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**SCIENTIFIC NOTEBOOK #371**

**DR. ANNE-MARIE LEJEUNE**

**20.01402.461**

**JUNE 3, 1999 TO DECEMBER 19, 2000**


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SOUTHWEST RESEARCH INSTITUTE  
CENTER FOR NUCLEAR WASTE REGULATORY ANALYSES  
SAN ANTONIO, TEXAS

Scientific notebook #371 documents work performed to study the interaction of low-volatile content basaltic magma with an horizontal tunnel, project # 20.01402.461. Work was conducted for the period June 3, 1999 through December 19, 2000.

Initial entry by Dr. Anne-Marie Lejeune

 14.01.02

## INITIAL ENTRY

### **Title of the experiments:**

Fluid dynamics of the interaction of basaltic magma with an horizontal tunnel.

### **Individual performing the experiments:**

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### **Description of the analogue experimental system**

#### ***Description of the Apparatus***

We have developed an analogue experimental system to model the flow of magma up a dyke and into a horizontal tunnel. This model (Fig. 1 and 2) consists of a vertical Hele-Shaw cell made up of two parallel plates, one of aluminum the other in glass, which represents the dyke. These plates are 200 mm wide and 500 mm high and 10 mm apart. The base of the cell is connected to a large aluminum reservoir, containing liquid. The internal dimensions of the reservoir are 153 mm in diameter and 485 mm high. Near the top of the Hele-Shaw cell is located a hydraulically operated gate, which can open in a fraction of a second, and which seals the cell from a glass cylinder, of 38 mm radius and 450 mm length, whose axis is horizontal and normal to the plates of the cell.

 14.01.02



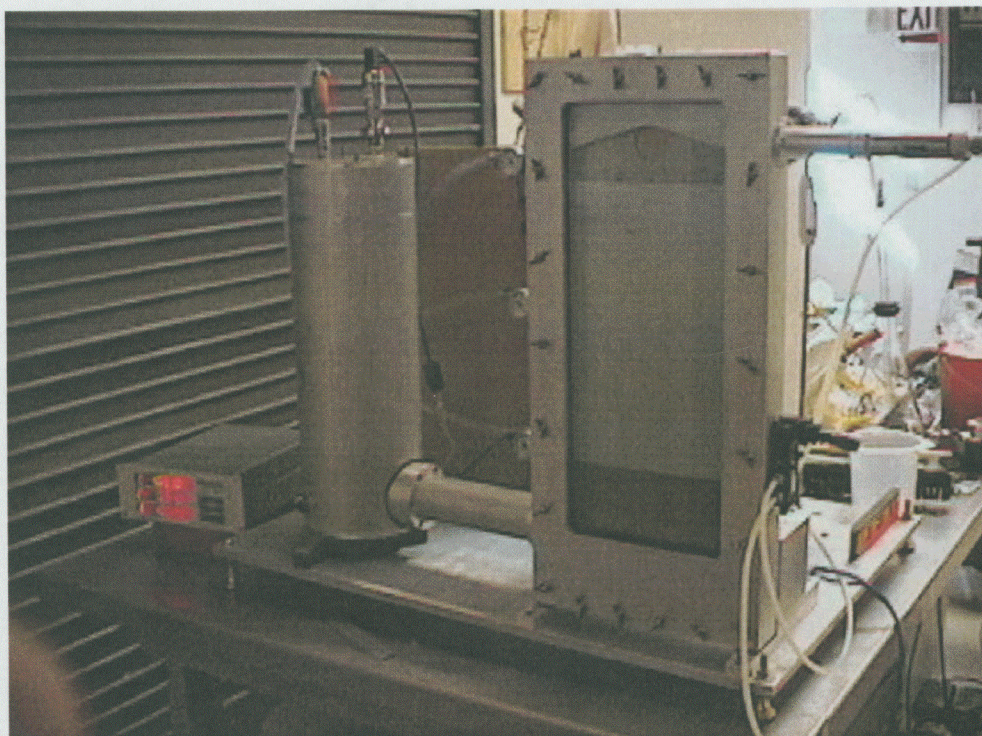


Fig. 1

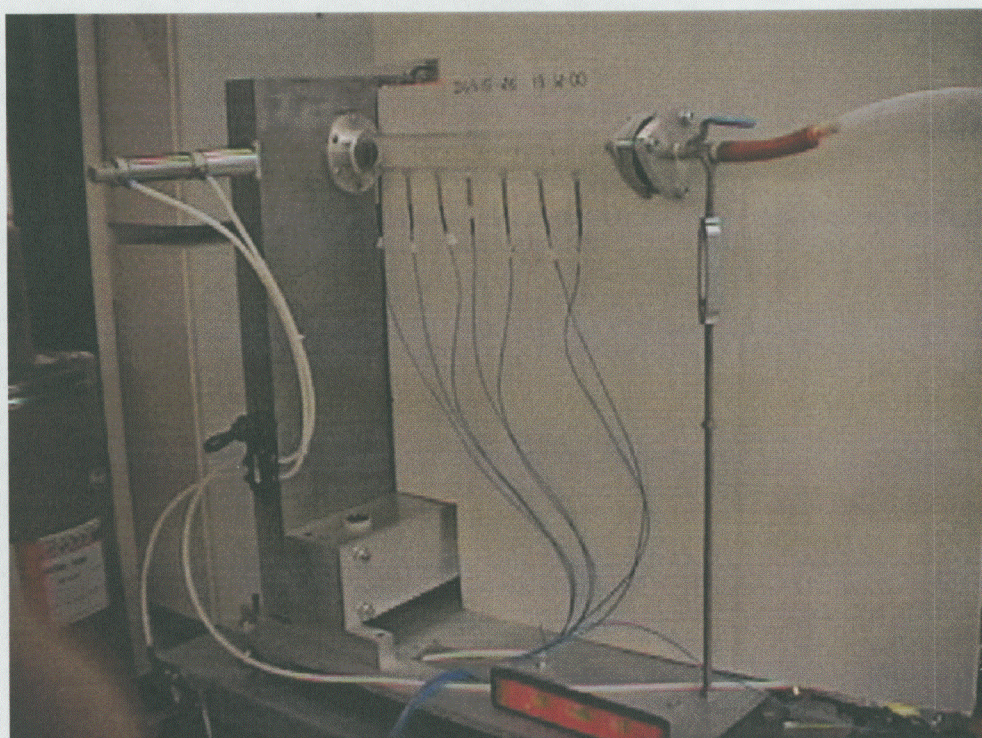


Fig. 2

Hele-Shaw cell

14.01.02




The whole system is sealed from the air, and the pressure at (i) the top of the reservoir, above the layer of liquid, (ii) the top of the Hele-Shaw cell, and (iii) the end of the cylinder can be controlled independently by three vacuum regulators (SMC handle operated vacuum regulators series T203) connected to a diaphragm vacuum pump (KNF Neuberger model N180.3 FT.18). The three pressures can be set independently, so as to control the pressure difference between the reservoir and the top of the dyke, and also between the top of the dyke and the tunnel. Pressures are measured with BOC Edwards active strain gauge (ASG NW16 - 1000 mbar). These gauges are regularly calibrated in the Calibration Laboratory of the Southwest Research Institute in San Antonio, and have an accuracy better than  $\pm 1$  mbar. The experimental system has been sealed from the atmosphere so that it may be operated at very low pressures. A series of miniature pressure sensors (113A21 sensors from PCB Piezotronics) is also emplaced at even distances along the bottom of the glass tube to record the changes of dynamic pressure during the flow propagation.

### ***Experimental Materials***

We are using three working fluids. The first one is pure Golden Syrup (PGS), a partially inverted refiners syrup comprising 31-38wt% sucrose, 42-50wt% invert sugar and the remainder dominantly water, manufactured by Tate & Lyle Co (UK). It has a Newtonian rheology with a strongly temperature-dependent viscosity. In order to cover a wider range of Reynolds numbers, we also used less viscous liquids: Golden Syrup diluted with 5 and 15wt.% de-ionized water and respectively called DGS5 and DGS15.

Viscosities of the samples used in our experiments were measured at Bristol University (UK) over a range of shear rates and temperatures between 0 and 40°C with a Haake RV20 Rotovisco rotating cylinder viscometer, using the sensor systems M5/MVI and M5/SVII. During these measurements, temperatures were set and controlled by a temperature vessel connected to a thermal liquid circulator. Densities are calculated by weighing different known volumes of each of the fluids at room temperature.

 14.01.02



### ***Experimental Methods***

Two series of experiments are carried out with the apparatus. The syrup is initially stored in the Hele-Shaw cell and the reservoir. A series of calibration experiments (named 'dyke experiments', Fig. 3) are conducted first to examine the initial ascent of syrup up the Hele-Shaw cell as a function of the pressure drop between the reservoir and the top of the ascending layer of syrup. This enables us to test the model of flow resistance in the reservoir-dyke part of the system independently of the tunnel.



Figure 3: Dyke experiment

The second main series of experiments involves measuring the flow in the tunnel following the opening of the gate between the tunnel and the Hele-Shaw cell. In these experiments, the cell is initially filled with syrup while the gate is closed. Then the pressure in the tunnel is lowered to a prescribed value below that in the cell, and the gate is opened. The rate of advance of the syrup is then measured, and the morphology of the flow front is observed in the tunnel by analysing high-speed video (Fig. 4) recordings of the experiments.

*[Signature]* 14.01.02



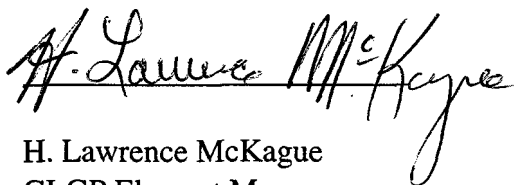


Fig.4

14.01.02



I have reviewed the laboratory notebook for Anne-Marie LeJuene, for the period from 6/3/99 to 12/19/00 and find it in compliance with QAP-001. There is sufficient information regarding procedure used for conducting the research and acquiring and analyzing the data so that another qualified scientist could repeat the activity or activities recorded in this scientific notebook

 10/5/01


H. Lawrence McKague  
GLGP Element Manager

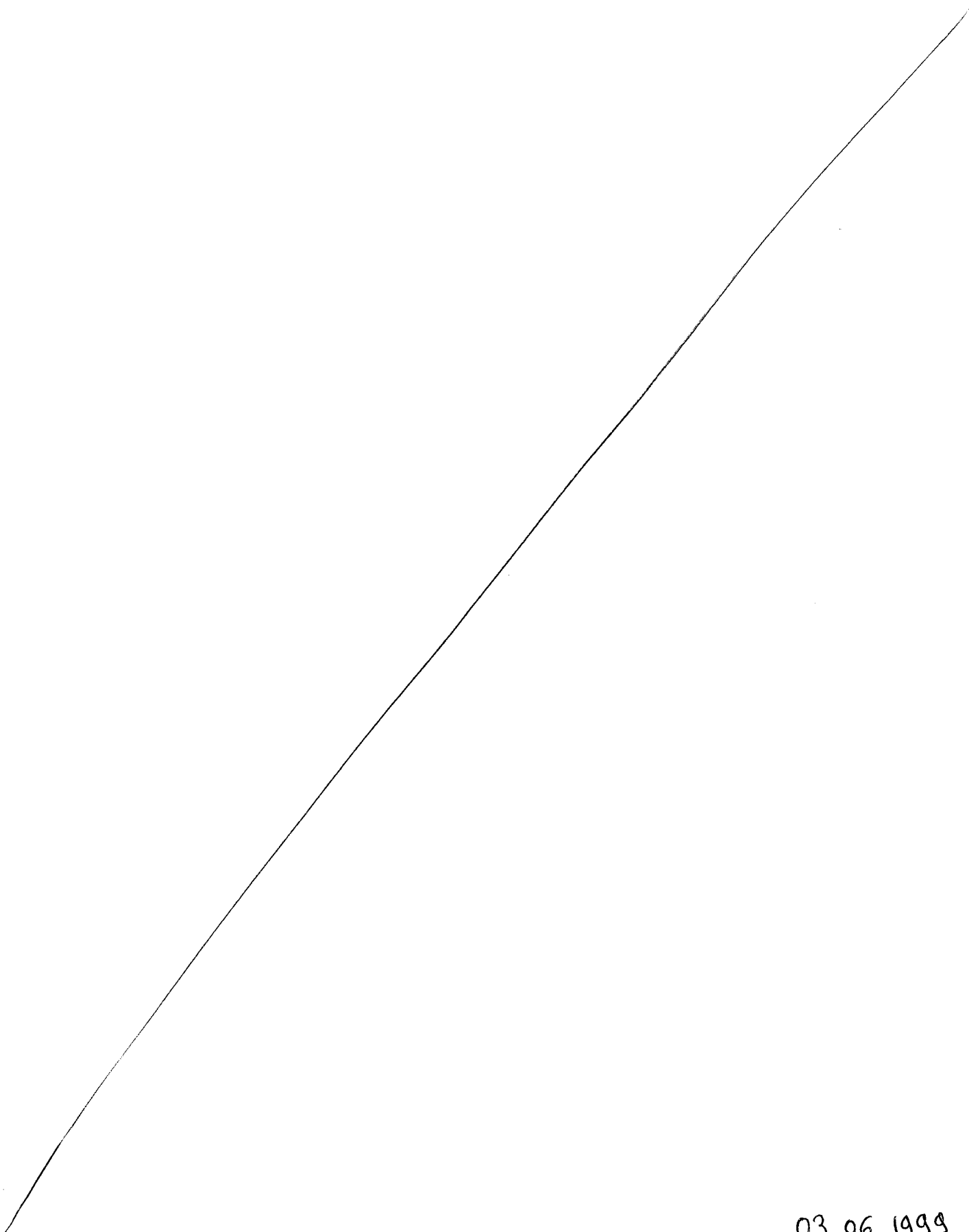


Flow rate experiments  
with pure golden syrup  
(expt no 1 to 108)

06/03/99 — 09/06/00

Anne Marie Lejeune

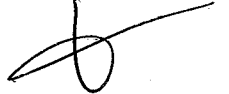
A stylized handwritten signature, likely belonging to Anne Marie Lejeune, consisting of a loop and a long horizontal stroke.



03.06.1999



# FLOW RATE MEASUREMENTS (golden syrup)

3 June 1999  


At atmospheric pressure

$$\begin{aligned} &= 138.5 \text{ mm} \\ \text{GS height in reservoir} &= H - 346.5 \text{ (137.5 mm)} \\ \text{GS visible in dyke} &= 71 \text{ to } 73 \text{ mm} \\ &\text{(GS not levelled in dyke)} \end{aligned}$$

## GS FLOW RATE 1 (video)

$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = 10 \text{ mbar}$$

$$T = 19.5^\circ\text{C}$$

GS in dyke = GS slowly rised  $\Rightarrow$  is there a leak at the gate?  
= 11 to 13 mm

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow & \left| \begin{aligned} P_{\text{reservoir}} &= 10.5 \text{ mbar} \\ P_{\text{tunnel}} &\text{ dropped them back to } 72 \text{ mbar} \\ &\text{at } 6''50 \end{aligned} \right. \end{aligned}$$

Note: From experiment GS FLOW RATE 1 to experiment  
GS FLOW RATE 73, replace  
 $\int \frac{P_{\text{tunnel}}}{T}$  by  $V_{\text{tunnel}}$  (vacuum?) 16.06.1999

level (mm)	time	reservoir (mm)	tunnel (mm)
150	13.23	10.5	73
200	33.28	10.5	74
250	1' 03.24	10.5	74
300	1' 47.80	10.5	74
350	2' 53.33	10.5	74
400	4' 48.88	10.5	74

Gate closed at 7' 03.46 when GS reached the bottom of H-tunnel entrance (—O—)  $\Rightarrow$   $\left| \begin{array}{l} P_{\text{tunnel}} = 77 \text{ mbar} \\ P_{\text{reservoir}} = 10 \text{ mbar} \\ T = 19.4^\circ \text{C} \end{array} \right.$

Pumped down in the dyke to check possible leakage  
 $\Rightarrow$  small air bubbles forming at the middle bottom screw just below the gate

03.06.1999



# GS FLOW RATE (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 9 \text{ mbar}$$

$$T = 19.5^\circ \text{C}$$

$$\text{GS in dyke} = 13 \text{ to } 15 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow P_{\text{reservoir}} = 15 \text{ mbar}$$

$$P_{\text{tunnel}} = 92 \text{ mbar at } 9''70 \text{ after initial drop-off}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	18.51	13	93
200	30.29	12.5	94
250	46.32	12.5	95
300	1' 09.01	12	95
350	1' 38.38	12	96
400	2' 20.07	12	96

Gate closed at 2' 57.54 when GS reached the bottom of the tunnel entrance  $\Rightarrow$

$$P_{\text{tunnel}} = 96 \text{ mbar}$$

$$P_{\text{reservoir}} = 10.5 \text{ mbar and eventually } 9 \text{ mbar}$$



$$P_{\text{tunnel}} = 40 \text{ mbar}$$

$$P_{\text{reservoir}} = 9 \text{ mbar}$$

$$T = 19.5^\circ\text{C}$$

$$\text{GS in dyke} = 14 - 17 \text{ mm}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

$$\begin{array}{|l} \text{LL} \rightarrow \\ \hline P_{\text{reservoir}} = 12 \text{ mbar} \\ P_{\text{tunnel}} = 39 \text{ mbar after } 7'' 51 \end{array}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	2' 7.79	12	40
150	1' 03.99	12	41
200	2' 19.18	11	41
250	6' 47.99	11	42

GS slowed down and almost reached a full stop ( $P_{\text{res}} = 11$ )  
 Gate closed at 24' 39.14 (GS in dyke = 259/261 mm)  $P_{\text{tun}} = 42$ ,

$$\begin{array}{|l} \text{LL} \rightarrow \\ \hline P_{\text{reservoir}} = 10 \text{ mbar} \\ P_{\text{tunnel}} = 43 \text{ mbar} \\ \text{GS in dyke} = 14 - 16 \text{ mm (still some on wall)} \end{array}$$

03.06.1999

# GS FLOW RATE 4 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 60.5 \text{ mbar} \\ P_{\text{reservoir}} &= 9.5 \text{ mbar} \\ T &= 19.5^\circ\text{C} \\ \text{GS in dyke} &= 14 - 17 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

$$\begin{aligned} \Rightarrow P_{\text{reservoir}} &= 13 \text{ mbar} \\ P_{\text{tunnel}} &= 60 \text{ mbar after } 7''39 \end{aligned}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	27.84	12.5	63
200	52.02	12	63
250	1' 29.45	12	64
300	2' 32.61	11.5	64
350	4' 29.77	11.5	64
400	10' 36.16	11.5	64
412/414	25' 16.51	11.5	64

Gate closed at 25'34.51

$$\begin{aligned} \Rightarrow P_{\text{reservoir}} &= 10 \text{ mbar} \\ P_{\text{tunnel}} &= 64 \text{ mbar} \end{aligned}$$



$$P_{\text{tunnel}} = 9.5 \text{ mbar}$$

$$P_{\text{reservoir}} = 80 \text{ mbar}$$

$$T = 19.6^\circ \text{C}$$

GS in dyke = 12/14 mm (GS still on walls)

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{array}{|l} \hookrightarrow P_{\text{reservoir}} \\ P_{\text{tunnel}} \end{array}$$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	4.25	?	?
100	10.42	?	80
150	20.04	13.5	80
200	34.11	12.5	80
250	54.52	11.5	80
300	1' 25.67	11.5	80
350	2' 08.28	11.5	80.5
400	3' 19.25	11.5	80.5

Gate closed at 4' 37.23 when GS reached the bottom of the tunnel entrance  $\Rightarrow$

$$P_{\text{tunnel}} = 81 \text{ mbar}$$

$$P_{\text{reservoir}} = 10 \text{ mbar}$$

03.06.1999

At atmospheric pressure, GS<sub>dyke</sub> = 71 - 73 mm  
 Removed wedges: GS is horizontally levelled, but not the plate limit  
 $\Rightarrow$  no need for wedges  
 Heights measured in the middle of the plate

GS FLOW RATE 6 (video)

$P_{\text{tunnel}} = 50 \text{ mbar}$   
 $P_{\text{reservoir}} = 10 \text{ mbar}$   
 $T = 18.5^\circ \text{C}$   
 GS in dyke = 10 mm (9 - 12 mm)

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	8.42	14.5	49
100	25.01	14	50
150	54.36	14	51
200	1'44.65	13.5	51
250	3'24.85	12	51
300	7'58.16	12	51
319	17'16.95	12	51.5

Gate closed at 17' 56.99

03.06.1999



# GS FLOW RATE 7 (video)

$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = 11.5 \text{ mbar}$$

$$T = 18.6^\circ \text{C}$$

$$\text{GS in dyke} = 8 \text{ mm} (7.9 \text{ mm})$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	5.91	16	70
100	15.26	16	71
150	30.29	15	72
200	52.18	14	72
250	1'25.00	14	72
300	2'17.06	14	72.5
350	3'40.07	14	72.5
400	6'16.33	14	73

Gate closed at 10'21.60 when GS reached the bottom of the tunnel entrance  $\Rightarrow \begin{cases} P_{\text{tunnel}} = 73 \text{ mbar} \\ P_{\text{reservoir}} = 12 \text{ mbar} \end{cases}$

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GS FLOW RATE 8 (video)  $\equiv$  GS FLOW RATE 2

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 12 \text{ mbar}$$

$$T = 18.7^\circ\text{C}$$

$$\text{GS in dyke} = 5 \text{ mm} (4-6 \text{ mm}) \quad (103 \text{ from } \text{L})$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	5.61 (5.01)	17	89
100	11.19	16	90
150	20.90	15	90
200	35.08	14.5	91
250	54.74	14	91
300	1'22.45	14	91
350	2'01.11	14	91
400	2'53.86	13	92

Gate closed at 3'51.66 when GS reached the bottom of the tunnel entrance.

03.06.1999



# GS FLOW RATE 9 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = 12 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$\text{GS in dyke} = 5 \text{ mm} \quad (4-6 \text{ mm})$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	4.96	?	?
100	10.39	17	98
150	19.17	17	100
200	30.75	16	100
250	47.44	15	100
300	1'09.69	15	100
350	1'39.60	14	100
400	2'19.96	14	100

Gate closed at 3'01.32 when GS reached the bottom of the tunnel entrance  $\Rightarrow$

$$\begin{cases} P_{\text{tunnel}} = 101 \text{ mbar} \\ P_{\text{reservoir}} = 14 \text{ mbar} \end{cases}$$

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GS FLOW RATE 10 (video)  $\equiv$  GS FLOW RATE 5

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$P_{\text{reservoir}} = 12 \text{ mbar}$$

$$T = 18.9^\circ \text{C}$$

GS in dyke = 4 mm (3-5 mm) GS still on walls

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	5.74	?	80
100	12.20	16	81
150	22.54	16	82
200	37.43	15	83
250	59.32	14.5	83
300	1'30.80	14	83.5
350	2'15.59	14	84
400	3'24.24	14	84

Gate closed at 4'46.97 when GS reached the bottom of the tunnel

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 84 \text{ mbar} \\ P_{\text{reservoir}} = 13 \text{ mbar} \end{cases}$$

03.06.1999





GS FLOW RATE 11 (video)  $\equiv$  GS FLOW RATE 4

$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$P_{\text{reservoir}} = 12 \text{ mbar}$$

$$T = 18.9^\circ\text{C}$$

$$\text{GS in dyke} = 5 \text{ mm (4-6 mm)}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	6.67	16	60
100	17.20	16	61
150	35.18	15	62
200	1'00.88	13.75	62.5
250	1'43.72	13.75	63
300	2'59.07	13.75	63
350	5'30.63	13.75	63
395	26'33.88	13.75	63

Gate closed at 26'51.64 -  $T = 19.0^\circ\text{C}$

At atmospheric pressure  $\left| \begin{array}{l} \text{GS in dyke} = 73 \text{ mm (71 to 74 mm)} \\ \text{GS}_{\text{reservoir}} = 11 - 351 \end{array} \right.$

Added GS in reservoir.

03.06.1999

# SECOND SET OF FLOW RATE MEASUREMENTS

7 June 1999

At atmospheric pressure

$$\begin{aligned} \text{GS height in reservoir} &= 4 - 264 \text{ mm} = 221 \text{ mm} \\ \text{GS visible in dyke} &= 158.5 \text{ mm} \quad (157.5 - 159.5 \text{ mm}) \\ T &= 18.1^\circ\text{C} \end{aligned}$$

GS FLOW RATE 12 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 50 \text{ mbar} \\ P_{\text{reservoir}} &= 11.5 \text{ mbar} \\ T &= 18.1^\circ\text{C} \\ \text{GS in dyke} &= 97 \text{ mm} \quad (96 - 98 \text{ mm}) \end{aligned}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow P_{\text{reservoir}} &= 12.25 \\ P_{\text{tunnel}} &\text{ down to } 24 \text{ mbar, back at } 49 \text{ mbar after } 10.66 \end{aligned}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	20.10	12.25	49
200	50.61	12.25	50
250	1'43.91	12.25	50
300	3'13.75	12.25	50
350	6'14.71	12.25	50
400	23'55.10	12.25	50.5

$$\begin{aligned} \text{Gate closed at } 25' 23.63 &- P_{\text{reservoir}} = 12 \text{ mbar} \\ &P_{\text{tunnel}} = 50.5 \text{ mbar} \end{aligned}$$

07.06.1999



$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = 12 \text{ mbar}$$

$$T = 18.4^\circ\text{C}$$

$$\text{GS in dyke} = 94.5 \text{ mm} (93.5 \text{ to } 95.5 \text{ mm})$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Leftrightarrow \left. \begin{array}{l} P_{\text{reservoir}} = 13.75 \text{ mbar} \\ P_{\text{tunnel}} = 68 \text{ mbar} \end{array} \right\} \text{ after } 5'' 64$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	15.22	13.75	69
200	33.68	13.75	69.5
250	59.91	13.5	70
300	1' 37.77	13.5	70
350	2' 33.84	13.25	70
400	3' 58.73	13.25	70

Gate closed at 5' 43.54 when GS reached the tunnel

$$\Rightarrow \left. \begin{array}{l} P_{\text{tunnel}} = 70 \text{ mbar} \\ P_{\text{reservoir}} = 13.25 \text{ mbar} \end{array} \right\}$$

07.06.1999



# GS FLOW RATE 14 (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 11.75 \text{ mbar}$$

$$T = 18.5^\circ \text{C}$$

GS in dyke = 93.5 mm (92.5 to 94.5 mm) still on walls

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \left. \begin{array}{l} P_{\text{reservoir}} = 14.5 \text{ mbar} \\ P_{\text{tunnel}} = 88 \text{ mbar} \end{array} \right\} \text{ after } 5''50$$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	9.90	14.5	89
200	20.81	14.5	89.5
250	35.85	14	89.5
300	56.85	14	90
350	1'25.70	14 sudden drop to 12.5	90
400	2'05.29	12.5	90

Gate closed at 2'47.78 when GS reached the tunnel entrance

$$\Rightarrow \left. \begin{array}{l} P_{\text{tunnel}} = 90 \text{ mbar} \\ P_{\text{reservoir}} = 12.5 \text{ mbar} \end{array} \right\}$$

07.06.1999

GS FLOW RATE 15 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = 11.75 \text{ mbar}$$

$$T = 18.5^\circ \text{C}$$

GS in dyke = 93 mm (92-94 mm) GS still on walls

Dyke valve closed - Gate opened at  $t_0 = 0$  \*

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	8.53	14.5	98
200	19.43	14.5	99
250	33.58	14.5	99
300	53.28	14	99
350	1'18.24	14	99.5
400	1'51.42	13	99.5

Gate closed at 2'23.80 when GS reached the tunnel

entrance  $\Rightarrow \begin{cases} P_{\text{tunnel}} = 100 \text{ mbar} \\ P_{\text{reservoir}} = 12.5 \text{ mbar} \end{cases}$

\* Gate stuck with GS  $\Rightarrow$  can't open properly

07.06.1999

Set up experiment for  $P_{\text{tunnel}} = 80 \text{ mbar}$

$$P_{\text{tunnel}} = 80.25 \text{ mbar}$$

$$P_{\text{reservoir}} = 11.5 \text{ mbar}$$

$$T = 18.6^\circ \text{C}$$

$$\text{GS in dyke} = 93 \text{ mm (92-94 mm)}$$

But the gate is stuck (GS infiltrated within it) and won't open  $\Rightarrow$  had to abort  $\Rightarrow$  clean the setup

$$\text{GS in dyke at atmospheric pressure} = 158.5 \text{ mm}$$

CLEANING the APPARATUS

8 June 1999

08.06.1999



at atmospheric pressure

$$\begin{aligned} \text{GS height in reservoir} &= H - 258 \text{ mm} = 227 \text{ mm} \\ \text{GS inside in dyke} &= 162.5 \text{ mm} \\ T &= 18.2^\circ\text{C} \end{aligned}$$

GS FLOW RATE 16 (video)

Air leaking inside the tunnel via the connection  $\Rightarrow$  put loads of silicone grease on O' rings, glass tube and had to push the glass tube against the door (should leave  $\sim 1$  mm in between to avoid glass breakage  $\Rightarrow$  to be sorted out) (change O' rings?)

$$\begin{aligned} P_{\text{tunnel}} &= 80 \text{ mbar} \\ P_{\text{reservoir}} &= 10.75 \text{ mbar} \\ T &= 18.3^\circ\text{C} \\ \text{GS in dyke} &= 101.5 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow P_{\text{reservoir}} &= 13.5 \text{ mbar} \\ P_{\text{tunnel}} &\text{ down to } 56 \text{ mbar, back to } 79 \text{ mbar after } 6'' 31 \end{aligned}$$

10.06.1999

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	10.01	13.5	80
200	23.80	13.25	80
250	43.46	13.25	80.5
300	1'12.54	13.25	80.5
350	1'53.99	12	80.5
400	2'50.89	12	81
Time 410	3'08.85	12	81
Gate closed	3'48.09 $\Rightarrow$ 11.5		81

when GS reached the tunnel entrance (435)

# GS FLOW RATE 17 (video)

$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$P_{\text{reservoir}} = 10.5 \text{ mbar}$$

$$T = 18.3^\circ\text{C}$$

$$\text{GS in dyke} = 99 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = 12.75 \text{ mbar} \\ P_{\text{tunnel}} \text{ down to } 44 \text{ mbar, back at } 60 \text{ mbar after } 4''4 \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	14.18	12.75	61
200	33.82	12.75	61.5
250	1'03.57	12.75	61.5
300	1'47.16	12.75	62
350	2'55.65	12.5	62
400	4'52.64	12.5	62
Line 410	5'36.42	12.5	62
435	7'39.70	12.5	62

Gate closed when GS reached the tunnel entrance

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 63 \text{ mbar} \\ P_{\text{reservoir}} = 11 \text{ mbar} \end{cases}$$

10.06.1999



# GS FLOW RATE 18 (video)

$$P_{\text{tunnel}} = 40 \text{ mbar}$$

$$P_{\text{reservoir}} = 11 \text{ mbar}$$

$$T = 18.4^{\circ}\text{C}$$

GS in dyke = 985 mm (still some on walls)

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = 11.5 \text{ mbar} \\ P_{\text{tunnel}} = 38 \text{ mbar after } 8'51 \end{cases}$$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	33.65	11.5	39
200	1'34.07	11.5	39
250	4'02.68	11.5	39
280	20'23.53	11.25	39

Gate closed at 20'23.53  $\Rightarrow \begin{cases} P_{\text{tunnel}} = 39.5 \text{ mbar} \\ P_{\text{reservoir}} = 11.25 \text{ mbar} \end{cases}$

10.06.1999

GS FLOW RATE 19 (video)  $\equiv$  GS FLOW RATE 15

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = 11.25 \text{ mbar}$$

$$T = 18.5^\circ\text{C}$$

$$\text{GS in dyke} = 99 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = 14 \text{ mbar} \\ P_{\text{tunnel}} = 100 \text{ mbar after } 6''45 \end{cases}$$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	19.81	14	102
250	35.72	14	102
300	57.42	14	102
350	1'24.73	12.5	103
400	2'02.72	12.5	103
435	2'37.99	12.5	103

Gate closed at 2'37.99 when GS reached the tunnel entrance

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 104 \text{ mbar} \\ P_{\text{reservoir}} = 11.25 \text{ mbar} \end{cases}$$

10.06.1999



GS FLOW RATE 20 (video)  $\equiv$  GS FLOW RATE 13

$$\begin{array}{|l} P_{\text{tunnel}} = 70.5 \text{ mbar} \\ P_{\text{reservoir}} = 11.25 \text{ mbar} \\ T = 18.5^\circ\text{C} \\ \text{GS in dyke} = 98 \text{ mm} \end{array}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{array}{|l} P_{\text{reservoir}} = 13 \text{ mbar} \\ P_{\text{tunnel}} = 70 \text{ mbar after } 4'41 \end{array}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	1'2.73	13	72
200	2'9.83	13	72.5
250	5'5.11	13	73
300	11'33.12	13	73
350	2'29.16	13	73.5
400	3'58.84	13	73.75
410	4'32.84	13	73.75
435	6'05.20	13	73.75

Gate closed at 6'05.20 when GS reached the tunnel entrance.

$$\Rightarrow \begin{array}{|l} P_{\text{tunnel}} = 74.75 \text{ mbar} \\ P_{\text{reservoir}} = 11 \text{ mbar} \end{array}$$

10.06.1999



# GS FLOW RATE 21 (video)

$$P_{\text{tunnel}} = 50.5 \text{ mbar}$$

$$P_{\text{reservoir}} = 22.75 \text{ mbar}$$

$$T = 18.6^\circ \text{C}$$

GS in dyke = 18 mm (still some GS on walls)

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow P_{\text{reservoir}} = 27.5 \text{ mbar at maximum}$$

$P_{\text{tunnel}}$  down to 38 mbar, back at 50 mbar at 1' or

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	7.73	27.5	48
100	27.06	26.5	49.5
150	1'00.40	26	50
200	2'06.17	26	50.5
250	5'04.54	24.5	50.5
274.5	21'00.79	24.5	50.5

Gate closed at 21'00.79  $\Rightarrow$   $P_{\text{tunnel}} = 51 \text{ mbar}$   
 $P_{\text{reservoir}} = 24 \text{ mbar}$

10.06.1999





# GS FLOW RATE 22 (video)

$$P_{\text{tunnel}} = 70.5 \text{ mbar}$$

$$P_{\text{reservoir}} = 23.5 \text{ mbar}$$

$$T = 18.6^\circ \text{C}$$

$$\text{GS in dyke} = 17.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	4.54	29.5	70
100	14.26	27.5	71.75
150	30.05	27.25	72
200	54.64	26.5	72.5
250	1'33.31	26	73
300	2'36.45	26	73
350	4'30.29	26	73
400	8'51.84	24.5	73
410	11'34.70	24.5	73
422.5	15'44.70	24.5	73
427.5	21'43.23	24.5	73
429	26'24.84	24.5	74

Gate closed at 26'29.26  $\Rightarrow \begin{cases} P_{\text{tunnel}} = 74 \text{ mbar} \\ P_{\text{reservoir}} = 24.5 \text{ mbar} \end{cases}$

N.B. End of videotape noticed at 14' 46.37

10.06.1999

# GS FLOW RATE 23 (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 23.25 \text{ mbar}$$

$$T = 18.7^\circ\text{C}$$

GS in dyke = 15 mm (still some on wall)

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	3.88	31	90
100	10.84	30	91
150	20.43	28	91
200	34.59	27	92
250	55.53	27	92
300	1'25.09	26.5	92
350	2'05.49	26	92.25
400	3'09.27	26	92.25
410	3'30.03	26	92.5
435	4'22.77	26	92.5

Gate closed at 4'22.77 when GS reached tunnel entrance

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 93 \text{ mbar} \\ P_{\text{reservoir}} = 23.25 \text{ mbar} \end{cases}$$

10.06.1999



# GS FLOW RATE 24 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = 23.25 \text{ mbar}$$

$$T = 18.7^{\circ}\text{C}$$

$$\text{GS in dyke} = 15.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	3.91	32	96
100	10.48	31	99
150	19.65	28.5	100
200	32.97	28	100
250	51.10	26.5	100.5
300	1'15.84	26.5	100.5
350	1'50.25	26.25	100.5
400	2'39.21	26	100.5
410	2'55.79	26	100.5
435	3'31.82	26	100.5

$$\text{Gate closed at } 3'31.82 \Rightarrow \begin{cases} P_{\text{tunnel}} = 101 \text{ mbar} \\ P_{\text{reservoir}} = 23.25 \text{ mbar} \end{cases}$$

10.06.1999



# GS FLOW RATE 25 (video)

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$P_{\text{reservoir}} = 23.25 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$\text{GS in dyke} = 15 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	4.33	31	78
100	6.71	29	80
150	25.45	28	81
200	44.16	26.5	81
250	1' 11.96	26.5	81.5
300	1' 52.52	26	81.75
350	2' 56.30	26	82
400	4' 45.37	26	82
410	5' 29.50	26	82
435	7' 27.45	26	82

$$\text{Gate closed at } 7' 27.45 \Rightarrow \begin{cases} P_{\text{tunnel}} = 82 \text{ mbar} \\ P_{\text{reservoir}} = 23.25 \text{ mbar} \end{cases}$$

10.06.1999





## GS FLOW RATE 26 (video)

$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$P_{\text{reservoir}} = 23 \text{ mbar}$$

$$T = 18.2^\circ\text{C}$$

$$\text{GS in dyke} = 28 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	4.86	26	58
100	19.30	26	59
150	43.75	24.5	60
200	1'29.79	24.5	60
250	2'53.25	24.5	60.5
300	5'52.10	24.5	60.5
322	8'46.83	22.5	60.5
343.5	25'41.52	22.5	61
343.5	30'11.88	22.5	61

Gate closed at 30' 11.88  $\Rightarrow \begin{cases} P_{\text{tunnel}} = 61 \text{ mbar} \\ P_{\text{reservoir}} = 22 \text{ mbar} \end{cases}$

11.06.1999



GS FLOW RATE 27 (video)  $\equiv$  GS FLOW RATE 23

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 22 \text{ mbar}$$

$$T = 18.3^\circ \text{C}$$

$$\text{GS in dyke} = 27 \text{ mm (still some on walls)}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
50	3.03	28	88
100	9.49	28	90
150	19.90	26.5	91
200	34.94	25	91
250	57.07	25	91.5
300	1'28.19	24.75	91.5
350	2'16.16	24.75	91.5
400	3'26.45	22.5	91.5
410	3'48.71	22.5	91.5
435	4'45.51	22.5	91.5

Door closed when GS reached the tunnel entrance

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 92 \text{ mbar} \\ P_{\text{reservoir}} = 21.75 \text{ mbar} \end{cases}$$

11.06.1999



# GS FLOW RATE 28 (video)

$$P_{\text{tunnel}} = 50 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric pressure}$$

$$T = 18.5^\circ\text{C}$$

$$GS \text{ in dyke} = 162.5 \text{ mm}$$

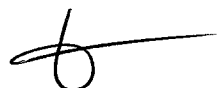
Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow & \left| \begin{aligned} P_{\text{reservoir}} &= \\ P_{\text{tunnel}} &= 50 \text{ mbar after } 6'' 32 \end{aligned} \right. \end{aligned}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	20.61	0	50
250	1'00.99	0	51
300	2'06.74	0	51
350	4'05.76	0	51.5
374.5	5'51.95	0	51.5
400	9'09.44	0	51.75
410	13'04.60	0	51.75
420	19'42.11	0	51.75
422.5	25'47.47	0	51.75

Gate closed at 25'47.47  $\Rightarrow P_{\text{tunnel}} = 52.25 \text{ mbar}$

11.06.1999



(GS FLOW RATE 29) (video)

$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.5^\circ \text{C}$$

$$\text{GS in dyke} = 162.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow P_{\text{reservoir}} &= \\ P_{\text{tunnel}} &= 68 \text{ mbar after } 4'18 \end{aligned}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	11.84	0	69
250	33.22	0	69.5
300	1'04.49	0	70
350	1'48.81	0	70
374.5	2'20.16	0	70
400	2'58.08	0	70
410	3'24.01	0	70
435	4'23.19	0	70

Gate closed at 4'23.19  $\Rightarrow P_{\text{tunnel}} = 70.5 \text{ mbar}$

11.06.1999



# GS FLOW RATE 29 (video)

$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.5^\circ \text{C}$$

$$\text{GS in dyke} = 162.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\begin{aligned} \Rightarrow & P_{\text{reservoir}} = \\ & P_{\text{tunnel}} = 68 \text{ mbar after } 4'18 \end{aligned}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	11.84	0	69
250	33.22	0	69.5
300	1'04.49	0	70
350	1'48.81	0	70
374.5	2'20.16	0	70
400	2'58.08	0	70
410	3'24.01	0	70
435	4'23.19	0	70

Gate closed at 4'23.19  $\Rightarrow P_{\text{tunnel}} = 70.5 \text{ mbar}$



GS FLOW RATE 30 (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.6^\circ\text{C}$$

$$\text{GS in dyke} = 162.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	8.65	0	90
250	22.23	0	91
300	41.29	0	91
350	1'07.21	0	91.25
374.5	1'23.27	0	91.5
400	1'42.64	0	91.5
410	1'54.02	0	91.5
435	2'19.09	0	91.5

Gate closed at 2'19.09  $\Rightarrow P_{\text{tunnel}} = 92 \text{ mbar}$

11.06.1999



# GS FLOW RATE 31 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.6^\circ\text{C}$$

$$\text{GS ice dyke} = 162.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	7.43	0	99
250	19.78	0	100
300	35.46	0	100
350	56.82	0	100
374.5	1' 10.03	0	100
400	1' 25.67	0	100
410	1' 34.74	0	100
435	1' 55.42	0	100

Gate closed at 1' 55.09  $\Rightarrow P_{\text{tunnel}} = 101 \text{ mbar}$

11.06.1999

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.7^\circ\text{C}$$

$$\text{GS in dyke} = 163 \text{ mm}$$

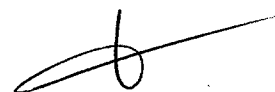
Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow P_{\text{tunnel}} = 79 \text{ mbar after } 4'' 09$$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	10.03	0	80
250	25.84	0	80
300	49.81	0	80.5
350	1' 21.41	0	80.5
374.5	1' 41.59	0	80.5
400	2' 07.65	0	80.5
410	2' 22.16	0	80.5
435	2' 59.13	0	80.5

Gate closed at 2' 59.13  $\Rightarrow P_{\text{tunnel}} = 81 \text{ mbar}$

11.06.1999



# GS FLOW RATE 33 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 60 \text{ mbar} \\ P_{\text{reservoir}} &= \text{atmospheric} \\ T &= 18.7^\circ\text{C} \\ \text{GS in dyke} &= 162.5 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

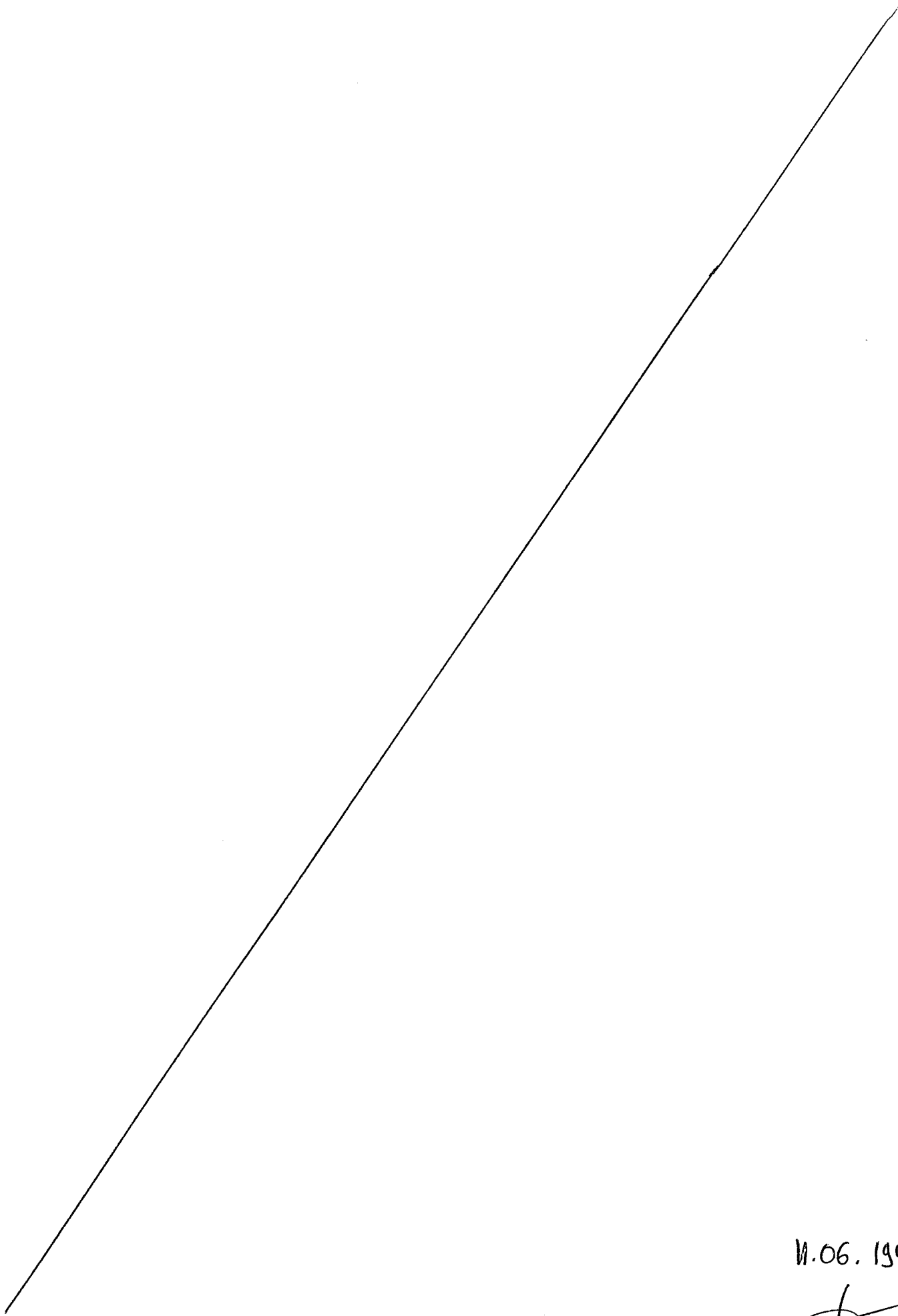
$$\Rightarrow P_{\text{tunnel}} = 58 \text{ mbar after } 4''26$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
200	15.03	0	58.5
250	43.58	0	59
300	1'24.91	0	59.5
350	2'30.67	0	59.75
374.5	3'20.18	0	60
400	4'29.48	0	60
410	5'16.72	0	60
435	7'34.16	0	60

Gate closed at 7'34.16  $\Rightarrow P_{\text{tunnel}} = 60.25 \text{ mbar}$

11.06.1999





11.06.1999

A stylized, handwritten mark or signature, possibly a cursive letter 'b' or a similar flourish, located below the date.



