

YANKEE ATOMIC ELECTRIC COMPANY

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BYR 2004-019

Document Control Desk
U.S. Nuclear Regulatory Commission
Washington, DC 20555-0001

Reference: (a) License No. DPR-3 (Docket No. 50-29)

Subject: Contaminated Concrete Calculation for the License Termination Plan (LTP)

This letter provides a hardcopy of the final calculation in support of the LTP¹ for the Yankee Nuclear Power Station (YNPS). The specific calculation provided is:

- (1) YA-CALC-00-001-04, "Assessment of Radionuclide Release from Contaminated Concrete at the Yankee Nuclear Power Station"

In support of Section 6.4.2 of the LTP, this calculation evaluates (1) the release of residual radioactive contaminants from the remaining subsurface concrete structures and (2) the associated dose due to that release, in consideration of allowing portions of existing structures to remain on site at the time of license termination. Analyses were performed using DUST-MS to assess the rate of release for each radionuclide from the concrete. Using the same assumptions that were applied to the soil DCGL calculation (and where appropriate, the same input parameters), RESRAD was used to calculate the dose from water pathways. Values for selected RESRAD input parameters were chosen to match the release rate calculated by DUST-MS.

The results of this analysis will be used with specific criteria to support the license termination process. This criterion will use the dose factors from this analysis to calculate concrete volumetric DCGLs that are equivalent to 0.5 mrem per year. These DCGLs will be used to support remediation decisions for all subsurface volumetrically contaminated concrete at the site through characterization sampling. If these subsurface

¹ YAEC Letter to USNRC, "Submittal of YNPS License Termination Plan and Proposed Revision to Possession Only License," dated November 24, 2003, BYR 2003-080.

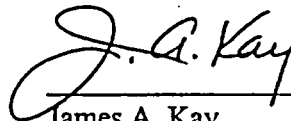
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structures are shown to exceed these DCGLs then remediation will be performed. The remediation activities could range from selective removal of the contamination or removal of the entire subsurface structure. The use of the 0.5 mrem DCGLs will also require that the soil DCGLs be reduced to be equivalent to 24.5 mrem for the final status surveys of the land areas. This will ensure that the dose from all pathways is within the NRC's site release criteria from 10CFR20 Subpart E.

This calculation is provided for your review. If you have any questions, please contact us.

Sincerely,

YANKEE ATOMIC ELECTRIC COMPANY



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Principal Licensing Engineer

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Calculation Title Page

Assessment of Radionuclide Release from Contaminated Concrete at the
Yankee Nuclear Power Station

Title

YA-CALC-00-001-04

Calculation Number

Executive Summary

Yankee Atomic Energy Company (YAEC) is considering allowing portions of existing structures at the Yankee Nuclear Power Station (YNPS) to remain on site at the time of license termination. Accordingly, release of residual radioactive contaminants (i.e., H-3, C-14, Co-60, Ni-63, Sr-90, and Cs-137) from remaining subsurface concrete structures (Darman, 2004) and dose due to that release must be evaluated. Analyses were performed using DUST-MS to assess the rate of release for each radionuclide from the concrete, based upon an assumed concentration of 1 pCi/g and a concrete density of 2.5 g/cm³. Using the same assumptions that were applied to the soil DCGL calculation (and where appropriate, the same input parameters), RESRAD was used to calculate the dose from water pathways. Values for selected RESRAD input parameters were chosen to match the release rate calculated by DUST-MS. The results indicated that Cs-137 yielded the highest dose.

Approvals

(Print & Sign Name)

Preparer: Terrence Sullivan (BNL)

Terrence Sullivan Date: 3/3/04

Reviewer: Estella Keefer

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Reviewer: Joseph Bisson

Date:

Reviewer: Peter Littlefield

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Reviewer: Alice Carson

Date:

Approval (Cognizant Manager): Greg Babineau

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Approval (Cognizant Manager): Greg Babineau *GM Babineau* Date: 3/4/04

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Purpose

Yankee Atomic Energy Company (YAEC) is considering allowing portions of existing structures to remain on site at the time of license termination. Analyses of core bores taken from the Spent Fuel Pit/Ion Exchange Pit wall have indicated the presence of H-3, C-14, Co-60, Ni-63, Sr-90, and Cs-137 (Darman, 2004). Release of residual radioactive contaminants, consisting of H-3, C-14, Co-60, Ni-63, Sr-90, and Cs-137, from subsurface concrete structures that may be left in place at the Yankee Nuclear Power Station (YNPS) is the subject of this assessment. Analyses were performed to assess the rate of release from the concrete and the resulting dose in the groundwater pathway.

Summary of Results

A two-prong approach was taken: (1) to determine the source term from the concrete to the groundwater and (2) to determine the dose from this source term. Two mechanisms were considered in determining the source term: diffusive release from the concrete and sorption onto backfill and soil that surround the facilities. Diffusive release was found to be the rate-limiting step for all six radionuclides in the analysis.

Additional analyses were performed to determine the impact that contaminant distribution in the walls has on release rate. These analyses showed that for every radionuclide except H-3 (that is, C-14, Co-60, Ni-63, Sr-90, and Cs-137), the peak release rate was only affected by the concentration within the first inch of the wall. Therefore, the effect of having a non-uniform distribution in concentration through the thickness of the wall is minimal for these radionuclides. Tritium has a higher concrete diffusion coefficient than the other radionuclides addressed. Accordingly, release of H-3 from concrete is influenced by concentrations within the first few inches of the wall.

Using a concentration of 1 pCi/g and a concrete density of 2.5 g/cm^3 , the total release to the subsurface was estimated for each radionuclide. Values for RESRAD input parameters were selected to match the release rate calculated by DUST-MS. Using the same assumptions that were used for the soil DCGL calculations, RESRAD was used to calculate the water pathway dose. Cesium-137 yielded the highest resulting dose. Estimates of the dose were made using measured data of contaminant concentrations in the first inch of concrete.

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Method of Calculation

YNPS is undergoing decontamination and decommissioning (D&D) and, eventually, license termination. The objective for decommissioning YNPS is to reduce residual radioactivity to levels that permit release of the site for unrestricted use in accordance with the Nuclear Regulatory Commission's (NRC's) site release criteria set forth in 10CFR20, Subpart E.

Yankee Rowe has identified five structures that may partially remain at the time of license termination:

- a. Primary Auxiliary Building (PAB) Primary Drain Collection Tank (PDCT) Cubicle
- b. PAB Gravity Drain Tank (GDT) Cubicle
- c. Spent Fuel Pit (SFP)
- d. Waste Disposal Building (WDB) Cubicles
- e. Elevator Pit

Because these partial structures may contain residual radioactivity, the possible dose attributable to these structures must be evaluated. Evaluating the dose depends on knowing the distribution of radionuclides in the remaining material and the potential mechanisms by which radionuclides in the material could reach groundwater. Therefore, this calculation addresses the potential release of radionuclide contamination from subsurface concrete structures and the associated dose.

Body of Calculation

1.0 Contamination Source

1.1 Contamination Data

Two cores were taken from the wall between the Spent Fuel Pit (SFP) and the north compartment of the Ion Exchange Pit (IX Pit). The cores were taken at an elevation approximately 5 feet from the IX Pit floor. At this elevation, the concrete wall was exposed to contaminated water on both the SFP side and the north compartment of the IX Pit side. For the purpose of this calculation, both sides of all concrete walls are considered to be contaminated. Although in the case of the SFP/IX Pit wall, this represents actual conditions, in other cases, only one side of the wall was exposed to contaminated water. Therefore, the assumed concentration profile represents a worst case. The SFP wall ranges in thickness from 4.5 feet at the bottom to 6 feet at the top. Removal of the wall down to an elevation of 1022'-8" is planned, and thus the thickness of the remaining portions of the wall will be less than 6 feet. However, for conservatism, the wall will be considered to have a constant thickness of 6 feet, when evaluating potential releases.

Concentration data are available for H-3 levels in the wall around the SFP as depicted in Figures 1 and 2 (Darman, 2004). Concentration data for other radionuclides (Cs-137, Co-60, C-14, Ni-63, and Sr-90) are available from a one-inch sample taken at the interface with the SFP (Darman, 2004). Measurable levels of H-3 were found throughout the entire core of the wall between the IX Pit and the SFP. The average H-3 concentration throughout the entire thickness of the concrete wall was 25 pCi/g (Darman, 2004). The average within one-foot of the SFP and IX pit was greater than 50 pCi/g. Several radionuclides, including Cs-137, Co-60, Ni-63, Sr-90, and C-14, were found within the first inch of the interface of the wall and the SFP. Contamination levels ranged from 1075 pCi/g for Cs-137 to 0.91pCi/g for Sr-90.

In addition, frisker data are available and provide insight on the distribution of contaminants, other than H-3, in the concrete. Frisker measurements were taken on the surfaces of one-inch segments from the core samples of the wall between the SFP and IX Pit (see Figures 1 and 2). Contamination levels greater than 350,000 dpm/100 cm² were identified on the SFP-side surface of the first one-inch segment of the core (Darman, 2004). The other surface of this segment (that is, one-inch deep into the SFP/IX wall) showed less than 15,000 dpm/100 cm²—more than an order of magnitude less. On the second one-inch segment of the core, contamination levels continued to decline with a maximum value less than 3500 dpm/100 cm². Frisker results at the far surface of the second one-inch core segment (approximately 2 inches from the SFP surface) showed background radiation levels.

Assuming a linear change in concentration between the two frisker measurements in each sample, the average concentration is one-half the value of the frisker measurement on each side of the core. Therefore, in the first inch, the average value is greater than 187,500 dpm/100 cm² ($0.5 \times (350,000 + 15,000)$). While in the second inch, the average

value is less than 1800 dpm/100 cm² ($0.5 \times (3500 + \text{background})$, which is assumed to be less than 100 dpm/100 cm²). This suggests that more than 98% of the activity ($100 \times 187,500 / (187,500 + 1800)$) is within the first inch of concrete, with the remainder in the second inch. Although frisker measurements do not represent the contamination levels of a particular radionuclide, the previously described distribution of contamination is assumed to be representative of each of the radionuclides under consideration with the exception of H-3 (e.g., Cs-137, Co-60, C-14, Ni-63, and Sr-90). Figures 1 and 2 (Darman, 2004) show the measured H-3 contamination data obtained from the cores in the SFP/IX Pit wall.

To calculate the magnitude of the source, the maximum potential volume of contaminated concrete is also needed. Dimensions of the walls for facilities that may be left *in situ* are shown in Table 1. To estimate the mass of concrete, the density of concrete is needed. Since a site-specific value is not known, a conservative density of 2.5 g/cm³ for the concrete has been assumed.

Table 1 Dimensions of subsurface structures after removal of above grade sections.

