

# Final Precursor Analysis

Accident Sequence Precursor Program -- Office of Nuclear Regulatory Research

Palo Verde Nuclear Generating Station, Units 1, 2, & 3	Loss of Offsite Power to All Three Units and Failure of a Unit 2 Emergency Diesel Generator.	
Event Date: 6/14/2004	LER: 528/04-006 IR: 50-528/04-012	CCDP <sup>1</sup> = $4 \times 10^{-5}$ (Unit 2) $9 \times 10^{-6}$ (Units 1 & 3)

## Event Summary

On June 14, 2004, at approximately 7:41 a.m. MST, a ground-fault occurred on Phase 'C' of a 230 kV transmission line in northwest Phoenix, Arizona, between the 'West Wing' and 'Liberty' substations located approximately 47 miles from the Palo Verde Nuclear Generating Station (PVNGS). A failure in the protective relaying resulted in the ground fault not isolating from the local grid for approximately 38 seconds. This uninterrupted fault cascaded into the protective tripping of a number of 230 kV and 500 kV transmission lines, a nearly concurrent trip of all three PVNGS units and the loss of six additional generation units nearby within approximately 30 seconds of fault initiation.

Offsite power was restored to the East Switchyard Bus at 0813, 32 minutes after power was lost. Licensed operators declared the grid stable at 0830, and at 0838 and 0844, power was restored to the Startup Transformers X01 and X03 respectively. All three units were shutdown and stabilized under hot shutdown conditions.

Important conditions and complications experienced during the event include:

- Unit 2 Emergency Diesel Generator (EDG) 'A' failed to load after receiving the start signal due to undervoltage on the Train 'A' 4.16 kV bus. The EDG could not maintain voltage with applied loads and was tripped by control room operators. The cause of the failure was a failed diode in Phase 'B' of the voltage regulator exciter circuit. The failed diode was not diagnosed until several hours after offsite power was restored to the first vital bus, and therefore would not have been recoverable prior to core damage during a postulated core uncover sequence, such as a station blackout event (SBO).
- Unit 2 Train 'A' engineered safeguards (ESF) busses were de-energized due to loss of the Train 'A' EDG. Offsite power was restored, supplying Train 'A' 4.16 kV bus at 0927.
- Units 1 and 3 had a failure of two 13.8 kV circuit breakers (one for each unit) to

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<sup>1</sup> For an initiating event assessment, the parameter of interest is the measure of the conditional core damage probability (CCDP). This value is obtained when calculating the probability of core damage for an initiating event with subsequent failure of one or more components following the initiating event.

close during the recovery of offsite power. If needed, alternate breakers were available to supply offsite power to another train of vital busses.

In addition to the equipment malfunctions, two operator performance weaknesses were displayed during the event:

- Unit 2 charging pump 'E' tripped on low suction pressure due to operator error. An operator failed to align the pump to the refueling water storage tank (RWST) and the pump became air bound, and therefore it could not have been recovered prior to postulated core damage (Ref. 1). The pump was recovered 9.5 hours later.
- Operators failed to drain the steam drain piping for the turbine-driven auxiliary feedwater (AFW) pumps until 11 hours after the event started.

Other complications that occurred during the event were:

- Unit 1 experienced an automatic letdown isolation failure.
- Unit 1 atmospheric dump valve (ADV) failed in the manual position.
- Unit 3 underwent an unexpected, automatic main steam isolation.

Further information about the event can be found in References 1 and 2.

## Analysis Results

### • Conditional Core Damage Probability (CCDP)

This event was modeled as an initiating event loss of offsite power (LOOP) with complications resulting from component failures and operator actions. The CCDP for this event is  $4 \times 10^{-5}$  (mean value) for Unit 2, and  $9 \times 10^{-6}$  for Units 1 and 3. The acceptance threshold for the Accident Sequence Precursor Program is a  $\text{CCDP} \geq 1 \times 10^{-6}$ . Therefore, these events are precursors.

	CCDP		
	5%	Mean	95%
Unit 1	$4 \times 10^{-7}$	$9 \times 10^{-6}$	$3 \times 10^{-5}$
Unit 2	$3 \times 10^{-6}$	$4 \times 10^{-5}$	$1 \times 10^{-4}$
Unit 3	$4 \times 10^{-7}$	$9 \times 10^{-6}$	$3 \times 10^{-5}$

### • Dominant Sequences

**Unit 2.** The dominant core damage sequences for the Unit 2 analysis are Loss of Offsite Power (LOOP), Station Blackout (SBO) Sequence 15-30 (53.8% of the total CCDP) and

LOOP Sequence 14 (22.5% of the total CCDP). The LOOP and SBO event trees with the dominant sequences highlighted are shown in Figure 1 and Figure 2.

The events and important component failures in LOOP/SBO Sequence 15-30 are:

- LOOP occurs,
- Reactor trip succeeds,
- Emergency power fails,
- Auxiliary feedwater fails,
- Operators fail to recover offsite power in 1 hour, and
- Operators fail to recover an EDG in 1 hour.

The events and important component failures in LOOP Sequence 14 are:

- LOOP occurs,
- Reactor trip succeeds,
- Emergency power succeeds, and
- Auxiliary feedwater fails.<sup>2</sup>

**Units 1 and 3.** The dominant core damage sequence for the Units 1 and 3 analysis is LOOP Sequence 14 (66.3% of the total CCDP). The LOOP event tree with the dominant sequence highlighted is shown in Figure 2.

## ● Results Tables

- The conditional probabilities for the dominant sequences are shown in Tables 1a and 1b.
- The event tree sequence logic for the dominant sequences are presented in Table 2a.
- Table 2b defines the nomenclature used in Table 2a.
- The most important cut sets for the dominant sequences are listed in Table 3a and 3b.
- Definitions and probabilities for modified or dominant basic events are provided in Table 4.

## Modeling Assumptions

### ● Analysis Type

This event was modeled as a loss of offsite power initiating event (IE-LOOP) using the Palo Verde 1, 2, & 3 Revision 3.11 Standardized Plant Analysis Risk (SPAR) model (Ref. 3). The subsequent reactor trip experienced by all three units is represented by this initiating event. The probability of IE-LOOP was set to 1.0. The probabilities of the other initiating events were set to 0.0 in the GEM code. Other changes to model the event are described below.

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<sup>2</sup> Palo Verde Units do not have the capability to feed and bleed. See Unique Design Features for more information.

