

308 D199702060001  
PA Research Task 2  
Scientific Notebook #077

ADAPTIVE MESH REFINEMENT

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**CNWRA  
CONTROLLED  
COPY 077**



Gordon Willmeyer

PA - Research Task #2

5/6/93

1

Numerical experiments with the code ADAVAR<sup>+</sup>, a test-bed for adaptive mesh refinement strategies.

Test can be used here in the COVE-2A exercise (SAND89-2558) for 1D unsaturated flow in fractured porous media similar to Yucca Mtn.

GW

Table 1: Material Properties <sup>\*</sup>

	TCw	PTn	TSw1	TSw2-3	CHnv	CHnz
$n_m$ <sup><math>\times \theta_s</math></sup>	0.08	0.40	0.11	0.11	0.46	0.28
$K_m$ (m/s)	$9.7 \times 10^{-12}$	$3.9 \times 10^{-7}$	$1.9 \times 10^{-11}$	$1.9 \times 10^{-11}$	$2.7 \times 10^{-7}$	$2.0 \times 10^{-11}$
$S_{r,m}$	0.002	0.100	0.080	0.080	0.041	0.110
$\alpha_m$ (1/m)	$0.821 \times 10^{-2}$	$1.5 \times 10^{-2}$	$0.567 \times 10^{-2}$	$0.567 \times 10^{-2}$	$1.600 \times 10^{-2}$	$0.308 \times 10^{-2}$
$\beta_m$	1.558	6.872	1.798	1.798	3.872	1.602
$n_f$	$1.4 \times 10^{-4}$	$2.7 \times 10^{-5}$	$4.1 \times 10^{-5}$	$1.8 \times 10^{-4}$	$4.6 \times 10^{-5}$	$4.6 \times 10^{-5}$
$K_f$ (m/s)	$5.3 \times 10^{-9}$	$1.6 \times 10^{-8}$	$0.9 \times 10^{-9}$	$3.1 \times 10^{-9}$	$9.2 \times 10^{-9}$	$9.2 \times 10^{-9}$
$S_{r,f}$	0.0395	0.0395	0.0395	0.0395	0.0395	0.0395
$\alpha_f$ (1/m)	1.285	1.285	1.285	1.285	1.285	1.285
$\beta_f$	4.23	4.23	4.23	4.23	4.23	4.23
$\alpha'_{bulk}$ (1/m)	$6.2 \times 10^{-7}$	$8.2 \times 10^{-6}$	$1.2 \times 10^{-6}$	$5.8 \times 10^{-7}$	$3.9 \times 10^{-6}$	$2.6 \times 10^{-6}$
$\frac{\partial n_f}{\partial \sigma'}$ (1/m)	$1.32 \times 10^{-6}$	$1.9 \times 10^{-7}$	$5.6 \times 10^{-8}$	$1.2 \times 10^{-7}$	$2.8 \times 10^{-8}$	$2.8 \times 10^{-8}$

from Sandia N

<sup>\*</sup> from (SAND88-0942), <sup>+</sup> Not controlled, this is a development platform

The test case used here considers flow in matrix only.

Input data file for ADAVAR:

Material Props.  
for Layer 1-5

Top & Bottom  
Elev. of Layer  
1-5

```

2 0 0 2 1 1 1
1.000d+00 1.000d+00 1.440d-02 1.100d+00 1.001d+13
5.000d-06 20 40 1 1 1.000d+12 0 1
1.001d+13
0.000d+00 1.000d+13
1.001d+13
530.4d+0 5 1.5d+1
8.210d-03 8.000d-02 1.600d-04 1.558d+00 1.000d-07 9.700d-12
1.500d-02 4.000d-01 4.000d-02 6.872d+00 1.000d-07 3.900d-07
5.670d-03 1.100d-01 8.800d-03 1.798d+00 1.000d-07 1.900d-11
5.670d-03 1.100d-01 8.800d-03 1.798d+00 1.000d-07 1.900d-11
1.600d-02 4.600d-01 1.886d-02 3.872d+00 1.000d-07 2.700d-07
530.4d+0 503.6d+0 25
503.6d+0 465.5d+0 25
465.5d+0 335.4d+0 25
335.4d+0 130.3d+0 25
130.3d+0 0.0d+0 25
-1.000d+02
2 1
-3.170d-12 -3.170d-12
0.000d+00 0.000d+00
    
```

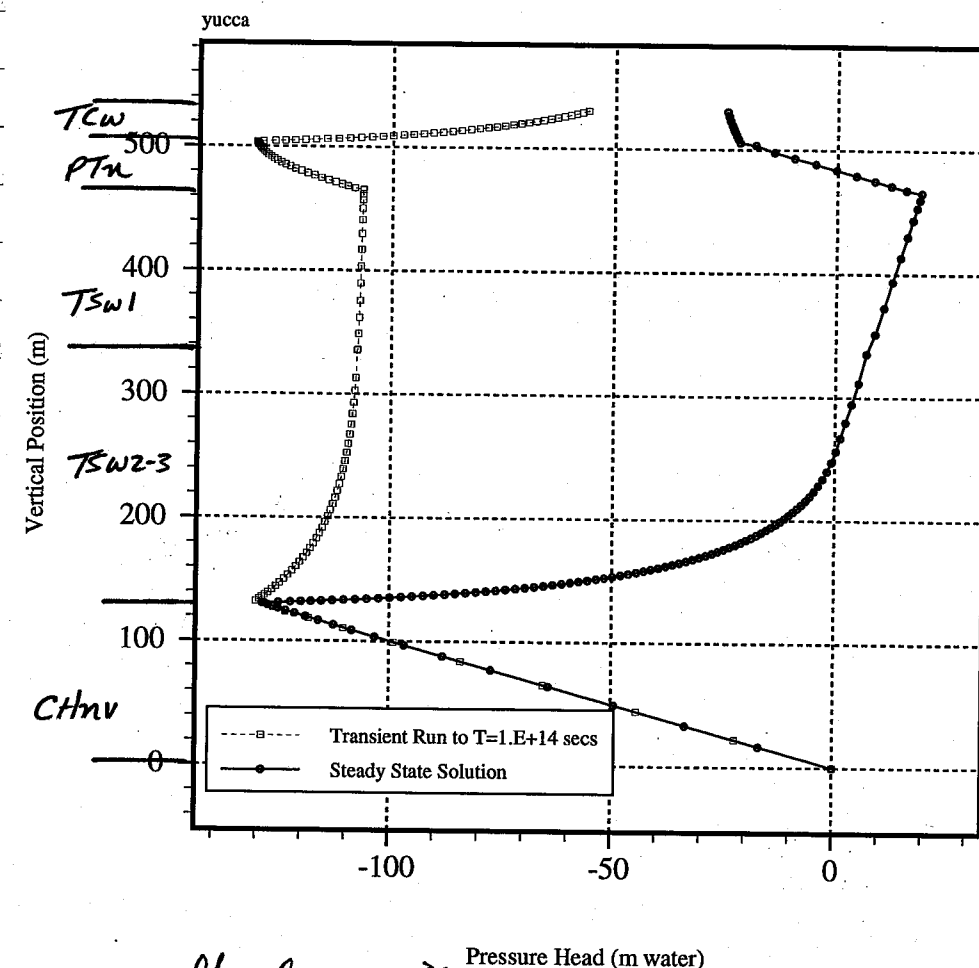
$\rightarrow$  1  $\Rightarrow$  SS  
 $\rightarrow$  0  $\Rightarrow$  Transient  
 $\rightarrow$  0  $\Rightarrow$  Redist for SS  
 $\rightarrow$  0  $\Rightarrow$  Non-adapt. for TR  
 $\rightarrow$  1  $\Rightarrow$  refine for TR  
 $\rightarrow$  2  $\Rightarrow$  redit. for TR

