

NUCLEAR ENGINEERING CALCULATION COVER SHEET

NEPM-QA-0221-1

1. Page 1 of 36
Total Pages 36

>2. TYPE: CALC >3. NUMBER: EC-ENVR-1059 >4. REVISION: 0

*>5. UNIT 3 *>6. QUALITY CLASS: Q

>7. DESCRIPTION: CRHE Accident Dispersion Factors (x/Q) RB U2 Intake

8. SUPERSEDED BY: _____

9. Alternate Number: _____

10. Cycle: _____

11. Computer Code/Model used: ARCON96

12. Discipline: R

>13. Are any results of this calculation described in the Licensing Documents?

☒ Yes, Refer to NDAP-QA-0730 and NDAP-QA-0731 ☐ No

>14. Is this calculation changing any method of evaluation described in the FSAR and using the results to support or change the FSAR? (Refer to PPL Resource Manual for Definition of FSAR)

☒ Yes, 50.59 screen or evaluation required. ☐ No

>15. Is this calculation Prepared by an External Organization?

☒ Yes ☐ No

EG771 Qualifications may not be required for individuals from external organizations (see Section 7.4.3).

>16. Prepared by: M. M. Waselus
Print Name(EG771 Qualification Required)

M. M. Waselus 7/14/05
Signature Date

>17. Reviewed by: K. E. Weise
Print Name(EG771 Qualification Required)

K. E. Weise 7-12-05
Signature Date

>18. Verified by: K. E. Weise
Print Name(EG771 Qualification Required)

K. E. Weise 7/12/05
Signature Date

>19. Approved by: M. G. Capiotis
Print Name(Qualified per NEPM-QA-0241 and
comply with Section 7.8 of NEPM-QA-0221)

M. G. Capiotis 7/12/05
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>20. Accepted by: TERRENCE F. MACKAY
Print Name(EG771 Qualification Required) and
comply with Section 7.9 of NEPM-QA-0221

Terrence F. Mackay 7/19/05
Signature Date

TO BE COMPLETED BY DCS

DCS SIGNATURE/DATE

ADD A NEW COVER PAGE FOR EACH REVISION
FORM NEPM-QA-0221-1, Revision 8, Page 1 of 1, ELECTRONIC FORM

* Verified Fields
> REQUIRED FIELDS

ADD A NEW COVER PAGE FOR EACH REVISION

* Verified Fields
> REQUIRED FIELDS

PP&L CALCULATION SHEET

Dept.	<u>0341 Rad & Eff Tech.</u>	PROJECT	
Date	<u>7/11/05</u>	<u>CRHE Accident Dispersion Factors</u>	Calc. No. <u>EC-ENVR-1059</u>
Designed By	<u>M. M. Waselus</u>	<u>(γ/Q) RB U2 Intake</u>	Sh. No. <u>2</u>
Checked By	<u>K. E. Weise</u>		

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Designed By	<u>M. M. Waselus</u>	<u>(γ/Q) RB U2 Intake</u>	Sh. No. <u>3</u>
Checked By	<u>K. E. Weise</u>		

1.0 PURPOSE

The purpose of this analysis is to calculate short term accident γ/Q 's for the SSES Control Room Habitability Envelope (CRHE) using the methodology provided in NUREG/CR-6331 - ARCON96 (Reference 1) and onsite meteorological data documented in Reference 2. The ARCON96 code uses hourly meteorological data and recently developed methods for estimating γ/Q 's in the vicinity of buildings to calculate relative concentrations at control room air intakes that would be exceeded no more than five percent of the time. These concentrations are calculated for averaging periods ranging from one hour to 30 days in duration. The term γ/Q (sec/m^3) is an expression of the relative dispersion occurring between a source (release) location and a receptor location. This relative dispersion is used to determine the expected atmospheric concentration at some defined distance away from the source for a known quantity of effluent released.

The potential release points evaluated in this analysis are defined as follows:

1. Reactor Building Unit 1 exhaust vent.
2. Reactor Building Unit 2 exhaust vent.
3. Turbine Building Unit 1 exhaust vent.
4. Turbine Building Unit 2 exhaust vent.
5. Standby Gas Treatment System exhaust vent.
6. Reactor Building Unit 1 closest distance.
7. Reactor Building Unit 2 closest distance.
8. Turbine Building Unit 1 closest distance.
9. Turbine Building Unit 2 closest distance.
10. Reactor Building Unit 1 main steam tunnel blowout panel.
11. Reactor Building Unit 2 main steam tunnel blowout panel.
12. Turbine Building Unit 1 main steam tunnel blowout panel.
13. Turbine Building Unit 2 main steam tunnel blowout panel.

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Checked By	<u>K. E. Weise</u>		

The CRHE outside air intake is located on the roof of the Unit 2 reactor building in the vicinity of column lines U and 36.