- **Unique Design Features**

***Lack of feed and bleed capability.*** Palo Verde Units 1, 2, and 3 do not have reactor coolant system power operated relief valves (PORVs). Thus Palo Verde does not have the capability to feed and bleed, because the head provided by the high pressure safety injection pumps is insufficient to lift the safety relief valves.

***Two SBO gas turbine generator sets.*** A non-safety alternate AC power source consisting of two gas turbine generators (GTGs) is available to provide power to cope with a SBO event. Each GTG can supply emergency power to any single unit; however, Units 2 and 3 cannot be supplied simultaneously. Therefore both GTGs can supply power to Units 1 and 2 or to Units 1 and 3 simultaneously.

- **Modeling Assumptions Summary**

***Key modeling assumptions.*** The key modeling assumptions are listed below and discussed in detail in the following sections. These assumptions are important contributors to the overall risk.

- **Offsite power to first vital bus recoverable within 1 hour.** Offsite power was restored to the Unit 2 Train 'A' vital bus 1 hour and 46 minutes after the LOOP occurred. However, offsite power was available 32 minutes after the event occurred. Therefore, in the event of a postulated core uncover sequence (i.e., a SBO condition), operators had approximately 30 minutes to close the three breakers required to restore offsite power to a vital bus. See Attachment B for further details.
- **Unit 2 EDG 'A' failed to start and was not recoverable within the time frame to prevent core uncover.** See Event Description for further details.

***Other assumptions.*** Other assumptions that have a negligible impact on the results due to relatively low importance include the following:

- **Unit 2 charging pump 'E' tripped on low suction pressure due to operator error.** See Event Description for further details.

- **Fault Tree Modifications**

***4160V AC power bus PBA and PBB fails (ACP-PBA-AC and ACP-PBB-AC).*** The gates ACP-PBA-AC-3 and ACP-PBB-AC-3 in fault trees ACP-PBA-AC and ACP-PBB-AC provides the branches for supplying the vital AC power via the GTGs. The gate was replaced with the basic event OEP-XHE-XL-NR01H (operator fails to recover AC power in 1 hour), which eliminates the ability of the GTGs to supply a single unit vital bus. This change was made because offsite power was available approximately the same time as the GTGs were available. When offsite power is available, it is the preferred power source. Therefore, operators will attempt to supply the vital busses with offsite power first. The modification was made to prevent crediting AC power recovery twice for certain SBO cutsets where the non-recovery probability of offsite power is multiplied by the probability of operators failing to align the GTGs to the safety buses. The modified fault trees are shown in Figure 3 and

Figure 4.

- **Basic Event Probability Changes**

Table 4 provides all the basic events that were modified to reflect the best estimate of the conditions during the event. The basis for these changes are provided below.

**ALL UNITS**

***Operators fail to recover offsite power in 2 hours (OEP-XHE-XL-NR02H).*** Basic event probability was changed to  $4 \times 10^{-3}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 3 hours (OEP-XHE-XL-NR03H).*** Basic event probability was changed to  $4 \times 10^{-3}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 4 hours (OEP-XHE-XL-NR04H).*** Basic event probability was changed to  $4 \times 10^{-4}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 6 hours (OEP-XHE-XL-NR06H).*** Basic event probability was changed to  $4 \times 10^{-4}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 8 hours (OEP-XHE-XL-NR08H).*** Basic event probability was changed to  $4 \times 10^{-4}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 10 hours (OEP-XHE-XL-NR10).*** Basic event probability was changed to  $4 \times 10^{-4}$ . See Attachment B for further details.

***Operators fail to recover offsite power in 24 hours (OEP-XHE-XL-NR24H).*** Basic event probability was changed to  $4 \times 10^{-4}$ . See Attachment B for further details.

***Diesel generator fails to run in the long term (ZT-DGN-FR-L).*** The mission time was changed to 0.75 hours to reflect the actual time when offsite power was recovered to the first vital bus and an additional 30 minutes.<sup>3</sup>

***Turbine-driven pump fails to run in the long term (ZT-TDP-FR-L).*** The mission time was changed to 1.25 hours to reflect the 95 percentile that offsite power was actually recovered to the first vital bus (1.75 hours) and an additional 30 minutes to align alternate sources of feeding the steam generators (SGs).<sup>4</sup>

**UNIT 2**

***Charging pump 'E' fails to start (CVC-MDP-FS-CHE).*** The event was set to TRUE based on actual plant conditions.

***Diesel generator 'A' fails to start (EPS-DGN-FS-A).*** The event was set to TRUE based

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<sup>3</sup> The total EDG mission time is 1.75 hours. The first hour of mission time is accounted for with the basic event ZT-DGN-FR-E.

<sup>4</sup> The total AFW TDP mission time is 2.25 hours. The first hour of mission time is accounted for with the basic event ZT-TDP-FR-E.

on actual plant conditions.

***Operators fail to recover offsite power in 1 hour (OEP-XHE-XL-NR01H).*** Basic event probability was changed to  $4 \times 10^{-2}$ . See Attachment B for further details.

### **UNITS 1 & 3**

***Operators fail to recover offsite power in 1 hour (OEP-XHE-XL-NR01H).*** Basic event probability was changed to 0.1. See Attachment B for further details.

#### ● **Other Items of Interest**

During the event there were a number of other equipment and/or operator issues noted in Reference 1. These issues, which did not result in changes in the SPAR model, are listed below.

***Units 1 and 3 failure of two 13.8 kV circuit breakers failed to close during the recovery of offsite power.*** The two breakers (1ENANS06K and 3ENANS05D) were manually cycled closed 51 minutes after the event initiated. This analysis does not credit the recovery of offsite power using a recovered breaker in the short term (within 1 hour) SBO sequence.<sup>5</sup> Alternate breakers (1ENANS06K and 3ENANS05B) were available to supply offsite power to the other vital busses in the short term. Both the recovered and alternate breakers were available to supply the vital busses for the longer term blackout sequences.

The two breaker failures appear to be from common cause. The switchyard is not modeled in the SPAR model, and therefore the CCDP contribution of the common cause failure is not present in the analysis results. However, the probability of the other breakers (i.e., breakers of the same type that could supply the vital busses) failing from the common cause is more than one order of magnitude less than the failure probability of operators to recover offsite power with no breaker failures. Thus, the total CCDP would not change if the common cause failure contribution was included in the analysis.

***Unit 1 ADV valve failed in the manual position.*** The operators were able to operate the valve by increasing the demand to failed valve; however the valve would not maintain the desired position. The inspection team determined that operators had been sufficiently trained to use the other three ADVs for decay heat removal (Ref. 1), and therefore this failure was not modeled.