$\rightarrow$  These are  
 $S_r$  not  $\theta_r$  !!

$\rightarrow$  infiltration rate at  
 top = .1 mm/yr

Gordon Wittmeyer

Results for steady-state run and transient run to steady state



Gordon Wittmeyer

Steady solver uses SOR with overrelaxation  $\omega = 1.5$  and a residual tolerance of  $1e-6$ .  
 Allow up to 150 Picard iterations per grid and up to 30 grid adaptations.  
 Transient solver uses Thomas algorithm for solver; allow up to 20 Picard iterations before time step is reduced by half.  
 Time step is allowed to grow by factor of 1.1 if convergence is achieved in less than 10 Picard iterations for transient case.

Gordon Withmeyer

5/7/93

Verification of ADAVAR by code benchmarking

grid  
 The fixed  $\omega$  option for ADAVAR has been compared to several other unstructured flow codes to ensure that the basic physics are correctly modelled. I have chosen a simple 1D vertical infiltration problem described by Celia et al.

WRR 26(7), July 1990

Problem domain: 1D Vertical column  
 100 cm in length. Soil properties given by van Genuchten model with

$$\theta_s = .368 \quad \theta_r = .102 \quad \alpha = .00335 \text{ 1/cm}$$

$$n = 2.0 \quad K_s = 9.22 \times 10^{-3} \text{ cm/s} \quad S_s = 1.0 \times 10^{-7}$$

$$\psi(z, 0) = -1000 \text{ cm}$$

$$\psi(z_{\text{top}}, t) = -75 \text{ cm}$$

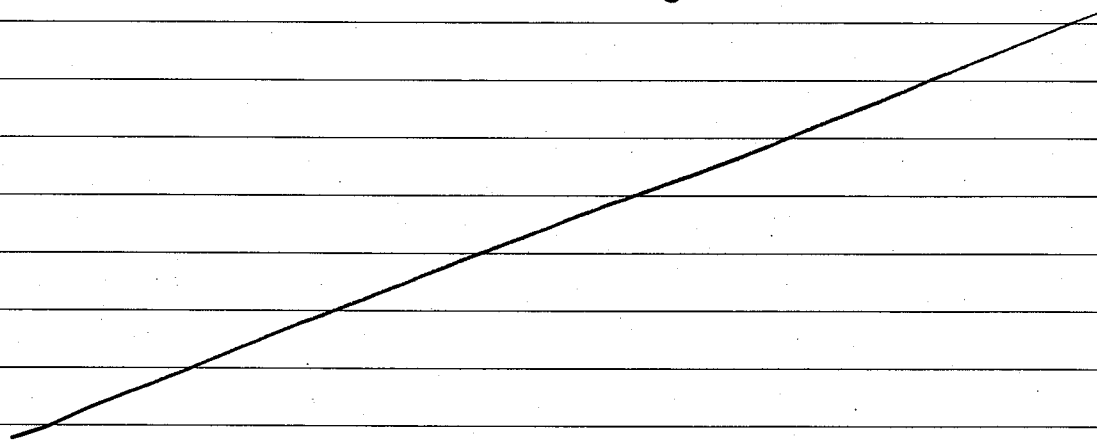
$$\psi(z_{\text{bot}}, t) = -1000 \text{ cm}$$

Nominal Problem

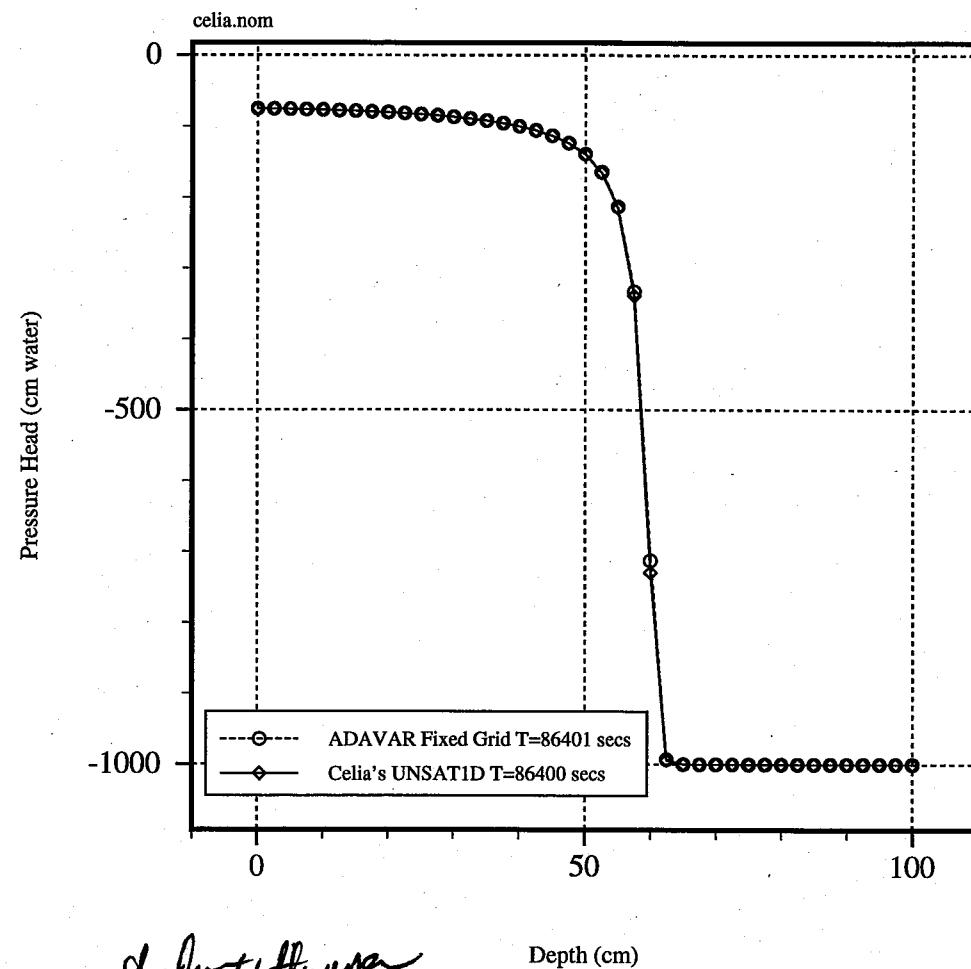
$$\Delta z = 2.5 \text{ cm} \quad \Delta t = 144 \text{ sec}$$