Structure	Component	Below Grade Dimensions*			Area (ft ²)	Volume (Full Wall Thickness)		Mass (g) Full Wall Thickness	Volume (m ³) 1" both sides of wall	Mass (g) 1" both sides of wall
		Height (ft)	Width (ft)	Thickness (ft)		ft ³	m ³			
PAB	floor			2.50	193.75	484.38	13.71	3.43E+07	9.14E-07	2.28E+06
PDCT	wall 1	18.50	12.50	1.00	231.25	231.25	6.54	1.64E+07	1.09E+00	2.73E+06
	wall 2	18.50	12.50	1.00	231.25	231.25	6.54	1.64E+07	1.09E+00	2.73E+06
	wall 3	18.50	15.50	1.00	286.75	286.75	8.12	2.03E+07	1.35E+00	3.38E+06
	wall 4	18.50	15.50	1.75	286.75	501.81	14.20	3.55E+07	1.35E+00	3.38E+06
PAB	floor			2.50	157.64	394.09	11.15	2.79E+07	7.44E-01	1.86E+06
GDT	wall 1	18.50	10.17	1.00	188.15	188.15	5.32	1.33E+07	8.87E-01	2.22E+06
	wall 2	18.50	10.17	1.00	188.15	188.15	5.32	1.33E+07	8.87E-01	2.22E+06
	wall 3	18.50	15.50	1.00	286.75	286.75	8.12	2.03E+07	1.35E+00	3.38E+06
	wall 4	18.50	15.50	1.00	286.75	286.75	8.12	2.03E+07	1.35E+00	3.38E+06
SFP	floor			3.00	555.56	1666.67	47.17	1.18E+08	2.62E+00	6.55E+06
	wall 1	14.67	16.50	6.00	242.06	1452.33	41.10	1.03E+08	1.14E+00	2.85E+06
	wall 2	14.67	16.50	6.00	242.06	1452.33	41.10	1.03E+08	1.14E+00	2.85E+06
	wall 3	14.67	33.67	6.00	493.94	2963.63	83.87	2.10E+08	2.33E+00	5.82E+06
	wall 4	14.67	33.67	6.00	493.94	2963.63	83.87	2.10E+08	2.33E+00	5.82E+06
WDB Cubicles	floor			1.17	126.00	147.42	4.17	1.04E+07	5.94E-01	1.49E+06
	wall 1	9.83	9.00	1.00	88.47	88.47	2.50	6.26E+06	4.17E-01	1.04E+06
	wall 2	9.83	9.00	1.00	88.47	88.47	2.50	6.26E+06	4.17E-01	1.04E+06
	wall 3	9.83	14.00	1.00	137.62	137.62	3.89	9.74E+06	6.49E-01	1.62E+06
	wall 4	9.83	14.00	1.00	137.62	137.62	3.89	9.74E+06	6.49E-01	1.62E+06
Elevator Pit	Floor			1.00	70.47	70.47	1.99	4.99E+06	3.32E-01	8.31E+05
	wall 1	6.50	7.83	1.00	50.90	50.90	1.44	3.60E+06	2.40E-01	6.00E+05
	wall 2	6.50	7.83	1.00	50.90	50.90	1.44	3.60E+06	2.40E-01	6.00E+05
	wall 3	6.50	9.00	1.08	58.50	63.18	1.79	4.47E+06	2.76E-01	6.90E+05
	wall 4	6.50	9.00	1.08	58.50	63.18	1.79	4.47E+06	2.76E-01	6.90E+05
TOTAL						1.45E+04	4.10E+02	1.02E+09	2.47E+01	6.17E+07

*References for wall dimensions are provided in Appendix A.

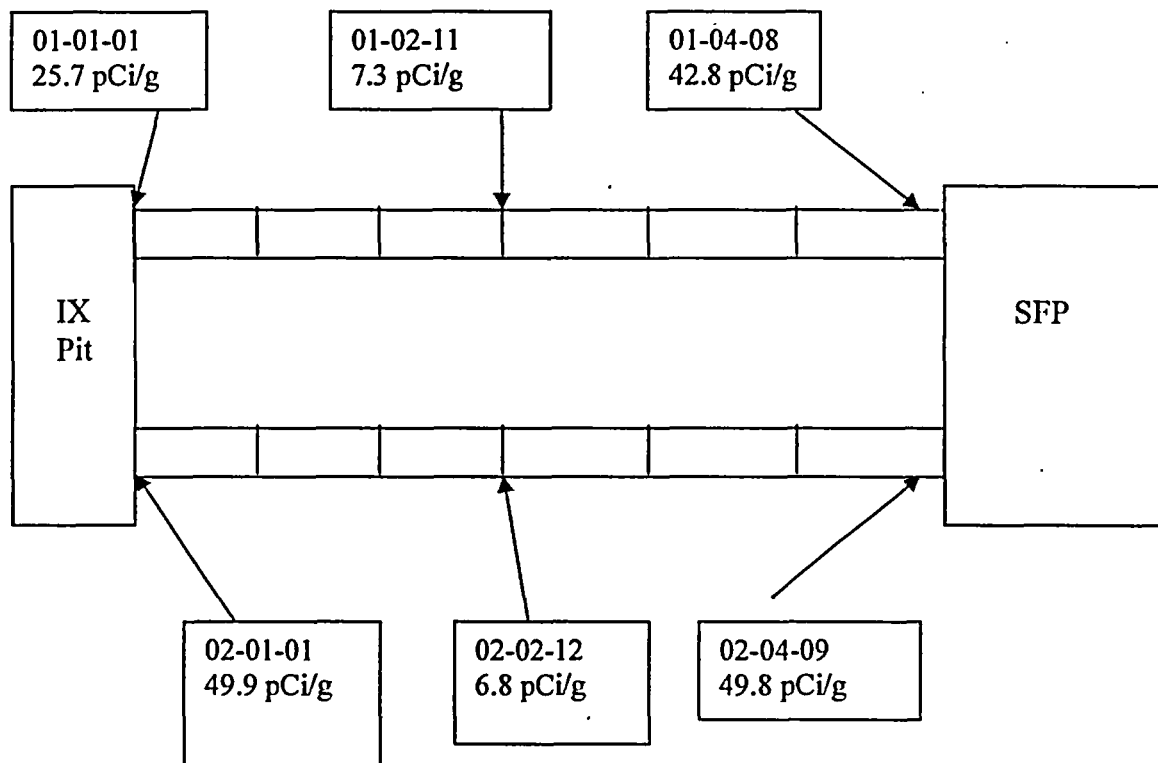


Figure 1 H-3 Contamination data between the Spent Fuel Pit and the Ion Exchange Pit

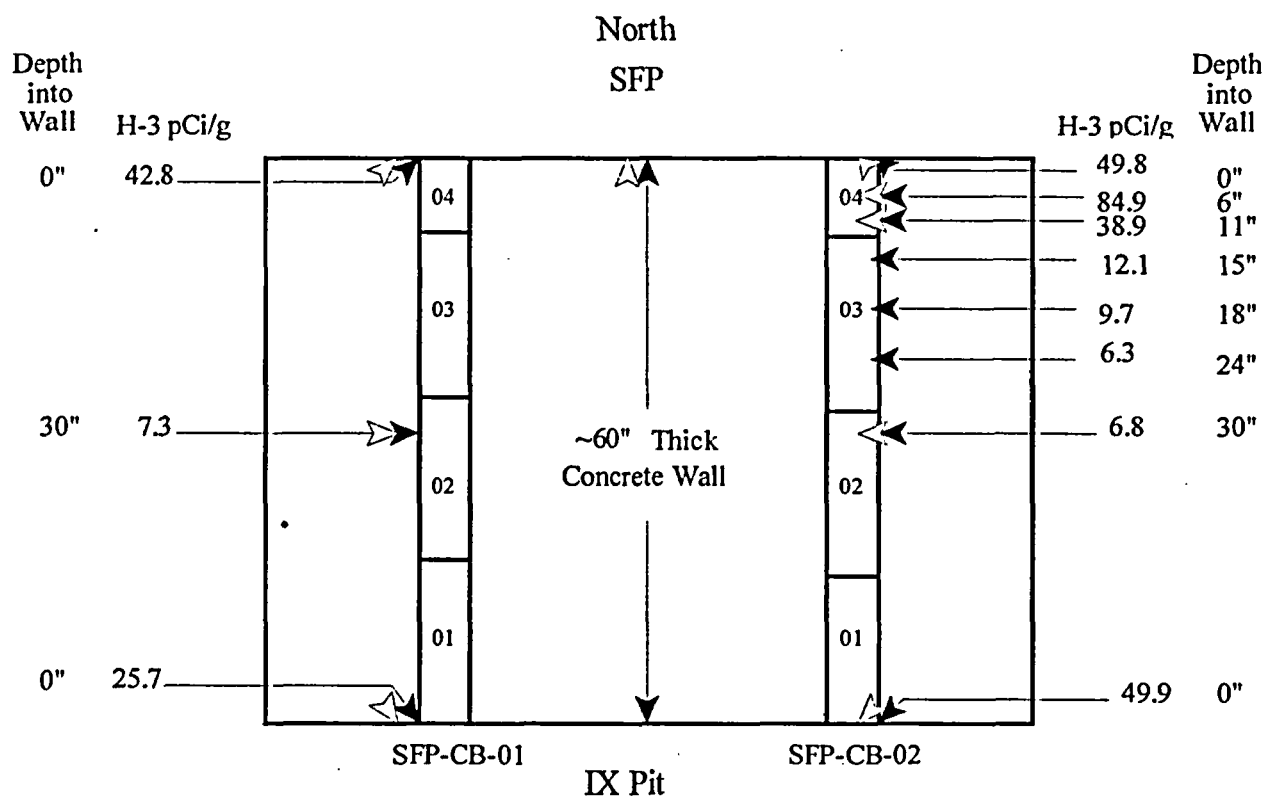


Figure 2 Rotated View of H-3 levels in concrete near the SFP.

The total volume and mass of the floors and walls in Table 1 are 410 m^3 and $1.02\text{E}+09 \text{ g}$ ($1.02\text{E}+06 \text{ kg}$), respectively. From Table 1, approximately 300 m^3 (the sum of the volumes of the four SFP walls plus floor) of the total 410 m^3 of concrete is associated with the SFP, and thus the SFP contributes more than 73% of the total volume of contaminated concrete.

As indicated by frisker data from the SFP/IX Pit wall, radionuclides such as C-14, Co-60, Ni-63, Sr-90, and Cs-137 are mainly present within the first inch of concrete. Thus, to determine the magnitude of the source associated with these radionuclides, the volume and mass of this portion of the concrete is needed. As indicated in Table 1, the volume that represents this portion of walls is approximately 25 m^3 , and the mass of this portion is $6.17\text{E}+07 \text{ g}$ ($6.17\text{E}+04 \text{ kg}$). The ratio of this portion of the wall volume to the total wall volume is 0.06. This value will be used when calculating the amount of contamination released from the first inch of concrete.

1.2 Contaminant Distributions

For evaluating diffusion releases, two profiles were considered for all radionuclides:

- a) Uniform throughout the entire width of the wall
- b) Non-uniform based on measured data.

For the uniform distribution model, the source estimate is normalized to an initial concentration of 1 pCi/g

For the model addressing non-uniform distributions of contaminants, the peak concentration is normalized to 1 pCi/g , and both surfaces are assumed to be contaminated symmetrically about the centerline of the wall. Two non-uniform distributions were developed—the first for H-3 and a second for radionuclides other than H-3 (that is, C-14, Co-60, Ni-63, Sr-90, and Cs-137). The first distribution is that displayed in Figures 1 and 2 for H-3. The second distribution assumes that all of the contamination is within the first inch of concrete. For the second distribution, a homogeneous distribution of 1 pCi/g is assumed in that first inch of wall thickness.

Using an initial concentration of 1 pCi/g simplifies the calculation of the actual annual releases and subsequent doses. Subsequently, a calculation is made by scaling the results for 1 pCi/g by the actual measured values.

2.0 Modeling Release from Contaminated Concrete

2.1 Overview

The concrete will eventually release radionuclides to the surrounding backfill and these radionuclides will undergo sorption during their movement through the backfill to a receptor (e.g., drinking water and irrigation) well. Therefore, the radionuclide concentration in the well is a function of the release rate from the concrete and the transport to the well. Three models were considered:

- The first model assumes that the concrete releases the entire inventory instantly and the well concentration is controlled by sorption in the backfill. This may be reasonable for radionuclides that have high sorption coefficients.
- The second model assumes that release is controlled by the concrete and that everything released from the concrete gets to the well instantly. This is a reasonable assumption for radionuclides that do not exhibit much sorption on the backfill or that are released slowly from the concrete.
- The third model assumes that whatever is released through the concrete must be transported to a well. This conceptual approach considers release and transport, whereas the first two consider only release.