References 7 to 23 provide details of the layout of the SSES plant structures, exhaust vents and components. By inspection of the locations of the potential release points relative to the location of the CRHE intake and the potential to be a source of post LOCA activity release, release points 3, 4, 5, 11 and 13 (listed below) are seen as limiting and are further evaluated in detail herein. The Reactor Building exhaust vents (release points 1 & 2) are not a source of post LOCA activity releases. The Reactor Building closest distance (release points 6 & 7) would only be potential release points during the 10 minute drawdown period. During this time there is negligible activity released to the Reactor Building available for release to the environment. The Turbine Building closest points (release points 8 & 9) are bounded by the Turbine Building exhaust vents (release points 3 & 4) which are at the same elevation as the CRHE intake. The Reactor Building and Turbine Building Unit 1 blowout panels (release points 10 & 12) are bounded by the Reactor Building and Turbine Building Unit 2 blowout panels (release points 11 & 13). See Figure 1 on page 10 for the relative locations of the 13 release points and the CRHE outside air intake. The specific locations requiring ARCON96 χ/Q s are:

3. Turbine Building Unit 1 exhaust vent.
4. Turbine Building Unit 2 exhaust vent.
5. Standby Gas Treatment System exhaust vent.
11. Reactor Building Unit 2 main steam tunnel blowout panel.
13. Turbine Building Unit 2 main steam tunnel blowout panel.

2.0 CONCLUSIONS AND RECOMMENDATIONS

The CRHE χ/Q 's for the above release points as determined in this calculation are listed as follows.

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Date	<u>7/11/05</u>	<u>CRHE Accident Dispersion Factors</u>	Calc. No.	<u>EC-ENVR-1059</u>	
Designed By	<u>M. M. Waselus</u>	<u>(γ/Q) RB U2 Intake</u>	Sh. No.	<u>5</u>	
Checked By	<u>K. E. Weise</u>				

#	Release Point	CRHE γ/Q 'S (sec/m ³) without Occupancy Correction Factors				
	Time Period	0 to 2 hours	2 to 8 hours	8 to 24 hours	1 to 4 days	4 to 30 days
3	TB Unit 1 Exhaust Vent	1.24E-03	9.55E-04	3.14E-04	1.99E-04	1.73E-04
4	TB Unit 2 Exhaust Vent	1.36E-03	1.03E-03	3.36E-04	2.20E-04	1.85E-04
5	SGTS Exhaust Vent	1.45E-03	1.12E-03	3.55E-04	2.29E-04	2.01E-04
11	RB Unit 2 MST Blowout Panel	1.94E-03	1.41E-03	5.12E-04	3.28E-04	2.68E-04
13	TB Unit 2 MST Blowout Panel	1.47E-03	1.01E-03	4.01E-04	2.95E-04	2.26E-04

These γ/Q values are to be used in subsequent CRHE radiological evaluations for SSES.

3.0 ASSUMPTIONS / INPUT

There are no assumptions in this analysis which require future confirmation.

The input data and assumptions used in this analysis are summarized as follows:

1. Reactor building grade elevation – 670' (Reference 9).
2. Turbine and Control building grade elevation – 676' (Reference 9).
3. Elevation of the 5 release points and references are shown on Table 2.
4. All release points are assumed to be ground level release type as discussed in References 4 and 6.
5. Plant north and true north are essentially the same at SSES.
6. Other input is referenced as appropriate throughout the analysis.

4.0 METHODOLOGY

The γ/Q 's for the SSES CRHE are determined using the ARCON96 computer code. ARCON96 mainly requires inputs involving physical relationships between release points and receptor locations. Table 1 lists the required inputs in order for ARCON96 to provide the γ/Q 's. ARCON96 also has default values for other parameters used in the dispersion model, but they are not normally changed. These parameters, as used herein, will remain the default values except for the Surface Roughness Length and

herein, will remain the default values except for the Surface Roughness Length and

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Checked By	<u>K. E. Weise</u>		

Averaging Sector Width Constant, which will be set at 0.2 and 4.3, respectively, in lieu of the default values of 0.1 and 4.0, in accordance with the recommendations in USNRC Regulatory Guide 1.194 (Reference 3).

Table 1 – Inputs required for ARCON96	
Meteorological Input	Receptor Input
Number of Met Data Files	Distance to receptor
Lower Measurement Height	Intake Height
Upper Measurement Height	Elevation Difference
Wind Speed	Direction to Source
Source Input	
Release Type	Output Files
Release Height	Output File Name fn.log
Building Area	CFD File Name fn.cfd
Vertical Velocity	Expanded Output no
Stack Flow	
Stack Radius	

Meteorological Input

The meteorological data files consist of five files documented in Reference 2. The meteorological data consists of five years of hourly data, covering the years from 1999 to 2003. Each record of the hourly data contains a location identifier, Julian day (1-366), hour (0 to 23), low-level direction, low-level speed, stability class (1=A to 7=G), upper level direction, and upper level speed. The identifier and upper level data is optional. Wind speeds are entered in tenths of a reporting unit with no decimal. Wind directions are from 1 to 360 in degrees.

These five files were combined into one file for ease of code execution. This file contains all the data for the SSES site from 1999-2003, which satisfies the ARCON96 (Reference 1) requirements for having 3 to 5 years of hourly data. The Upper and Lower Measurement Heights are 10m and 60 m, respectively, and the Wind Speed units are m/s (Reference 2).

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Checked By	K. E. Weise				

Source Input

Five Source (or Release) points are analyzed. These sources are chosen to primarily support Condition IV type accidents, but are not limited to just these accidents. The release points along with the release height and references are listed in Table 2.

Table 2 – Release Points and Release Heights					
#	Description	Release Elevation, ft	Release Height, ft (1)	Release Height, m	Reference
3	Turbine Building Unit 1 exhaust vent	874.7	204.7	62.4	16
4	Turbine Building Unit 2 exhaust vent	874.7	204.7	62.4	16
5	Standby Gas Treatment System exhaust vent	874.7	204.7	62.4	16
11	RB Unit 2 main steam tunnel blowout panel	802.5	132.5	40.4	18
13	TB Unit 2 main steam tunnel blowout panel	717.5	47.5	14.5	19,21

1. Release height = Release elevation (ft) – 670 ft (grade elevation for RB).

The Building Area used for determining the wake effects is 2685 m² per Reference 5 (included as Attachment 6).