$$T_{\text{final}} = 86401 \text{ seconds} \approx 1 \text{ Day (+1 sec)}$$

Results compared at 1 Day



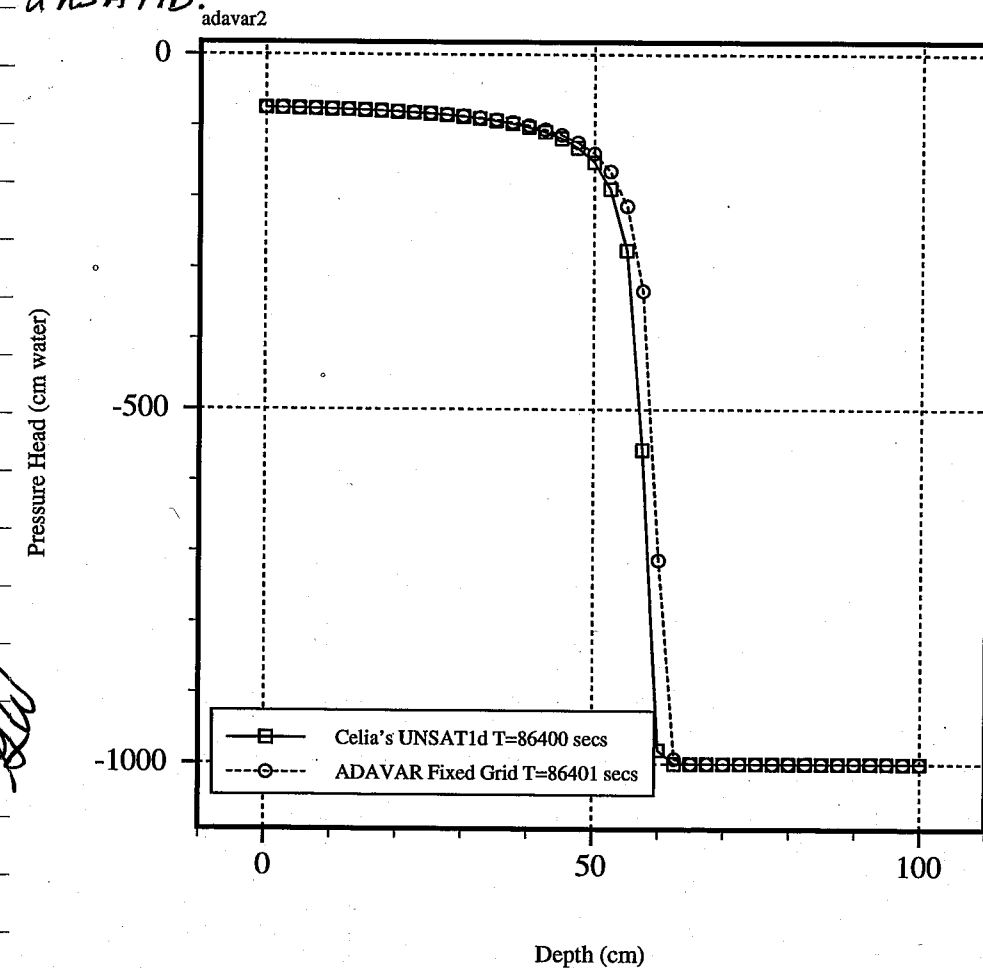
The solutions here are nearly indistinguishable.



John W. Dwyer

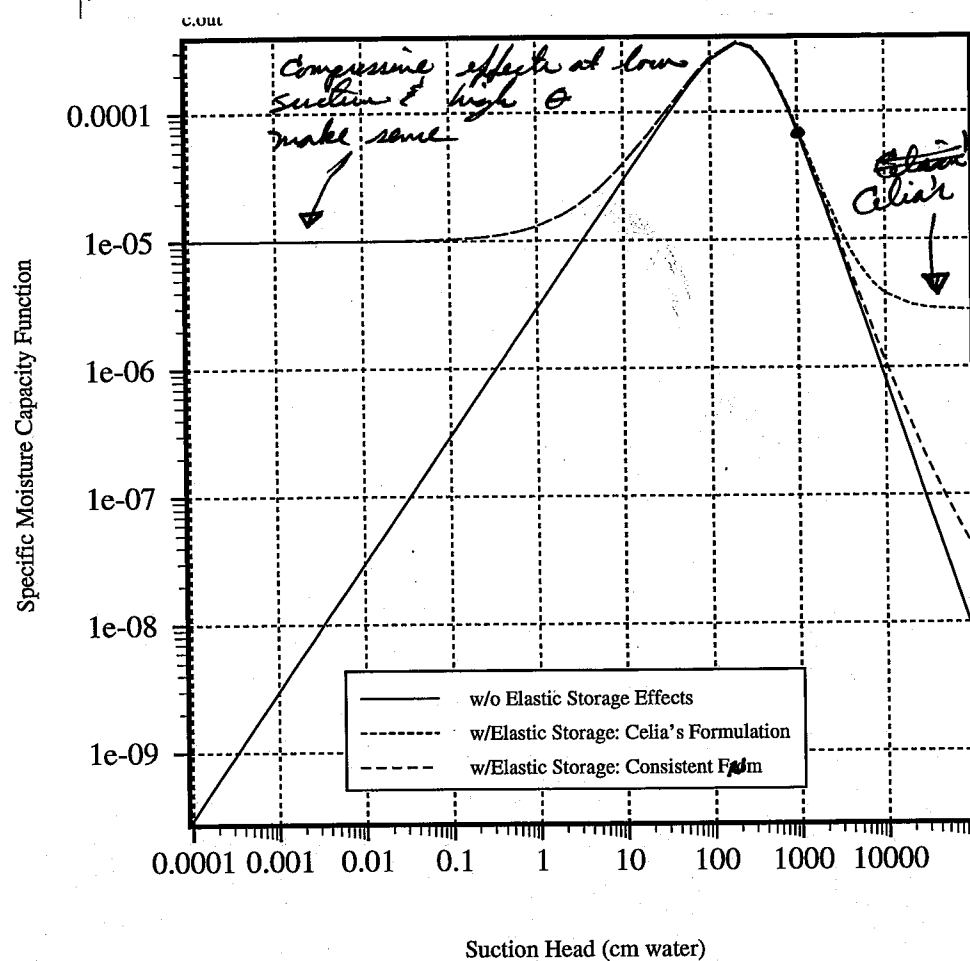
Increasing storage decreases diffusivity which decreases the rate at which the front advances

For the case where the elastic storage is increased from  $1.0 \times 10^{-7}$  to  $1.0 \times 10^{-5}$  difference in the solutions for ADAVAR and Celia's UNSAT1D code become apparent. In the following plot the <sup>increase</sup> decrease in  $S_s$  causes the front ~~to~~ predicted by UNSAT1D to be retarded relative to ADAVAR. It appears that this is the result of inconsistent implementation of the storage term in UNSAT1D!