***Unit 1 letdown failed to isolate.*** The ion exchanger bypass valves opened to prevent overheating the resin and to remove high temperature water from the ion exchanger. No damage occurred due to the malfunction. The failure to isolate did not affect any mitigating system or reactor coolant pump seal cooling.

***Unit 3 experienced a unexpected main steam line isolation.*** An automatic isolation occurred due to fault causing the steam bypass control system to be re-energized in automatic. During a LOOP event, the main condenser is unavailable as a heat sink (loss

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<sup>5</sup> The time to close the remaining breakers, energize the vital busses, and align and start high pressure injection and AFW within 1 hour is highly unlikely.

of circulating water), and decay heat removal is provided by the steam generator (SG) ADVs. Emergency operating procedures (EOPs) direct operators to manually initiate a main steam isolation signal. Therefore, regardless of the fault, the main steam isolation valves will be closed during a LOOP event.

***Operator delay to drain the steam drain piping of the turbine-driven AFW pumps.*** A potential turbine overspeed trip during startup is possible if sufficient water accumulates in the steam piping supplying the turbine. Operators delayed draining the piping for 11 hours after the reactor tripped. This was not modeled in the analysis because of two reasons. First, the turbine-driven pump ran without problems during the event. Second, the turbine-driven AFW pump mission time during the event was approximately 2.25 hours and procedure requires operators to drain the AFW steam piping every 2 hours during a main steam isolation. Therefore it is believed that there was insufficient time for enough water to accumulate (prior to expiration of the mission time) that could potentially cause an overspeed trip of the pump.

## References

1. NRC Augmented Inspection Team (AIT) Report 50-528/04-012-00, dated July 16, 2004.
2. LER 528/04-006, "Loss of Offsite Power—Three Unit Trip," dated August 13, 2004.
3. Idaho National Engineering and Environmental Laboratory, "Standardized Plant Analysis Risk Model for Palo Verde 1, 2, & 3," Revision 3.11, December 31, 2004.
4. Idaho National Engineering and Environmental Laboratory, "The SPAR-H Human Reliability Analysis Method INEEL/EXT-02-01307", May 2004.

**Table 1a. Conditional core damage probabilities of dominating sequences (Unit 2).**

Event tree name	Sequence no.	CCDP <sup>1</sup>	Contribution
SBO	15-30	2.1E-005	53.8
LOOP	14	8.8E-006	22.5
<b>Total (all sequences)<sup>2</sup></b>		<b>3.9E-005</b>	<b>100</b>

1. Values are point estimates. (File name: GEM (528-04-006) Unit 2 LOOP.wpd)

2. Total CCDP includes all sequences (including those not shown in this table).

**Table 1b. Conditional core damage probabilities of dominating sequences (Units 1 & 3).**

Event tree name	Sequence no.	CCDP <sup>1</sup>	Contribution
LOOP	14	6.1E-006	66.3
<b>Total (all sequences)<sup>2</sup></b>		<b>9.2E-006</b>	<b>100</b>

1. Values are point estimates. (File name: GEM (528-04-006) Units 1&3 LOOP.wpd)

2. Total CCDP includes all sequences (including those not shown in this table).

**Table 2a. Event tree sequence logic for dominating sequences.**

Event tree name	Sequence no.	Logic ("I" denotes success; see Table 2b for top event names)
SBO	15-30	/RPS EPS AFW-B OPR-01H DGR-01H
LOOP	14	/RPS /EPS AFW-L

**Table 2b. Definitions of top events listed in Table 2a.**

Top Event	Definition
AFW-B	Auxiliary feedwater fails during SBO
AFW-L	Auxiliary feedwater fails during LOOP
DGR-01H	Operator fails to recover EDG in 1 hour
EPS	Emergency power system fails
OPR-01H	Operator fails to recover offsite power in 1 hour
RPS	Reactor fails to trip



**Table 3a. Conditional cut sets for the dominant sequences (Unit 2).**

CCDP	Percent Contribution	Minimum Cut Sets (of basic events)		
Event Tree: SBO, Sequence 15-30				
4.2E-006	20.5	EPS-XHE-XL-NR01H AFW-TDP-FS-A	OEP-XHE-XL-NR01H	EPS-DGN-CF-STRT
3.5E-006	17.1	EPS-XHE-XL-NR01H AFW-TDP-TM-A	OEP-XHE-XL-NR01H	EPS-DGN-CF-STRT
2.2E-006	10.4	EPS-XHE-XL-NR01H AFW-TDP-FR-A	OEP-XHE-XL-NR01H	EPS-DGN-CF-STRT
1.8E-006	8.8	EPS-XHE-XL-NR01H AFW-TDP-FS-A	OEP-XHE-XL-NR01H	EPS-DGN-TM-DGB
2.1E-005	100	Total (all cutsets) <sup>1</sup>		
CCDP	Percent Contribution	Minimum Cut Sets (of basic events)		
Event Tree: LOOP, Sequence 14				
1.2E-006	13.7	OEP-XHE-XL-NR01H AFW-MDP-TM-B	AFW-TDP-FS-A	
8.0E-007	9.1	OEP-XHE-XL-NR01H	OEP-XHE-XL-NR03H	AFW-MDP-TM-B
6.6E-007	7.5	AFW-PMP-CF-RUN		
6.1E-007	7.0	OEP-XHE-XL-NR01H	AFW-MDP-TM-B	AFW-TDP-FR-A
6.0E-007	6.8	AFW-XHE-XM-TRAINN	AFW-MDP-TM-B	AFW-TDP-FS-A
8.8E-006	100	Total (all cutsets) <sup>1</sup>		

1. Total CCDP includes all cutsets (including those not shown in this table).

**Table 3B. Conditional cut sets for the dominant sequences (Units 1 & 3).**

CCDP	Percent Contribution	Minimum Cut Sets (of basic events)		
Event Tree: LOOP, Sequence 14				
6.6E-007	10.9	AFW-PMP-CF-RUN		
6.0E-007	9.9	AFW-XHE-XM-TRAINN	AFW-MDP-TM-B	AFW-TDP-FS-A
4.8E-007	7.8	AFW-MDP-CF-START	AFW-TDP-FS-A	
4.0E-007	6.5	AFW-MDP-CF-START	AFW-TDP-TM-A	
3.1E-007	5.0	AFW-XHE-XM-TRAINN	AFW-MDP-TM-B	AFW-TDP-FR-A
6.1E-006	100	Total (all cutsets) <sup>1</sup>		

1. Total CCDP includes all cutsets (including those not shown in this table).

Table 4. Definitions and probabilities for modified and dominant basic events.