The remaining values for Source input (vertical velocity, stack flow and stack radius) are specified as 0 since only ground level release types are being analyzed.

Receptor Input

The receptor considered in the calculation is the SSES CRHE outside air intake. The CRHE Intake is approximately located at column lines U and 36 on the roof of the Unit #2 Reactor Building. Reference 12 provides a sketch of the general arrangement of several of the release points. No dimensions are taken from Reference 12, it is used for general orientation only. The CRHE intake elevation is taken as the Reactor Building roof elevation of 872' (Reference 11). Grade elevation for the SSES site at the Reactor Building is 670' (Reference 9). Therefore, the CRHE intake height is 202' [872' – 670']

Building is 670' (Reference 9). Therefore, the CRHE intake height is 202' [872' – 670']

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or 61.6 m. The Turbine Building elevations are measured from the Turbine Building grade elevation of 676' (Reference 9) and the elevation difference is +6 feet or +1.8 m. This only affects release point 13, TB Unit 2 main steam blowout panel.

For release points 3, 4 and 5 the release height is conservatively set equal to the intake height at a value of 0. (No credit is taken for any elevation difference).

With the combinations of release points and intake identified, the direction and distance between the release point and the intake is determined by scaling from the reference drawings. Wind direction data are recorded as the direction from which the wind blows (e.g., a north wind blows from the north, a wind blowing out of the west is recorded with a direction of 270 degrees). The direction input to ARCON96 is the wind direction that would carry the plume from the release point to the intake. For example, an analyst standing at the intake facing west to the release point, would enter 270 degrees; an analyst facing north, would enter 360 degrees, etc.

The source-to-receptor distance is the shortest horizontal distance between the release point and the intake. ARCON96 uses this distance and the elevations of the source and receptor to calculate the slant path. For releases within building complexes, the distance between the release point and the intake could be through intervening buildings. In these cases, the length of the shortest path is taken around or over the intervening building as the source-to-receptor distance (e.g., "taut string length"). Taut string distances are not used in this analysis and the horizontal values from Table 3 are conservatively used directly in ARCON96. The source-to-receptor horizontal distances and direction are listed in Table 3. The values were determined by scaling from the reference drawings.

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Designed By	<u>M. M. Waselus</u>	<u>(Y/Q) RB U2 Intake</u>		Sh. No. <u>9</u>
Checked By	<u>K. E. Weise</u>			

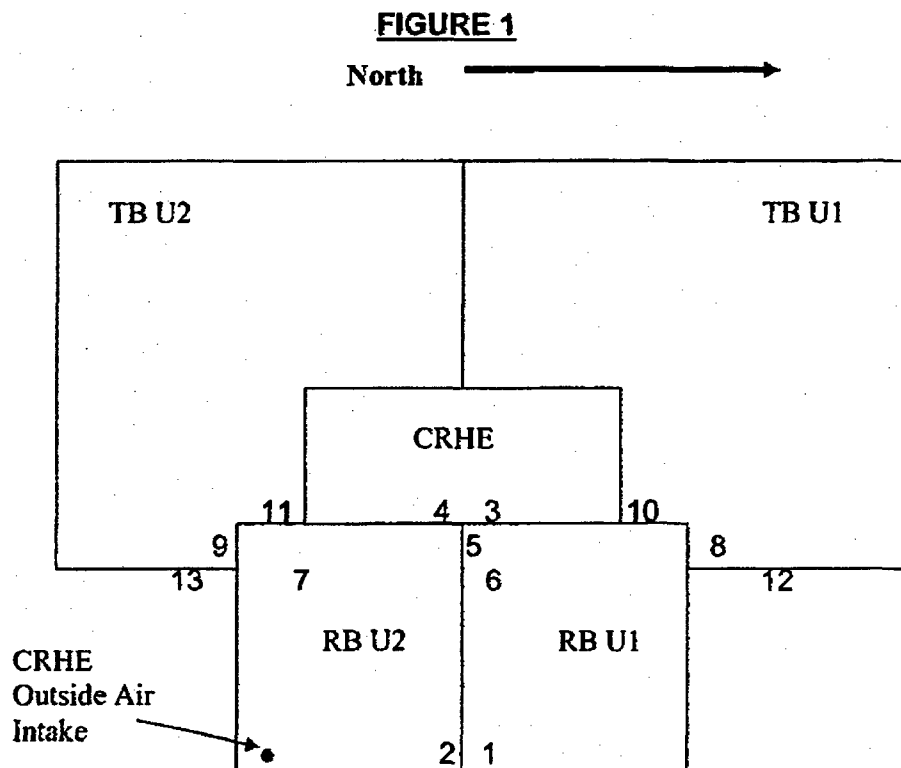
Table 3 - Release Point Horizontal Distances and Directions				
#	Description	Horizontal Distance meters	Direction degrees	Reference
3	TB Unit 1 exhaust vent	66.1	322	11,16,22
4	TB Unit 2 exhaust vent	62.6	317	11,16,22
5	SGTS exhaust vent	60.98	320	11,16,22
11	RB Unit 2 MST blowout panel	47.26	299	11,17,23
13	TB Unit 2 MST blowout panel	40.85	255	19,21

