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U. S. Nuclear Regulatory Commission
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Ladies and Gentlemen:

ULNRC-05219



**DOCKET NUMBER 50-483
CALLAWAY PLANT UNIT 1
FIGURE 14.9 CALLAWAY PLANT
PRESSURE AND TEMPERATURE LIMITS REPORT**

Attached is the Callaway Plant Pressure and Temperature Limits Report (PTLR), Revision 4. Revision 4 incorporates changes associated with the Replacement Steam Generator Program. This report is provided to the NRC Staff for information. It has been prepared in accordance with the requirements of Technical Specification 5.6.6.c.

If you have any questions concerning this report, please contact us.

Very truly yours,

A handwritten signature in black ink that reads "Keith D. Young".

Keith D. Young
Manager, Regulatory Affairs

DJW/jdg

Attachment: Callaway Pressure and Temperature Limits Report, Revision 4

A001

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FIGURE 14.9
CALLAWAY PLANT
PRESSURE AND TEMPERATURE LIMITS REPORT
Revision 4

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

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Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

1.0 Reactor Coolant System (RCS) Pressure and Temperature Limits Report (PTLR)

This PTLR for Callaway Plant has been prepared in accordance with the requirements of Technical Specification (TS) 5.6.6. The TS addressed in this report are listed below:

LCO 3.4.3 RCS Pressure and Temperature (P/T) Limits

LCO 3.4.12 Cold Overpressure Mitigation System (COMS)

2.0 Operating Limits

The parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. The limits were developed in accordance with the NRC-approved methodology specified in Specification 5.6.6 (Ref. 1). NRC approval of this methodology was received in Amendment No. [134], (Ref. 3).

The methodology listed in WCAP-14040-NP-A, Revision 2 was used with one exception:

- a) ASME Code Case N-514 was used.

The revised P/T Limit curves account for a requirement of 10 CFR 50, Appendix G, that the temperature of the closure head flange and vessel flange regions must be at least 120°F higher than the limiting RT_{NOT} for these regions when the pressure exceeds 20% of the preservice hydrostatic test pressure (3107 psig).

2.1 RCS Pressure and Temperature (P/T) Limits (LCO 3.4.3)

2.1.1 The RCS temperature rate-of-change limits are:

- a. A maximum heatup of 100°F in any 1-hour period.
- b. A maximum cooldown of 100°F in any 1-hour period.
- c. A maximum temperature change of 10°F in any 1-hour period during inservice hydrostatic and leak testing operations above the heatup and cooldown limit curves.

2.1.2 The RCS P/T limits for heatup, cooldown, inservice hydrostatic and leak testing, and criticality are specified by Figures 2.1-1 and 2.1-2.

2.2 Cold Overpressure Mitigation System (COMS) Setpoints (LCO 3.4.12)

The pressurizer power-operated relief valves (PORVs) shall each have lift settings in accordance with Figure 2.2-1. The (COMS) arming temperature is 275°F. These lift setpoints have been developed using the NRC approved methodologies specified in Technical Specification 5.6.6.

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

2.2 (continued)

The maximum allowed PORV setpoint for COMS is derived by analysis which models the performance of the COMS assuming limiting mass and heat input transients with incorporation of 10% relaxation of the Appendix G limits in accordance with ASME Code Case N-514. Operation with a PORV setpoint less than or equal to the maximum setpoint ensures that Appendix G criteria will not be violated with consideration for: (1) pressure and temperature instrumentation uncertainties; (2) single failure of one PORV; and (3) effects of reactor coolant pump operation.

To ensure mass and heat input transients more severe than those assumed cannot occur, Technical Specifications place limitations on the number of safety injection pumps and centrifugal charging pumps that are capable of injecting, unisolating accumulators, and starting reactor coolant pumps during the appropriate COMS MODES. These limitations are outlined in TS LCO 3.4.6, LCO 3.4.7, and LCO 3.4.12.