Event Name	Description	Probability/ Frequency (per hour)	Modified
AFW-MDP-CF-START	CCF OF EFW MDPS B & N TO START	7.9E-005	No
AFW-MDP-TM-B	AFW MDP B UNAVAILABLE DUE TO T&M	5.0E-003	No
AFW-PMP-CF-RUN	COMMON CAUSE FAILURE OF ALL AFW PUMPS	6.6E-007	No
AFW-TDP-FR-A	AFW TDP A FAILS TO RUN	3.1E-003	No
AFW-TDP-FS-A	AFW TDP A FAILS TO START	6.0E-003	No
AFW-TDP-TM-A	AFW TDP A UNAVAILABLE DUE TO T&M	5.0E-003	No
AFW-XHE-XM-TRAINN	OPERATOR FAILS TO ALIGN AND START AFW TRAIN	2.0E-002	No
CVC-MDP-FR-CHE	CHARGING PUMP CHE FAILS TO RUN	IGNORE	Yes <sup>1</sup>
CVC-MDP-FS-CHE	CHARGING PUMP CHE FAILS TO START	TRUE	Yes <sup>2</sup>
EPS-DGN-CF-STRT	COMMON CAUSE FAILURE OF EDGS TO START	8.4E-005	No
EPS-DGN-FR-DGA	DIESEL GENERATOR A FAILS TO RUN	IGNORE	Yes <sup>1</sup>
EPS-DGN-FS-DGA	DIESEL GENERATOR A FAILS TO START	TRUE	Yes <sup>2</sup>
EPS-DGN-TM-DGB	DG B UNAVAILABLE DUE TO T&M	9.0E-003	No
EPS-XHE-XL-NR01H	OPERATOR FAILS TO RECOVER EDG IN 1 HR	8.4E-001	No
IE-LOOP	LOOP INITIATING EVENT OCCURS	1.0	Yes <sup>3</sup>
OEP-XHE-XL-NR01H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	1.0E-001	Yes <sup>4</sup>
OEP-XHE-XL-NR02H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-003	Yes <sup>5</sup>
OEP-XHE-XL-NR03H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-003	Yes <sup>5</sup>
OEP-XHE-XL-NR04H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-004	Yes <sup>5</sup>
OEP-XHE-XL-NR06H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-004	Yes <sup>5</sup>
OEP-XHE-XL-NR08H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-004	Yes <sup>5</sup>
OEP-XHE-XL-NR10H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-004	Yes <sup>5</sup>
OEP-XHE-XL-NR24H	OPERATOR FAILS TO RECOVER OFFSITE POWER IN 1 HR	4.0E-004	Yes <sup>5</sup>
ZT-DGN-FR-L	TURBINE DRIVEN PUMP FAILS TO RUN IN THE LONG TERM	6.0E-004	Yes <sup>6</sup>
ZT-TDP-FR-L	EDG FAILS TO RUN IN THE LONG TERM	6.3E-005	Yes <sup>6</sup>

1. Unit 2 only– changed to correctly model the common cause failure probability to run.

2. Unit 2 only– changed to reflect actual plant conditions during the event.

3. All other initiating event frequencies set to zero.

4. Non-recovery probabilities are different between the Unit 2 analysis and the Units 1 & 3 analysis (see Attachment B for further details).

5. Non-recovery probabilities the same for all three units (see Attachment B for further details).

6. Changed mission times (see Basic Event Probability Changes for further details).

## Attachment A Sequences of Key Events

### Unit 1 Sequence of Key Events

6/14/04

0741	Startup Transformer# 2 Breaker 945 Open Excessive Main Generator and Field Currents Noted Engineered Safeguards Features Bus Undervoltage Loss of Offsite Power Load Shed Train "A" and "B" Emergency Diesel Generator Train "A" and "B" Start Signal Low Departure from Nucleate Boiling Ratio Reactor Trip Master Turbine Trip Main Turbine Mechanical Over Speed Trip Emergency Diesel Generator "A" Operating (10 Second Start Time) Emergency Diesel Generator "B" Operating (13 Second Start Time*)
0751	Manual Main Steam Isolation System Actuation
0758	Declared Notice of Unusual Event (loss of essential power for greater than 15 minutes)
0810	Both Gas Turbine Generator Sets Started, #1 GTG is supplying power to NAN S07
0813	Closed 500 k 552-942. The East bus is powered from Hass #1
0838	Restored power to Startup Transformer X01
0844	Restored power to Startup Transformer X03
0855	Fire reported in 120 ft Aux building. Fire brigade confirmed that no fire existed but paint was heated causing fumes. Later it was confirmed that fumes were caused by the elevated temperature of the letdown heat exchanger when it failed to isolate.
0900	HI Temp Abnormal Operation Procedure entered for Letdown heat exchanger outlet temperature off scale high.
1002	Reset Generator Protective Trips (volts/hertz; Backup under-frequency) Palo Verde Switchyard Ring Bus restored
1159	Paralleled DG B with bus and cooled down engine restoring the in house buses
1207	Emergency Coordinator terminated NUE for all three units
1248	Paralleled DG A with bus and cooled down

2209            Noted grid voltage greater than 535.5 volts Shift Manager Coordinated with ECC

**6/15/04**

0005            Restored CVCS letdown per Std Attachment 12 started Chg Pump 'A'

0155            Established RCP seal injection and controlled bleed off

0241            Started 2A RCP, had to secure due to low running amps other two units had RCP's running (what were the amps at the time) exiting of EOP delayed due to switchyard conditions

0305            Exited Loss of Letdown AOP after restoration of letdown per Standard App. 12 of EOP's

0345            Palo Verde Switchyard E-W voltage at approx. 530.7 kV

0818            Started RCP's 2A and 1A

0920            Started RCP's 2B and 1B

0930            Exited EOP 40EP- 9E007 Loss of Offsite Power/Loss of Forced Circulation

**Unit 2 Sequence of Key Events**

**6/14/04**

0740            4.16 kV Switchgear 3 Bus Trouble Alarm Generator Negative Sequence Alarm  
4.16 kV Switchgear 4 Bus Trouble Alarm