The approximate roof elevations for the structures are listed as follows:

- | | | |
|---------------------|------|--------------|
| 1. Turbine Building | 786' | Reference 9 |
| 2. Control Building | 810' | Reference 9 |
| 3. Reactor Building | 872' | Reference 11 |

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The overall site/building arrangement is shown on Reference 10. The relative locations of the release points corresponding to the above are shown as follows on Figure 1:



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Designed By	<u>M. M. Waselus</u>	<u>(γ/Q) RB U2 Intake</u>	Sh. No. <u>11</u>
Checked By	<u>K. E. Weise</u>		

5.0 RESULTS

The results of the analysis are provided on the ARCON96 computer outputs (Attachments 1 to 5) and summarized on Table 5. As noted in Reference 6, section 4.2.6, ARCON96 output does not include the CRHE occupancy correction factors that may be applied in CRHE dose evaluations.

Table 5 – CRHE γ/Q 's as a Function of Release Point without Occupancy Correction								
Release Point	0 to 2 hours sec/m ³	2 to 8 hours sec/m ³	8 to 24 hours sec/m ³	1 to 4 days sec/m ³	4 to 30 days sec/m ³	ARCON96 file	Reference	
TB Unit 1 Exhaust Vent	1.24E-03	9.55E-04	3.14E-04	1.99E-04	1.73E-04	RB2TB1EV.log	Attachment 1	
TB Unit 2 Exhaust Vent	1.36E-03	1.03E-03	3.36E-04	2.20E-04	1.85E-04	RB2TB2EV.log	Attachment 2	
SGTS Exhaust Vent	1.45E-03	1.12E-03	3.55E-04	2.29E-04	2.01E-04	RB2SGTSV.log	Attachment 3	
RB Unit 2 MST Blowout Panel	1.94E-03	1.41E-03	5.12E-04	3.28E-04	2.68E-04	RB2MSTP.log	Attachment 4	
TB Unit 2 MST Blowout Panel	1.47E-03	1.01E-03	4.01E-04	2.95E-04	2.26E-04	RB2TBMST.log	Attachment 5	

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Dept. <u>0341 Rad & Eff Tech.</u>	PROJECT	
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Designed By <u>M. M. Waselus</u>	<u>(y/Q) RB U2 Intake</u>	Sh. No. <u>12</u>
Checked By <u>K. E. Weise</u>		

6.0 REFERENCES

1. NUREG/CR-6331, Atmospheric Relative Concentrations in Building Wakes, Revision 1, May, 1997 (ARCON96 computer code).
2. EC-ENVR-1057, Offsite χ/Q values for SSES Based on 1999 – 2003 Meteorological Data, Revision 0.
3. USNRC Regulatory Guide 1.194, Atmospheric Relative Concentrations for Control Room Radiological Habitability Assessments at Nuclear Power Plants, June, 2003.
4. NEI-99-03, Control Room Habitability Assessment Guidance, Nuclear Energy Institute, 6/2001.
5. Building Cross Sectional Area calculated herein included as Attachment 6.
6. USNRC Regulatory Guide 1.183, Alternative Radiological Source Terms For Evaluating Design Basis Accidents At Nuclear Power Reactors, July 2000.
7. PPL Drawing E-106446 Sheet 10 Revision 16.
8. PPL Drawing E-106446 Sheet 15 Revision 9.
9. PPL Drawing E-106312 Revision F.
10. PPL Drawing E105002 Sheet 1 Revision 12.
11. PPL Drawing E-105004 Sheet 7 Revision 27.
12. FSAR Figure 6.4-2. Revision 49.
13. PPL Drawing E-105004 Sheet 4 Revision 25.
14. PPL Drawing E-106454 Sheet 14 Revision 11.
15. PPL Drawing E-106458 Sheet 14 Revision 8.
16. PPL Drawing E-106429-8 Revision 16.
17. PPL Drawing E-105007 Sheet 1 Revision 9.
18. PPL Drawing E-105618 Revision 1.
19. PPL Drawing E-105670 Revision 8.
20. PPL Drawing E-105005 Sheet 1 Revision 9.
21. PPL Drawing E-105004 Sheet 3 Revision 26.
22. PPL Drawing E-106429-10 Revision 15.
23. PPL Drawing E-105004 Sheet 6 Revision 22.
21. PPL Drawing E-105004 Sheet 3 Revision 26.

PP&L CALCULATION SHEET

Dept. 0341 Rad & Eff Tech.

Date 7/11/05

Designed By M. M. Waselus

Checked By K. E. Weise

PROJECT

CRHE Accident Dispersion Factors

(Y/Q) RB U2 Intake

Calc. No. EC-ENVR-1059

Sh. No. 13

24. PPL Drawing E-105329 Revision 9.

25. PPL Drawing E-105257 Revision 9.

26. PPL Drawing E-105259 Revision 8.

27. PPL Drawing E-105004 Sheet 5 Revision 27.

Attachment 1 – RB2TB1EV.log
ARCON96 Output
for
Turbine Building Unit 1 Exhaust Vent

RB2TB1EV.log

Program Title: ARCON96.

Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NRC Contacts: J. Y. Lee Phone: (301) 415 1080
e-mail: jy11@nrc.gov
J. J. Hayes Phone: (301) 415 3167
e-mail: jjh@nrc.gov
L. A. Brown Phone: (301) 415 1232
e-mail: lab2@nrc.gov

Code Developer: J. V. Ramsdell Phone: (509) 372 6316
e-mail: j_ramsdell@pnl.gov

Code Documentation: NUREG/CR-6331 Rev. 1

This program was prepared for an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibilities for any third party's use, or the results of such use, of any portion of this program or represents that its use by such third party would not infringe privately owned rights.