All three of these approaches will be considered where appropriate. The results of the first two models, sorption-controlled and diffusion-controlled release, will be compared and the approach that has the lowest release rates will be used to calculate release rate information needed for RESRAD simulations. The lowest release rate is used because both of these processes (release from the concrete and transport to the well) need to occur before contaminants can reach a well. Therefore, the rate-limiting step is the process with the lowest release rate.

An important outcome of modeling diffusion-controlled releases is the identification of a diffusion profile that can be used to help develop characterization data needs. An analysis of these diffusion profiles is presented in Section 2.2.5.

2.2 Modeling Approaches

2.2.1 Instantaneous Release

Using the mass from Table 1 of $1.02\text{E}+09$ g, the concrete would contain $1.02\text{E}+09$ pCi if the walls were homogeneously contaminated to 1 pCi/g. Assuming instantaneous equilibrium with the backfill and the water, the concentration in the contaminated zone, C_{cz} , can be calculated from the following equation (Yu, 2001):

$$C_{cz} = M_r / (A \times T \times \eta \times \beta \times R_d) \text{ (pCi/l)} \quad (1)$$

Where:

M_r = activity released, $1.02\text{E}+09$ pCi

A = area perpendicular to flow in the contaminated zone (m^2)

T = thickness parallel to flow in the contaminated zone (m)

β = 1000 conversion factor for m^3 to liters

R_d = retardation coefficient = $1 + \rho K_d / \eta$ (dimensionless)

ρ = bulk density = 1.51 g/cm^3

K_d = distribution coefficient (cm^3/g)

η = saturated zone porosity = 0.43 (dimensionless)

The specified parameter values for bulk density and porosity were those values used in dose assessments performed using RESRAD for soil contamination at Yankee Rowe (YA 2004).

In calculating the area perpendicular to flow, all five remaining structures were assumed to be oriented in the direction of groundwater flow for conservatism. This orientation provides the least amount of water flow through the concrete and, therefore, results in the lowest amount of dilution. Considering the information in Table 1 and selecting the longest side of each facility (l_i), this length, L , can be calculated:

$$L = \sum l_i \quad (2)$$

Table 2 contains the value of l_i for each building, the wall thickness for the two confining walls of that building, and the value of L . Length of longest sides for each facility in Table 1.

Table 2 Length of longest sides for each facility in Table 1.

Location	l_i (ft)	Wall One Thickness (ft)	Wall Two Thickness (ft)
PAB PDCT	15.50	1.75	1
PAB GDT	15.50	1	1
SFP	33.67	6	6
WDB Cubicles	14.00	1	1
Elevator Pit	9.00	1.08	1.08
L (total in ft)	87.67	10.83	10.08
L (total in m)	26.7	3.3	3.07

This total length, L , is the summation of the longest sides of each structure, and is equal to 26.7 m, the length that will be backfilled. Using this value for the length and using the total volume of the walls given in Table 1, 410 m³, the area perpendicular to flow is 15.4 m².

In order for a comparison with the diffusion release model to be made, the fraction of the total inventory that is captured by the well must be determined. Assuming that depletion effects are not important unless the total inventory is released, the total inventory delivered to the well within the first year, which is equivalent to the release rate, can be calculated from (Yu, 2001),

$$I_w = C_{cz} \times V_d \times A \times \beta \quad (\text{pCi/y}) \quad (3)$$

Where:

C_{cz} = the concentration in the contaminated zone (pCi/l)

V_d = Darcy Velocity in the saturated zone = $K_{sat} \times H = 250.6$ m/y

When H = hydraulic gradient = 0.1 m/m, (YA, 2004); and

K_{sat} = the saturated hydraulic conductivity in the saturated zone = 2506 m/y (YA, 2004)

A = area perpendicular to flow in the contaminated zone (m²)

β = 1000 conversion factor for m³ to liters

If I_w exceeds the total inventory available for release, it is limited to the total inventory.

Table 3 presents the contaminated zone concentration, total and fractional release results for the above parameters.

Table 3 Maximum concentration for instantaneous release and fractional release for release controlled by sorption on the backfill from concrete homogeneously contaminated to 1 pCi/g.

Radionuclide	K_d^* (cm ³ /g)	Contaminated zone concentration** (C _{cz} pCi/l, Eqn (1))	Release rate (I _w) (pCi/y, Eqn (2))	Fractional Release in the first year
H-3	0.06	5.1E+03	1.02E+09	1.0
C-14	11	1.3E+02	5.6E+08	0.55
Co-60	235	6.2E+00	2.7E+07	0.026
Ni-63	424	3.4E+00	1.5E+07	0.0146
Sr-90	31.5	4.6E+01	2.0E+08	0.196
Cs-137	446	3.3E+00	1.4E+07	0.014

* Mean values used in Yankee Rowe assessment for soil DCGLs (YA, 2004).

** Value in contaminated zone. Depletion would occur in less than 1 year. Therefore, the average concentration in the well, which can be calculated as the inventory (pCi) divided by the volumetric flow rate (l/y), is 230 pCi/l for the year. This is less than the contaminated zone value.

If the contamination is limited to the first inch of concrete, the associated inventory would be 0.06 of the inventory of the full wall contamination, and the inventory released would decrease similarly. Thus, the fractional release would remain the same.

2.2.2 Diffusion-Controlled Release

Previous estimates of release rates assumed that the entire inventory was instantaneously released from the concrete into the contacting water. This is a very conservative assumption, as there are several studies that show that release from concrete is not instantaneous but is controlled by diffusion or solubility (Sullivan, 1993). Therefore, a more realistic conceptual model for estimating release from the concrete assumes that diffusion is the rate-controlling mechanism. A one-dimensional finite difference model was set up to represent the system as shown in Figure 3. The DUST-MS code was used to perform the analysis (Sullivan, 1993).

Diffusion coefficients of ions in pure water are generally around 1.0E-05 cm²/s (Freeze, 1979). In porous media, such as soil, the effective diffusion coefficient is much smaller than in pure water because of the longer paths caused by particles in the porous media. For a wide range of ions in porous media, reductions by a factor of 0.5 to 0.01 are frequently observed (Freeze, 1979). In the porous media/water regions surrounding the concrete, the diffusion coefficient was set to 1.0E-06 cm²/s (Freeze, 1979) to provide rapid transport away from the concrete and thereby enhance the predicted rate of release. This value is in the middle of the range of observed values (Freeze, 1979). The diffusion coefficient of each radionuclide in the concrete is discussed later.

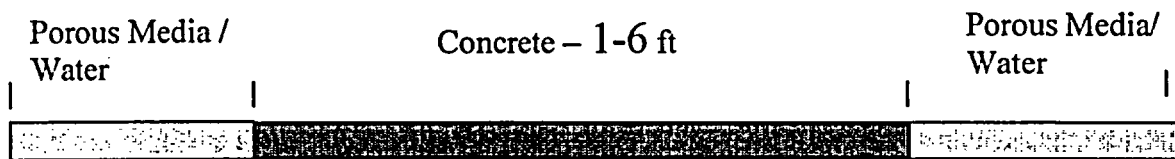


Figure 3 Conceptual model for diffusion release through concrete into porous media

For large computational cells sizes, finite difference models are known to over-predict diffusion releases at boundaries having sharp changes in diffusion coefficients. To overcome this, the concrete was modeled with 300 computational cells. All simulations used a 0.01 cm cell for the first 50 and last 50 cells. The cell size for the internal 200 computational volumes was adjusted to match the desired distance. For example, for a one-foot thick wall (30.48 cm), there were 50 cells of 0.01 cm, 200 cells of 0.1474 cm, and 50 cells of 0.01 cm for a total thickness of 30.48 cm and a total of 300 cells.

The non-homogeneous distribution for H-3 was modeled using the data in Figure 2. A non-homogeneous distribution for the remaining nuclides used a uniform concentration in concrete within the first inch of both wall surfaces and zero concentration in the remaining thickness of concrete.

Contamination is assumed to exist in the walls and floors of the five structures listed in Table 1. Table 1 contains seven different thicknesses (1 ft, 1.08 ft, 1.17 ft, 1.75 ft, 2.5 ft, 3 ft, and 6 ft.) and release calculations were performed for each thickness. Release rate estimates were calculated using the one-dimensional finite difference computer code, DUST-MS (results for each wall and floor in the five buildings are presented in Appendix B, and summarized in Table 4). Release from the concrete is assumed to be controlled by diffusion. The initial distribution of contaminants was assumed to be a uniform concentration of 1 pCi/g.

2.2.2.1 Experimental Diffusion Coefficients

Studies have been conducted for the diffusion in concrete of the radionuclides under consideration at YNPS (H-3, C-14, Co-60, Ni-63, Sr-90, and Cs-137). In general of these radionuclides, H-3 diffuses the fastest and C-14 diffuses at the slowest rate. Literature values for H-3 diffusion range from $6.0\text{E-}09 \text{ cm}^2/\text{s}$ to $5.5\text{E-}07 \text{ cm}^2/\text{s}$ (Matsuzuro, 1976; Serne, 2001; Szanto, 2002). For the purposes of analysis, a diffusion coefficient (D) of $5.5\text{E-}07 \text{ cm}^2/\text{s}$ will be used as the base case. This is the highest value and will provide an upper bound on diffusive releases.

Diffusion coefficients in concrete for Cs-137 range from $4.0\text{E-}11 \text{ cm}^2/\text{s}$ to $3.0\text{E-}09 \text{ cm}^2/\text{s}$ (Atkinson, 1986). Diffusion coefficients for Co-60 range from $5.0\text{E-}12 \text{ cm}^2/\text{s}$ to $4.0\text{E-}11 \text{ cm}^2/\text{s}$ (Muurinen, 1983). Diffusion coefficients for Sr-90 range from

1.0E-11 cm²/s to 5.2E-10 cm²/s in Portland cement (Sullivan, 1988). Diffusion coefficients for Ni-63 range from 8.7E-10 cm²/s to 1.1E-09 cm²/s in concrete (Jakob, 1999). An average diffusion coefficient for Ni-63 in concrete is given as 5.0E-10 cm²/s (Serne, 2001). Although higher values have been found for many of these radionuclides in different concretes encapsulating radioactive wastes, these values are not relevant to this situation, as the radioactivity in the wastes is known to degrade concrete performance (Sullivan, 1988) and thus are not representative of the concrete at YNPS. The highest value in each of the ranges was used in modeling releases from the concrete.

In the chemical environment associated with concrete, carbon is not readily transported through the concrete because carbon will form carbonates. Experiments have estimated diffusion coefficients based on leaching data. The estimated diffusion coefficient values range from 7.0E-15 cm²/s to 1.0E-12 cm²/s (Habeyab, 1985; Serne, 2001). These values suggest that C-14 is not mobile in concrete systems. For this study, a value 1.0E-12 cm²/s was used. This will provide an upper bound estimate of C-14 releases.

Table 4 summarizes the values selected for modeling diffusion from concrete.

Table 4 Concrete diffusion coefficients selected from the literature for evaluation of release

Radionuclide	Diffusion Coefficient (cm ² /s)
H-3	5.5E-07
C-14	1.0E-12
Co-60	4.0E-11
Ni-63	1.1E-09
Sr-90	5.2E-10
Cs-137	3.0E-09

2.2.2.2 Predicted Release Rates And Cumulative Release For Homogeneously Contaminated Walls

Figure 4 presents the release rate for H-3 in pCi/y over a ten-year period from a six-foot thick wall initially contaminated uniformly to 1 pCi/g. Other radionuclides had similar release curves but at lower magnitudes due to their lower diffusion coefficients. The release rate in Figure 4 declines rapidly between years 1 and 2 due to the high initial leach rate caused by the sharp gradient. For this reason, the first year release rate, which is the maximum, is used in developing a source term for RESRAD calculations. In general, the release rate from a solid source that maintains the external boundary at zero concentration is greatest initially and decreases by the square root of time adjusted for decay until depletion effects occur (Crank, 1956). The general trend of decreasing release rates over time is evident in Figure 4.