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

MATERIAL PROPERTY BASIS

LIMITING MATERIAL: LOWER SHELL PLATE R2708-3
LIMITING ART VALUES AT 20 EFPY: 1/4T, 100.4°F
3/4T, 84.2°F

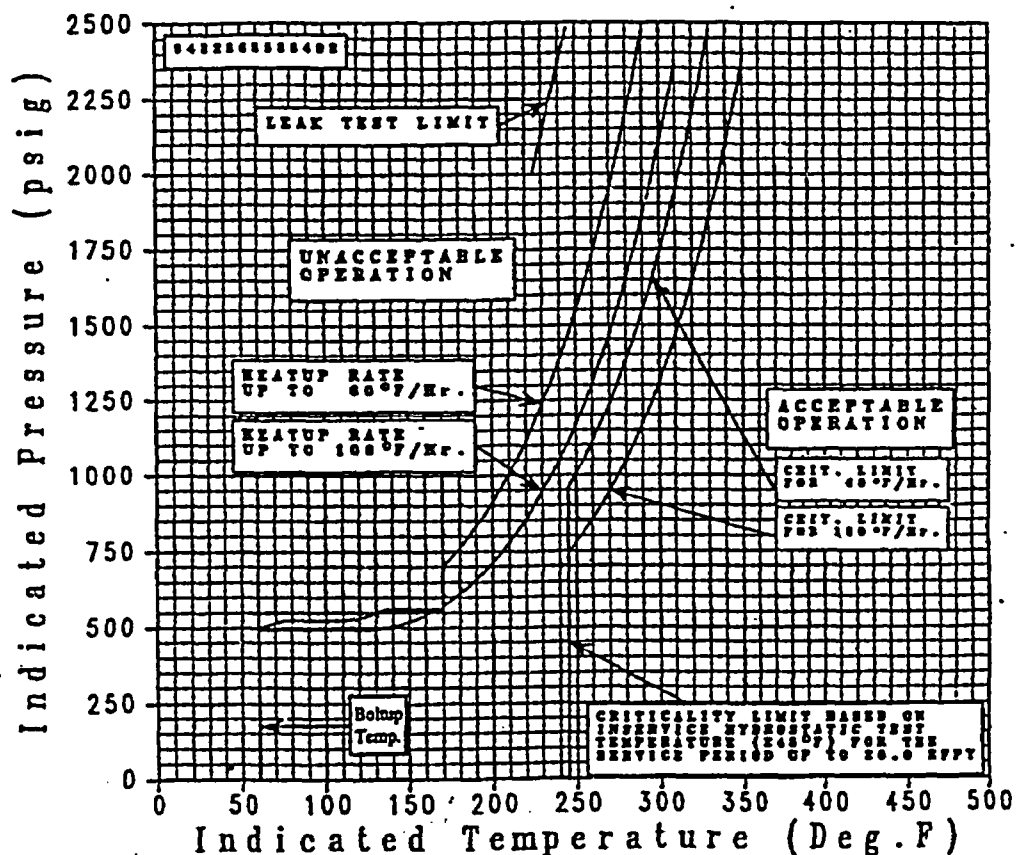


FIGURE 2.1-1 Callaway Unit 1 Reactor Coolant System Heatup Limitations (Heatup Rates of 60 and 100°F/hr) Applicable for the First 20 EFPY (With Margins for Instrumentation Errors). Includes vessel flange requirements of 170°F and 561 psig per 10CFR 50, Appendix G.

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

TABLE 2.1-1									
Callaway Plant Heatup Limits at 20 EPFY									
With Margins for Instrumentation Errors									
60°F/hr		60°F/hr Crit. Limit		100°F/hr		100°F/hr Crit. Limit		Leak Test Limit	
Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)
60	0	245	0	60	0	245	0	225	2000
60	500	245	544	60	494	245	546	245	2485
65	507	245	533	65	494	245	531		
70	516	245	527	70	494	245	519		
75	524	245	524	75	494	245	509		
80	524	245	524	80	494	245	502		
85	524	245	527	85	494	245	497		
90	524	245	533	90	494	245	494		
95	524	245	541	95	494	245	494		
100	524	245	551	100	494	245	495		
105	524	245	563	105	494	245	499		
110	524	245	577	110	494	245	504		
115	527	245	593	115	494	245	511		
120	533	245	611	120	494	245	520		
125	541	245	631	125	494	245	531		
130	551	245	653	130	495	245	643		
135	561	245	677	135	499	245	557		
140	561	245	703	140	504	245	574		
145	561	245	732	145	511	245	592		
150	561	245	763	150	520	245	612		
155	561	245	796	155	531	245	634		
160	561	245	832	160	543	245	658		
165	561	245	871	165	557	245	685		
170	561	245	912	170	561	245	714		
170	703	245	957	170	574	245	745		
175	732	250	1006	175	592	250	779		
180	763	255	1058	180	612	255	816		
185	796	260	1113	185	634	260	856		
190	832	265	1173	190	658	265	899		
195	871	270	1238	195	685	270	946		
200	912	275	1306	200	714	275	996		
205	957	280	1381	205	745	280	1049		
210	1006	285	1460	210	779	285	1107		
215	1058	290	1544	215	816	290	1169		
220	1113	295	1636	220	856	295	1236		
225	1173	300	1732	225	899	300	1307		
230	1238	305	1837	230	946	305	1384		
235	1306	310	1948	235	996	310	1467		
240	1381	315	2066	240	1049	315	1555		
245	1460	320	2193	245	1107	320	1649		
250	1544	325	2328	250	1169	325	1750		
255	1636	330	2472	255	1236	330	1858		
260	1732			260	1307	335	1973		
265	1837			265	1384	340	2096		
270	1948			270	1467	345	2227		
275	2066			275	1555	350	2367		
280	2193			280	1649				
285	2328			285	1750				
290	2472			290	1858				
				295	1973				
				300	2096				
				305	2227				
				310	2367				