0741            Main Transformer B Status Trouble Alarm  
Main Transformer A Status Trouble Alarm  
ESF Bus Undervoltage Channel A-2  
ESF Bus Undervoltage Channel B-2  
LOP/Load Shed B  
ESF Bus Undervoltage Channel B-3  
DG Start Signal B  
LOP/Load Shed A  
ESF Bus Undervoltage Channel A-4  
DG Start Signal A  
LO DNBR Channels A, B, C, & D Trip  
RPS Channels A, B, C, & D Trip  
Main Generator 500 kV Breaker 935 Open  
Mechanical Overspeed Trip of Main Turbine

0751            Manually initiated Main Steam Isolation Signal

0755            Declared an Alert for Loss of All Offsite Power to Essential Busses for Greater than 15 minutes

0901	Energized 13.8 kV Busses 2E-NAN-S03 and 2E-NAN-S05
0927	Energized 4.16 kV Bus 2E-PBA-S03
0951	Exited Alert
1001	Energized 13.8 kV Bus 2E-NAN-S01
1024	Energized 13.8 kV Bus 2E-NAN-S02
1132	Started Charging Pump A
1618	Engineering and Maintenance review concluded that Charging Pump E was available for service after fill and vent
1714	Started Charging Pump E
1716	Started RCP 1A
1722	Started RCP 2A
1806	Stopped RCPs 1A and 2A on low motor amperage. ECC contacted to adjust grid voltage as-low-as-possible
2040	Started RCPs 1A and 2A
2051	Stopped RCPs 1A and 2A on low running amperage
<b>6/15/04</b>	
0400	Started RCPs 1A and 2A
0610	Exited Emergency Operating Procedures

### **Unit 3 Sequence of Key Events**

**6/14/04**

0740	Generator Under Voltage Negative Sequence Trip Master Turbine Trip 3ENANS01 Bus Under Voltage Reactor Trip Circuit Breakers Open
0741	Exciter Voltage Regulator Mode Change Unit 3 Main Generator 500 kV Breaker 985 Opens Engineered Safeguards Features Bus Undervoltage Loss of Offsite Power Load Shed A and B Emergency Diesel Generator A and B Start Signal Main Turbine Overspeed Mechanical Trip Turbine Bypass Valves Quick Open

0742	Low Steam Generator Pressure Alarm Unit 3 Main Generator 500 kV Breaker 988 Opens
0743	Automatic Main Steam Isolation on Low Steam Generator Pressure
2341	Started Reactor Coolant Pump 1A
2345	Started Reactor Coolant Pump 2A
<b>6/15/04</b>	
0040	Exited Emergency Operating Procedures
1637	Started Reactor Coolant Pump 1B
<b>6/16/04</b>	
0207	Started Reactor Coolant Pump 2B

## Attachment B

### Offsite Power Recovery Modeling

#### Background and Modeling Details of Offsite Power Recovery<sup>6</sup>

The time required to restore offsite power to plant emergency equipment is a significant factor in modeling the conditional core damage probability (CCDP) given a loss of offsite power (LOOP). Standardized Plant Analysis Risk (SPAR) LOOP/Station Blackout (SBO) models include various sequence-specific AC power recovery factors that are based on the time available to recover power to prevent core damage. For a sequence involving failure of all of the cooling sources, approximately 1 hour would be available to recover power to help avoid core damage. On the other hand, sequences involving successful early inventory control and decay heat removal, but failure of long-term decay heat removal, would accommodate several hours to recover AC power prior to core damage.

In this analysis, offsite power recovery probabilities are based on (1) known information about when power was restored to the switchyard and (2) estimated probabilities of failing to realign power to emergency buses for times after offsite power was restored to the switchyard. Power restoration times were reported by the licensee to the Augmented Inspection Team (AIT). The east switchyard bus was energized from offsite power (Hass-1) in 32 minutes. After the power was restored to the switchyard bus, operators would need to close three Unit 2 breakers (2ENANS05D, 2ENANS03A, and 2EPBAS03L) to supply offsite power to the Unit 2 Train 'A' vital bus. In the event of a blackout condition, operators would have sufficient time (approximately 30 minutes) to shut the three breakers to restore AC power to a vital bus.<sup>7</sup>

Failure to recover offsite power to plant safety-related loads (if needed because emergency diesel generators (EDGs) fail to supply the loads), given recovery of power to the switchyard, could result from (1) operators failing to restore proper breaker line-ups, (2) breakers failing to close on demand, or (3) a combination of operator and breaker failures. The dominant contributor to failure to recover offsite power to plant safety-related loads in this situation is operators failing to restore proper breaker line-ups. The SPAR-H Human Reliability Analysis Method (Ref. 4) was used to estimate non-recovery probabilities as a function of time following restoration of offsite power to the switchyard.

#### Diagnosis and Dependency

The SPAR Human Reliability Analysis Method considers the following three factors:

- Probability of failure to diagnose the need for action,
- Probability of failure to successfully perform the desired action, and
- Dependency on other operator actions involved in the specific sequence of interest.

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<sup>6</sup> This section provides background information and details involving recovery of offsite power for this event. In an ASP analysis, offsite power recovery constitutes the recovery of power to the unit vital busses once power has been restored to the switchyard. ASP analyses do not deal with offsite recovery actions outside the switchyard.

<sup>7</sup> The grid was declared stable per Technical Specifications (TS) 49 minutes after the LOOP occurred. During a postulated SBO event, if operators waited until the grid was stable (per TS) they would have approximately 11 minutes to restore power to a vital bus. However, operators would shut two of three breakers as soon as the switchyard was re-energized. Therefore, operators would have sufficient time (approx. 11 minutes) to shut one breaker.

This analysis does not consider the probability of failure to diagnose the need to recover AC power because a loss of offsite power diagnosis is obvious. Operators have an overwhelming amount of plant signals which tell them that a LOOP has occurred. Dependency between operator power recovery tasks and any other operator tasks is also not considered. Dependency is considered when multiple operator actions are present in the same cutset. This analysis does not have any cutsets containing multiple human error basic events. Thus, each estimated AC power non-recovery probability is based solely on the probability of failure to successfully perform the desired action.

### **Performance Shaping Factors**

The probability of failure to perform an action is the product of a nominal failure probability ( $1 \times 10^{-3}$ ) and the following eight performance shaping factors (PSFs):

- Available time
- Stress
- Complexity
- Experience/training
- Procedures
- Ergonomics
- Fitness for duty
- Work processes

### **Time**

For each AC power non-recovery probability, the PSF for Available Time is assigned a value of 10 if the time available to perform the action is approximately equal to the time required to perform the action (i.e., 1 hour), 1.0 if the time available is between 2 and 4 times the time required, and 0.1 if the time available is greater than 5 times the time required. This analysis credits 1 hour as the minimum time that offsite power can be recovered to the first vital bus.