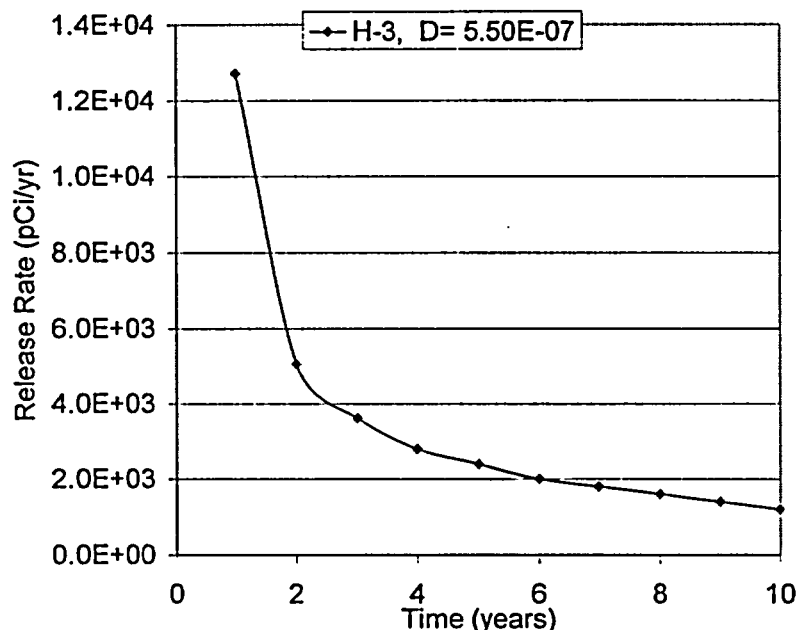


Figure 4 H-3 release rate (pCi/y) over ten years for a six-foot thick wall uniformly contaminated to 1 pCi/g using a diffusion coefficient, $D = 5.5E-07$ cm²/s.

Appendix B presents the first year fractional release rate and total annual release rate from each wall and floor in the five subsurface facilities for H-3, Cs-137, Co-60, Sr-90, C-14, and Ni-63. The last row of these tables presents the average fractional release from the entire facility and the total release (Ci). The average fractional release is the total release divided by the total inventory. Thus, it is most heavily weighted by the facilities with the largest volume of concrete which in this case is the SFP. The fractional release rate is the percentage of the total inventory that is released. The total release rate is the peak annual release rate (Ci/y) for concrete uniformly contaminated to 1 pCi/g. Table 5 summarizes the results and is the summation of releases from all walls and floors.

Table 5 Average fractional release and total release from all subsurface facilities for initial uniform contamination of 1 pCi/g in all walls and floors.

Radionuclide	Average fractional release	Peak Release Rate (pCi/y)
H-3	6.29E-02	6.45E+07
C-14	3.02E-04	3.10E+05
Co-60	1.02E-03	1.05E+06
Ni-63	4.88E-03	5.00E+06
Sr-90	3.41E-03	3.49E+06
Cs-137	7.82E-03	8.02E+06 ¹

Comparing the results from Tables 3 and 5 for peak release rates, it is seen that the release rates for each radionuclide are lower in the diffusion-controlled transport model than in the sorption-limited transport model. This implies that release to the wells cannot be faster than the rate supplied by diffusion from the concrete. The reason that diffusion is rate-controlling is due primarily to the high flow velocity in the saturated zone that leads to more than 4E+06 liters of water per year passing through the contaminated zone. This high flow rate is effective in "flushing" the system in the sorption-limited case leading to higher predicted releases than for diffusion-controlled transport. Therefore, the diffusion-controlled release rates in Table 5 are used for developing parameters for RESRAD to calculate dose.

As shown in the tables in Appendix B the peak release rate per unit surface area is relatively constant for the diffusion model. This implies that it is the amount of surface area that is critical to estimating release. Most of the contamination released within the first year resides within one inch of the surface; therefore, having a thicker wall with uniform contamination does not impact the amount of contamination released.

2.2.2.3 Predicted Release Rates For Walls Contaminated Uniformly For The First Inch

Characterization data indicate that for C-14, Co-60, Ni-63, Sr-90, and Cs-137 the contamination is confined within two inches of the surface and 98% of the inventory is within 1 inch of the surface. This is consistent with lower diffusion rates of these contaminants into the concrete as compared to that of H-3, which shows a much larger spatial distribution of contaminants. Calculations were performed for each wall thickness and each radionuclide having a uniformly contaminated zone of one inch thickness. In these models, the outer inch had contamination of 1 pCi/g while the interior section had a concentration of 0 pCi/g.

Comparing Tables 5 and 6, the predicted maximum release rates are nearly identical for all radionuclides except for H-3. This indicates all of the release is constrained to contamination residing within 1 inch of the wall for everything except H-3. Also supporting this conclusion is that on average for all of the wall thicknesses, although the volume of the wall within 1 inch of the surface is 0.06 of the total wall volume, the

fraction of these radionuclides released is much less than 0.06 of the total inventory of these radionuclides contained within the total wall thickness.

For the case assuming 1-inch thickness of contamination, the predicted total release of H-3 in the first year is approximately one-half (46%) the amount predicted when contamination is assumed throughout the entire wall. However, this distribution is not appropriate for H-3 as it is known that H-3 is not confined to the first inch of concrete, as seen in Figures 1 and 2.

Table 6 Average fractional release and total release from all subsurface facilities for initial uniform contamination of 1 pCi/g in the first inch of the walls and floors.

Radionuclide	Average fractional release	Peak Release Rate (pCi/y)
H-3	6.29E-02	2.97E+07
C-14	3.02E-04	3.10E+05
Co-60	1.02E-03	1.05E+06
Ni-63	4.88E-03	5.00E+06
Sr-90	3.41E-03	3.49E+06
Cs-137	7.82E-03	8.02E+06

2.2.2.4 Predicted Release Rates For Spatially Varying Initial Conditions

The preceding analysis suggests that releases from the concrete due to spatial variability in concentration will not influence the peak release rate for any radionuclide other than H-3 unless the variability occurs over the first inch. To examine the impact of spatial variability on release of H-3, the data presented in Figures 1 and 2 were used to generate the distributions shown in Figure 5. Figure 5 contains a unique curve for each of the 3 wall thicknesses. In all cases, symmetry is assumed about the centerline of the wall. The distributions for all three thicknesses are similar for the first six inches as this contains only measured data. After six inches, the concentration for the one-foot thick wall decreases more slowly than for the thicker walls. This is due to the measured concentrations (Figure 2) and assumed symmetry about the mid-plane of each wall. The symmetry assumption for the one-foot wall requires the concentration at 12 inches to equal to the surface concentration. The surface concentration is higher than the measured concentration at 12 inches. The second curve is the concentration distribution for the 2.5-foot thick wall. It is identical to that of the 6-foot thick wall for the first 1.25 feet. After that, the concentrations used to simulate the 2.5 feet wall increase due to symmetry. The third curve is for the 6-foot thick wall and is based on the data in Figures 1 and 2. In these simulations, the concentrations are normalized to the peak value, which is set to 1 pCi/g. Therefore, there is less total mass in the system as compared to the homogeneous distribution of 1 pCi/g throughout the wall thickness. The concentration in the first inch of the wall in the non-homogeneous distribution case is 59% of the peak value.

Simulations were made for 1, 2.5, and 6 foot thick walls. In each case, the peak release rate occurred in the first year and was between 820 pCi/y - 830 pCi/y. This suggests that even for H-3, the first year's release is controlled by the distribution in the first six inches. The non-homogeneous distribution release rate is 65% of the value obtained for the homogeneous case, which had a peak release rate of 1270 pCi/y. The average concentration in the first six inches of the non-homogeneous case is 0.67 pCi/g. This suggests that the release is approximately proportional to the total mass available, or average concentration, in the first six inches.

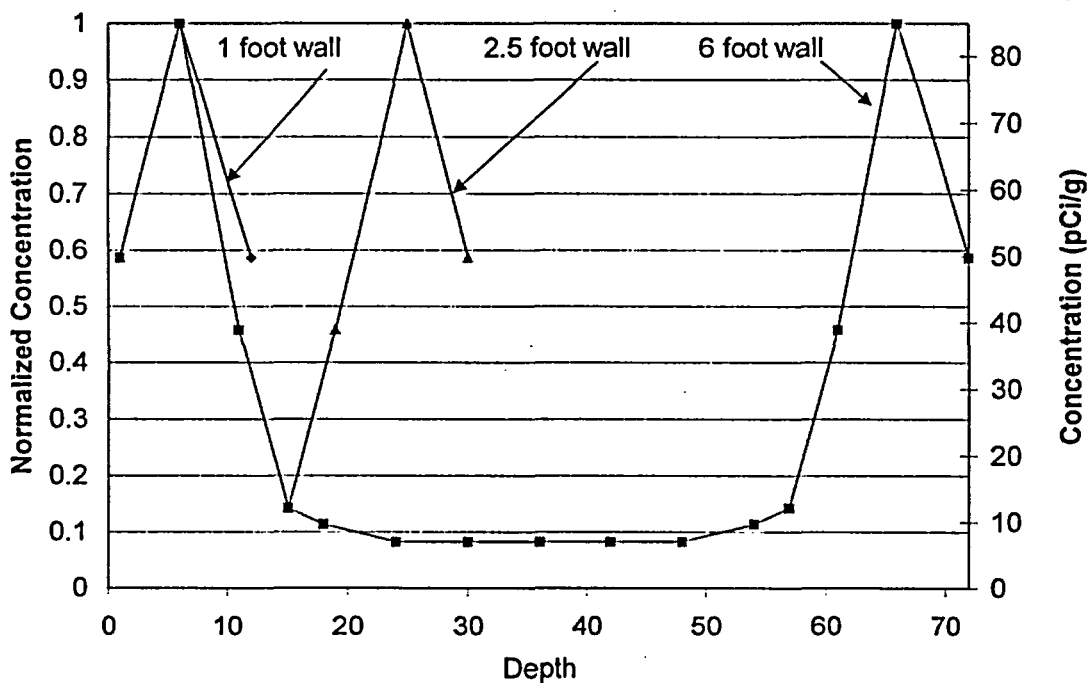


Figure 5 Modeled distributions of H-3 for 1, 2.5 and 6 foot thick concrete segments

2.2.2.5 Predicted Well Concentrations As A Function Of Transport Distance

The most complete modeling approach is to use the predicted diffusion release rates as a flux to the backfill and then calculate transport through the backfill as a function of distance. These calculations are presented to obtain an estimate of the impacts of transport after release. However, they will not be used in estimating releases for RESRAD as discussed later. The maximum distance to a well would be one-half the distance of the hypothetical length of the contaminated zone parallel to the aquifer (26.7 m). The simulations used the mean K_d values (Table 2) and saturated zone properties used in the YNPS analysis for soil contamination. The source was assumed to decrease only due to radioactive decay. For a homogeneous distribution of contaminants in the

source zone and diffusion-controlled release, the decrease in the source will always be greater than for decay alone.

The modeling results showed essentially no decrease in concentration for H-3, C-14, and Sr-90 at a distance of 13.3 m. This is due to the lower K_d values and high flow velocity. These contaminants are moving several to hundreds of meters per year, and there is no time for decay prior to reaching the well.

The three remaining radionuclides (Ni-63, Co-60, and Cs-137) are moving less than 1 m/y due to sorption and undergo decay prior to reaching the monitoring point. Co-60 showed an order of magnitude decrease in peak concentration between the wall and a monitoring point approximately 13 meters downstream. Cs-137 and Ni-63 peak concentrations decreased by a factor of 5 and 2, respectively, over this distance. The decrease in concentration is correlated with the half-life of the radionuclide, duration of the source, and the distribution coefficient.

