.983	0.40	69	2.281
7.40	34	1.945	0.20	70	2.439
7.20	35	1.911	0.00	71	2.596
7.00	36	1.889			

Table 1 (Part 2 of 2)

Unrodded Fxy for Each Core Height

for Cycle Burnups Greater Than or Equal to 10500 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	4.778	6.80	37	2.144
13.80	2	4.129	6.60	38	2.139
13.60	3	3.480	6.40	39	2.127
13.40	4	2.831	6.20	40	2.115
13.20	5	2.450	6.00	41	2.101
13.00	6	2.153	5.80	42	2.089
12.80	7	2.149	5.60	43	2.077
12.60	8	2.121	5.40	44	2.067
12.40	9	2.096	5.20	45	2.057
12.20	10	2.055	5.00	46	2.047
12.00	11	2.032	4.80	47	2.038
11.80	12	2.026	4.60	48	2.028
11.60	13	2.019	4.40	49	2.017
11.40	14	2.022	4.20	50	2.006
11.20	15	2.027	4.00	51	1.994
11.00	16	2.031	3.80	52	1.982
10.80	17	2.033	3.60	53	1.969
10.60	18	2.035	3.40	54	1.957
10.40	19	2.036	3.20	55	1.945
10.20	20	2.041	3.00	56	1.931
10.00	21	2.048	2.80	57	1.916
9.80	22	2.056	2.60	58	1.891
9.60	23	2.065	2.40	59	1.858
9.40	24	2.072	2.20	60	1.841
9.20	25	2.078	2.00	61	1.839
9.00	26	2.084	1.80	62	1.835
8.80	27	2.089	1.60	63	1.836
8.60	28	2.095	1.40	64	1.853
8.40	29	2.100	1.20	65	1.853
8.20	30	2.106	1.00	66	1.877
8.00	31	2.112	0.80	67	2.127
7.80	32	2.119	0.60	68	2.605
7.60	33	2.127	0.40	69	3.195
7.40	34	2.135	0.20	70	3.786
7.20	35	2.142	0.00	71	4.377
7.00	36	2.145			

Nuclear Operating Company

SOUTH TEXAS PROJECT

Unit 2 Cycle 12

CORE OPERATING LIMITS REPORT

Revision 1

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report for STPEGS Unit 2 Cycle 12 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

1)	2.1	SAFETY LIMITS
2)	2.2	LIMITING SAFETY SYSTEM SETTINGS
3)	3/4.1.1.1	SHUTDOWN MARGIN
4)	3/4.1.1.3	MODERATOR TEMPERATURE COEFFICIENT LIMITS
5)	3/4.1.3.5	SHUTDOWN ROD INSERTION LIMITS
6)	3/4.1.3.6	CONTROL ROD INSERTION LIMITS
7)	3/4.2.1	AFD LIMITS
8)	3/4.2.2	HEAT FLUX HOT CHANNEL FACTOR
9)	3/4.2.3	NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR
10)	3/4.2.5	DNB PARAMETERS

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

2.1 SAFETY LIMITS (Specification 2.1):

2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature (T_{avg}) shall not exceed the limits shown in Figure 1.

2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.

2.2.2 The Over-temperature ΔT and Over-power ΔT setpoint parameter values are listed below:

Over-temperature ΔT Setpoint Parameter Values

τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
τ_4 measured reactor vessel average temperature lead/lag time constant, $\tau_4 = 28$ sec
τ_5 measured reactor vessel average temperature lead/lag time constant, $\tau_5 = 4$ sec
τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
K_1 Overtemperature ΔT reactor trip setpoint, $K_1 = 1.14$
K_2 Overtemperature ΔT reactor trip setpoint T_{avg} coefficient, $K_2 = 0.028/°F$
K_3 Overtemperature ΔT reactor trip setpoint pressure coefficient, $K_3 = 0.00143/psig$
T' Nominal full power T_{avg}, $T' \leq 592.0$ °F
P' Nominal RCS pressure, P' = 2235 psig
$f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

(1) For $q_t - q_b$ between -70% and +8%, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;

(2) For each percent that the magnitude of $q_t - q_b$ exceeds -70%, the ΔT Trip Setpoint shall be automatically reduced by 0.0% of its value at RATED THERMAL POWER; and

(3) For each percent that the magnitude of $q_t - q_b$ exceeds +8%, the ΔT Trip Setpoint shall be automatically reduced by 2.65% of its value at RATED THERMAL POWER.

Over-power ΔT Setpoint Parameter Values

τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 2$ sec
τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 2$ sec
τ_7 Time constant utilized in the rate-lag compensator for T_{avg}, $\tau_7 = 10$ sec
K_4 Overpower ΔT reactor trip setpoint, $K_4 = 1.08$
K_5 Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient, $K_5 = 0.02/°F$ for increasing average temperature, and $K_5 = 0$ for decreasing average temperature
K_6 Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient $K_6 = 0.002/°F$ for $T > T''$, and $K_6 = 0$ for $T \leq T''$
T'' Indicated full power T_{avg}, $T'' \leq 592.0$ °F
$f_2(\Delta I) = 0$ for all (ΔI)

2.3 SHUTDOWN MARGIN (Specification 3.1.1.1):

The SHUTDOWN MARGIN shall be:

2.3.1 Greater than 1.3% $\Delta\rho$ for MODES 1 and 2*
*See Special Test Exception 3.10.1

2.3.2 Greater than the limits in Figure 2 for MODES 3 and 4.

2.3.3 Greater than the limits in Figure 3 for MODE 5.

2.4 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):

2.4.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 4.