Celia's formulation:  $S(\psi) = (S_s \frac{\theta}{\theta_s} + \frac{\partial \theta}{\partial \psi})$   
 Note that at  $\theta_{min} = \theta_r$ ,  $S_s \frac{\theta}{\theta_s}$  can make a very large contribution to  $S(\psi)$  at very high suction.

My formulation  $S(\psi) = (S_s \frac{\theta - \theta_r}{\theta_s - \theta_r} + \frac{\partial \theta}{\partial \psi})$ , residual or unextractable moisture should not be included in compressive media effects. This is consistent or at least more so.



This does not really appear to explain the difference between ADAVAR and UNSATRO after all. Note that at  $\psi = -1000$  cm, the storage term is not affected by the method used to account for compressive effects. Note again that  $\psi = -1000$  is the lowest pressure (highest suction) attained in the Celia test problem.

(Lumped Mass too!)

Celia's Modified Picard Formulation

( $\delta$ -formulation;  $\delta_i^m = h_i^{n+1,m+1} - h_i^{n+1,m}$ )

For node  $i$ :

$$\begin{aligned} & (C_i + S_s \frac{\theta_i^{n+1,m}}{\theta_s}) \frac{\delta_i^m}{\Delta t} - \frac{1}{(\Delta z)^2} \left[ K_{i+1/2}^{n+1,m} (\delta_{i+1}^m - \delta_i^m) \right. \\ & \left. - K_{i-1/2}^{n+1,m} (\delta_i^m - \delta_{i-1}^m) \right] = \frac{1}{(\Delta z)^2} \left[ K_{i+1/2}^{n+1,m} (h_{i+1}^{n+1,m} - h_i^{n+1,m}) \right. \\ & \left. - K_{i-1/2}^{n+1,m} (h_i^{n+1,m} - h_{i-1}^{n+1,m}) \right] + \frac{K_{i+1/2}^{n+1,m} - K_{i-1/2}^{n+1,m}}{\Delta z} \\ & - \left( \frac{\theta_i^{n+1,m} - \theta_i^n}{\Delta t} \right) - S_s \frac{\theta_i^{n+1,m}}{\theta_s} \left( \frac{h_i^{n+1,m} - h_i^n}{\Delta t} \right) \end{aligned}$$

$n$  - time level ;  $m$  - iterate level

Convert to  $h$  or  $\psi$  based form

$$\begin{aligned}
 & \left( C_i^{n+1,m} + S_s \frac{\theta_i^{n+1,m}}{\theta_s} \right) \frac{h_i^{n+1,m+1} - h_i^{n+1,m}}{\Delta t} \\
 & \text{note the sign!!} \quad - \frac{1}{(\Delta z)^2} \left[ K_{i+1/2} (h_{i+1}^{n+1,m} - h_i^{n+1,m}) \right. \\
 & \quad \left. - (K_{i+1/2} + K_{i-1/2}) (h_i^{n+1,m} - h_{i-1}^{n+1,m}) \right. \\
 & \quad \left. + K_{i-1/2} (h_{i-1}^{n+1,m} - h_i^{n+1,m}) \right] = \\
 & \quad \frac{1}{(\Delta z)^2} \left[ K_{i+1/2} h_{i+1}^{n+1,m} - (K_{i+1/2} + K_{i-1/2}) h_i^{n+1,m} \right. \\
 & \quad \left. + K_{i-1/2} h_{i-1}^{n+1,m} \right] + \frac{K_{i+1/2} - K_{i-1/2}}{\Delta z} \\
 & \quad - \left( \frac{\theta_i^{n+1,m} - \theta_i^n}{\Delta t} \right) + S_s \frac{\theta_i^{n+1,m}}{\theta_s} \frac{h_i^{n+1,m} - h_i^n}{\Delta t}
 \end{aligned}$$

$$\begin{aligned}
 & \left( C_i^{n+1,m} + S_s \frac{\theta_i^{n+1,m}}{\theta_s} \right) \frac{h_i^{n+1,m+1} - h_i^{n+1,m}}{\Delta t} \\
 & - \frac{1}{(\Delta z)^2} \left[ K_{i+1/2} h_{i+1}^{n+1,m} - (K_{i+1/2} + K_{i-1/2}) h_i^{n+1,m} \right. \\
 & \quad \left. + K_{i-1/2} h_{i-1}^{n+1,m} \right] = \frac{K_{i+1/2} - K_{i-1/2}}{\Delta z} - \left( \frac{\theta_i^{n+1,m} - \theta_i^n}{\Delta t} \right) \\
 & \quad + S_s \frac{\theta_i^{n+1,m}}{\theta_s} \frac{h_i^{n+1,m} - h_i^n}{\Delta t} \Rightarrow \text{Term } \Sigma_i
 \end{aligned}$$

My formulation

$$\begin{aligned}
 & - \frac{1}{(\Delta z)^2} \left[ K_{i+1/2} h_{i+1}^{n+1,m} - (K_{i+1/2} + K_{i-1/2}) h_i^{n+1,m} \right. \\
 & \quad \left. + K_{i-1/2} h_{i-1}^{n+1,m} \right] = \frac{K_{i+1/2} - K_{i-1/2}}{\Delta z} - \left( \frac{\theta_i^{n+1,m+1} - \theta_i^n}{\Delta t} \right)
 \end{aligned}$$

$$\begin{aligned}
 \theta_i^{n+1,m+1} & \approx \theta_i^{n+1,m} + \frac{\partial \theta}{\partial h} \bigg|_i (h_i^{n+1,m+1} - h_i^{n+1,m}) \\
 \frac{\partial \theta}{\partial h} \bigg|_i & \approx \left( C_i^{n+1,m} + S_s S_i^{n+1,m} \right) \\
 S_i^{n+1,m} & = \frac{\theta_i^{n+1,m} - \theta_r}{\theta_s - \theta_r}
 \end{aligned}$$

add effect of elastic storage  
Taylor series used to obtain the so-called modified Picard, non-converging form.



$$\frac{\theta_i^{n+1,m+1} - \theta_i^n}{\Delta t} \approx$$

$$\frac{\theta_i^{n+1,m} - \theta_i^n}{\Delta t} + (C_i + S_s S_i) \frac{h_i^{n+1,m+1} - h_i^{n+1,m}}{\Delta t}$$