**Figure 14.9.
PRESSURE AND TEMPERATURE LIMITS REPORT**

MATERIAL PROPERTY BASIS

LIMITING MATERIAL: LOWER SHELL PLATE R2708-3

LIMITING ART VALUES AT 20 EFY: 1/4T, 100.4°F

3/4T, 84.2 °F

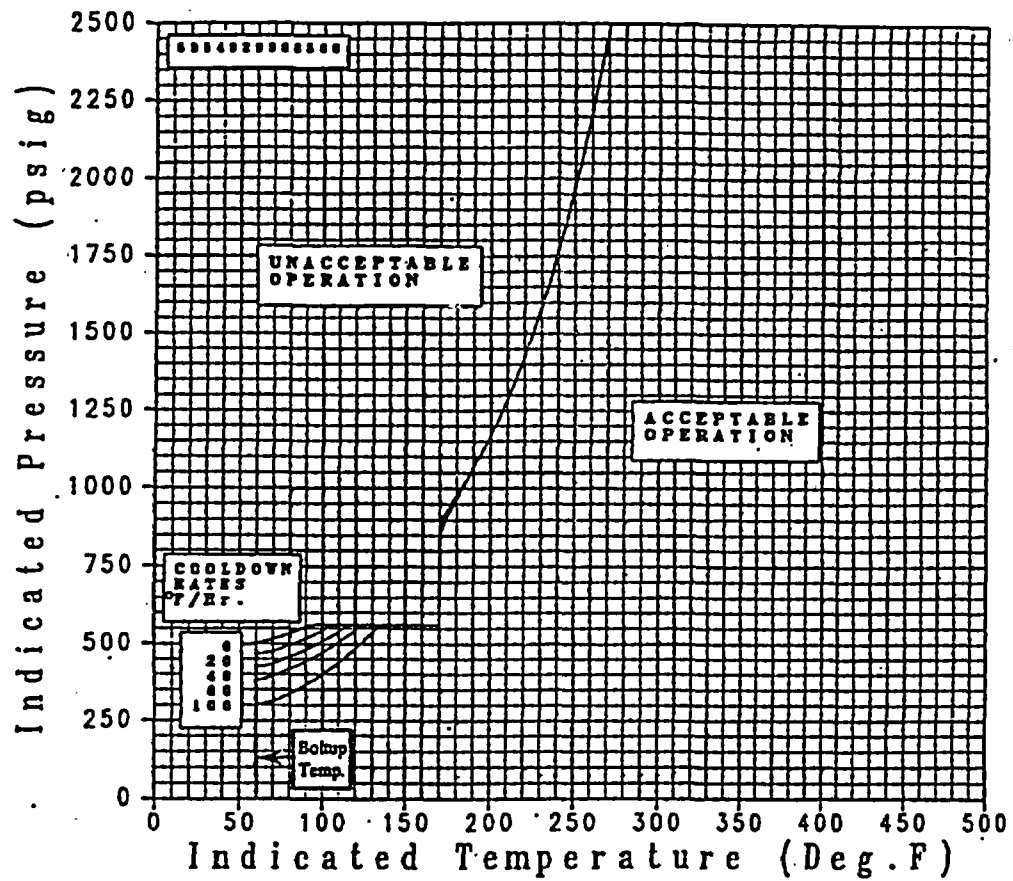


FIGURE 2.1-2 Callaway Unit 1 Reactor Coolant System Cooldown Limitations (Cooldown Rates of 0, 20, 40, 60 and 100°F/hr) Applicable for the First 20 EFY (With Margins for Instrumentation Errors). Includes vessel flange requirements of 170°F and 561 psig per 10CFR 50, Appendix G

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT.

TABLE 2.1-2									
Callaway Plant Cooldown Limits at 20 EFPY									
With Margins for Instrumentation Errors									
Steady State		20°F/hr		40°F/hr		60°F/hr		100°F/hr	
Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)	Temp. (°F)	Press. (psig)
60	0	60	0	60	0	60	0	60	0
60	500	60	468	60	427	60	386	60	302
65	507	65	468	65	427	65	386	65	302
70	516	70	476	70	436	70	396	70	313
75	525	75	486	75	446	75	406	75	325
80	534	80	496	80	457	80	418	80	338
85	544	85	506	85	468	85	430	85	351
90	555	90	518	90	481	90	443	90	366
95	561	95	531	95	494	95	457	95	382
100	561	100	544	100	508	100	472	100	400
105	561	105	559	105	524	105	489	105	419
110	561	110	561	110	540	110	506	110	439
115	561	115	561	115	550	115	526	115	461
120	561	120	561	120	561	120	546	120	485
125	561	125	561	125	561	125	561	125	511
130	561	130	561	130	561	130	561	130	539
135	561	135	561	135	561	135	561	135	561
140	561	140	561	140	561	140	561	140	561
145	561	145	561	145	561	145	561	145	561
150	561	150	561	150	561	150	561	150	561
155	561	155	561	155	561	155	561	155	561
160	561	160	561	160	561	160	561	160	561
165	561	165	561	165	561	165	561	165	561
170	561	170	561	170	561	170	561	170	561
170	899	170	885	170	873	170	864	170	856
175	937	175	925	175	917	175	911	175	910
180	977	180	969	180	963	180	961	180	969
185	1020	185	1015	185	1014	185	1016		
190	1066	190	1065						
195	1116								
200	1170								
205	1228								
210	1289								
215	1355								
220	1426								
225	1503								
230	1584								
235	1672								
240	1766								
245	1866								
250	1973								
255	2088								
260	2211								
265	2342								
270	2482								

Figure 14.9
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CALLAWAY COMS
Maximum Allowable PORV Setpoints

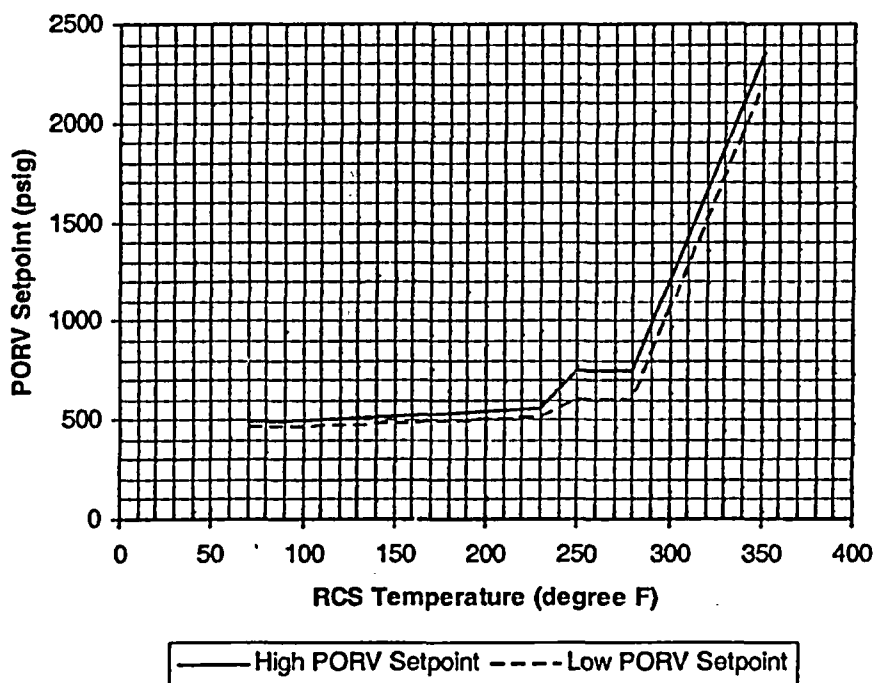


Figure 2.2-1 Maximum Allowed PORV Setpoint for the Cold Overpressure Mitigation System

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

TABLE 2.2-1
CALLAWAY PLANT COMS MAXIMUM ALLOWABLE PORV SETPOINTS AT 20 EFPY

Breakpoint Number	Maximum Allowable Function Generator Setpoints (Breakpoints)		Low Setpoint (psig)
	Temperature – RCS (°F)	High Setpoint (psig)	
1	70	496	466
2	80	496	466
3	90	496	466
4	180	527	497
5	230	558	512
6	250	750	597
7	270	750	597
8	280	750	597
9	350	2335	2185

Note: Setpoints assume that all 4 or less RCPs are in operation.

