

# LABORATORY NOTEBOOK

CNWRA/SwRI

308  
Scientific Notebook #305  
Q200005230005

**NOTEBOOK NO.** \_\_\_\_\_  
**ISSUED TO** \_\_\_\_\_  
**ON** \_\_\_\_\_ **19** \_\_\_\_\_  
**DEPARTMENT** \_\_\_\_\_  
**RETURNED** \_\_\_\_\_ **19** \_\_\_\_\_

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## INSTRUCTIONS

1. **The primary purpose of this notebook is to protect your and the Company's Patent-Rights by keeping records of all original work in a form acceptable as evidence if any legal conflict arises.**
2.
  - When starting a page, enter the title, project number, and book number.
  - Use ink for permanence -- avoid pencil.
  - Record your work as you progress, including any spur-of-the-moment ideas which may be developed later.
  - Avoid making notes on loose paper to be recycled.
  - Record your work in such a manner that a co-worker can continue from where you stop. You might be ill and to protect your priority it could be urgent that the work continue while you are absent.
3.
  - Give a complete account of your experiments and the results, both positive and negative, including your observations.
  - Record all diagrams, layouts, plans, procedures, new ideas, or anything pertinent to your work including the details of any discussions with suppliers, or other people outside the Company.
  - Do not try to erase any incorrect entries; draw lines deleting them, note the corrections, sign and date the changes. This extra care is worthwhile because of the necessity of original data to prove priority of new discoveries.
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  - After entering your data, sign and date the entries.
  - Explain your work to at least two witnesses who are not co-inventors, and have them sign and date the pages in the place provided.
  - Record the names of operators and witnesses present during any demonstration and have at least two witnesses sign the page. If no witnesses are present during an experiment of importance, repeat it in the presence of two witnesses.
5. Since computer programs can be patented these instructions apply to the development of computer software. In this case a description of the structure and operation of the program should be recorded in the notebook, together with a basic flow diagram which illustrates the essential features of the program. In the course of developing the code, the number of lines of code written each day should be recorded in the notebook, together with a statement of the portion of the flow diagram to which the section of code is directed.
6. This notebook and its contents are the exclusive property of the Company. It is confidential and the contents are not to be disclosed to anyone unless authorized by the Company. You must return it when completed, upon request, or upon termination of employment. It should be kept in a protected place.  
**If loss occurs, notify your supervisor immediately, and make a written report describing the circumstances of the loss.**

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This Notebook is a continuation of the work recorded in Notebook 284

<sup>ECP 8/24/00</sup> <sup>ECP 8/24/00</sup> <sup>ECP 8/24/00</sup>  
 This work ~~has~~ ~~had~~ ~~is~~ has evolved from thermal hydrological modeling of the drift scale - (top of mountain to water table) into coupled geothermal thermal hydrological modeling of mountain drift scale to drift scale water test

Along the way, benchmark comparisons are being done by Lauren Browning and Bill Murphy using the equilibrium code EQ3/6

I'm using multiFlo in the coupled METRA GEM and GEM standalone mode.

I refer to multiFlo 1.2B as either multiFlo or mf and I refer to the version of multiFlo which implements the operator splitting time integration ~~also~~ algorithm as <sup>ECP 8/24/00</sup>

MultiFlo X

The executables are located at

~ spainter/bin/multiFlo and

~ spainter/dhughson/multiFlo X

→ Putting my initials AND today's DATE (18 months after <sup>Some</sup> the fact) makes this better. ECP 8/24/2000

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check on the effect of time integration in GEM. maximum difference between multiFlo and EQ3/6 for the time dependent heating box is about 8% for  $\text{CO}_3^{2-}$ . Refer to page 94 in notebook 284.