# THIRD SET OF FLOW RATE MEASUREMENTS

14 June 1999

At atmospheric pressure

$$\begin{aligned} \text{GS height in reservoir} &= 4.162 \text{ mm} = 323 \text{ mm} \\ \text{GS visible in dyke} &= 259 \text{ mm} \end{aligned}$$

GS FLOW RATE 34 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 50 \text{ mbar} \\ P_{\text{reservoir}} &= \text{atmospheric} \\ T &= 17.9^\circ \text{C} \\ \text{GS in dyke} &= 259 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
275	14.70	0	49
300	41.23	0	49.5
325	1'12.65	0	49.5
350	1'50.75	0	50
375	2'39.29	0	50
400	3'40.84	0	50
410	4'20.70	0	50
435	6'00.76	0	50

Gate closed at 6'00.76  $\Rightarrow P_{\text{tunnel}} = 51.5 \text{ mbar}$

14.06.1999

$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.0^\circ \text{C}$$

$$\text{GS in dyke} = 260.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	7.31	70
300	20.12	70
325	35.51	70
350	53.96	70.5
375	1'15.51	70.5
400	1'42.51	70.5
410	1'57.20	71
435	2'32.06	71

Gate closed at 2'32.06  $\Rightarrow P_{\text{tunnel}} = 72 \text{ mbar}$

### GS FLOW RATE 36 (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$T = 18.1^\circ \text{C}$$

$$\text{GS in dyke} = 260.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	5.23	90
300	14.46	90
325	25.19	90
350	37.65	90
375	51.40	90.25
400	1'08.58	90.25
410	1'17.89	90.25
435	1'38.99	90.25

Gate closed at 1'38.99  $\Rightarrow P_{\text{tunnel}} = 91.5 \text{ mbar}$

14.06.1999

# GS FLOW RATE 37 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$T = 18.2^{\circ}\text{C}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$\text{GS in dyke} = 261 \text{ mm}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	4.54	100
300	12.36	100
325	21.36	100
350	31.26	100
375	43.23	100
400	57.13	100
410	1'04.92	100.5
435	1'22.66	100.5

Gate closed at 1'22.66  $\Rightarrow P_{\text{tunnel}} = 102 \text{ mbar}$

# GS FLOW RATE 38 (video)

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$T = 18.2^{\circ}\text{C}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$\text{GS in dyke} = 261.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	5.56	80
300	16.21	80
325	27.75	80
350	42.28	80.25
375	58.71	80.5
400	1'18.71	80.5
410	1'29.87	80.5
435	1'55.56	80.5

Gate closed at 1'55.56  $\Rightarrow P_{\text{tunnel}} = 80.5 \text{ mbar}$

14.06.1999

$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$T = 18.3^\circ\text{C}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

$$\text{GS in dyke} = 260 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	8.49	59.5
300	23.89	59.5
325	42.42	60
350	1'04.84	60
375	1'31.21	60
400	2'06.23	60
410	2'27.25	60
435	3'16.33	60

Gate closed at 3'16.33  $\Rightarrow P_{\text{tunnel}} = 61.5 \text{ mbar}$

GS FLOW RATE 40 (video)

$$P_{\text{tunnel}} = 40 \text{ mbar}$$

$$T = 18.3^\circ\text{C}$$

$$P_{\text{reservoir}} = \text{atmospheric}$$

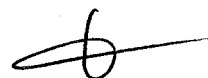
$$\text{GS in dyke} = 261 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{tunnel}}$ (mbar)
275	15.51	37.5
300	48.39	38
325	1'29.62	38
350	2'26.93	38
375	3'53.62	38
400	6'31.27	38.25
410	9'12.52	38.25
430	24'45.30	38.25

Gate closed at 25'02.40  $\Rightarrow P_{\text{tunnel}} = 39.5 \text{ mbar}$

14.06.1999



# GS FLOW RATE 41 (video)

$$P_{\text{tunnel}} = 50 \text{ mbar}$$

$$P_{\text{reservoir}} = 21.5 \text{ mbar}$$

$$T = 18.6^\circ \text{C}$$

$$\text{GS in dyke} = 133.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	8.41	22	49
175	22.93	22	49.5
200	39.90	22	50
225	1'02.36	22	50
250	1'31.92	22	50
275	2'08.42	22	50.25
300	3'00.62	22	50.5
325	4'09.99	22	50.5
350	6'12.40	22	50.5
375	10'32.25	22	50.5
383 381	14'25.97	22	50.5
388 386	22'38.17	22	50.5
389 387	29'23.67	22	50.5
389 387	35'04.05	22	50.5

Gate closed at 35'04.05  $\Rightarrow$

$$P_{\text{tunnel}} = 51 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

14.06.1999

*[Signature]*



$$P_{\text{tunnel}} = 70.25 \text{ mbar}$$

$$P_{\text{reservoir}} = 20.75 \text{ mbar}$$

$$T = 18.7^\circ\text{C}$$

$$GS \text{ in dyke} = 132.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	5.63	25.5	70
175	13.45	23.5	70
200	23.37(?)	23.5	70.5
225	33.70	23.5	71
250	46.97	23.5	71
275	1'02.30	23.5	71
300	1'21.41	23.25	71
325	1'44.46	23.25	71.5
350	2'14.24	23.25	71.5
375	2'49.63	22	71.5
400	3'35.54	22	71.75
410	4'03.70	22	71.75
435	5'13.72	22	71.75

Gate closed at 5'13.72  $\Rightarrow$

$$P_{\text{tunnel}} = 72.5 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

14.06.1999



# GS FLOW RATE 43 (video)

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$\text{GS in dyke} = 132.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$

Level (mm)	Time	$P_{\text{reservoir}} \text{ (mbar)}$	$P_{\text{tunnel}} \text{ (mbar)}$
150	3.85		
175	8.86		
200	14.77	24.5	90
225	21.55		91
250	29.33	24	91
275	38.87	24	91
300	50.12	24	91
325	1'02.74	24	91.5
350	1'18.26	23.75	91.5
375	1'35.37	23.75	91.5
400	1'56.60	22.5	91.5
410	2'08.79	22.5	91.5
435	2'37.27	22.5	91.5

Gate closed at 2'37.27  $\Rightarrow$

$$P_{\text{tunnel}} = 92 \text{ mbar}$$

$$P_{\text{reservoir}} = 21.75 \text{ mbar}$$

14.06.1999



$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$P_{\text{reservoir}} = 20.75 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$GS \text{ in dyke} = 132.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	3.50	27	-
175	-	-	-
200	13.12	25	100
225	-	-	-
250	26.38	24.5	100
275	34.59	24	100
300	43.79	24	100
325	54.82	24	100
350	1'07.51	24	100
375	1'22.72	24	100
400	1'38.43	24 $\rightarrow$ 22.5	100
410	1'48.70 / 1'50.70 (?)	22.5	100
435	2'11.62	22	100

Gate closed at 2'11.62  $\Rightarrow$

$$P_{\text{tunnel}} = 10 \text{ mbar}$$

$$P_{\text{reservoir}} = 21.75 \text{ mbar}$$

14.06.1999



# GS FLOW RATE 45 (video)

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

$$T = 18.9^\circ \text{C}$$

$$\text{GS in dyke} = 132.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$


Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	4.45	24	79
175	10.62	24	80
200	17.65	24	80
225	27.27	24	80
250	37.55	24	80
275	49.77	24	80
300	1'04.14	24	80.5
325	1'20.20	24	80.5
350	1'41.17	22.5	80.5
375	2'05.55	22.5	80.5
400	2'35.15	22.5	80.5
410	2'54.50	22.5	80.5
435	3'37.03	22.5	80.5

Gate closed at 3'37.03  $\Rightarrow$

$$P_{\text{tunnel}} = 81 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

14.06.1999



$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

$$T = 18.9^\circ \text{C}$$

$$GS \text{ in dyke} = 132.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow$

$$P_{\text{reservoir}} =$$

$$P_{\text{tunnel}} =$$

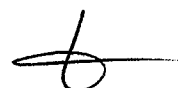
level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	5.39	23	58
175	14.07	23	58.5
200	25.44	23	59
225	38.98	23	59
250	54.74	23	59.5
275	1'15.53	23	59.5
300	1'41.19	23	59.5
325	2'13.97	23	59.5
350	2'58.75	23	60
375	4'01.46	23	60
400	5'37.17	23	60
410	7'04.04	23	60
430	10'12.58	23	60
435	12'45.79	23	60

Gate closed at 12'45.79  $\Rightarrow$

$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

14.06.1999



# GS FLOW RATE 47 (video)

$$P_{\text{tunnel}} = 40 \text{ mbar}$$

$$P_{\text{reservoir}} = 21 \text{ mbar}$$

$$T = 18.9^\circ \text{C}$$

GS in dyke = 132 mm? (GS still on walls)

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
150	10.93	22	39
175	28.28	22	39.5
200	51.89	22	40
225	1'24.64	22	40
250	2'09.86	22	40
275	3'27.06	22	40
300	5'58.88	22	40
314.5	11'16.45	22	40.5
317	16'54.79	22	40.5
317.5	24'09.66	22	40.5

$$\text{Gate closed at } 24'09.66 \Rightarrow \begin{cases} P_{\text{tunnel}} = 41 \text{ mbar} \\ P_{\text{reservoir}} = 21 \text{ mbar} \end{cases}$$

14.06.1999

*[Signature]*



# GS FLOW RATE 48 (video)

$$P_{\text{tunnel}} = 50 \text{ mbar}$$

$$P_{\text{reservoir}} = 30 \text{ mbar}$$

$$T = 18.3^\circ \text{C}$$

$$\text{GS in dyke} = 81 \text{ mm}$$

At atmospheric pressure,

$$\text{GS in dyke} = 259 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow \begin{cases} P_{\text{reservoir}} = \\ P_{\text{tunnel}} = \end{cases}$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	7.25	32	50
125	16.89	31.75	51
150	31.14	31.75	51
175	47.98	31.75	51.5
200	1'10.56	31.75	51.5
225	1'41.64	31.5	52
250	2'23.57	31.5	52
275	3'27.60	31.5	52
300	5'08.43	31.5	52
325	8'15.35	31.5	52.5
339.5	13'13.43	31.5	52.5
345	20'52.13	31.5	52.5
346	28'01.79	31.5	52.5
346	32'00.33	31.5	52.5

Gate closed at 32'00.33

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 53 \text{ mbar} \\ P_{\text{reservoir}} = 29.5 \text{ mbar} \end{cases}$$

# GS FLOW RATE 49 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 70 \text{ mbar} & T &= 18.5^\circ\text{C} \\ P_{\text{reservoir}} &= 29.25 \text{ mbar} & \text{GS in dyke} &= 77 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	5.74	34	70
125	11.98	34	70.5
150	19.89	33.5	71.
175	29.68	33.5	71.5
200	41.03	33.5	72
225	56.33	33	72
250	1'13.21	31.5	72
275	1'33.11	31.5	72.5
300	2'00.38	31.5	72.5
325	2'31.89	31.5	72.5
350	3'14.87	31.5	72.5
375	4'08.38	31.5	72.5
400	5'21.92	31.5	72.5
410	6'10.57	31.5	72.5
435	8'34.41	31.5	72.5

Gate closed at 8'34.41  $\Rightarrow$

$$\begin{aligned} P_{\text{tunnel}} &= 73.5 \text{ mbar} \\ P_{\text{reservoir}} &= 29.25 \text{ mbar} \end{aligned}$$

15.06.1999

$$P_{\text{tunnel}} = 90 \text{ mbar}$$

$$T = 18.6^\circ\text{C}$$

$$P_{\text{reservoir}} = 29.25 \text{ mbar} \quad \text{GS in dyke} = 76 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	4.23	35.5	90
125	8.54	35.5	90
150	13.28	35	90.5
175	19.62	34	91
200	26.46	34	91.5
225	34.75	34	91.5
250	44.89	33.5	92
275	56.35	32	92
300	1'09.96	32	92
325	1'26.15	32	92
350	1'44.17	32	92
375	2'05.90	32	92
400	2'32.71	32	92.5
410	2'48.68	32	92.5
435	3'27.27	32	92.5

Gate closed at 3'27.27  $\Rightarrow$   $P_{\text{tunnel}} = 93 \text{ mbar}$   
 $P_{\text{reservoir}} = 29.25 \text{ mbar}$

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$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$T = 18.6^\circ\text{C}$$

$$P_{\text{reservoir}} = 29.25 \text{ mbar}$$

$$\text{GS in dyke} = 74 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	4.27	36	100
125	7.80	36	100
150	12.47	36	100
175	17.63	34.5	100.5
200	23.95	34.5	100.5
225	31.89	34.5	101
250	40.57	32.75	101
275	50.42	32.75	101.5
300	1'01.88	32.75	102
325	1'14.79	32.75	102
350	1'30.38	32.75	102
375	1'47.86	32.75	102
400	2'09.48	32.5	102
410	2'22.32	32.5	102
435	2'49.52	32.5	102

Gate closed at 2'49.52  $\Rightarrow$

$$P_{\text{tunnel}} = 103 \text{ mbar}$$

$$P_{\text{reservoir}} = 29.25 \text{ mbar}$$

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$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$P_{\text{reservoir}} = 29.25 \text{ mbar}$$

$$GS \text{ in dyke} = 75 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	5.33	35	78
125	10.72	35	79
150	missed	35	79
175	25.46	35	79.5
200	35.45	34.5	79.5
225	47.13	32.5	80
250	1'00.27	32.5	80
275	1'16.76	32.5	80
300	1'36.36	32.5	80
325	1'59.21	32.5	80
350	2'28.87	32.5	80
375	3'04.84	32.5	80
400	3'49.65	30.75	80
410	4'15.95	30.75	80.5
435	5'24.11	30.75	80.5

Gate closed at 5'24.11  $\Rightarrow$   $P_{\text{tunnel}} = 80.75 \text{ mbar}$   
 $P_{\text{reservoir}} = 29.25 \text{ mbar}$

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$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$T = 18.8^\circ\text{C}$$

$$P_{\text{reservoir}} = 29.25 \text{ mbar}$$

$$\text{GS in dyke} = 74 \text{ mm}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	7.26	34	60
125	14.52	34	60
150	missed	34	60
175	36.02	34	60
200	50.65	33.5	60.5
225	1'09.96	31.5	60.5
250	1'33.58	31.5	61
275	2'03.75	31.5	61
300	2'43.44	31.5	61
325	3'37.28	31.5	61
350	5'04.20	31.5	61
375	7'42.70	31.5	61
392	12'54.07	31.5	61
400	18'34.62	31.5	61
399.5	25'00.00	31.5	61
399.5	26'35.45	31	61

Gate closed at 26'35.45  $\Rightarrow$   $P_{\text{tunnel}} = 61.5 \text{ mbar}$   
 $P_{\text{reservoir}} = 29.25 \text{ mbar}$

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$$\begin{aligned} P_{\text{tunnel}} &= 40 \text{ mbar} \\ P_{\text{reservoir}} &= 29.5 \text{ mbar} \end{aligned}$$

$$\begin{aligned} T &= 19.0^\circ\text{C} \\ \text{GS iz dyke} &= 73 \text{ mm} \end{aligned}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
100	11.99	32.25	39
125	26.92	32.25	39.5
150	47.27	32.25	39.5
175	1'15.78	32.25	40
200	1'59.69	32.25	40
225	3'14.58	32.25	40
250	6'17.83	32	40.5
257	10'04.81	32	40.5
259	14'20.81	32	40.5
260	19'50.07	32	40.5
260	23'58.14	32	40.5

Gate closed at 23'58.14  $\Rightarrow$   $\begin{aligned} P_{\text{tunnel}} &= 41 \text{ mbar} \\ P_{\text{reservoir}} &= 30.25 \text{ mbar} \end{aligned}$

15.06.1999



$$P_{\text{tunnel}} = 70 \text{ mbar}$$

$$T = 19.2^\circ\text{C}$$

$$P_{\text{reservoir}} = 40.75 \text{ mbar}$$

$$\text{GS in dyke} = 8 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	2.69	-	-
50	6.14	-	-
75	10.99	-	70
100	16.71	48	70
125	24.52	45.5	71
150	33.69	45.5	71
175	46.09	45.5	71.5
200	1'00.62	45	72
225	1'17.81	45	72
250	1'40.12	44.5	72
275	2'10.14	44.25	72
300	2'47.89	44	72
325	3'37.29	44	72
350	4'51.98	44	72.5
375	6'45.23	44	72.5
388	8'34.92	44	72.5
400	10'48.19	44	72.5
406.5	13'38.34	44	72.5
410	19'29.53	44	72.5
414	26'00.56	44	72.5
414	31'42.38	44	72.5

Gate closed at 31'42.38  $\Rightarrow$   $P_{\text{tunnel}} = 72.5 \text{ mbar}$   
 $P_{\text{reservoir}} = 40.5 \text{ mbar}$

$$\begin{aligned} P_{\text{tunnel}} &= 90.5 \text{ mbar} & T &= 19.3^\circ\text{C} \\ P_{\text{reservoir}} &= 40.75 \text{ mbar} & \text{GS in dyke} &= 6 \text{ mm (still some GS on walls)} \end{aligned}$$

Dyke valve closed - Gate opened at  $h_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	2.36	-	-
50	4.89	-	88
75	8.03	-	89
100	11.25	48	90
125	missed	48	90.5
150	21.31	48	91
175	28.07	44	91
200	35.91	44	91.5
225	45.69	44	91.5
250	56.59	44	92
275	1'09.75	44	92
300	missed	44	92
325	1'44.29	44	92
350	2'08.01	44	92
375	2'36.84	44	92
400	3'12.59	44	92
410	3'34.67	44	92
435	4'29.09	44	92

Gate closed at 4'29.09  $\Rightarrow$   $\begin{cases} P_{\text{tunnel}} = 92.5 \text{ mbar} \\ P_{\text{reservoir}} = 39.5 \text{ mbar} \end{cases}$

# GS FLOW RATE 57 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$T = 19.4^\circ\text{C}$$

$$P_{\text{reservoir}} = 40.5 \text{ mbar}$$

GS in dyke = 6 mm (GS still on walls)

Dyke valve closed - Gate opened at  $t_0 = 0$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	1.98	-	-
50	3.94	5.2	96
75	-	-	-
100	9.57	-	-
125	13.10	-	-
150	17.07	48	99
175	-	-	-
200	28.64	44.5	100
225	37.02	44.5	100
250	45.11	44.5	100
275	55.26	44.5	100
300	1'07.23	44.5	100.5
325	1'21.28	44.5	100.5
350	1'37.64	44.5	100.5
375	1'57.44	44.5	100.5
400	2'21.23	44	100.5
410	2'36.28	44	100.5
435	3'10.79	44	100.5

Gate closed at 3'10.79  $\Rightarrow$   $P_{\text{tunnel}} = 101 \text{ mbar}$   
 $P_{\text{reservoir}} = 40 \text{ mbar}$

15.06.1999

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$T = 19.4^\circ\text{C}$$

$$P_{\text{reservoir}} = 40.5 \text{ mbar}$$

$$\text{GS in dyke} = 6 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	2.38	-	76
50	-	-	-
75	8.28	48.5	79
100	-	-	-
125	17.28	-	-
150	23.85	45	80
175	-	-	-
200	41.43	45	81
225	53.55	45	81
250	1'08.16	44.75	81
275	1'25.40	44.75	81
300	1'46.50	44.5	81.5
325	2'12.71	44.25	81.5
350	2'46.84	44.25	81.5
375	3'31.37	44	81.5
400	4'38.21	44	81.5
410	5'22.72	44	81.5
425.5	6'22.68	44	81.5
435	7'37.94	44	81.5

Gate closed at 7' 37.94  $\Rightarrow$

$$P_{\text{tunnel}} = 82 \text{ mbar}$$

$$P_{\text{reservoir}} = 40.25 \text{ mbar}$$

15.06.1999



$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$T = 19.5^\circ\text{C}$$

$$P_{\text{reservoir}} = 40.5 \text{ mbar}$$

$$\text{GS in dyke} = 6 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	2.80	49.5	-
50	6.12	-	60
75	11.04	-	61
100	-	46.5	62
125	25.42	46	62
150	36.03	46	62.5
175	49.25	45.5	63
200	1'07.13	45.5	63
225	1'29.15	45.25	63
250	1'58.87	41.5	63
275	2'43.25	41.5	63
300	3'47.32	41.5	63
325	5'45.58	41.5	63.5
339	8'42.02	41.5	63.5
350	14'46.27	41.5	63.5
350	21'34.94	41.5	63.5

Gate closed at 21'34.94  $\Rightarrow$   $P_{\text{tunnel}} = 63.5 \text{ mbar}$   
 $P_{\text{reservoir}} = 39.75 \text{ mbar}$

$$\begin{aligned} P_{\text{tunnel}} &= 40 \text{ mbar} \\ P_{\text{reservoir}} &= 40.75 \text{ mbar} \end{aligned}$$

$$T = 19.6^\circ\text{C}$$

$$GS \text{ in dyke} = 6 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	4.61	46	38
50	11.63	46	39
75	23.49	46	40
100	39.79	43.5	40
125	1'04.35	43.5	40.5
150	1'45.29	43.5	40.5
166.5	2'33.18	43.5	40.5
175	3'07.71	43.5	40.5
185.5	4'36.73	43.5	41
191.5	6'33.60	43.5	41
194	9'17.02	43.5	41
195	16'24.92	43.5	41
195	21'52.03	43.5	41

Gate closed at 21'52.03  $\Rightarrow$  
$$\begin{aligned} P_{\text{tunnel}} &= 41 \text{ mbar} \\ P_{\text{reservoir}} &= 40.5 \text{ mbar} \end{aligned}$$

15.06.1999

$$P_{\text{tunnel}} = 50 \text{ mbar}$$

$$T = 19.6^\circ\text{C}$$

$$P_{\text{reservoir}} = 41 \text{ mbar}$$

$$\text{GS in dyke} = 6 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
25	3.48	48	48
50	8.81	48	49
75	16.58	45	50
100	26.52	44.75	50
125	40.28	44.75	50.5
150	53.24	44.75	51
175	1' 25.24	44.5	51
200	2' 04.70	44.25	51.5
225	3' 05.27	44	51.5
242.5	4' 24.78	44	51.5
250	5' 09.75	44	51.5
262	8' 11.32	44	51.5
266.5	12' 29.10	44	51.5
267	18' 53.74	44	51.5
267.5	21' 04.58	44	51.5
267.5	24' 36.08	44	51.5

Gate closed at 24' 36.08

$$\Rightarrow \begin{cases} P_{\text{tunnel}} = 52 \text{ mbar} \\ P_{\text{reservoir}} = 40.25 \text{ mbar} \\ T = 19.7^\circ\text{C} \end{cases}$$



At atmospheric pressure, GS in dyke = 259 mm

$$P_{\text{tunnel}} = 50 \text{ mbar} \quad T = 19.3^\circ\text{C}$$

$$P_{\text{reservoir}} = 10.5 \text{ mbar} \quad \text{GS in dyke} = 201 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0 \Rightarrow P_{\text{tunnel}} = 48 \text{ mbar}$  after 7"50

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	15.74	10.5	49
250	34.39	10.5	49
275	57.89	10.5	49.5
300	1' 27.19	10.5	49.5
325	2' 03.69	10.5	50
350	2' 51.42	10.5	50
375	3' 59.88	10.5	50
400	5' 39.02	10.5	50.25
410	6' 52.40	10.5	50.25
421	8' 09.84	10.5	50.25
433.5	10' 42.62	10.5	50.25
435	11' 40.16	10.5	50.25

Gate closed at 11' 40.16  $\Rightarrow$   $P_{\text{tunnel}} = 51 \text{ mbar}$   
 $P_{\text{reservoir}} = 10.5 \text{ mbar}$

16.06.1999



$$P_{\text{tunnel}} = 70.5 \text{ mbar} \quad T = 19.4^\circ \text{C}$$

$$P_{\text{reservoir}} = 10.5 \text{ mbar} \quad \text{GS in dyke} = 200 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	8.40	11.25	70
250	17.59	11.25	70
275	28.71	11.25	70.5
300	41.48	11.25	70.5
325	55.33	11.25	71
350	1'14.58	11.25	71
375	1'35.40	11.25	71
400	2'03.22	11.25	71
410	2'18.88	11.25	71
435	2'57.19	11.25	71

Gate closed at 2'57.19  $\Rightarrow$   $P_{\text{tunnel}} = 72.5 \text{ mbar}$   
 $P_{\text{reservoir}} = 11 \text{ mbar}$

16.06.1999

$$\left| \begin{array}{l} P_{\text{tunnel}} = 90 \text{ mbar} \\ P_{\text{reservoir}} = 11 \text{ mbar} \end{array} \right.$$

$$T = 19.5^\circ\text{C}$$

$$GS \text{ in dyke} = 1995 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	6.65	12	89
250	13.46	12	90
275	21.11	12	90
300	30.01	12	90
325	40.01	12	90.5
350	51.81	12	90.5
375	1'05.32	12	91
400	1'21.76	12	91
410	1'31.02	12	91
435	1'51.40	12	91

Gate closed at 1'51.40  $\Rightarrow$   $\left| \begin{array}{l} P_{\text{tunnel}} = 92 \text{ mbar} \\ P_{\text{reservoir}} = 11 \text{ mbar} \end{array} \right.$

16.06.1999

# GS FLOW RATE 65 (video)

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$T = 19.6^\circ\text{C}$$

$$P_{\text{reservoir}} = 10.75 \text{ mbar}$$

$$\text{GS in dyke} = 199.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	6.39	13.5	98
250	12.13	12.75	99
275	20.12	12.75	99
300	27.22	12.75	99
325	36.19	12.75	99.5
350	47.10	12.75	99.5
375	59.58	12.5	99.5
400	1' 13.20	12.5	100
410	1' 20.62	12.5	100
435	1' 37.21	12.5	100

Gate closed at 1' 37.21  $\Rightarrow$

$$P_{\text{tunnel}} = 101 \text{ mbar}$$

$$P_{\text{reservoir}} = 11 \text{ mbar}$$

16.06.1999

$$P_{\text{tunnel}} = 80 \text{ mbar}$$

$$P_{\text{reservoir}} = 11 \text{ mbar}$$

$$T = 19.7^\circ\text{C}$$

$$\text{GS in dyke} = 199.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	7.54	12	79
250	14.99	12	79.5
275	24.15	12	80
300	34.28	12	80
325	46.34	12	80
350	1'00.40	12	80
375	1'16.20	12	80.5
400	1'37.02	12	80.5
410	1'49.00	12	80.5
435	2'15.94	12	80.5

Gate closed at 2'15.94  $\Rightarrow$   $P_{\text{tunnel}} = 81.5 \text{ mbar}$   
 $P_{\text{reservoir}} = 11 \text{ mbar}$

16.06.1999



$$P_{\text{tunnel}} = 60 \text{ mbar}$$

$$T = 19.7^\circ \text{C}$$

$$P_{\text{reservoir}} = 11 \text{ mbar}$$

$$\text{GS in dyke} = 199.5 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow P_{\text{tunnel}} = 58 \text{ mbar after } 3'42''$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	9.80	11.25	59
250	20.59	11.25	59.5
275	34.63	11.25	60
300	50.72	11.25	60
325	1'09.39	11.25	60
350	1'34.11	11.25	60.5
375	2'03.64	11.25	60.5
400	2'42.79	11.25	60.5
410	3'10.54	11.25	60.5
435	4'17.98	11.25	60.5

Gate closed at 4'17.98  $\Rightarrow$

$$P_{\text{tunnel}} = 61.5 \text{ mbar}$$

$$P_{\text{reservoir}} = 11 \text{ mbar}$$

$$\begin{aligned} P_{\text{tunnel}} &= 40 \text{ mbar} \\ P_{\text{reservoir}} &= 11 \text{ mbar} \end{aligned}$$

$$T = 19.8^\circ\text{C}$$

$$\text{GS in dyke} = 199 \text{ mm}$$

Dyke valve closed - Gate opened at  $t_0 = 0$

$$\Rightarrow P_{\text{tunnel}} = 37.5 \text{ mbar after } 6''16$$

Level (mm)	Time	$P_{\text{reservoir}}$ (mbar)	$P_{\text{tunnel}}$ (mbar)
225	21.36	11	38
250	46.88	11	38
275	1'19.47	11	38
300	2'05.73	11	38
325	3'17.27	11	38.5
343.5	4'58.17	11	38.5
350	5'38.89	11	38.5
357.5	7'18.76	11	39
365	10'26.72	11	39
370	20'57.94	11	39
370.5	30'07.00	11	39

Gate closed at 30'07.00  $\Rightarrow$

$$\begin{aligned} P_{\text{tunnel}} &= 39 \text{ mbar} \\ P_{\text{reservoir}} &= 11 \text{ mbar} \\ T &= 19.9^\circ\text{C} \end{aligned}$$

16.06.1999



<u>Marks</u>	<u>Middle Real heights (mm)</u>	<u>Side</u>
25	25	-
50	50	50
75	75	-
100	100	100
125	125	-
150	149.5	150
175	174.5	-
200	199.5	200.5
225	224.5	-
250	249.5	249.5
275	274	-
300	299	300
325	323.5	-
350	349	349.5
375	373.5	-
400	398.5	399
410 (line)	410	410
435 (door)	435	435

16. 06. 1999



GS FLOW RATE 69 (video)

$$\begin{array}{|l} P_{\text{tunnel}} = 100 \text{ mbar} \\ P_{\text{reservoir}} = 11 \text{ mbar} \end{array}$$

$$T = 20.0^\circ \text{C}$$

$$\text{GS in dyke} = 198.5 \text{ mm}$$

Door opened at  $t_0 = 0$  (dyke valve and tunnel valve closed)

$P_{\text{tunnel}}$ (mbar)	Time
48	1.21
40	5.63
34	9.13
28	14.53
24	19.62
22	23.57
20	29.40
19	36.71
17	58.78
17	1'55.89
17	2'04.28

→ gate closed

Maximum GS level reached = 225 mm

16. 06. 1999



# GS FLOW RATE 70 (video)

$$\begin{array}{l|l} P_{\text{tunnel}} = 100 \text{ mbar} & T = 20.0^{\circ}\text{C} \\ P_{\text{reservoir}} = 30.5 \text{ mbar} & \text{GS in dyke} = 79 \text{ mm} \end{array}$$

Dyke valve and tunnel valve closed - Gate opened at  $t_0 = 0$

$P_{\text{tunnel}}$ (mbar)	Time	$P_{\text{reservoir}}$ (mbar)
40	1.57	
32	5.44	32
26	9.71	
22	14.50	
20	18.09	30
18	28.18	
17	42.61	
16.5	1' 31.42	

→ gate closed

Maximum GS level reached = 106 mm

# GS FLOW RATE 71 (video)

$$\begin{array}{l|l} P_{\text{tunnel}} = 100 \text{ mbar} & T = 20.1^{\circ}\text{C} \\ P_{\text{reservoir}} = 40 \text{ mbar} & \text{GS in dyke} = 20 \text{ mm} \end{array}$$

Dyke valve and tunnel valve closed - Gate opened at  $t_0 = 0$

$P_{\text{tunnel}}$ (mbar)	Time	$P_{\text{reservoir}}$ (mbar)
34	1.53	
24	7.16	
20	11.52	40
19	14.17	
18	17.39	
17	26.37	
16.5	1' 05.29	40
16.5	1' 10.22	

→ gate closed

Maximum GS level reached = 46 mm

16.08.1999

$$P_{\text{tunnel}} = 100 \text{ mbar}$$

$$T = 20.1^\circ\text{C}$$

$$P_{\text{reservoir}} = 20.25 \text{ mbar}$$

$$\text{GS in dyke} = 133.5 \text{ mm}$$

Dyke valve and tunnel valve closed - Gate opened at  $h_0 = 0$

$P_{\text{tunnel}} \text{ (mbar)}$	Time
40	3.31
34	6.48
30	9.18
26	13.17
22	18.79
20	23.07
19	28.24
18	34.58
17	55.66
16.5	1' 22.18
16.5	1' 58.02
16.5	2' 10.70

→ Gate closed

Maximum GS level reached = 158.5 mm

$$P_{\text{reservoir}} = 22.75 \text{ mbar}$$

16.06.1999



# GS FLOW RATE 73 (video)

$$\begin{aligned} P_{\text{tunnel}} &= 100 \text{ mbar} \\ P_{\text{reservoir}} &= \text{atmospheric} \end{aligned}$$

$$\begin{aligned} T &= 20.1^\circ \text{C} \\ \text{GS in dyke} &= 260.5 \text{ mm} \end{aligned}$$

Dyke valve and tunnel valve closed - Gate opened at  $h_0 = 0$

$P_{\text{tunnel}}$ (mbar)	Time
52	1.52
46	4.41
40	7.36
34	11.35
30	14.41
26	19.29
24	21.84
22	25.86
20	31.46
19	35.91
18	43.67
17	1' 02.77
16.5	1' 39.21
16.5	1' 44.32

→ gate closed

Maximum GS level reached = 286 mm

16.06.1999

SET 1

Reservoir at 10 mbar

Tunnel

70 - 90 - 40 - 60 - 80  
50 - 70 - 90 - 100 - 80 - 0

SET 2

Reservoir at 10 mbar

Tunnel

50 - 70 - 90 - 100 - 80 - 60 - 40 - 100  
 - 70  
 door pb

20 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40 - 100 (7)

0 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40 - 70

SET 3

(1) 10 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40

(2) 20 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40

(3) 30 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40

(1) 0 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40

(4) 40 mbar

50 - 70 - 90 - 100 - 80 - 60 - 40

Should do SET 1 at 0 mbar (71-73 in data)

\* expts keeping tunnel valve closed  
 100 mbar

10  
30  
40  
20  
0

16.06.1999

Checked first that both the dike and tunnel are levelled.

<u>Pressure gauges</u>	$P_1 = 992.7 - 992.8 \text{ mbar}$	atmospheric pressure
	$P_2 = 991.6 - 991.7 \text{ mbar}$	
	$P_3 = 992.1 - 992.2 \text{ mbar}$	

$$T = 20.4^\circ\text{C}$$

<u>GS in reservoir</u>	$h_r = H - \begin{array}{ l} 312.5 \\ 313.0 \\ 313.0 \end{array} = 172 \text{ mm}$
------------------------	--

<u>GS in dike</u>	$h_d = 110 \text{ mm}$
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At 17:00	$P_1 = 990.8 - 990.9 \text{ mbar}$	tunnel
	$P_2 = 992.6 - 992.7 \text{ mbar}$	dike
	$P_3 = 990.8 - 990.9 \text{ mbar}$	reservoir
	$T = 25.3 - \textcircled{25.4} - 25.5^\circ\text{C}$	

Gate N<sub>2</sub> pressure = 330 kPa

Pressure decreased in the tunnel	$P_1 = 950.0 - 950.1 \text{ mbar}$
	$P_2 = 992.6 - 992.7 \text{ mbar}$
	$P_3 = 990.8 - 990.9 \text{ mbar}$
	$T = 25.3^\circ\text{C}$

Before opening the tunnel gate

$$\begin{aligned} h_{\text{dike}} &= 110.0 \text{ mm} \\ P_1 &= 950.6 \text{ mbar} \\ P_2 &= 992.3 - 992.4 \text{ mbar} \\ P_3 &= 990.8 - 990.9 \text{ mbar} \\ T &= 24.8^\circ \text{C} \\ P_{N_2} &= 320 \text{ kPa} \end{aligned}$$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar) ← tunnel	$P_2$ (mbar) ← dike	$P_3$ (mbar) ← reservoir
220	2" 85	955.3		
	10.89	952.4	953.9	
	22.32	951.6	953.0	
270	36.79	951.1	952.6	990.9
340	47.79	950.8	952.3	
350	1' 03.00	950.6	952.1	
280	1' 14.32	950.5	951.9	
300	1' 36.10	950.4	951.8	
320	2' 09.35	950.3	951.7	
340	3' 02.42	950.1	951.6	
348.5	3' 38.95	950.1	951.5	
355.5	4' 18.95	950.1	951.5 - 951.6	$\left\{ \begin{array}{l} 990.9 \\ T = 24.7^\circ \text{C} \\ 990.9 - 991.0 \end{array} \right.$
362.5	5' 34.19	950.0 - 950.1	951.4 - 951.5	
365.5	6' 31.23	950.1	951.4 - 951.5	990.9 - 991.0
368	7' 40.60	950.0 - 950.1	951.4 - 951.5	$\left\{ \begin{array}{l} 990.9 - 991.0 \\ T = 24.7^\circ \text{C} \end{array} \right.$
369	8' 59.32	950.1 - 950.2	951.5 - 951.6	
369.5	10' 37.13	950.1 - 950.2	951.5 - 951.6	991.0 - 991.1
370.25	13' 38.60	950.2	951.6	$\left\{ \begin{array}{l} 991.1 \\ T = 24.6^\circ \text{C} \end{array} \right.$

$h_{dike}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)
-----------------	------	--------------	--------------	--------------

370.25	16'51.51	950.2-950.3	951.6-951.7	991.1
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$T = 24.6^\circ\text{C}$

370.25	18'14.57	950.3-950.2	951.6	991.1
--------	----------	-------------	-------	-------

$T = 24.6^\circ\text{C}$

370.25	20'11.51	950.3	951.6-951.7	991.1-991.2
--------	----------	-------	-------------	-------------

$T = 24.6^\circ\text{C}$

Gate closed at 20'34.79  
at 18H00  $\Rightarrow$

$P_1 = 950.3$  mbar

$P_2 = 951.2$  mbar

$P_3 = 991.1-991.2$  mbar

$T = 24.6^\circ\text{C}$

At 18H30

$P_1 = 991.3-991.4$  mbar

$P_2 = 992.4-992.5$  mbar

$P_3 = 991.2-991.3$  mbar

$T = 24.2^\circ\text{C}$

04.11.1999



# GS FLOW RATE 75

At atmospheric pressure

$h_s = 109 \text{ mm}$  (still some GS on walls)

$P_1 = 991.4 \text{ mbar}$

$P_2 = 992.5 \text{ mbar}$

$P_3 = 991.4 \text{ mbar}$

Pressure lowered in the tunnel

$P_1 = 970.5 - 970.6 \text{ mbar}$

$P_2 = 992.4 - 992.5 \text{ mbar}$

$P_3 = 991.5 - 991.6 \text{ mbar}$

$T = 24.1 - 24.2^\circ \text{C}$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$
-------------------------------	------	---------------------	---------------------	---------------------

	2.83	973.5	974.2	991.5
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140	12.67	971.7	972.7	
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160	22.43	971.1	972.2	991.5 - 991.6
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180	35.70	970.8 - 970.7	971.7 - 971.8	991.5 - 991.6
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200	57.20	970.4	971.4 - 971.5	991.5 - 991.6
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$T = 24.1^\circ \text{C}$

220	1' 28.39	970.0 - 970.1	971.1 - 971.2	991.6
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233.5	2' 11.67	969.9	971.0	991.6
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240	2' 49.23	969.8 - 969.9	970.9 - 971.0	991.6
-----	----------	---------------	---------------	-------

244.5	3' 34.58	969.8/9	970.9	991.6
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248.25	4' 49.27	969.7/8	970.8/9	991.6/7
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249.25	6' 20.64	-	970.7/8	991.6
--------	----------	---	---------	-------

249.5	8' 05.96	-	-	991.6/7
-------	----------	---	---	---------

249.75	10' 06.20	-	970.8	-
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-	12' 10.55	969.8/9	970.8/9	991.7/8
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-	13' 50.17	-	-	991.7
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-	15' 02.64	-	-	-
---	-----------	---	---	---

-	15' 20.80	-	-	-
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$T = 24.1^\circ \text{C}$

Gate closed at 15' 20.80 =>

$$P_1 = 969.112 \text{ mbar}$$

$$P_2 = 970.516 \text{ mbar}$$

$$P_3 = 991.718 \text{ mbar}$$

Once the pump is switched off

$$P_1 = 991.718 \text{ mbar}$$

$$P_2 = 992.718 \text{ mbar}$$

$$P_3 = 991.819 \text{ mbar}$$

$$T = 24^\circ \text{C}$$

04.1.1999

# GS FLOW RATE 76

At atmospheric pressure

$$h_D = 110 \text{ mm}$$

$$P_1 = 996.1/2 \text{ mbar}$$

$$P_2 = 995.5/6 \text{ mbar}$$

$$P_3 = 995.7/8 \text{ mbar}$$

$$T = 21.9^\circ \text{C}$$

Pressure lowered in the tunnel

$$P_1 = 934.8/9 \text{ mbar}$$

$$P_2 = 995.7 \text{ mbar}$$

$$P_3 = 995.8 \text{ mbar}$$

At 10400

$$h_D = 110.5 \text{ mm}$$

$$P_1 = 935.1/2 \text{ mbar}$$

$$P_2 = 995.8/9 \text{ mbar}$$

$$P_3 = 995.8/9 - 996.0 \text{ mbar}$$

$$T = 21.4^\circ \text{C}$$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$
	3.17	937.7		
160	11.89	933.2	932.8	
200	23.32	932.5	932.2	995.9
240	38.45	932.0	931.8	995.9
260	48.32	931.8	931.6	995.9
280	59.19	931.6	931.4	995.8
300	1' 12.26	931.5/6	931.3	995.9
320	1' 27.10	931.4/5	931.1/2	995.9
340	1' 44.23	931.3/4	931.1	995.9/996.0
360	2' 04.42	931.2	931.0	995.9
380	2' 28.19	931.1/2	930.9/931.0	995.9
400	2' 56.01	931.0/1	930.9	995.9/996.0
410 410	3' 14.01	931.0/1	930.9	995.9/996.0
420	3' 30.73	931.0	930.8	996.0

05.11.1995

Gate closed at 4' 02.79 when GS reached its bottom (435)

↳  $P_1 = 930.6/7 \text{ mbar}$   
 $P_2 = 995.9/996.0 \text{ mbar}$   
dike valve opened  
 $T = 21.4^\circ\text{C}$

At 10H30  $P_1 = 995.5/6 \text{ mbar}$   
 $P_2 = 996.7/8 \text{ mbar}$   
 $P_3 = 996.1/2 \text{ mbar}$   
 $T = 21.3^\circ\text{C}$

05.11.1999

# GS FLOW RATE 77

At 11430  $h_{dike} = 108.5 \text{ mm}$  (still some GS on wall)  
 $P_1 = 996.415 \text{ mbar}$   
 $P_2 = 997.516 \text{ mbar}$  atmospheric pressure  
 $P_3 = 996.2 \text{ mbar}$   
 $T = 23^\circ\text{C}$

Tunnel pressure lowered  
 $P_1 = 986.516 \text{ mbar}$   
 $P_2 = 997.415 \text{ mbar}$   
 $P_3 = 996.2 \text{ mbar}$

Stopwatch problem. Reset experiment.