### **Stress**

The PSF for Stress is assigned a value of 2 (corresponding to High Stress) for all AC power non-recovery probabilities. Factors considered in assigning this PSF level "higher than nominal level" include sudden onset of the LOOP initiating event, actual and/or postulated compounding equipment failures, and resulting core uncover and eminent core damage. Extreme Stress is not appropriate because offsite power to the East bus in the switchyard was actually recovered in about 30 minutes.<sup>8</sup> The operators knew early that a success path to re-energize a vital bus was viable within the time frame associated with the postulated short-term core uncover sequence (1 hour given failure of auxiliary feedwater). Therefore, this event did not present "a level of disruptive stress in which the performance of most people will deteriorate drastically."

### **Complexity**

The PSF for Complexity is assigned a value of 2 (corresponding to Moderately Complex) for all non-recovery probabilities except OEP-XHE-XL-NR01H for Units 1 and 3. Factors considered in assigning this PSF level "involved concurrent actions" such as communications and coordination of three organizations outside the control room: the other two control rooms and utility switchyard

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<sup>8</sup> In addition, the gas turbine generators (GTGs) could have been aligned to a single unit vital bus within 30 minutes. The GTGs were running 29 minutes after the LOOP occurred.



operators. "Highly Complex" is not appropriate because the task of closing three breakers is a routine task performed periodically during plant normal operations.

The PSF for Complexity is assigned a value of 5 (corresponding to Highly Complex) for probability OEP-XHE-XL-NR01H for Units 1 and 3. Factors considered in assigning this PSF level involved additional variables and actions due to the failure of two 13.8 kV breakers to close; one in each unit. The actual recovery of the breaker took over 1 hour to complete (Ref. 1). Therefore, recovery of the breaker is not an option for short-term offsite power recovery. The operators would have to determine that recovery of the failed breaker is not viable within the short time frame and an alternate success path to energize the other vital bus is required for success.

#### **All Other PSFs**

For all of the AC power non-recovery probabilities, the PSFs for experience/training, procedures, ergonomics, fitness for duty, and work processes are set to be nominal (i.e., are assigned values of 1.0). Details of the event, plant response, and crew performance did not warrant a change from nominal for these PSFs.

**Table C.1. AC power non-recovery probabilities.**

Non-recovery Factor	Units	Nominal Value	PSF			Non-recovery Probability
			Time Available	Stress	Complexity	
OEP-XHE-XL-NR01H	1 & 3	$1 \times 10^{-3}$	10	2	5	0.1
OEP-XHE-XL-NR01H	2	$1 \times 10^{-3}$	10	2	2	$4 \times 10^{-2}$
OEP-XHE-XL-NR02H	All	$1 \times 10^{-3}$	1	2	2	$4 \times 10^{-3}$
OEP-XHE-XL-NR03H	All	$1 \times 10^{-3}$	1	2	2	$4 \times 10^{-3}$
OEP-XHE-XL-NR04H	All	$1 \times 10^{-3}$	0.1	2	2	$4 \times 10^{-4}$
OEP-XHE-XL-NR06H	All	$1 \times 10^{-3}$	0.1	2	2	$4 \times 10^{-4}$
OEP-XHE-XL-NR08H	All	$1 \times 10^{-3}$	0.1	2	2	$4 \times 10^{-4}$
OEP-XHE-XL-NR10H	All	$1 \times 10^{-3}$	0.1	2	2	$4 \times 10^{-4}$
OEP-XHE-XL-NR24H	All	$1 \times 10^{-3}$	0.1	2	2	$4 \times 10^{-4}$