With multiFloX at time 349.9 yr,  $T = 87.42^\circ\text{C}$   $P = 7.4957 \times 10^7 \text{ Pa}$

Component	$S = 1 \text{ cm}^{-1}$ multiFloX (1)	$S = 10 \text{ cm}^{-1}$ (2)	$S = 100 \text{ cm}^{-1}$ (3)
$\text{Cl}^-$	$1.8968 \times 10^{-3}$	$1.8972 \times 10^{-3}$	$1.8968 \times 10^{-3}$
$\text{Ca}^{2+}$	$1.8785 \times 10^{-3}$	$1.0141 \times 10^{-5}$	$1.8814 \times 10^{-3}$
$\text{H}^+$	$2.9208 \times 10^{-7}$	$2.0951 \times 10^{-9}$	$2.9251 \times 10^{-7}$
$\text{CO}_2(\text{aq})$	$1.0137 \times 10^{-3}$	$9.1547 \times 10^{-6}$	$1.0152 \times 10^{-3}$
$\text{SiO}_2(\text{aq})$	$5.6337 \times 10^{-3}$	$5.6337 \times 10^{-3}$	$5.6337 \times 10^{-3}$
$\text{OH}^-$	$1.3446 \times 10^{-6}$	$1.7866 \times 10^{-4}$	$1.3427 \times 10^{-6}$
$\text{HCO}_3^-$	$1.8578 \times 10^{-3}$	$2.2304 \times 10^{-3}$	$1.8578 \times 10^{-3}$
$\text{CO}_3^{2-}$	$7.0798 \times 10^{-7}$	$1.0740 \times 10^{-4}$	$7.0708 \times 10^{-7}$
$\text{CaCO}_3(\text{aq})$	$6.9689 \times 10^{-6}$	$6.9688 \times 10^{-6}$	$6.9689 \times 10^{-6}$

① maximum timestep in masin.inp set to 100 years  
Time step ~~is~~ at 349 years is  $0.1656$  years in metra and  $6.82 \times 10^{-2}$  to  $9.743 \times 10^{-2}$  yr in GEM

→ Change max dt in masin.inp to 1.0 years  
Time step at 349 years is  $0.1656$  years in metra and  $3.219 \times 10^{-2}$  to  $5.292 \times 10^{-2}$  years in GEM  
concentrations at  $t = 349.9$  yr are identical.

→ change maxdt to 0.1 GEM time step  $6.614 \times 10^{-3}$  years exactly the same concentrations again

② change  $S$  from  $1/\text{cm}$  to  $10/\text{cm}$  } specific mineral surface area  $\text{cm}^2/\text{cm}^3$   
③ change  $S$  from  $10/\text{cm}$  to  $100/\text{cm}$

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Component	④ $S = 1000 \text{ cm}^{-1}$	⑤ $S = 10^4 \text{ cm}^{-1}$
$\text{Cl}^-$	$1.8968 \times 10^{-3}$	$1.8968 \times 10^{-3}$
$\text{Ca}^{2+}$	$2.9331 \times 10^{-3}$	$3.2866 \times 10^{-3}$
$\text{H}^+$	$4.9108 \times 10^{-7}$	$4.9375 \times 10^{-7}$
$\text{CO}_2(\text{aq})$	$1.8850 \times 10^{-3}$	$1.7118 \times 10^{-3}$
$\text{SiO}_2(\text{aq})$	$5.6337 \times 10^{-3}$	$5.6337 \times 10^{-3}$
$\text{OH}^-$	$8.1851 \times 10^{-7}$	$8.1864 \times 10^{-7}$
$\text{HCO}_3^-$	$2.1024 \times 10^{-3}$	$1.9093 \times 10^{-3}$
$\text{CO}_3^{2-}$	$4.9989 \times 10^{-7}$	$4.5678 \times 10^{-7}$
$\text{CaCO}_3(\text{aq})$	$6.9869 \times 10^{-6}$	$6.9689 \times 10^{-6}$

MultiFloX definitely Buggy

Does the same thing happen with multiFlo 1.2/3 ?