After a few minutes  $h_{dike} = 109 \text{ mm}$   
 $P_1 = 986.617 \text{ mbar}$   
 $P_2 = 997.617 \text{ mbar}$   
 $P_3 = 996.112 \text{ mbar}$   
 $T = 23.3^\circ\text{C}$

Dike valve closed and gate opened at  $t = 0$

$h_{dike} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	
	2.60	987.8	988.8	996.2	
120	12.45	987.2	988.5	996.2	
140	43.04	987.0	988.2	996.2	
56 156	1'32.48	986.7	988.0	996.1	
160	1'52.92	986.7	988.0	996.112	
165	2'31.19	986.617	987.9	996.1	$T = 23.5^\circ\text{C}$
169.25	4'03.26	986.617	987.9/988.0	996.112	
170.5	5'11.42	986.6	987.9/988.0	996.0/996.1	
171	8'01.45	986.6	987.8/9	996.1	
171	9'52.07	986.516	987.9	996.0/1	
171	12'09.79	986.516	987.9	996.0/1	
171	13'13.86	986.516	987.9	996.0	
171	15'08.60	986.516	987.9/988.0	996.0/1	05.11.19.3

Gate closed at 15' 30. 32

↳

$$P_1 = 986.516 \text{ mbar}$$

$$P_2 = 987.516 \text{ mbar}$$

$$P_3 = 996.011 \text{ mbar}$$

$$T = 23.7^\circ\text{C}$$

05.11.1999

# GS FLOW RATE 78

At atmospheric pressure

$h_d = 109 \text{ mm}$   
 $P_1 = 995.819 \text{ mbar}$   
 $P_2 = 997.314 \text{ mbar}$   
 $P_3 = 995.718 \text{ mbar}$   
 $T = 24.0^\circ\text{C}$

Tunnel pressure lowered

$P_1 = 965.2/3 \text{ mbar}$   
 $P_2 = 997.314 \text{ mbar}$   
 $P_3 = 995.7 \text{ mbar}$

At 12H15, dike valve closed and gate opened ( $t = 0$ )

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T(^{\circ}\text{C})$
120	3.85				
140	10.03	966.0	967.4	995.7	
160	17.94	965.2	966.7	-	
180	27.57	964.617	966.2	-	
200	40.37	964.3	965.7	-	
220	55.22	963.9/964.0	965.5	-	
240	1'15.59	963.5/6	965.1/2	-	23.9
260	1'44.03	963.4	964.9	-	
275.75	2'15.31	963.3	964.8	-	
280	2'28.07	963.2	964.7	-	
289.25	2'54.25	963.0	964.6	-	23.9
300	3'41.88	963.0	964.5/6	995.6	
307.5	4'25.91	962.9	964.4	995.6	23.9
313	5'32.34	962.819	964.4	995.7	
316.5	6'38.41	962.718	964.314	995.617	
318.5	7'58.09	962.7	964.3	995.6	24.1
320	9'29.03	962.6	964.2	-	24.1
321	11'04.41	962.5/6	964.2	995.5/6	
321	12'53.72	962.415	964.1	995.415	24.1
321	14'52.22	962.5/6	964.1	995.5	24.1

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^{\circ}\text{C}$ )
3.21	16'15.37	962.415	964.1	995.415	24.1
3.21	17'24.85	962.4	-	-	24.1
3.21	18'39.59	962.4	-	995.4	24.1
3.21	20'08.34	962.314	964.011	995.415	24.2

Gate closed at 20'08.34

$$\begin{aligned} \Rightarrow & \left| \begin{aligned} P_1 &= 961.415 \text{ mbar} \\ P_2 &= 963.617 \text{ mbar} \\ P_3 &= 995.314 \text{ mbar} \\ T &= 24.2^{\circ}\text{C} \end{aligned} \right. \end{aligned}$$

05.11.1999



# GS FLOW RATE 79

At atmospheric pressure

$$\begin{aligned}h_d &= 109 \text{ mm} \\P_1 &= 994.718 \text{ mbar} \\P_2 &= 996.8 \text{ mbar} \\P_3 &= 994.617 \text{ mbar} \\T &= 25.3^\circ\text{C}\end{aligned}$$

At 13 H 45, tunnel pressure lowered

$$\begin{aligned}P_1 &= 989.213 \text{ mbar} \\P_2 &= 996.718 \text{ mbar} \\P_3 &= 994.6 \text{ mbar} \\T &= 25.1^\circ\text{C}\end{aligned}$$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^\circ\text{C}$ )
	8.83	989.7	991.8	994.7	25.1
120	19.86	989.6	991.7	994.6	
127.5	34.23	989.5	991.6	994.6	25.2
134	56.73	989.4	991.5	994.6	25.2
140	1'36.01	989.3/4	991.4/5	-	25.3
142	2'09.07	-	-	-	25.3
143.25	3'01.76	-	-	-	25.4
143.5	4'26.48	989.3	991.4	-	25.4
143.75	5'37.73	-	-	994.6	-
144	6'36.54	989.2	991.3/4	994.5/6	25.4
144.25	7'37.89	989.2/3	-	-	-
144.25	8'51.79	-	-	-	-
144.25	10'07.57	989.1/2	991.3	994.5	-
144.25	10'30.38	-	991.3	994.5/6	-

Gate closed at 10'30.38 (13 H 55)  $\Rightarrow$

$$\begin{aligned}P_1 &= 989.112 \text{ mbar} \\P_2 &= 990.819 \text{ mbar} \\P_3 &= 994.516 \text{ mbar}\end{aligned}$$

05.11.1999



# GS FLOW RATE 80

At atmospheric pressure

$$\begin{aligned} h_d &= 110 \text{ mm} \\ P_1 &= 994.1/2 \text{ mbar} \\ P_2 &= 996.0/1 \text{ mbar} \\ P_3 &= 994.1/2 \text{ mbar} \\ T &= 25.5^\circ\text{C} \end{aligned}$$

At 15H00, tunnel pressure lowered

Videotape 2

$$\begin{aligned} P_1 &= 942.9/943.0 \text{ mbar} \\ P_2 &= 995.8/9 \text{ mbar} \\ P_3 &= 994.0/1 \text{ mbar} \\ T &= 25.1^\circ\text{C} \end{aligned}$$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)
------------------------	------	--------------	--------------	--------------

140	5.03	946.8	947.5	
180	12.13	?	?	
200	16.28	942.8	944.5	
220	21.41	942.3	944.0	
240	27.72	941.7	943.4	994.1
260	34.97	941.3	943.0	994.1
280	43.16	941.0	942.8	994.1
300	52.69	940.7	942.5	994.1
320	1'04.63	940.4/5	942.1/2	994.0/1
340	1'19.13	940.2/3	942.0	994.0/1
360	1'37.57	939.9/940.0	941.7/8	994.0/1
380	2'00.97	939.8/9	941.6	994.0/1
400	2'33.78	939.7	941.5	994.0/1
410	2'55.50	939.6	941.3/4	994.0
420	3'24.22	939.5	941.2/3	994.0/1
?	4'13.16	939.4	941.2	
435	4'25.34			

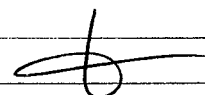
$T = 25.0^\circ\text{C}$

Gate closed at 4'25.34 when GS reached its bottom - Dike valve opened

$$\begin{aligned} \Rightarrow P_1 &= 935.6/7 \text{ mbar} \\ P_2 &= 995.4/5 \text{ mbar} \\ P_3 &= 993.9/994.0 \text{ mbar} \\ T &= 25.0^\circ\text{C} \end{aligned}$$

at 15H05

05.11.1999



# GS FLOW RATE 81

At atmospheric pressure

$$\begin{aligned} h_D &= 110 \text{ mm} \\ P_1 &= 993.7/8 \text{ mbar} \\ P_2 &= 994.5/6 \text{ mbar} \\ P_3 &= 993.7/8 \text{ mbar} \\ T &= 24.2^\circ\text{C} \end{aligned}$$

Tunnel pressure lowered

$$\begin{aligned} P_1 &= 978.3/4 \text{ mbar} \\ P_2 &= 994.5 \text{ mbar} \\ P_3 &= 993.8/9 \text{ mbar} \\ T &= 24.1^\circ\text{C} \end{aligned}$$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
120	6.29	980.0	980.7	993.8	24.1
140	18.89	979.3	980.0	993.9	
160	37.89	978.9	979.6	993.9	
180	1'08.05	978.5	979.4	993.9	
193	1'45.39	978.4	979.1/2	993.9	
200	2'30.05	978.3/4	979.1	993.8/9	
204.5	3'14.36	978.2/3	979.1	993.8	
207	4'27.02	978.2/3	979.0/1	993.8/9	24.1
208	5'36.93	978.2/3	979.0	993.8/9	
208.75	6'35.73	978.1/2	979.0	993.8/9	24.0
208.75	7'44.70	978.2	979.0	993.9	
208.75	8'53.80	978.1/2	978.9/979.0	993.8/9	24.0
208.75	10'03.23	978.2/3	978.9/979.0	993.8/9	24.0
208.75	10'30.05	978.2			

Gate closed at 10'30.05  $\Rightarrow$   
~ 16H30

$$\begin{aligned} P_1 &= 978.0/1 \text{ mbar} \\ P_2 &= 978.4/5 \text{ mbar} \\ P_3 &= 993.8/9 \text{ mbar} \end{aligned}$$

At 16H40

$$\begin{aligned} P_1 &= 993.7/8 \text{ mbar} \\ P_2 &= 994.4 \text{ mbar} \\ P_3 &= 993.9/994.0 \text{ mbar} \\ T &= 23.9^\circ\text{C} \end{aligned}$$

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*[Signature]*

# GS FLOW RATE 82

At atmospheric pressure

$h_d = 109.5 \text{ mm}$   
 $P_1 = 993.8/9 \text{ mbar}$   
 $P_2 = 994.2/3 \text{ mbar}$   
 $P_3 = 993.9/994.0 \text{ mbar}$   
 $T = 23.7^\circ\text{C}$

At 17H00, tunnel pressure lowered

$P_1 = 969.3/4 \text{ mbar}$   
 $P_2 = 994.1/2 \text{ mbar}$   
 $P_3 = 993.9 \text{ mbar}$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
120	4.17	971.8	972.1		
140	12.01	971.0	971.5	993.9	
160	21.54	970.4	970.9	993.9	
180	34.10	970.0/1	970.4/5	-	23.7
200	52.73	969.7/8	970.1/2	-	-
220	1' 18.95	969.4/5	969.9/970.0	993.9/994.0	
234	1' 44.23	969.3/4	969.8/9	-	
240	2' 02.32	969.3/4	969.7/8	993.9	23.7
249.5	2' 33.76	969.2/3	969.6/7	993.9/994.0	
255.5	3' 04.32	-	-	994.0	23.7
260	3' 45.69	969.1/2	969.6	993.9/994.0	
263	4' 34.86	969.2	969.6/7	-	23.7
265.5	5' 52.32	969.1/2	969.6/7	993.9/994.0	
266.5	7' 03.69	969.2	969.6	993.9/994.0	23.7
267	8' 28.45	969.1/2	969.6/7	993.9	
267	9' 44.23	969.2	969.6/7	993.9	23.6/7
267	10' 43.57	969.2/3	969.6/7	993.9	23.7
267	12' 00.42	969.2/3	969.6/7	993.9/994.0	23.6
267	12' 30.26				

Gate closed at 12' 30.26  $\Rightarrow$   
17H12

$P_1 = 968.5/6 \text{ mbar}$   
 $P_2 = 969.1/2 \text{ mbar}$   
 $P_3 = 993.9/994.0 \text{ mbar}$

05.11.1999

*[Signature]*

# GS FLOW RATE 83

At atmospheric pressure  
( $P_1$  already lowered)

$$\begin{aligned} h_d &= 109 \text{ mm} \\ P_1 &= 959.9 / 960.0 \text{ mbar} \\ P_2 &= 994.2 \text{ mbar} \\ P_3 &= 993.9 / 994.0 \text{ mbar} \\ T &= 23.4^\circ\text{C} \end{aligned}$$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^\circ\text{C}$ )
------------------------	------	--------------	--------------	--------------	--------------------------

120	3.04	963.5	963.2		
140	8.17	961.9	962.2		
160	14.35	961.3	961.5	993.9	
180	22.42	960.9	961.2	993.9	
200	31.95	960.5	960.8	993.9/994.0	
220	43.92	960.2/3	960.5/6	993.9	
240	59.95	960.0/1	960.3	993.9	
260	1'22.23	959.8	960.1	-	23.5
280	1'54.13	959.7	960.0	993.9	23.4
291.25	2'18.04	959.6	959.8/9	993.9	23.5
300	2'47.13	959.5/6	959.8/9	993.9/994.0	23.5
310	3'25.42	959.4/5	959.8	-	23.5
315.75	4'01.45	959.4/5	959.7/8	-	23.5
320	4'46.38	959.5/6	959.7/8	993.9	23.4
323.75	5'33.79	959.5	-	-	-
326	6'21.01	-	-	993.9/994.0	-
327.75	7'24.45	-	-	-	-
328.25	8'29.54	959.5/6	-	-	-
329.25	9'33.42	959.6	959.8	-	-
329.25	10'46.73	959.5/6	959.8	-	-
329.25	12'00.04	959.6/7	959.8/9	-	-

Video stopped at 12'23.92

329.25	13'17.69	959.7	959.8/9	994.0	23.4
329.25	15'35.04	-	959.9/960.0	993.9/994.0	-
329.25	16'00.04				

Gate closed at 16'00.04  $\Rightarrow$

$$\begin{aligned} P_1 &= 959.3/4 \text{ mbar} \\ P_2 &= 959.3/4 \text{ mbar} \\ P_3 &= 994.0/1 \text{ mbar} \end{aligned}$$

At 17H55

$$\begin{aligned} P_1 &= 994.1 \text{ mbar} \\ P_2 &= 994.1/2 \text{ mbar} \\ P_3 &= 994.0/1 \text{ mbar} \end{aligned}$$

05.11.1999

At atmospheric pressure

$h_D = 110 \text{ mm}$   
 $P_1 = 994.3/4 \text{ mbar}$   
 $P_2 = 992.9/993.0 \text{ mbar}$   
 $P_3 = 993.9/994.0 \text{ mbar}$   
 $T = 19.8^\circ\text{C}$

Tunnel pressure lowered

$P_1 = 948.4/5 \text{ mbar}$  ASG1  
 $P_2 = 993.0/1 \text{ mbar}$  ASG2  
 $P_3 = 993.9/994.0 \text{ mbar}$  ASG3

Dike valve closed and gate opened at  $t = 0$ 

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
120	4.20	949.7	948.4	994.0	
140	10.05	949.2	948.0		
160	18.27	948.8	947.6		
180	27.80	948.5/6	947.4		
200	39.83	948.3/4	947.1		
220	53.23	948.1	947.0	994.0	19.9
240	1'10.05	948.0	946.8	993.9	
260	1'28.67	947.9	946.7	994.0	19.9
280	1'58.61	947.7/8	946.5/6	994.0	
291.25	2'10.14	947.7	946.5/6		
300	2'23.67	947.6/7	946.5		
312.75	2'45.49	947.6	946.4/5	994.0	
320	3'02.61	947.6	946.4	993.9	
330.75	3'26.61	947.5/6	946.4	994.0	19.9
340	3'54.17	947.5	946.4	994.0	
348.25	4'18.93	947.5	946.3	994.0	
354.5	4'43.64	947.5	946.3/4	994.0	
360	5'08.80	947.5	946.3	994.0/1	
366	5'33.77	947.4/5	946.3/4	994.0	19.9
371.25	6'03.61	947.3/4	946.3	994.0	
376	6'32.17	947.3/4	946.2/3	993.0	
380	7'06.05	947.3/4	946.2/3	994.0/1	19.9
384.75	7'45.33	947.3/4	946.3	994.0	19.9
389.5	8'35.02	947.3/4	946.2/3	994.0	
391.75	9'09.96	947.3/4	946.2	994.0	
394.25	10'00.17	947.1/2	946.0/1	994.0	19.9
396.75	10'42.77	947.1/2	946.1/2	994.0	
398.25	11'33.89	946.8	945.8	994.0	
400	12'11.67	946.8/9	945.8	994.0	

Pump stopped  
 for ~3 s!

Pump stopped  
 again for ~3 s!

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ (°C)
401.5	12' 30.00	947.5/6	946.5/6	994.0	→ pump stopped for ~3s
402.5	13' 11.39	947.1/2	946.2	994.0	
403.5	13' 48.52	947.2	946.2/3	994.0	
404.75	14' 34.46	947.2/3	946.3	994.0	→ pump stopped for ~3s
404.75	15' 29.33	947.1/2	946.2	994.0	
406	16' 22.93	PUMP STOPPED AGAIN			
406	17' 24.80	947.0/1	946.1/2	994.0/1	
407.25	18' 00.83	947.1	946.1/2	994.1	→ pump stopped for ~3s
408.25	19' 11.61	947.0/1	946.1	994.0/1	
		Pump stopped for ~3s			20 °C
408.25	20' 59.33	947.0	946.1/2	994.0/1	
408.25	21' 17.93				

Gate closed at 21' 17.93  $\Rightarrow$

$P_1 = 946.9/947.0$ mbar
$P_2 = 946.0/1$ mbar
$P_3 = 994.0/1$ mbar
$T = 20^\circ\text{C}$

At 1100

$P_1 = 994.3/4$ mbar
$P_2 = 994.1/2$ mbar
$P_3 = 993.9/994.0$ mbar
$T = 20.5^\circ\text{C}$
$h_D = 108.5$ mm (still some GS on walls)
$h_R = H - 315.5 = 169.5$ mm

$\Rightarrow$  more GS added in the set-up for the next series of expts

# GS FLOW RATE 85

At atmospheric pressure 13400	$P_1 = 992.3/4 \text{ mbar}$	ASG1
	$P_2 = 993.5/6 \text{ mbar}$	ASG2
	$P_3 = 992.0/1 \text{ mbar}$	ASG3

$$T = 22.1^\circ\text{C}$$

$$\text{GS in reservoir} = h_r = 4 - 179.5 = 305.5 \text{ mm}$$

$$\text{GS in dike} = h_d = 243.5 \text{ mm}$$

Tunnel pressure lowered at 13405	$P_1 = 981.6/7 \text{ mbar}$
	$P_2 = 993.4/5 \text{ mbar}$
	$P_3 = 992.0 \text{ mbar}$
	$T = 22.2/3^\circ\text{C}$

Dike valve closed, gale opened at  $t=0$

$h_{\text{dike}} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
	8.21	982.2	983.3	992.0	
253.5	17.03	982.0	983.3	992.0	
260	32.90	981.9/982.0	983.1/2	992.0	22.3
267.5	52.56	981.8/3	983.1	992.0	22.3
275.5	1'14.06	981.8	983.0	-	22.2
280	1'31.90	981.8	982.9/983.0	-	-
285.5	1'53.43	981.7	982.9	-	-
291	2'25.37	981.6/7	982.9	-	-
295	2'51.43	981.6	982.8	991.9/992.0	22.3
298.5	3'20.68	981.5/6	982.7/8	991.9	22.2
301.25	3'53.40	981.4/5	982.7/8	991.9/992.0	22.3
304	4'31.03	981.4/5	982.6	991.9	22.3
306	5'07.40	981.3/4	982.5/6	991.8/9	22.2
308	5'56.43	981.2/3	982.5	991.7/8	22.3
309.25	6'51.74	981.2/3	982.4/5	991.7/8	22.3
310.25	7'55.53	981.2	982.3/4	991.7/8	22.3
311.5	9'06.43	981.1/2	982.3	991.7	22.3
311.5	10'37.33	981.0/1	982.2/3	991.6/7	22.3

Videos stopped at 11'25.49

312.25	11'58.40	981.0/1	982.1/2	991.6	22.3
312.25	13'18.09	980.9/981.0	982.1/2	991.6	-
312.25	14'02.62	980.9/981.0	982.0/1	991.6	-
312.25	15'08.81	980.9/981.0	982.0/1	991.6	-

Gale closed at 15'08.81  $\Rightarrow$

$P_1 = 980.2/3 \text{ mbar}$
$P_2 = 981.5 \text{ mbar}$

08.11.1999



# GS FLOW RATE 86

At atmospheric pressure

$$\begin{aligned} P_1 &= 990.2/3 \text{ mbar} \\ P_2 &= 990.6/7 \text{ mbar} \\ P_3 &= 990.1/2 \text{ mbar} \\ T &= 22.5^\circ\text{C} \\ h_D &= 243.5 \text{ mm} \end{aligned}$$

Tunnel pressure lowered

$$\begin{aligned} P_1 &= 970.3/4 \text{ mbar} \\ P_2 &= 990.6/7 \text{ mbar} \\ P_3 &= 990.0/1 \text{ mbar} \\ T &= 22.5^\circ\text{C} \end{aligned}$$

Dike valve closed and gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^\circ\text{C}$ )
	2.07	973.5	973.5		
260	15.79	971.5	971.9	990.1/2	
280	38.69	971.1/2	971.5/6	990.1	
300	1'08.32	970.9/971.0	971.4	-	
308.5	1'25.01	970.8/9	971.2	990.0/1	
320	1'50.69	970.7	971.1/2	990.0/1	22.5
329	2'15.79	970.6	971.1	990.0	-
340	3'03.17	970.5/6	971.0	990.1	-
346.25	3'27.03?	970.4/5	971.0	990.0/1	-
351.75	4'04.45	970.4	970.9/971.0	-	-
355.25	4'36.38	-	970.9/971.0	990.1	-
358.5	5'10.13	-	970.8/9	-	-
362	5'55.29	-	970.8/9	-	-
364.5	6'48.95	970.3/4	970.8/9	990.0/1	22.5
366.25	7'38.01	970.3/4	-	-	-
367.75	8'21.07	970.3	-	-	-
368.25	9'18.89	970.2/3	970.7/8	-	-
369	10'08.32	video stopped			
370	10'29.73	970.2/3	970.7/8	990.0	22.5
370.25	11'30.69	970.1/2	-	-	-
370.25	12'39.23	970.1/2	-	-	-
370.5	13'47.42	-	-	989.9/990.0	-
370.5	14'49.63	-	970.6/7	989.8/9	-
370.5	26'38.32	970.0	970.5/6	989.8	-
370.5	26'58.67	gate closed			

$$\begin{aligned} \hookrightarrow P_1 &= 968.6 \text{ mbar} \\ P_2 &= 969.9 \text{ mbar} \\ P_3 &= 989.7/8 \text{ mbar} @ 15H10 \end{aligned}$$

# GS FLOW RATE 87

At 15H40, at atmospheric pressure

$P_1 = 989.415 \text{ mbar}$   
 $P_2 = 989.9 \text{ mbar}$   
 $P_3 = 989.415 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$   
 $h_d = 243.5 \text{ mm}$

Tunnel pressure lowered

$P_1 = 958.819 \text{ mbar}$   
 $P_2 = 989.819 \text{ mbar}$   
 $P_3 = 989.415 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$

Dike valve closed and gate opened at  $t=0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
	4.01	961.0	961.0		
260	9.45	959.8	960.2	989.4	
280	21.45	959.3/4	959.7/8	989.415	
300	36.48	959.1	959.5/6	989.415	22.6
320	53.54	958.9	959.3	989.4	
340	1'16.01	958.6/7	959.1	989.3/4	
360	1'46.19	958.4/5	958.8/9	989.4	22.6
372	2'06.95	958.3/4	958.8/9	-	-
380	2'24.89	958.3	958.7/8	-	-
388.25	2'49.01	958.3	958.7	989.3/4	-
400	3'26.04	958.2	958.6/7	989.415	-
407	3'52.17	958.1	958.6	989.3/4	-
410	4'09.26	958.1/2	958.5/6	989.4	-
420	5'01.51	958.1	958.5/6	-	-
424.25	5'41.60	958.1	-	-	-
428.5	6'19.29	958.0/1	958.4/5	989.3/4	22.6
431.5	7'02.95	-	958.5/6	989.415	-
434	7'36.01	-	958.4/5	989.4	-
435	8'26.86	-	-	-	-

Gate closed at 8'26.86 when GS reached the tunnel entrance  
Dike valve immediately opened

$\hookrightarrow$   $P_1 = 956.0/1 \text{ mbar}$   
 $P_2 = 989.8 \text{ mbar}$   
 $P_3 = 989.3/4 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$

@ ~ 15H50/15H55

End of videotape 2

# GS FLOW RATE 88

At 16 H25, at atmospheric pressure

Videotape 3

$P_1 = 989.2 \text{ mbar}$   
 $P_2 = 989.4/5 \text{ mbar}$   
 $P_3 = 989.2 \text{ mbar}$   
 $T = 22.4^\circ \text{C}$   
 $h_D = 243 \text{ mm}$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ \text{C})$
243	0	984.1/2	989.4/5	989.1/2	22.4
NONE	7.04	984.5	984.8	-	-
249.5	19.35	984.4	984.7	-	-
254.75	42.57	-	984.7/8	-	-
260	1'08.01	-	984.6/7	989.2	22.5
263	1'31.92	984.3/4	-	-	22.4
266.75	2'04.69	-	984.6	989.1/2	-
269.25	2'41.38	-	984.5/6	-	-
271.25	3'25.60	-	-	-	-
272.75	4'05.17	984.2/3	-	-	-
273.5	4'48.07	-	-	-	-

Video stopped at 5'12.79

273.5	5'35.79	984.2/3	984.4/5	989.1/2	22.4
274.5	7'01.89	-	984.5/6	-	-
274.5	9'02.17	-	984.4/5	-	-
275	11'46.19	984.2	984.4/5	989.1	22.5
275	13'29.42	-	-	989.1/2	-
275	14'17.01	984.2/3	984.4	989.1	-
275	15'17.07	984.2	984.4/5	-	-
275	15'42.63	-	-	-	-

Gate closed at 15'42.63  $\Rightarrow$

$P_1 = 984.1/2 \text{ mbar}$   
 $P_2 = 983.8/9 \text{ mbar}$   
 $P_3 = 989.1 \text{ mbar}$

08.11.1999

GS FLOW RATE 89

At 17H00, at atmospheric pressure

$P_1 = 989.1/2 \text{ mbar}$   
 $P_2 = 989.3/4 \text{ mbar}$   
 $P_3 = 989.0/1 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$   
 $h_D = 243.5 \text{ mm}$

$h_{\text{dike}} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
243.5	0	973.7/8	989.4/5	989.0/1	22.6
249.75	7.10	974.6	974.8		
260	18.51	974.4	974.7	989.1	22.6
273.5	37.73	974.2	974.5		
280	48.48	974.2	974.4	989.1/2	22.7
290.5	1'07.83	974.0/1	974.3	989.0/1	-
300	1'30.45	973.9/974.0	974.2	989.1	-
308.75	1'58.92	973.7/8	974.1	989.1	22.6
317.25	2'28.63	973.7	974.0/1	989.1	-
320	2'48.29	973.7	974.0	989.1/2	-
325	3'14.29	973.6/7	973.9	989.1	22.6
329.75	3'48.10	-	-	-	-
333	4'22.10	973.5/6	973.8/9	-	22.5
335.5	5'05.23	-	973.8	-	-
338	5'52.89	973.4/5	973.7/8	-	-
340	6'51.83	-	-	-	22.4
342	8'04.01	-	973.7	989.0/1	-
343	9'03.29	973.3/4	-	-	22.3
343.75	10'46.54	973.2/3	973.6/7	989.0	22.3
344.25	13'20.26	973.1/2	973.5/6	988.9/989.0	22.4
344.25	15'00.51	-	973.4/5	-	22.4
344.25	20'23.26	973.1	973.3	988.8/9	22.3
344.25	20'44.89				

Gate closed at 20'44, 89  $\Rightarrow$

$P_1 = 971.7/8 \text{ mbar}$   
 $P_2 = 972.6 \text{ mbar}$   
 $P_3 = 988.8/9 \text{ mbar}$   
 $T = 22.2^\circ\text{C}$

at 17H20

Video stopped at 9'27.89

08.11.1999

# GS FLOW RATE 90

At atmospheric pressure

$$\begin{aligned} P_1 &= 988.415 \text{ mbar} \\ P_2 &= 988.112 \text{ mbar} \\ P_3 &= 988.5 \text{ mbar} \\ T &= 21.7^\circ\text{C} \\ h_b &= 243.5 \text{ mm} \end{aligned}$$

$h_{\text{dike}} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
243.5	0	947.9/948.0	988.112	988.415	21.6
260	7.75	948.415	948.112	988.5	
280	17.47	948.011	947.617	988.5	21.5
309	34.34	947.6	947.2		
320	42.19	947.415	947.112	988.516	21.5
340	57.03	947.2	946.9	988.5	-
360	1'14.63	946.9	946.6	-	-
380	1'36.31	946.7	946.4	-	-
400	2'03.09	946.516	946.2	988.516	-
410	2'20.31	946.4	946.112	988.516	21.5
424	2'42.47	946.3	946.0	988.6	21.6
435	3'07.22				

Gate closed at 3'07.22 when GS reached the tunnel entrance  
Dike valve opened  $\Rightarrow$

$$\begin{aligned} P_1 &= 944.213 \text{ mbar} \\ P_2 &= 988.2 \text{ mbar} \\ P_3 &= 988.6 \text{ mbar} \\ T &= 21.7^\circ\text{C} \end{aligned}$$

At 18H15

$$\begin{aligned} P_1 &= 988.7 \text{ mbar} \\ P_2 &= 988.3 \text{ mbar} \\ P_3 &= 988.617 \text{ mbar} \end{aligned}$$

08.1.1999

At 10405, at atmospheric pressure

$P_1 = 990.1/2 \text{ mbar}$

$P_2 = 988.8/9 \text{ mbar}$

$P_3 = 989.7 \text{ mbar}$

$T = 19.8^\circ\text{C}$

$h = 243.5 \text{ mm}$

Room heater switched on (low level)

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
243.5	0	964.8/9	989.3/4	989.9/990.0	20.0
250	9.04	966.5	964.1	-	20.0
260	18.60	964.9	964.0	989.9	20.1
270	30.69	964.8	963.8/9	-	-
280	42.92	964.7/8	963.8	-	-
291.5	58.76	964.6/7	963.6/7	-	-
300	1'13.79	964.5/6	963.5/6	989.9/990.0	-
312.5	1'35.07	964.4	963.5/6	-	-
320	1'53.35	-	963.4/5	-	-
331.25	2'18.32	964.3	963.4	-	-
340	2'46.32	964.2/3	963.3	-	20.2
351	3'18.48	964.2	-	-	-
360	3'58.57	964.1/2	963.2/3	990.0	-
367.75	4'27.45	964.0/1	963.1/2	-	-
373.25	5'04.17	964.0	963.2	-	-
380	5'55.01	963.9/964.0	963.1/2	-	-

Video stopped at 6'18.57

386.75	6'36.86	963.9	963.1/2	990.0/1	20.2
389.25	7'07.04	-	-	-	-
392.5	7'45.01	963.8/9	963.1	-	20.3
395.5	8'26.89	-	963.1/2	-	-
398.25	9'11.26	963.7/8	963.0/1	-	-
400	9'45.29	963.8	-	990.0	20.4
402.25	10'26.45	963.7/8	-	990.0/1	-
404.75	11'27.23	963.7/8	-	990.0	-
406.25	12'27.89	963.7	-	-	-
407.75	13'29.63	-	-	-	-
409.25	14'28.83	963.6/7	-	990.0/1	-
410.25	15'30.42	963.7	963.1/2	-	-

Video on for a few seconds at 12'04.69

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T(^{\circ}\text{C})$
411.25	16'35.32	963.7	963.1/2	990.1	20.4
411.75	17'48.51	963.6/7	963.1/2	990.0/1	20.4

Pump stopped working for a few seconds  
 $\Rightarrow$  all readings off!

961.0      960.5      990.1      20.4

Pressures readjusted manually (with vacuum regulators) at 19'11.00

to 963.8/9      963.3/4      990.1/2      20.4

$\Rightarrow$  GS level goes up to 414.25 mm on the dike

414.25      20'19.54      963.9      963.4      990.1      20.4

GS level starts to go down  $\Rightarrow$  decided to stop the expt  
 at 20'46.89

$\Rightarrow$   $\left\{ \begin{array}{l} P_1 = 962.2/3 \text{ mbar} \\ P_2 = 962.6/7 \text{ mbar} \\ P_3 = 990.1 \text{ mbar} \\ T = 20.4^{\circ}\text{C} \end{array} \right.$

at 10H35

At 10H45  $\left\{ \begin{array}{l} P_1 = 990.5/6 \text{ mbar} \\ P_2 = 990.3/4 \text{ mbar} \\ P_3 = 990.2 \text{ mbar} \\ T = 20.4^{\circ}\text{C} \end{array} \right.$

09.11.1999



# GS FLOW RATE 92

At 11H30, at atmospheric pressure

$$\begin{aligned} P_1 &= 990.3 \text{ mbar} \\ P_2 &= 990.6/7 \text{ mbar} \\ P_3 &= 989.8/9 \text{ mbar} \\ T &= 21.0^\circ\text{C} \\ h_0 &= 243.5 \text{ mm} \end{aligned}$$

$h_{\text{dike}} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
243.5	0	939.2/3	990.6/7	989.8/9	21.1
250	3.55				
260	6.58				
270	10.52	938.0			
280	14.77	938.0	938.4		
300	24.11	937.7	938.1	989.8	21.1
320	35.05	937.4	937.8	989.9	-
340	47.08	937.2	937.6	-	-
360	1'00.96	937.0	937.3/4	989.8	-
380	1'17.43	936.7	937.2	-	-
400	1'36.64	936.6	937.1	-	-
410	1'47.55	-	937.0	989.9	-
420	1'57.14	936.5	936.9/937.0	-	-
435	2'18.27	936.4	936.8	989.8	-

Gate closed at 2'18.27 when GS reached the tunnel entrance

$$\begin{aligned} \Rightarrow \quad P_1 &= 935.1/2 \text{ mbar} \\ P_2 &= 990.7/8 \text{ mbar} \\ P_3 &= 989.9 \text{ mbar} \\ T &= 21.1^\circ\text{C} \end{aligned} \quad \text{at 11H40}$$

09.11.1999



New series of experiments performed with  $P_{\text{reservoir}} \neq \text{atmospheric}$   
 At atmospheric pressure,

GS in reservoir =  $h_{R_0} = 305.5 \text{ mm}$

GS in dike =  $h_{D_0} = 243.5 \text{ mm}$

At 8H30

$P_1 = 990.3/4 \text{ mbar}$  tunnel  
 $P_2 = 989.4/5 \text{ mbar}$  dike  
 $P_3 = 969.3/4 \text{ mbar}$  reservoir  
 $T = 20.1^\circ\text{C}$   
 $h_D = 110.5 \text{ mm}$

$$\Rightarrow h_R = h_{R_0} + \frac{(h_{D_0} - h_D) A_D}{A_R} = 319.97 \text{ mm}$$

At 8H35, tunnel pressure lowered

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
110.5	0	948.8/9	989.5/6	969.3/4	20.2
120	4.60	950.3	949.1		-
140	11.38	949.6/7	948.5	967.2/3	-
160	20.73	949.2	948.1/2	967.6	-
180	31.38	948.9/949.0	947.8	968.0	-
200	45.01	948.7	947.6	968.2	-
220	1'00.19	948.4/5	947.4	968.5/6	-
240	1'18.89	948.2/3	947.1/2	968.7/8	-
260	1'41.92	948.1	947.1	968.9/969.0	-
280	2'10.83	947.9/948.0	946.9/947.0	969.1/2	-
291.5	2'31.04	947.9	946.8	969.1/2	20.2
300	2'47.76	947.8/9	946.8/9	969.2/3	-
311.25	3'12.51	947.7/8	946.7/8	969.3	-
320	3'37.23	947.7/8	946.7	969.4	-
331.25	4'10.95	947.6/7	946.6	969.5	-
340	4'50.01	947.6/7	946.6	969.5	-
351.25	5'40.19	947.5/6	946.5	969.6/7	-
360	6'49.01	947.5	946.5	969.6/7	-
368	7'53.13	947.5	946.5	969.7/8	-

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ (°C)
------------------------	------	--------------	--------------	--------------	----------

371	8'38.32	947.4/5	946.4/5	969.7/8	20.2
374.5	9'23.13	947.4/5	946.4/5	969.7/8	-
377.5	10'21.10	947.4/5	946.4/5	969.8	-
380	11'19.54	947.4/5	946.4/5	969.8	-

Video stopped recording at 11'39.67

382.25	12'33.60	947.4/5	946.4/5	969.8	20.2
383.75	13'43.38	947.4/5	946.5/6	969.8/9	-
385.5	15'11.92	-	-	969.9/970.0	-
386.25	16'20.54	-	-	969.9	-
387.75	19'23.10	-	-	969.9/970.0	20.3
388.5	22'17.48	-	946.6	970.0	-
389.25	23'48.32	-	946.6/7	969.9/970.0	-
389.5	26'01.01	-	-	970.0	-
389.5	27'36.38	947.5/6	946.7	970.0/1	-
389.5	29'02.76	-	946.7/8	970.1	-

Pump stopped running at ~ 29'39 ← battery flat

1) Valve closed at 29'56.35

Gate

↪ got a new battery

10.11.1999

# GS FLOW RATE 94

At 10400

$$P_1 = 991.6/7 \text{ mbar}$$

$$P_2 = 991.1/2 \text{ mbar}$$

$$P_3 = 991.2/3 \text{ mbar}$$

$$T = 20.7^\circ\text{C}$$

Reservoir pressure lowered down to 969.8 mbar  $\Rightarrow h_p = 107 \text{ mm}$   
(still some GS on wa)

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
-------------------------------	------	---------------------	---------------------	---------------------	----------------------

107	0	959.7/8	991.1/2	969.8	20.9
120	5.72	961.5	961.1	967.6	-
140	14.13	961.0	960.6	968.1	-
160	24.57	960.6	960.3	968.5	-
180	37.57	960.4	960.1	968.8	-
190	45.59	960.3	960.0	968.9	-
200	55.31	960.2	959.9	969.1	-
210	1'05.53	960.1	959.7	969.3	-
220	1'17.07	960.0/1	959.7	969.4	-
230	1'30.31	959.9/960.0	959.6/7	969.4/5	-
240	1'46.03	959.8/9	959.5/6	969.6	20.9
250.25	2'05.78	959.7/8	959.5	969.7	-
260	2'29.07	-	959.4	969.8	-
270.25	2'58.57	959.7	959.3/4	969.8/9	-
276.25	3'18.44	959.7	959.3/4	969.9	-
280	3'37.41	959.6/7	-	-	-
285	3'57.03	-	959.3	969.9/970.0	-
290	4'25.03	-	959.2/3	970.0	20.9
293.75	4'55.28	959.6	-	970.0/1	-
297.75	5'28.66	959.6/7	-	970.1/2	-
300	5'57.41	959.5/6	-	-	-
303.5	6'33.19	959.6	-	-	-
305.25	7'05.50	-	-	-	-
307.5	8'03.22	959.5/6	959.1/2	-	21.0
310	9'10.41	-	-	-	-
311.25	10'15.47	-	-	970.2/3	-
312.25	12'02.44	959.6	959.2/3	970.2/3	21.0
313.25	14'13.41	959.5/6	959.2/3	970.3	-
313.25	16'26.28	-	-	970.2/3	21.1
313.25	18'09.03	-	959.1/2	-	-
313.25	19'33.59	-	-	-	-
313.25	20'00.07	-	-	-	-

10.11.1999

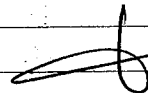
Gate closed at 20' 00.07

↳  $\left| \begin{array}{l} P_1 = 959.415 \text{ mbar} \\ P_2 = 957.9/958.0 \text{ mbar} \\ P_3 = 970.1/2 \text{ mbar} \end{array} \right.$  at  $\approx 10435$

Dike valve opened  $\Rightarrow \left| \begin{array}{l} P_1 = 959.5 \text{ mbar} \\ P_2 = 990.9/991.0 \text{ mbar} \\ P_3 = 971.5 \text{ mbar} \\ T = 21.1^\circ\text{C} \end{array} \right.$

Video was stopped at 9' 40.31

10.11.1998



# GS FLOW RATE 95

At 1110

$h_{dike} = 103 \text{ mm}$

still some GS on walls but pretty much OK (add 2 mm)

$P_1 = 938.718 \text{ mbar}$

$P_2 = 991.5 \text{ mbar}$

$P_3 = 969.213 \text{ mbar}$

$T = 21.7^\circ\text{C}$

$h_{dike} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
120	4.14	940.5	940.3		
140	8.08	939.1	939.3	965.8	
160	13.11	?	?	?	
180	18.83	938.5	938.7	967.1	
200	26.02	938.2	938.3	967.6	
230	38.73	?	?	?	
240	43.49	937.718	937.9/938.0	968.1	21.7
260	55.33	937.516	937.7	968.415	-
280	1'09.49	937.4	937.6	968.617	-
300	1'25.55	937.213	937.5	968.819	-
320	1'45.58	937.1	937.314	969.0	-
340	2'10.67	937.011	937.213	969.112	21.7
360	2'41.14	936.9/937.0	937.112	969.4	-
371.25	3'01.61	936.9	937.1	-	-
380	3'22.89	936.819	-	969.5	-
391	3'50.36	936.718	937.011	969.516	21.8
400	4'19.20	936.8	-	969.617	-
410	4'56.80	936.718	-	969.718	-
420	5'41.29	-	-	-	-
426	6'14.33	936.7	936.9/937.0	969.8	-
430.75	6'48.55	-	937.011	969.9	21.8
435	7'30.67	-	-	-	-

Gate closed at 7'30.67 - Valve opened

$\Rightarrow$   $P_1 = 936.617 \text{ mbar}$   
 $P_2 = 991.617 \text{ mbar}$   
 $P_3 = 971.718 \text{ mbar}$   
 $T = 21.8^\circ\text{C}$

at 1120

10.11.1999

# GS FLOW RATE 96

10.11.1999

At 14H10

$P_1 = 964.4/5 \text{ mbar}$   
 $P_2 = 991.7/8 \text{ mbar}$   
 $P_3 = 969.5/6 \text{ mbar}$   
 $T = 23.7^\circ\text{C}$   
 $h_D = 111 \text{ mm}$

Readjust pressures

$P_1 = 963.9/964.0 \text{ mbar}$   
 $P_2 = 991.6/7 \text{ mbar}$   
 $P_3 = 969.1/2 \text{ mbar}$   
 $T = 23.7^\circ\text{C}$   
 $h_D = 110 \text{ mm}$

Dike valve closed and gate opened at  $t=0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
120	4.76	966.9	968.3	966.6/7	23.7
140	12.76	965.8	967.3	967.3	-
160	23.10	965.2	966.7	967.8	-
180	35.92	964.8/9	966.3	968.1/2	-
200	53.48	964.5	966.0	968.4	-
210	1'04.54	964.3	965.7	968.6	-
220	1'17.04	964.2	965.7	968.8	23.6
230	1'33.57	964.1	965.5/6	968.9	-
240	1'53.51	963.9	965.3/4	968.9/969.0	-
250	2'18.23	963.8	965.3	969.1	-
260	2'55.45	963.6/7	965.1/2	969.1/2	23.6
264.75	3'25.38	963.5/6	965.1	969.2/3	-
270	4'05.42	963.4/5	965.0/1	-	-
273.25	4'34.10	963.5	965.0	969.3	-
275.5	5'10.57	963.4/5	964.9/965.0	-	-

Video switched off at 5'54.60

278.25	6'14.23	963.3/4	964.8/9	969.3	23.6
280	7'08.29	963.3/4	964.8	-	-
281	8'32.32	963.2/3	964.7/8	-	23.5
281.25	11'17.89	-	964.6	-	-
281.25	13'15.89	963.1/2	964.5	969.2/3	-
281.25	15'09.79	-	964.4/5	-	23.3

gate closed at 15'32.13  $\Rightarrow$

$P_1 = 962.9/963.0 \text{ mbar}$   
 $P_2 = 963.9/964.0 \text{ mbar}$   
 $P_3 = 969.2/3 \text{ mbar}$   
 $T = 23.7^\circ\text{C}$

at 14H30

# GS FLOW RATE 97

At 14 H 55

$P_1 = 989.0 \text{ mbar}$   
 $P_2 = 989.6/7 \text{ mbar}$   
 $P_3 = 968.2/3 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$   
 $h_D = 109 \text{ mm}$

Battery = 12.07 V

Tunnel pressure lowered

$P_1 = 962.4/5 \text{ mbar}$   
 $P_2 = 989.5/6 \text{ mbar}$   
 $P_3 = 968.0/1 \text{ mbar}$   
 $T = 22.6^\circ\text{C}$   
 $h_D = 107.75 \text{ mm}$

Dike valve closed - Gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
107.75	0	962.3	989.5	968.0/1	22.6
120	5.21	964.3	964.8	965.3	-
140	13.27	963.3	963.8	965.9/966.0	-
160	23.71	962.7	963.3	966.4	22.7
180	36.30	962.3	962.8	966.7/8	-
190	45.18	962.1	962.6	966.8	-
200	54.15				
210	1'05.12	961.7/8	962.2/3	967.2	22.7
220	1'18.93	961.5	962.0	967.4	-
230	1'33.65	961.4	961.9	967.5	-
243.75	2'01.68	961.2/3	961.7/8	967.7	22.7
250	2'16.84	961.2	961.6/7	-	-
256.75	2'35.56	961.1	961.5/6	-	-
260	2'50.40	961.0/1	-	967.7/8	-
264.25	3'06.06	961.0	961.5	967.8	22.8
269	3'30.53	960.9/961.0	961.4/5	967.9/968.0	22.7
274	4'03.21	960.8/9	961.3/4	967.9	22.8
277.5	4'32.77	-	-	967.9/968.0	-
280	5'00.33	-	961.3	968.0	-

Video stopped at 5'18.84

282.75	5'38.30	960.8/9	961.3	968.0	22.9
284	6'17.18	960.8	-	-	-
286.25	7'25.15	-	961.2	968.0/1	-

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T(^{\circ}\text{C})$
288	9'23.81	960.8	961.2	968.1	23.0
289	11'36.81	960.8/9	961.2/3	968.0/1	-
289.25	13'43.90	960.8	-	-	23.1
289.5	15'02.53	-	-	-	-
289.5	16'12.81	960.8/9	961.3	968.0/1	23.2
289.75	17'21.27	-	961.3/4	968.1	-
289.75	18'36.09	960.9	-	968.0/1	23.3
-	19'46.90	-	-	-	-
-	20'55.59	960.9/961.0	961.4/5	968.1	-
-	22'03.62	-	-	968.0/1	-

Gate closed at 22'29.65  $\Rightarrow$

$P_1 = 960.2/3$  mbar  
 $P_2 = 960.9/961.0$  mbar  
 $P_3 = 968.0/1$  mbar

Battery = 12.04V at 15H25



At 16H00

$P_1 = 989.7/8 \text{ mbar}$

$P_2 = 990.5/6 \text{ mbar}$

$P_3 = 969.3/4 \text{ mbar}$

$T = 23.8^\circ \text{C}$

$h_d = 114 \text{ mm}$

Battery = 12 V

Tunnel pressure lowered  $\Rightarrow$ 

$P_1 = 954.1/2 \text{ mbar}$

$P_2 = 990.6/7 \text{ mbar}$

$P_3 = 969.3/4 \text{ mbar}$

$T = 23.8^\circ \text{C}$

Reservoir and tunnel pressures readjusted  $\Rightarrow h_d = 110.5 \text{ mm}$  at 16H00Dike valve closed - gate opened at  $t = 0$ 

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ \text{C})$
110.5	0	953.7/8	990.6/7	968.7/8	23.6
130	5.57				
140	8.78	955.8	956.7	965.9	
170	19.25				
180	23.69	954.8	955.7/8	966.7	23.6
200	33.97	954.4	955.3/4	967.2	-
220	46.59	954.0/1	955.0	967.6	-
240	1' 02.03	953.8	954.8	967.8	23.6
250.25	1' 12.78	953.7	954.7	967.9	-
260	1' 22.53	953.6/7	954.6	968.1	23.6
270	1' 35.88	953.5	954.5	968.2	-
280	1' 50.44	953.4	954.4	968.3	-
290	2' 08.57	953.3/4	954.3	968.4/5	-
300	2' 31.41	953.2/3	954.2/3	968.5/6	-
308.75	2' 53.03	953.1/2	954.2	968.6/7	-
315.5	3' 16.07	-	954.1/2	968.7	-
320	3' 36.78	-	954.0/1	968.7/8	-
326.5	4' 06.85	953.0/1	-	-	-
332.75	4' 47.75	953.0	954.1	968.8/9	-
336.75	5' 30.53	953.0/1	954.0/1	968.9	-
340	6' 22.57	952.9/953.0	-	-	-

Video stopped at 7' 10.63

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
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343.25	7' 39.50	952.9/953.0	953.9/954.0	968.9	23.6
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345	8' 46.91	-	-	-	-
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346	9' 57.72	-	-	-	-
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346.75	11' 35.34	-	-	-	-
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346.75	13' 29.34	952.9	954.0	-	-
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-	15' 01.85	952.9/953.0	953.9/954.0	968.8/9	23.7
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-	17' 33.69	-	-	-	-
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Gate closed at 18' 01.72  $\Rightarrow$

$P_1 = 952.8/9 \text{ mbar}$

$P_2 = 953.5/6 \text{ mbar}$

$P_3 = 968.8/9 \text{ mbar}$

$T = 23.7^\circ\text{C}$

Battery = 11.97V at 16H25

10.11.1999

# GS FLOW RATE 99

At 17H05

$$P_1 = 989.5/6 \text{ mbar}$$

$$P_2 = 990.5/6 \text{ mbar}$$

$$P_3 = 968.6/7 \text{ mbar}$$

$$T = 24^\circ\text{C}$$

$$h_d = 110 \text{ mm}$$

$$\text{Battery} = 11.92 \text{ V}$$

Tumond pressure lowered down to 943.2/3 mbar

Dike valve closed - Gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
110	0	943.2/3	990.5/6	968.4/5	24.0
120	2.58				
140	6.52	944.3	945.3		
160	10.83	943.5	944.5	964.9	
190	19.29				
200	22.39	942.3	943.3	965.8	
220	29.49	941.9	942.9	966.2	23.9
240	38.43	941.5	942.5	966.7	
270	54.05				
280	1'00.73	940.9	942.0	967.2/3	
300	1'15.55	940.7	941.8	967.5	
309.5	1'24.11	940.6	941.6	967.6	
320	1'33.83	940.5	941.5/6	967.8	
329.5	1'45.02	940.3/4	941.5	967.9	23.9
340	1'58.05	940.2/3	941.3/4	968.0	-
349.5	2'11.70	940.2	941.3	968.0/1	-
360	2'28.89	940.1	941.2	968.2	-
370	2'49.33	939.9/940.0	941.0/1	968.3	-
380	3'13.77	-	941.0	968.3/4	-
390	3'42.83	939.9	940.8/9	968.4/5	-
397	4'09.49	939.8/9	-	968.5	-
404.5	4'43.73	939.7/8	940.7/8	968.5/6	-

Video stopped recording at 5'09.70

410	5'30.49	939.6/7	940.7/8	968.6	23.9
414.75	6'02.23	-	940.6/7	-	-
420	7'00.43	-	-	968.6/7	23.8
424	8'03.89	939.5/6	940.5/6	968.7	-
426.25	9'09.17	-	-	968.7/8	-

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T(^{\circ}\text{C})$
428.25	10'19.64	939.415	940.415	968.718	23.8
429.75	12'03.39	939.5	940.4	-	-
431	14'08.43	939.4	-	968.7	-
431.25	16'23.67	939.314	940.213	-	-
431.5	18'05.96	-	940.2	-	-
431.75	20'27.39	-	940.112	-	23.7
432	24'31.93	-	940.1	968.718	-
432	28'42.14	-	940.0	-	23.6
432	30'51.96	-	939.9/940.0	-	-
432	32'46.77	939.3	939.9	-	-
432	34'39.39	-	939.8/9	-	-
432	35'03.96	-	-	-	-

Jake closed at 35'03.96  $\Rightarrow$

$P_1 = 939.0/1 \text{ mbar}$   
 $P_2 = 939.3 \text{ mbar}$   
 $P_3 = 968.8/9 \text{ mbar}$   
 $T = 23.6^{\circ}\text{C}$