Due to the complexity of picking an appropriate geometry and distance to a receptor well that is representative of the five subsurface structures and the fact that the peak concentration does not change substantially for most radionuclides, this approach will not be used to estimate source term concentrations in RESRAD calculations.

2.2.2.6 Discussion

Modeling was performed to assess whether it is sorption on the backfill or diffusion from the concrete that controls the rate of radionuclide release. The results indicate that diffusion is the rate controlling mechanism for all radionuclides in this study.

A series of diffusion calculations were performed to examine the affects of contaminant spatial distribution in the walls and to examine the impacts of wall thickness on peak release rates. The wall thickness did not impact the total release rate. Analysis showed that for all radionuclides, except H-3, diffusion release was controlled by the first inch of contaminated concrete. In fact, in simulations, the predicted peak release did not differ for a concrete wall with a one-inch thick contaminated zone at the surface versus a wall that was uniformly contaminated. For H-3, the distribution of contamination did make a difference. The peak release rate for the non-homogeneous case was reduced by the ratio of the inventory in the first six inches of the wall for the non-homogeneous case to that in the wall for the homogeneous case.

Modeling of the inputs of sorption after release was investigated but is not used in the determination of source term and dose.

The analyses suggest that the impacts of a non-uniform contaminant distribution are minimal for every radionuclide except H-3. For H-3 lower releases did occur, but this was primarily due to less mass available for release with the non-homogeneous distribution. For this reason, the values obtained for a homogeneous distribution of

contaminants throughout the wall thickness, Table 5, are used as the basis for calculating the source term for use in RESRAD.

2.2.3 Diffusion Profiles And Their Impact On Data Collection

It is important to determine what characterization data are necessary in order to calculate peak release rates in a system where these rates are controlled by diffusion. To address this consideration, modeling was performed for diffusion releases with a uniform initial concentration of 1 pCi/g throughout the wall. Profiles were generated for 1 and 6-foot thick walls for H-3 and Cs-137. Previous results demonstrated that for a uniform initial concentration, the peak release occurs in the first year (Figure 4). Therefore, the diffusion profiles in the concrete after 1 year will provide guidance about the depth of the diffusion front, and therefore, the depth to which characterization information is required.

Figure 6 presents the diffusion profile for H-3 in a one-foot thick wall. The figure displays concentration versus depth from the surface up to 6 inches. Symmetry is assumed about the midpoint (6 inches) due to the uniform initial condition in the concrete. Examining the figure, the boundary concentration dropped from 1 pCi/g initially to 0.4 pCi/g. From the surface, the concentration increases gradually reaching a maximum of 0.93 pCi/g after 4 or 5 inches. The concentration remains constant from this point until the 6 inch distance. The drop from 1 pCi/g to 0.93 pCi/g represents radioactive decay over the time step.

Figure 7 presents a similar diffusion profile for Cs-137 in a 1-foot thick wall. In this case, the surface concentration decreases to less than 0.03 pCi/g and rises to almost 1 pCi/g over the first ¼ inch. After this, the concentration remains constant to the 6 inches represented in the graph. Radioactive decay for Cs-137 over one-year reduces the initial concentration of 1 pCi/g to 0.975 pCi/g in the central core of the concrete after one year.

Figure 7 shows that most of the release for Cs-137 comes from within the first ¼ inch of the surface. The frisker data suggest that the concentration is not homogeneous in the first inch of the concrete and that it may decrease by a factor of 10 or more between the surface and one-inch into the concrete. In this case, using the assumption of a homogeneous distribution over the one-inch section will be non-conservative. Assuming that the decrease in concentration is linear it can be shown that the surface concentration can not exceed twice the average concentration. Therefore, the use of a homogeneous distribution may lead to an underestimate by approximately a factor of 2.

Figure 8 presents the diffusion profile for H-3 in a six-foot thick wall. The graph displays the concentration from the surface to the midpoint of the wall at 36 inches. The results are almost identical to those from the one-foot wall (Figure 6).

As shown in Figures 6 and 8, if H-3 contamination is not within the first four or five inches of the surface, it will not contribute to the peak release that occurs in the first year. Therefore, characterization data at deeper depths are not as important in determining

dose. As shown in Figure 7, if Cs-137 contamination does not reside within the first inch, it will not impact the peak release. This is because Cs-137 has the highest diffusion coefficient of all of the contaminants modeled, with the exception of H-3.

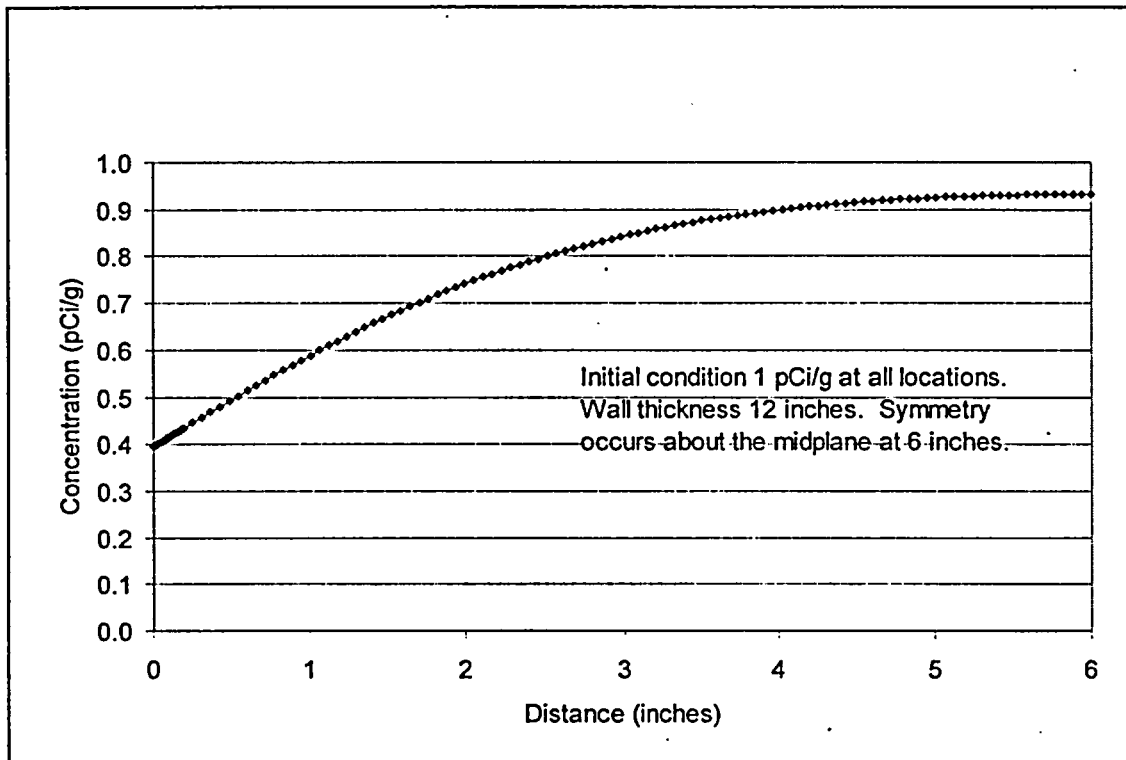


Figure 6 H-3 diffusion profile after one year for a one-foot thick wall with a uniform initial concentration of 1 pCi/g.

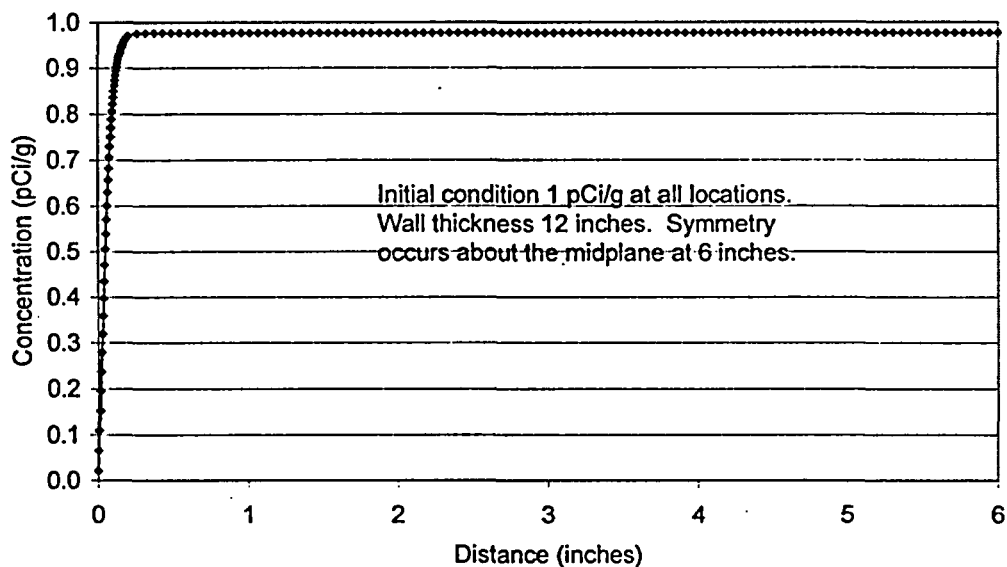


Figure 7 Cs-137 diffusion profile after one year from a one-foot thick wall with a uniform initial concentration of 1 pCi/g.

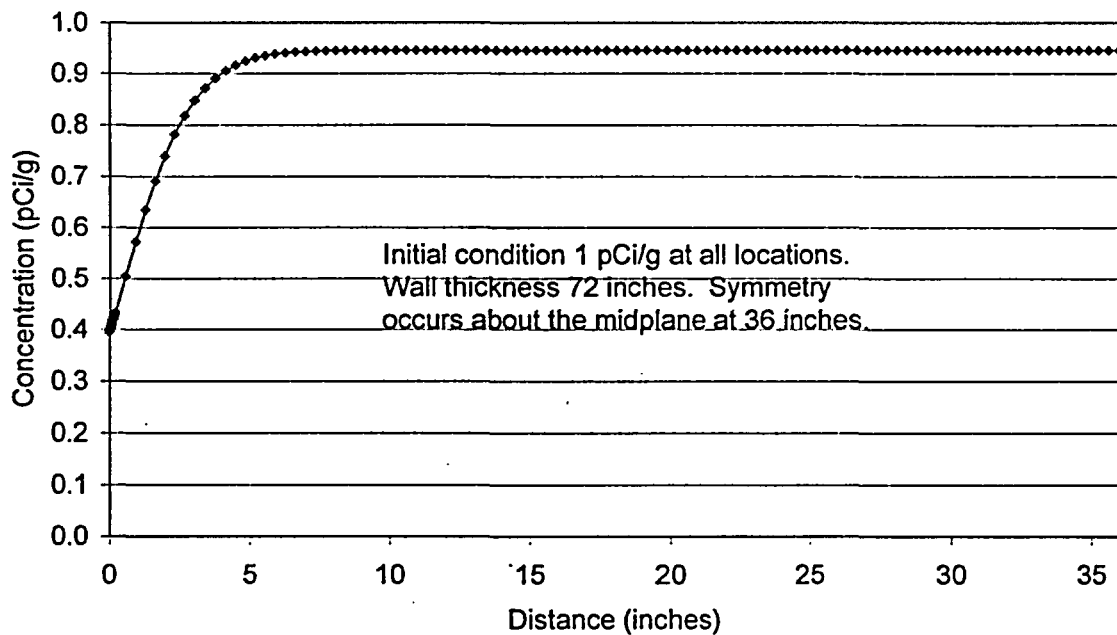


Figure 8 H-3 diffusion profile after one year for a six-foot thick wall with a uniform initial concentration of 1 pCi/g.