Comp	$S = 1 \text{ cm}^{-1}$	$S = 10 \text{ cm}^{-1}$	$S = 100 \text{ cm}^{-1}$	$S = 10^3 \text{ cm}^{-1}$
$\text{Cl}^-$	$1.8968 \times 10^{-3}$	SAME	SAME	$1.8968 \times 10^{-3}$
$\text{Ca}^{2+}$	$1.8785 \times 10^{-3}$	SAME	SAME	$1.8786 \times 10^{-3}$
$\text{H}^+$	$2.9208 \times 10^{-7}$	SAME	"	$2.9210 \times 10^{-7}$
$\text{CO}_2(\text{aq})$	$1.0137 \times 10^{-3}$	SAME	"	$1.0138 \times 10^{-3}$
$\text{SiO}_2(\text{aq})$	$5.6337 \times 10^{-3}$	SAME	"	$5.6337 \times 10^{-3}$
$\text{OH}^-$	$1.3446 \times 10^{-6}$	SAME	"	$1.3445 \times 10^{-6}$
$\text{HCO}_3^-$	$1.8578 \times 10^{-3}$	SAME	"	same
$\text{CO}_3^{2-}$	$7.0798 \times 10^{-7}$	SAME	"	$7.0796 \times 10^{-7}$
$\text{CaCO}_3(\text{aq})$	$6.9689 \times 10^{-6}$	SAME	"	$6.9688 \times 10^{-6}$

→ metra dt = 0.1657 yr GEM dt =  $7.787 \times 10^{-2}$  yr

Comp  
 $\text{Cl}^-$  SAME  
 $\text{Ca}^{2+}$  SAME  
 $\text{H}^+$  SAME  
 $\text{CO}_2(\text{aq})$  SAME  
 $\text{SiO}_2(\text{aq})$  SAME  
 $\text{OH}^-$  SAME  
 $\text{HCO}_3^-$  SAME  
 $\text{CO}_3^{2-}$  SAME  
 $\text{CaCO}_3(\text{aq})$  SAME

This with metra dt = 0.1656 years  
gem dt =  $6.6140 \times 10^{-4}$  years

Difference between multiFlo and EQ3/6 does not appear to be a time integration problem

Still need to look at activity coefficients and thermodynamic data base

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With  
 $S = 10 \text{ cm}^{-1}$   $OT(NSTP\text{MAX} + 1) = 100$  col (2) pg 2  
 $S = 10 \text{ cm}^{-1}$   $OT(NSTP\text{MAX} + 1) = 10$  col (1) pg 2  $\pm 1 \text{ digit}$   
 $S = 10 \text{ cm}^{-1}$   $OT(NSTP\text{MAX} + 1) = 1$  col (1) pg 2

Results

Reaction kinetics  $n = \frac{W a^*}{\gamma} + (n_0 - \frac{W a^*}{\gamma}) \exp\left(\frac{-K S t}{W a^*}\right)$

$S = \text{mineral surface area } \text{cm}^{-1}$

$K = \text{rate const. moles/cm}^2/\text{s}$

$\gamma = 1$

$W = \text{mass of water Kg}$

$a^* = 10^{-2.72} \text{ moles/Kg}$

$W = 110 \text{ Kg}$   $a^* = 10^{-2.72} \text{ moles/Kg}$

$K = 10^{-11.34} \text{ moles/cm}^2/\text{s}$

$S = (10/\text{cm}) 10^6 \text{ cm}^3$

$\frac{(110 \text{ Kg}) 10^{-2.72} \text{ moles/Kg}}{(10^{-11.34} \text{ moles/cm}^2/\text{s}) (10/\text{cm}) 10^6 \text{ cm}^3} = 4600 \text{ s}$

$= 1.45 \times 10^4 \text{ years}$

with  $S = 10 \text{ cm}^{-1}$

$TSTEP(1) = 1.5e-3 \text{ y}$   $OT(1) = 1.e-8 \text{ y}$   
 $OT(2) = 10 \text{ y}$

Same results as col (1) pg 2

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Change tolc from 0.5 to 1e-10

Relative error on  $\text{Ca}^{+2}$   $\text{H}^+$   $\text{CO}_2(\text{aq})$  changed  
 from about 0.039 EP to 2.57e-2  
 8/24/00

but results are same as pg 2 col (1)

Change tolc from 1e-10 to 1e-15

Relative Error on  $\text{Ca}^{+2}$   $\text{H}^+$   $\text{CO}_2(\text{aq}) \sim 3e-10$   
 but results are still the same as pg 2 col (1)

Begin a series of benchmark runs between  
 MULTIFLO and EQ3/6 to track down the  
 source of the 8% discrepancy from page 94  
 in notebook 284.