Battery = 11.86 V at 17H47

10.11.1999

GS FLOW RATE 100

At 18H10

$P_1 = 989.5/6 \text{ mbar}$   
 $P_2 = 990.0/1 \text{ mbar}$   
 $P_3 = 968.9 \text{ mbar}$   
 $T = 23.6^\circ\text{C}$   
 $h_b = 110 \text{ mm}$

Battery = 11.83V

Tunnel pressure lowered down to 928.1/2 mbar  
 Dike valve closed - Gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ\text{C})$
110	0	928.1/2	989.8/3	968.6/7	23.6
140	4.83				
160	7.79	929.0			
180	11.48				
200	15.57	927.8	928.4	965.0	
220	20.48				
240	25.60	927.0	927.6	966.1	
260	31.69				
280	38.86	926.4/5	927.0	966.7	
300	47.23	926.3/4	926.9	966.9	
320	56.73	926.1/2	926.6/7	967.2/3	
340	1'07.95	925.9	926.5	967.5	
360	1'21.10	925.8	926.4	967.7/8	23.6
380	1'36.51	925.7	926.2	967.9/968.0	-
400	1'57.01	925.5/6	926.1	968.1	-
410	2'09.57	925.4/5	926.1	968.2/3	-
420	2'21.45	925.4	925.9/926.0	968.3/4	-
435	2'47.38	925.3/4	-	968.4/5	-

Gate closed / valve opened at 2'47.38 when GS reached the tunnel entrance

↳

$P_1 = 925.0 \text{ mbar}$   
 $P_2 = 990.0/1 \text{ mbar}$   
 $P_3 = 971.4/5 \text{ mbar}$   
 $T = 23.6^\circ\text{C}$

10.11.1999

18 H15

$P_1 = 989.9 / 990.0 \text{ mbar}$

$P_2 = 990.4 / 5 \text{ mbar}$

$P_3 = 989.8 / 9 \text{ mbar}$

$T = 23.7^\circ \text{C}$

Battery = 11.83 V

10. 11. 1999

At 7:30

Battery = 13.76 V (charged overnight from 18:30)  
not complete

$$P_1 = 992.9/993.0 \text{ mbar}$$

$$P_2 = 991.9/992.0 \text{ mbar}$$

$$P_3 = 992.5/6 \text{ mbar}$$

$$T = 21.1^\circ\text{C}$$

$$h_d = 243.5 \text{ mm}$$

Pump started at 07:35. At 8:10, battery = 12.45 V

Reservoir pressure lowered

$$P_1 = 993.3/4 \text{ mbar}$$

$$P_2 = 992.5/6 \text{ mbar}$$

$$P_3 = 979.0 \text{ mbar}$$

$$T = 21.1^\circ\text{C}$$

$$h_d = 154 \text{ mm}$$

Tunnel pressure lowered

$$P_1 = 958.8/9 \text{ mbar}$$

$$P_2 = 992.6/7 \text{ mbar}$$

$$P_3 = 978.8/9 \text{ mbar}$$

$$T = 21.2^\circ\text{C}$$

$h_{dike}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^\circ\text{C}$ )
154	0	958.5/6	992.5/6	978.9/979.0	21.2
170	7.93				
180	12.64	959.4/5	958.8	977.0	
200	23.89	959.1/2	958.5	977.4	21.2
220	37.02	958.8/9	958.2	977.6/7	-
230	46.70	958.8			
240	54.02	958.7	958.0	977.9	-
250.25	1'04.29	958.5	957.8	978.0	21.2
260	1'15.87	958.4/5	957.7/8	978.2	
270	1'27.80	958.4	957.7	978.3	
280	1'42.70	958.2/3	957.5/6	978.3/4	21.2
290	1'57.61	958.1/2	-	978.4	-
300	2'16.05	958.1/2	957.4/5	978.5	-
309.5	2'37.20	958.0/1	957.3/4	978.5/6	-
320	3'02.29	958.0	-	978.6/7	21.2
329.5	3'31.77	-	957.2/3	978.7/8	-
335.75	3'54.89	957.9/958.0	-	978.8	-
340	4'15.17	957.9	-	978.8/9	-

h <sub>dike</sub> (mm)	time	P <sub>1</sub> (mbar)	P <sub>2</sub> (mbar)	P <sub>3</sub> (mbar)	T (°C)
345.25	4' 38.61	957.9	957.2	978.8/9	21.2
349.5	5' 01.14	957.8/9	-	978.9	-
353.5	5' 24.20	957.8	-	978.9/979.0	-
357.25	5' 55.70	957.8/9	957.1/2	-	-
360	6' 19.33	957.8	-	-	-

Video stopped at 6' 34.80

364	6' 56.14	957.7/8	957.1/2	979.0	21.2
367	7' 34.23	-	-	-	-
369.75	8' 20.89	-	-	-	-
372	9' 07.80	-	-	-	-
374.75	10' 15.52	957.7	-	-	21.2
377	11' 40.08	-	-	979.0/1	-
378.5	13' 02.11	957.7/8	957.2/3	979.1/2	-
380	14' 07.02	-	957.2	-	-
381.5	16' 24.23	-	957.2/3	-	21.3
381.5	17' 56.36	957.8	957.3	979.2	-
382	20' 11.77	-	-	979.2/3	-
382	22' 32.58	957.8/9	957.4	-	-
382	25' 06.02	-	957.4/5	979.3	-
382	27' 32.33	957.9/958.0	-	979.3/4	21.4
382	28' 02.89	-	-	-	-

Gate closed/valve opened at 28' 02.89 =>

P <sub>1</sub> = 957.7/8 mbar
P <sub>2</sub> = 993.3/4 mbar
P <sub>3</sub> = 980.7 mbar

At 8440

P <sub>1</sub> = 993.8/9 mbar
P <sub>2</sub> = 993.4/5 mbar
P <sub>3</sub> = 980.4/5 mbar
Battery = 12.37 V



# GS FLOW RATE 10<sup>-2</sup>

At 9:30

Battery = 12.28 V

$P_1 = 994.2/3 \text{ mbar}$

$P_2 = 994.0/1 \text{ mbar}$

$P_3 = 979.7 \text{ mbar}$

$T = 21.6^\circ \text{C}$

$h_d = 152 \text{ mm}$

Tunnel pressure lowered down to 970.2/3 mbar.  
Dike valve closed / gate opened at  $t = 0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ \text{C})$
152	0	970.2/3	994.0/1	979.6/7	21.6
160	5.37	971.5	971.2	977.9	
170	12.15				
180	18.24	971.0	970.8	978.3	21.6
190	26.15	970.8	970.5	978.5	-
200	35.49	970.5/6	970.3/4	978.6/7	-
210	46.43	970.4	970.2	978.8	-
220	56.56	970.3/4	970.1	978.8/9	-
230	1'09.77	970.2	969.9/970.0	979.0	-
240	1'25.77	970.0/1	969.8/9	979.0/1	-
250.25	1'45.06	969.9	969.6/7	979.1/2	-
260	2'05.97	969.8	969.5/6	979.3	-
270	2'35.74	969.7	969.4/5	979.4	-
280	3'13.47	969.6	969.3/4	979.4/5	-
284.5	3'31.97	969.5/6	969.3	-	-
290	4'09.12	969.4/5	969.2/3	979.5	-
293.5	4'33.30	-	-	979.5/6	-

Video stopped at 4'58.12

297.75	5'12.33	969.4	969.2	979.5/6	21.6
300	5'37.77	969.3/4	969.1/2	-	-
302.5	6'17.37	969.3	-	979.6	-
305.5	7'19.77	-	969.0/1	-	-
308.25	8'54.33	-	969.0	-	-
309.5	10'08.97	969.2/3	-	979.6/7	-
310.75	11'45.30	-	968.9/969.0	-	-
310.75	13'16.81	969.1/2	968.8/9	979.6	-
311	15'14.18	-	-	979.6/7	-
311.5	17'35.77	-	-	-	-

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T(^{\circ}\text{C})$
311.5	22'34.68	969.0/1	968.8	979.6	21.6
312	26'42.47	-	968.7/8	-	-
312	28'58.33	968.9/969.0	-	979.5/6	21.7
312	30'05.87	-	968.7	-	21.6
312	31'22.97	-	-	-	21.7
312	32'37.81	-	-	-	-
312	33'48.09	-	968.6/7	-	-

Gate closed, valve opened at 33'48.09

$\hookrightarrow$   $P_1 = 968.4/5 \text{ mbar}$   
 $P_2 = 993.8/9 \text{ mbar}$   
 $P_3 = 980.6/7 \text{ mbar}$   
 $T = 21.7^{\circ}\text{C}$

at 10H05

At 10H10

Battery = 12.21 V

$P_1 = 994.1/2 \text{ mbar}$

$P_2 = 993.8/9 \text{ mbar}$

$P_3 = 979.7 \text{ mbar}$

$T = 21.7^{\circ}\text{C}$

11.11.1999

# GS FLOW RATE 103

At 10H35

Battery = 12.17 V

$P_1 = 994.0/1 \text{ mbar}$

$P_2 = 993.8/9 \text{ mbar}$

$P_3 = 979.5/6 \text{ mbar}$

$T = 21.7^\circ\text{C}$

$h_d = 151.5 \text{ mm}$

Tunnel pressure lowered down to 949.6/7 mbar at 10H40.  
Dike valve closed, gate opened at  $t = 0$

$h_{\text{dike}} \text{ (mm)}$	time	$P_1 \text{ (mbar)}$	$P_2 \text{ (mbar)}$	$P_3 \text{ (mbar)}$	$T(^{\circ}\text{C})$
151.5	0	949.6/7	993.6/7	979.3/4	21.7
160	3.52	950.7	950.5		
180	9.39	949.9/950.0	949.6	976.6	
200	16.67	949.4	949.2	976.9	21.7
220	24.70	949.1	948.9	977.3	-
240	34.80	948.8	948.6	977.6	-
260	46.43	948.5	948.3/4	977.8	-
280	1'00.36	948.3	948.1	978.0	21.7
290	1'08.36	948.1/2	947.9/948.0	978.2/3	-
300	1'18.08	948.0/1	947.8/9	978.3/4	-
320	1'38.46	947.9	947.7	978.5	21.7
329.5	1'50.29	947.8	947.6	978.6	-
340	2'05.11	947.7	947.5	978.7	-
349.5	2'18.93	947.6/7	-	-	-
360	2'37.58	947.5/6	947.4	978.8/9	-
370	2'56.29	947.4/5	947.3/4	978.9/979.0	-
380	3'21.67	947.3/4	947.2/3	979.0	-
390	3'47.36	-	947.2	979.0/1	-
400	4'22.52	947.2/3	947.0/1	979.1	-
410	5'06.05	947.1/2	946.9/947.0	979.1/2	-
420	5'56.83	947.1	946.9	-	-
424.5	6'25.73	947.0/1	946.8/9	979.2/3	-
428.75	7'04.20	-	-	-	-
432.5	7'43.33	947.0	-	-	-
435	8'30.02	946.9/947.0	-	-	-

Gate closed / valve opened at 8'30.02 when GS reached the bottom of the tunnel entrance

11.11.1999

⇒

$$P_1 = 946.5/6 \text{ mbar}$$

$$P_2 = 993.7/8 \text{ mbar}$$

$$P_3 = 980.6/7 \text{ mbar}$$

$$T = 21.7^\circ\text{C}$$

at 10:450

⇒

$$P_1 = 994.0/1 \text{ mbar}$$

$$P_2 = 993.7/8 \text{ mbar}$$

$$P_3 = 980.6/7 \text{ mbar}$$

$$\text{Battery} = 12.15 \text{ V}$$

4.4.1999

# GS FLOW RATE 104

At 10H20

Battery = 12.12 V

$P_1 = 993.9 / 994.0$  mbar

$P_2 = 993.8 / 9$  mbar

$P_3 = 979.1 / 2$  mbar

$T = 21.9^\circ\text{C}$

$h_2 = 150$  mm (still some GS on walls)

Tunnel pressure lowered down to 975.1/2 mbar  
Dike valve closed / gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T(^{\circ}\text{C})$
150	0	975.1/2	993.7/8	979.0/1	21.9
160	7.61	976.3	976.3	977.8	21.9
170	15.36	976.1	976.1	978.0	-
180	24.23	975.8	975.8/9		
190	34.02	975.7/8	975.8	978.2/3	21.9
200	46.02	975.5/6	975.6	978.4	-
210	1'00.83	975.4	975.4/5	978.5	-
220	1'18.52	975.3	975.3/4	978.6	-
230	1'39.39	975.2	975.2/3	978.7/8	-
240	2'07.67	975.0/1	975.1/2	978.8	-
250.25	2'51.55	974.9/975.0	975.0	978.8/9	21.9
254.5	3'15.89	974.8/9	974.9/975.0	978.9/979.0	-
260	3'54.23	-	974.9	979.0	-
263	4'31.46	974.8	974.8/9	-	-
266	5'17.80	974.7/8	-	-	-
268	5'58.23	974.6/7	974.7/8	-	-
269.25	6'50.14	-	974.7	-	-
270.5	7'57.02	-	974.7/8	-	-
271.75	9'49.02	974.5/6	974.6/7	978.9/979.0	-
272	11'39.05	974.4/5	-	-	-
272.25	13'13.55	-	-	978.9	-
272.5	15'04.33	-	974.5/6	978.9/979.0	22.0
272.75	17'11.52	974.3/4	-	978.8/9	-
273	18'43.52	-	-	-	-
273	20'35.29	-	-	-	22.0
273	22'12.08	974.3	974.5	-	-
273	23'37.05	974.2/3	974.4/5	978.7/8	-
273	24'33.23	974.2	974.4	978.7	22.1
273	25'00.55	-	-	-	-

11.11.1999 /

Videos stopped at 6'18.43

Gate closed / valve opened at 25'00.55

↳

$$P_1 = 973.6 \text{ mbar}$$

$$P_2 = 993.6/7 \text{ mbar}$$

$$P_3 = 979.6/7 \text{ mbar}$$

$$T = 22.1^\circ\text{C}$$

at 11H50

↳

$$P_1 = 993.5/6 \text{ mbar}$$

$$P_2 = 993.7/8 \text{ mbar}$$

$$P_3 = 979.2/3 \text{ mbar}$$

$$T = 22.1^\circ\text{C}$$

$$\text{Battery} = 12.08 \text{ V}$$

U. H. 1999

# GS FLOW RATE 105

At 12H05

Battery = 12.06 V

$P_1 = 993.3/4$  mbar

$P_2 = 993.6/7$  mbar

$P_3 = 978.5/6$  mbar

$T = 22.2^\circ\text{C}$

$h_D = 150$  mmr

Tunnel pressure lowered

$P_1 = 938.4/5$  mbar

$P_2 = 993.6$  mbar

$P_3 = 978.3/4$  mbar

$T = 22.2^\circ\text{C}$

$h_D = 149$  mmr

Pressures readjusted  $\Rightarrow$

$P_1 = 938.8/9$  mbar

$P_2 = 993.6/7$  mbar

$P_3 = 979.3/4$  mbar

$T = 22.2^\circ\text{C}$

$h_D = 155$  mmr

Dike valve closed / gate opened at  $t = 0$

$h_{\text{dike}}$ (mmr)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T(^{\circ}\text{C})$
155	0	938.8/9	993.6/7	979.3/4	22.2
160	2.26	942.5	942.1	975.7	
180	6.19	940.0	940.4	975.9	
200	11.89	939.5	939.8/9		
220	17.92	939.1	939.5	976.8	
240	24.95	938.7	939.2	977.1/2	
260	33.45	938.4	938.7	977.5/6	
280	43.38	938.1/2	938.5	977.7/8	
300	53.54	937.9/938.0	938.2/3	978.0	
320	1'06.45	937.7	938.1/2	978.1/2	22.3
340	1'21.60	937.5/6	938.0	978.3/4	-
360	1'39.13	937.3/4	937.8	978.5	-
380	2'01.01	937.2	937.6/7	978.7	-
390	2'13.83	937.1/2	937.6	978.8	-
400	2'28.23	937.1	937.5/6	978.9	
410	2'43.51	937.0/1	937.4/5	979.0	
420	2'59.57	936.9/937.0	937.4	-	
428.5	3'15.79	-	-	-	
435	3'30.67	-	-	-	

11.11.1999

Gate closed at 3/30.67 when GS reached the bottom of the tunnel entrance

$$\begin{array}{l|l} \Rightarrow & P_1 = 936.2/3 \text{ mbar} \Rightarrow 993.0/1 \text{ mbar} \\ & P_2 = 993.6 \text{ mbar} \\ & P_3 = 979.3 \text{ mbar} \\ & T = 22.4^\circ\text{C} \end{array}$$

H. H. 1999

*[Signature]*



# GS FLOW RATE 106

At 13H35

Battery = 11.96 V

$P_1 = 991.9/992.0$  mbar

$P_2 = 992.8/9$  mbar

$P_3 = 977.8/9$  mbar

$T = 22.8^\circ\text{C}$

$h_D = 153$  mm

Tunnel pressure lowered down to 962.8/9 mbar  
Dike valve closed / gate opened at  $t = 0$

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ ( $^\circ\text{C}$ )
153	0	962.8/9	992.7/8	977.6/7	22.9
160	3.76	964.7	965.6	975.4	-
180	12.83	963.9	964.6	975.8	22.9
200	23.79	963.3	964.2	976.2	-
220	37.26	962.9/963.0	963.7/8	976.5	-
240	54.54	962.6	963.5	976.7	-
250.25	1'05.19	962.4	963.3	976.8/9	-
260	1'17.51	962.3	963.1/2	976.9/977.0	-
270	1'31.23	962.2	963.0	977.0	-
280	1'47.26	962.0/1	962.9	977.2	-
290	2'05.42	961.9	962.7/8	977.2/3	-
300	2'29.17	961.8	962.6	977.3/4	22.9
309.5	2'57.17	961.6	962.5	977.4	-
317	3'23.45	961.5/6	962.4	-	-
320	3'36.69	961.4/5	-	977.4/5	-
324.5	3'55.51	-	962.3/4	-	-
329.5	4'30.01	961.3/4	962.3	977.5	-
334	5'01.01	961.3	962.2/3	-	-
337.75	5'39.73	-	962.1/2	977.5/6	-

Video stopped at 6'01.48

340	6'11.48	961.2/3	962.1/2	977.5/6	22.9
343	7'01.63	961.1/2	962.1	-	-
345	7'48.51	-	962.0/1	977.6/7	-
346.75	8'37.17	-	-	977.6	-
348	9'55.95	961.1	-	977.5/6	-
349.25	11'44.67	961.0/1	961.9/962.0	977.6	-
350	14'03.01	-	-	-	-
350	16'01.57	960.9/961.0	961.9	977.5/6	-

$h_{\text{dike}}$ (mm)	time	$P_1$ (mbar)	$P_2$ (mbar)	$P_3$ (mbar)	$T$ (°C)
350.5	18'15.17	960.8/9	961.8/9	977.5/6	23.0
-	20'47.60	-	-	977.5	-
351	23'51.89	960.7/8	961.7/8	-	-
-	26'05.45	960.7	961.6/7	977.4/5	-
-	28'51.45	960.6/7	-	977.4	-
-	31'27.57	-	-	-	-
-	33'37.35	960.6	-	-	23.1
-	34'25.67	960.5/6	961.5/6	977.3/4	-
-	35'01.57				

Gate closed after 35'01.57 at 14H15  $\Rightarrow$


$P_1 = 960.1/2$  mbar  
 $P_2 = 961.1/2$  mbar  
 $P_3 = 977.3/4$  mbar  
 $T = 23.1^\circ\text{C}$

Battery = 1.90 V

$\Rightarrow$ 
 $P_1 = 991.9$  mbar  
 $P_2 = 992.5/6$  mbar  
 $P_3 = 978.4/5$  mbar

11. 11. 1999

*[Signature]*

И. И. 1999  


GS FLOW RATE 108

At 15H50

Battery = 11.78 V

$P_1 = 991.516 \text{ mbar}$

$P_2 = 992.415 \text{ mbar}$

$P_3 = 977.213 \text{ mbar}$

$T = 23.4^\circ \text{C}$

$h_D = 152 \text{ mm}$

Tunnel pressure lowered down to 926.718 mbar at 15H55  
Dike valve closed / gate opened at  $t=0$

$h_{\text{dike}} (\text{mm})$	time	$P_1 (\text{mbar})$	$P_2 (\text{mbar})$	$P_3 (\text{mbar})$	$T (^\circ \text{C})$
152	0	926.718	992.5	977.1	23.4
160	2.16				
180	5.31	928.4	929.2	972.7	
200	9.25				
220	13.19				
240	17.75	926.9	927.8	973.8	
260	23.41	926.5	927.4	974.2	
280	29.57	926.1	927.0	974.6	
310	40.03				
320	44.34	925.718	926.6	975.112	
340	53.72	925.5	926.4	975.4	23.4
360	1'03.44	925.3	926.213	975.7	-
380	1'16.16	925.112	926.011	975.819	-
400	1'30.94	924.9/925.0	925.9	976.1	-
420	1'47.34	924.819	925.819	976.3	-
435	2'02.16	924.8	925.718	976.3	-

Gate closed / valve opened at 2'02.16 when GS reached the tunnel entrance at 16H00



$P_1 = 924.112 \text{ mbar}$

$P_2 = 992.5 \text{ mbar}$

$P_3 = 979.1 \text{ mbar}$

$T = 23.4^\circ \text{C}$



$P_1 = 991.819 \text{ mbar}$

$P_2 = 992.415 \text{ mbar}$

$P_3 = 978.819 \text{ mbar}$

11. 11. 1999

At 16H40

$P_1 = 991.6/7 \text{ mbar}$   
 $P_2 = 991.9 \text{ mbar}$   
 $P_3 = 977.3/4 \text{ mbar}$   
 $T = 23.2^\circ\text{C}$   
 $h_D = 153 \text{ mm}$

Pump switched off at 16H42

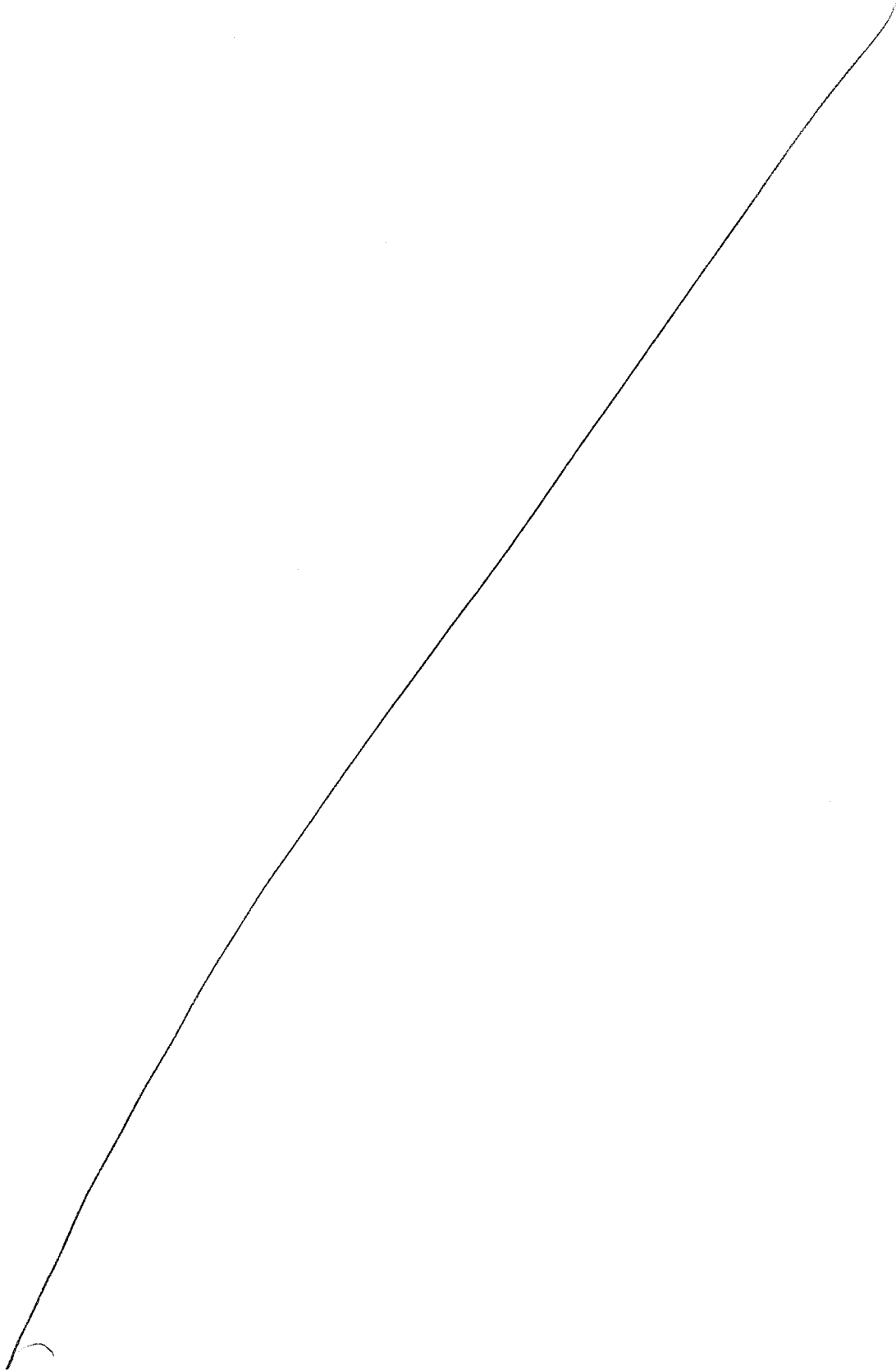
Battery = 11.83V  $\Rightarrow$  start charging at 16H44

At 17H50

$P_1 = 991.6/7 \text{ mbar}$   
 $P_2 = 991.7/8 \text{ mbar}$   
 $P_3 = 991.6/7 \text{ mbar}$   
 $T = 22.9^\circ\text{C}$   
 $h_D = 243.5 \text{ mm}$

11.11.1999

Flow rate experiments  
with DGS 5  
(expt no 109 to 123)



09.09.2000

A handwritten mark or signature, possibly a stylized letter 'L' or a similar symbol, located below the date.

02.09.00

11 H35

Expt 109

0685

①

$$\begin{cases} P_1 = 984.6/7 \\ P_2 = 983.3/4 \\ P_3 = 984.6/7 \end{cases}$$

$$T = 20^\circ \text{C}$$



$$h_{\text{dike}} = 32 \text{ mm}$$

02.09.00

$$H_{\text{res}} = \underset{\substack{485 \\ \text{07.03.02}}}{h} - \underset{\substack{\text{07.03.02}}}{399.5 \text{ mm}} = 92.5 \text{ mm}$$

$$N_2 \text{ gate} = 800 \text{ kPa}$$



$$\begin{cases} P_1 = 984.6/7 \\ P_2 = 983.3 \\ P_3 = 943.4/5/6/7/8 \end{cases}$$

02.09.2000



02.09.2000

(2)

11H45

⇒  $P_1 = 984.5/6$   
 $P_2 = 983.2/3$   
 $P_3 = 934.8/2/3$

$P_1$  984.5/6  
 $P_2$  (valve closed) 983.3/2  
 $P_3$

944.0 → 944.7  
 Not very stable

↳ redirect tunnel to  
 vac. req n° 1

02.09.2000

5m 1.08

10cm 5.08

13 7.49

15 9.40

18 12.24

20 14.68 934.5

24 20.65

26 24.30 931.4/5

28 28.93 930.4/5

31 37.93 929.5/6

33 - 929.1

34 51.68 928.8/9

02.09.2000

02.09.2000

360 1'05.47 928.3/4

370 1'16.12 928.1/2

380 1'31.06 { 927.9  
928.0

res 984.5

983.2

390 1'57.18

984.5

983.2

927.7/8

395 2'16.47 984.4/5 983.2 927.7/8

397 2'33.27 (927.7) 984.5 983.2

398.75 3'03.21 984.5 983.2 927.6/7

400.75 3'41.62 984.5 983.2 927.6/7

400.75 4'33.03 984.5 - 927.5

401.75 5'35.03 - 983.1/2 -

402.75 7'27.03 984.4/5 983.1 927.4

same 8'53.30 984.4/5 983.1/2 927.3/4

02.09.2000

02.09.00

20°C

3

Same 10' 19.12

984.4/5 983.1/2 927.3

✓ 403. ~~25~~ 12' 56.24

984.5 983.2 927.3

✓ 403.5 15' 19.97

984.5/4 983.1/2 927.2/3

404 ~~25~~ 19' 32.56  
25

984.5/6 983.2 927.2

404.5 22' 46.90  
25 07.03.02

984.5/6 983.2/3 927.1/2

405 ~~25~~ 28' 49.65  
25 07.03.02

984.5/4 983.2/11 927.0  
926.9

407 45' 21

984.3/4 983.0 926.7

20°C

Same 52.37

984.2/3 982.9 926.5

same 1100 min 4

984.2 982.8/9 926.4/5

Stop at 12 HSS

404.25  
404/5

$$\Delta P = 58 \text{ mbar}$$

02.09.2000

Expl 110

02.09.00

DE85

At 134 40

$$\begin{cases} P_1 = 983.4 \\ P_2 = 982.2/1 \\ P_3 = 983.4 \\ T = 20.5^\circ\text{C} \end{cases}$$

$$P_{N_2} = 800 \text{ kPa}$$
$$h_{dyke} = 31.5 \text{ mm (still a bit on walls)}$$

$$\rightarrow \begin{cases} P_1 = 983.3 \\ P_2 = 982.0 \\ P_3 = 953.0 / 952.9 \end{cases}$$

02.09.2000

6	2.23			
8	4.69			
10	7.02	959.1		
15	15.33	954.3		
18	23.23	952.6		
20	30.87	951.5		
22	42.58	950.6		
23	52.29	950.2	983.3 <sup>1</sup>	982.0 <sup>2</sup>
24	1'07.77	949.9	-	-/1
246.25	1'29.02	949.8	-	982.0/1
25	2'11.55	949.6/7	983.3	982.0
251.5	3'16.70	949.6	-	982.0/981.5
same	4'17.96	949.5/6	983.2/3	981.9
same	5'22.52	949.4/5	983.1/2	981.9
252	14'48.80	949.2	983.0	981.7 <sup>9</sup>
closed 14H05	252	16'50.36	949.1	983/982.9 981.7

$T = 21^{\circ}\text{C}$

02.09.2000

*[Signature]*

# Expt III

02.09.00

At 14H35

$$\begin{cases} P_1 = 982.4/3 \\ P_2 = 981.2 \\ P_3 = 982.4 \\ T = 21^\circ\text{C} \end{cases}$$

↳ 15H05

$$\begin{cases} P_1 = 981.7/8 \\ P_2 = 980.5/6 \\ P_3 = 972.0/971.9 \\ T = 21^\circ\text{C} \\ h = 32 \text{ mm} \end{cases}$$

5	3.88	974.8		
7	11.23	973.2	981.7	980.5
9	29.83	972.1	981.7/8	980.5/6
95	47.43	971.9	981.7/8	980.6
96	1' 16.05	971.8	981.8	980.5/6
96.25	2' 22.14	971.8/9	981.7/8	-
96.5	4' 36.61	971.8/7	981.7	980.5/6
96.5	11' 02.02	971.6/7	981.6	980.4
↳ stop 11' 42.80 @ 15H20 219				

02.09.2000

Exp 112

02.03.00

At 15H50

$$\begin{aligned} P_1 &= 981.1/2 \\ P_2 &= 979.9/980.0 \\ P_3 &= 981.1/2 \\ T &= 21^\circ\text{C} \end{aligned}$$

At 15H55

$$\begin{aligned} P_1 &= 981.1/2 \\ P_2 &= 979.9 \\ P_3 &= 937.0 / 936.9 \\ T &= 21^\circ\text{C} \\ h_b &= 32\text{mm} \end{aligned}$$

~~07.03.02~~

5

1.01

9

4.19

950.3

14

8.23

939.3

19

12.89

24

18.67

929.9

02.03.00

29	28.67	927.8		
31	34.35	927.1		
33	41.54	926.5		
34	47.19	926.2		
35	51.79	926.1		
36	59.29	925.8		
37	1'09.48	925.6	981.1979	
38	1'26.26	925.4/5		
387.25	1'46.04	925.3	-	-
39	2'01.35	925.3	-	-
392.8	2'20.42	925.3/4	981.16	979.1/8
393.75	2'43.95	925.3	-	979.8/9
<del>6</del> 07.03.02				
394.25	4'14.48	-	-	
same	7'23.17	925.3/4	981.0/1	979.6/7
same	12'51.26	925.3	980.9	
→ close 13'15.95		T=21°C	16H10	9/2/00 2:07 PM



Exp 11/3 -1

At 16 H 40

07.03.08

$$P_1 = 980.617$$

$$P_2 = 979.514$$

$$P_3 = \cancel{935.2} 937.0/1$$

$$T = 22^\circ\text{C}$$

$$h = 32 \text{ mm}$$

8 3.29

11 5.93 951.0

15 9.89 945.0

19 15.14

21 18.55 939.9

24 24.87

26 30.80 937.7

28 39.83 936.8

30 54.58 936.2 929.4/ 980.6

31 1'08.49 935.9 - -5/-

32 1'39.02 935.7/8 979.4/5 980.5/6

02.09.2000

113-2

02.09.00

		(3)	(2)	(1)
323.5	2'22.46	935.7/8	979.4/5	980.5/6
same	4'54.67	935.8/9	979.4/5	980.5/6
—	8'21.27	935.7/8	979.3/4	980.5
	↳ stop			

02.09.2000

Exp 11/4-1

At 17 H<sub>2</sub>S

$$\left\{ \begin{array}{l} P_1 = 980.3/4 \text{ mbar} \\ P_2 = 979.2/3 \text{ mbar} \\ P_3 = 961.2/3 \text{ mbar} \\ T = 22^\circ\text{C} \\ h = 32 \text{ mm} \end{array} \right.$$

→ P<sub>3</sub> 959.5

5 1.66

7 4.78 967.3

9 8.41 964.7

11 13.03 962.9

13 20.16 961.3

14 25.22 960.7

15 32.03 960.2

16 45.59 959.7/8 (1) 980.4 (2) 979.3

165.25 1103.19 959.6 980.3/4 979.3/

167.5 2103.50 959.5 980.3/4 979.1'

T=22°C same 3138.63 959.5 980.3/4 979.2/3

02.09.2000

Expt 114-2

02.09.00

same

5'02.34

959.516

980.3/4

979.2/3

same

10'07.88

959.6

980.3

979.2

↳ closed

02.09.2000

Expt 115

02.09.00

17H40

$$\begin{aligned} p_1 &= 980.2/3 \\ p_2 &= 979.1/0 \\ p_3 &= 976.1/0 \\ h &= 32 \text{ mm} \\ T &= 25^\circ\text{C} \end{aligned}$$

4 2.12 977.6

5 10.06 976.7

54.5 20.5g 976.5/6 980.3 979.1/2

56.5 51.21 976.4/5 980.2/3 -

- 2'26.12 976.4/5 980.3 978.1/2

- 4'41.21 976.4/5 980.3/4 979.1/2

- 5'26.37 (closed) 976.5 -

T = 21.5°C  
17H50

02.09.2000

needs  $h_d = 110 \text{ mm}$

86/11  
76/10

07.03.02

$$h_d = 243.5 \text{ mm}$$

→ atm

→  $P_{\text{such}} h_d \approx 110$   
/ 50

$$h_d = 180$$

07.03.02

---

200.5

02.09.2000

n 35

110

34 mbar

252 mm

n 10

111

10 mbar

96.5 mm

2.09.2000

n ~~54~~ 112

55 mbar

~~6~~

n ~~55~~ 113

44 mbar

45

n ~~55~~ 114

21 mbar

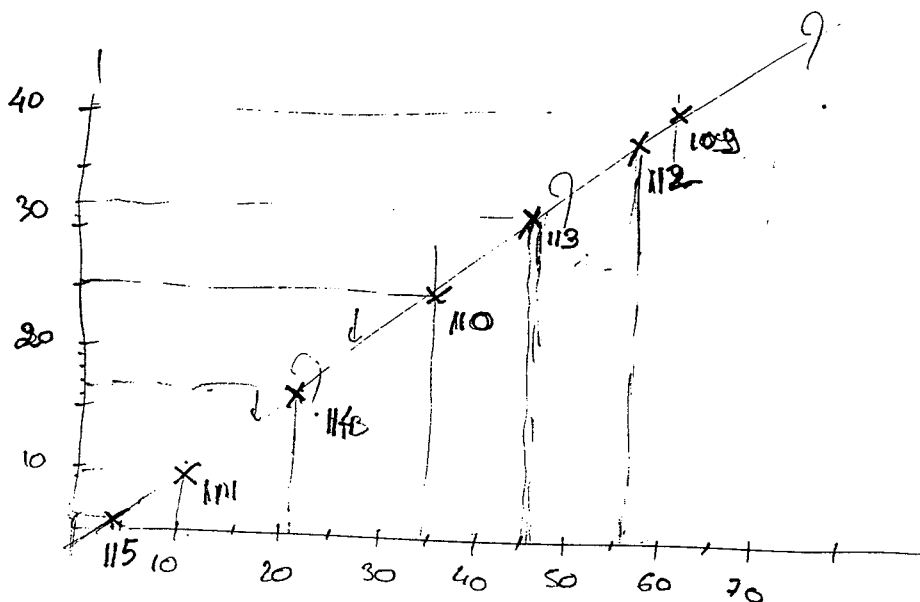
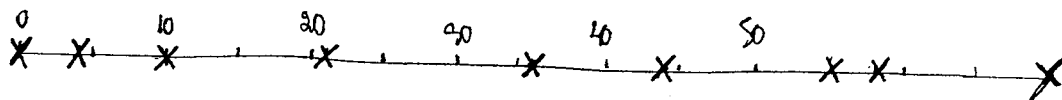
20

n ~~55~~ 115

4 mbar

70

→ fill up w/ more GS



02.09.2000

Exp'r 1/6-1

02.09.00

At 18H00

$$\left\{ \begin{array}{l} P_1 = 980.3/4 \\ P_2 = 979.2/3 \\ P_3 = 915.5/6 \\ T = 21.5^\circ\text{C} \\ h_d = 32 \text{ mm} \end{array} \right.$$

6 1.18

9 3.49 952.9

15 7.93 935

20 11.93

25 16.03 919

29 20.30 915.6

33 26.03 913.6

36 31.62 912.5/9

39 38.49 911.6/5

41

02.09.2000



43 53.43

909.2

~ 56 ~ closed gate 909.2/3

18H02

$$\begin{cases} P_1 = 980.4/5 \\ P_2 = 979.2/3 \\ P_3 = 909.4/5 \end{cases}$$

check  $\begin{cases} h_{res} = H - 392.5 \end{cases}$

At 18H25  $\begin{cases} h_{dyke} = 32 \text{ mm} \\ \begin{cases} P_1 = 980.3/4 \\ P_2 = 979.1/2 \\ P_3 = 980.3/4 \end{cases} \end{cases}$

$T = 21^\circ\text{C}$

In prep of expt

117 more GS added to reservoir

$$\begin{cases} h_{\text{dike}} = H - 315 \text{ mm} = 170 \\ h_{\text{res}} = ~~108~~ 108 \text{ mm} \end{cases}$$

18A40

07.03.02

prepare more GS at 5%

big 10l bottle = 3093.6/7 g

$$+GS = -4255.5/6 = 161.9 \text{ g GS}$$

07.03.02

58.095 H<sub>2</sub>O

Th. Tot weight 4313.7

Real 4313.8/8 g

07.03.02

02.09.2000

Expt 117

①

18H55

$$\begin{cases} h_{res} = H - 31.5 \text{ cm} = 170 \text{ mm} \\ h_{dike} = 108 \text{ mm} \end{cases}$$

$$\begin{cases} T = 21.5^\circ\text{C} \\ P_1 = 980.5/6 \\ P_2 = 979.3/4 \\ P_3 = 980.4/5 \end{cases}$$

$$\hookrightarrow \begin{cases} P_1 = 980.4/5 \\ P_2 = 979.3/4 \\ P_3 = 970.7/6 \end{cases}$$

~~07.03.02~~

Expt 117

(2)

Lab # = 522

02.09.00

12	3.49	973.2		
14	10.67	971.8		
15	16.27	971.4	980.5	979.3
16	24.58	970.8	980.4	979.3/4
17	42.77	970.4	980.5	979.4
173.75	1' 16.02	970.3	980.5	979.3/4
174.75	1' 41.89	970.2	980.4/5	979.3/4
175.5	2' 41.08	970.1/2	980.4/5	979.3
same	3' 57.33			
176	5' 13.27	970.1	980.4/5	-
same	7' 17.93	970.0/1	980.5/4	979.3/4
same	8' 23.02	970.0/1	980.5	979.3/4
same	9' 45.39	970.0/1	980.5/6	-
-	10' 02.17 closed			

$$\begin{cases} p_1 = 980.5 \\ p_2 = 979.3/4 \\ p_3 = 969.3/4 \\ T = 21^\circ\text{C} \end{cases}$$

19410

02.09.2000

At 19 HIS

$$\begin{cases} P_1 = 980.6/5 \\ P_2 = 979.3/4 \\ P_3 = 951.3/4 \\ T = 21^\circ\text{C} \\ h = 108.5 \text{ mm} \end{cases}$$

13	2.28	9663.9		
16	6.16	958.9		
19	10.91	955.2		
21	14.85	953.6		
23	19.57	952.1		
25	25.78/95	1.1		
27	34.22	950.1		
29	47.69	949.3	979.4/80.6	
30	1'00.07	948.9	-	980.5/6
31	1'19.16	948.6	979.3/4	980.6
315 <del>317.25</del>	1'43.66	948.5	979.3/4	980.5/6
317.5	2'26.34	948.4	979.3/4	-
same	3'25.59	948.4	-	-
317.7	4'32.47	948.4	-	-

02.09.2000



318  
~~same~~  
07.03.02  
348

7'31.88

948.4

979.3/4

980.5/6

9'14.37

T = 21°C

348

10'23.07

318

10'34.13  
closed

LL

19130

P<sub>1</sub> = 980.6/5

P<sub>2</sub> = 979.3/4

P<sub>3</sub> = 947.8

T = 21°C

At 9425

$$\left\{ \begin{array}{l} P_1 = 983.6/7 \\ P_2 = 982.2 \\ P_3 = 983.6/7 \\ T = 19^\circ\text{C} \\ h_g = 108\text{ mm} \\ h_R = 1 - 315 \end{array} \right.$$

Expt 119-1

At 9435

$$\left\{ \begin{array}{l} P_1 = 983.7/8 \\ P_2 = 982.3/4 \\ P_3 = 963.9/964.0 \\ T = 19^\circ\text{C} \end{array} \right.$$

12	2.13	971.6		
14	6.60	969.0		
16	11.54	967.4		
18	18.51	966.2		
19	23.42	965.7		
20	29.19	965.2		
21	37.57	964.8		
22	50.86	964.4	983.7	982.3/2
23	1'15.54	964.0/1	983.7/8	982.3

03.09.2000



Exp 119-2

③

①

②

234.25

1'47.89

964.0

983.7/8

982.3

236 ~~935.75~~

2'17.45

964.0/963.9

983.7/8

982.13

07.03.02

236.25

2'57.92

964.0/963.9

983.6/7

982.2/3

T = 19°C

same

4'14.01

964.0/963.9

983.7/8

982.3/4

same

6'25.69

964.0/1

983.7/6

982.2/3

same

8'57.23

964.0/1

983.7

982.2/3

T = 19°C

same

10'05.38

964.0/1

~~983.7~~

982.2/3

L → stop @ 10'20.57

07.03.02

$$\begin{cases} P_1 = 983.7 \\ P_2 = 982.3/2 \\ P_3 = 963.9 \\ T = 19^\circ\text{C} \end{cases}$$

9445

03.09.2000



Expt 120

At 9H55

$$\begin{cases} P_1 = 983.8/7 \\ P_2 = 982.3/4 \\ P_3 = 964.0/1 \end{cases}$$

At 10H10

$$\begin{cases} P_1 = 983.8 \text{ mbar} \\ P_2 = 982.5 \text{ mbar} \\ P_3 = 978.9 \text{ mbar} \\ h_d = 108 \text{ mm} \\ T = 19^\circ\text{C} \end{cases}$$

12	7.05	979.5	982.4/5	983.7/8
13	18.43	979.3	-	-
134.75	29.52	979.2	982.5/4	983.8
138	52.33	979.1	982.5/4	983.8
139	1' 30.39	979.0/1	-	-
Same	2' 09.43	979.0/1	982.5	-
same	2' 55.87	-	982.4/5	983.7/8
same	3' 53.55	979.0	-	-
same	6' 05.36	-	982.5	983.7/8
same	7' 23.00	-	982.4/5	-
same	8' 10.03	-	-	-
	↳ closed			↳

03.09.2000

gate closed



$$\begin{cases} P_1 = 983.8 \\ P_2 = 982.4/5 \\ P_3 = 978.9/979.0 \\ T = 19.5^\circ\text{C} \end{cases}$$

10H20

03.09.2000

9/2/00 3:55 PM

# Expt 121-1

At 10H30

$$\left\{ \begin{array}{l} P_1 = 983.7/8 \text{ mbar} \\ P_2 = 982.4/5 \text{ mbar} \\ P_3 = 934.3 \text{ mbar} \\ h_d = 108.5 \text{ mm} \\ T = 19.5^\circ\text{C} \end{array} \right.$$

13	1.77	954.7
18	6.08	949.7
24	12.87	<del>93</del> 9.3
28	19.33	<del>937.4</del> 07.03.02
31	25.61	<del>936.2</del> 07.03.02
33	31.05	935.6
35	38.27	935.0
37	47.05	934.7
39	1'00.17	934.3
40	1'10.55	934.1
41	1'23.58	934.0

Exp 121-2

05.03.00

			(3)	(2)	(1)
42	1' 45.02	933.8	982.4/5	983.7	
42.5/5	2' 05.67	933.7	982.5	983.7/8	
43	2' 38.14	-	-	-	
(431.5) no	432.5	3' 24.39	-	-	
432.5	4' 03.58	933.7/8	982.5/6	983.8	
T=19.5°C	<del>433.5</del>	5' 22.14	933.8	982.5/4	-
434 (433.5)					
same	6' 46.02	-	-	-	
same	8' 47.14	-	982.5/6	-	
T=20°C	same	10' 09.27	933.8/9	982.5/6	983.7/8
same	12' 21.49	-	-	-	
same	14' 11.83	933.8	982.5	-	

↳ close

$$\begin{cases} P_1 = 983.7/8 \\ P_2 = 982.5/6 \\ P_3 = 933.8 \\ T = 20^\circ\text{C} \end{cases}$$

at 10H45

03.09.2000

# Expt 122-1

At 11435

$$\left\{ \begin{array}{l} P_1 = 983.3/4 \text{ mbar} \\ P_2 = 982.2/3 \text{ mbar} \\ P_3 = 943.5/6 \text{ mbar} \\ h = 108.5 \text{ mm} \\ T = 20^\circ\text{C} \end{array} \right.$$