So I get

$$(C_i + S_s S_i) \frac{h_i^{n+1,m+1} - h_i^{n+1,m}}{\Delta t} - \frac{1}{(\Delta z)^2} \left[ K_{i+1/2} h_i^{n+1,m} - (K_{i+1/2} + K_{i-1/2}) h_i^{n+1,m+1} + K_{i-1/2} h_i^{n+1,m+1} \right] = \frac{K_{i+1/2} - K_{i-1/2}}{\Delta z} h_i^{n+1,m} - \left( \frac{\theta_i^{n+1,m} - \theta_i^n}{\Delta t} \right)$$

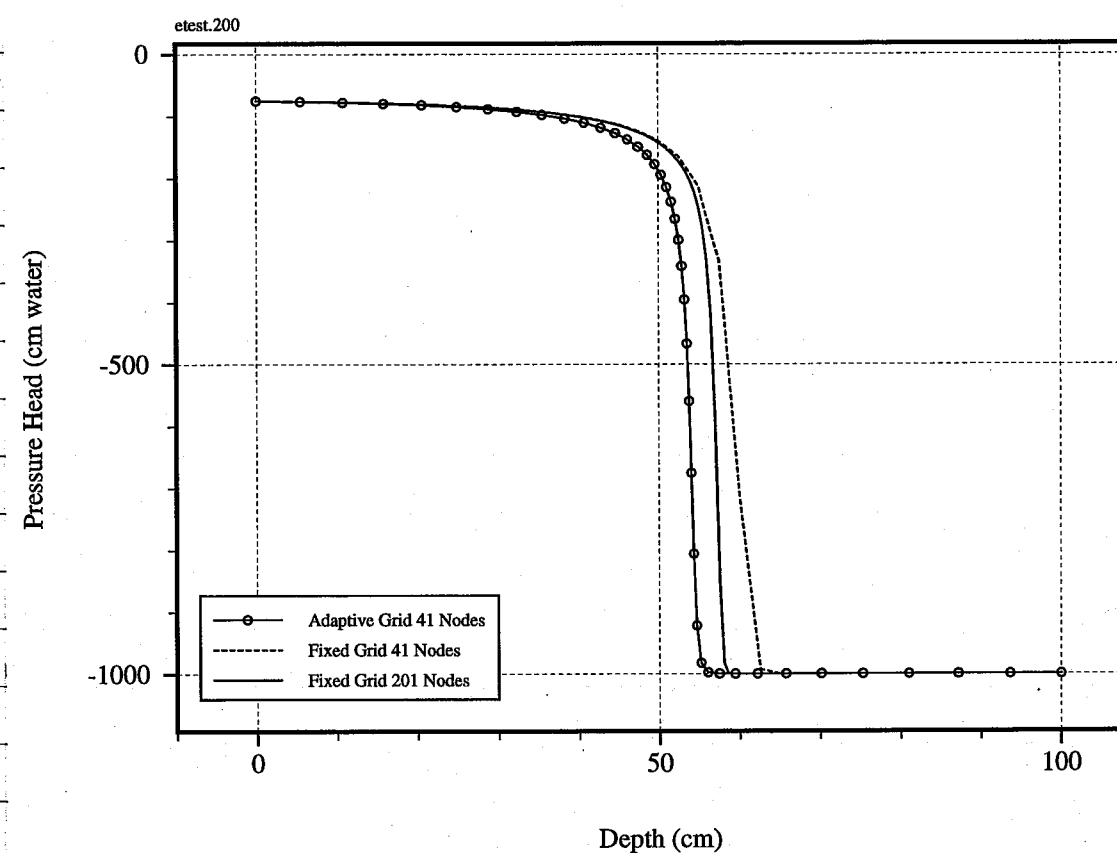
I do not get the  $\Sigma_i$  term identified on page 11 which Celia gets in his formulation! This is the cause of our differences. Clearly as  $S_s \rightarrow 0$ ,  $\Sigma_i \rightarrow 0$  and the formulations are identical.

Gerhard Wittmeyer

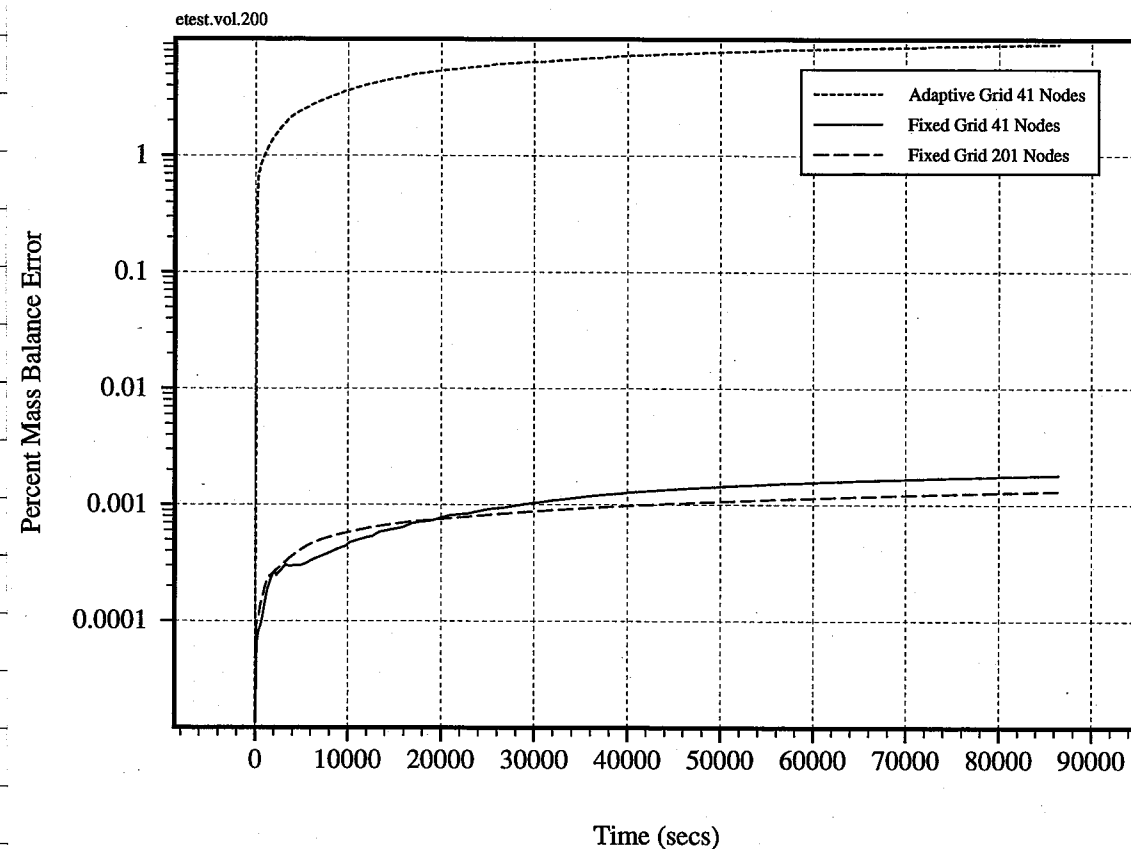
5/10/93

Documenting Mass Balance Error With Adaptive Grids. Others (Gardali & Verrilli, WRR 28(12), 1992 pp 3255-3267) have shown that moving grid finite element solutions to transient infiltration are not mass or volume conserving. My work shows this too. Consider the 1D test problem described on page 5.