First Run Called Bill-25

Isothermal at 25°C

Component	$M(t=10^{16} \text{ yr})$	$M(t=349.9 \text{ y})$
$\text{Cl}^-$	2.2493e-3	SAME
$\text{Ca}^{+2}$	2.5e-3	SAME
$\text{H}^+$	6.7097e-8	SAME
$\text{CO}_2(\text{aq})$	3.4064e-4	SAME
$\text{SiO}_2(\text{aq})$	1.0e-3	1.735e-3
$\text{OH}^-$	1.8075e-7	SAME
$\text{HCO}_3^-$	2.7451e-3	SAME
$\text{CO}_3^{2-}$	2.7492e-6	SAME
$\text{CaCO}_3(\text{aq})$	7.0061e-6	SAME

EP 8/24/00

EQ3

I Am

improving

the

quality of

this work.

EP

8/24/00

repeated  
 following  
 page

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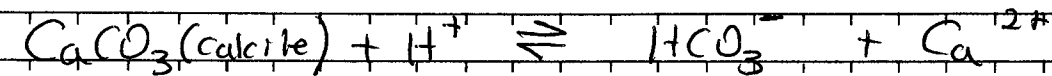
Date

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Comp	MX(t=10 <sup>-6</sup> )	EQ3	% difference
Cl <sup>-</sup>	2.2493e-3	2.2493e-3	0
Ca <sup>2+</sup>	2.5e-3	2.5e-3	0
H <sup>+</sup>	6.7097e-8	6.7097e-8	0
CO <sub>2</sub> (aq)	3.4064e-4	3.4064e-4	0
SiO <sub>2</sub> (aq)	1.0e-3	1.0e-3	0
OH <sup>-</sup>	1.8075e-7	1.7929e-7	.814
HCO <sub>3</sub> <sup>-</sup>	2.7451e-3	2.7289e-3	.594
CO <sub>3</sub> <sup>2-</sup>	2.7492e-6	2.6959e-6	1.977
CaCO <sub>3</sub> (aq)	7.0061e-6	7.0807e-6	-1.054

This is the same pattern of differences as on page 94 of NB # 284

Since Ca<sup>2+</sup> and H<sup>+</sup> are the same, let's look at



For this reaction log K = 1.8487 @ 25 C in both EQ3 and master temp. V8.R5 data bases

MULTIFLOX		EQ3	
$\gamma$	$a$	log a	log $\gamma$
HCO <sub>3</sub> <sup>-</sup>	10 <sup>-2.6009</sup>	-2.6021	-.0381
Ca <sup>2+</sup>	10 <sup>-2.753083</sup>	-2.7556	-.1535
H <sup>+</sup>	10 <sup>-7.20825</sup>	-7.2095	-.0362

$$\frac{a_{\text{HCO}_3^-} a_{\text{Ca}^{2+}}}{a_{\text{H}^+}} = 1.8518$$

$$\frac{10^{-2.6009} \cdot 10^{-2.753083}}{10^{-7.20825}} = 1.854267$$

Neither multiflo nor EQ3 honor the K = 1.8487  
But EQ3 is closer  
0.17% vs. 0.3% in log K  
0.72% vs. 1.3% in K

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Concentrations for Ca<sup>2+</sup> and H<sup>+</sup> are identical in MX and EQ3 yet  $\alpha$  and  $\gamma$  are different.