Program Run 7/ 9/2005 at 08:47:05

* AF***** ARCON INPUT *****

Number of Meteorological Data Files = 1
Meteorological Data File Names
C:\ARCON96\SQ99_0-1.MET

Height of lower wind instrument (m) = 10.0
Height of upper wind instrument (m) = 60.0
Wind speeds entered as miles per hour

Ground-level release
Release height (m) = .0
Building Area (m^2) = 2685.0
Effluent vertical velocity (m/s) = .00
Vent or stack flow (m^3/s) = .00
Vent or stack radius (m) = .00

Direction .. intake to source (deg) = 322

l di Wind direction sector width (deg) = 90
 l di Wind direction window (deg) = 277 - 007
 anc Distance to intake (m) = 66.1
 ke Intake height (m) = .0
 ain Terrain elevation difference (m) = .0

out Output file names

12TB RB2TB1EV.log
 12TB RB2TB1EV.cfd

.mm Minimum Wind Speed (m/s) = .5
 ace Surface roughness length (m) = .20
 or Sector averaging constant = 4.3

ial Initial value of sigma y = .00
 ial Initial value of sigma z = .00

unde Expanded output for code testing not selected

l n Total number of hours of data processed = 43824
 s o Hours of missing data = 297
 s d Hours direction in window = 6049
 s e Hours elevated plume w/ dir. in window = 0
 s o Hours of calm winds = 454
 s d Hours direction not in window or calm = 37024

TRIB DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

PE	AVER. PER.	1	2	4	8	12	24	96	168	360	720
LI	UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LI	LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
RAN	ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
RAN	IN RANGE	6503.	8237.	10974.	15307.	18889.	26551.	40991.	42163.	42457.	43155.
RAN	BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZE	ZERO	37024.	35244.	32428.	27949.	24411.	16602.	1966.	458.	0.	0.
X/	TOTAL X/Qs	43527.	43481.	43402.	43256.	43300.	43153.	42957.	42621.	42457.	43155.
ZE	% NON ZERO	14.94	18.94	25.28	35.39	43.62	61.53	95.42	98.93	100.00	100.00

PE 95th PERCENTILE X/Q VALUES

	1	2	4	8	12	24	96	168	360	720
	1.24E-03	1.21E-03	1.14E-03	1.03E-03	8.21E-04	5.51E-04	2.87E-04	2.44E-04	2.09E-04	1.89E-04

X/Q 95% X/Q for standard averaging intervals

2	0 to 2 hours	1.24E-03
8	2 to 8 hours	9.55E-04
24	8 to 24 hours	3.14E-04
4	1 to 4 days	1.99E-04
30	4 to 30 days	1.73E-04

		HOURLY VALUE RANGE	
		MAX X/Q	MIN X/Q
CE	CENTERLINE	1.64E-03	2.51E-04
SE	SECTOR-AVERAGE	9.54E-04	1.46E-04

PROGRAMAL PROGRAM COMPLETION

Attachment 2 – RB2TB2EV.log
ARCON96 Output
for
Turbine Building Unit 2 Exhaust Vent

RB2TB2EV.log

Program Title: ARCON96.

Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NRC Contacts: J. Y. Lee Phone: (301) 415 1080
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Code Documentation: NUREG/CR-6331 Rev. 1

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Program Run 7/ 9/2005 at 08:47:46

* AF ***** ARCON INPUT *****

per Number of Meteorological Data Files = 1
sorc Meteorological Data File Names
:\AF C:\ARCON96\SQ99_0~1.MET

ght Height of lower wind instrument (m) = 10.0
ght Height of upper wind instrument (m) = 60.0
d s Wind speeds entered as miles per hour

and Ground-level release
eas Release height (m) = .0
ldir Building Area (m^2) = 2685.0
luer Effluent vertical velocity (m/s) = .00
t o Vent or stack flow (m^3/s) = .00
t o Vent or stack radius (m) = .00

```

sectl Direction .. intake to source (deg) = 317
i di Wind direction sector width (deg) = 90
i di Wind direction window (deg) = 272 - 002
tanc Distance to intake (m) = 62.6
ake Intake height (m) = .0
cair Terrain elevation difference (m) = .0

```

```

put Output file names
32TH RB2TB2EV.log
32TH RB2TB2EV.cfd

```

```

imur Minimum Wind Speed (m/s) = .5
face Surface roughness length (m) = .20
tor Sector averaging constant = 4.3

```

```

tial Initial value of sigma y = .00
tial Initial value of sigma z = .00

```

```

ande Expanded output for code testing not selected

```

```

al r Total number of hours of data processed = 43824
rs c Hours of missing data = 297
rs c Hours direction in window = 5830
rs c Hours elevated plume w/ dir. in window = 0
rs c Hours of calm winds = 454
rs c Hours direction not in window or calm = 37243