The preceding conclusions are based on a uniform distribution of contaminants. If the concentrations within the concrete vary greatly from the assumed distribution, these conclusions may not be valid. If the non-uniform distribution was substantially different from the measured values shown in Figures 1 and 2 (for example, peak concentration in the interior is 10 times the surface concentration) it is conceivable that the peak release could be higher than for the uniform case. However, this is not likely as the data suggest that H-3 diffuses relatively rapidly through concrete and this would tend to smooth out any large differences in concentration.

3.0 Modeling the Source Term For RESRAD

The modeling performed above suggests that the concrete will control release. However, RESRAD assumes that the source is controlled by the sorption properties of the contaminated zone. This conceptual model differences require adjustments to be made in the release rate parameter values to make the calculations in RESRAD match the desired release rates from DUST. In addition, RESRAD assumes that the contaminated zone is above the water table, whereas in this case, it is assumed to be in the water table. This requires adjustment of the parameters used in the soil DCGL analysis (YA, 2004).

3.1 Matching DUST-MS and RESRAD Release Rates

The release model from DUST-MS does not match that found in RESRAD. Therefore, a method to make the DUST-MS predicted release consistent with that of RESRAD is needed. This is accomplished by examining the release equations in RESRAD and choosing a release rate parameter, K_d , that guarantees the desired release rate is used in RESRAD. The following equations describe how this is accomplished. RESRAD assumes that release is controlled by the following equation (Yu, 2001),

$$R(t) = L(t) \times \rho_b \times A \times T \times S(t) \quad (4)$$

Where:

$R(t)$ = the time-dependent release rate (pCi/y)

$L(t)$ = the leach rate (1/y) for the contaminant

ρ_b = the bulk density of the source zone (kg/m³)

A = the area of the contaminated zone (m²)

T = the thickness of the contaminated zone (m)

$S(t)$ = the average concentration of the radionuclide available for leaching (pCi/kg)

The desired leach rate is the value calculated by DUST-MS for each different wall thickness. The RESRAD Leach Rate, $L(t)$, is calculated from the following expression (Yu, 2001),

$$L(t) = I/(\theta \times T \times R_{dcz}) \quad (5)$$

Where:

I = infiltration rate (m/y)
 θ = moisture content in the contaminated zone
 R_{dcz} = retardation coefficient in the contaminated zone (dimensionless)

The moisture content in RESRAD is calculated from the following expression (Yu, 2001).

$$\theta = \eta(I/K_{sat})^{1/(2b+3)} \quad (6)$$

Where:

η = porosity of the contaminated zone (dimensionless)
 I = infiltration rate (m/y)
 K_{sat} = saturated hydraulic conductivity of the contaminated zone (m/y)
 b = empirical 'b' parameter depending on soil type (0.975 from [YA, 2004])

The infiltration rate is calculated as a function of precipitation, irrigation, evapotranspiration coefficient, and run-off from the following (Yu, 2001).

$$I = (1-Ce)((1-Cr)Pr + Ir) \quad (7)$$

Where:

Ce = evapotranspiration coefficient = 0.625 (YA, 2004)
 Cr = run-off coefficient = 0.6 (YA, 2004)
 Pr = annual precipitation = 1.2 m/y (YA, 2004), and
 Ir = irrigation rate = 0.435 m/y (YA, 2004)

Using the above values, the infiltration rate is calculated to be 0.34 m/y.

The retardation coefficient is represented by the equation

$$R_{dcz} = 1 + \rho_b K_d / \theta \quad (8)$$

Where:

K_d = distribution coefficient (m³/kg)

The geometry of the contaminated zone is determined by the dimensions of the subsurface structures. Therefore, the best way to match the release rate from DUST-MS and RESRAD is to adjust the distribution coefficient. Substituting the expressions into the equation for release rate one obtains the following:

$$R(t) = I/(\theta \times T \times R_{dcz}) \times \rho_b \times A \times T(t) \times S(t) \quad (9)$$

Assuming that the thickness of the unsaturated zone does not change and using the expression for R_{dcz} yields

$$R(t) = \{I/(\theta \times (1 + \rho_b K_d/\theta))\} \times \rho_b \times A \times S(t) = I \times \rho_b \times A \times S(t)/(\theta + \rho_b K_d) \quad (10)$$

Solving for K_d yields:

$$K_d = I \times \rho_b \times A \times S(t)/R(t) \rho_b - \theta/\rho_b \quad (11)$$

Using an initial concentration of 1 pCi/g in the contaminated zone, the area of the source zone and the leach rate $R(t)$ calculated from DUST-MS; the appropriate value for the contaminated zone K_d was calculated and used in RESRAD. Calculated contamination zone K_d values are presented after the discussion of RESRAD dose calculations.

3.2 Selection Of Contaminated Zone Geometry For RESRAD

RESRAD treats the source of contamination as a single region. Therefore, for modeling purposes, the different building structures are lumped together in a single source. RESRAD requires three parameters to define the geometry of the contaminated zone: area, thickness, and length parallel to aquifer flow. Previously, in the section that calculates instantaneous release, the geometry was defined for the backfill region within the walls of the subsurface structure. This is not appropriate for defining a source zone composed of the walls and floors of the buildings and therefore, different geometry parameters are calculated for this case.

The most conservative assumption is that all of the facilities are lined up with the longest dimension in the direction of flow. Including the wall thickness and length in Table 2, the distance parallel to flow is 33.1 m (26.7 m + 3.3m + 3.07m). The area of the source zone is calculated as the area of the floors plus the area of the walls in the plane of the floors. This was calculated by adding the wall thickness to the widths of the walls in Table 1 and summing for all facilities. The area obtained using this procedure is 143.5 m². The volume of the contaminated structures is 410 m³ (Table 1). The effective height of the contaminated zone is obtained by dividing the volume of the contaminated structures by the area. This procedure results in an effective height of 2.86 m. These values are slightly different than in Section 2.2.2.5 due to the differences in conceptual models. In Section 2.2.2.5, the effects of sorption were examined and the conservative assumption was that the shortest distance between the source and the receptor well was the sum of the lengths of the buildings parallel to flow. In this section, the more conservative assumption is to use the total length parallel to flow, which includes the thickness of the walls. Due to the selection of the mass balance model in RESRAD, which places all of the released mass into the receptor well, this difference in distance does not significantly impact results.

3.3 Dilution Effects

RESRAD allows a choice between two models for examining dilution effects that occur when the flow from the unsaturated zone enters the saturated zone. The first is the mass balance model and the second is the non-dispersion model. YNPS selected the non-dispersion model when calculating soil derived concentration guideline limits (DCGLs).

The mass balance model is independent of the radionuclide and assumes that the entire source released from the contaminated zone enters the well. Dilution occurs if the amount of water passing through the contaminated zone is less than the well pumping volume. Numerically, the dilution factor, F is expressed as:

$$F = I A / U_w \quad \text{if } I A < U_w \quad (12)$$

$$F = 1 \quad \text{if } I A > U_w \quad (13)$$

Where:

I = the infiltration rate (m/y),

A = area of the contaminated zone perpendicular to infiltration (m²), and

U_w = the well pumping rate (m³/y)

However, when the source is in the saturated zone, the proper values for the dilution expression are the aquifer flow through the source and the area perpendicular to flow.

Using the parameter values used in the soil DCGL analysis, the site-specific infiltration rate was calculated from the input parameters to be 0.34 m/y (Section 4.1) and the area of contaminated structures to be 143.5 m² (Section 4.2). The flow through the facility as calculated by RESRAD is the product of the infiltration rate and cross-sectional area and equals 48.8 m³/y. The pumping rate used in previous analyses (YA, 2004) is 1323 m³/y. Therefore, using Eqn. 12, the RESRAD calculated dilution factor would be 0.037. In contrast, the saturated zone flow rate is 250.6 m/y and the area perpendicular to flow is 12.3 m². Thus, the amount of water flowing through the contaminated zone in the conceptual model used in this analysis is 3085 m³/y, not 48.8 m³/y. Since the actual flow rate (3085 m³/y) exceeds the pumping rate (1323 m³/y), the dilution factor should be set to 1.

If the assumption that the entire inventory is placed uniformly in the water flowing past the contaminated zone in the aquifer is used, the dilution factor calculated by RESRAD needs to be manipulated by proper choice of input parameters. RESRAD calculates the concentration leaving the contaminated zone, C_{cz} , as the release rate divided by the water volume.

$$C_{cz} = R / (I A) \quad (14)$$

Where:

R = the release rate (Ci/y)

The well concentration in the absence of an unsaturated zone is the concentration in the contaminated zone multiplied by the dilution factor.

$$C_w = C_{cz} \times F = \{R/(IA_{cz})\} \times IA_{cz}/U_w = R/U_w \quad (15)$$

To make the well concentration equal to the value that is appropriate for a contaminated zone in the saturated zone, U_w must be set to the volume of water that flows through the contaminated zone, 3085 m³/y. This value is used in the RESRAD simulations for well pumping rate in the concrete analysis.

The dilution factor for the non-dispersion model depends on aquifer flow and geometrical arguments that are not applicable for a source in the saturated zone. Therefore, this model is not recommended for this application. In addition, the RESRAD manual states that the non-dispersion model should not be used for source zones less than 1000 m² due to geometrical assumptions that are not appropriate for a small contamination zone. Thus use of the mass balance method is appropriate.

3.4 Saturated Zone K_d

The source is located in the saturated zone and therefore, further dilution, by accounting for the distribution coefficient, is not warranted. Conceptually, this is equivalent to taking the release inventory and immediately placing it in the well. For the first set of model calculations, a K_d of 0 is used in the contaminated zone.

This is conservative. However, the modeling in the previous section indicates that dilution will not be important for radionuclides (H-3, C-14, and Sr-90) that move relatively fast in the soil and will lead to no more than a factor of 10 decrease in concentration for the other radionuclides in the simulation (Co-60, N-63, and Cs-137). In addition, due to the location of the source zone in the saturated zone and the models in RESRAD, it is difficult to calculate the travel from the source, through clean fill, to the well.

4.0 RESRAD Dose Modeling

Using the release rates calculated by DUST-MS and the above assumptions pertaining to geometry (area and volume), well pump rate, zero K_d in the saturated zone, and distribution coefficient in the contaminated zone, RESRAD was used in the deterministic mode to calculate peak dose.

A few parameter values used in the analysis are different than those used by YNPS in calculating soil DCGLs (YA, 2004). These were changed to fit the conditions being simulated for release controlled by diffusion from concrete in the saturated zone.

In calculating soil DCGLs, the cover thickness is zero. However, in this analysis, the depth to the water table will be at least 2 feet and, because of the assumption that the source is in the aquifer, a cover thickness of 2 feet (0.6 m) is used. In the soil DCGLs,

the depth for root penetration was 1.17 m and the unsaturated zone thickness was 1.82 m. Therefore, the roots did not penetrate the saturated zone. Retaining the root depth value used in the soil DCGL analysis implies the roots penetrate the saturated zone. The root depth value of 1.17 m will be changed to 0.5 m for the analysis. This prevents the non-water pathways from being non-zero, which is appropriate for the conditions being modeled, because most of the contamination will be bound in the concrete and unavailable for release to plants even if the roots were near the concrete.

A second difference between the assumption used in the analyses of the soil DCGLs and the concrete release model is that the water table drop rate is set to zero. In the soil DCGL analysis (YA, 2004), a RESRAD default value of 0.001 m/y was used. The soil DCGL analysis had a 1.8 m unsaturated zone and the results were not sensitive to the water table drop rate. In the current analysis, the unsaturated zone has zero thickness and a non-zero water table drop rate causes a non-zero unsaturated zone thickness to form. This leads to RESRAD calculating transport through the unsaturated zone to reach the aquifer. This effect is not desired because the source is assumed to reside in the saturated zone.