Pressure Heads from ADAVAR



## Mass Balance Errors



Not only does the adaptive grid solution lag behind the fixed grid solution at  $T = 86401$  sec, it shows a much greater mass balance undershoot throughout time.

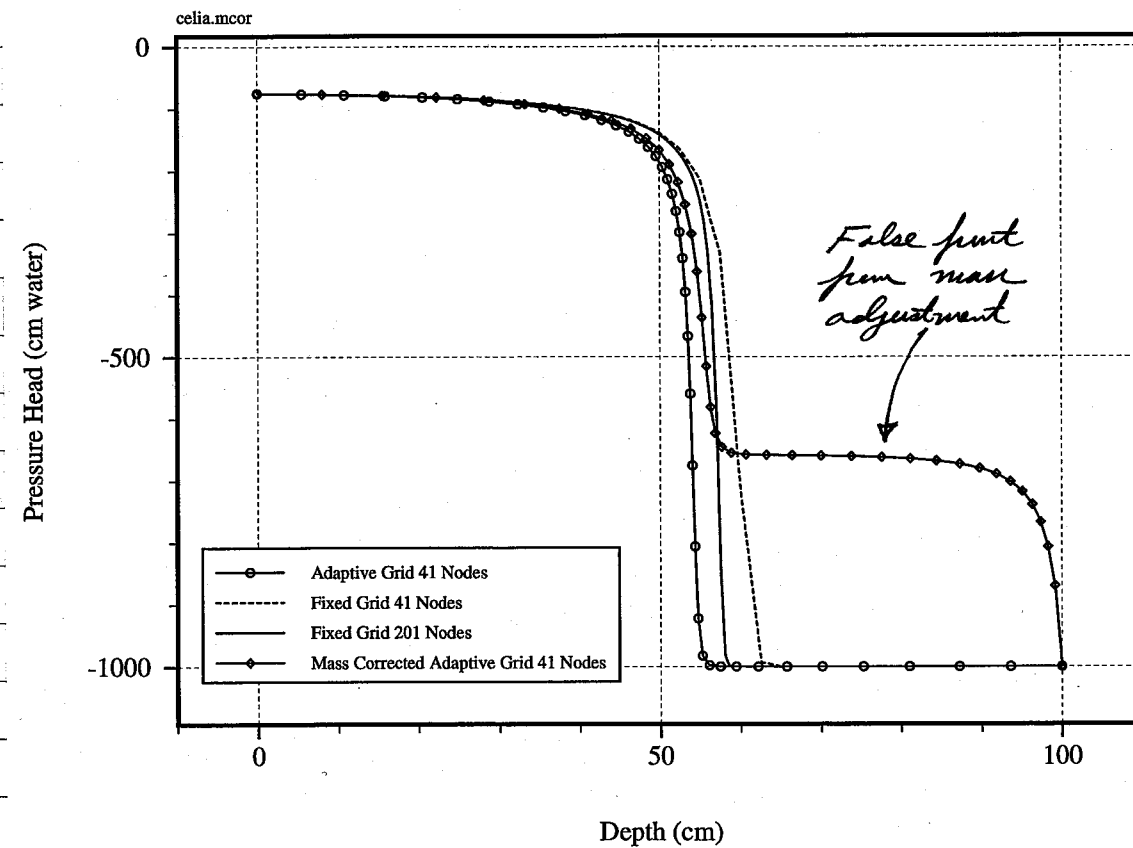
$$e(t) = \text{Percent Mass Balance Error} = \frac{\text{Net Inflow} - \text{Mass Acc.}}{\text{Net Inflow}} \times 100$$

At  $T = 86401$  sec

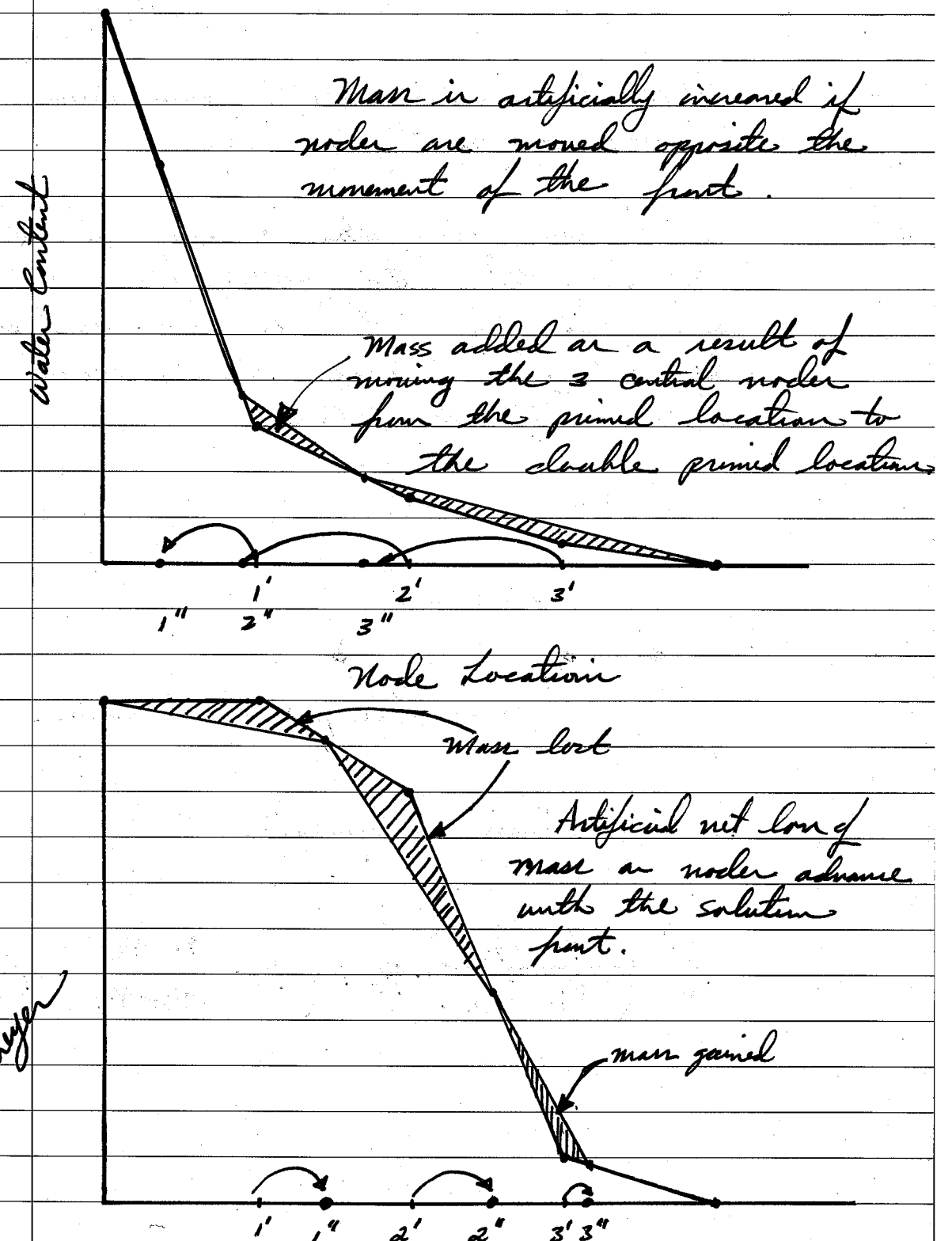
Grid	$e(86401)$
Fixed 41:	- .001809% (Undershoot)
Fixed 201:	- .001311% (Undershoot)
Adaptive 41:	- 9.075% (Undershoot)