```

TRIH DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

. PH	AVR. PER.	1	2	4	8	12	24	96	168	360	720
R L	UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
N L	LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
RAI	ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
RAI	IN RANGE	6284.	7988.	10648.	14825.	18317.	25854.	40946.	42128.	42457.	43155.
RAI	BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZH	ZERO	37243.	35493.	32754.	28431.	24983.	17299.	2011.	493.	0.	0.
L X	TOTAL X/Qs	43527.	43481.	43402.	43256.	43300.	43153.	42957.	42621.	42457.	43155.
N ZH	% NON ZERO	14.44	18.37	24.53	34.27	42.30	59.91	95.32	98.84	100.00	100.00

h PH 95th PERCENTILE X/Q VALUES

1.36E-03	1.33E-03	1.25E-03	1.11E-03	8.93E-04	5.94E-04	3.13E-04	2.63E-04	2.25E-04	2.02E-04
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

X/Q 95% X/Q for standard averaging intervals

o 2	0 to 2 hours	1.36E-03
o 8	2 to 8 hours	1.03E-03
o 24	8 to 24 hours	3.36E-04
o 4	1 to 4 days	2.20E-04
o 30	4 to 30 days	1.85E-04

		HOURLY VALUE RANGE	
		MAX X/Q	MIN X/Q
CE	CENTERLINE	1.82E-03	2.78E-04
SE	SECTOR-AVERAGE	1.06E-03	1.62E-04

NRGORMAL PROGRAM COMPLETION

**Attachment 3 – RB2SGTSV.log
ARCON96 Output
for
Standby Gas Treatment System Exhaust Vent**

RB2SGTSV.log

FTitrogram Title: ARCON96.

Develoed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NACNRC Contacts: J. Y. Lee Phone: (301) 415 1080
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J. J. Hayes Phone: (301) 415 3167
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Calcode Developer: J. V. Ramsdell Phone: (509) 372 6316
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Code Documentation: NUREG/CR-6331 Rev. 1

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Program Run 7/ 9/2005 at 06:43:20

* AF***** ARCON INPUT *****

per Number of Meteorological Data Files = 1
sorc Meteorological Data File Names
:\AF C:\ARCON96\SQ99_0~1.MET

yht Height of lower wind instrument (m) = 10.0
yht Height of upper wind instrument (m) = 60.0
1 st Wind speeds entered as miles per hour

ind- Ground-level release
sae Release height (m) = .0
ldir Building Area (m^2) = 2685.0
luer Effluent vertical velocity (m/s) = .00
t oi Vent or stack flow (m^3/s) = .00
t oi Vent or stack radius (m) = .00

```

act1 Direction .. intake to source (deg) = 320
l di Wind direction sector width (deg) = 90
l di Wind direction window (deg) = 275 - 005
anc Distance to intake (m) = 61.0
ke Intake height (m) = .0
ain Terrain elevation difference (m) = .0

```

```

out Output file names
2sg RB2sgtsv.log
2sg RB2sgtsv.cfd

```

```

mmum Minimum Wind Speed (m/s) = .5
lace Surface roughness length (m) = .20
or Sector averaging constant = 4.3

```

```

ial Initial value of sigma y = .00
ial Initial value of sigma z = .00

```

```

nde Expanded output for code testing not selected

```

```

l n Total number of hours of data processed = 43824
s o Hours of missing data = 297
s d Hours direction in window = 5965
s e Hours elevated plume w/ dir. in window = 0
s o Hours of calm winds = 454
s d Hours direction not in window or calm = 37108

```

TRIB DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

PE	AVER. PER.	1	2	4	8	12	24	96	168	360	720
LI	UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LI	LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
RAN	ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
RAN	IN RANGE	6419.	8132.	10828.	15071.	18596.	26160.	40812.	42116.	42457.	43155.
RAN	BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZE	ZERO	37108.	35349.	32574.	28185.	24704.	16993.	2145.	505.	0.	0.
X/	TOTAL X/Qs	43527.	43481.	43402.	43256.	43300.	43153.	42957.	42621.	42457.	43155.
ZE	% NON ZERO	14.75	18.70	24.95	34.84	42.95	60.62	95.01	98.82	100.00	100.00

```

PE 95th PERCENTILE X/Q VALUES
1.45E-03 1.40E-03 1.33E-03 1.20E-03 9.51E-04 6.37E-04 3.31E-04 2.81E-04 2.42E-04 2.19E-04

```

```

X/Q 95% X/Q for standard averaging intervals

```

```

2 0 to 2 hours 1.45E-03
8 2 to 8 hours 1.12E-03
24 8 to 24 hours 3.55E-04
4 1 to 4 days 2.29E-04
30 4 to 30 days 2.01E-04

```


		HOURLY VALUE RANGE	
		MAX X/Q	MIN X/Q
CE	CENTERLINE	1.91E-03	2.92E-04
SE	SECTOR-AVERAGE	1.11E-03	1.70E-04

PROGRAMAL PROGRAM COMPLETION

Attachment 4 – RB2MSTP.log
ARCON96 Output
for
Reactor Building Unit 2 Main Steam Tunnel Blowout Panel

RB2MSTP.log

ITi@rogram Title: ARCON96.

Bd Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

I Data: June 25, 1997 11:00 a.m.

MacNRC Contacts: J. Y. Lee Phone: (301) 415 1080
e-mail: jy11@nrc.gov
J. J. Hayes Phone: (301) 415 3167
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L. A. Brown Phone: (301) 415 1232
e-mail: lab2@nrc.gov

CalCode Developer: J. V. Ramsdell Phone: (509) 372 6316
e-mail: j_ramsdell@pnl.gov

CumCode Documentation: NUREG/CR-6331 Rev. 1

TranThe program was prepared for an agency of the United States Government. Neither
ted:he United States Government nor any agency thereof, nor any of their
es, employees, makes any warranty, expressed or implied, or assumes any legal
ly disability or responsibilities for any third party's use, or the results of such
anyse, of any portion of this program or represents that its use by such third
puloarty would not infringe privately owned rights.