13 1.95 960.1

16 5.13 953.5

20 9.83 949.9

23 14.51 947.5

26 20.48 946.3

28 26.10 945.5

30 33.23 944.8

31 38.01 944.5

32 43.45 944.1

33 50.01

34 58.26 943.9

35 1' 10.86 943.2

36 1' 33.13 943.5 982.1/2 983.2

943.3 982.1/2 983.3

Exp 122-2 03.09.00

365.75 1'56.89

943.2 982.1/2 983.3

368.5 2'27.45

943.1/2 982.1/2 -

369.5 3'06.13

943.1/2 982.0/1 -

T=20°C

same 4'23.42

943.1/2 - -

same 5'25.07

- 982.1/2 983.3/4

same 7'06.79

- 982.0/1 -

same 8'41.01

943.2.3 - 983.3

- 9'55.86

943.1/2 - -

- 10'08.67

- - -

↳ dose

(L)  $\left\{ \begin{array}{l} P_1 = 983.3 \\ P_2 = 982.1/0 \\ P_3 = 943.1/2 \\ T = 20^\circ C \end{array} \right.$

11H45

03.09.2000

Expr 25-1

At  $\text{H}_2\text{O}$ ,

$$\begin{cases} P_1 = 982.9 / 983.0 \text{ mbar} \\ P_2 = 981.7 \text{ mbar} \\ P_3 = 957.2 / 3 \text{ mbar} \\ T = 20.5^\circ\text{C} \\ h = 108 \text{ mm} \end{cases}$$

12	1.66	968.5		
15	6.13	963.6		
18	12.03	961.3		
20	16.88	960.2		
22	23.97	959.1		
23	28.91			
24	34.66	958.1		
25	42.22	957.8		
26	53.66	957.5	981.6/7	982.9/8
27	1'16.37	957.2	981.7	982.9
274.5	1'44.41	957.1	981.6/7	982.8/9
276	2'23.66	957.0/1	-	982.9
		$T = 20.5^\circ\text{C}$		
276.25	3'25.85	957.0/1	-	-

03.09.2000

# Exp 123-2

03.09.00

		③	②	①
276.5	4'35.47	957.1	981.7/6	982.9
same	6'48.03	957.0/1	981.7/6	982.8/9
same	7'35.34	-	-	-
T = 20.5°C				
same	8'31.44	-	-	982.8
same	9'23.47	957.0	981.5/6	982.8
same	10'54.25	-	981.5/6	-
same	11'35.19	-	-	-
gated closed				

12H45

$\Rightarrow$ 

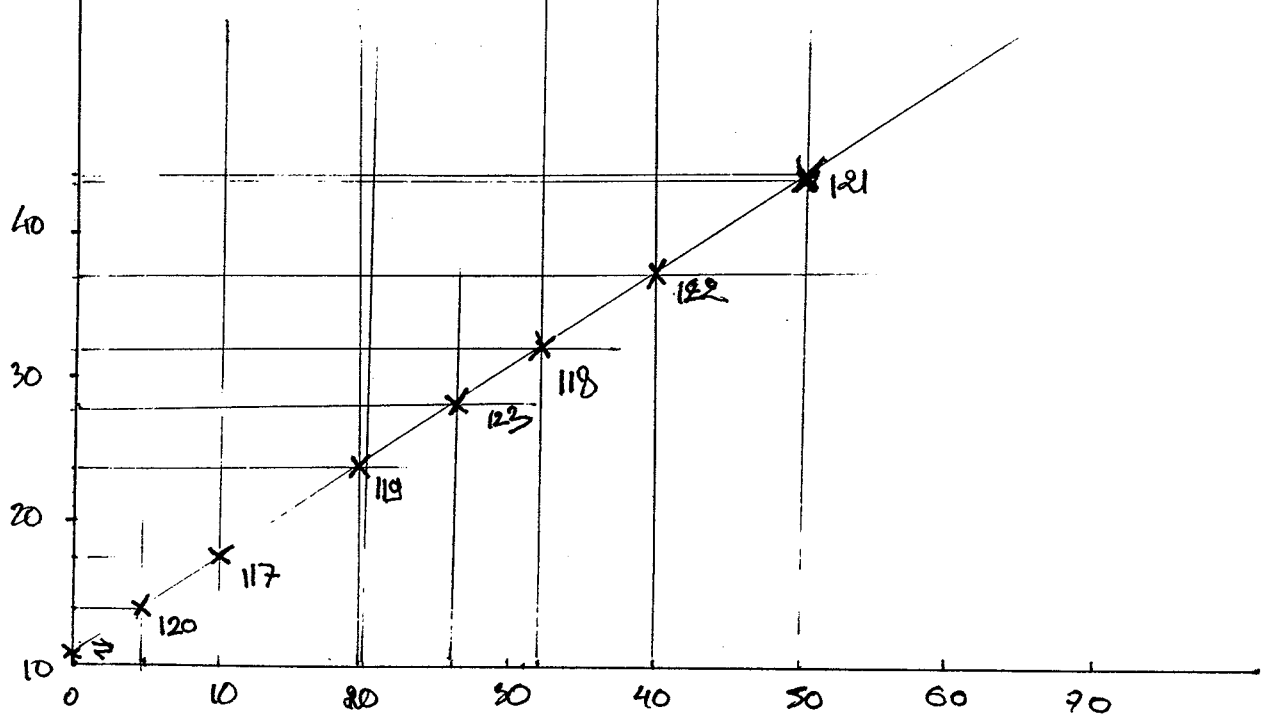
$$\begin{cases} P_1 = 982.8 \text{ mbar} \\ P_2 = 981.5/6 \text{ mbar} \\ P_3 = 956.9/957.0 \text{ mbar} \\ T = 20.5^\circ \text{C} \\ h = \\ H_{res} = H - \end{cases}$$

$\Rightarrow$  tunnel expts  
 with  $h_{dike} = 108 \text{ mm}$

03.09.2000

*[Signature]*



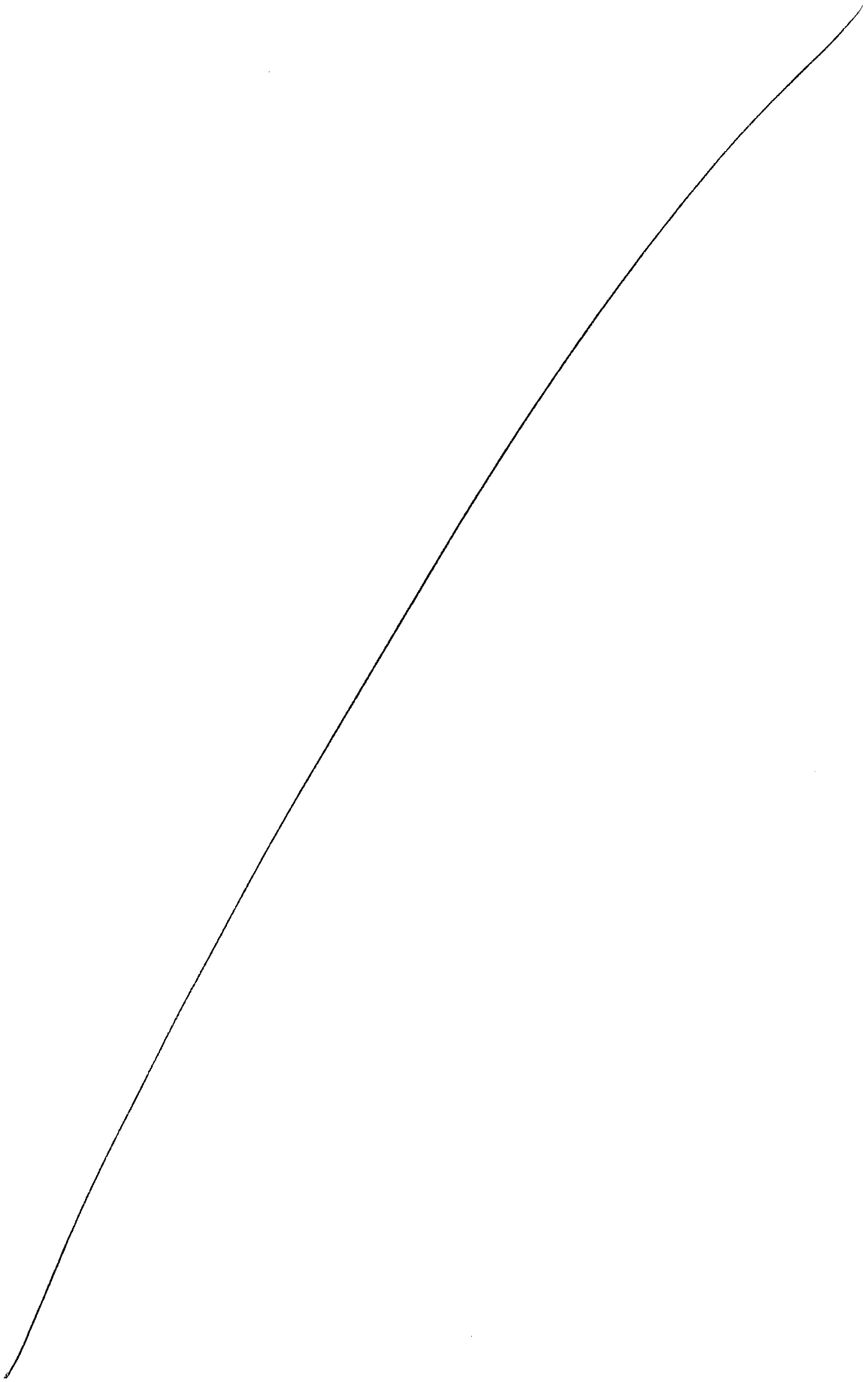


02.09.00		117	10 mbar	
		118	32 mbar	$\sim 318 \text{ mm}$
03.09.00	$\sim 20$	119	19.8 mbar	236 mm
	$\sim 15$	120	4.8 mbar	139 mm
	$\sim 20$	121	50 mbar	433.5 mm
	$\sim 40$	122	40.2 mbar	369.5 mm
	$\sim 25$	123	26 mbar	276.5 mm

03.09.2000

*[Signature]*

Flow rate experiments  
with DGS15  
(expt no 124 to 130)



06.09.2020 k'

Expt 124-0  
DGS15

Wedn. 06.09.00

(1)

At 9H30

$$P_1 = 983.5/6$$

$$P_2 = 982.4/5$$

$$P_3 = 983.7/8$$

$$T = 20^\circ\text{C}$$

$$h_d = 149.5 \text{ to } 150.5 \text{ mm}$$

$$h_{\text{res}} = H - (279 \text{ to } 280 \text{ mm})$$

Remove some DGS15 from reservoir & prepare for adyke expt.

At 10H25

$$P_1 = 983.8/9$$

$$P_2 = 982.6/7$$

$$P_3 = 984.0/983.9$$

$$T = 19.5^\circ\text{C}$$

$$h_d = 105 \text{ mm} \Rightarrow \text{add a bit more}$$

$$N_2 \text{ gate} = \boxed{800 \text{ kPa}} \\ \boxed{810}$$

07.03.02

07.03.02

At 10H55

$$P_1 = 983.8$$

$$P_2 = 982.6/7$$

$$P_3 = 983.9/984.0$$

$$T = 19.5^\circ\text{C}$$

$$h_d = 108 \text{ mm}$$

$$h_{\text{res}} = \text{same as GSW5} = 170 \text{ mm}$$

06.09.2000

EXP 121  
DGS15

At 11H15

$$\left\{ \begin{array}{l} P_1 = 983.8/9 \\ P_2 = 982.6/5 \\ P_3 = 963.4/5 \\ h_d = 108 \text{ mm} \\ T = 19.5^\circ \text{C} \end{array} \right.$$

②

DGS15

Video from 33:26:26

$$P_1 = 983.9/984.0$$

$$P_2 = 982.7$$

$$P_3 = 963.2/3$$

$$T = 19.5^\circ \text{C}$$

at 11H20

15	2.71	975.0		
18	7.09	970.6		
20	10.71	968.2		
22	15.56	966.0		
23	19.65	964.5		
24	26.49	963.8		
248.75	45.47	963.1	961.7/8	983.8
249.00 (75)	1'45.15	963.1	961.8	983.8/9
249.00 (25)	3'25.93	963.1	961.8	983.8/9
same	5'20.33	963.1/2	961.8/9	983.8

06.09.2000

h

Expt 124-2  
06815

06.05.00  
(3)

249 (.25) 6'23.74

963.1/0 961.8 983.8.

249 (.25) 6'41.68 closed



NH30

$$P_1 = 983.8$$

$$P_2 = 964.4/5$$

$$P_3 = 962.1$$

$$T = 19.5^\circ \text{C}$$

06.09.2000

Expt 125-1  
DGSIS

(4)

At VMSS

$$\begin{cases} P_1 = 983.5/4 \\ P_2 = 981.8.9 \\ P_3 = 943.5/6 \rightarrow \text{had to recalculate after} \\ T = 19.5^\circ\text{C} \\ h = 108 \text{ mm} \end{cases}$$

dosing a value in chart  
(942.8)

0
0
0

$$\hookrightarrow P_3 = 943.7/8$$

15	1.01	973.5	
19	4.69	966.9	
25	9.95	958.0	
30	15.54	950.4	
34	22.23	946.6	
36	28.45	944.8	943.5
37	35.13	944	942.8
376 <sup>25</sup> or 3765	47.60	943.7	942.4
"	1' 19.19	943.8/7	942.6/7
"	2' 09.60	943.8/9	942.7/8
			983.4/5
			983.4/5
			983.4/5

06.09.2000

Expt 125-2  
DGSIS

376.5  
(5)

376.5 (er. 25) Sum	3'40.42 5'14.83	943.8/9	942.7/6	983.3/4
--------------------------	--------------------	---------	---------	---------

↳ closure

12 M 10

$$\left\{ \begin{array}{l} P_1 = 983.3/4 \\ \cancel{P_2 = 946.2} \quad P_2 = 982.2 \\ P_3 = 942.5/4 \quad 982.2/3 \\ T = 19.5^\circ\text{C} \end{array} \right.$$

07.03.02



At 12H30

$$\begin{cases} P_1 = 983.1/0 \\ P_2 = 982.1/0 \\ P_3 = 953.3/2 \\ T = 20^\circ\text{C} \\ h_d = 108 \text{ mm} \end{cases}$$

15 1.69 973.5

19 5.85 967.3

23 10.57 961.9

26 15.50 957.9

28 20.63 956.0

29 24.94 955.1

30 32.16 954.3

305 42.53 953.9 952.9 983.0/1

306 103.53 953.9/954.0 952.9 983.1/0  
953.0

305.5 156.82 954.0/1 953.0/1

305.5 231.37 - - 983.0/1

305.5 345.78 - - -

- 418.31 954.1 953.1 983.0/1

Expt 126-2  
DGSIS

⑦

	$P_3$	$P_2$	$P_1$	
305.5	4147.37	954.1/0	953.0/1	983.0/1

closure

12H35

$$\left\{ \begin{array}{l} P_1 = 983.0/1 \\ P_3 = 952.0/953.0 \\ T = 20^\circ\text{C} \\ P_2 = 981.9/982.0 \end{array} \right.$$

06.09.00

06.09.2000

Exp 127-1

DGS15

(3)

At 12 HSS

$$\left\{ \begin{array}{l} P_1 = 982.718 \\ P_2 = 981.6 \\ P_3 = 972.819 \\ T = 20^\circ\text{C} \\ h = 108 \text{ mm} \end{array} \right.$$

13	2.15			
15	6.56	975.7		
16	10.47	974.6		
17	20.27	973.6	972.2/3	
172	31.93	973.3/4	972.0/1	982.7
172.5	1'04.27	973.2/3	972.0/1	982.7
-	1'49.18	-	-	982.6/7
-	2'29.62	-	-	-
-	3'06.03	-	972.0/1	-
-	3'49.43	973.2	971.9/972.0	982.6
-	4'25.18	-	-	-
-	4'47.71	-	-	-

(C) closure  $\Rightarrow P_1 = 982.617_{13400}$   $P_3 = 972.7$   $T = 20$

06.09.2000

# Expt 128

DGS15

At 13 M10

$$P_1 = 982.4/5$$

$$P_2 = 981.4/3$$

$$P_3 = 977.3/4$$

$$T = 20.5^\circ\text{C}$$

$$h = 108 \text{ mm}$$

12

0.96

13

4.58

978.2

14

13.14

977.6

976.3

142

23.23

977.5

976.2

982.4

142.5

53.83

977.4/5

976.2/3

982.4

142.5

1'24.93

-

-

-

-

1'57.33

-

-

982.4/5

-

2'27.02

-

-

-

3'14.08

977.4

976.1/2

982.3/4

-

3'52.55

-

-

-

closure =>

$$P_1 = 982.3/4$$

$$P_3 = 977.3$$

$$P_2 = 976.8/9$$

$$T = 20^\circ\text{C}$$

13 M15

06.09.2000



Exp 129-1

DGS 15

10

At 13H25

$$P_1 = 982.2$$

$$P_2 = 981.2$$

$$P_3 = 932.8/9$$

$$T = 20^\circ\text{C}$$

$$h = 108 \text{ mm}$$

Ready  $\left| \begin{array}{l} P_1 = 982.2/3 \\ P_2 = 981.1 \end{array} \right.$

$$P_3 = 933.0$$

15	0.65	
19	4.18	965.7
24	8.15	957.4
29	12.81	949.0
34	17.65	943.4
39	22.59	937.8
41	28.18	935.3
43	34.90	932.9
closed gate	40.47	

↳

$$P_1 = 982.2$$

$$P_3 = 932.2$$

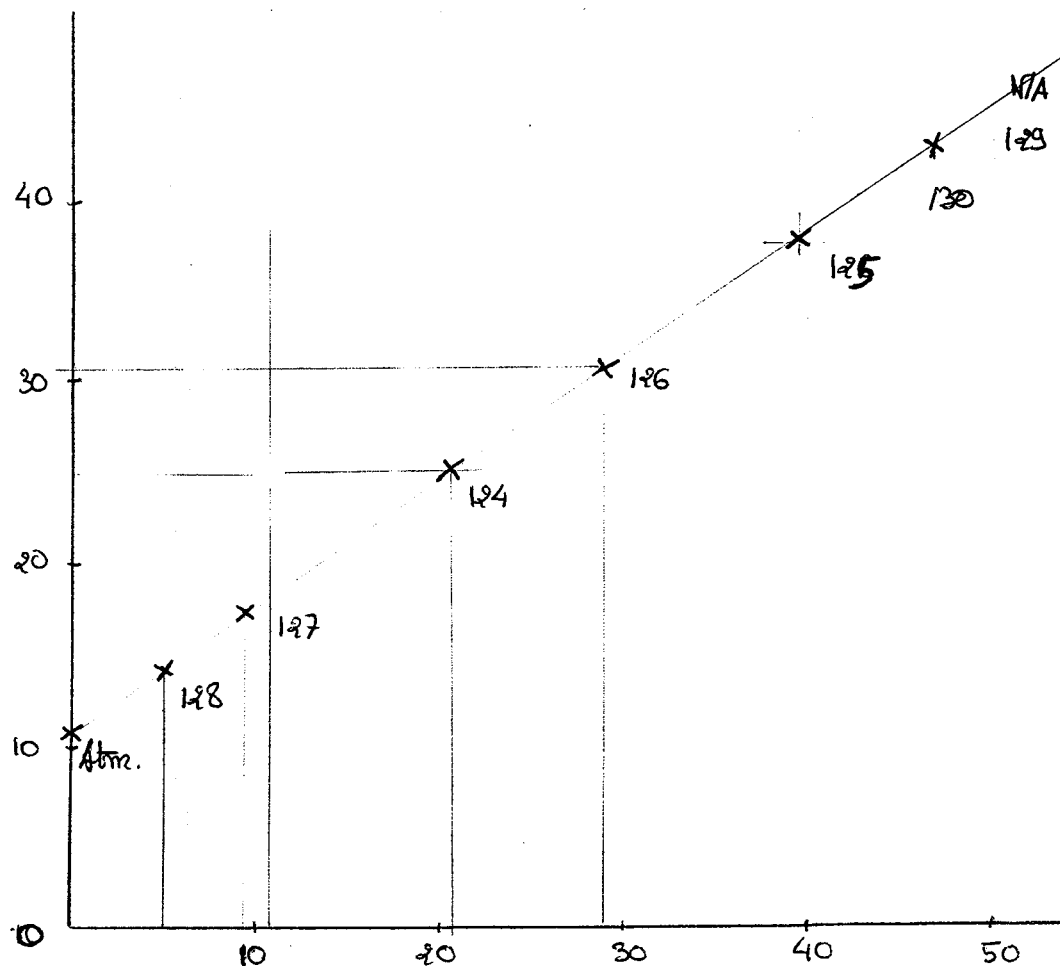
13H35

$$T = 20.5^\circ\text{C}$$

06.09.2000



DG815



Expt#	$\Delta P(\text{mbars})$	$h(\text{mm})$
124	20.7	249
125	39.5	376.5
126	29.0	305.5
127	9.4	172.5
128	5.0	142.5
129	$\sim 50.0$	N/A

Expt#	$\Delta P(\text{mbars})$	$h(\text{mm})$
130	46.8	425.5

06.09.2000

*[Signature]*

Exp 120-1  
DGS 15

(11)

ISHD5

$$P_1 = 980.8/9$$

$$P_2 = 979.7/8$$

$$P_3 = 944.8/9 \rightarrow \text{readjust to } 945.7/8$$

$$T = 21^\circ \text{C}$$

$$h = 108 \text{ mm}$$

$$\Delta P = 35!$$

1/6

↓  
readjust  
to 935.7/8 mbar

~~$P_3 = 945.8/9$~~  607.03.02

ISH10

$$P_1 = 980.7/8$$

$$P_2 = 979.7$$

$$P_3 = 935.6/7$$

$$T = 21^\circ \text{C}$$

06.09.2000



Expt 130-2  
D6515

15	.088			
20	5.13		952.9	
25	9.41		954.2	
30	14.19	94	7.0	
35	19.85		940.6	
39	26.63		936.7	
41	32.75	939.9	933.8	
42	39.09	939.0	933.1	
427.5	54.37	933.7	932.7	980.8/7
427	1'26.22	933.8/9	932.9/933.0	980.7/8
426.5	2'24.34	933.9/94.0	933.1/0	-
425.5	3'06.69	934.0	933.1/2	-
-	3'37.34	934.0	933.1/2	980.7/8
-	4'00.78	-	-	-
-	4'31.91	934.0/1	933.1/2	-
-	4'48.13	closure $\Rightarrow$ $P_1 = 980.7/6$ $P_3 = 932.3/4$ $P_2 = 940.3/4$ $T = 21^\circ C$		



Expt 130-3  
DGS 15

15H20

$$P_1 = 980.6/7$$

$$P_2 = 979.6/7$$

$$P_3 = 980.8$$

$$T = 21^\circ\text{C}$$

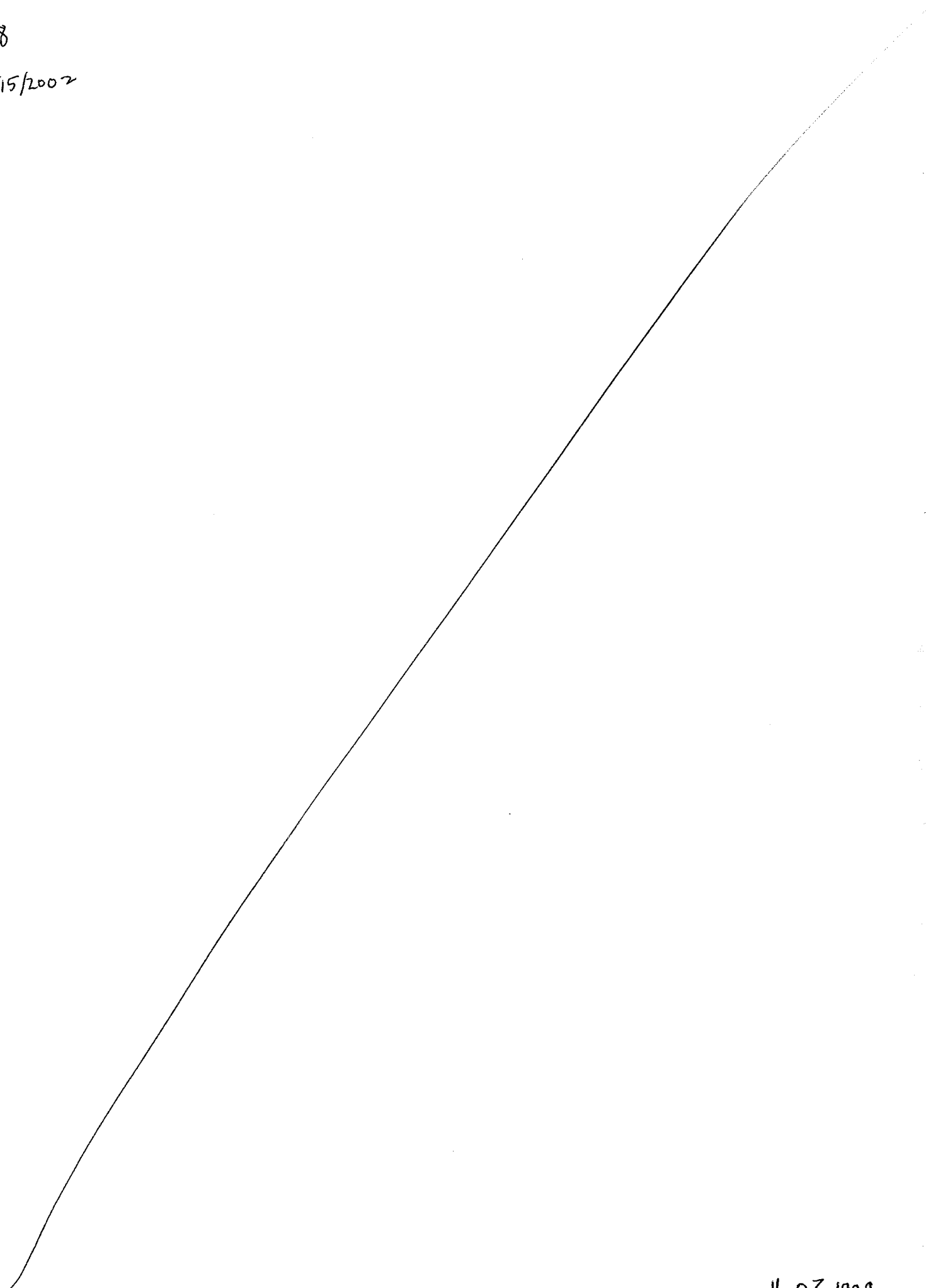
$$h = 108\text{mm}$$

06.09.2000

re = Rebecca Emmot

Tunnel experiments  
with pure golden syrup  
(expt no D to 34)

188  
re  
1/15/2002



11.07.1999

# Tunnel GSO (video)

189  
re 1/15/2002

At atmospheric pressure

$$\begin{array}{|l} \text{GS level in reservoir} = H - 150 \text{ mm} \\ \text{GS level in dyke} = 272 \text{ mm} \\ T = 23.4^\circ \text{C} \end{array}$$

Tunnel visible length = 372.5 mm

Tunnel visible part marked every 20 mm

For the experiment

$$\begin{array}{|l} V_{\text{reservoir}} = 0 \\ V_{\text{dyke}} = 33 \text{ mbar} \\ V_{\text{tunnel}} = 80 \text{ mbar} \end{array}$$

Reservoir valve left opened, dyke valve closed

Mark	Time	
2	5.63	$V_{\text{tunnel}} = 50 \text{ mbar}$
10	12.57	
12	28.00 (?)	
14	40.59	
16	55.88	
18	1' 07.22	
22	1' 35.44	$V_{\text{tunnel}} = 50 \text{ mbar}$ $V_{\text{dyke}} = 36 \text{ mbar}$

07.03.02  
After 3',  $h_{\text{GS}}$  at tunnel entrance = 23 mm

Valve closed at 5' 19.48  $\Rightarrow V_{\text{tunnel}} = 46 \text{ mbar}$

Tunnel GS 1 (video)

$$\begin{aligned} \text{GS height in reservoir} &= 485 - 170.5 \text{ mm} = 315 \\ \text{GS height in dyke} &= 250.5 \text{ mm} \end{aligned}$$

at atmospheric pressure

For the experiment

$$\begin{aligned} V_{\text{reservoir}} &= 0 \\ V_{\text{dyke}} &= 36 \text{ mbar} \\ V_{\text{tunnel}} &= 100 \text{ mbar} \end{aligned}$$

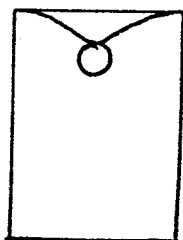
Reservoir valve left opened, dyke valve closed  
level of GS in dyke at the top of the gate

$$\text{---} \bigcirc \text{---} \Rightarrow h =$$

$T = ?$

Gate opened at  $t_0 = 0 \Rightarrow$  initial vacuum drop in tunnel  
back to 36 mbar at 3" 87

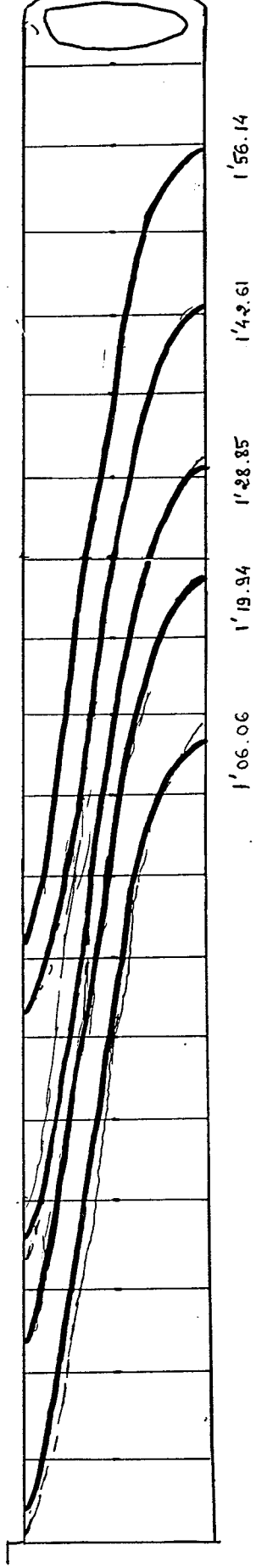
Gate closed at 2' 16.33  $\Rightarrow V_{\text{tunnel}} = 51 \text{ mbar}$   
Valve



191  
re 1/15/200

Tunnel GSI - 100 mbar vacuum

$P = 900 \text{ mbar}$



20.07.1999

192  
re 1/15/2002

Tunnel GSI

Red marks on screen  
(black marks on tunnel)

Bottom

Top

1	13.47	13.26	1' 11.69
2	18.53	18.17	1' 18.01
3	23.13	23.35	1' 24.89
4	29.03	29.45	1' 33.32
5	35.09	35.07	1' 39.89
6	41.37	41.42	1' 44.92
7	47.44	47.86	1' 49.51
8 (not visible)	54.66	55.54	1' 55.17
9	1' 01.91	1' 02.13	2' 06.01
10	1' 08.03		2' 13.76
11	1' 14.72		
12	1' 21.34		
13	1' 28.19		
14	1' 34.19		
15	1' 41.31		
16	1' 48.37		
17	1' 56.03		
18	2' 03.28		

20.07.1999

Flow front  
profile

Time

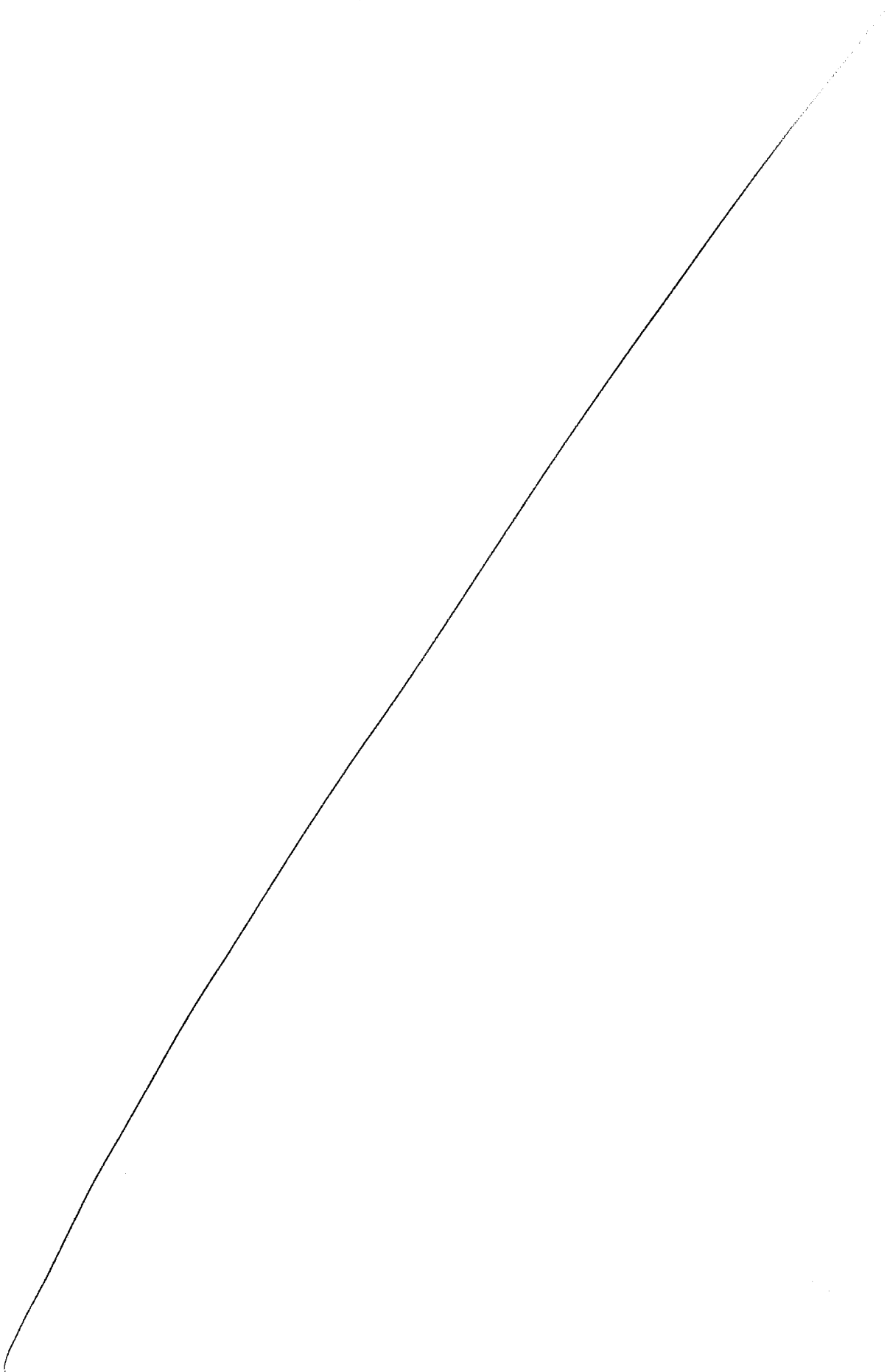
193  
re 1/15/2002

1	1'06.06	
2	1'19.82	1'20.06
3	1'29.22	1'28.47
4	1'42.94	1'42.27
5	1'55.91	1'56.37

20.07.1999



194  
re 1/15/2002



20.07.1999  
L

Tunnel GS2 (video)

195  
re 1/15/2002

GS height in dyke = 241 mm  
at atmospheric pressure

For the experiment

$$\begin{array}{|l} V_{\text{reservoir}} = 0 \\ V_{\text{dyke}} = 36 \text{ mbar} \\ V_{\text{tunnel}} = 50.5 \text{ mbar} \end{array}$$

Reservoir valve left opened, dyke valve closed  
level of GS in dyke at the top of the gate

$$\text{---} \bigcirc \text{---} \Rightarrow h =$$

$T = ?$

Gate opened at  $h_0 = 0 \Rightarrow$  initial vacuum drop in tunnel  
back to 44 mbar after 4"76

15.07.1999

Mark

Time

6

1'06.73

8

1'56.17

10

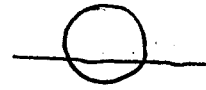
3'07.07

12

5'42.45

14

10'11.63



7 mm



3.5 mm



0 mm

Gate closed at 10'44.17  $\Rightarrow$   $V_{tunnel} = 47 \text{ mbar}$   
 $V_{dyke} = 36 \text{ mbar}$

15.07.1999

*[Signature]*

# Tunnel GS3 (video)

GS height in dyke = 240 mm  
at atmospheric pressure

For the experiment

$$\begin{array}{|l} V_{\text{reservoir}} = 0 \\ V_{\text{dyke}} = 36 \text{ mbar} \\ V_{\text{tunnel}} = 81 \text{ mbar} \end{array}$$

Reservoir valve left opened, dyke valve closed  
level of GS in dyke at the top of the tunnel entrance

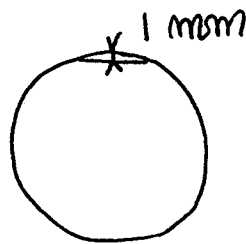
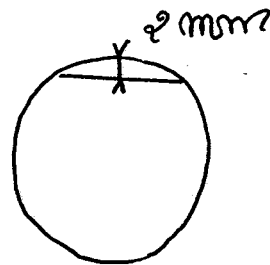
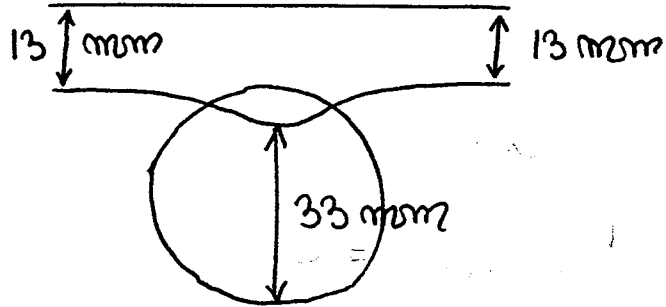
$$\text{---} \bigcirc \text{---} \Rightarrow h =$$

$$T = 22.7^\circ \text{C}$$

Gate opened at  $t_0 = 0 \Rightarrow$  initial vacuum drop in tunnel  
back to 72 mbar at 4"37

Mark	Time
2	13.75
6	29.57
8	36.07
10	44.94
12	54.53
	1'13.25

$$V_{\text{tunnel}} = 73 \text{ mbar}$$



is reached  
end of tunnel

~ 3' 27

Tunnel valve closed at 3' 50" 13

15.07.1999

*[Signature]*

# Tunnel GS 4 (video)

GS height in reservoir =  $H - 183 \text{ mm}$

GS height in dyke =  $240 \text{ mm}$

at atmospheric pressure

For the experiment,

$$V_{\text{reservoir}} = 0$$

$$V_{\text{dyke}} = 36 \text{ mbar}$$

$$V_{\text{tunnel}} = 200 \text{ mbar}$$

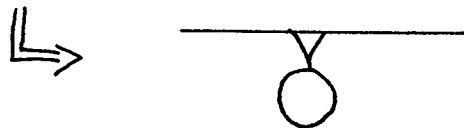
Reservoir valve left opened, dyke valve closed.

Level of GS in dyke at the top of the tunnel entrance

$$\text{---} \bigcirc \text{---} \Rightarrow h =$$

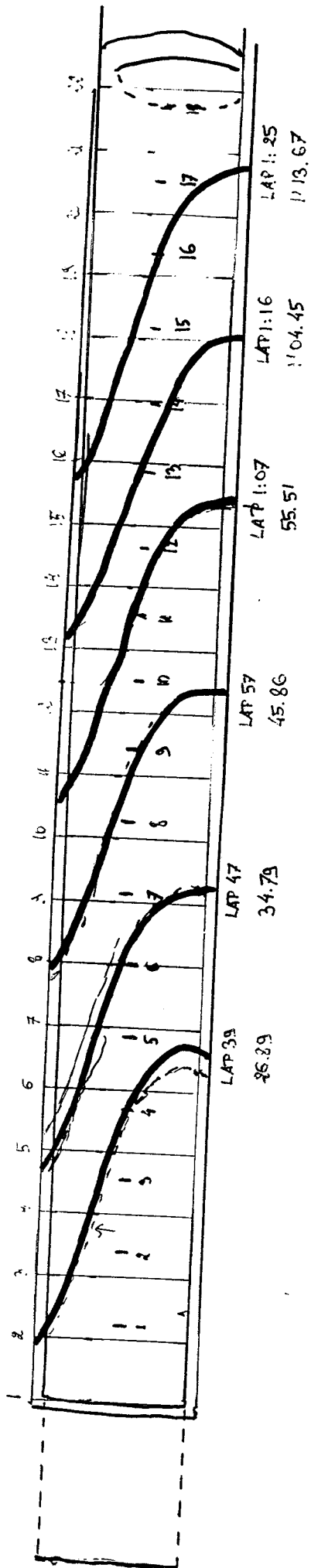
$$T = 20.3^\circ \text{C}$$

Gate opened at  $t_0 = 0$  - Tunnel valve closed after  $1' 18.80$



re 1/15/2002

Tunnel GS4 - 200 miles between  
T = 800 miles



20.07.1999

*[Signature]*

Tunnel GS 4

201 15  
re 1/15/200

Red marks  
on screen?

Bottom?

Top

1	<del>7.15</del> 6.74	24.24
2	9.45	26.47
3	12.76	28.97
4	16.89	32.09
5	20.29	35.18
6	23.73	37.56
7	27.04	40.30
8	30.10	45.59
9	33.29	48.49
10	36.35	52.15
11	40.10	55.71
12	43.17	59.18
13	46.67	1' 03.18
14	49.89	1' 06.65
15	53.35	1' 10.53
16	56.48	1' 14.15
17	1' 00.01	1' 17.47
18	1' 03.45	
19	1' 06.79	
20	1' 10.04	
21	1' 13.29	
22	1' 16.83	

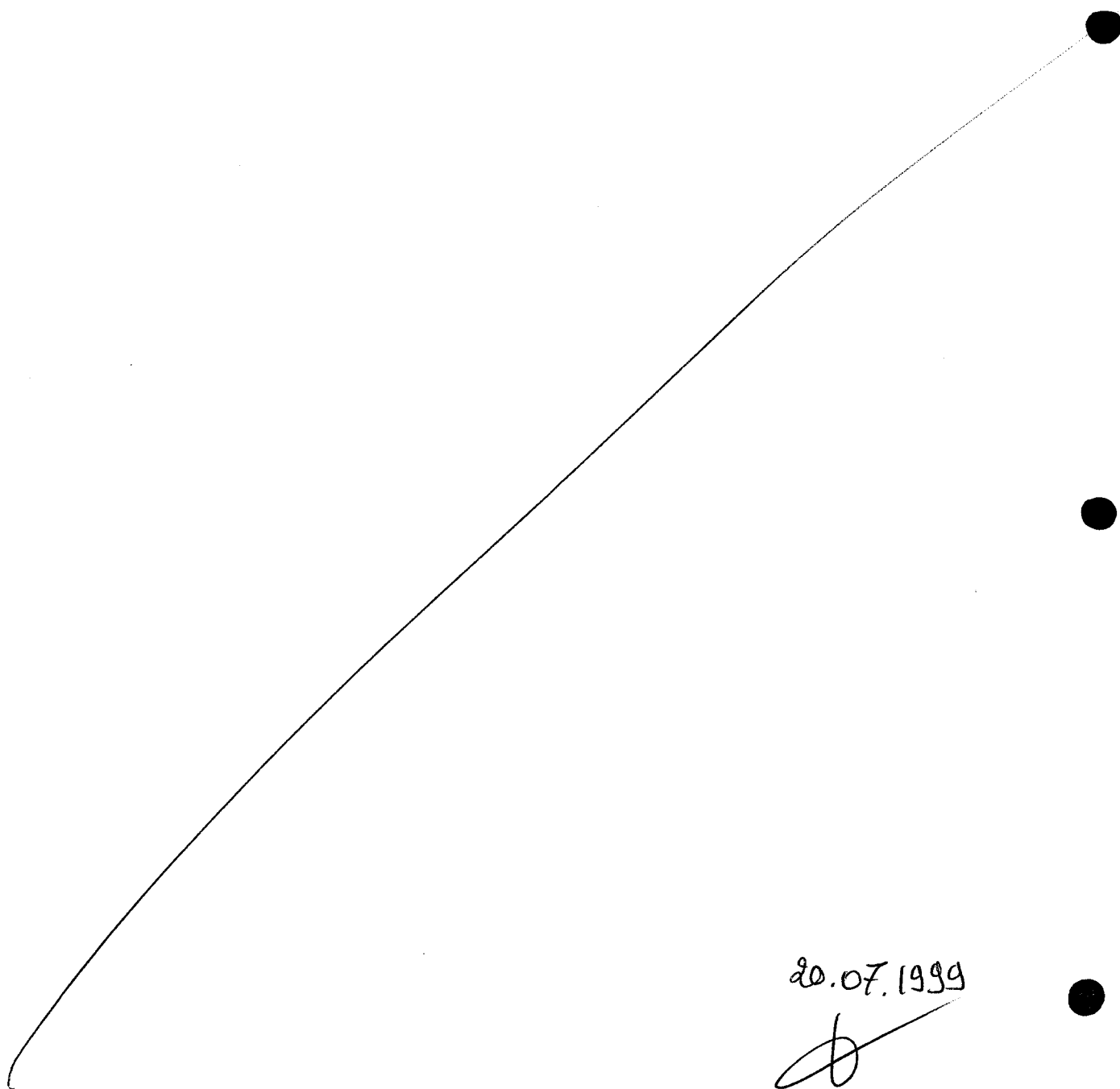
20.07.1999



10 Flow front  
profile

Time

1	26.89
2	34.79
3	45.86
4	55.51
5	1' 04.45
6	1' 13.67



20.07.1999

Tunnel GS 5 (video)

| GS height in reservoir =  $H - 188 \text{ mm}$

| GS height in dyke =  $248 \text{ mm}$

at atmospheric pressure

For the experiment,

$$V_{\text{reservoir}} = 0$$

$$P_{\text{reservoir}} = 1000 \text{ mbar} \\ (1013.25 \text{ mbar!})$$

$$V_{\text{dyke}} = 36 \text{ mbar}$$

$$V_{\text{tunnel}} = 400 \text{ mbar}$$

Reservoir valve left opened, dyke valve closed.

level of GS in dyke above tunnel entrance:

$$\frac{\text{=====}}{\bigcirc} \text{ } 3 \text{ mm} \Rightarrow h =$$

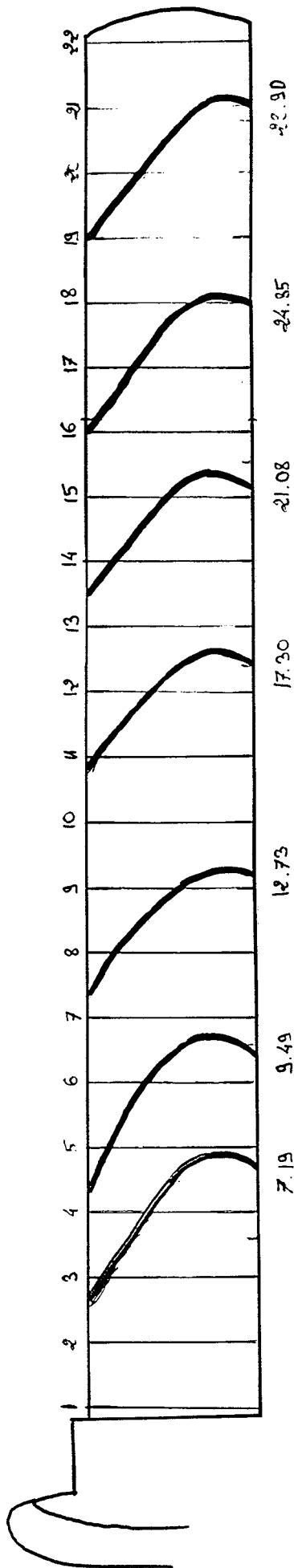
$$T = 20.7^\circ \text{C}$$

Gate opened at  $t_0 = 0$  - Tunnel valve closed after  $31''07$ .

re 1/15/2002

G55 - 400 mbar vacuum

P = 600 mbar



19.07.1999

# Tunnel G55

205 ~~18~~  
re 1/15/200

Red marks  
on screen?