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

3.0 Reactor Vessel Material Surveillance Program

The reactor vessel material surveillance program is in compliance with Appendix H to 10 CFR 50, entitled "Reactor Vessel Material Surveillance Program Requirements" and Section 5.3 of the Callaway Final Safety Analysis Report. The surveillance capsule withdrawal schedule is presented in FSAR Table 5.3-10. The surveillance capsule reports are as follows:

1. WCAP-11374, Revision 1, June 1987, "Analysis of Capsule U from the Union Electric Company Callaway Unit 1 Reactor Vessel Radiation Surveillance Program."
2. WCAP-12946, June 1991, "Analysis of Capsule Y from the Union Electric Company Callaway Unit 1 Reactor Vessel Radiation Surveillance Program."
3. WCAP-14895, July 1997, "Analysis of Capsule V from the Union Electric Company Callaway Unit 1 Reactor Vessel Radiation Surveillance Program."
4. WCAP-15400, June 2000, "Analysis of Capsule X from the AmerenUE Callaway Unit 1 Reactor Vessel Radiation Surveillance Program."

4.0 Reactor Vessel Surveillance Data Credibility

Regulatory Guide 1.99, Revision 2, describes general procedures acceptable to the NRC staff for calculating the effects of neutron radiation embrittlement of the low-alloy steels currently used for light-water-cooled reactor vessels. Position C.2 of Regulatory Guide 1.99, Revision 2, describes the method for calculating the adjusted reference temperature and Charpy upper-shelf energy of reactor vessel beltline materials using surveillance capsule data. The methods of Position C.2 can only be applied when two or more credible surveillance data sets become available from the reactor in question.

To date four surveillance capsules have been removed and analyzed from the Callaway Plant reactor vessel. To use these surveillance data sets, they must be shown to be credible. In accordance with the discussion of Regulatory Guide 1.99, Revision 2, there are five requirements that must be met for the surveillance data to be judged credible.

The purpose of this evaluation is to apply the credibility requirements of Regulatory Guide 1.99, Revision 2, to the Callaway Plant reactor vessel surveillance data and determine if the Callaway Plant surveillance data is credible.

Criterion 1: Materials in the capsules should be those judged most likely to be controlling with regard to radiation embrittlement.

The beltline region of the reactor vessel is defined in Appendix G to 10 CFR Part 50, "Fracture Toughness Requirements," as follows:

"the reactor vessel (shell material including welds, heat affected zones, and plates or forgings) that directly surrounds the effective height of the active core and adjacent regions of the reactor vessel that are predicted to experience sufficient neutron radiation damage to be considered in the selection of the most limiting material with regard to radiation damage."

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The Callaway Plant reactor vessel consists of the following beltline region materials:

- Intermediate shell plate R2707-1,
- Intermediate shell plate R2707-2,
- Intermediate shell plate R2707-3,
- Lower shell plate R2708-1,
- Lower shell plate R2708-2,
- Lower shell plate R2708-3, and
- Intermediate shell longitudinal weld seams, lower shell longitudinal weld seams, and an intermediate to lower shell circumferential weld seam. All vessel beltline weld seams were fabricated with weld wire heat number 90077. The intermediate to lower shell circumferential weld seam 101-171 was fabricated with Flux Type 124 Lot Number 1061. The intermediate and lower shell longitudinal weld seams were fabricated with Flux Type 0091 Lot Number 0842.

The Callaway Plant surveillance program utilizes longitudinal and transverse test specimens from lower shell plate R2708-1. The surveillance weld metal was fabricated with weld wire heat number 90077, Flux Type 124 Lot Number 1061.

At the time when the surveillance program was selected it was believed that copper and phosphorus were the elements most important to embrittlement of reactor vessel steels. Since all plate materials had approximately the same content of copper and phosphorus, lower shell plate R2708-1 was chosen for the surveillance program since it had the highest initial RT_{NDT} and the lowest initial upper shelf energy of the plate material. In addition, the current pressurized thermal shock (PTS) evaluation shows that if surveillance data is not used, lower shell plate R2708-1 is the plate that is predicted to have the highest embrittlement rate.

Per Regulatory Guide 1.99, Revision 2, "weight-percent copper" and "weight-percent nickel" are the best-estimate values for the material, which will normally be the mean of the measured values for a plate or forging or for weld samples made with the weld wire heat number that matches the critical vessel weld. Since the surveillance weld metal was made with the same weld wire heat as all of the vessel beltline weld seams, it is representative of the limiting beltline weld metal.

Based on the above discussion, the Callaway Plant surveillance materials are those judged most likely to be controlled with regard to radiation embrittlement and the Callaway Plant surveillance program meets this criteria.

- Criterion 2: Scatter in the plots of Charpy energy versus temperature for the irradiated and unirradiated conditions should be small enough to permit the determination of the 30 ft-lb temperature and upper shelf energy unambiguously.

Plots of Charpy energy versus temperature for the unirradiated and irradiated condition are

Figure 14.9
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presented in WCAP-15400, June 2000, "Analysis of Capsule X from the AmerenUE Callaway Unit 1 Reactor Vessel Radiation Surveillance Program."

Based on engineering judgement, the scatter in the data presented in these plots is small enough to permit the determination of the 30 ft-lb temperature and the upper shelf energy of the Callaway Plant surveillance materials unambiguously. Hence, the Callaway Plant surveillance program meets this criterion.