The saturated zone K_d 's were set to zero. This assumption was used to provide an upper bound on well concentrations. The analysis of release and transport presented earlier suggests that sorption does not have a major effect on well concentrations and will cause a decrease of less than a factor of 10 for all radionuclides.

The contaminated zone geometry was changed to fit the conditions for release from subsurface facilities. This permits the use of a soil concentration of 1 pCi/g to be used in the contaminated zone to represent concrete contamination of 1 pCi/g. To obtain predicted dose at other concentrations, the RESRAD results need to be scaled to the actual contamination levels found during characterization work. Contaminated zone parameters are presented in Table 7.

Table 7 Contaminated zone geometry factors and source concentration.

Concentration (pCi/g)	Area (m ²)	Thickness (m)	Length parallel to flow (m)	Volume (m ³)
1	143.5	2.86	33.3	410

Table 8 summarizes all values, other than source term geometry (Table 7) and contaminated zone K_d (Table 9), used in the current analyses that differ from the values used in the soil DCGL analyses (YA, 2004).

Table 8 RESRAD input values changed from soil DCGL calculations

Parameter	Value in this analysis	Value in Soil DCGL analysis (YA, 2004)
Cover thickness	0.6 m	0 m
Well pumping rate	3085 m ³ /y	1383 m ³ /y
K _d	0 for all nuclides	Non-zero for all nuclides
Unsaturated zone thickness	0 m	1.8 m
Contaminated zone density	2.5 g/cm ³	1.51 g/cm ³
Water table drop rate	0 m/y	0.001 m/y
Root depth penetration	0.5 m	1.17 m
Dilution	Mass Balance model	Non-dispersion model

Table 9 summarizes the results for the peak well concentrations predicted by RESRAD and dose using the release rates calculated for diffusion-controlled release, Table 5, and the parameters used in the YNPS analysis for soil DCGLs with the exceptions discussed above. In addition, the contaminated zone K_d values calculated using the procedure described above are presented. The fractional release rates from the diffusion calculations in DUST-MS and those obtained in RESRAD using the K_d value and Eqn. 4 are supplied for comparison. The agreement between the DUST-MS and RESRAD release rates indicates that RESRAD is using the desired source strength for the calculation.

Table 9 Peak well concentration and dose for release for all subsurface structures uniformly contaminated to 1 pCi/g throughout the wall thickness for each radionuclide.

Radionuclide	Peak well concentration (pCi/l) (RESRAD)	Peak Dose (mrem/y) (RESRAD)	Contaminated Zone K _d (cm ³ /g)	DUST-MS Fractional Release Rate (1/y)	RESRAD Fractional Release Rate (1/y)*
H-3	18.6	8.4E-04	0.73	6.29E-02	6.29E-02
C-14	0.1	2.7E-03	159	3.02E-04	3.02E-04
Co-60	0.3	1.4E-02	47	1.02E-03	1.02E-03
Ni-63	1.6	1.5E-03	9.8	4.88E-03	4.88E-03
Sr-90	1.1	1.3E-01	14.1	3.41E-03	3.40E-03
Cs-137	2.5	2.7E-01	6.1	7.82E-03	7.83E-03

* Fractional release rate is equivalent to the RESRAD parameter, Leach Rate, Eqn (4).

The results in Table 9 indicate that if the entire set of walls and floors is contaminated uniformly to 1 pCi/g with each radionuclide. Cesium-137 and Sr-90 are predicted to have the largest dose. Modeling of diffusion-controlled release from the concrete for these radionuclides demonstrated that even if the contamination is limited to the first inch of concrete, the peak release rate does not change.

In the sample SFP-CB-02-01-01 (Darman, 2004) average concentrations were measured for the first inch of concrete. These values, and the projected dose for each radionuclide if all walls and floors were contaminated to the measured levels are shown in Table 10. The projected dose for each nuclide (column 3 of Table 10) was obtained by multiplying the dose for contamination at 1 pCi/g (column 3 in Table 9) by the corresponding measured concentration.

Table 10 Measured concentrations in the first inch of the concrete and projected dose for contamination in the first inch at each surface and no contamination in the interior of the walls.

Radionuclide	Measured Concentration (pCi/g)	Projected Dose (mrem/y)
H-3	49.9	4.2E-02
C-14	2.32	6.3E-03
Co-60	48.1	6.7E-01
Ni-63	435	6.5E-01
Sr-90	0.91	1.2E-01
Cs-137	1075	2.9E+02

With the measured contamination levels, Cs-137 dominates the projected dose. All other doses are less than 1 mrem/y at the measured concentration levels.

The H-3 dose presented in Table 10 may not be conservative as the measured concentration data show an increase up to six inches into the concrete. The peak value at 6 inches is less than a factor of 2 higher than the value in Table 9. To account for the difference between the surface and peak concentration, the projected dose is increased by a factor of 2. The resulting dose is less than 0.1 mrem/y and therefore, at these levels, H-3 is not of great concern.

5.0 Conclusion

Release of residual radioactive contaminants (i.e., H-3, C-14, Co-60, Ni-63, Sr-90, and Cs-137) from subsurface concrete structures at the YNPS and the associated annual doses have been evaluated. There are five different structures that may remain at license termination, and all may have concrete containing residual radioactivity. Most of the concrete walls and floors that may remain are below the water table. Thus, for these analyses it is assumed that the entire facility is below the water table. Analyses were performed to assess the rate controlling release mechanism in the groundwater pathway. Two mechanisms were considered, diffusive release from the concrete and sorption onto backfill and soil that surrounds the facilities. Diffusive release was found to be the rate-limiting step for all six radionuclides in the analysis. Further analyses were performed to determine the impact of the contaminant distribution in the walls on release rate. The analyses showed that for every radionuclide except H-3, the peak release rate was impacted only by the concentration within the first inch of the wall. Therefore, the impact of having a non-homogeneous concentration distribution is minimal. Tritium, which has a higher concrete diffusion coefficient than the other radionuclides, has release

rates that were influenced by concentrations within the first few inches of the wall. Based on a concentration of 1 pCi/g and a concrete density of 2.5 g/cm³, the total release to the subsurface was estimated for each radionuclide. Values of RESRAD input parameters were selected to match the release rate calculated by DUST-MS. RESRAD then calculated the water pathway dose using the same assumptions used in the soil DCGL calculations performed for YNPS. The dose results for 1 pCi/g showed that Cs-137 and Sr-90 had the highest doses. Using measured data of existing contaminant concentrations in the first inch of concrete, estimates of the dose were made. Cs-137 dominated the dose and had a predicted dose greater than 200 mrem/y. All other radionuclides had a predicted dose of less than 1 mrem/y. These actual measured results clearly indicate the need to remediate the radioactivity to meet the site release criteria.

In a more general manner, the results of this analysis will be used with specific criteria to support the license termination process. This criterion will use the dose factors from this analysis to calculate concrete volumetric DCGLs that are equivalent to 0.5 mrem per year. These DCGLs will be used to support remediation decisions for all subsurface volumetrically contaminated concrete at the site through characterization sampling. If these subsurface structures are shown to exceed these DCGLs then remediation will be performed. The remediation activities could range from selective removal of the contamination or removal of the entire subsurface structure. The use of the 0.5 mrem DCGLs will also require that the soil DCGLs be reduced to be equivalent to 24.5 mrem for the final status surveys of the land areas. This will ensure that the dose from all pathways is within the NRC's site release criteria from 10CFR20 Subpart E.

For diffusion-controlled release, the peak release rate is expected in the first year of the analysis. Examinations of the H-3 diffusion profile after one year suggest that only contamination within the first five inches will impact release. This was true for both the 1 and 6 foot wall thicknesses that were simulated. Evaluations were performed for Cs-137 as well. Cs-137 had the second highest diffusion coefficient in the simulations and can be used as a surrogate for the other radionuclides, except H-3. The Cs-137 diffusion profile at 1 year showed that only contamination within the first half-inch of wall thickness will impact peak release. This suggests that characterization data should focus on the first inch for all radionuclides except H-3 and should focus on the first five inches for H-3. Outside of this region, confirmatory data should be collected to determine if the uniform concentration assumption used in these analyses is appropriate.

Appendix A
Yankee Rowe Reference Drawings for Facility Component Dimensions

Table A1: Yankee Rowe Reference Drawings for Facility Component Dimensions

Structure	Component	Below-Grade* Dimensions (feet)		
		Component height	Component width	Component thickness
Primary Auxiliary Building (drain collection tank cubicle) References for dimensions: Height: Yankee Drawing No. 9699-FM-57A Width: Yankee Drawing Nos. 9699-FC-40D & 9699-RC-40A Thickness: Yankee Drawing No. 9699-FC-40F	floor			2.50
	wall 1	18.50	12.50	1.00
	wall 2	18.50	12.50	1.00
	wall 3	18.50	15.50	1.00
	wall 4	18.50	15.50	1.75
PAB (gravity drain tank cubicle) References for dimensions: Height: Yankee Drawing No. 9699-FM-57A Width: Yankee Drawing Nos. 9699-FC-40D & 9699-RC-40A Thickness: Yankee Drawing No. 9699-FC-40F	floor			2.50
	wall 1	18.50	10.17	1.00
	wall 2	18.50	10.17	1.00
	wall 3	18.50	15.50	1.00
	wall 4	18.50	15.50	1.00
Spent Fuel Pool References for dimensions: Height: Yankee Drawing No. 9699-FC-45B Width: Yankee Drawing No. 9699-FM-21A Thickness: Yankee Drawing No. 9699-FC-95C	floor			3.00
	wall 1	14.67	16.50	6.00
	wall 2	14.67	16.50	6.00
	wall 3	14.67	33.67	6.00
	wall 4	14.67	33.67	6.00
WDB Cubicle Reference for all dimensions: Yankee Drawing No. 9699-FC-50C	floor			1.17
	wall 1	9.83	9.00	1.00
	wall 2	9.83	9.00	1.00
	wall 3	9.83	14.00	1.00
	wall 4	9.83	14.00	1.00
Elevator Pit Reference for all dimensions: Yankee Drawing No. 9699-FC-43C	floor			1.00
	wall 1	6.50	7.83	1.00
	wall 2	6.50	7.83	1.00
	wall 3	6.50	9.00	1.08
	wall 4	6.50	9.00	1.08

Appendix B

Release Rates for Each Wall and Floor Section Calculated Using the DUST-MS Code

**Table B1: DUST-MS Predicted diffusion-controlled release of H-3
($D=5.5 \times 10^{-7} \text{ cm}^2/\text{s}$) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	H-3 Fractional Release	H-3 Release (Ci/y)*
PAB	floor			2.50	6.98E-02	2.39E-06
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	1.74E-01	2.85E-06
	wall 2	18.50	12.50	1.00	1.74E-01	2.85E-06
	wall 3	18.50	15.50	1.00	1.74E-01	3.53E-06
	wall 4	18.50	15.50	1.75	9.92E-02	3.52E-06
PAB	floor			2.50	6.98E-02	1.95E-06
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	1.74E-01	2.32E-06
	wall 2	18.50	10.17	1.00	1.74E-01	2.32E-06
	wall 3	18.50	15.50	1.00	1.74E-01	3.53E-06
	wall 4	18.50	15.50	1.00	1.74E-01	3.53E-06
SFP	floor			3.00	5.80E-02	6.84E-06
	wall 1	14.67	16.50	6.00	2.90E-02	2.99E-06
	wall 2	14.67	16.50	6.00	2.90E-02	2.99E-06
	wall 3	14.67	33.67	6.00	2.90E-02	6.09E-06
	wall 4	14.67	33.67	6.00	2.90E-02	6.09E-06
WDB Cubicle	floor			1.17	1.49E-01	1.55E-06
	wall 1	9.83	9.00	1.00	1.74E-01	1.09E-06
	wall 2	9.83	9.00	1.00	1.74E-01	1.09E-06
	wall 3	9.83	14.00	1.00	1.74E-01	1.69E-06
	wall 4	9.83	14.00	1.00	1.74E-01	1.69E-06
Elevator Pit	floor			1.00	1.74E-01	8.68E-07
	wall 1	6.50	7.83	1.00	1.74E-01	6.27E-07
	wall 2	6.50	7.83	1.00	1.74E-01	6.27E-07
	wall 3	6.50	9.00	1.08	1.61E-01	7.21E-07
	wall 4	6.50	9.00	1.08	1.61E-01	7.21E-07
				Average**/Totals	6.29E-02	6.45E-05

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.