BDOT  $B = \text{bot parameter}$   $I = \text{ionic strength}$   
 $\log \gamma = \frac{A_\gamma z^2 \sqrt{I}}{1 + \alpha B_\gamma \sqrt{I}} + B I$   $\alpha = \text{hard core diameter}$   
 $A_\gamma = \text{Debye-Hückel } A$   $B_\gamma = \text{Debye-Hückel } B$   
 $z = \text{charge}$

MultiFlo output Parameters @ 25 C  
 $A = 0.5114$   
 $B = 0.3288$   
 $B = 4.1e-2$

For Ca<sup>2+</sup> from the database  $\alpha = 6$

then  $\log \gamma =$  MultiFlo output  $I = 7.5028e-3$

then  $\log \gamma = 0.151636$   $\gamma = 0.705284$

FOR HCO<sub>3</sub><sup>-</sup> from database  $\alpha = 4$

then  $\log \gamma = 0.04007$   $\gamma = 0.911855$

For H<sup>+</sup> from database  $\alpha = 9$

then  $\log \gamma = 0.035567$   $\gamma = 0.92137$

EQ3 @ 25C  $A = 0.5114$   $B = 0.3288$   $B = 0.041$   
 $\alpha$  is the same as above but  $I = 7.489962e-3$

Comp	log $\gamma$	$\gamma$
H <sup>+</sup>	0.035542	0.92142
Ca <sup>2+</sup>	0.151525	0.705465
HCO <sub>3</sub> <sup>-</sup>	0.040043	0.91192

My initials here must mean that I believe the line outs are correctly done. ECP 8/24/00

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From Page No. Concentration and Activity Coefficient Comparison  
MX and EQ3 - Summary

Parameters  $A = 0.5114$   $B = 0.3288$   $\bar{B} = 4.1e-2$

Comp	$\bar{a}$	$\bar{z}$	Are identical in
$\text{Ca}^{++}$	6	2	both codes
$\text{H}^+$	9	1	
$\text{HCO}_3^-$	4	1	

MX				EQ3			
$I = 7.5028e-3$				$I = 7.489962e-3$			
Comp	M	$\gamma(1)$	$\gamma(2)$	M	$\gamma(1)$	$\gamma(2)$	
$\text{HCO}_3^-$	$2.7451e-3$	0.91315	0.911855	$2.7289e-3$	0.9160	0.91192	
$\text{Ca}^{2+}$	$2.5e-3$	0.70628	0.705284	$2.5e-3$	0.7023	0.705465	
$\text{H}^+$	$6.7097e-8$	0.92267	<del>0.92137</del>	$6.7097e-8$	0.9200	0.92142	

$\gamma(1)$  reported by program in output file

$\gamma(2)$  calculated using B-dot formula, parameters reported in output file (same for both), and Ionic strength reported in output file

I can not see one thing wrong but an accumulation of small errors and inconsistencies

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From Page No. Check BOOT Parameters MX and data0.com.R2

MX (mask temp. V8.R5)				EQ3 (data0.com.R2)			
I	A	B	$\bar{B}$	I	A	B	$\bar{B}$
0	.4939	.3253	.0374	0.01	SAME	SAME	.0394
25	.5114	.3288	.041	SAME	SAME	SAME	SAME
60	.5465	.3346	.044	SAME	SAME	SAME	.0438
100	.5995	.3421	.046	SAME	SAME	SAME	SAME
150	.6855	.3525	.047	SAME	SAME	SAME	SAME
200	.7994	.3639	.047	SAME	SAME	SAME	SAME
250	.9593	.3766	.034	SAME	SAME	SAME	SAME
300	1.218	.3925	0	SAME	SAME	SAME	SAME

I found 3 differences in the temperature dependent boot parameters between multiphase and EQ3 database data0.com.R2