1. From the SPAR model.

## Attachment C

### Event Tree and Fault Tree Figures

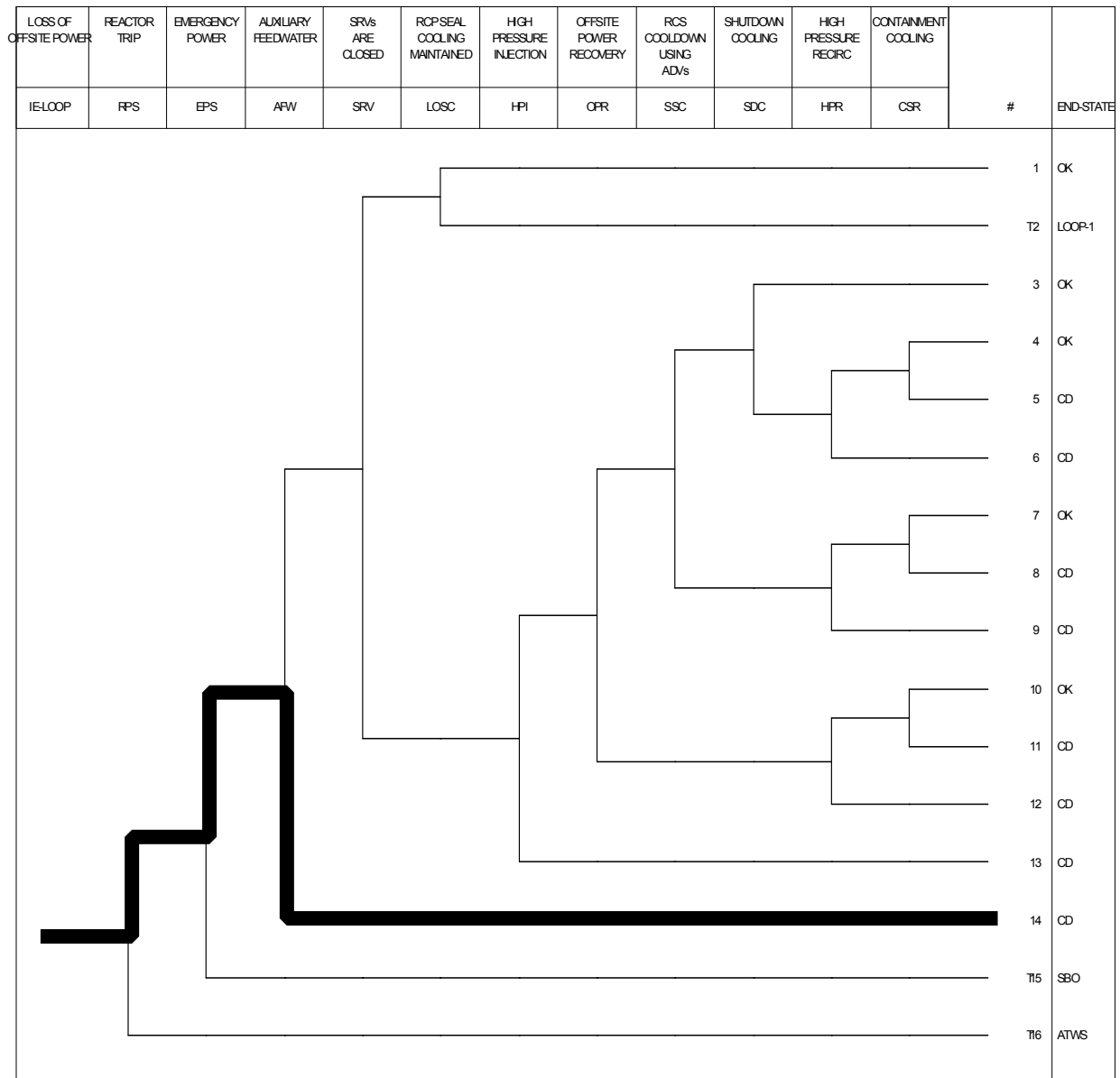


Figure 1: Palo Verde LOOP event tree (with dominant sequence highlighted).

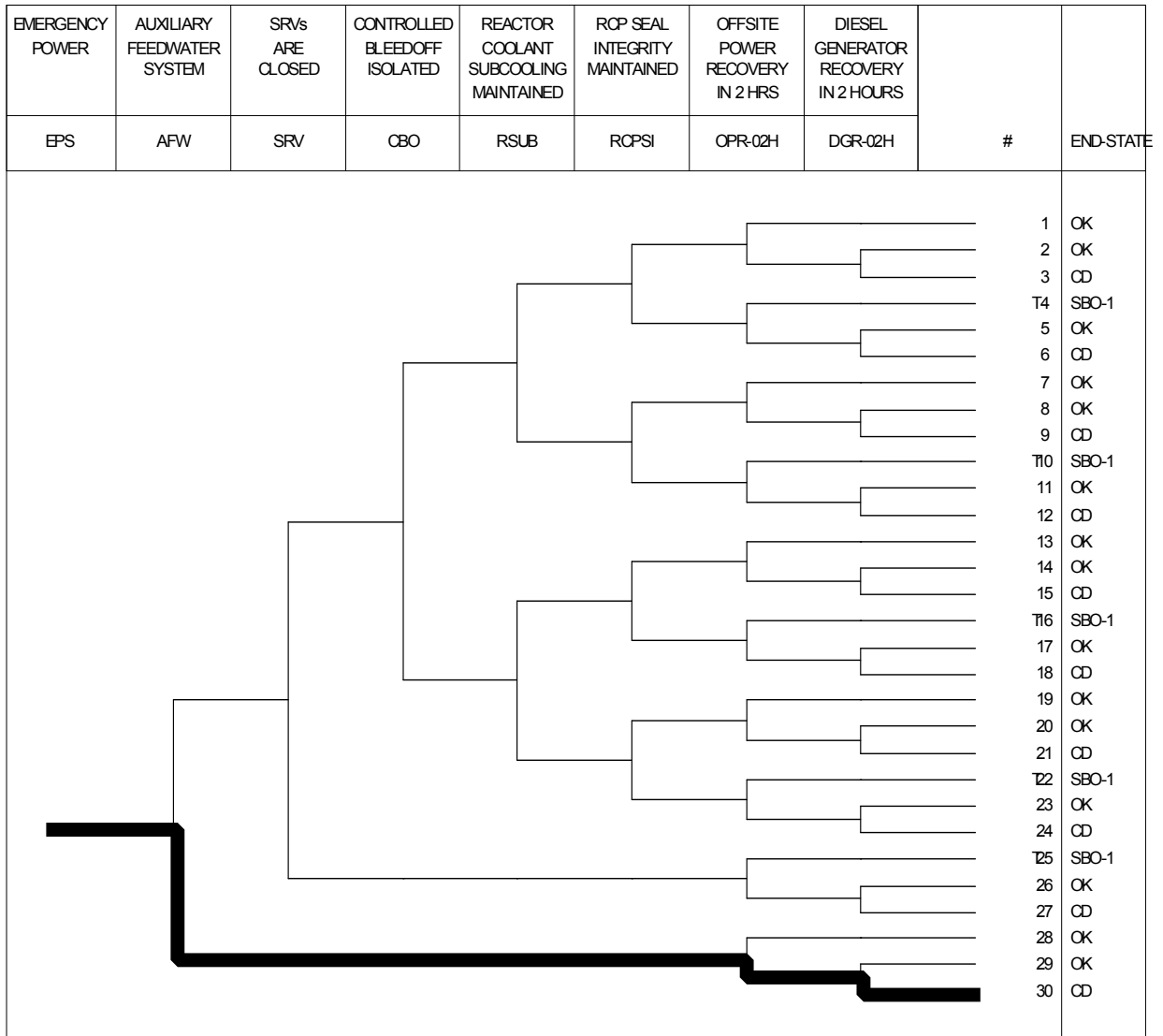


Figure 2: Palo Verde SBO event tree (with dominant sequence highlighted).