Bottom?

Nose

Top

1	2.11	2.05	4.35
2	3.19	3.13	6.47
3	3.96	3.88	7.57
4	5.37	5.23	9.27
5	7.14	7.10	10.50
6	8.72	8.47	11.70
7	9.80	9.69	13.07
8	11.31	11.03	14.38
9	12.33	12.35	15.69
10	13.08	13.59	17.01
11	15.17	15.07	18.69
12	16.66	16.25	19.95
13	17.83	17.69	21.50
14	19.41	18.91	22.69
15	20.55	20.32	24.31
16	22.03	21.75	25.60
17	23.23	23.17	27.09
18	24.75	24.50	28.23
19	25.93	25.86	29.85
20	27.34	27.25	30.92
21	28.58	28.57	
22	30.19	30.29	

20.07.1999

Flow front  
profile

Time

1	7.27	7.19	7.12	
2	9.52	9.54	9.40	
3	12.77	12.76	12.65	
4	17.43	17.26	17.21	
5	21.11	21.17	21.09	20.93
6	24.93	24.76	24.77	24.93
7	28.89	28.92	28.93	28.87

20.07.1999



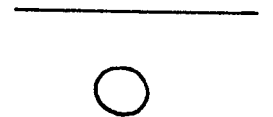
## Tunnel GS 5 (video)

GS height in reservoir =  $H - 180 \text{ mm}$   
GS height in dyke =  $244 \text{ mm}$   
at atmospheric pressure

For the experiment,

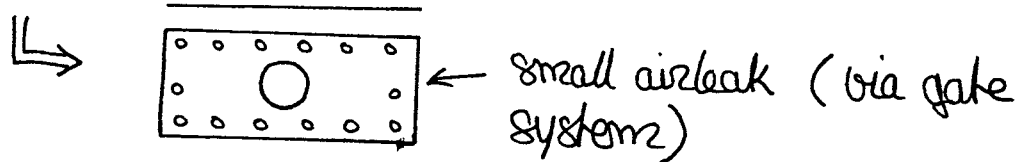
$V_{\text{reservoir}} = 0$   
 $V_{\text{dyke}} = 36 \text{ mbar}$   
 $V_{\text{tunnel}} = 800 \text{ mbar}$

Reservoir valve left opened, dyke valve closed.  
level of GS in dyke at the top of the dyke



$T = 20.8^\circ\text{C}$

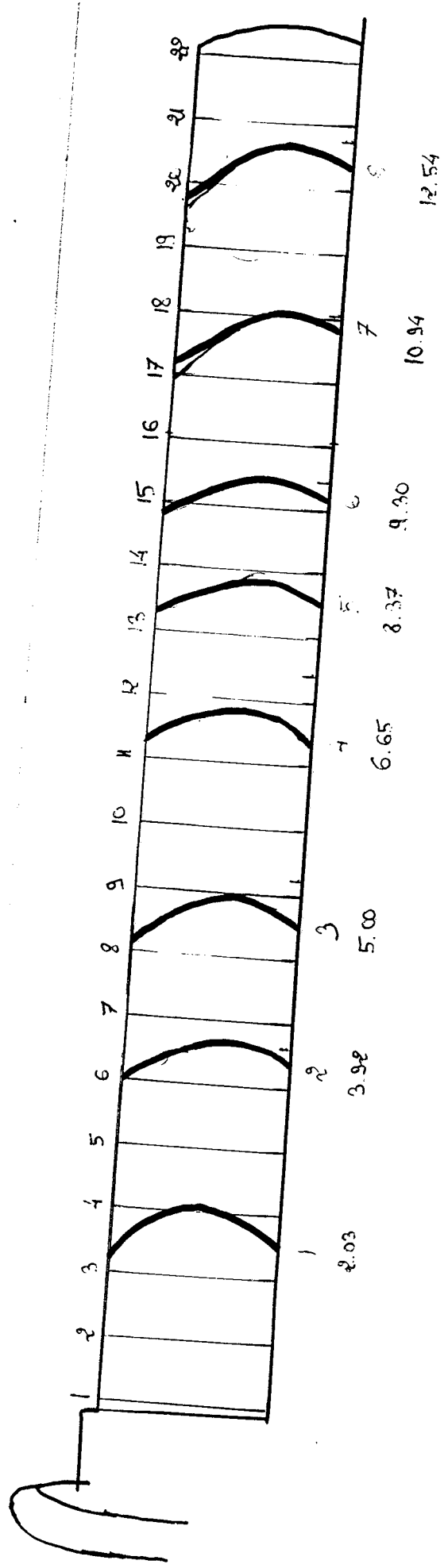
Gate opened at  $t_0 = 0$  - Tunnel valve closed after 16" 18



200  
re 1/15/2002

Tunnel G56 - 800 mbar vacuum

P = 200 mbar



20.07.1999

*[Signature]*

Red marks  
on screen

Time

2	1.57	1.54 <sup>x</sup>		
3	1.68 <sup>(1)</sup>			
4	2.08 <sup>(*)</sup>	2.03 <sup>+</sup>		
5	2.46 <sup>(2)</sup>	2.50 <sup>B</sup>		
6	3.45			
7	4.07 <sup>(3)</sup>	4.19 <sup>0</sup>	4.23 <sup>x</sup>	4.23 <sup>A</sup>
8	4.67 <sup>(2)</sup>	4.63 <sup>+</sup>		
9	5.01 <sup>(1)</sup>			
10	5.77	5.82 <sup>B</sup>		
11	6.24 <sup>(*)</sup>			
12	6.75 <sup>(3)</sup>	6.75	7.01 <sup>x</sup>	7.04 <sup>A</sup>
13	7.84 <sup>(1)</sup>	7.89 <sup>0</sup>	7.72 <sup>+</sup>	
14	8.41 <sup>(2)</sup>			
15	9.03	9.16 <sup>B</sup>		
16	9.69 <sup>(3)</sup>	9.78 <sup>(*)</sup>	9.69 <sup>x</sup>	
17	10.31			
18	10.82	11.01 <sup>A</sup>		
19	11.46 <sup>(1)</sup>			
20	12.17 <sup>(2)</sup>	12.19 <sup>x</sup>	12.19 <sup>B</sup>	
21	12.69 <sup>(3)</sup>			
22	13.40 <sup>(*)</sup>	13.42 <sup>A</sup>		



Flow front  
profile

Time

1	2.02		2.03	2.04		
2	4.02	3.93	3.86		3.87	
3	5.02		5.03	4.95		
4	6.73	6.59			6.55	6.73
5	8.33		8.50	8.23	8.42	
6	9.43				9.11	9.36
7		10.87	10.92	11.04		
8	12.58	12.67	12.53		12.36	

20.07.1999



# Tunnel marks positions for GS1

On screen

1	21	22.25
2	43.25	21.25
3	64.5	22.75
4	87.25	21
5	108.25	21.25
6	129.5	20.25
7	149.75	21.25
8	171	20.75
9	191.75	20.5
10	212.25	19.75
11	232	20.25
12	252.25	21.5
13	273.75	21.75
14	295.5	20.5
15	316	21.5
16	337.5	23
17	360.5	21.5
18	382	

⇒ 21.24 average  
20 real

↳  $\frac{1 \text{ mm on screen}}{\text{scale}} = 0.9418$

20.07.1999



Tunnel diameter  
on screen = 48 mm

20.07.1999



Red marks positions for GS4/GS5/GS6

213 ~~27~~  
re 1/15/200.

→ calculated with scale  
1:1. 1604  
Real (from gate)

32.6109 → add 30 mm

	On screen
1	2.25
2	17.25
3	32.25
4	47.25
5	62.25
6	77.25
7	92.25
8	107.25
9	122.25
10	137.25
11	152.25
12	167.25
13	182.25
14	197.25
15	212.25
16	227.25
17	242.25
18	257.25
19	272.25
20	287.25
21	302.25
22	317.25

10.07.1999



Tunnel visible length  $\overset{32.5}{=} 31.9 \text{ mm}$  (ad  
 on screen  
 (real  $372.5 \text{ mm}$ )  $\leftarrow$  add  $30 \text{ mm}$  for gate  
 Tunnel diameter  
 on screen  $= 38.5 \text{ mm}$   
 (real  $40 \text{ mm}$ )

screen      real  
 1 mm      1.1677  
             1.0389

Black marks on tunnel  
(on screen)

Real (measured  
on tunnel)

1	20.5	
2	38.25	17.75
3	55.5	17.25
4	72.5	17.0
5	90	17.5
6	107.25	17.25
7	124	16.75
8	141	17
9	158.5	17.5
10	175	16.5
11	190.5	15.5
12	207	16.5
13	225	18
14	<del>241.5</del> 241.5	16.5
15	260	18.5
16	277.5	17.5
17	295	17.5
18	313.5	18.5

$\Rightarrow$  average      17.24  
 real      20

$\rightarrow$  1 mm Screen = 1.1604  
 Scale

~~0.07.03.02~~

20.07.1999

(657)

H - 260.5 mm = reservoir

dyke = 165 mm

at atm

dyke 36 mbar

$V_{\text{tunnel}} = 1000$  mbar  
07.03.02

levelled

record rate  
1000

T = 20.9 6mm lens

343 MB

GS7.avi whole  
GS7.avi frame  
- 6800 → 0  
(6.8s)

$V_{\text{res}} = 0$

$V_{\text{dyke}} = 38.7$  07.03.02  
58.5

valve reservoir closed!  $\Rightarrow P_{\text{res}} \neq \text{atm (atm)}$

688

H - 166 mm = reservoir

dyke 253 mm

atm

record rate  
1000 6mm lens

16 H15

T = 21.3 °C

688.avi

$V_{\text{res}} = \text{atm}$   
Dyke 40 mbar  $\nearrow$  top GS  
O

308 MB

$P_{\text{tunnel}} = 0$  mbar

re  
1/15/2001 (GS9)

$$h_{res} = H - 179 \text{ mm}$$
$$dyke = 249 \text{ mm}$$

$$P_{res} = atm$$

$$P_{tunnel} = 600 \text{ mbar}$$

$$V_{dyke} = 40 \text{ mbar}$$

$$T = 24.7^\circ C \rightarrow h_{res} = H - 206 \text{ mm}$$

04.09.99

17H30

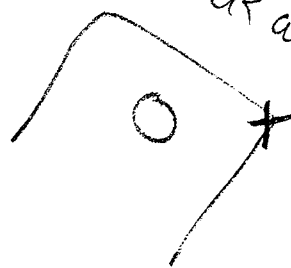
$$\text{Zoom lens} = 12.5 \text{ mm} / 10$$

$$250 \text{ mm} \rightarrow 32.8$$

$$\rightarrow 23.4^\circ C \text{ (Use of light)}$$

didn't press button of camera

leak at top of tank (beginning wipe out!)



$\rightarrow$  to redo

$$\rightarrow h = H - 234 \text{ mm}$$

Reservoir

04.09.1999

GS9 . avi 94M

21/7/2

re 1/15/2000

(GS10)

$$res = M - 186 \text{ mm}$$

$$dyke = 240 \text{ mm}$$

$$P_{res} = atm$$

181100

$$P_{tunnel} = 600$$

$$V_{dyke} = 40$$

$$\rightarrow res M - 214 \text{ mm}$$

T=

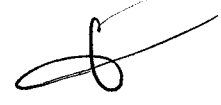
Camera same as GS9

$$L \rightarrow 23.6^{\circ}C \text{ (lamp)}$$

after

163K

04.09.1999





re 1/15/2002

14 410

$$h_{\text{dyke}} = 267 \text{ mm}$$

$$h_{\text{res}} = H - 156 \text{ mm}$$

zoom lens (12.5 mm) open at 2  
no secondary light  
250 E (resoln  $\approx 240 \times 210$ )

$$T = 22.1^\circ \text{C}$$

$$P_{\text{dyke}} = 36 \text{ mbar} \quad \text{GS to the top}$$

few bubbles  
v. small

(< 1 mm  $\varnothing$ ) homogeneously  
distrib.

$$\rightarrow h_{\text{res}} = H - 182 \text{ mm}$$

$$V_{\text{tunnel}} = 600 \text{ mbar}$$

$$\rightarrow H = 210 = h_{\text{res final}}$$

save in GSU. avi 209 Mb

05.09.1999

GS 12

re 1/15/2007

$$h_{dyke} = 273 \text{ mm}$$

$$h_{res} = H - 155 \text{ mm} \quad 15H20$$

{ zoom lens (12.5mm) open at 2.8  
secondary light { photons beard red head lamp head)  
1000 (240x210)

$$T = 22.4^{\circ}\text{C} \text{ without light (before exp)}$$

$$V_{dyke} = 36 \text{ mbar} \quad \text{GS to top}$$

$$\rightarrow h_{res} = H - 179 \text{ mm}$$

$$V_{tunnel} = 1000 \text{ mbar}$$

$$\rightarrow H - 208 = h_{res \text{ final}}$$

$$T = 22.6^{\circ}\text{C}$$

save in GS12. avi (413 MB)

let camera running too long

$\rightarrow$  missed start!

05.09.1999

(GS13)

$$h_{\text{dyke}} = 269 \text{ mm}$$

$$h_{\text{res}} = H - 158 \text{ mm}$$

(PH10)

{ zoom lens (12.5 mm) open at > 4  
secondary light  
500 E (240x210)

$$T = 22.7^\circ \text{C}$$

$$V_{\text{dyke}} = 36 \text{ mbar} \quad \text{G8 to top}$$

(will prob. have a leak  
↳ door to clean)

→  $h_{\text{res}} = H - 184 \text{ mm}$

$$V_{\text{tunnel}} = 100 \text{ mbar}$$

$$\rightarrow h_{\text{res}} = H - 212 \text{ mm}$$

$$T = 22.8^\circ \text{C}$$

save in GS13. avi

(206 Mb)

had a leak  
(gate contour  
inside  
dyke)



05.09.1999

*[Signature]*

265

GS14

$$h_{dyke} = \cancel{278} \text{ mm}$$

$$h_{res} = H - 162 \text{ mm}$$

17H40

{ zoom lens (12.5 mm) open at 8  
 secondary light  
 250 E

$$T = 22.6^{\circ} \text{C}$$

$$V_{dyke} = 36 \text{ mbar (GS to top)}$$

$$\rightarrow h_{res} = H - 186 \text{ mm}$$

$$V_{tunnel} = 700 \text{ mbar}$$

$$\rightarrow h_{res_{fin}} = H - 216 \text{ mm}$$

$$T = 22.7^{\circ} \text{C}$$

save in GS14. avi

(166 Mb)

05.08.1999

GS15

18M35

$$h_{\text{dyke}} = 257 \text{ mm}$$

$$h_{\text{res}} = H - 167 \text{ mm}$$

{ Zoom lens (12.5 mm) open at 8  
Secondary light  
250 E

$$T = 23.0^\circ \text{C}$$

$$V_{\text{dyke}} = 36 \text{ mbar (GS top)}$$

still



$$\rightarrow h_{\text{res}} = H - 193 \text{ mm} \rightarrow \text{data}^{\circ}$$

$$V_{\text{tunnel}} = 800 \text{ mbar}$$

$$\rightarrow h_{\text{res}} = H - 220$$

$$T = 22.9^\circ \text{C}$$

save GS15. avi (138 Mb)

05.09.1999

GS16

$$h_{dyke} = 253 \text{ mm}$$

$$h_{res} = H - 171 \text{ mm}$$

lens of camera same

19440

$$T = 22.8^{\circ}\text{C}$$

$$V_{dyke} = 36 \text{ mbar} \quad (\text{less air Hcon GS15})$$

$$\hookrightarrow h_{res} = H - 197 \text{ mm}$$

$$V_{tunnel} = 1000 \text{ mbar}$$

$$T = 22.8^{\circ}\text{C}$$

$$\hookrightarrow h_{res_{fin}} = H - 225$$

save as GS16.air (92 MB)

T=22

$$h_{dyke} = 246 \text{ mm}$$

$$h_{res} = H - 177 \text{ mm}$$

21400

(lens (12.5 mm) open at H  
secondary light  
125E (6555 (240 x 210))

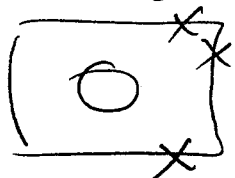
$$T = 23.4^{\circ}\text{C}$$

~~070302~~ ~~dyke~~ = 36 mbar  
 $\rightarrow h_{res} = H - 204 \text{ mm}$

$$V_{tunnel} = 500 \text{ mbar}$$

$$T = 23.9$$

~~070302~~ leak  
bucke



$$\rightarrow h_{res fin} = H - 234 \text{ mm}$$

Save as GS17awi (115 Mb)

15-12-2000

Insert mol in place at the top of the dike  
(stuck with silicone sealant)

At 18H00

$$P_1 = 983.7/8 \text{ mbar}$$

$$P_2 = 985.5/6 \text{ mbar}$$

$$P_3 = 983.4/5 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

$$H_{\text{res}} = h - 325 = 160 \text{ mm}$$

$$h_{\text{dyke}} = 105.5 \Rightarrow h_{\text{dyke}} = 175.5 \text{ mm}$$

Nicolet

$$\text{Time / pt} = 20 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrig } 1\%$$

7 transducers operation

High-speed video 500 FPS

DGS0 pumped up the dike

$$P_{\text{dike}} = 923.2/3 \text{ mbar}$$

$$H_{\text{res}} = h - 366.5 = 118.5 \text{ mm}$$

At 18H10

$$P_1 = 983.6/7 \text{ mbar}$$

$$P_2 = 985.7/8 \text{ mbar}$$

$$P_3 = 983.6/7 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

P data saved as files

{ f\_000001.tiff to f\_004368 or Vdgs0\_18  
Pdg0\_18



226  
re 1/15/2002

DG30-13  
15-12-2000

Insert m<sup>o</sup> 1 in place at the top of the dike

At 18H55

$P_1 = 984.1/2$ mbar
$P_2 = 985.9/986.0$ mbar
$P_3 = 983.8$ mbar
$T = 23.5^\circ\text{C}$
$H_{\text{res}} = H - 331 = 154$ mm
$h_{\text{dike}} = 101$ mm $\Rightarrow 171$ mm

Nicolet

Time / pt = 20 $\mu\text{s}$
Trigger position = pretrig 1%

High-speed video 500 FPS

At 19H10

$P_1 = 984.0/1$ mbar
$P_2 = 985.8/9$ mbar
$P_3 = 983.7$ mbar
$T = 24^\circ\text{C}$

DG30 pumped up the cell

$P_{\text{dike}} = 919.7/8$ mbar
$H_{\text{res}} = H - 369 = 116$ mbar

6 bubbles about 6 mm in size at the top of the cell ( = )

Changed glass tube and readjusted pressures  $P_{\text{dike}} = 914.5/6$  mbar

At 19H35

$P_1 = 982.8/9$ mbar
$P_2 = 985.5/6$ mbar
$P_3 = 983.4$ mbar
$T = 24^\circ\text{C}$

Bubbles coming out of the gate  $\Rightarrow$  need to clean the gate

15-12-2000

Insert no 1 in place at the top of the dike

At 20 H 15

$$P_1 = 983.4 \text{ mbar}$$

$$P_2 = 985.3/4 \text{ mbar}$$

$$P_3 = 983.1 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

$$H_{res} = H - 335 = 150 \text{ mmHg}$$

$$P_{dyke} = 97.5 \text{ mmHg} \Rightarrow 167.5 \text{ mmHg}$$

Nicot

$$T_{onr}/pt = 250 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrig } 1\%$$

High-speed video 30 FPS

DGSO pumped up the cell

$$P_{dyke} = 917.3/4 \text{ mbar}$$

$$H_{res} = H - 374 = 111 \text{ mmHg}$$

Few bubbles trapped.

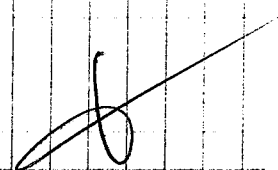
At 20 H 30

$$P_1 = 682.1 \text{ mbar}$$

$$P_2 = 985.0/1 \text{ mbar}$$

$$P_3 = 982.9 \text{ mbar}$$

$$T = 24^\circ\text{C}$$



re 1/15/2002

15-12-2000

Insert m.o.l in place at the top of the dyke

At 21 H 10

$$P_1 = 983.415 \text{ mbar}$$

$$P_2 = 985.213 \text{ mbar}$$

$$P_3 = 983.011 \text{ mbar}$$

$$T = 24^\circ\text{C}$$

$$H_{\text{res}} = H - 336 = 149 \text{ mm}$$

$$h_{\text{dyke}} = 97 \text{ mm} \Rightarrow 167 \text{ mm}$$

Nicolet

$$\text{Time / pt} = 40 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 250 FPS

DGSO pumped up the cell

$$P_{\text{dyke}} = 912.5 \text{ mbar}$$

$$H_{\text{res}} = h - 375 = 110 \text{ mm}$$

Few bubbles.

At 21 H 20

$$P_1 = 182.718 \text{ mbar}$$

$$P_2 = 985.213 \text{ mbar}$$

$$P_3 = 983.011 \text{ mbar}$$

$$T = 24^\circ\text{C}$$

Bubbles escaping  
from gate

At 21 H 20, after the run

$$P_1 = 983.415 \text{ mbar}$$

$$P_2 = 985.213 \text{ mbar}$$

$$P_3 = 983.011 \text{ mbar}$$

$$T = 24^\circ\text{C}$$

DGSO-222

16-12-2000

Insert no 1 in place at the top of the dyke

At 11450

$$P_1 = 990.8/9 \text{ mbar}$$

$$P_2 = 991.9 / 992.0 \text{ mbar}$$

$$P_3 = 990.8/9 \text{ mbar}$$

$$T = 22^\circ \text{C}$$

$$H_{\text{res}} = H - 322.5 = 162.5 \text{ mm}$$

$$h_{\text{dyke}} = 107.5 \text{ mm} \Rightarrow 177.5 \text{ mm}$$

Kicohet

$$\text{Time / pt} = 100 \mu\text{s}$$

$$\text{Trigger position} = \text{prebig } 1\%$$

High-speed video 125 FPS

DGSO Pumped up the cell

$$P_{\text{dyke}} = 922.1/2 \text{ mbar}$$

$$H_{\text{res}} = H - 364 = 121 \text{ mm}$$

At 12408

$$P_1 = 589.9 \text{ mbar}$$

$$P_2 = 992.0/1 \text{ mbar}$$

$$P_3 = 990.6/7 \text{ mbar}$$

$$T = 23^\circ \text{C}$$

re 1/15/2002

16-12-2000

Insert m<sup>o</sup> 1 in place at the top of the dyke

At 13H32

$$P_1 = 991.3/4 \text{ mbar}$$

$$P_2 = 992.9/993.0 \text{ mbar}$$

$$P_3 = 991.0/1 \text{ mbar}$$

$$T = 24^\circ\text{C}$$

$$H_{\text{res}} = H - 326 = 159 \text{ mm}$$

$$h_{\text{dyke}} = 103 \text{ mm} = 173 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 250 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 30 FPS

DGSO pumped up the cell  
at 13H35

$$P_{\text{dyke}} = 917.8/9 \text{ mbar}$$

$$H_{\text{res}} = H - 370 = 115 \text{ mm}$$

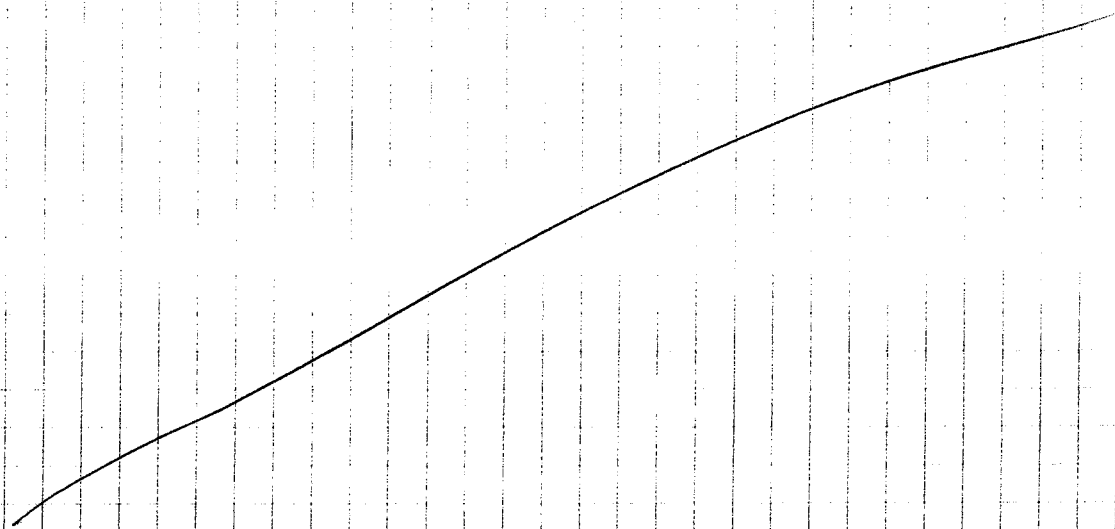
At 13H39

$$P_1 = 790.9/791.0/791.1 \text{ mbar}$$

$$P_2 = 992.9/993.0 \text{ mbar}$$

$$P_3 = 991.0/1 \text{ mbar}$$

$$T = 24^\circ\text{C}$$



*[Handwritten signature]*

16-12-2000

Insert m.o.l in place at the top of the cell

\* 14H25

$$\begin{aligned} P_1 &= 991.3/4 \text{ mbar} \\ P_2 &= 993.0/1 \text{ mbar} \\ P_3 &= 990.9/991.0 \text{ mbar} \\ T &= 24^\circ\text{C} \\ H_{\text{res}} &= H - 325 = 160 \text{ mm} \\ h_{\text{dyke}} &= 106 \text{ mm} \Rightarrow 176 \text{ mm} \end{aligned}$$

(added more  
DGSO after  
previous expt.)

Kicolet

$$\begin{aligned} \text{Time/pt} &= 250 \mu\text{s} \\ \text{Trigger position} &= \text{pretrigger } 1\% \end{aligned}$$

High-speed video 30 FPS

DGSO pumped up the cell

$$\begin{aligned} P_{\text{dyke}} &= 929.6/7 \\ H_{\text{res}} &= H - 364 \text{ mm} = 121 \text{ mm} \end{aligned}$$

\* 14H32

$$\begin{aligned} P_1 &= 889.5/6 \text{ mbar} \\ P_2 &= 993.0/1 \text{ mbar} \\ P_3 &= 990.9/991.0 \text{ mbar} \\ T &= 24^\circ\text{C} \end{aligned}$$

\* 14H35 after run  
once the valve at the end  
of the tunnel is closed

$$\begin{aligned} P_1 &= 888.7/8 \text{ mbar} \\ P_2 &= 992.9/993.0 \text{ mbar} \\ P_3 &= 990.8/9 \text{ mbar} \\ T &= 24^\circ\text{C} \end{aligned}$$

re 1/15/2002

DGSO 2000

16-12-2000

Insert no 1 is place at the top of the cell

At 15H30

$$P_1 = 992.1/2 \text{ mbar}$$

$$P_2 = 993.8/9 \text{ mbar}$$

$$P_3 = 991.7/8 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

$$H_{\text{res}} = H - 325 = 160 \text{ mm}$$

$$h_{\text{dyke}} = 104.5 \text{ mm} \Rightarrow 174.5 \text{ mm}$$

Kicodet

$$\text{Time/pt} = 250 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrig } 1\%$$

High-speed video 30 FPS

At 15H40, DGSO pumped up the cell

$$P_{\text{dyke}} = 992.5/6 \text{ mbar}$$

$$H_{\text{res}} = H - 368 = 117 \text{ mm}$$

$$P_3 = 992.4/5 \text{ mbar}$$

For the expt

$$P_1 = 994.5/6/7 \text{ mbar}$$

$$P_2 = 994.6/7/8 \text{ mbar}$$

$$P_3 = 992.5/6/7 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

measured just before  
opening the gate

During the experiment,  $P_1 = 995.3 \text{ mbar}$

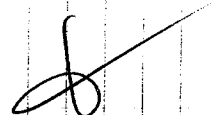
At 15H47,

$$P_1 = 993.2/3 \text{ mbar}$$

$$P_2 = 995.0/1 \text{ mbar}$$

$$P_3 = 992.8/9 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$



16-12-2000

Insert mol in place at the top of the cell

At 16H20

$$P_1 = 993.415 \text{ mbar}$$

$$P_2 = 995.213 \text{ mbar}$$

$$P_3 = 993.011 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

$$H_{\text{res}} = H - 328.5 \text{ mm} = 156.5 \text{ mm}$$

$$h_{\text{dyke}} = 102 \text{ mm} \Rightarrow 172 \text{ mm}$$

Nicolet

$$\text{Time / pt} = 40 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 250 FPS

At 16H27, DGSO pumped up the cell

$$P_{\text{dyke}} = 992.213 \text{ mbar}$$

$$H_{\text{res}} = H - 370 = 115 \text{ mm}$$

$$P_1 = 993.6 \text{ mbar}, P_3 = 993.2 \text{ mbar}$$

At 16H32

$$P_1 = 992.314 \text{ mbar}$$

$$P_2 = 995.213 \text{ mbar}$$

$$P_3 = 993.011 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

At the end of the run, when closing the tunnel valve,

$$P_1 \sim 517.7 \text{ mbar (valve closed)}$$

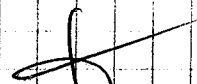
At 16H36

$$P_1 = 993.415 \text{ mbar}$$

$$P_2 = 995.2 \text{ mbar}$$

$$P_3 = 993.0 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$





1/15/2002

16-12-2000

Insert no 1 in place at the top of the cell

At 17H00

$P_1 = 993.6/7$ mbar
$P_2 = 995.4/5$ mbar
$P_3 = 993.3/4$ mbar
$T = 24.0^\circ\text{C}$
$H_{res} = H - 321.5 = 163.5$ mm
$h_{dyke} = 109$ mm $\Rightarrow$ 179 mm

(more DGSO added after previous expt)

Nicolet | Time/pt = 40  $\mu$ s  
 Trigger position = retrig 1%

High-speed video 250 FPS

At 17H06, DGSO pumped up the cell

$P_1 = 993.4/5$ mbar	$P_3 = 993.4/5$ mbar	$P_{dyke} = 931.5/6$ mbar
		$H_{res} = H - 360 = 125$ mm

At 17H10

$P_1 = 993.0/1$ mbar
$P_2 = 995.5/6$ mbar
$P_3 = 993.4/5$ mbar
$T = 24.0^\circ\text{C}$

Big bubbles coming out from gate.

$P_1 \approx 322$  mbar

At 17H15

$P_1 = 993.8/9$ mbar
$P_2 = 995.6/7$ mbar
$P_3 = 993.5/6$ mbar
$T = 24^\circ\text{C}$

16-12-2000

Insert no 1 in place at the top of the cell

At 17H40

$$P_1 = 994.1/2 \text{ mbar}$$

$$P_2 = 995.9/996.0 \text{ mbar}$$

$$P_3 = 993.9/994.0 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

$$H_{\text{res}} = H - 326 = 159 \text{ mm}$$

$$h_{\text{dyke}} = 118.5 \text{ mm} \Rightarrow 188.5 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 40 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 250 FPS

At 17H45, DGSO pumped up the cell

$$P_{\text{dyke}} = 992.9/993.0 \text{ mbar}$$

$$H_{\text{res}} = H - 364 = 121 \text{ mm}$$

$$T = 23.5^\circ\text{C}$$

$$P_1 = 993.9/994.0 \text{ mbar}$$

$$P_3 = 994.0/1 \text{ mbar}$$

At 17H55,

$$P_1 = 993.4/5 \text{ mbar}$$

$$P_2 = 995.9/996.0 \text{ mbar}$$

$$P_3 = 994.0/1 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

(during run,

$$P_1 = 425.0 \text{ mbar}$$

At 18H00, after the run

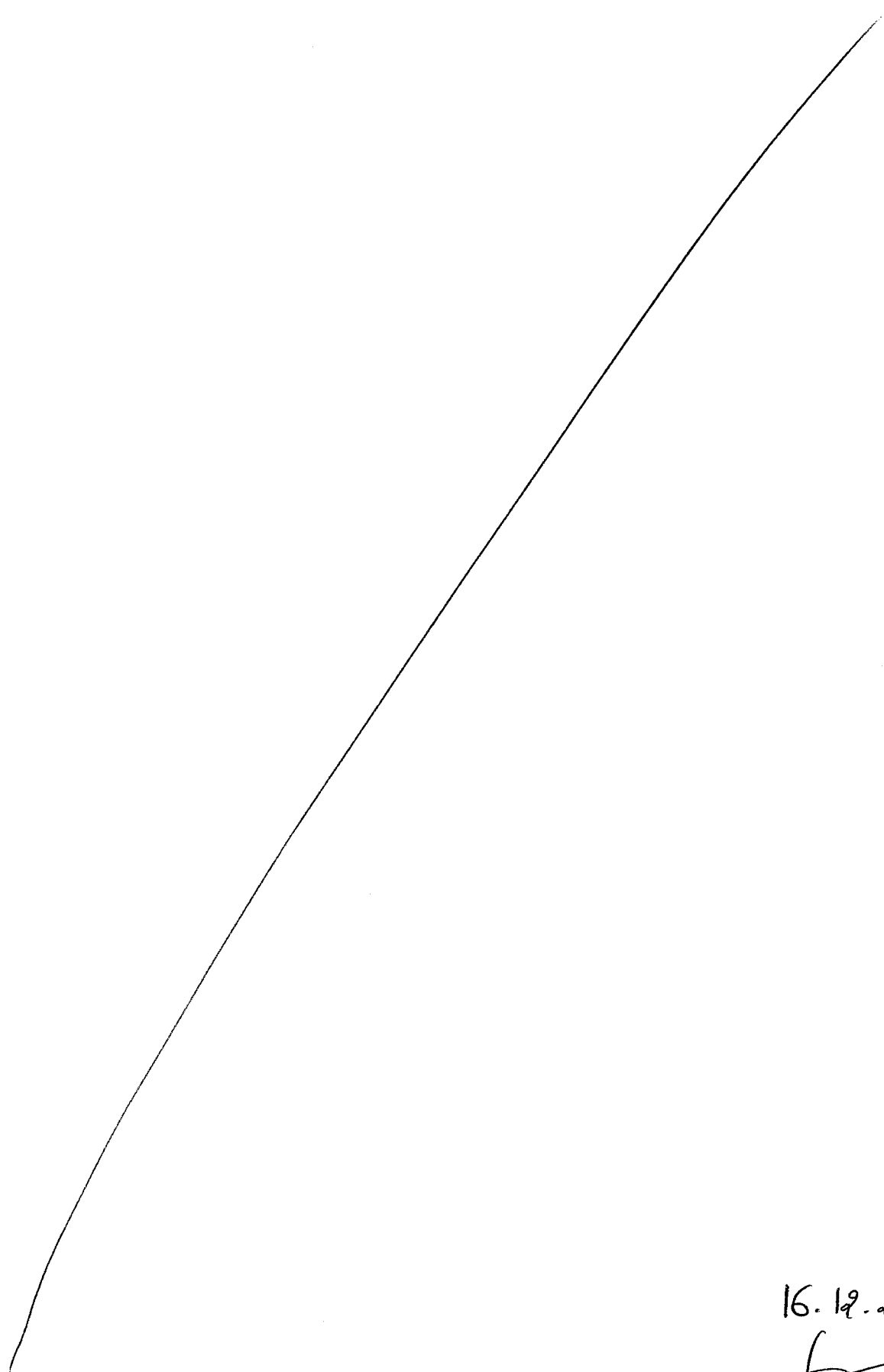
$$P_1 = 994.2 \text{ mbar}$$

$$P_2 = 995.8/9 \text{ mbar}$$

$$P_3 = 993.9/994.0 \text{ mbar}$$

$$T = 23^\circ\text{C}$$

238  
re 1/15/2002

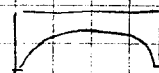


16.12.2000

A handwritten signature or mark, possibly a stylized 'S' or 'G', located below the date.

17-12-2000

Insert no 2 in place at the top of the cell



At 13H30

$$P_1 = 994.6/7 \text{ mbar}$$

$$P_2 = 996.4/5 \text{ mbar}$$

$$P_3 = 994.6/7 \text{ mbar}$$

$$T = 23.0^\circ \text{C}$$

$$H_{\text{res}} = H - 313.5 = 171.5 \text{ mm}$$

$$h_{\text{dyke}} = 117 \text{ mm} \Rightarrow 187 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 20 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 500 FPS

Wee leak between the cell and the tunnel via the gate (D650 rises up in the cell while pumping down the pressure in the tunnel):

$$P_{\text{dyke}} \rightarrow 991.0 \text{ mbar}$$

$$h_{\text{dyke}} \rightarrow 152 \text{ mm} (\Rightarrow 222 \text{ mm})$$

$$P_{\text{tunnel}} \text{ cannot go below } \sim 700 \text{ mbar}$$

$\Rightarrow$  try with D650 at top of the cell then lowering  $P_{\text{tunnel}}$

$\Rightarrow$  while decreasing the pressure in the cell,  $P_{\text{tunnel}}$  decreases as well, down to the same value as  $P_{\text{dyke}}$ :

$$P_{\text{tunnel}} = 953.5 \text{ mbar}$$

$$P_{\text{dyke}} = 954.3/4 \text{ mbar}$$

then

$$949.4/5 \text{ mbar}$$

$$950.3/4 \text{ mbar}$$

$\Rightarrow$  change O-rings in gate mechanism

$$P_{\text{tunnel}} = 947.7/8 \text{ mbar}$$

$$P_{\text{dyke}} = 948.4/5 \text{ mbar}$$



bubbles come out

At 14H33,

$$P_{\text{tunnel}} = 922.4 \text{ mbar}$$

$$P_{\text{dyke}} = 922.4/5 \text{ mbar} \iff \text{DESO up the cell}$$

$$P_3 = 993.2/3 \text{ mbar}$$

$$H_{\text{res}} = 4 - 352 = 133 \text{ mm}$$

$$T = 25.0^\circ\text{C}$$

After changing O'ring and using loads of silicone grease, the lowest pressure achievable in the tunnel is 62.0/1/2 mbar (still a little noise of air at the rear of the gate but system is stable)  $\Rightarrow$  go for  $\Delta P \sim 900 \text{ mbar}$

At 14H42

$$P_1 = 92.5/6 \text{ mbar}$$

$$P_2 = 995.3/4 \text{ mbar}$$

$$P_3 = 993.0/1 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

During the experiment,  $P_1 = 103.3 \text{ mbar}$  just before closing the valve. Also big bubble came out from the door.

At 14H46, after the run

$$P_1 = 993.6/7 \text{ mbar}$$

$$P_2 = 995.3/4 \text{ mbar}$$

$$P_3 = 993.0/1 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

Question: Could the jet be triggered by the big bubble coming out of the door? Is there always a bubble coming out of the door?

17.12.2000,

17-12-2000

Insert m.o. in place at the top of the cell

At 15H35

$$P_1 = 992.8/9 \text{ mbar}$$

$$P_2 = 994.5/6 \text{ mbar}$$

$$P_3 = 992.5/6 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

$$H_{res} = H - 317 = 168 \text{ mm}$$

$$h_{dyke} = 114 \text{ mm} \Rightarrow 184 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 40 \mu\text{s}$$

$$\text{Trigger position} = \text{prebig } 1\%$$

High-speed video 250 FPS

The pressure in the tunnel is stable, but after a while, a big bubble comes out from the closed gate (deso is at the top of the cell)

$$P_{\text{tunnel}} = 959.8 \text{ mbar}$$

$$P_{\text{dyke}} = 953.3 \text{ mbar}$$

Bubbles keep coming out from the door plate.

$$P_{\text{tunnel}} = 962.3 \text{ mbar rising slowly}$$

$$P_{\text{dyke}} = 948.7/8 \text{ mbar}$$

Close the valve at the end of the tunnel and leave the system resting for a few minutes.

$\Rightarrow$  at 15H50

$$P_{\text{dyke}} = 935.6/7 \text{ mbar}$$

$$P_{\text{tunnel}} = 992.5/6 \text{ (tunnel valve closed)}$$

$$P_3 = 992.1/2 \text{ mbar}$$

At 15H52

$$P_{dyke} = 992.5 \text{ mbar}$$

$$P_1 = 996.0/1 \text{ mbar}$$

$$P_3 = 992.0/1 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

$$H_{res} = H - 357 = 128 \text{ mm}$$

At 15H58

$$P_1 = 991.2/3 \text{ mbar} \quad (\text{went up to } 315 \text{ mbar})$$

$$P_2 = 993.9/994.0 \text{ mbar}$$

$$P_3 = 991.9/992.0 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

Transducer  $P_2$  didn't record any signal.

17.12.2000

6

DGSO-31

17-12-2000

Insert no. 2 in place at the top of the cell

At 17H05

$$P_1 = 991.4 \text{ mbar}$$

$$P_2 = 992.6 \text{ mbar}$$

$$P_3 = 991.3/4 \text{ mbar}$$

$$T = 22.0^\circ\text{C} \text{ (air conditioning off)}$$

$$H_{res} = H - 320 = 165 \text{ mm}$$

$$h_{dyke} = 110 \text{ mm} \Rightarrow 180 \text{ mm}$$

Kicodet

$$\text{Time/pt} = 50 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 125 FPS

At 17H15, DGSO pumped up the cell

$$P_{dyke} = 913.5 \text{ mbar}$$

$$H_{res} = H - 357 = 128 \text{ mm}$$

$$P_3 = 991.2/3 \text{ mbar}$$

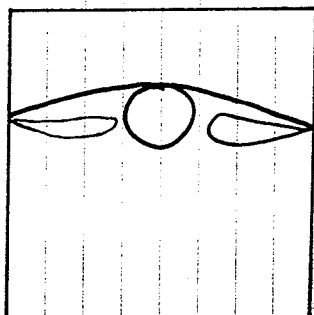
$$T = 22.0^\circ\text{C}$$

However  $P_1$  (tunnel pressure decreases)

$$P_1 = 965.8/9 \text{ mbar}$$

$$P_2 = 917.6/7 \text{ mbar}$$

Big bubbles come out from both sides of the gate into the cell:



OK if valve at the end of the tunnel is closed  $\Rightarrow$  no more air bubbles

Lower pressure in the tunnel.



At 17H20

$$P_1 = 491.5/6 \text{ mbar}$$

$$P_2 = 992.5 \text{ mbar}$$

$$P_3 = 991.2/3 \text{ mbar}$$

$$T = 22.0^\circ\text{C}$$

At 17H23, after run

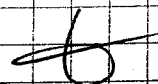
$$P_1 = 991.1/2 \text{ mbar}$$

$$P_2 = 992.3/4 \text{ mbar}$$

$$P_3 = 991.1/2 \text{ mbar}$$

$$T = 22.0^\circ\text{C}$$

17.12.2000



17-12-2000

Insert no 2 in place at the top of the cell

At 18H00

$$P_1 = 990.8/9 \text{ mbar}$$

$$P_2 = 992.0/1 \text{ mbar}$$

$$P_3 = 990.8/9 \text{ mbar}$$

$$T = 22.5^\circ\text{C}$$

$$H_{res} = H - 324 = 161 \text{ mm}$$

$$h_{dyke} = 106 \text{ mm} \Rightarrow 176 \text{ mm}$$

Nicotet

$$\text{Time / pt} = 125 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 60 FPS

Same as before when pumping up DGSO in the cell

$$P_2 = 910.2/3 \text{ mbar}$$

$$P_1 = 939.6 \text{ mbar and decreasing}$$

but no bubble this time.

At 18H05

$$P_1 = 945.2/3 \text{ mbar}$$

$$P_2 = 924.2/3 \text{ mbar}$$

$$P_3 = 990.8/9 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

$$H_{res} = H - 363 = 122 \text{ mm}$$

At 18H11

$$P_1 = 689.7/8 \text{ mbar}$$

$$P_2 = 992.2/3 \text{ mbar}$$

$$P_3 = 990.8 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

one big bubble from  
the siphon

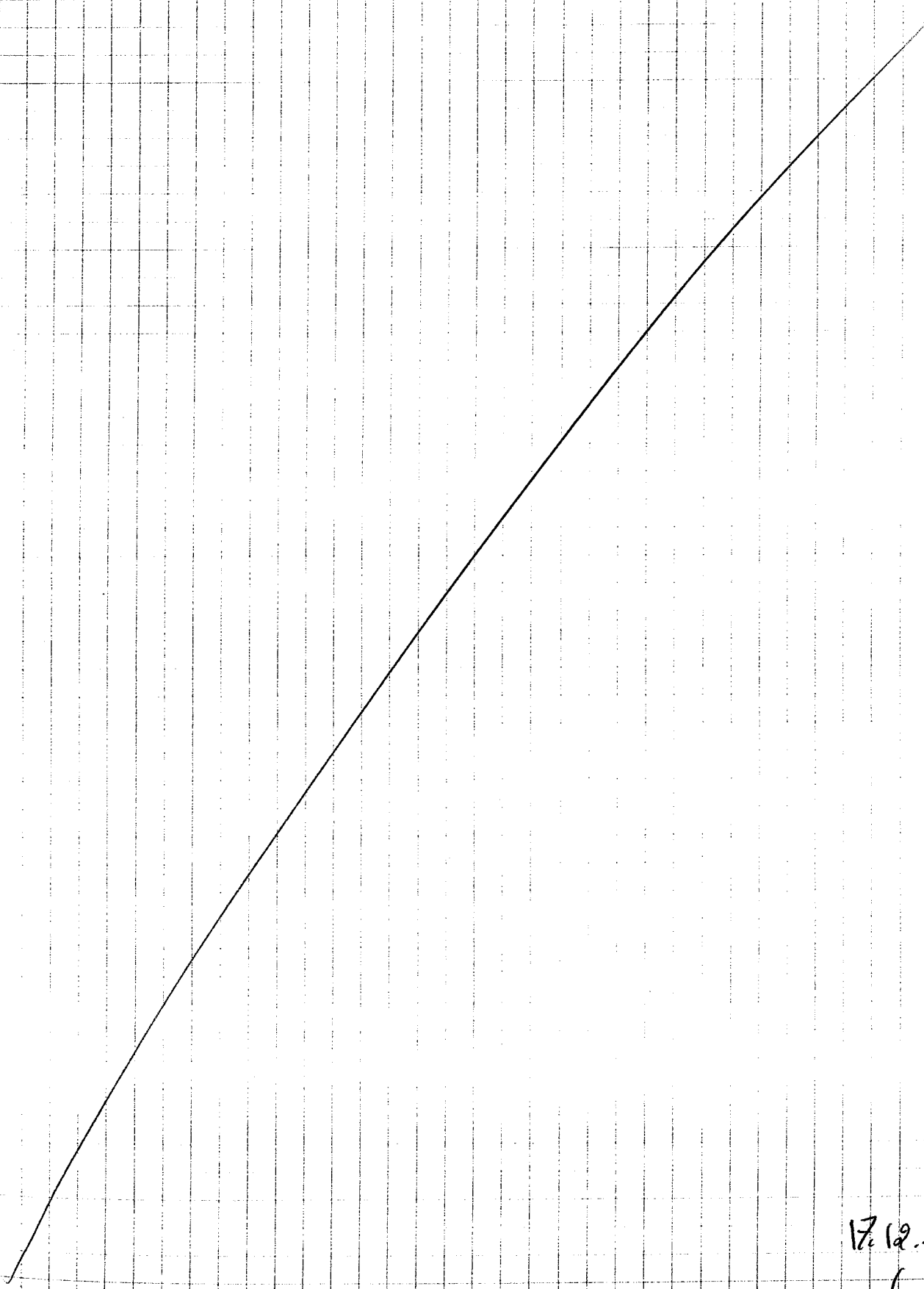
18H13

$$P_1 = 990.9 \text{ mbar}$$

$$P_2 = 992.2/3 \text{ mbar}$$

$$P_3 = 990.8 \text{ mbar}$$

$$T = 23^\circ\text{C}$$



17.12.2000

*[Signature]*

17-12-2000

Insert no 2 in place at the top of the cell

At 18H46

$$P_1 = 990.8/9 \text{ mbar}$$

$$P_2 = 991.9/992.0 \text{ mbar}$$

$$P_3 = 990.7/8 \text{ mbar}$$

$$T = 22.5^\circ\text{C}$$

$$H_{\text{res}} = H - 327 = 158 \text{ mm}$$

$$h_{\text{dyke}} = 103 \text{ mm} \Rightarrow 173 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 250 \mu\text{s}$$

$$\text{Trigger position} = \text{ptrig} 1\%$$

High-speed video 30 FPS

At 18H55, DGSO pumped up the cell

$$P_{\text{dyke}} = 925.2/3 \text{ mbar}$$

$$H_{\text{res}} = H - 366 = 119 \text{ mm}$$

$$T = 23.0^\circ\text{C}$$

$$P_1 = 990.7/8 \text{ mbar}$$

$$P_3 = 990.5/6 \text{ mbar}$$

Bubbles are coming out of the gate  $\Rightarrow$  next time, use silicone sealant around the outside of the gate.