The major source of mass balance error occurs during the process of interpolating the solution from the old grid to the new grid. I simply use the linear basis function for the interpolating function. Mass balance can be improved by explicitly adjusting the nodal values of head so that the total system mass is the same from one grid to the next. However, this procedure distorts the true head distribution and often causes a new, non-physical, wetting front to propagate. See next page for an example of this. Note that the mass balance error for the mass adjusted adaptive grid solution is - .6915%.

## Pressure Heads from ADAVAR



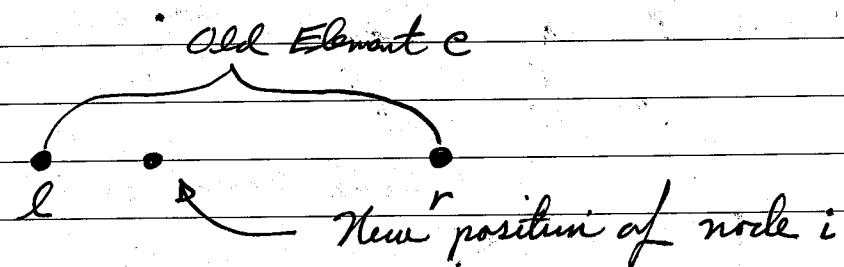
The reason for mass balance error arising, resulting due to the process of grid mapping may be demonstrated by a simple graphing exercise.  $\Rightarrow$

Front Movement  $\rightarrow$ 

5/11/93

More on improving mass conservation in the adaptive grid method:

I have implemented a new method for interpolating the pressure head at the old grid points to the new grid points by solving a local elliptic equation with Dirichlet B.C.s.



1. Using linear interpolation

$$\psi_i' = \left( \frac{\kappa - \kappa_l}{\kappa_r - \kappa_l} \right) \psi_r + \left( 1 - \frac{\kappa - \kappa_l}{\kappa_r - \kappa_l} \right) \psi_l$$

2. Local elliptic Problem on  $e$

With  $\psi_r$  &  $\psi_l$  known solve for  $\psi_i$ :

$$\begin{aligned} * \left( \frac{\kappa_l + \kappa_i}{2} \right) \frac{\psi_i - \psi_l}{\kappa_i - \kappa_l} - \left( \frac{\kappa_i + \kappa_r}{2} \right) \frac{(\psi_r - \psi_i)}{(\kappa_r - \kappa_i)} &= 0 \\ \psi_i &= \frac{(\kappa_r - \kappa_i) \left( \frac{\kappa_l + \kappa_i}{2} \right) \psi_l + (\kappa_i - \kappa_l) \left( \frac{\kappa_i + \kappa_r}{2} \right) \psi_r}{\left[ (\kappa_r - \kappa_i) \left( \frac{\kappa_l + \kappa_i}{2} \right) + (\kappa_i - \kappa_l) \left( \frac{\kappa_i + \kappa_r}{2} \right) \right]} \end{aligned}$$

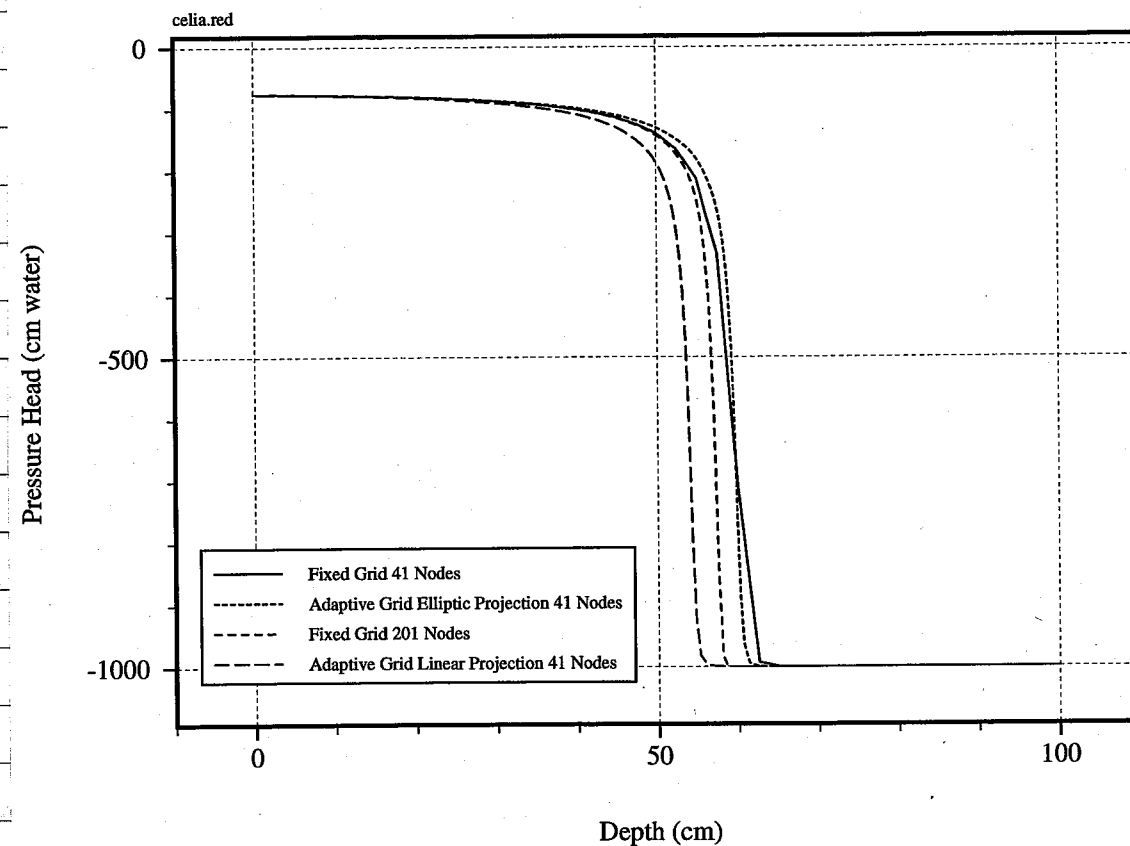
Since  $\kappa_i = \kappa(\psi_i)$ , we must iterate to find a good solution to the above equation.