After all this I was told I should have been using the EQ6 results

Comp	MX ( $t=10^{-16}$ )	EQ6	% diff	EQ6 (com)
$\text{Cl}^-$	$2.2493e-3$	$2.2493e-3$	0	
$\text{Ca}^{2+}$	$2.5e-3$	$2.4984e-3$	.064	-2.7558
$\text{H}^+$	$6.7097e-8$	$6.7463e-8$	-.52	-7.2072
$\text{CO}_2(\text{aq})$	$3.4064e-4$	$3.4217e-4$	-.45	
$\text{SiO}_2(\text{aq})$	$1.0e-3$			
$\text{OH}^-$	$1.8075e-7$	$1.7828e-7$	1.39	
$\text{HCO}_3^-$	$2.7451e-3$	$2.7259e-3$	.70	-2.6026
$\text{CO}_3^{2-}$	$2.7492e-6$	$2.6780e-6$	2.66	
$\text{CaCO}_3(\text{aq})$	$7.0061e-6$	$7.0307e-6$	-.35	

EQ6  $\frac{A_{\text{HCO}_3^-}}{A_{\text{Ca}^{2+}}} = 1.8488$

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With masin.inp file used previous pages & switch to master 25.V8.R5 database gives runtime FP over flow error. S Parker rearrange primary & secondary species as follows:

Primary	itype	clat	Secondary
$\text{Cl}^-$	-1	$2.5\text{e-}10$	$\text{OH}^-$
$\text{Ca}^{2+}$	7	$2.5\text{e-}3$	$\text{CO}_2(\text{aq})$
$\text{H}^+$	3	$2.5\text{e-}3$ ec	$\text{CO}_3^{2-}$
$\text{HCO}_3^-$	4	$-2.00$ $\text{CO}_2(\text{g})$	$\text{CaCO}_3(\text{aq})$
$\text{SiO}_2(\text{aq})$	7	$1.\text{e-}3$	

With these changes the following results are obtained

Comp	MA	EQ6	%diff
$\text{Cl}^-$	$2.2809\text{e-}3$	$2.2493\text{e-}3$	1.4
$\text{Ca}^{2+}$	$2.50\text{e-}3$	$2.4984\text{e-}3$	0.064
$\text{H}^+$	$6.7183\text{e-}8$	$6.7463\text{e-}8$	-0.415
$\text{HCO}_3^-$	$2.7136\text{e-}3$	$2.7259\text{e-}3$	-0.451
$\text{SiO}_2(\text{aq})$	$1.0\text{e-}3$		
$\text{OH}^-$	$1.7888\text{e-}7$	$1.7828\text{e-}7$	0.34
$\text{CO}_2(\text{aq})$	$3.3970\text{e-}4$	$3.4217\text{e-}4$	-0.72
$\text{CO}_3^{2-}$	$2.6899\text{e-}6$	$2.6780\text{e-}6$	0.44
$\text{CaCO}_3(\text{aq})$	$7.0307\text{e-}6$	$7.0307\text{e-}6$	0

	EQ3	File archive
$\text{Cl}^-$	$2.2493\text{e-}3$	
$\text{Ca}^{2+}$	$2.5\text{e-}3$	~dhughson/multiHo/
$\text{H}^+$	$6.7097\text{e-}8$	inputbak/
$\text{HCO}_3^-$	$2.7289\text{e-}3$	masin.inp.1
$\text{SiO}_2(\text{aq})$	$1.0\text{e-}3$	
$\text{OH}^-$	$1.7929\text{e-}7$	EQ results for
$\text{CO}_2(\text{aq})$	$3.4064\text{e-}4$	Bill 25 taped
$\text{CO}_3^{2-}$	$2.6959\text{e-}6$	on page 12
$\text{CaCO}_3(\text{aq})$	$7.0807\text{e-}6$	

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TITLE

ENFE

From Page No.