At 19H00

$$P_1 = 890.0/1 \text{ mbar}$$

$$P_2 = 991.9 \text{ mbar}$$

$$P_3 = 990.4/5 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

When tunnel section eventually filled up,  $P_1 = 891.3/4 \text{ mbar}$

When D620 reached pressure transducer

m <sup>o</sup> 4 ( $P_{T4}$ )	$P_1 = 891.1/2 \text{ mbar}$
m <sup>o</sup> 5 ( $P_{T5}$ )	$P_1 = 891.0/1 \text{ mbar}$
m <sup>o</sup> 7 ( $P_{T7}$ )	$P_1 = 890.9/1 \text{ mbar}$

Towards the end of the run,  $P_1 = 890.8 \text{ mbar}$

At the end of the run,  $P_1 = 890.5 \text{ mbar}$



end of tunnel

At 19407	$P_1 = 990.6/7 \text{ mbar}$
	$P_2 = 991.9 \text{ mbar}$
	$P_3 = 990.4/5 \text{ mbar}$
	$T = 23.5^\circ\text{C}$

Transducer  $P_2$  didn't record any signal.

17.12.2000

17-12-2000

Insert 2 in place at the top of the cell

At 19445

$$\begin{aligned}
 P_1 &= 990.4/5 \text{ mbar} \\
 P_2 &= 991.6/7 \text{ mbar} \\
 P_3 &= 990.2/3 \text{ mbar} \\
 T &= 22.0^\circ \text{C} \quad (\text{heating on}) \\
 H_{\text{res}} &= H - 322 = 163 \text{ mm} \\
 h_{\text{dyke}} &= 109 \text{ mm} \Rightarrow 179 \text{ mm}
 \end{aligned}$$

(DGS0 added after previous run)

Nicotet

$$\text{Time/pt} = 350 \mu\text{s}$$

$$\text{Trigger position} = \text{prebias } 1\%$$

High-speed video 30 FPS

This time, lower  $P_{\text{tunnel}}$  before lowering  $P_{\text{dyke}} \Rightarrow$  same as before

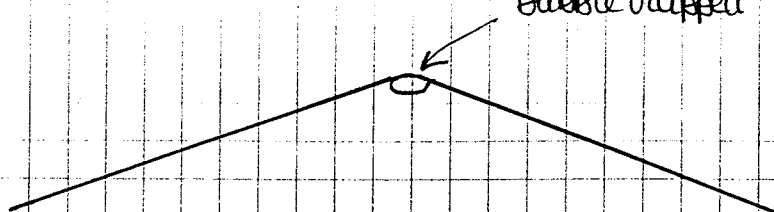
At 19455, DGS0 pumped up the cell

$$\begin{aligned}
 P_{\text{dyke}} = P_2 &= 924.4/5 \text{ mbar} \\
 P_3 &= 989.9/990.0 \text{ mbar} \\
 T &= 22.0^\circ \text{C} \\
 H_{\text{res}} &= H - 359 = 126 \text{ mm}
 \end{aligned}$$

At 20400,

$$\begin{aligned}
 P_1 &= 915.1/2 \text{ mbar} \\
 P_2 &= 991.3/4 \text{ mbar} \\
 P_3 &= 989.9/990.0 \text{ mbar} \\
 T &= 22.5^\circ \text{C}
 \end{aligned}$$

bubble trapped



After 1'13.15 in the air

$$P_1 = 916.2/3 \text{ mbar}$$

After 1'16.32

$$P_1 = 915.9 \text{ mbar}$$

At 20H10

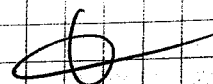
$$P_1 = 990.1 \text{ mbar}$$

$$P_2 = 991.4 \text{ mbar}$$

$$P_3 = 989.9/990.0 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

17.12.2000



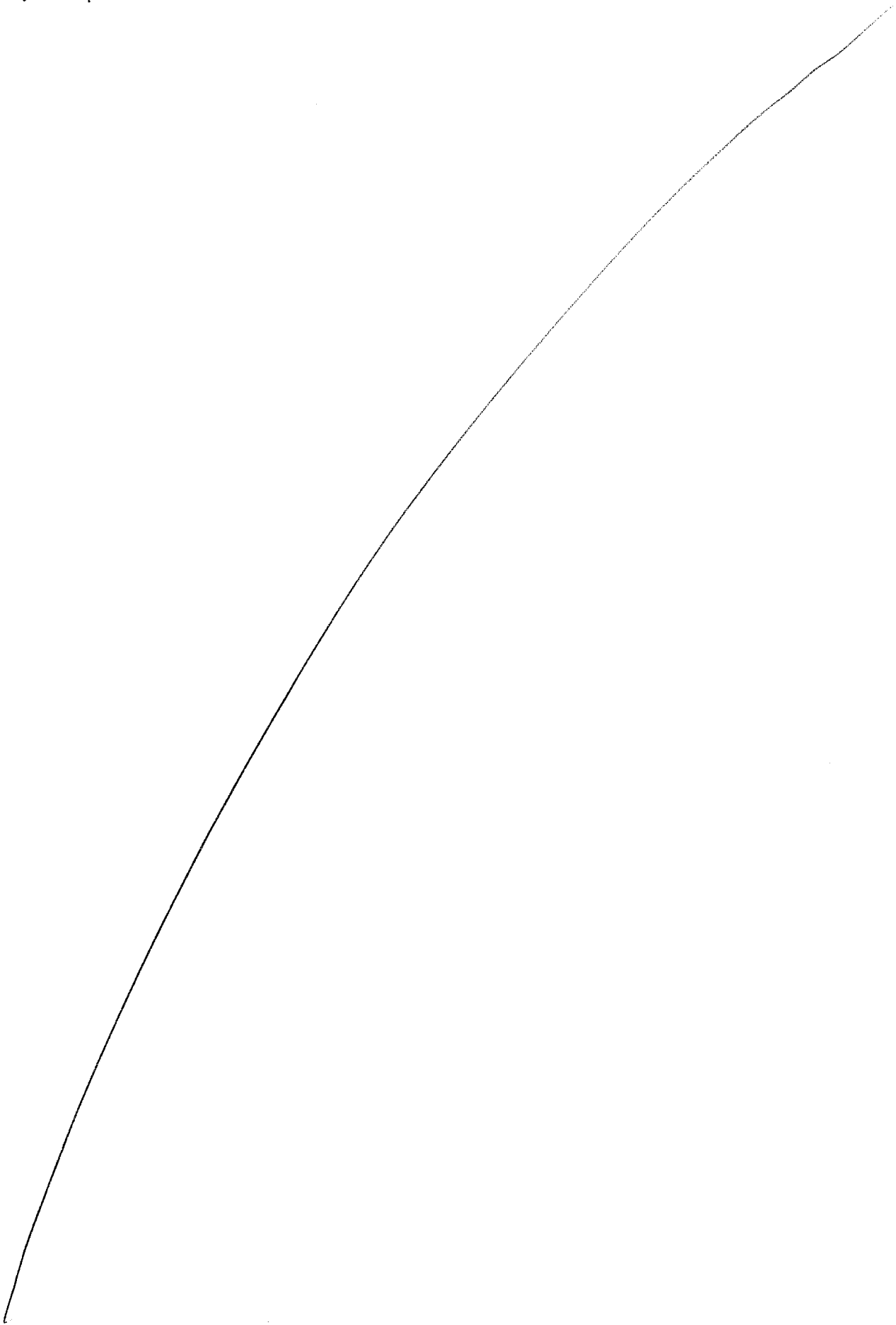
re 1/15/2002

Tunnel experiments with DGS5  
(expt n° 1 to 6)

03.09.2000



re 1/15/2002



03.09.2000

A handwritten signature or mark, possibly a stylized 'b' or a similar character, located below the date.

# Exp'r GS W5-1

page 1

03.03.00  
251 65  
re 1/15/200

$$\begin{cases} P_1 = 981.2 \\ P_2 = 980.1/2 \\ P_3 = 981.2/3 \\ T = 22^\circ\text{C} \end{cases}$$

at 15 H00

↳ Lower tunnel pressure  
 $P_1 = G \ 007630$  ( $\Delta P \approx 200 \text{ mba}$ )  
 $P_3 = G \ 008236$  (tunnel)  
 $P_3 = G \ 007631$  (dyke)  
 (Gimel cal)

High speed video set up @  $\begin{cases} 60 \text{ FPS} \\ \text{display size } 256 \times 120 \\ 01 \ 09-03-00 \end{cases}$   $\begin{cases} 1 \text{ min} \\ 28 \text{ sec} \end{cases}$  07.03.02

Nicolet setup @  $\begin{cases} \text{time/point } 250 \text{ } \cancel{300} \mu\text{s} \text{ (4.0 KHz)} \\ \text{scope time } 4.256 \text{ min} \\ \text{trigger position: pretrig } 1\% \text{ (7.62 } \cancel{1.31} \text{ sec)} \end{cases}$  07.03.02  
 1.310 sec  
 07.03.02

checked all leveled  
 from Nicolet  
 from videos

Nicolet data: files

W51/00/15.wf  
 in filename  
 GS W 5.1.wf  
 07.03.02  
 03.09.2000

15H30 10/10/2002

GSWS-1  
page 2

$$P_1 = 981.1/2$$

$$P_2 = 980.0/1$$

$$P_3 = 779.4/3$$

$$T = 22^\circ\text{C}$$

→ GSW to top of dike

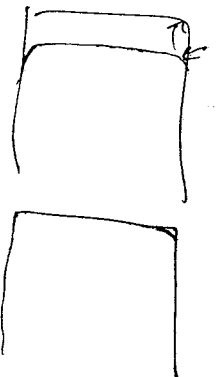
→ pb: air bubbles coming out of

16H20 from gate or from tunnel?



+ air bubble trapped  
top right corner

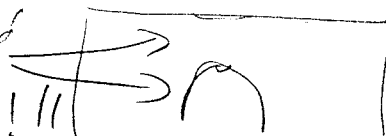
Due to shape  
of it  
when rising



→ dike not levelled  
on purposed  
slightly inclined  
dike higher → higher SS

17H05 still air bubbles being trapped

17H30 come from gate!!!



03.09.2002

At 17H35

top dyke 918.5 mbar =  $P_2$  re 4/15/16

GSL05-1  
page 3

7 bubbles (top)

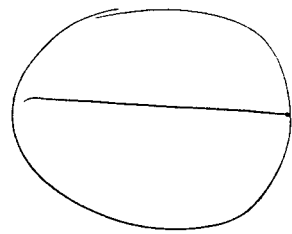
$P_1$  reservoir = 980.3/4

$P_3$  tunnel = 779.1 mbar

$T = 22.5^\circ \text{C}$

$P = 779.0 / 778.9$  cor.

back of dike



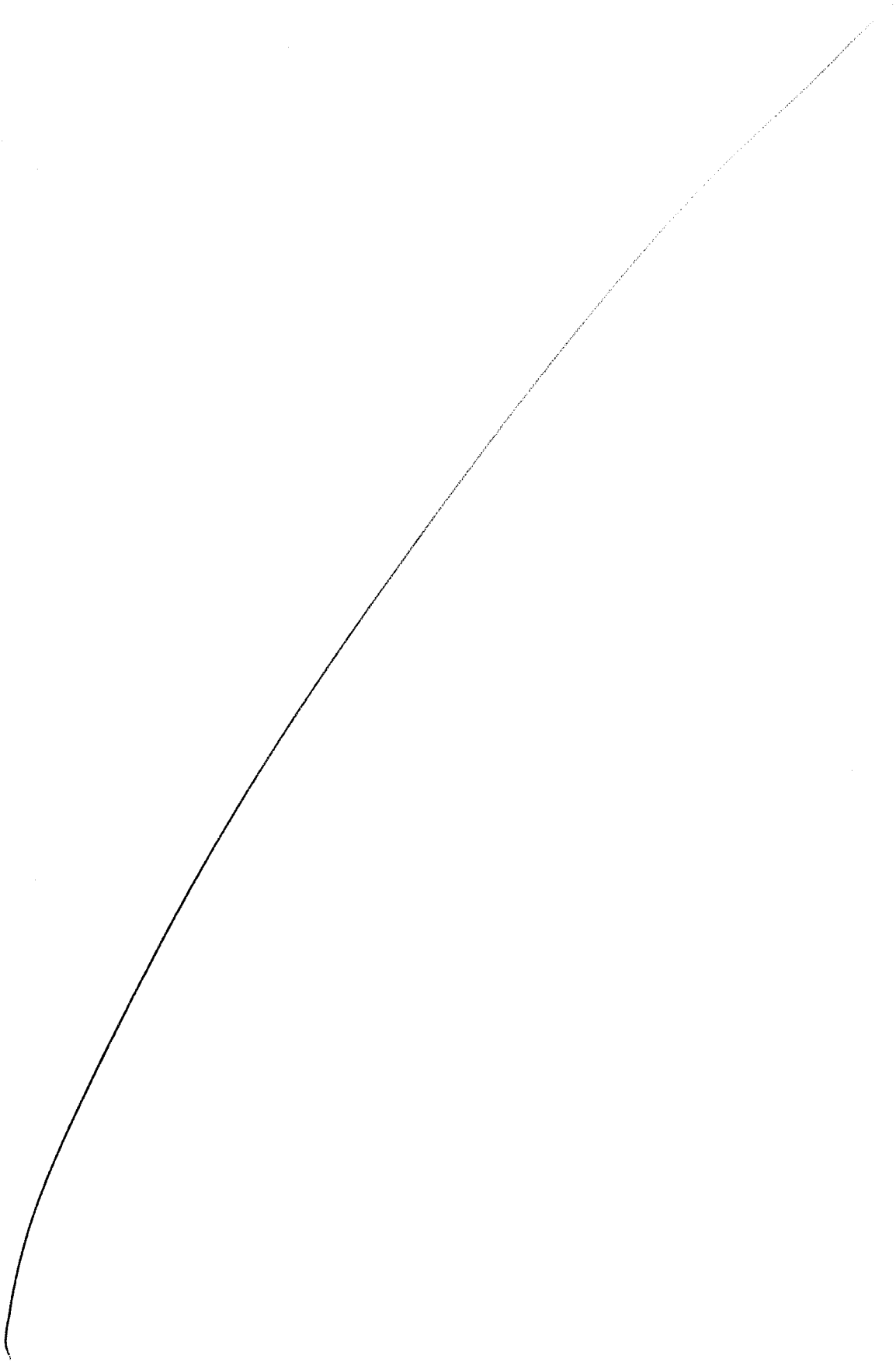
1.03.36 end tunnel

forgot tunnel value !!!

03.09.2000

254

re 1/15/2002



03.09.2000

A handwritten signature or mark, possibly a stylized '6' or a cursive name, located below the date.

# Expt GSWS - 2-1

03.03.00  
255  
1/15/2000 re

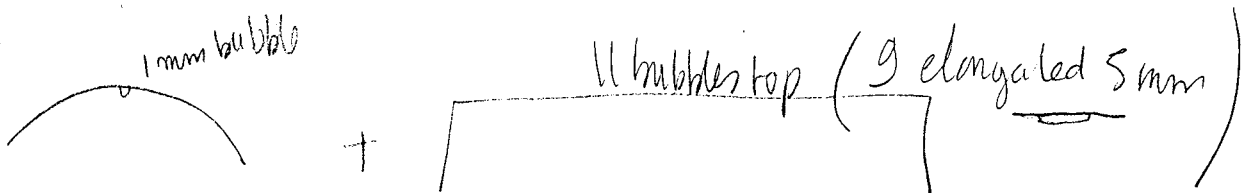
added more GSWS  $\rightarrow$   $\left[ \begin{array}{l} P_{\text{res}} = H-272 \\ h_{\text{dyke}} \quad 156.5 \rightarrow 158 \end{array} \right.$

18H40  $\left\{ \begin{array}{l} P_1 = 980.1/2 \text{ mbar} \\ P_2 = 979.1/2 \text{ mbar} \\ P_3 = 980.1/2 \text{ mbar} \\ T = 22.5^\circ\text{C} \end{array} \right.$

Level tunnel

GSWS to top of dyke  $P_2 = 925.5/6 \text{ mbar}$   
 $\rightarrow$  close dyke valve

Lower tunnel pressure ( $\Delta P \approx 200 \text{ mbar}$ )  
( $P_{\text{initial}} 979.9/980.0$ )



03.03.2000

re 1/15/2002

Expt 6502

200 mbar

high speed video

{ 02 09-03-00  
60 FPS

cam video

0:27:26:00

Nicolet sweep time

2.185 min ( $250 \mu s = \Delta T$ )

$$\left\{ \begin{array}{l} P_1 = 980.4/3 \text{ mbar} \\ P_2 = 979.3/4 \text{ mbar} \\ P_3 = 979.5 \text{ mbar} \\ T = 22^\circ \text{C} \end{array} \right.$$

19H30

$t = 4.02 \text{ sec}$  840.1 =  $P_3$  !!!

19 H 35

$$\left\{ \begin{array}{l} P_1 = 980.4 \\ P_2 = 979.3/4 \\ P_3 = 980.4/5 \\ T = 22^\circ \text{C} \end{array} \right.$$

→ HS video saved

T saved Nicolet

Labview C:\data\8552.dat

gs052.wft

w5200\*as.wft

1 to 8

03.09.2000

03.09.00

Ar 20 H30

$$\begin{cases} P_1 = 980.7/8 \\ P_2 = 979.6/5 \\ P_3 = 980.7 \\ T = 21.5^\circ\text{C} \end{cases}$$

Frame/time code	Temps (video)	Elapsed time (Pc)
1	0	0
1000		16.650
233	3.8667	<del>0.233</del> 07.03.02
61	1.0000	<del>1.000</del> 07.03.02
<del>53</del>		1.000
189	3.1333	3.133
377	6.2667	6.267
545	9.0667	9.067
647	10.7667	10.7667
999	16.6333	16.633
1001	16.6667	

03.09.2000



re 1/15/2002



500 FPS  $\longleftrightarrow$   $\sim$  8 sec  
250 FPS  $\longleftrightarrow$  17.4680 sec

Download images into PC:

ReadCam

$\rightarrow$  File

$\rightarrow$  Read Camera ...

setup camera on  
'live' mode

GSCS-2 Lasted  $\sim$  10 sec. max

04.09.2000

04.09.00

①

Exp 6505-3

300 mbars

10H30

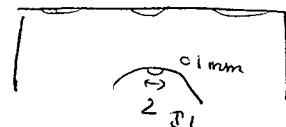
$$\left\{ \begin{array}{l} P_1 = 983.617 \\ P_2 = 982.213 \\ P_3 = 983.617 \\ T = 19^\circ \text{C} \\ h_d = 156.5 \text{ to } 158 \text{ mm (had to be out of level to prevent bubbles)} \\ h_R = H - 272 \text{ mm} \end{array} \right.$$

10H45

$$\left\{ \begin{array}{l} P_1 = 983.718 \\ P_2 = 982.213 \\ P_3 = 983.7 \\ T = 19^\circ \text{C} \end{array} \right.$$

→ rise in dike  $P_2 = 928.5 \text{ mbar}$

thin elongated  
3 at top v 7



high speed video

$$\left\{ \begin{array}{l} 03 \text{ } 09-04-00 \Rightarrow 108 \text{ sec} \\ 500 \text{ FPS} \end{array} \right.$$

Nicolet

$$\left\{ \begin{array}{l} \text{sweptime} = 10.486 \text{ sec} \\ \text{sample time/pt} = 20 \mu\text{s (50 kHz)} \\ \text{trigger position: 1\% pretrigger (104.838 ms)} \end{array} \right.$$

04.09.2000

Mr 11/100

dyke OK

P lowered in tunnel

Expt GS05-3

$$\rightarrow \begin{cases} P_3 = 683.54 \text{ mbar} \\ P_1 = 983.617 \\ P_2 = 982.314 \\ T = 19.5^\circ \text{C} \end{cases}$$

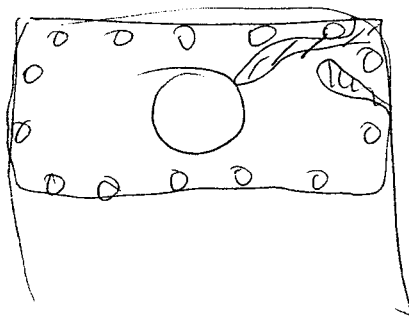
$$P_3 = 683.213$$

Just before opening gate  $P_3 = 683.0 / 682.9 \text{ mbar}$

$$\text{Mr 11/15} \begin{cases} P_1 = 983.516 \\ P_2 = 982.112 \\ P_3 = 983.5 \\ T = 20^\circ \text{C} \end{cases}$$

Note

Bubbles escaping from door

and  
entrained  
in tunnel

04.09.2000

Expr GSW-3

data saved in file:

Nicolet

gs53. wfr

↳ w5300 \* as. wfr

\* = 1 to 8

Aspeed video 4000 frames saved in S003TC.1

Lab view c:\data\gs53.dat

04.09.2000



1/15/2000  
Expt GSW5-4 ① 600 mbars

④

clean tunnel and its end  
 check and clean door

check tunnel air-proof (check at <sup>pressure</sup> ~~vacuum~~ of <sup>0.03.02</sup>  
 $\sim 350$  mbars)

Tunnel level

close valve  $\Rightarrow$   $P$  held ok,

$$\begin{cases} h_{\text{dike}} = 155.5 \text{ to } 156.5 \text{ mm} \\ h_R = H - 273 \text{ to } 274 \text{ mm} \end{cases}$$

At 12H20

$$\begin{cases} P_1 = 983.3/2 \text{ mbars} \\ P_2 = 982.2 \text{ mbars} \\ P_3 = 983.3/2 \text{ mbars} \\ T = 21.5^\circ\text{C} \end{cases}$$

GS up the dike:

Try to get rid of air in door mechanism:

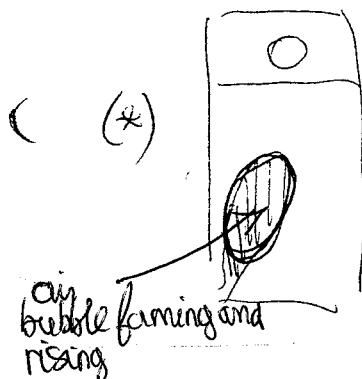
- tunnel at  $P_{\text{atm}}$  (air goes <sup>gate</sup> ~~tunnel~~  $\rightarrow$  dike)
- lower  $P$  in reservoir and dike at same value

tunnel = 383.3/4 12H25  
 then close valve

$\rightarrow$  12H30 385.0

- then have  $P_{\text{dike}}$  lower than  $P_{\text{res}}$
- so GS cover gate  $\Rightarrow$  wait

nothing much happens  
 but an air leak at bottom of tank (\*)



04.09.2000

*[Signature]*

Expt GSW5-4

(2)

04-09-00

263

re 1/15/200

→ go back to Normal routine: few air bubbles trapped in GSW5 due to bottom air leak

→ wait for a while until they have all disappear.

DGS5

At 13 H00

$$\left\{ \begin{array}{l} P_1 = 983.0 / 982.9 \\ P_2 = 981.8 / 9 \\ P_3 = 982.9 / 983.0 \\ T = 22^\circ \text{C} \end{array} \right.$$

→ tunnel down to  $P_3 = 382.817 \text{ mbar}$   
valve closed

DGS up the dyke: • very very slowly when reached top of gate ⇒ OK

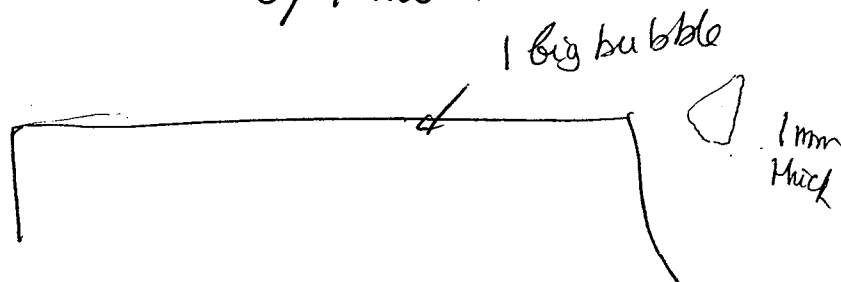


• top of dyke: one big  
→ wait

04.09.2000

7/264 re 1/15/2002  $P_2$  dike top = 928.6/7 mbar

(5)



$P_1$  reservoir = 982.8 mbar  
 $P_2$  back to atm = 981.7  
 $P_3$  tunnel = 381.2/1  
 $T = 21.5^\circ C$

High speed video 500 FPS - 04 09-04-00

Normal video 29:23:15

Wiscotet sweep time 10.486 s ( $\Delta t = 20 \mu s$ )

13 H 20  $\left\{ \begin{array}{l} 381.2 \text{ mbar} = P_3 \\ 982.718 = P_1 \\ 981.2 = P_2 \end{array} \right.$

(\*)

no air leak at gate but one at bottom of dike →

04.09.2000

Exp 1680507  
OK as no bubble reach top before the expt ⑦ ended

At 13 H30

$$\begin{cases} P_1 = 982.7/6 \\ P_2 = 981.5/6 \\ P_3 = 982.6/7 \\ T = 22^\circ\text{C} \end{cases}$$

Data saved in file:

Nicolet gsw54.wfr

↳ w5400 \* as.wfr

Hspeedvideo 2500 frames saved in 5004TC.1

labview C:\data\gsw54.dat

video 29:23:15 → 29:50:25

04.09.2000





# Expt GSW5-5

①

800bars

N.B. pressure transducer cable no 3

(pin might be damaged in near future (slightly bent, pin OK))

Considering using high speed video @ 1000 FPS

→ recording time = 4.3670 sec

↳ Nicolet timebase :

{ Sweep time = 5.243 sec  
 $\Delta t = 10 \mu s$  (100 KHz)  
 (pre trig = 52.419 ms (1%))

At 14 H45

{  $P_1 = 981.7/8$   
 $P_2 = 980.7/8$   
 $P_3 = 981.8/9$   
 $T = 22.5^\circ C$   
 $h = 155.5$  to  $157$  mm  
 $h_R = H - 275$   
 to  $275.5$  mm

↳ tunnel down to ~~2784~~ 07.03.09

had difficulties in getting lower than 185mb  
 check integrity of tunnel and trap

→ OK  
 check around vacuum control system  
 (S when trying to lower P further, P not stable (181 to 185))

04.09.2000

*[Signature]*

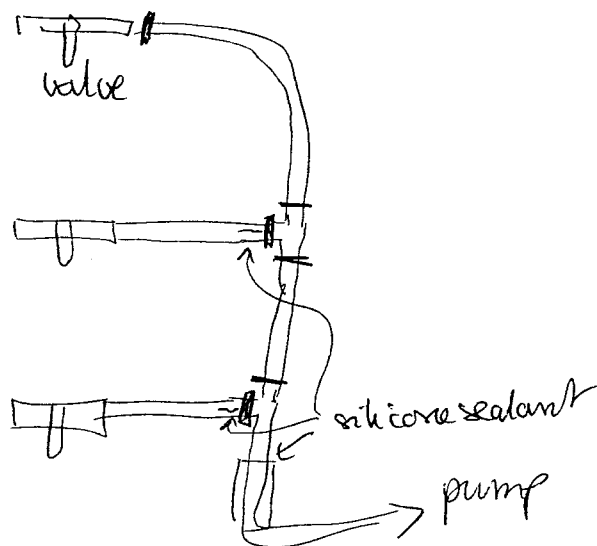
Expt GSWS-5

②

04.09.00

07.03.02

⇨ inspection revealed cracks in tubing



⇒ problems sorted out using silicone sealant!

pump down straight  
to ~100 mbar!

GSWS to top of dyke

bubble state: good!

4 ~5 mm ones at top  
+ few tiny ones

$P_2 = 926.9 / 927 \text{ mbar}$   
at top of dyke  
 $P_1 = 981.6 \text{ mbar}$   
 $T = 22.5^\circ\text{C}$

04.09.2000

Exp 82005  
268  
re 1/15/2002  
(3)

(10)

At 15H15

$$\left\{ \begin{array}{l} P_1 = 981.4/5 \\ P_2 = 980.5/6 \\ P_3 = 181.0/180.9 \\ T = 23^\circ\text{C} \end{array} \right.$$

Start 15H20

→ ~ 232 mbar in tunnel at end of exp

bubbles came from gate mechanism

At 15H35

$$\left\{ \begin{array}{l} P_1 = 981.2/1 \text{ mbar} \\ P_2 = 980.2/3 \text{ mbar} \\ P_3 = 981.2 \text{ mbar} \\ T = 23^\circ\text{C} \end{array} \right.$$

Data saved in

video ~~21.5.22~~ 07.03.02  
Nicole 85055. wfr  
Labview 8555. dat  
high speed video 3000 frames in 5005 tc. 1  
07.03.02

Up to 36:20:29  
→ 05500 \* 02. wfr  
exp to be redone if (bubbles)

04.09.2000

Expt GSWS-6  
(1)

Scombas

04.09.00  
11 <sup>stet...</sup><sub>re</sub>

N.B. pressure transducer cable no 3 broken: spin cut  
and stick into transducer.!

put cable in place and will see how it runs  
( $\Rightarrow$  checkrun first w/ Nicolet)

4.368 s

High speed video setup at  $\left\{ \begin{array}{l} 1000 \text{ FPS} \\ 06 \quad 09-04-00 \end{array} \right.$

Nicolet setup at  $\left\{ \begin{array}{l} \text{sweptime} = \frac{2.621}{07.03.02} \text{ sec} \\ \Delta t = 5 \mu\text{s} \quad (200 \text{ KHz}) \\ \text{Prebig (1\%)} \quad 26.209 \text{ ms} \end{array} \right.$

Normal video from 30:20:29

Use same procedure as in expt GSWS-4 to get rid of air  
trapped in gate mechanism

$$\text{At } 16 \text{ Hz } \left\{ \begin{array}{l} P_1 = 980.8/9 \\ P_2 = 980.0/979.9 \\ P_3 = 980.9/981.0 \\ T = 23^\circ\text{C} \\ h_d = 154 \text{ to } 155 \text{ mm} \\ b_{\text{res}} = H - \left\{ \begin{array}{l} 274 \\ 275.5 \end{array} \right\} \end{array} \right.$$

04.09.2000

re 1/15/2002

Expt GSW 5-6

(2)

(12)

At 16 H40

$$\begin{cases} P_1 = 980.4/5 \\ P_2 = 979.8/9 \\ P_3 = 980.7 \\ T = 23^\circ\text{C} \end{cases}$$

$P_3$  does not decrease further down than 150 mbar  
still pb with tubing near control panel. Add more silicone sealant



$P_3 = 30.4/3$  mbar lowest reachable

(etching of tunnel system fine)

(from 30.0 to 40.7 in v.  $\phi 07.03.02$  5 mm)

Dyke

$P_2$  dyke = 926.1/2 mbar

at top  
1 bubble ~ 5 mm  
otherwise  
very few

At 17 H05

$$\begin{cases} P_1 = 980.5 \\ P_2 = 979.8/7 \\ P_3 = 979.5/6 \\ T = 24^\circ\text{C} \end{cases} \phi 07.03.02$$

04.09.2000

At 17H40

$$\left\{ \begin{array}{l} P_1 = 980.5/4 \\ P_2 = 979.7/8 \\ P_3 = 980.7/8 \\ T = 23.5^\circ\text{C} \\ h_d = 153 \text{ to } 154 \text{ mm} \\ h_R = H - \frac{277}{275.5 \text{ mm}} \end{array} \right.$$

(13)  
271 ~~85~~  
08/15/2002

During clean up, broke the end of the glass tube (bore) into its "reinforcement"

→ carry on expts without P data  
next

→ ~~07.03.02~~ can't because  
does not have a spare tube  
cut at end ready (all  $\bar{v} = 1$ )

### Data save

Nicobar W5600 \* as .wtf files in gsw56. wtf  
Labview gsw56. dat  
high speed 2500 frames  
saved in  
5006tc.1

camvideo up to 30:50:14

→ (prepare overnight the  
spare  
one with  
P transducer

04.09.2000



re 1/15/2002

(14)

# Summary of expts done with GSW5

dyke  $\begin{cases} h_i = 32 \text{ mm} \\ h_i = 108 \text{ mm} \end{cases}$

↳ Give up w/ 243 mm

tunnel  $\begin{cases} 200 \\ 400 \text{ } 300 \text{ } \text{to } 07.03.02 \\ 600 \\ 800 \\ \sim 1000 \end{cases}$

↳ go direct to GSW15  
and unload GSW5

plan

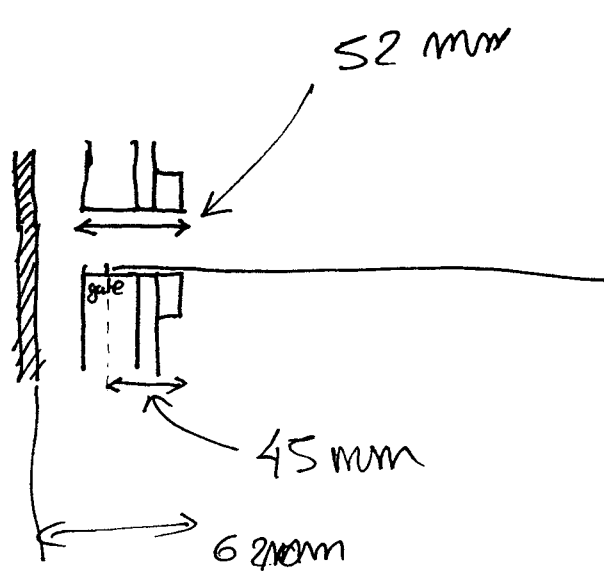
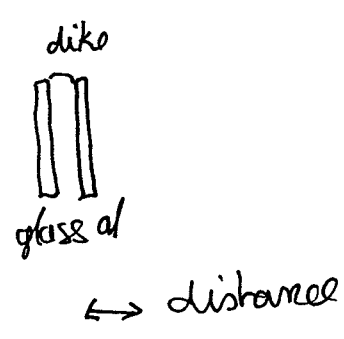
$\begin{bmatrix} 50 \\ 100 \\ 200 \\ 400 \\ 600 \\ 800 \\ 1000 \end{bmatrix}$

7  
tunnels

then dyke at 110 mm to 07.03.02

04.09.2000





04.09.2000

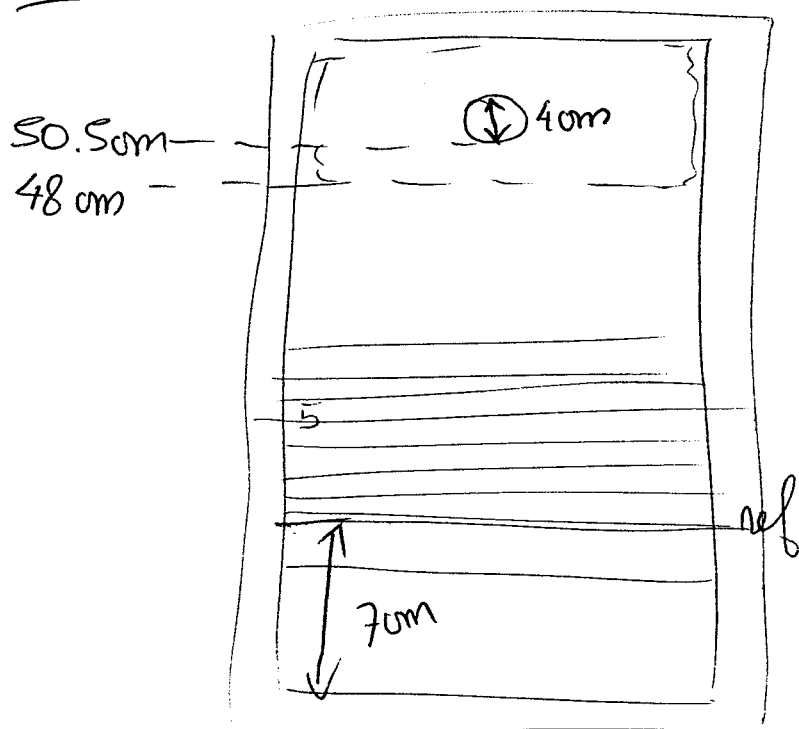




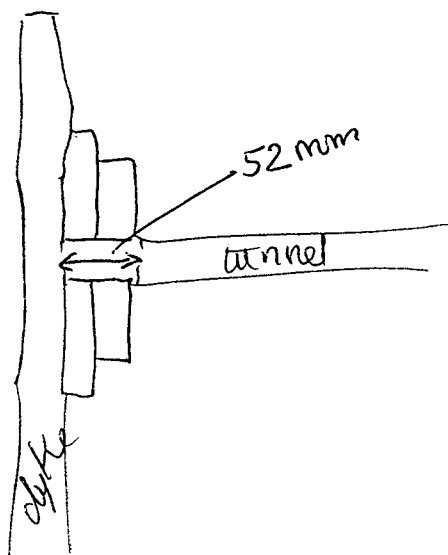
re 1/15/2002

HScoll

15



line  $\circ$  = ref line  
for dyke exposure  
at 70m above  
bottom of dyke  
reservoir

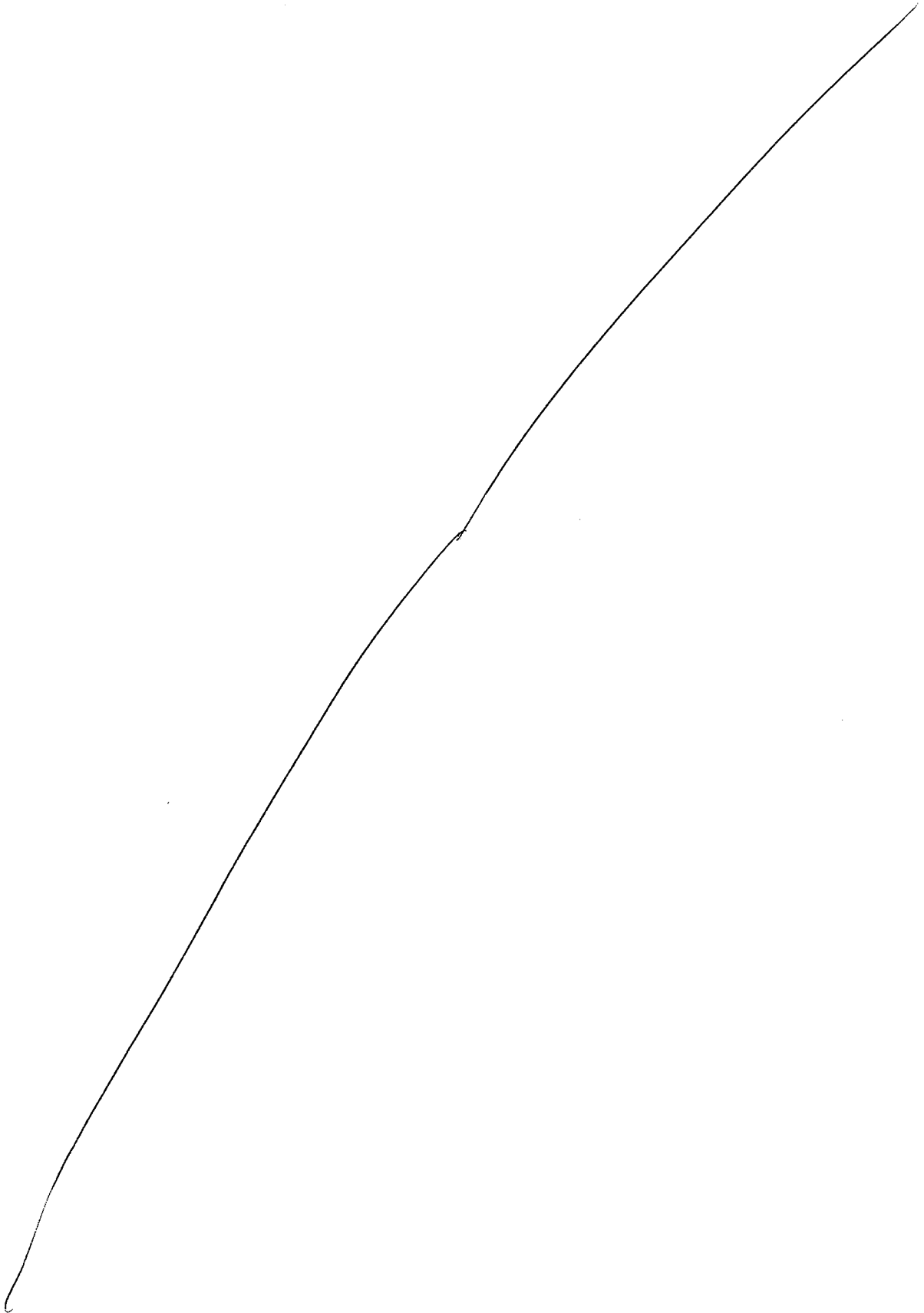


215 93  
re 4/15/2002

Tunnel experiments with DGS 15  
(expt no 1 to 30)

+

re 1/15/2002



04.09.2000

Prepare more DG815

flask vide 642.7g

+ GS 1208.5g

↳ 565.8g

↓  
needs 84.87g H<sub>2</sub>O

↓  
Theo 1293.4g  
Real 1293.4g

re 1/15/2002

①

At 8H00

$$\begin{cases} P_1 = 983.5/6 \\ P_2 = 982.4/5 \\ P_3 = 983.8/7 \\ T = 19^\circ\text{C} \end{cases}$$

More GSW15:

649.5g

1388.1g

↳ 738.6g GS

↳ needs 110.7g g H<sub>2</sub>O

↳ Theo 1498.8g  
real 1499.0

At 11H00

$$\begin{cases} P_1 = 984.0/1 \\ P_2 = 983.2/3 \\ P_3 = 984.4 \\ T = 21.5^\circ\text{C} \end{cases}$$

(AC off while preparing GSW15)

05.09.2000

①

- Transducers set on new tube in the morning

Tunnel hold 35 mbar vacuum

Nicolet

time/pt = 200  $\mu$ s (5.0 kHz)  
triggers

DGS15-1  
①

EXPT DGS15-~~1~~

$$h_d = 158.75 \rightarrow 159.25 \text{ mm}$$

$$h_R = H - (270 \text{ to } 271 \text{ mm})$$

At 1155

$$\begin{cases} P_1 = 983.8/9 \\ P_2 = 982.7 \\ P_3 = 983.9 \\ T = 21^\circ \text{C} \end{cases}$$

$P_2$  topdyke 928.1 mbar  
 $\sim 6$  bubbles (5 mm)

280  
re 1/15/2002

$$P_3 = 683.0 / 682.9$$

$$P_2 = 982.4$$

$$P_1 = 983.4 / 5$$

DGS15-1

2

At 12H50

$$P_1 = 983.1 / 2$$

$$P_2 = 982.1 / 2$$

$$P_3 = 983.2 / 3$$

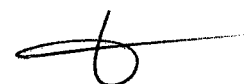
$$T = 21.5^\circ\text{C}$$

Lasted

< 1s

Fagot to switch on the Ptransducers conditioner  
units!!!  $\Rightarrow$  no Pdata available.