IRur@rogram Run 7/ 9/2005 at 10:34:08

* AF***** ARCON INPUT *****

ver Number of Meteorological Data Files = 1
sorc Meteorological Data File Names
:\AF C:\ARCON96\SQ99_0-1.MET

yht Height of lower wind instrument (m) = 10.0
yht Height of upper wind instrument (m) = 60.0
i sy Wind speeds entered as miles per hour

ind- Ground-level release
ase Release height (m) = 40.4
ldir Building Area (m^2) = 2685.0
luer Effluent vertical velocity (m/s) = .00
: or Vent or stack flow (m^3/s) = .00
: or Vent or stack radius (m) = .00

```

acti Direction .. intake to source (deg) = 299
l di Wind direction sector width (deg) = 90
l di Wind direction window (deg) = 254 - 344
:anc Distance to intake (m) = 47.3
:ake Intake height (m) = 61.6
:air Terrain elevation difference (m) = 0

```

```

out Output file names
:2MS RB2MSTP.log
:2MS RB2MSTP.cfd

```

```

:umw Minimum Wind Speed (m/s) = .5
:face Surface roughness length (m) = .20
:cor Sector averaging constant = 4.3

```

```

:ial Initial value of sigma y = .00
:ial Initial value of sigma z = .00

```

```

:nde Expanded output for code testing not selected

```

```

:al r Total number of hours of data processed = 43824
:as c Hours of missing data = 297
:as c Hours direction in window = 6493
:as c Hours elevated plume w/ dir. in window = 0
:as c Hours of calm winds = 668
:as c Hours direction not in window or calm = 36366

```

DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

PER	AVER. PER.	1	2	4	8	12	24	96	168	360	720
LI	UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LI	LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
RAN	ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
RAN	IN RANGE	7161.	9051.	11968.	16489.	20083.	27657.	41411.	42301.	42457.	43155.
RAN	BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZE	ZERO	36366.	34430.	31434.	26767.	23217.	15496.	1546.	320.	0.	0.
X/	TOTAL X/Qs	43527.	43481.	43402.	43256.	43300.	43153.	42957.	42621.	42457.	43155.
ZE	% NON ZERO	16.45	20.82	27.57	38.12	46.38	64.09	96.40	99.25	100.00	100.00

95th PERCENTILE X/Q VALUES

	1	2	4	8	12	24	96	168	360	720
	1.94E-03	1.86E-03	1.71E-03	1.55E-03	1.26E-03	8.57E-04	4.60E-04	3.85E-04	3.28E-04	2.94E-04

95% X/Q for standard averaging intervals

Interval	95% X/Q
0 to 2 hours	1.94E-03
2 to 8 hours	1.41E-03
8 to 24 hours	5.12E-04
1 to 4 days	3.28E-04
4 to 30 days	2.68E-04

		HOURLY VALUE RANGE	
		MAX X/Q	MIN X/Q
CE	CENTERLINE	2.89E-03	2.36E-04
SE	SECTOR-AVERAGE	1.68E-03	1.38E-04

NROGORMAL PROGRAM COMPLETION

Attachment 5 – RB2TBMST.log
ARCON96 Output
for
Turbine Building Unit 2 Main Steam Tunnel Blowout Panel

RB2TBMST.log
ARCON96 Output
for
Turbine Building Unit 2 Main Steam Tunnel Blowout Panel

RB2TBMST.log

Program Title: ARCON96.

Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NRC Contacts: J. Y. Lee Phone: (301) 415 1080
e-mail: jy11@nrc.gov
J. J. Hayes Phone: (301) 415 3167
e-mail: jjh@nrc.gov
L. A. Brown Phone: (301) 415 1232
e-mail: lab2@nrc.gov

Code Developer: J. V. Ramsdell Phone: (509) 372 6316
e-mail: j_ramsdell@pnl.gov

Code Documentation: NUREG/CR-6331 Rev. 1

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Program Run 7/ 9/2005 at 10:39:56

***** ARCON INPUT *****

Number of Meteorological Data Files = 1
Meteorological Data File Names
:\AF C:\ARCON96\SQ99_0~1.MET

Height of lower wind instrument (m) = 10.0
Height of upper wind instrument (m) = 60.0
Wind speeds entered as miles per hour

Ground-level release
Release height (m) = 14.5
Building Area (m^2) = 2685.0
Effluent vertical velocity (m/s) = .00
Vent or stack flow (m^3/s) = .00
Vent or stack radius (m) = .00

acti Direction .. intake to source (deg) = 255
 l di Wind direction sector width (deg) = 90
 l di Wind direction window (deg) = 210 - 300
 anc Distance to intake (m) = 40.8
 ke Intake height (m) = 61.6
 ain Terrain elevation difference (m) = 1.8

ut Output file names
 2TB RB2TBMST.log
 2TB RB2TBMST.cfd

mum Minimum Wind Speed (m/s) = .5
 ace Surface roughness length (m) = .20
 or Sector averaging constant = 4.3

ial Initial value of sigma y = .00
 ial Initial value of sigma z = .00

unde Expanded output for code testing not selected

l n Total number of hours of data processed = 43824
 :s c Hours of missing data = 297
 :s d Hours direction in window = 9752
 :s e Hours elevated plume w/ dir. in window = 0
 :s c Hours of calm winds = 454
 :s d Hours direction not in window or calm = 33321