2.4.2 The EOL, ARO, HFP, MTC shall be less negative than –62.6 pcm/°F.

2.4.3 The 300 ppm, ARO, HFP, MTC shall be less negative than –53.6 pcm/°F (300 ppm Surveillance Limit).

Where: BOL stands for Beginning-of-Cycle Life,
EOL stands for End-of-Cycle Life,
ARO stands for All Rods Out,
HFP stands for Hot Full Power (100% RATED THERMAL POWER),
HFP vessel average temperature is 592 °F.

2.4.4 The Revised Predicted near-EOL 300 ppm MTC shall be calculated using the algorithm from T.S. 6.9.1.6.b.10:

Revised Predicted MTC = Predicted MTC + AFD Correction - 3 pcm/°F

If the Revised Predicted MTC is less negative than the S.R. 4.1.1.3b limit and all of the benchmark data contained in the surveillance procedure are met, then an MTC measurement in accordance with S.R. 4.1.1.3b is not required.

2.5 ROD INSERTION LIMITS (Specification 3.1.3.5 and 3.1.3.6):

2.5.1 All banks shall have the same Full Out Position (FOP) of either 255 steps withdrawn or 259 steps withdrawn.

2.5.2 The Control Banks shall be limited in physical insertion as specified in Figure 5.

2.5.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

2.6 AXIAL FLUX DIFFERENCE (Specification 3.2.1):

2.6.1 AFD limits as required by Technical Specification 3.2.1 are determined by CAOC Operations with an AFD target band of +5, -10%.

2.6.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 6, as required by Technical Specifications.

2.7 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):

2.7.1 $F_Q^{RTP} = 2.55$.

2.7.2 K(Z) is provided in Figure 7.

2.7.3 The F_{xy} limits for RATED THERMAL POWER (F_{xy}^{RTP}) within specific core planes shall be:

2.7.3.1 Less than or equal to 2.102 for all cycle burnups for all core planes containing Bank "D" control rods, and

2.7.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.

2.7.3.3 $PF_{xy} = 0.2$.

These F_{xy} limits were used to confirm that the heat flux hot channel factor $F_Q(Z)$ will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these F_{xy} limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

2.7.4 Core Power Distribution Measurement Uncertainty for the Heat Flux Hot Channel Factor

2.7.4.1 If the Power Distribution Monitoring System(PDMS) is operable, as defined in the Technical Requirements Manual, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ using the PDMS shall be calculated by:

2.7.4.2 $\mathbf{U_{FQ} = (1.0 + (U_Q/100))*U_E}$

Where:

U_Q = Uncertainty for power peaking factor as defined in Equation 5-19 of Reference 3.6

U_E = Engineering uncertainty factor of 1.03.

This uncertainty is calculated and applied automatically by the BEACON computer code.

2.7.4.3 If the moveable detector system is used, the core power distribution measurement uncertainty (U_{FQ}) to be applied to the $F_Q(Z)$ and $F_{xy}(Z)$ shall be calculated by:

$U_{FQ} = U_{QU} * U_E$

Where:

U_{QU} = Base F_Q measurement uncertainty of 1.05.
U_E = Engineering uncertainty factor of 1.03.

2.8 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.8.1 $F_{\Delta H}^{RTP} = 1.62$[1]

2.8.2 $PF_{\Delta H} = 0.3$

2.8.3 Core Power Distribution Measurement Uncertainty for the Enthalpy Rise Hot Channel Factor

2.8.3.1 If the Power Distribution Monitoring System (PDMS) is operable, as defined in the Technical Requirements Manual, the core power distribution measurement uncertainty ($U_{F\Delta H}$) to be applied to the $F_{\Delta H}^{N}$ using the PDMS shall be calculated by:

$U_{F\Delta H} = 1.0 + (U_{\Delta H}/100)$

Where:

$U_{\Delta H}$ = Uncertainty for power peaking factor as defined in Equation 5-19 of Reference 3.6

This uncertainty is calculated and applied automatically by the BEACON computer code.

2.8.3.2 If the moveable detector system is used, the core power distribution measurement uncertainty ($U_{F\Delta H}$) shall be:

$U_{F\Delta H} = 1.04$

[1] Applies to all fuel in the Unit 2 Cycle 12 Core.

2.9 **DNB PARAMETERS (Specification 3.2.5):**

2.9.1 The following DNB-related parameters shall be maintained within the following limits: [1]

2.9.1.1 Reactor Coolant System T_{avg}, ≤ 595 °F [2],

2.9.1.2 Pressurizer Pressure, > 2200 psig [3],

2.9.1.3 Minimum Measured Reactor Coolant System Flow [4] > 403,000 gpm.

3.0 REFERENCES

3.1 Letter from D. E. Robinson (Westinghouse) to D. F. Hoppes (STPNOC), "South Texas Project Nuclear Operating Company South Texas Project Electric Generating Station Unit 2 Cycle 12 Final Reload Evaluation (RE) Revision 2," ST-UB-NOC-05002587, Rev. 2, October 21, 2005.

3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.