A comparison of the solutions to problem on page 5 is shown for both method 1 and 2 (linear & elliptic) on the following page.

\* Same as:

$$-\frac{\kappa_{i-1/2}}{\Delta \kappa_{i-1/2}} \psi_{i-1} + \left( \frac{\kappa_{i-1/2} + \kappa_{i+1/2}}{\Delta \kappa_{i-1/2} \Delta \kappa_{i+1/2}} \right) \psi_i - \frac{\kappa_{i+1/2}}{\Delta \kappa_{i+1/2}} \psi_{i+1} = 0$$

## Pressure Heads from ADAVAR



The adaptive grid solution using elliptic projection shows a wetting front which precedes all others. However, problems with mass balance still occur.

The adaptive grid solution with linear projection recorded a mass balance error of  $-9.075\%$  after 86401 sec.

The adaptive grid solution with elliptic projection recorded a mass balance error of  $+4.41\%$  after 86401 seconds.

Increasing the number of nodes in the adaptive scheme from 41 to 101 results in the mass balance error decreasing from  $+4.41\%$  to  $+1.87145\%$  at  $T=86401$  sec. However, the time step was reduced to 36 sec from 144 to reach convergence. If, in addition to increasing the nodes from 41 to 101, we allow the time step to adapt too, the mass balance error is reduced to  $+1.1935\%$ .

Gordon Withmeyer



6/17/93

Testing the adaptive guiding algorithm  
for some more extreme problems.

Problem: 100 cm vertical domain  
50  
100 elements

$$\psi_t = 0 \text{ cm} - 75$$

$$\psi = -10,000 \text{ cm}$$

$$\psi_b = -10,000 \text{ cm}$$

Run for 86401 sec  
≈ 1 day

elapsed time for 50 element fixed  
grid is 179.4 sec.

Mass balance errors are still so severe  
for the adaptive procedure that  
something must be done. I will record  
here the effect of the number of  
elements on the final mass balance  
ratio. Again, the mass balance  
error test is for the rather  
extreme infl. problem above.

$T = 86401 \text{ sec.}$

No. Elem.	Error
15	-2.0147 (+101.47%)
50	-1.0321 (+3.21%)

This problem is too time consuming for  
continued testing of the mass balance  
problem. Therefore, I will revert to the  
old "Cela" problem.

No. Elem.	Error	Error(Fixed Gr.)
10	-1.3098 (+30.98%)	-.99999
20	-1.2015 (+20.15%)	
50	-1.0216 (+2.16%)	
100	-1.0012 (+.12%)	

Gordon Willmeyer

6/23/93

Some more timing marks.

1. Celiai problem, page 5 but on a 60 cm domain

a.) 40 elements adaptive.

 $\Delta t = 144$  sec.elapsed  $T = 142$  sec.

MBE = -9.83 %

b.) 40 elements fixed grid

elapsed  $T = 55.4$  sec.

MBE = -.011 %

2. Celiai problem same as page 5  
100 cm domain,  $S_s = 1 \times 10^{-5}$ 

a) 40 fixed elements

elapsed time = 47.467 sec

MBE = .00181 %

b) 40 adaptive elements

elapsed time = 135.42 sec

MBE = 8.321 %

3. Celiai problem same as page 5  
domain = 100 cm,  $S_s = 1.0 \times 10^{-8}$ 

a) fixed grid 40 elements

elapsed time = 45.617 sec.

MBE = -.00134 %

(celia.out.fix)

b) adaptive grid 40 elements

elapsed time = 134 sec

MBE = -9.29 % (fix.plt)

(celia.out.adapt)

c) Celiai UNS at 10. (mytest.out)

elapsed time = ~~33.7~~ <sup>test</sup> <sub>6/23/93</sub>

71 sec Wall clock

(mytest.plt)

d) fixed grid 200 elements

elapsed time 317.78 sec

MBE = -.00133 %

e) fixed grid 500 elements

elapsed time 1025.74 sec

MBE = -.00133 %

Gordon Willmeyer

Pages 1 through 26 of this Scientific Notebook were reviewed for compliance with QAP-001 in response to Corrective Action Request 94-02. Corrections and clarifications were made as appropriate. In some cases, the date of a change will reflect the date of this review rather than the date of the original Scientific Notebook entry.

Randy Todd  
SWRI-QA  
12/09/94

This research project was formally closed as of January 19, 1996. This research notebook describes efforts at developing an adaptive meshing algorithm for modelling 1D unsaturated flow. The results of this effort are outlined in several CNURA semi-annual research reports.

Gordon Wittmeyer

2/5/96

I have reviewed this scientific notebook and find that it complies with QAP-001 with one exception. There is no mention of the QA status of the code(s) used. This is not significant because the code(s) were used strictly for the purpose of testing calculational algorithms.

There is sufficient technical information so that another qualified individual could repeat the analyses.

PA Boara, PA Element  
2/5/97

**ADDITIONAL INFORMATION FOR SCIENTIFIC NOTEBOOK #: 077**

<b>Document Date:</b>	05/06/1993
<b>Availability:</b>	Southwest Research Institute® Center for Nuclear Waste Regulatory Analyses 6220 Culebra Road San Antonio, Texas 78228
<b>Contact:</b>	Southwest Research Institute® Center for Nuclear Waste Regulatory Analyses 6220 Culebra Road San Antonio, TX 78228-5166 Attn.: Director of Administration 210.522.5054
<b>Data Sensitivity:</b>	<input checked="" type="checkbox"/> "Non-Sensitive" <input type="checkbox"/> Sensitive <input type="checkbox"/> "Non-Sensitive - Copyright" <input type="checkbox"/> Sensitive - Copyright
<b>Date Generated:</b>	12/07/1994
<b>Operating System:</b> (including version number)	SUN OS; UNIX
<b>Application Used:</b> (including version number)	ADAVAR
<b>Media Type:</b> (CDs, 3 1/2, 5 1/4 disks, etc.)	9- 3 1/2 disks
<b>File Types:</b> (.exe, .bat, .zip, etc.)	Various
<b>Remarks:</b> (computer runs, etc.)	Media contains: Bar archive data files.