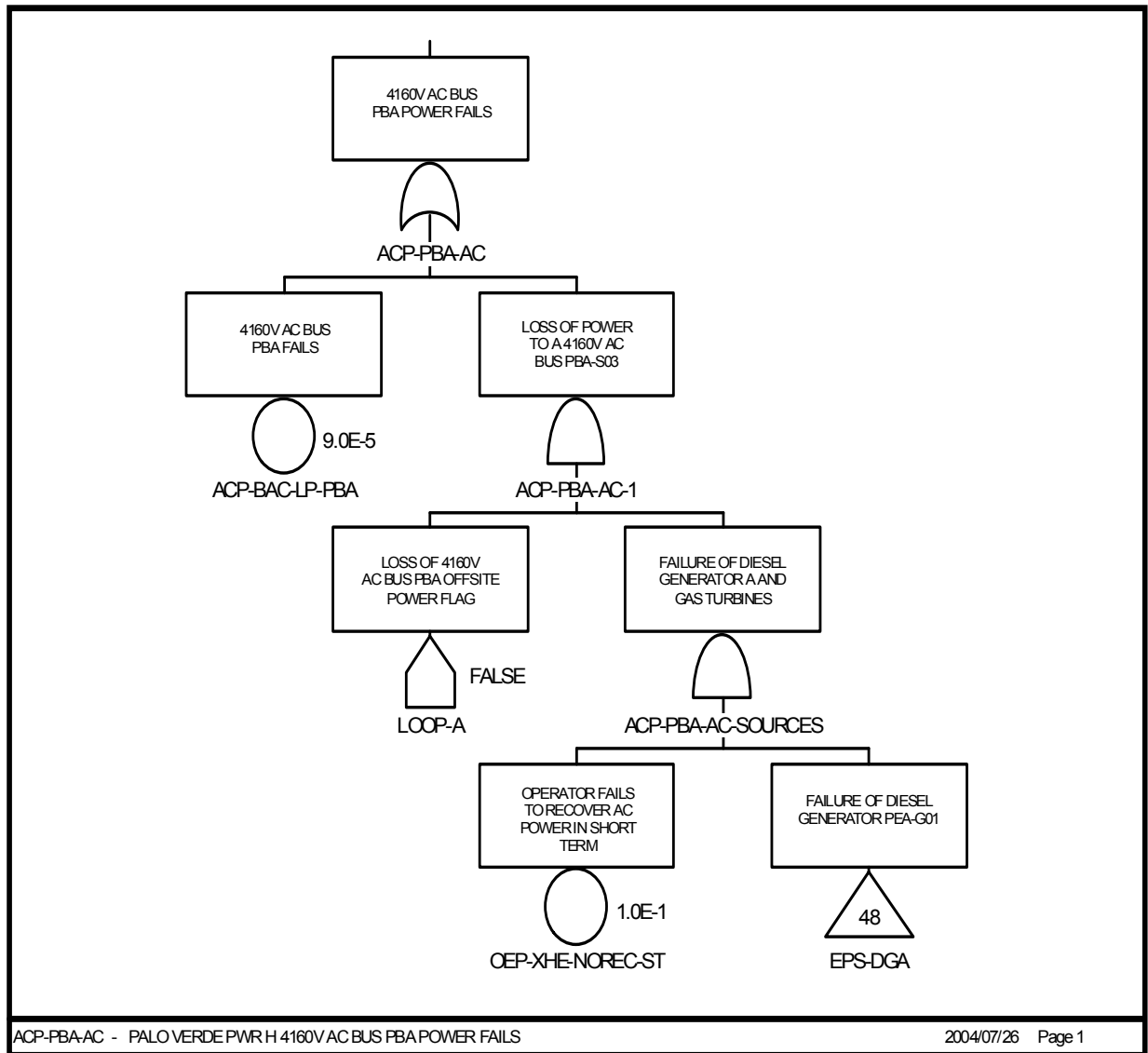


Figure 3: Modified fault tree ACP-PBA-AC.

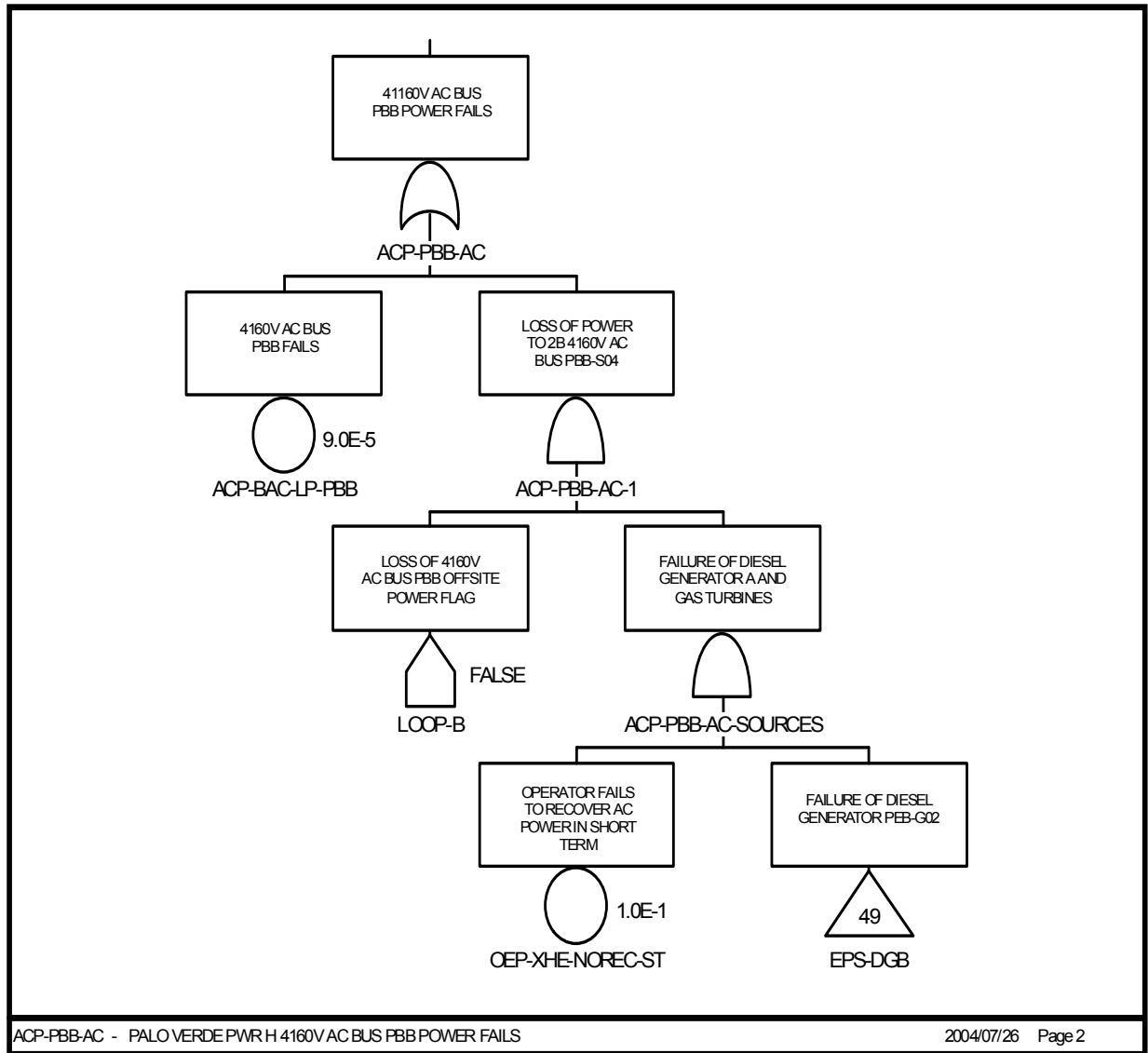


Figure 4: Modified fault tree ACP-PBB-AC.