3.3 STPNOC Calculation ZC-7035, Rev. 2, "Loop Uncertainty Calculation for RCS Tavg Instrumentation," Section 10.1.

3.4 STPNOC Calculation ZC-7032, Rev. 4, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," Section 2.3, Page 9.

3.5 Condition Report Engineering Evaluation 04-5927-9, Revision 0, "Reload Safety Evaluation and Core Operating Limits Report for South Texas Unit 2 Cycle 12."

3.6 WCAP-12472-P-A, BEACON Core Monitoring and Operations Support System, August 1994.

---

1 A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

2 Includes a 1.9 °F measurement uncertainty per Reference 3.3.

3 Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Includes a 9.6 PSI measurement uncertainty as read on QDPS display per Reference 3.4.

4 Includes a 2.8% flow measurement uncertainty.

Figure 1

Reactor Core Safety Limits - Four Loops in Operation

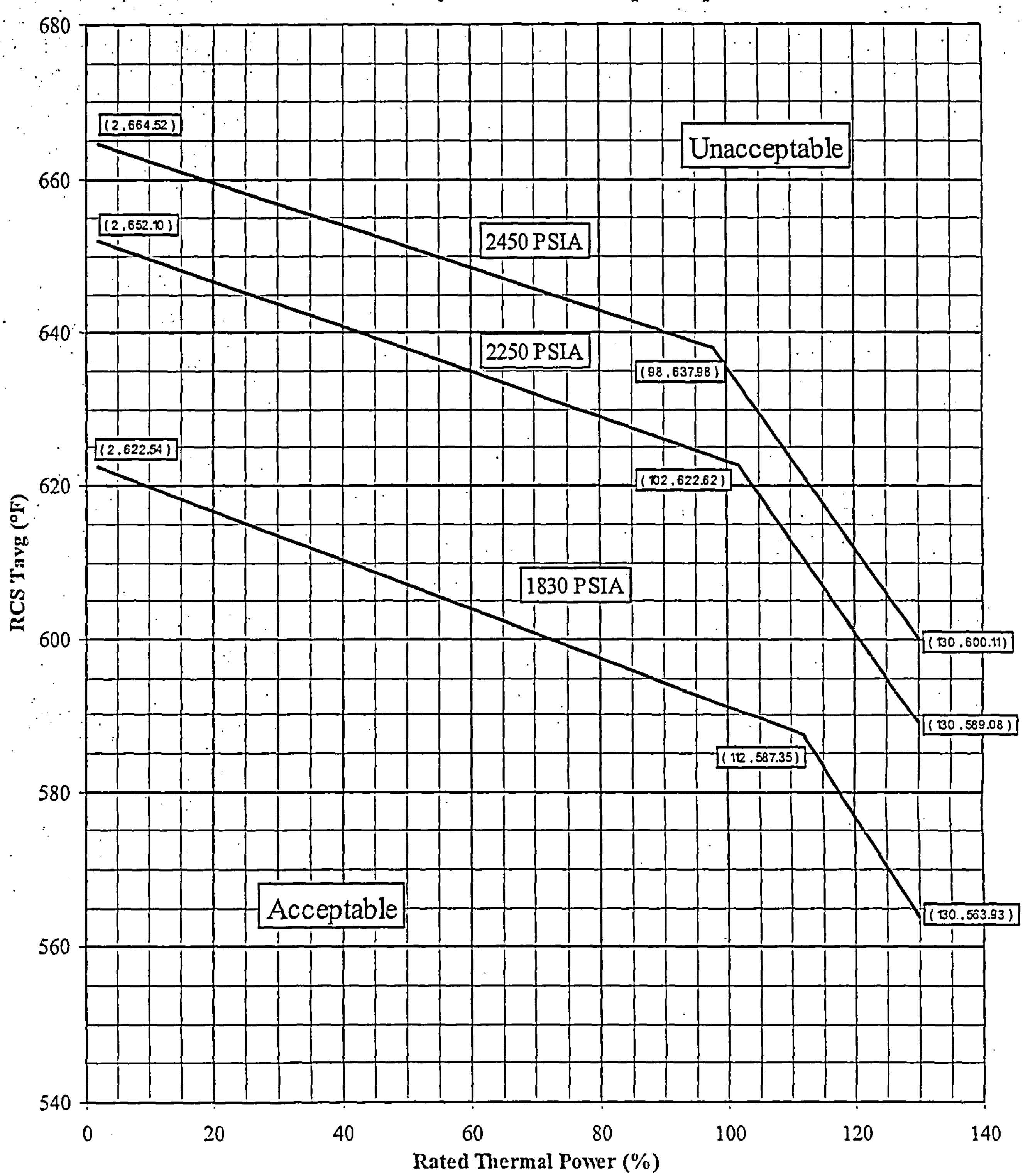


Figure 2

Required Shutdown Margin for Modes 3 & 4

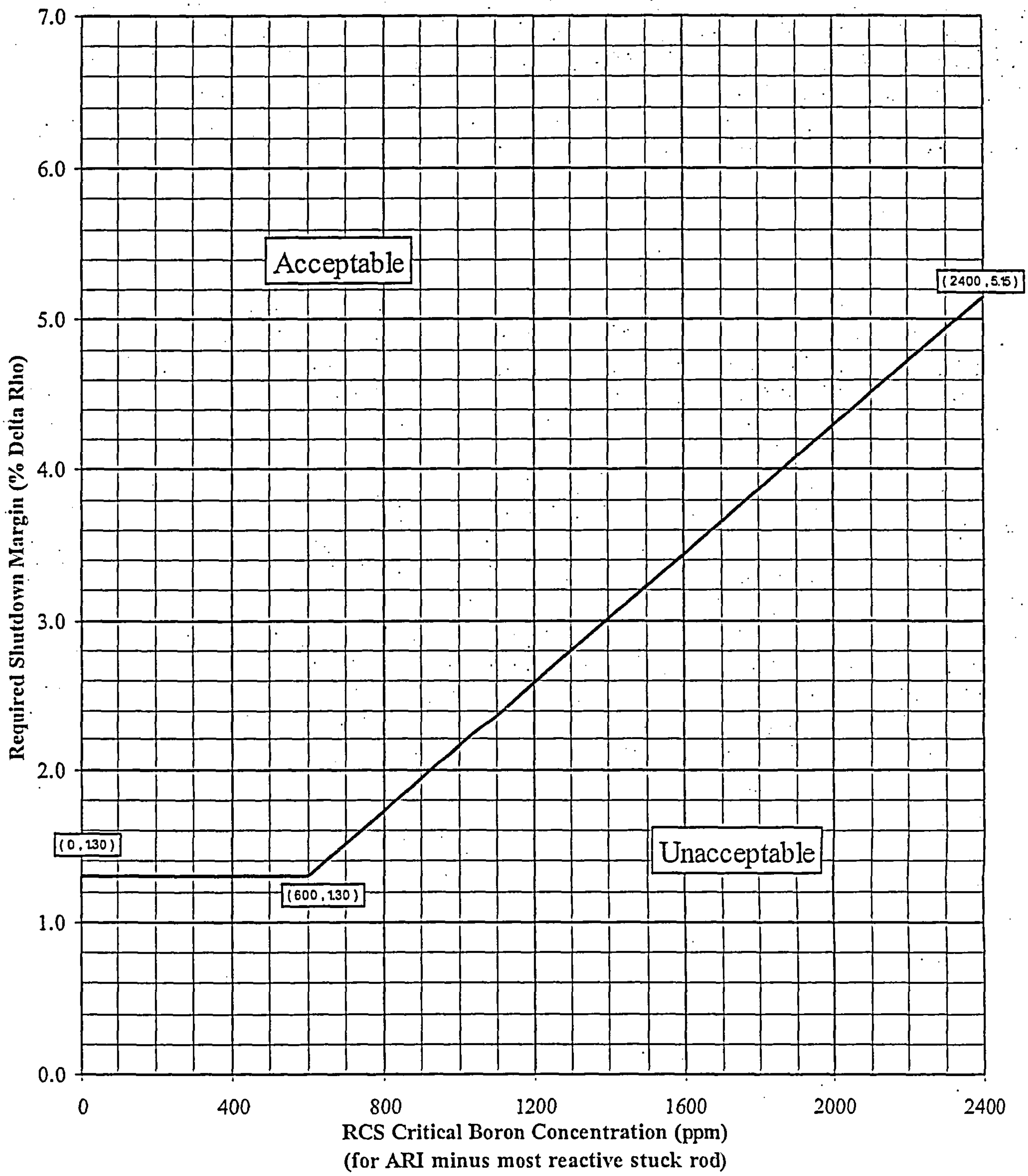


Figure 3

Required Shutdown Margin for Mode 5

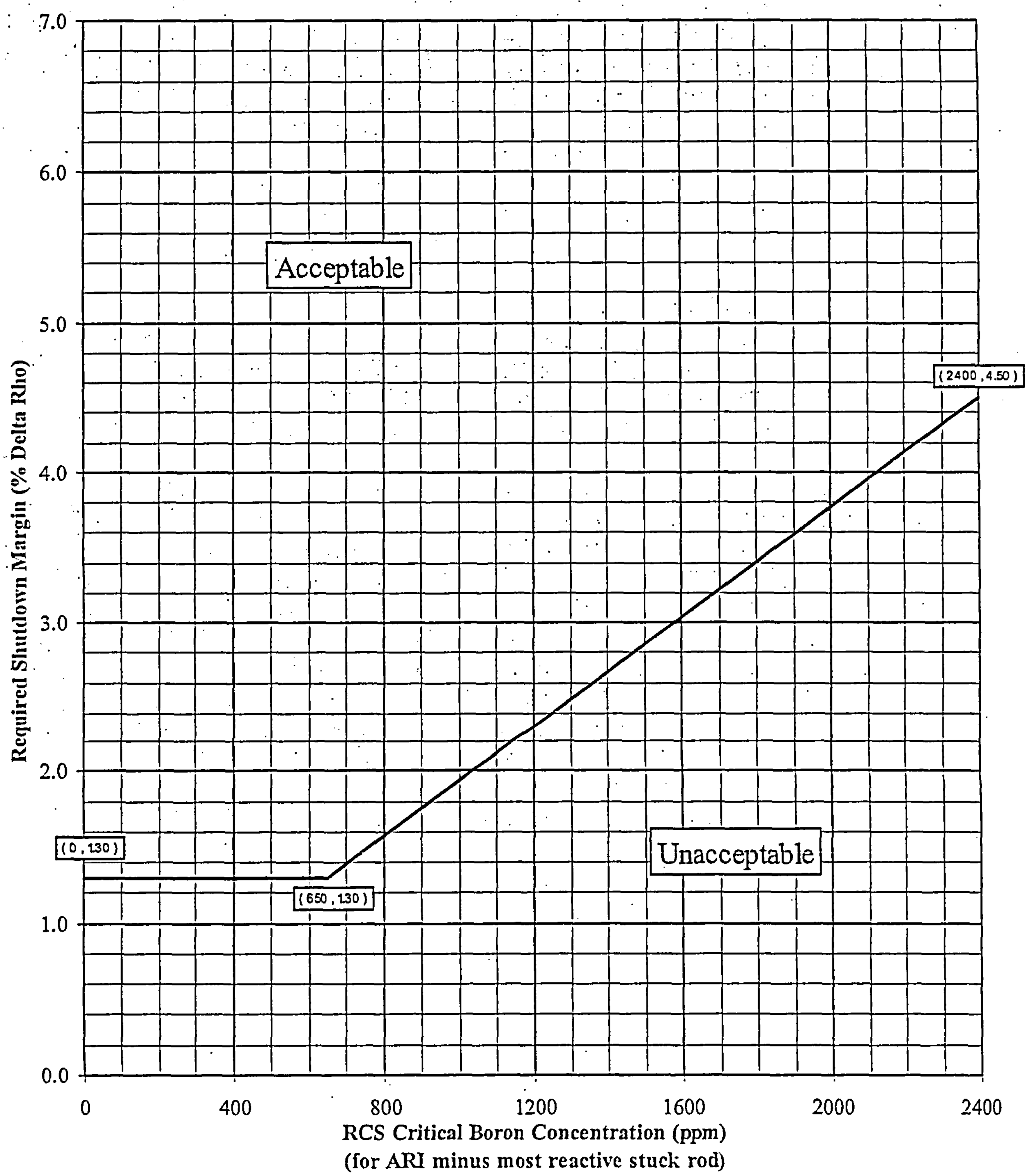


Figure 4

MTC versus Power Level