05.09.2000



1/ DGS15-2 ①

At 14H15

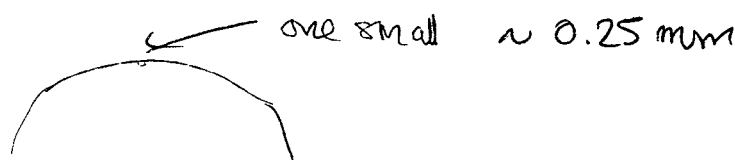
$$\left\{ \begin{array}{l} P_1 = 981.8/9 \\ P_2 = 981.0/980.9 \\ P_3 = 982.0/981.9 \\ T = 23^\circ\text{C} \\ h_D = 157 \text{ to } 158 \text{ mm} \\ h_{res} = H - 271 \text{ to } 271.5 \text{ mm} \end{array} \right.$$

281  
re 1/15/2000  
EXPT DGS15-2

Check tunnel (762.7 mbar) 77.4/5 mbar

$P_{\text{Dyke}} = 924.8/9 \text{ mbar}$

Bubbles



3 "large" at top  thickness < 1 mm

05.09.2000



Labview  
282  
re 1/15/2002

sampling rate : 10000 samples/sec  
buffer size : 20000

High speed video

2000 FPS  
display size  $288 \times 420 \Rightarrow \sim 2 \text{ sec}$   
02 09-05-00

Video from ~~31.12.99~~ (31.20:17)  
07.03.02

Nicolet

time/pt = 2  $\mu\text{s}$  (500 KHz)  
sweep time = 1.049 sec  
pretrigger 1%  $\Rightarrow$  10.484 ms


At 14H55

$\left\{ \begin{array}{l} P_1 = 981.2/3 \text{ mbar} \\ P_2 = 980.5/4 \text{ mbar} \\ P_3 = 979.5/6 \text{ mbar} \\ T = 23^\circ \text{C} \end{array} \right.$

At 16H20

$\left\{ \begin{array}{l} P_1 = 980.3/2 \\ P_2 = 979.6/7 \\ P_3 = 980.4/5 \\ T = 24^\circ \text{C} \end{array} \right.$

05.09.2000



DGS 15-2

(3)

05-09-2000

Data saved as :

Nicolet

dgs 15\_2 x  $\begin{array}{c} a \\ b \\ as \end{array}$  . wtf in folder

Pdgs 15\_2

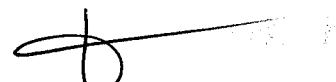
MSvideo

4368 frames in folder Vdgs15\_2

Labview

dgs 15\_2 . dat

05.09.2000



re  
1/15/2002

Expt DGS 15-3

①

At 17 H30

$$\left\{ \begin{array}{l} P_1 = 979.8/7 \\ P_2 = 979.1/2 \\ P_3 = 980.0 / 979.9 \\ T = 23.5 \\ h_d = 156 \text{ to } 157 \text{ mm} \\ h_R = H - (272 \text{ to } 273 \text{ mm}) \end{array} \right.$$

High speed video

2000 FPS

display size 256x120

03 09-05-00

Video from 31:54:19

Nicdet

$\left\{ \begin{array}{l} \text{time/pt} = 4 \text{ us} \text{ (} 250 \text{ KHz)} \\ \text{Sweep time} = 2.097 \text{ sec} \\ \text{meas 1\%} \Rightarrow 20.968 \text{ ms} \end{array} \right.$  07.03.02

Labview

$\left\{ \begin{array}{l} \text{sampling at } 10000 \text{ samples/sec} \\ \text{buffer size: } 20000 \\ \text{das 15_3.dat} \end{array} \right.$

Check tunnel elongicity at 200 mbar (fine)

→ prepare dyke at 17 H45 (10 428 mbar)  
lgate

05.09.2000



Expt DGS 15-3  
②

$$\left[ \begin{array}{l} P_2 \text{ dyke} = 926.5 \text{ mbar} \\ P_1 = 979.6/7 \\ P_3 = 979.6 \\ T = 24^\circ\text{C} \end{array} \right.$$

18400

→ At 18405

Just before opening gate,  $P_{\text{channel}} = 379.6/7$   
at end of expt  
gap of 25 mm at top of dike

$$\left[ \begin{array}{l} P_1 = 979.6/7 \\ P_2 = 979.1/2 \\ P_3 = 379.3/4 \\ T = 24^\circ\text{C} \end{array} \right.$$



At 18407

$$\left\{ \begin{array}{l} P_1 = 979.7/6 \\ P_2 = 979.1 \\ P_3 = 979.8/9 \\ T = 24^\circ\text{C} \end{array} \right.$$

(~10 psi)

1/15/2002 Expl DGS 15-3  
③

Data saved as: Folder Dgs15\_3

Nicole dg3/001 as. wft

Labview dgs15\_3.dat

48 video frames in folder Vdgs15\_3

05.09.2000



Expt DGS15-4

①

05-09-2000

At 19 H 00

$$P_1 = 979.7/8$$

$$P_2 = 979.0/1$$

$$P_3 = 979.9/980.0$$

$$T = 23^\circ\text{C}$$

$$R_{\text{dyke}} = 153 - 154 \text{ mm}$$

$$h_{\text{res}} = H - (275 \text{ to } 276.5 \text{ mm})$$

Check tunnel etanchéité at 95 mbar

Prepare dyke at 360 mbar

$$P_{\text{dyke}} = 924.8/9 \text{ mbar at 19 H 15}$$

$$P_1 = 979.6/7$$

$$P_3 = 979.8/9$$

$$T = 23^\circ\text{C}$$

At dyke top

1 bubble

1 bubble

+  
few small ones  
all < 1 mm thickness

$$\hookrightarrow P_{\text{tunnel}} = 579.1/2 \text{ mbar}$$

05.09.2000

Expt DGS15-4

(2)

High speed video

$\left\{ \begin{array}{l} 2000 \text{ FPS} \\ 04 \end{array} \right. (2.1835 \text{ sec})$   
09-05-00

Nicobak

$\left\{ \begin{array}{l} \text{sweep time} = 2.097 \text{ sec} \\ \Delta t = 4 \mu\text{s} \end{array} \right.$

Labview

$\left\{ \begin{array}{l} 10000 \text{ samples/sec} \\ \text{buffer} = 20000 \\ \text{dgs15\_4.dat} \end{array} \right. (636)$

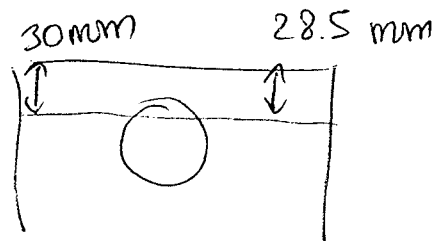
Video from

32:29:08

At 19 H 30

$\left\{ \begin{array}{l} P_1 = 979.9 / 980.0 \\ P_2 = 979.1 / 2 \\ P_3 = 579.1 \\ T = 23^\circ\text{C} \end{array} \right.$

End of expt: dyke



05.09.2000

At 19 H35

$$\begin{aligned} P_1 &= 980.0/1 \\ P_2 &= 979.1/2 \\ P_3 &= 980.1/2 \\ T &= 23^\circ \text{C} \end{aligned}$$

Exp DG85.4  
③  
05-09-2000


Labview : acquisition stop before signal!  
(data in dg815\_4.dat)

↳ take smaller  
sampling rate

Nicolet saved in folder Pdgs15\_4  
as file dg4 001 as .wft

MS video saved in folder Vdgs15\_4 (4366 frames)

05.09.2000



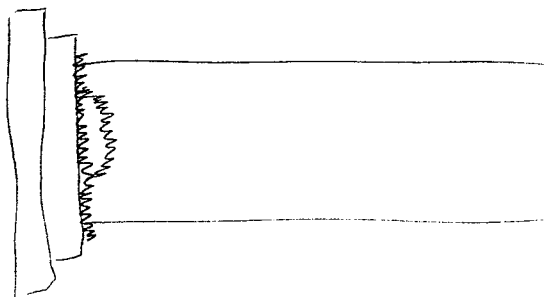


Expt DGS 15 - 3

①

Tube broken at its dyke end while pulling it back in place (heard noise at previous expt)

↳ silicone sealant on crack and all around <sup>(#)</sup> connector



Fingers crossed for last expt!

At 20 H<sub>2</sub>O

$$P_1 = 980.4/5$$

$$P_2 = 979.6/7$$

$$P_3 = 980.6/7$$

$$T = 22.5^\circ\text{C}$$

$$h_{\text{dyke}} = 151 \text{ to } 152 \text{ mm}$$

$$R_{\text{res}} = H - (277 \text{ to } 278 \text{ mm})$$

Check tunnel etanchéité  $\Rightarrow$  had more sealant

valve closed at 270 mbar not bad at all!

↳ then down to 230

↳ 275 mbar heard cracking

05.09.2000

*[Signature]*

⇒ decide to run

Expt DGS15-5

(2)

re 1/15/2002

05.09.00

Prepared dyke at 404 mbar

Top of dyke = 922.1/2 mbar

3 bubbles (○)

$\left\{ \begin{array}{l} P_1 = 980.6/7 \text{ mbar} \\ P_3 = 980.5/6 \\ T = 220^\circ \text{C} \\ P_2 = 979.8/7 \end{array} \right.$

20H35

Video from 32:59:17

Nicolet

time / pt 100  $\mu$ s

Trigger position: PreTrig = 524.188 ms  
(1%)

Sweep time = 52.429 sec (524288  
pts)

High speed video

60  $\mu$  / sec ⇒ recording  
60 FPS

05 09-05-00

Don't bother w/ Labview

05.09.2000



re 1/15/2006  
Exp'r DGS 15-5  
(3)

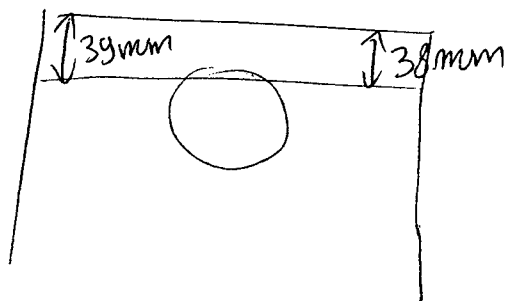
Mr 20 HSO

$$P_1 = 980.8/9$$

$$P_2 = 980.0/980.1$$

$$P_3 = 879.4/5$$

$$T = 22^\circ\text{C}$$



Mr 20 HSS,

$$P_1 = 980.9/981.0$$

$$P_2 = 980.0/979.9$$

$$P_3 = 981.2/1$$

$$T = 22^\circ\text{C}$$

Save data

Nicole

folder Pdgs 15\_5

as files dg5001as.wfl

High Speed video

folder Vdgs 15\_5

(500 frames)

05.09.2006

# Expt DGS15-6

①

glass tube broken

little pieces of glass near entrance

silicone sealant around tunnel connector

still DGS on tunnel floor (see picture)

At 15H45

$$P_1 = 980.3/2$$

$$P_2 = 979.4/3$$

$$P_3 = 980.4/5$$

$$T = 21^\circ\text{C}$$

$$h_{\text{dyke}} = 151 \text{ mm} \quad (\text{levelled})$$

$$h_{\text{res}} = H - 274 \text{ mm}$$

Check tunnel etancheity at  $P = \text{~~102~~ mbar}$  07.03.02

Prepuning dyke @ 430 mbar 102  $\rightarrow$  120 in  $\approx$  1 min

Nicolet  $\left[ \begin{array}{l} \text{sweep time} = 1.049 \text{ sec} \quad (524288 \text{ pts}) \\ \text{time / pt} = 2 \mu\text{s} \quad (500 \text{ KHz}) \\ \text{Pre Trig } 1\% \quad (10.484 \text{ ms}) \end{array} \right.$

High Speed video  $\left[ \begin{array}{l} 06 \quad 09-06-00 \\ 2000 \text{ FPS} \end{array} \right.$

06.09.2000


re 1/15/2002

Trans	Nicolet Channel
6	3B
5	3A
8	4B
7	4A
4	2B
3	2A
2	1B
1	1A

18H20

$P_1 = 979.817$
$P_2 = 978.819$
$P_3 = 979.9 / 980.0$
$T = \text{avg } 152 \text{ mm}$
$h_a = 22^\circ \text{C}$

06.09.2000



Dyke = ~~926.6 mbar~~

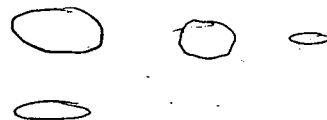
re 1/15/2002

927.2 ~~to~~ 06.09.00 5 bubbles at top

$P_1 = 979.6/7$

$P_3 = 979.9/980$

$T = 22^\circ\text{C}$



17H35

Data saved as

dg6 co \* as. wfb

↳ Pdg815\_6

06.09.2000

DG815-7

12 Dec 2000

$$\left\{ \begin{array}{l} H_{res} = H - 320.5 \text{ mm} \\ h = 107 \text{ mm} \end{array} \right\} \text{ at } P_{atm}$$

$$\left\{ \begin{array}{l} P_1 = 993.1/2 \\ P_2 = 994.5 \end{array} \right.$$

$$P_3 = 993.3/4$$

$$\left\{ \begin{array}{l} P_{dyke} = 938.1/2 \\ h_{dyke \text{ top}} \\ H_{res} = H - 364 \text{ mm} \end{array} \right.$$

16 H30

$$P_3 = 993.2/3$$

$$P_1 = 33.3/2/4 \text{ (tunnel)}$$

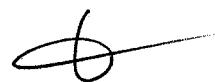
$$T = 22^\circ\text{C}$$

$$\left\{ \begin{array}{l} P_2 = 935.8 \text{ (adjusted as bubble came out of hole top)} \\ P_1 = 33.4/5 \end{array} \right.$$

19 H40

$$\left\{ \begin{array}{l} P_1 = 993.0/1 \text{ mbar} \\ P_2 = 994.2/3 \text{ mbar} \\ P_3 = 993.2/3 \text{ mbar} \\ T = 22^\circ\text{C} \end{array} \right.$$

12.12.2000



# Expt DGS15-8

$\Delta P \approx 600 \text{ mbar}$

1000 FPS  
display size  $256 \times 128$   
08 H-13-00

Nicole time/pt = 5 s

$R_{\text{res}} = H - 323 \text{ mm}$   
 $R_{\text{dyke}} = 103 \text{ mm}$

$P_1 = 987.3/4$   
 $P_2 = 989.0/988.9$   
 $P_3 = 987.2/1$   
 $T = 23.5^\circ\text{C}$

16 HSO

17H00

$P_{\text{dyke}} = 927.6$   
 $P_{\text{tunnel}} = 386.3/4$

$T = 23.5$

$P_2 = 989.0/1$   
 $P_3 = 972$

13.12.2000





P<sub>1</sub> ~~387.1/0~~ 386.9 07.03.02

P<sub>2</sub> 989.1/2 17H05

P<sub>3</sub> 987.2/3

↳ 410 in tunnel

17H10 { P<sub>1</sub> 987.5/6  
P<sub>2</sub> 989.1/2  
P<sub>3</sub> 987.3/4  
T 23.5°C

13.12.2000



## Expt DGS 15 - 9

$$\Delta P \approx 300 \text{ mbar}$$

1000 FPS

display size 256 x 120

09 12-13-00

1500  
3000

Nicolek time/pt = 5ms

$$h_{\text{res}} = H - 327 \text{ mm}$$

$$h_{\text{dyke}} = 100.5 \text{ mm}$$

$$\left\{ \begin{array}{ll} P_1 & 988.1/2 \\ P_2 & 989.6/7 \\ P_3 & 987.9 \\ T & 23 \end{array} \right. \quad 18H10$$

$$\left\{ \begin{array}{ll} P_{\text{dyke}} & = 931.1 \text{ mbar} \\ P_{\text{panel}} & = 687.4/5 \\ T & = 23^\circ \text{C} \end{array} \right. \quad (H_{\text{res}} = h - 373 \text{ mm})$$

18H30

$$P_2 = 989.8/9$$

$$P_3 = 988.1/0$$

re 1/15/2000

$$\left\{ \begin{array}{ll} P_1 & 988.5/6 \\ P_2 & 990.0/1 \\ P_3 & 988.2 \\ T & = 23.5 \end{array} \right.$$

18H40

13.12.2000



Expt DGSIS-10

500 FPS 1/15/2002

$\Delta$  Nicot = 10  $\mu$ s

$\Delta P = 100$  mbar

$P_1 = 989.1$   
 $P_2 = 990.6$  ~~18~~ 07.03.02 19H15  
 $P_3 = 988.7$  ~~18~~ 07.03.02  
 $T = 23^\circ\text{C}$

$h_{dy} = 97.5$   
 $H_{res} = H-333$

$P_{dyke} = 932.7$  ~~18~~ 07.03.02

19H20  $\left\{ \begin{array}{l} P_1 = 885.8 \\ P_2 = 990.6/7 \\ P_3 = 988.8/9 \\ T = 23 \end{array} \right.$

19H20  $\left\{ \begin{array}{l} P_1 = 989.2B \\ P_2 = 990.8/9 \\ P_3 = 989.0 \\ T = 23 \end{array} \right.$

13.12.2000



Expt DGS 15-11

$\Delta P \approx 200 \text{ mbar}$

500 FPS

$\Delta t_{\text{Mic}} = 10 \mu\text{s}$

$P_1 = 990.8/9$

$P_2 = 992.2/3$

$P_3 = 990.6/7$

$T = 23^\circ\text{C}$

21 H30

$P_{\text{dy}} = 96$

$H_{\text{res}} = H - 334 \text{ mm}$

$P_{\text{dyke}} = 932.2$

$P_{\text{unnel}} = 990.7/8$

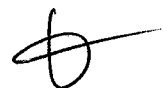
$P_2 = 992.3/4$

$P_3 = 990.7/8$

$T 23^\circ\text{C}$

21 H35

13.12.2000



re 1/15/2002

21455

P <sub>1</sub>	991.1/2
P <sub>2</sub>	992.5/6
P <sub>3</sub>	990.9/991
T	23°C

13.12.2000



re 1/15/2002

P <sub>1</sub>	996.7/6
P <sub>2</sub>	998.1/0
P <sub>3</sub>	996.5/6
T	23

10H05

DG812

$h_{res} = H-335$

$h_{dy} = 94$

250 FPS

Nic  $\Delta t = 40 \mu s$

Prebig 209.675 ml

Payke 938.9/939.0  $\Rightarrow \Delta P = 60$

10H20

$\hookrightarrow \Delta P \approx 70$

P <sub>1</sub>	925.5/4
P <sub>2</sub>	998.2/1
P <sub>3</sub>	996.5/6/5
T	23

~~07.03.02~~

14.12.2000



DG8 15-13

$$\left\{ \begin{array}{l} P_1 = 995.9 / 996.0 \\ P_2 = 997.4 / 5 \\ P_3 = 995.7 / 8 \\ T = 23 \end{array} \right.$$

11H20

$$h_{dyk} = 98 \text{ mm} \quad \underline{1}$$

$$H_{res} = h = 334$$

$$p_{dyke} = 990.4 / 5 \Rightarrow H_{res} = h = 379$$

$$\left\{ \begin{array}{l} P_1 \quad 594.7 / 5 \quad 07.03.02 \\ P_2 \quad 997.2 / 3 \\ P_3 \quad 995.5 / 6 \\ T \quad 23 \end{array} \right.$$

11H25

11H30

$$\left\{ \begin{array}{l} P_1 \quad 995.6 / 7 \\ P_2 \quad 997.2 / 1 \\ P_3 \quad 995.4 / 5 \\ T \quad 23 \end{array} \right.$$

1000 / 2500

14.12.2000



Expt DG815-14

$$\Delta P \approx 800$$

2000 FPS

$$\Delta t_{vic} = 1 \mu s$$

$$12H10 \left\{ \begin{array}{l} P_1 = 995.0/1 \\ P_2 = 996.5/6 \\ P_3 = 994.6/7 \\ T = 23.5 \\ h_{dy} = 95 \text{ mm} \end{array} \right.$$

$$h_{Res} = H - 334 \text{ mm}$$

$$1 \rightarrow \left\{ \begin{array}{l} h_{dyke} = 939.5/6 \\ h_R = H - 376 \text{ mm} \end{array} \right.$$

$$12H15 \left\{ \begin{array}{l} P_1 = 994.3/2 \\ P_2 = 996.5/6 \\ P_3 = 994.6 \\ T = 24 \end{array} \right.$$

$$12H25 \left\{ \begin{array}{l} P_1 = 994.8/ \\ P_2 = 996.4 \\ P_3 = 994.5/4 \\ T = 24 \end{array} \right.$$

14.12.2000

Expl DGSIS-15

$\Delta P_a 700$

$$13H20 \left\{ \begin{array}{l} P_1 = 993.8/9 \\ P_2 = 995.6/7 \\ P_3 = 993.4 \\ T = 24 \\ h_{dy} = 93 \text{ mm} \\ W = h - 336 \\ \text{res} \end{array} \right.$$

1000 FT28

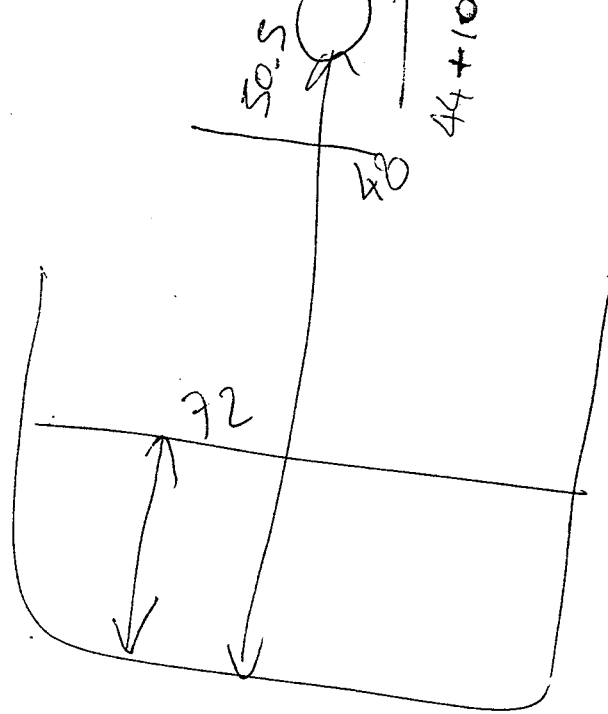
1  $\mu$ sec

$$L \rightarrow \left\{ \begin{array}{l} P_{dyke} = 935.2/3 \\ W_{res} = h - 379 \end{array} \right.$$

$$13H27 \left\{ \begin{array}{l} P_1 = 992.8/11 \\ P_2 = 995.7/8 \\ P_3 = 993.5/6 \\ T = 24 \end{array} \right. \quad 07.03.02$$

14.12.2000

re 1/15/2002



(9) H35

$P_1 = 994.6$
$P_2 = 995.6/7$
$P_3 = 994.6/7$
$T = 21.5^\circ\text{C}$

8-5150

6-5150

6-5150 7

14.12.2000

Expt DG815-16

1/15/2002

2ms  
1000 FPS

1A50  
07.03.02

$$\left\{ \begin{array}{l} P_1 = 993.6/7 \\ P_2 = 995.1/2 \\ P_3 = 993.3/4 \\ T = 23.5^\circ\text{C} \\ h_{dy} = 89 \text{ mm} \\ h_{res} = H - 339 \text{ mm} \end{array} \right.$$

1A55

$$\left\{ \begin{array}{l} P_{dyke} = 937.4 \\ h_{res} = H - 381 \end{array} \right.$$

$$\left\{ \begin{array}{l} P_1 = 993.4/83 \quad 07.03.02 \\ P_2 = 995.1/0 \\ P_3 = 993.3 \\ T = 23.5^\circ\text{C} \end{array} \right.$$

07.03.02

14.12.2000

6

RE

1/15/2002

EXP-DGS15-17

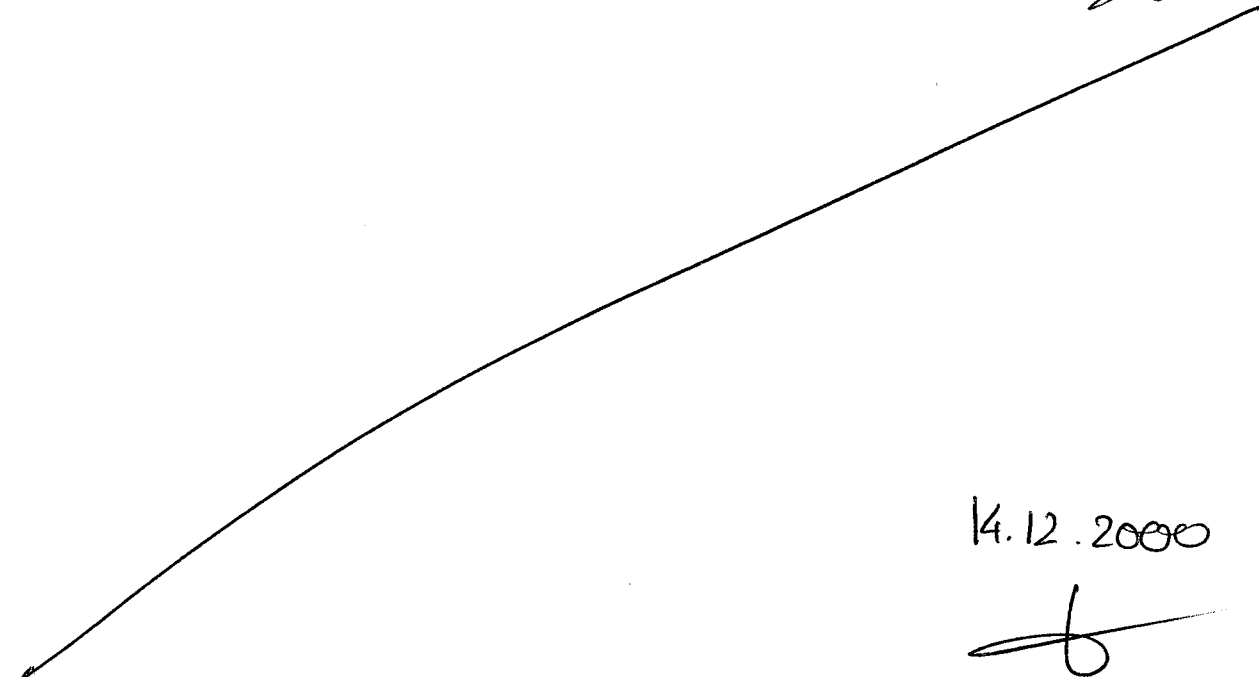
$\left\{ \begin{array}{l} p_1 = 993.3/4 \\ p_2 = 994.7/8 \\ p_3 = 993.1/0 \\ T. \end{array} \right. \quad \begin{array}{l} h_{dy} = 87.5 \text{ mm} \\ h_{Res} = M-340 \\ 23^\circ C \end{array}$

$p_{dy} / x_0 = 935.2/3$  M-385

1000 FRS

less

Tunnel 99.2 / 81  
14.12.00



14.12.2000

*[Signature]*

DGS 15-18

18-12-2000

Insert mol isz place at the top of the cell

At 14H11

$$P_1 = 993.2/3 \text{ mbar}$$

$$P_2 = 995.0/1 \text{ mbar}$$

$$P_3 = 993.0/1 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

$$H_{res} = H - 339 = 146 \text{ mm}$$

$$h_{dyke} = 90 \text{ mm} \Rightarrow 160 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 1 \mu\text{s}$$

$$\text{Trigger position} = \text{prebig } 1\%$$

High-speed video 1000 FPS

At 14H15, DGS 15 pumped up the cell

$$P_{dyke} = 937.7/8 \text{ mbar}$$

$$H_{res} = H - 380 = 105 \text{ mm}$$

At 14H20,

$$P_1 = 993.8/9 \text{ mbar}$$

$$P_2 = 995.1/2 \text{ mbar}$$

$$P_3 = 993.0/1 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

At 14H25, once expt is finished

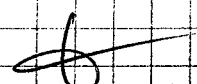
$$P_1 = 993.3/4 \text{ mbar}$$

$$P_2 = 995.1/2 \text{ mbar}$$

$$P_3 = 993.1 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

18-12-2000



re 1/15/2002

DG 515-19

18-12-2000

insert mol in place at the top of the cell

At 15H04

$$P_1 = 993.8/9 \text{ mbar}$$

$$P_2 = 995.5/6 \text{ mbar}$$

$$P_3 = 993.5/6 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

$$H_{\text{res}} = H - 342 = 143 \text{ mm}$$

$$h_{\text{dyke}} = 87 \text{ mm} \Rightarrow 157 \text{ mm}$$

At 15H06, DG 515 pumped up the cell

$$P_{\text{dyke}} = 937.3/4 \text{ mbar}$$

$$H_{\text{res}} = H - 383.5 = 101.5 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 1 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 1000 FPS

At 15H12

$$P_1 = 108.8 \text{ to } 109.1 \text{ mbar (lowest achievable pressure)}$$

$$P_2 = 995.6/7 \text{ mbar}$$

$$P_3 = 993.6/7 \text{ mbar}$$

$$T = 24.0^\circ\text{C}$$

At 16H00

$$P_1 = 994.6/7 \text{ mbar}$$

$$P_2 = 996.2/3 \text{ mbar}$$

$$P_3 = 994.3/4 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

Transducer  $P_2$  didn't record any signal  $\Rightarrow$  use cable 8 for the next run

18.12.2000

18-12-2000

Insert mol in place at the top of the cell

Note: transducer  $P_2$  recorded on channel 2 (1B) but used cable 8 (problem during the previous exp either with  $P_2$  itself or with cable 2)

At 16H09

$$\begin{array}{l} P_1 = 994.7/8 \text{ mbar} \\ P_2 = 996.2/3/4 \text{ mbar} \\ P_3 = 994.4/5 \text{ mbar} \\ T = 23.0^\circ\text{C} \\ H_{\text{res}} = H - 944 = 141 \text{ mm} \\ h_{\text{dyke}} = 85 \text{ mm} \Rightarrow 155 \text{ mm} \end{array}$$

Nicolet

$$\begin{array}{l} \text{Time/pt} = 1 \mu\text{s} \\ \text{Trigger position} = \text{pretrig } 1\% \end{array}$$

High-speed video 1000 FPS

At 16H11, DGS15 pumped up the cell

$$\begin{array}{l} P_{\text{dyke}} = 936.9/937.0 \text{ mbar} \\ H_{\text{res}} = H - 387 = 98 \text{ mm} \end{array}$$

At 16H15,

$$\begin{array}{l} P_1 = 992.3/4/5 \text{ mbar} \\ P_2 = 996.4/5/6 \text{ mbar} \\ P_3 = 994.6/7 \text{ mbar} \\ T = 23.5^\circ\text{C} \end{array}$$

At 16H45

$$\begin{array}{l} P_1 = 995.3/4 \text{ mbar} \\ P_2 = 996.9/997.0 \text{ mbar} \\ P_3 = 995.1/2 \text{ mbar} \\ T = 23.0^\circ\text{C} \end{array}$$

18.12.2000



re 1/15/2002

DS 515-21

18-12-2000

Insert no 1 in place at the top of the cell

At 17H02

$$\begin{aligned} P_1 &= 995.6/7 \text{ mbar} \\ P_2 &= 997.2/3 \text{ mbar} \\ P_3 &= 995.4/5 \text{ mbar} \\ T &= 23.5^\circ\text{C} \\ H_{\text{res}} &= H - 342 = 143 \text{ mm} \\ h_{\text{dyke}} &= 88 \text{ mm} \Rightarrow 158 \text{ mm} \end{aligned}$$

Nicoleh

$$\begin{aligned} \text{Time /pt} &= 5 \mu\text{s} \\ \text{Trigger position} &= \text{pretrig 1\%} \end{aligned}$$

High-speed video 1000 FPS

DS815 Pumped up the cell

$$\begin{aligned} P_{\text{dyke}} &= 939.0/1 \text{ mbar} \\ H_{\text{res}} &= H - 388 = 97 \text{ mm} \end{aligned}$$

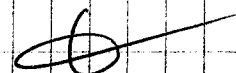
At 17H07

$$\begin{aligned} P_1 &= 694.9/695.0 \text{ mbar} \\ P_2 &= 997.3/4 \text{ mbar} \\ P_3 &= 995.6/7 \text{ mbar} \\ T &= 23.5^\circ\text{C} \end{aligned}$$

At 17H15

$$\begin{aligned} P_1 &= 996.0 \text{ mbar} \\ P_2 &= 997.5/6 \text{ mbar} \\ P_3 &= 995.7/8 \text{ mbar} \\ T &= 23.0^\circ\text{C} \end{aligned}$$

18.12.2000



18-12-2000

Insert n° 1 in place at the top of the cell

At 17H38

$$P_1 = 996.3/4 \text{ mbar}$$

$$P_2 = 997.9 \text{ mbar}$$

$$P_3 = 996.2/3 \text{ mbar}$$

$$T = 22.5^\circ\text{C}$$

$$H_{\text{res}} = H - 343 = 142 \text{ mm}$$

$$h_{\text{dyke}} = 86.5 \text{ mm} \Rightarrow 156.5 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 5 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 500 FPS

DGS15 pumped up the cell

$$P_{\text{dyke}} = 938.8 \text{ mbar}$$

$$H_{\text{res}} = H - 385 = 100 \text{ mm}$$

At 17H43

$$P_1 = 895.2/3/4 \text{ mbar}$$

$$P_2 = 997.9/998.0 \text{ mbar}$$

$$P_3 = 996.3/4 \text{ mbar}$$

$$T = 22.5^\circ\text{C}$$

leak from the gate (see on the video)

At 17H45

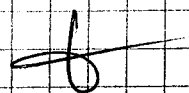
$$P_1 = 996.4/5 \text{ mbar}$$

$$P_2 = 998.0/1 \text{ mbar}$$

$$P_3 = 996.3/4 \text{ mbar}$$

$$T = 22.5^\circ\text{C}$$

18.12.2000



RE 1/15/2002

18-12-2000

Present mo 1 in place at the top of the cell

At 18H20

$$P_1 = 997.4/5 \text{ mbar}$$

$$P_2 = 998.9 \text{ mbar}$$

$$P_3 = 997.2/3 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

$$H_{\text{res}} = H - 343 = 142 \text{ mm}$$

$$h_{\text{dyke}} = 86.5 \text{ mm} \Rightarrow 156.5 \text{ mm}$$

Kicohet

$$\text{Time}/\text{pt} = 50 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 250 FPS

DGS15 pumped up the cell

$$P_{\text{dyke}} = 938.9/939.0 \text{ mbar}$$

$$H_{\text{res}} = H - 385 = 100 \text{ mm}$$

At 18H27

$$P_1 = 996.3/4 \text{ mbar}$$

$$P_2 = 999.2/3 \text{ mbar}$$

$$P_3 = 997.5/6 \text{ mbar}$$

$$T = 23.0^\circ\text{C}$$

Leak on the gate

At 18H34

$$P_1 = 997.9/998.0 \text{ mbar}$$

$$P_2 = 999.4/5 \text{ mbar}$$

$$P_3 = 997.7/8 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

18.12.2000



18-12-2000

Insert no 1 in place at the top of the cell

At 18H48

$$\begin{aligned} P_1 &= 998.2/3 \text{ mbar} \\ P_2 &= 999.8/9 \text{ mbar} \\ P_3 &= 998.0/1 \text{ mbar} \\ T &= 23.5^\circ\text{C} \\ H_{\text{res}} &= H - 343 = 142 \text{ mm} \\ h_{\text{dyke}} &= 86.5 \text{ mm} \Rightarrow 156.5 \text{ mm} \end{aligned}$$

Nicolet

$$\begin{aligned} \text{Time / pt} &= 10 \mu\text{s} \\ \text{Trigger position} &= \text{pretrigger 1\%} \end{aligned}$$

High-speed video 500 FPS

At 18H54, DGS15 pumped up the dike

$$\begin{aligned} P_{\text{dyke}} &= 942.5 \text{ mbar} \\ H_{\text{res}} &= H - 385.5 = 99.5 \text{ mm} \end{aligned}$$

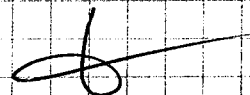
At 18H59

$$\begin{aligned} P_1 &= 797.0/1 \text{ mbar} \\ P_2 &= 1000.0 \text{ mbar} \\ P_3 &= 998.3/4 \text{ mbar} \\ T &= 23.5^\circ\text{C} \end{aligned}$$

At 19H19

$$\begin{aligned} P_1 &= 999.0/1 \text{ mbar} \\ P_2 &= 1000.0 \text{ mbar} \\ P_3 &= 998.8/9 \text{ mbar} \\ T &= 23.5^\circ\text{C} \end{aligned}$$

18.12.2000



re 1/15/2002

DGS15-20

18-12-2000

Insert mol in place at the top of the cell

At 19H20

$$P_1 = 999.1/2 \text{ mbar}$$

$$P_2 = 1000.0 \text{ mbar}$$

$$P_3 = 998.9 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

$$H_{\text{res}} = H - 344 = 141 \text{ mm}$$

$$h_{\text{dyke}} = 86 \text{ mm} \Rightarrow 156 \text{ mm}$$

Nicolet

$$\text{Time/pt} = 5 \mu\text{s}$$

$$\text{Trigger position} = \text{pretrigger } 1\%$$

High-speed video 500 FPS

Run the experiment with cell not filled up :  $h_{\text{dyke}} = 86 \text{ mm}$   
and compare with experiment DGS15-20  $\Rightarrow 156 \text{ mm}$

At 19H25

$$P_1 = 997.7/8 \text{ mbar}$$

$$P_2 = 1000.0 \text{ mbar}$$

$$P_3 = 998.9/999.0 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

$$h_{\text{dyke}} = 86 \text{ mm} \Rightarrow 156 \text{ mm}$$

At 19H30

$$P_1 = 999.3/4 \text{ mbar}$$

$$P_2 = 1000.0 \text{ mbar}$$

$$P_3 = 999.0/1 \text{ mbar}$$

$$T = 23.5^\circ\text{C}$$

18.12.2000



D 5815-26

19-12-00

Dyke not filled to top

$\Delta P = 300 \text{ mbar}$   
500 FPS  
5ms

W. 445

$P_1$	1001.0
$P_2$	1001.0 / 1000.0
$P_3$	1001.0
$h_{dy}$	84.5
$H_{res} = h -$	345.5
$T$	21°C

10/4/01

$P_1$	=	700. <del>415</del> <sup>0703.02</sup> 2/1/3
$P_2$	=	1001/1002
$P_3$	=	1001
$T$	=	21

2200  
2200  
2200

$P_1 = 1001$   
 $P_2 = 1002 / 1001$   
 $P_3 = 1001$

19-12-2000

320

1/15/2002

DG815-27

19-12-00

$$\Delta P = 700$$

1000 FPS

1  $\mu$ sP<sub>1</sub> 1000P<sub>2</sub> 1002P<sub>3</sub> 1000h<sub>dy</sub> 84.5H<sub>res</sub> = h - 34.5

T 24

dyke not filled to top

P<sub>1</sub> 300. 1/2 07.03.02P<sub>2</sub> 1002P<sub>3</sub> 1000

T 24°C

P<sub>1</sub> ~~900~~ 1000P<sub>2</sub> 1002P<sub>3</sub> 1000

T 24

19.12.2000

DGS 15-28

19-12-00

$\Delta P = 100 \text{ mbar}$

~~1250~~ ~~18~~ ~~425~~ 30 FPS

250  $\mu\text{s}$  07.03.02

$\sqrt{P_1}$  999.2/3

$P_2$  1000.0

$P_3$  999.2/3

T 23.5

$h_{dy}$  85 mm

$M_{res} = h - 345$

dike not filled up  
to top

12450  $\left[ \begin{array}{l} P_1 \text{ 999.1/10 } 07.03.02 \\ P_2 \text{ 1001.0/1000.0} \\ P_3 \text{ 999.1/2} \\ T \text{ 24}^\circ\text{C} \end{array} \right.$

$\Rightarrow$  decided  
to change  
FPS and



327 no  
1/15/2002

$P_1$  899.2 / 3  
 $P_2$  1000.0  
 $P_3$  999.0 / 998.9  
 $T$  24°C  
 $\mu_y = 85.5$

$P_1$  up to 970 initially decreasing  
 $P_1$  recorded vocally on small video

$\rightarrow$  897.2 / 3 when transect filled

13420  
 $P_1 = 998.3/4$   
 $P_2 = 999.9$   
 $P_3 = 998.2$   
 $T = 23$

1000  
 (600)

19.12.2000



DGS 15-29

A-12-00

$$\Delta P = 860$$

1000 FPS

2 u

P<sub>1</sub> 998.3/4P<sub>2</sub> 999.8/9P<sub>3</sub> 998.1/2

T=23

h<sub>dy</sub> 84h<sub>res</sub> = H-346dike not  
filled to  
topminimum P<sub>tunnel</sub> readable 128 mbargo for  
↳  $\Delta P = 860$  mbar

07.03.02

P<sub>1</sub> 123.0P<sub>2</sub> 998.6P<sub>3</sub> 998.0 / 997.9 382

T 23.5

P<sub>1</sub> 997.7/8P<sub>2</sub> 999.1/2P<sub>3</sub> 997.5/6

T 23

19.12.2000

324 re  
1/15/2002

DG815-30

19-12-00

$\Delta P = 400$   
500 FPS  
5  $\mu$ s

P<sub>1</sub> 997.0/1

P<sub>2</sub> 998.5/4

P<sub>3</sub> 996.9/8

T 23

h<sub>du</sub> 84.5

h<sub>res</sub> = h - 346

dike not filled to top

14H19

P<sub>1</sub> 995.2/3

P<sub>2</sub> 998.5/6/4

P<sub>3</sub> 996.9

T 23

14H40

P<sub>1</sub> 996.7/8

P<sub>2</sub> 998.2/3/1

P<sub>3</sub> 996.6/5

T 23.5

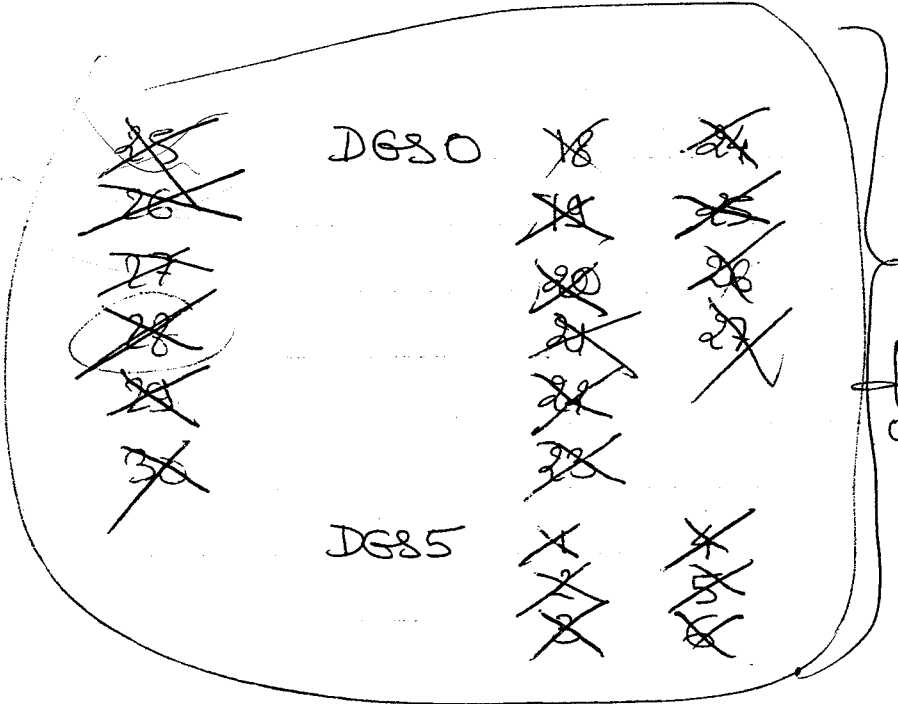
19.12.2000

1/15/2002

re

CD

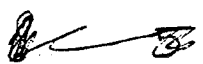
DG815 {  
~~18~~  
~~19~~  
~~20~~  
~~21~~  
~~22~~  
~~23~~  
~~24~~  
 07.03.02



ASG

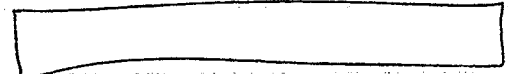
{ tunnel AN 008463 SN 0050000 334 (Dec 04, 00)  
 dike AN 008466 SN 0050000 371 (Dec 06, 00)  
 reservoir AN 008464 SN 0050000 333 (Dec 04, 00)

insert glass plate thickness 6.5 mm  
 length 45.5 cm  
 width 19.65 cm



{ 80 280  
 133.5 330  
 188 380  
 229 430

Positions of  
 P transducers  
 (retires 30 mm)

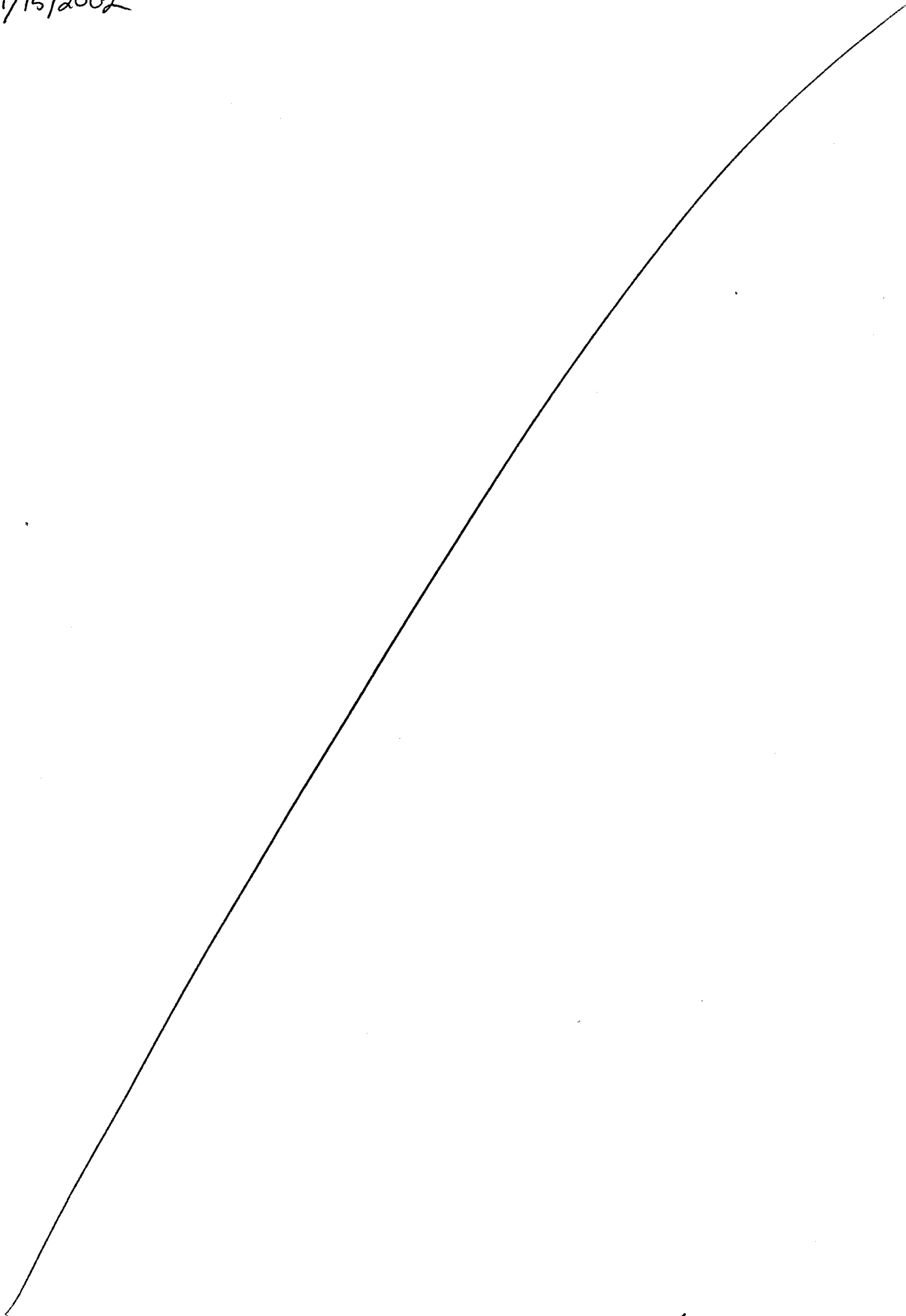


from tube cut

19.12.2000

{ 28  
 29

2014  
re 1/15/2002



19.12.2000

A handwritten signature, possibly reading 'J. J. J.', written in black ink.

327  
re 1/15/00:

I have reviewed scientific notebook 371 and find it in compliance with QAP-001. There is sufficient information regarding procedure used for conducting the research and acquiring and analyzing the data so that another qualified scientist could repeat the activity or activities recorded in this scientific notebook.

H. Lawrence McKague 1/15/02

H. Lawrence McKague  
GLGP Element Manager

H. Lawrence McKague

RE 1/15/2002

~~RYM c  
1/15/02~~