**Table B2: DUST-MS Predicted diffusion-controlled release of Cs-137
($D=3.0 \times 10^{-9} \text{ cm}^2/\text{s}$) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	Cs-137 Fractional Release	Cs-137 Release (Ci/y)*
PAB	floor			2.50	8.68E-03	2.97E-07
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	2.15E-02	3.53E-07
	wall 2	18.50	12.50	1.00	2.15E-02	3.53E-07
	wall 3	18.50	15.50	1.00	2.15E-02	4.37E-07
	wall 4	18.50	15.50	1.75	1.23E-02	4.37E-07
PAB	floor			2.50	8.68E-03	2.42E-07
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	2.15E-02	2.87E-07
	wall 2	18.50	10.17	1.00	2.15E-02	2.87E-07
	wall 3	18.50	15.50	1.00	2.15E-02	4.37E-07
	wall 4	18.50	15.50	1.00	2.15E-02	4.37E-07
SFP	floor			3.00	7.22E-03	8.52E-07
	wall 1	14.67	16.50	6.00	3.63E-03	3.73E-07
	wall 2	14.67	16.50	6.00	3.63E-03	3.73E-07
	wall 3	14.67	33.67	6.00	3.63E-03	7.62E-07
	wall 4	14.67	33.67	6.00	3.63E-03	7.62E-07
WDB cubicle	floor			1.17	1.84E-02	1.92E-07
	wall 1	9.83	9.00	1.00	2.15E-02	1.35E-07
	wall 2	9.83	9.00	1.00	2.15E-02	1.35E-07
	wall 3	9.83	14.00	1.00	2.15E-02	2.10E-07
	wall 4	9.83	14.00	1.00	2.15E-02	2.10E-07
Elevator Pit	floor			1.00	2.15E-02	1.07E-07
	wall 1	6.50	7.83	1.00	2.15E-02	7.76E-08
	wall 2	6.50	7.83	1.00	2.15E-02	7.76E-08
	wall 3	6.50	9.00	1.08	2.00E-02	8.93E-08
	wall 4	6.50	9.00	1.08	2.00E-02	8.93E-08
				Average**/Totals	7.82E-03	8.02E-06

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.

**Table B3: DUST-MS Predicted diffusion-controlled release of Co-60
(D=4.0 10⁻¹¹ cm²/s) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	Co-60 Fractional Release	Co-60 Release (Ci/y)*
PAB	floor			2.50	1.13E-03	3.88E-08
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	2.82E-03	4.62E-08
	wall 2	18.50	12.50	1.00	2.82E-03	4.62E-08
	wall 3	18.50	15.50	1.00	2.82E-03	5.73E-08
	wall 4	18.50	15.50	1.75	1.61E-03	5.72E-08
PAB	floor			2.50	1.13E-03	3.16E-08
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	2.82E-03	3.76E-08
	wall 2	18.50	10.17	1.00	2.82E-03	3.76E-08
	wall 3	18.50	15.50	1.00	2.82E-03	5.73E-08
	wall 4	18.50	15.50	1.00	2.82E-03	5.73E-08
SFP	floor			3.00	9.41E-04	1.11E-07
	wall 1	14.67	16.50	6.00	4.70E-04	4.84E-08
	wall 2	14.67	16.50	6.00	4.70E-04	4.84E-08
	wall 3	14.67	33.67	6.00	4.70E-04	9.87E-08
	wall 4	14.67	33.67	6.00	4.70E-04	9.87E-08
WDB Cubicle	floor			1.17	2.41E-03	2.52E-08
	wall 1	9.83	9.00	1.00	2.82E-03	1.77E-08
	wall 2	9.83	9.00	1.00	2.82E-03	1.77E-08
	wall 3	9.83	14.00	1.00	2.82E-03	2.75E-08
	wall 4	9.83	14.00	1.00	2.82E-03	2.75E-08
Elevator Pit	floor			1.00	2.82E-03	1.41E-08
	wall 1	6.50	7.83	1.00	2.82E-03	1.02E-08
	wall 2	6.50	7.83	1.00	2.82E-03	1.02E-08
	wall 3	6.50	9.00	1.08	2.61E-03	1.17E-08
	wall 4	6.50	9.00	1.08	2.61E-03	1.17E-08
				Average**/Totals	1.02E-03	1.05E-06

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.

**Table B4: DUST-MS Predicted diffusion-controlled release of C-14
(D=1.0 10 12 cm²/s) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	C-14 Fractional Release	C-14 Release (Ci/y)
PAB	floor			2.50	3.35E-04	1.15E-08
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	8.36E-04	1.37E-08
	wall 2	18.50	12.50	1.00	8.36E-04	1.37E-08
	wall 3	18.50	15.50	1.00	8.36E-04	1.70E-08
	wall 4	18.50	15.50	1.75	4.77E-04	1.69E-08
PAB	floor			2.50	3.35E-04	9.35E-09
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	8.36E-04	1.11E-08
	wall 2	18.50	10.17	1.00	8.36E-04	1.11E-08
	wall 3	18.50	15.50	1.00	8.36E-04	1.70E-08
	wall 4	18.50	15.50	1.00	8.36E-04	1.70E-08
SFP	floor			3.00	2.79E-04	3.29E-08
	wall 1	14.67	16.50	6.00	1.39E-04	1.43E-08
	wall 2	14.67	16.50	6.00	1.39E-04	1.43E-08
	wall 3	14.67	33.67	6.00	1.39E-04	2.92E-08
	wall 4	14.67	33.67	6.00	1.39E-04	2.92E-08
WDB Cubicle	floor			1.17	7.14E-04	7.45E-09
	wall 1	9.83	9.00	1.00	8.36E-04	5.24E-09
	wall 2	9.83	9.00	1.00	8.36E-04	5.24E-09
	wall 3	9.83	14.00	1.00	8.36E-04	8.14E-09
	wall 4	9.83	14.00	1.00	8.36E-04	8.14E-09
Elevator Pit	floor			1.00	8.36E-04	4.17E-09
	wall 1	6.50	7.83	1.00	8.36E-04	3.01E-09
	wall 2	6.50	7.83	1.00	8.36E-04	3.01E-09
	wall 3	6.50	9.00	1.08	7.74E-04	3.46E-09
	wall 4	6.50	9.00	1.08	7.74E-04	3.46E-09
				Average**/Totals	3.02E-04	3.10E-07

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.

**Table B5: DUST-MS Predicted diffusion-controlled release of Sr-90
(D=5.2 10 10 cm²/s) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	Sr- 90 Fractional Release	Sr-90 Release (Ci/y)*
PAB	floor			2.50	3.78E-03	1.30E-07
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	9.42E-03	1.54E-07
	wall 2	18.50	12.50	1.00	9.42E-03	1.54E-07
	wall 3	18.50	15.50	1.00	9.42E-03	1.91E-07
	wall 4	18.50	15.50	1.75	5.38E-03	1.91E-07
PAB	floor			2.50	3.78E-03	1.05E-07
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	9.42E-03	1.25E-07
	wall 2	18.50	10.17	1.00	9.42E-03	1.25E-07
	wall 3	18.50	15.50	1.00	9.42E-03	1.91E-07
	wall 4	18.50	15.50	1.00	9.42E-03	1.91E-07
SFP	floor			3.00	3.14E-03	3.70E-07
	wall 1	14.67	16.50	6.00	1.57E-03	1.61E-07
	wall 2	14.67	16.50	6.00	1.57E-03	1.61E-07
	wall 3	14.67	33.67	6.00	1.57E-03	3.29E-07
	wall 4	14.67	33.67	6.00	1.57E-03	3.29E-07
WDB Cubicle	floor			1.17	8.06E-03	8.41E-08
	wall 1	9.83	9.00	1.00	9.42E-03	5.90E-08
	wall 2	9.83	9.00	1.00	9.42E-03	5.90E-08
	wall 3	9.83	14.00	1.00	9.42E-03	9.18E-08
	wall 4	9.83	14.00	1.00	9.42E-03	9.18E-08
Elevator Pit	floor			1.00	9.42E-03	4.70E-08
	wall 1	6.50	7.83	1.00	9.42E-03	3.39E-08
	wall 2	6.50	7.83	1.00	9.42E-03	3.39E-08
	wall 3	6.50	9.00	1.08	8.73E-03	3.90E-08
	wall 4	6.50	9.00	1.08	8.73E-03	3.90E-08
				Average**/Totals	3.41E-03	3.49E-06

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.

**Table B6: DUST-MS Predicted diffusion-controlled release of Ni-63
($D=1.1 \times 10^{-9} \text{ cm}^2/\text{s}$) from concrete uniformly contaminated to 1 pCi/g**

Structure	Component	Component height (ft)	Component width (ft)	Component thickness (ft)	Ni-63 Fractional Release	Ni-63 Release (Ci/y)*
PAB	floor			2.50	5.42E-03	1.86E-07
(drain collection tank cubicle)	wall 1	18.50	12.50	1.00	1.35E-02	2.21E-07
	wall 2	18.50	12.50	1.00	1.35E-02	2.21E-07
	wall 3	18.50	15.50	1.00	1.35E-02	2.74E-07
	wall 4	18.50	15.50	1.75	7.70E-03	2.74E-07
PAB	floor			2.50	5.42E-03	1.51E-07
(gravity drain tank cubicle)	wall 1	18.50	10.17	1.00	1.35E-02	1.80E-07
	wall 2	18.50	10.17	1.00	1.35E-02	1.80E-07
	wall 3	18.50	15.50	1.00	1.35E-02	2.74E-07
	wall 4	18.50	15.50	1.00	1.35E-02	2.74E-07
SFP	floor			3.00	4.50E-03	5.31E-07
	wall 1	14.67	16.50	6.00	2.25E-03	2.31E-07
	wall 2	14.67	16.50	6.00	2.25E-03	2.31E-07
	wall 3	14.67	33.67	6.00	2.25E-03	4.72E-07
	wall 4	14.67	33.67	6.00	2.25E-03	4.72E-07
WDB Cubicle	floor			1.17	1.15E-02	1.20E-07
	wall 1	9.83	9.00	1.00	1.35E-02	8.46E-08
	wall 2	9.83	9.00	1.00	1.35E-02	8.46E-08
	wall 3	9.83	14.00	1.00	1.35E-02	1.32E-07
	wall 4	9.83	14.00	1.00	1.35E-02	1.32E-07
Elevator Pit	floor			1.00	1.35E-02	6.73E-08
	wall 1	6.50	7.83	1.00	1.35E-02	4.86E-08
	wall 2	6.50	7.83	1.00	1.35E-02	4.86E-08
	wall 3	6.50	9.00	1.08	1.25E-02	5.60E-08
	wall 4	6.50	9.00	1.08	1.25E-02	5.60E-08
				Average**/Totals	4.88E-03	5.00E-06

* Total Inventory for uniform contamination at 1 pCi/g is 1.02E-03 Ci.

** The last row contains the average fractional release rate (Ci/y) and the total release rate (Ci) in the first year, the year of peak release. The total release is the sum of all preceding values in the column. The average release rate is the total release rate divided by the total inventory.