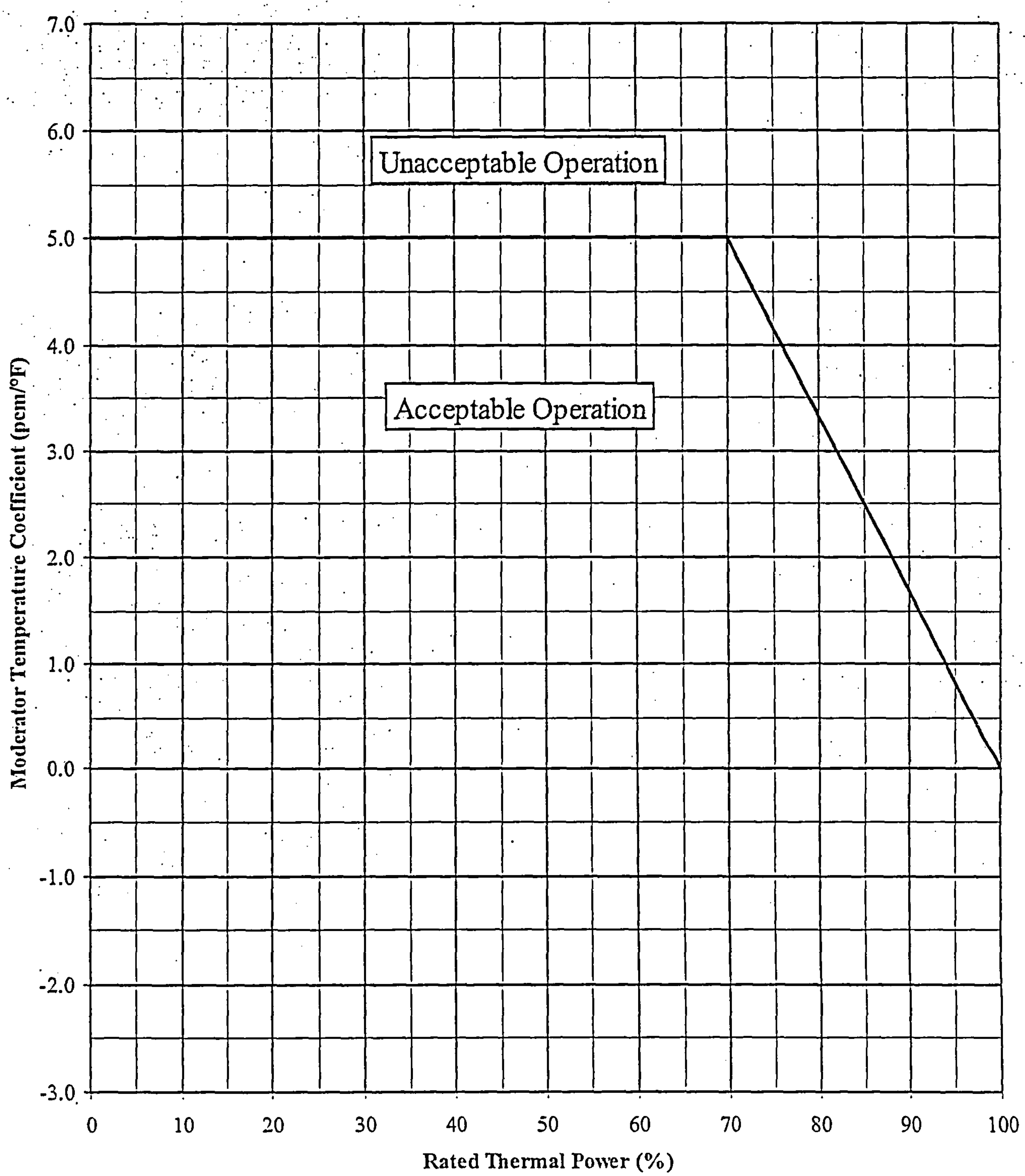


Figure 5

Control Rod Insertion Limits* versus Power Level

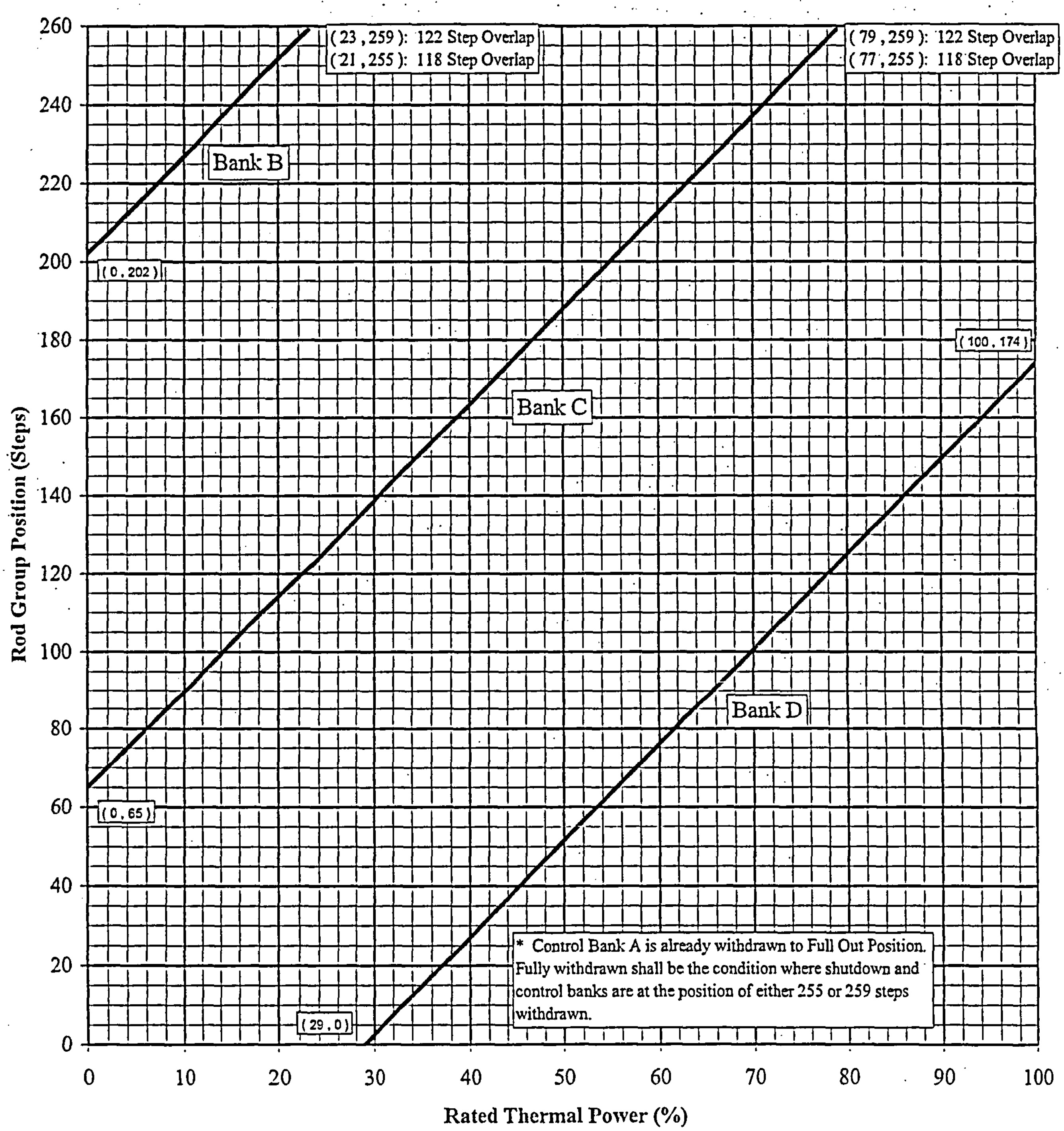


Figure 6

AFD Limits versus Power Level

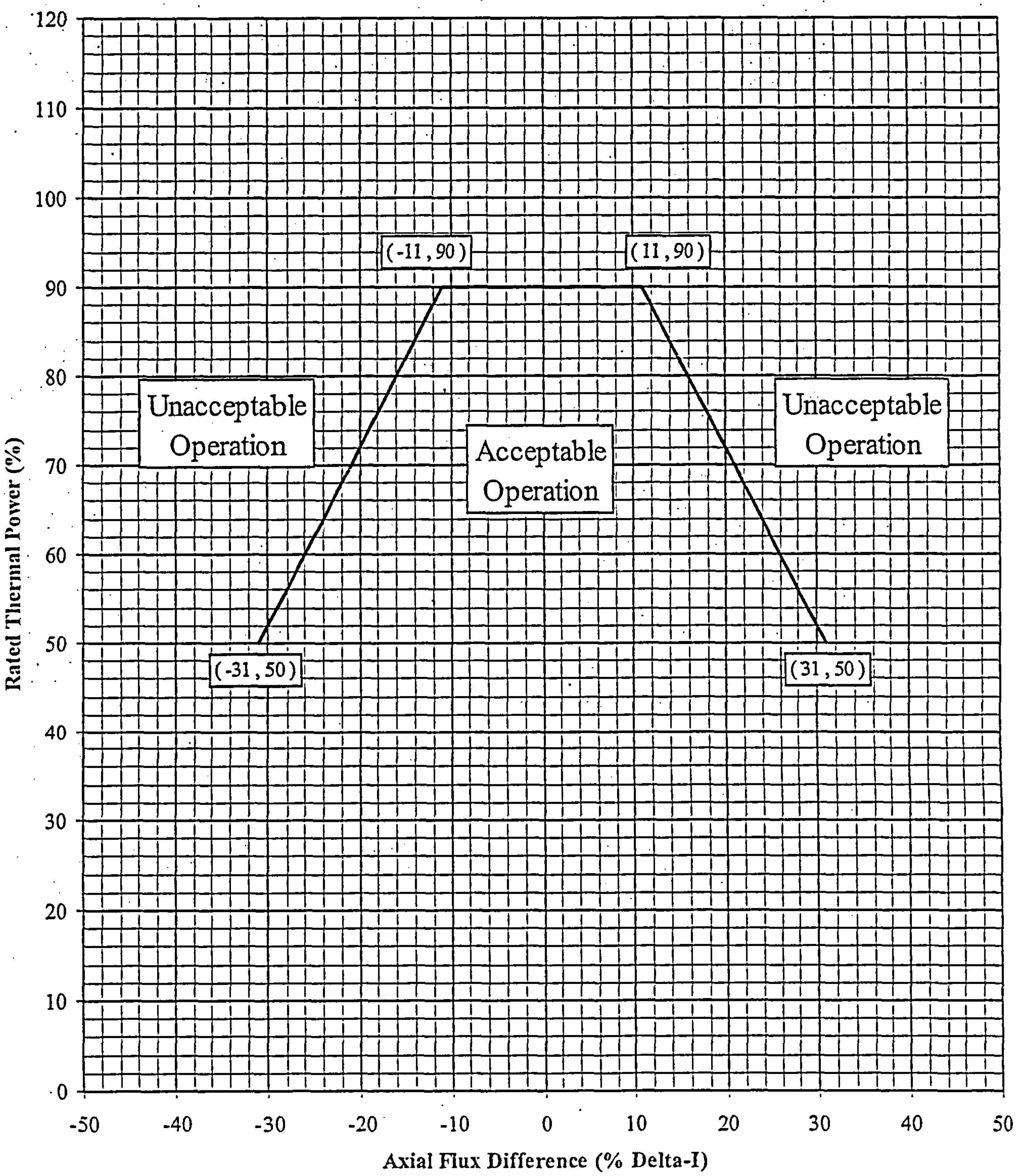
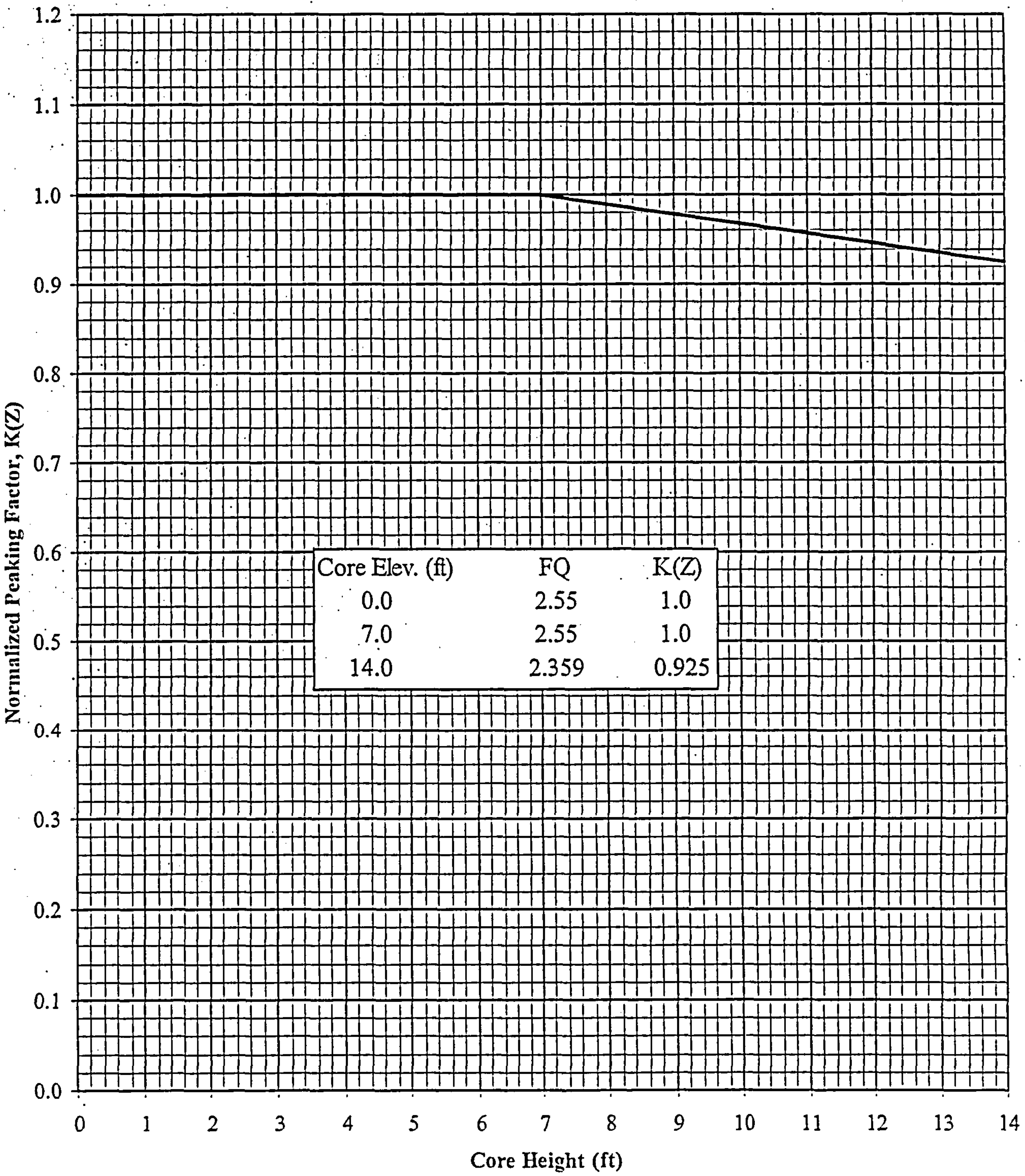