Criterion 3: When there are two or more sets of surveillance data from one reactor, the scatter of ΔRT_{NDT} values about a best-fit line drawn as described in Regulatory Position 2.1 normally should be less than 28°F for welds and 17°F for base metal. Even if the fluence range is large (two or more orders of magnitude), the scatter should not exceed twice those values. Even if the data fail this criterion for use in shift calculations, they may be credible for determining decrease in upper shelf energy if the upper shelf can be clearly determined, following the definition given in ASTM E185-82.

The functional form of the least squares method as described in Regulatory Position 2.1 will be utilized to determine a best-fit line for this data and to determine if the scatter of the ΔRT_{NDT} values about this line is less than 28°F for welds and less than 17°F for the plate.

Following is the calculation of the best-fit line as described in Regulatory Position 2.1 of Regulatory Guide 1.99, Revision 2.

Figure 14.9
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Table 4.0-1 Callaway Plant Surveillance Capsule Data						
Material	Capsule	Capsule F^(a)	FF^(b)	ΔRT_{NDT}^(c)	FF X ΔRT_{NDT}	FF²
Lower Shell R2708-1 (Longitudinal)	U	0.331	0.696	0.0 ^(e)	0.0	0.48
	Y	1.27	1.07	25.15	26.91	1.14
	V	2.52	1.25	16.45	20.56	1.56
	X	3.33	1.32	25.71	33.94	1.74
Lower Shell Plate R2708-1 (Transverse)	U	0.331	0.696	25.86	18.00	0.48
	Y	1.27	1.07	46.39	49.64	1.14
	V	2.52	1.25	44.82	56.03	1.56
	X	3.33	1.32	30.77	40.62	1.74
	Sum:		8.6411	215.15	245.7	9.84
Surveillance Weld Material^(d)	$CF_{05} = \sum(FF * RT_{NDT}) + \sum(FF^2) = (245.70) + (9.84) = 25.0^{\circ}F$					
	U	0.331	0.696	68.53 ^(d)	47.70	0.48
	Y	1.27	1.07	36.92 ^(d)	39.50	1.14
	V	2.52	1.25	48.21 ^(d)	60.26	1.56
	X	3.33	1.32	51.81 ^(d)	68.39	1.74
	Sum:		4.32	205.47	215.85	4.92
	$CF_{Surv. Weld} = \sum(FF * RT_{NDT}) + \sum(FF^2) = (215.85^{\circ}F) + (4.92) = 43.9^{\circ}F$					

Notes:

- (a) f = calculated fluence from capsule X dosimetry analysis results, ($\times 10^9$ n/cm², E>1.0 MeV). These values were re-evaluated as part of capsule X analysis. (See Section 6 of WCAP-15400).
- (b) FF = fluence factor = $f^{(0.28 - 0.1 \log f)}$.
- (c) ΔRT_{NDT} values are the measured 30 ft-lb shift.
- (c) These measured ΔRT_{NDT} values do not include the adjustment ratio procedure of Reg. Guide 1.99 Revision 2, Position 2.1, since this calculation is based on the actual surveillance weld metal measured shift values and based on the copper and nickel content the ratio would be 1. In addition, the only surveillance data available is from the Callaway Unit 1 reactor vessel, therefore, no temperature adjustment is required.
- (e) The actual value is -7.33, but for conservatism a value of zero is considered.

The scatter of ΔRT_{NDT} values about the functional form of a best-fit line drawn as described in Regulatory Position 2.1 is presented in Table 4.0-2.

Per the 27th Edition of the CRC Standard Mathematical Tables (page 497), for a straight line fit by the method of least squares, the values b_0 and b_1 are obtained by solving the normal equations

$$\begin{aligned}
 nb_0 + b_1 \sum x_i &= \sum y_i \quad \text{and} \\
 b_0 \sum x_i + b_1 \sum x_i^2 &= \sum x_i y_i
 \end{aligned}$$

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These equations can be re-written as follows ($b_0 = a$ and $b_1 = b$):

$$\sum_{i=1}^n y_i = an + b \sum_{i=1}^n x_i \quad \text{and}$$

$$\sum_{i=1}^n x_i y_i = a \sum_{i=1}^n x_i + b \sum_{i=1}^n x_i^2$$

Lower shell plate R2708-1:

Based on the data provided in Table 4.0-1 these equations become:

$$215.15 = 3a + 8.6411b \quad \text{and}$$

$$245.70 = 8.6411a + 9.84b$$

Thus, $b = 24.8405$ and $a = 0.1669$, and the equation of the straight line which provides the best fit in the sense of least squares is:

$$Y' = 24.8405 (X) + 0.1669$$

The scatter in predicting a value Y corresponding to a given X value is:

$$e = Y - Y'$$

Table 4.0-2 Callaway Plant Lower Shell Plate R2708-1					
Base Material	FF	Measured ΔRT_{NDT} (30 ft-lb)(°F)	Best Fit ^(a) ΔRT_{NDT} (°F)	Scatter of ΔRT_{NDT} (°F)	<17°F (Base Metals)
Lower Shell Plate R2708-1 (Longitudinal)	0.696	0.00	17.4	-17.4	NO
	1.07	25.15	26.75	-1.6	Yes
	1.25	16.45	31.25	-14.8	Yes
	1.32	25.71	33.0	-7.29	Yes
Lower Shell Plate R2708-1 (Transverse)	0.696	25.86	17.4	8.46	Yes
	1.07	46.39	26.75	19.64	NO
	1.25	44.82	31.25	13.57	Yes
	1.32	30.77	33.0	-2.23	Yes

NOTES:

(a) Best Fit Line Per Equation 2 of Reg. Guide 1.99 Rev. 2 Position 1.1.