DRIE DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

PER	AVER. PER.	1	2	4	8	12	24	96	168	360	720
LI	UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LI	LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
RAN	ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
RAN	IN RANGE	10206.	12801.	16612.	22124.	26303.	33407.	42414.	42583.	42457.	43155.
RAN	BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZE	ZERO	33321.	30680.	26790.	21132.	16997.	9746.	543.	38.	0.	0.
X/	TOTAL X/Qs	43527.	43481.	43402.	43256.	43300.	43153.	42957.	42621.	42457.	43155.
ZE	% NON ZERO	23.45	29.44	38.27	51.15	60.75	77.42	98.74	99.91	100.00	100.00

95th PERCENTILE X/Q VALUES

1.47E-03	1.40E-03	1.27E-03	1.13E-03	9.07E-04	6.43E-04	3.82E-04	3.24E-04	2.87E-04	2.47E-04
----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

X/Q 95% X/Q for standard averaging intervals

2	0 to 2 hours	1.47E-03
8	2 to 8 hours	1.01E-03
24	8 to 24 hours	4.01E-04
4	1 to 4 days	2.95E-04
30	4 to 30 days	2.26E-04

		HOURLY VALUE RANGE	
		MAX X/Q	MIN X/Q
CE	CENTERLINE	2.02E-03	2.21E-04
SE	SECTOR-AVERAGE	1.18E-03	1.29E-04

NROGORMAL PROGRAM COMPLETION

Attachment 6 –Building Cross Sectional Area Calculation

Analysis Of Vertical Cross-Sectional Area (Minimum) Of Reactor Building For Evaluation Of χ/Q 's

The general arrangement of the reactor building is shown in SSES design drawing E106312, Revision F (Reference 9). Above the turbine building roof elevation, the reactor building area includes the superstructure area and the area associated with the blowout panels and duct spaces between Column Lines P and M (see SSES design drawing E105004, Sheet 6, Revision 22; Reference 23). Below the turbine building roof elevation, credit is only taken for the reactor building area between Column Lines U and P, including the concrete outer walls.

1. Reactor Building Roof to Bottom Of Superstructure

References: SSES Drawings

E105007, Sheet 1, Revision 9 (Reference 20)

E105329, Revision 9 (Reference 24)

Reactor Building Roof Elevation = $873'-1\frac{1}{2}" = 873.12 \text{ ft}$

Superstructure Bottom Elevation = $809'-7\frac{5}{8}" = 809.64 \text{ ft}$

$\therefore \text{Height} = 873.12 \text{ ft} - 809.64 \text{ ft} = 63.49 \text{ ft}$

Width Of Superstructure = $161'-9\frac{5}{8}" = 161.80 \text{ ft}$

Area = $63.49 \text{ ft} \times 161.80 \text{ ft} = 10273 \text{ ft}^2$

2. Reactor Building Bottom Of Superstructure to Turbine Building Roof Elevation

References: SSES Drawings

E105004, Sheet 7, Revision 27 (Reference 11)

E105007, Sheet 1, Revision 9 (Reference 20)

E105004, Sheet 6, Revision 6 (Reference 22)

E105329, Revision 9 (Reference 24)

E105257, Revision 9 (Reference 25)

E105259, Revision 8 (Reference 26)

E105004, Sheet 5, Revision 27 (Reference 27)

Superstructure Bottom Elevation = $809'-7\frac{5}{8}" = 809.64 \text{ ft}$

Turbine Building Roof Elevation = $789'-8\frac{3}{4}" = 789.73 \text{ ft}$

$\therefore \text{Height} = 809.64 \text{ ft} - 789.73 \text{ ft} = 19.91 \text{ ft}$

Width = $(1'-6") + \text{Distance Column U to Column P} + (16'-0") + (1'-9\frac{5}{16}")$

Width = $(1'-6") + (26'-6") + (27'-6") + (17'-6") + (8'-0") + (25'-6") + (29'-0")$
 $+ (16'-0") + (1'-9\frac{5}{16}")$

Width = 153.28 ft

Area = $19.91 \text{ ft} \times 153.28 \text{ ft} = 3052 \text{ ft}^2$

$+ (16'-0") + (1'-9\frac{5}{16}")$

Width = 153.28 ft

3. Turbine Building Roof Elevation to Grade Elevation

References: SSES Drawings

E105007, Sheet 1, Revision 9 (Reference 20)

E105257, Revision 9 (Reference 25)

E105259, Revision 8 (Reference 26)

Turbine Building Roof Elevation = $789'-8\frac{3}{4}" = 789.73 \text{ ft}$

Grade Elevation = $676'-0"$

$\therefore \text{Height} = 789.73 \text{ ft} - 676 \text{ ft} = 113.73 \text{ ft}$

Width = $(1'-6") + \text{Distance Column U to Column P} + (1'-6")$

Width = $(1'-6") + (26'-6") + (27'-6") + (17'-6") + (8'-0") + (25'-6") + (29'-0") + (1'-6")$

Width = 137 ft

Area = $113.73 \text{ ft} \times 137 \text{ ft} = 15581 \text{ ft}^2$

4. Total Reactor Building Minimum Cross-Sectional Area

Total Area = $10273 \text{ ft}^2 + 3052 \text{ ft}^2 + 15581 \text{ ft}^2$

Total Area = $28906 \text{ ft}^2 \times (.0929 \text{ m}^2 / \text{ft}^2) = 2685 \text{ m}^2$