Figure 7

K(Z) - Normalized FQ(Z) versus Core Height



Core Elev. (ft)	FQ	K(Z)
0.0	2.55	1.0
7.0	2.55	1.0
14.0	2.359	0.925

Table 1 (Part 1 of 2)
Unrodded F_{xy} for Each Core Height
for Cycle Burnups Less Than 9000 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	5.271	6.80	37	1.955
13.80	2	4.497	6.60	38	1.948
13.60	3	3.723	6.40	39	1.940
13.40	4	2.949	6.20	40	1.933
13.20	5	2.563	6.00	41	1.928
13.00	6	2.303	5.80	42	1.927
12.80	7	2.269	5.60	43	1.927
12.60	8	2.209	5.40	44	1.928
12.40	9	2.156	5.20	45	1.933
12.20	10	2.104	5.00	46	1.938
12.00	11	2.073	4.80	47	1.946
11.80	12	2.053	4.60	48	1.955
11.60	13	2.043	4.40	49	1.960
11.40	14	2.037	4.20	50	1.965
11.20	15	2.033	4.00	51	1.968
11.00	16	2.029	3.80	52	1.965
10.80	17	2.023	3.60	53	1.958
10.60	18	2.016	3.40	54	1.954
10.40	19	2.010	3.20	55	1.952
10.20	20	2.010	3.00	56	1.952
10.00	21	2.010	2.80	57	1.945
9.80	22	2.010	2.60	58	1.944
9.60	23	2.014	2.40	59	1.944
9.40	24	2.017	2.20	60	1.945
9.20	25	2.021	2.00	61	1.948
9.00	26	2.026	1.80	62	1.948
8.80	27	2.034	1.60	63	1.945
8.60	28	2.043	1.40	64	1.957
8.40	29	2.054	1.20	65	1.980
8.20	30	2.065	1.00	66	2.031
8.00	31	2.073	0.80	67	2.229
7.80	32	2.069	0.60	68	2.756
7.60	33	2.054	0.40	69	3.447
7.40	34	2.038	0.20	70	4.138
7.20	35	2.010	0.00	71	4.829
7.00	36	1.976			

Table 1 (Part 2 of 2)
Unrodded Fxy for Each Core Height
for Cycle Burnups Greater Than or Equal to 9000 MWD/MTU

Core Height (Ft.)	Axial Point	Unrodded Fxy	Core Height (Ft.)	Axial Point	Unrodded Fxy
14.00	1	4.128	6.80	37	2.142
13.80	2	3.681	6.60	38	2.141
13.60	3	3.234	6.40	39	2.129
13.40	4	2.788	6.20	40	2.116
13.20	5	2.497	6.00	41	2.102
13.00	6	2.254	5.80	42	2.092
12.80	7	2.190	5.60	43	2.081
12.60	8	2.133	5.40	44	2.071
12.40	9	2.084	5.20	45	2.060
12.20	10	2.043	5.00	46	2.051
12.00	11	2.014	4.80	47	2.042
11.80	12	2.013	4.60	48	2.035
11.60	13	2.017	4.40	49	2.025
11.40	14	2.026	4.20	50	2.015
11.20	15	2.031	4.00	51	2.003
11.00	16	2.036	3.80	52	1.992
10.80	17	2.042	3.60	53	1.982
10.60	18	2.045	3.40	54	1.972
10.40	19	2.046	3.20	55	1.960
10.20	20	2.048	3.00	56	1.944
10.00	21	2.049	2.80	57	1.925
9.80	22	2.051	2.60	58	1.899
9.60	23	2.054	2.40	59	1.873
9.40	24	2.058	2.20	60	1.846
9.20	25	2.062	2.00	61	1.837
9.00	26	2.066	1.80	62	1.833
8.80	27	2.069	1.60	63	1.832
8.60	28	2.073	1.40	64	1.832
8.40	29	2.078	1.20	65	1.862
8.20	30	2.084	1.00	66	1.932
8.00	31	2.091	0.80	67	2.144
7.80	32	2.099	0.60	68	2.520
7.60	33	2.107	0.40	69	2.976
7.40	34	2.116	0.20	70	3.433
7.20	35	2.127	0.00	71	3.889
7.00	36	2.137			