Figure 14.9
PRESSURE AND TEMPERATURE LIMITS REPORT

Table 4.0-2 indicates that one measured plate ΔRT_{NDT} value is below the lower bound 1σ of $17^\circ F$ by less than $1^\circ F$. Meaning the best fit line is slightly over predicting this measured ΔRT_{NDT} value. Table 4.0-2 also indicates that one measured plate ΔRT_{NDT} value is above the upper bound 1σ of $17^\circ F$ by less than $3^\circ F$. From a statistical point of view $\pm 1\sigma$ ($17^\circ F$) would be expected to encompass 68% of the data. Therefore, it is still statistically acceptable to have two of the plate data points fall outside the $\pm 1\sigma$ bounds. The fact that two of the measured plate ΔRT_{NDT} values are outside of 1σ bound of $17^\circ F$ can be attributed to several factors, such as 1) the inherent uncertainty in Charpy test data, 2) the use of a symmetric hyperbolic tangent Charpy curve fitting program versus an asymmetric tangent Charpy curve fitting program or hand drawn curves using engineering judgment, and/or 3) rounding errors.

In summary, all measured plate is within acceptable range. Therefore, the plate data meets this criteria.

Weld Metal:

Based on the data provided in Table 4.0-1 the equations become:

$$205.47 = 3a + 4.321b \quad \text{and}$$

$$215.13 = 4.321a + 4.897b$$

Thus, $b = 60.9$ and $a = -19.3$, and the equation of the straight line which provides the best fit in the sense of the least squares is:

$$Y' = 60.9 (X) - 19.3$$

The scatter in predicting a value of Y corresponding to a given X value is:

$$e = Y - Y'$$

Table 4.0-3 Callaway Plant Surveillance Weld Metal				
FF	Measured ΔRT_{NDT} (30 ft-lb) ($^\circ F$)	Best Fit ^(a) ΔRT_{NDT} ($^\circ F$)	Scatter of ΔRT_{NDT} ($^\circ F$)	$<28^\circ F$ (Weld Metal)
0.696	68.53	30.55	37.98	NO
1.07	36.92	46.97	-10.05	Yes
1.25	48.21	54.88	-6.67	Yes
1.32	51.81	57.95	-6.14	Yes

NOTES:

(a) Best Fit Line Per Equation 2 of Reg. Guide 1.99 Rev. 2 Position 1.1.

One measured weld ΔRT_{NDT} is below the lower 1σ at $28^\circ F$. The fact that one of the measured weld ΔRT_{NDT} is out of 1σ bound of $28^\circ F$ can be attributed to several factors, such as 1) the inherent uncertainty in Charpy test data, 2) the use of a symmetric hyperbolic tangent Charpy curve fitting program versus an asymmetric tangent Charpy curve fitting program or hand drawn curves using engineering judgement, and/or 3) rounding errors.

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Criterion 4: The irradiation temperature of the Charpy specimens in the capsule should match the vessel wall temperature at the cladding/base metal interface within $\pm 25^{\circ}\text{F}$.

The capsule specimens are located in the reactor between the neutron pads and the vessel wall and are positioned opposite the center of the core. The test capsules are in baskets attached to the neutron pads. The location of the specimens with respect to the reactor vessel beltline provides assurance that the reactor vessel wall and the specimens experience equivalent operating conditions such that the temperatures will not differ by more than 25°F . Hence this criterion is met.

Criterion 5: The surveillance data for the correlation monitor material in the capsule should fall within the scatter band of the data base for that material.

The Callaway Plant surveillance program does not contain correlation monitor material. Therefore, this criterion is not applicable to the Callaway Plant surveillance program.

Based on the preceding positive responses to all five criteria of Regulatory Guide 1.99, Revision 2, Section B, the Callaway Plant surveillance data is credible.

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5.0 Supplemental Data Tables

- Table 5.0-1 Comparison of Callaway Plant Surveillance Material 30-ft-lb Transition Temperature Shifts and Upper Shelf Energy Decreases with Regulatory Guide 1.99, Revision 2, Predictions.
- Table 5.0-2 Calculation of Chemistry Factors Using Surveillance Capsule Data.
- Table 5.0-3 Provides the unirradiated reactor vessel toughness data. The boltup temperature is also included in this Table.
- Table 5.0-4 Provides a summary of the pressure vessel neutron fluence values at 20 EFPY used for the calculation of ART values.
- Table 5.0-5 Provides a summary of the adjusted reference temperature (ARTs) for reactor vessel beltline materials at the $\frac{1}{4}$ -T and $\frac{3}{4}$ -T locations for 20 EFPY.
- Table 5.0-6 Shows the calculation of the ART at 20 EFPY for the limiting reactor vessel material (lower shell plate R-2708-3).
- Table 5.0-7 Provides RT_{PTS} values for 35 EFPY.

6.0 References

1. Technical Specification 5.6.6, "Reactor Coolant System (RCS) PRESSURE AND TEMPERATURE LIMITS REPORT (PTLR)."
2. NRC letter dated [March 24, 2000], [CALLAWAY PLANT, UNIT 1 – ISSUANCE OF AMENDMENT RE: PRESSURE TEMPERATURE LIMITS REPORT]
3. License Amendment No. [134], dated [March 24, 2000], from [Jack Donohew, Senior Project Manager, Section 2] to [Garry L. Randolph, Vice President and Chief Nuclear Officer].
4. WCAP-14040-NP-A, Revision 2, "Methodology Used to Develop Cold Overpressure Mitigating System Setpoints and RCS Heatup and Cooldown Limit Curves," January, 1996.
5. WCAP-16140, July 2004, "Callaway Replacement Steam Generator Program NSSS Engineering Report"

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Table 5.0-1 Comparison of Callaway Unit 1 Surveillance Material 30 ftlb Transition Temperature Shifts and Upper Shelf Energy Decreases with Regulatory Guide 1.99, Revision 2, Predictions						
Materials	Capsule	Fluence ($\times 10^{19}$ n/cm ²)	30 ft-lb Transition Temperature Shift		Upper Shelf Energy Decrease	
			Predicted (°F) ^(a)	Measured (°F) ^(b)	Predicted (%) ^(a)	Measured (%) ^(c)
Lower Shell Plate R2708-1 (Longitudinal)	U	0.331	30.62	0.0 ^(d)	14.5	0
	Y	1.27	47.08	25.15	20	6
	V	1.252	55.0	16.45	23.5	0
	X	3.33	58.08	25.71	25	5
Lower Shell Plate R2708-1 (Transverse)	U	0.331	30.62	25.86	14.5	11
	Y	1.27	47.08	46.39	20	13
	V	1.252	55.0	44.82	23.5	3
	X	3.33	58.08	30.77	25	5
Weld Metal	U	0.331	22.13	68.53	14.5	11
	Y	1.27	34.02	36.92	20	14
	V	1.252	39.75	48.21	23.5	8
	X	3.33	41.98	51.81	25	8
HAZ Metal	U	0.331	—	65.93	—	0
	Y	1.27	—	56.38	—	14
	V	1.252	—	56.1	—	0
	X	3.33	—	42.11	—	0

NOTES:

- (a) Based on Regulatory Guide 1.99, Revision 2, methodology using the mean weight percent values of copper and nickel of the surveillance material.
- (b) Calculated using measured Charpy data plotted using CVGRAPH, Version 4.1.
- (c) Values are based on the definition of upper shelf energy given in ASTM E18582.
- (d) Actual measured value for ΔRT_{NDT} is -7.33 . This physically should not occur, therefore for conservatism a value of zero will be used.

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Table 5.0-2 Calculation of Chemistry Factors Using Surveillance Capsule Data						
Material	Capsule	Capsule f ^(a)	FF ^(b)	ΔRT _{NDT} ^(c)	FF x ΔRT _{NDT}	FF ²
Lower Shell Plate R2708-1 (Longitudinal)	U	0.331	0.696	0.0 ^(e)	0.0	0.48
	Y	1.27	1.07	25.15	26.91	1.14
	V	2.52	1.25	16.45	20.56	1.56
	X	3.33	1.32	25.71	33.94	1.74
Lower Shell Plate R2708-1 (Transverse)	U	0.331	0.696	25.86	18.00	0.48
	Y	1.27	1.07	46.39	49.64	1.14
	V	2.52	1.25	44.82	56.03	1.56
	X	3.33	1.32	30.77	40.62	1.74
	SUM				245.70	9.84
CF _{OS} = Σ(FF * RT _{NDT}) + Σ(FF ²) = (245.70) + (9.84) = 25.0°F						
Surveillance Weld Material ^(d)	U	0.331	0.696	68.53 ^(d)	47.70	0.48
	Y	1.27	1.07	36.92 ^(d)	39.5	1.14
	V	2.52	1.25	48.21 ^(d)	60.26	1.56
	X	3.33	1.32	51.81 ^(d)	68.39	1.74
	SUM				215.85	4.92
CF _{Surv. Weld} = Σ(FF * RT _{NDT}) + Σ(FF ²) = (215.85°F) + (4.92) = 43.9°F						

NOTES:

- (a) f = calculated fluence from capsule X dosimetry analysis results, (10^8 n/cm², E > 1.0 MeV). All updated fluence values from the Capsule X analysis (Table C-1 of WCAP 15400).
- (b) FF = fluence factor = $f^{(0.28 - 0.1 \log f)}$.
- (c) ΔRT_{NDT} values are the measured 30 ft-lb shift.
- (d) These measured ΔRT_{NDT} values do not include the adjustment ratio procedure of Reg. Guide 1.99 Revision 2, Position 2.1, since this calculation is based on the actual surveillance weld metal measured shift values and based on the copper and nickel content the ratio would be 1. In addition, the only surveillance data available is from the Callaway Unit 1 reactor vessel, therefore, no temperature adjustment is required.
- (e) The actual value is -7.33, but for conservatism a value of zero is considered.

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TABLE 5.0-3			
Reactor Vessel Beltline Material Unirradiated Toughness Properties			
Material Description	Cu (%)	Ni(%)	Initial RT_{NDT}^(a)
Closure Head Flange R2704-1	--	--	30°F ^(c)
Vessel Flange R2701-1	--	--	40°F ^(c)
Intermediate Shell Plate R2707-1	0.05	0.58	40°F
Intermediate Shell Plate R2707-2	0.06	0.61	10°F
Intermediate Shell Plate R2707-3	0.06	0.62	-10°F
Lower Shell Plate R2708-1	0.07	0.58	50°F
Lower Shell Plate R2708-2	0.06	0.57	10°F
Lower Shell Plate R2708-3	0.08	0.62	20°F
Intermediate and Lower Shell Longitudinal Weld Seams ^(b)	0.04	0.06	-60°F
Intermediate to Lower Shell Circumferential Weld Seam ^(b)	0.04	0.06	-60°F

^(a) The initial RT_{NDT} values for the plates and welds are based on measured data (WCAR-12948).

^(b) All vessel beltline weld seams were fabricated with weld wire heat number 90077. The intermediate to lower shell circumferential weld seam 101-171 was fabricated with Flux Type 124 Lot Number 1061. The intermediate and lower shell longitudinal weld seams were fabricated with Flux Type 0091 Lot 0842. The surveillance weld metal was fabricated with weld wire heat number 90077, Flux Type 124 Lot number 1061. Per Regulatory Guide 1.99, Revision 2, "weight-percent copper" and "weight-percent nickel" are the best-estimate values for the material, which will normally be the mean of the measured values for a plate or forging or for weld samples made with the weldwire heat number that matches the critical vessel weld. The surveillance weld metal was made with the same weld wire heat as all of the vessel beltline weld seams and is therefore representative of all of the beltline weld seams.

^(c) These values are used for considering flange requirements for the heatup/cooldown curves. Per the methodology given in WCAR-14040-NP-A (Ref. 4), the minimum boltup temperature is 60°F.

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TABLE 5.0-4 Fluence (10^{19} n/cm², E > 1.0 MeV) on the Pressure Vessel Clad/Base Metal Interface for Callaway Plant				
EFPY	0°	15°	30°	45°
12.40	0.445	0.649	0.756	0.768
16	0.565	0.822	0.956	0.964
24	0.832	1.21	1.40	1.40
32	1.10	1.59	1.85	1.83
54	1.83	2.64	3.07	3.02

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TABLE 5.0-5 Summary of Adjusted Reference Temperature (ART) Values at the ¼-T and ¾-T Locations for 20 EFY		
Material	20 EFY ART^(a)	
	¼-T ART (°F)	¾-T ART (°F)
Intermediate Shell Plate R2707-1	96.4	79.0
Intermediate Shell Plate R2707-2	77.4	56.6
Intermediate Shell Plate R2707-3	57.4	36.6
Lower Shell Plate R2708-1	124.0	105.4
Using Surveillance Capsule Data	90.9	83.2
Lower Shell Plate R2708-2	77.4	56.6
Lower Shell Plate R2708-3	100.4 ^(b)	84.2 ^(b)
Intermediate & Lower Shell Longitudinal Weld Seams 101- 124A & 101-142A (90° Azimuth)	-15.4	-30.8
Using Surveillance Capsule Data	0.8	-17.2
Intermediate & Lower Shell Longitudinal weld Seams 101- 124B&C and 101-142B&C (210° & 330° Azimuth)	-6.6	-23.2
Using Surveillance Capsule Data	7.3	-5.8
Intermediate to Lower Shell Circumferential Weld Seam 101- 171	-6.0	-22.6
Using Surveillance Capsule Data	7.8	-5.0

(a) $ART = \text{Initial } RT_{NDT} + \Delta RT_{NDT} + \text{Margin } (°F)$

(b) These ART values are used to generate the heatup and cooldown curves.

Note: When two or more credible surveillance data sets become available, the data sets may be used to determine ART values as described in Regulatory Guide 1.99, Revision 2, Position 2.1. If the ART values based on surveillance capsule data are larger than those calculated per Regulatory Guide 1.99, Revision 2, Position 1.1, the surveillance data must be used. If the surveillance capsule data gives lower values, either may be used.

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TABLE 5.0-6		
Calculation of Adjusted Reference Temperature Values at 20 EFY for the Limiting Callaway Plant Reactor Vessel Material (Lower Shell Plate R27083)		
Parameter	ART Value	
Location	¼-T	¾-T
Chemistry Factor, CF (°F)	51.0	51.0
Fluence, f (10^{19} n/cm ²) ^(a)	0.7174	0.2547
Fluence Factor, FF ^(b)	0.91	0.63
$\Delta RT_{NDT} = CF \times FF$, (°F)	46.4	32.1
Initial RT_{NDT} , I (°F)	20	20
Margin, M (°F) ^(c)	34	32.1
ART = I + (CF x FF) + M (°F) per Regulatory Guide 1.99, Rev. 2	100.4	84.2

(a) Fluence, f, is based upon f_{surf} (10^{19} n/cm², E > 1.0 MeV) = 1.204 at 20 EFY. The Callaway Plant reactor vessel wall thickness is 8.63 inches at the beltline region.

(b) Fluence Factor (FF) per Regulatory Guide 1.99, Revision 2, is defined as
 $FF = f^{(0.28 - 0.10 \log f)}$

(c) Margin is calculated as $M = 2(\sigma_I^2 + \sigma_{\Delta}^2)^{0.5}$. The standard deviation for the initial RT_{NDT} margin term σ_I , is 0°F since the initial RT_{NDT} is a measured value. The standard deviation for ΔRT_{NDT} term σ_{Δ} , is 17°F for the plate, except that σ_{Δ} need not exceed 0.5 times the mean value of ΔRT_{NDT} .

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TABLE 5.0-7							
RT_{PTS} Calculations for Callaway Plant Beltline Region Materials at 35 EFPY^(d)							
Material	Fluence (10¹⁹ n/cm², E > 1.0 MeV)	FF	CF (°F)	ΔRT_{PTS}^(c) (°F)	Margin (°F)	RT_{NDT(U)}^(a) (°F)	RT_{PTS}^(b) (°F)
Intermediate Shell Plate R2707-1	2.074	1.20	31.0	37.2	34.0	40	111
Intermediate Shell Plate R2707-2	2.074	1.20	37.0	44.4	34.0	10	88
Intermediate Shell Plate R2707-3	2.074	1.20	37.0	44.4	34.0	-10	68
Lower Shell Plate R2708-1	2.074	1.20	44.0	52.8	34.0	50	137
Using S/C Data	2.074	1.20	26.3	31.6	17.0	50	99
Lower Shell Plate R2708-2	2.074	1.20	37.0	44.4	34.0	10	88
Lower Shell Plate R2708-3	2.074	1.20	51.0	61.2	34.0	20	115
Inter. and Lower Shell Long. Weld Seams 101-124A & 101-142A (90° Azimuth)	1.167	1.04	29.7	30.9	30.9	-60	2
Using S/C Data	1.167	1.04	43.7	45.4	28.0	-60	13
Inter. and Lower Shell Long. Weld Seams 101-124B&C & 101-142B&C (210° & 330° Azimuth)	2.042	1.19	29.7	35.3	35.3	-60	11
Using S/C Data	2.042	1.19	43.7	52.0	28.0	-60	20
Intermediate to Lower Shell Circumferential Weld Seam 101-171	2.074	1.20	29.7	35.6	35.6	-60	11
Using S/C Data	2.074	1.20	43.7	52.4	28.0	-60	20

- (a) Initial RT_{NDT} values are measured values
 (b) RT_{PTS} = RT_{NDT(U)} + Margin + ΔRT_{PTS}
 (c) ΔRT_{PTS} = CF * FF
 (d) Projected no. of EFPY at the EOL.