Initial Simulation for Drift-Mountain Scale  
Reactive Transport modeling - Yucca mtn site

~dhughson/multiHo/murphy/agu

Simulation results for 1, 10, 100, 1000, & 10000 yrs

Model DCM - 20 hydrostratigraphic layers  
Nevada-State Coordinates  $170716\text{E}$   $170489\text{E}$   
ECP 8/24/00 233748 N  
INSTANT quality! ECP 8/24/1000

Thermal-hydrologic properties same as Tables  
3-18, 3-30, and 3-31 in TSPA-VA TBD

Thermal load equivalent to approx 85 MTU/acre

Primary Aqueous Species Secondary Aqueous Sp.

$\text{Cl}^-$	charge balance	$\text{OH}^-$
$\text{Ca}^{2+}$	Initial conc.	$\text{HCO}_3^-$
$\text{H}^+$	Mineral Constraining	$\text{CO}_3^{2-}$
$\text{CO}_2(\text{aq})$	Gas constraining	$\text{CaCO}_3(\text{aq})$
$\text{SiO}_2(\text{aq})$	Initial Conc.	Gas

Minerals

 $\text{CO}_2(\text{g})$ 

To Do

1. Activity coefficient calculation ok.
2. pH constraint on reaction rate
3. Representative mineralogy with appropriate speciation
4. Heterogeneous chemistry & parameters
5. Comparison with analysis for ambient conditions.
6. Thermal load

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From Page No.

May 7 1999 Hydrology for Lauren's  
geochem model

$$\text{volf of top block} = 6.94e-5$$

$$\text{say } 20 \text{ mm/yr} = 6.33e-7 \text{ kg/m}^2/\text{s}$$

$$\text{So apply } 20 \text{ mm/yr} / \text{volf} = 9.1e-3 \text{ kg/m}^2/\text{s} \text{ to top}$$

200 Ptn 24 and Ch3zc fractures are still dry

200 8/24/00

$$\text{try } 40 \text{ mm/yr} = 1.824e-2 \text{ kg/m}^2/\text{s}$$

Part of Ptn and CH fractures still dry

$$\text{try } 60 \text{ mm/yr} = 2.736e-2 \text{ kg/m}^2/\text{s}$$

$$\text{Still dry, try } 80 \text{ mm/yr} = 3.65e-2$$

still dry

$$\text{All fractures are wet at } 8.5e-2 \text{ kg/m}^2/\text{s} = 186.4 \text{ mm/yr}$$

Mass balance

$$\begin{array}{ll} \text{In fracture} = 4.13e-5 \text{ kg/s} & \text{Out fracture} = -1.351e-8 \text{ kg/s} \\ \text{matrix} = 1.503e-8 \text{ kg/s} & \text{matrix} = -4.13e-5 \text{ kg/s} \\ \hline 4.1315e-5 \text{ kg/s} & 4.1314e-5 \text{ kg/s} \end{array}$$

$$\text{Flux in} = 186.5 \text{ mm/yr} \quad \text{OK}$$

This work in support of

Begun by L. W. M. Murphy, D. L. Hughson - Benchmarking & Calibration of a model for Predicting Reactive Transport at Yucca Mountain Nevada, EOS Transactions, AGU 1999 Spring meeting Vol 80 No 17 April 27, 1999 H.51E-08 p.5155  
It has been completed

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ENFE

From Page No.

This is the beginning of a new Project

An archaeological site at Akrotiri, Greece, as a natural analog for radionuclide transport: Implications for validity of performance assessments.

To be presented at Fall 1999 Meeting of the Materials Research Society Nov 29-Dec 3, 1999

Computer files will be stored in two places

PC O:\documents\akrotiri and  
SUN /home/dhughson/multiflo/murphy/akrotiri

Reference: Murphy, W.M., E.C. Darcy, R.T. Green, J.D. Prikryl, S. Mohanty, B.W. Leslie, A. Nedungadi, A test of long-term predictive geochemical transport modeling at the Akrotiri archaeological site, J. of Cont. Hyd. 29(1998) 245-279

- Reconstruct field data from notebooks & old files
- data visualization & hypothesis formulation
- Construction of alternative conceptual models
- hypothesis testing using alternative conceptual models
- Insights into PA abstraction of Unsaturated zone flow & transport

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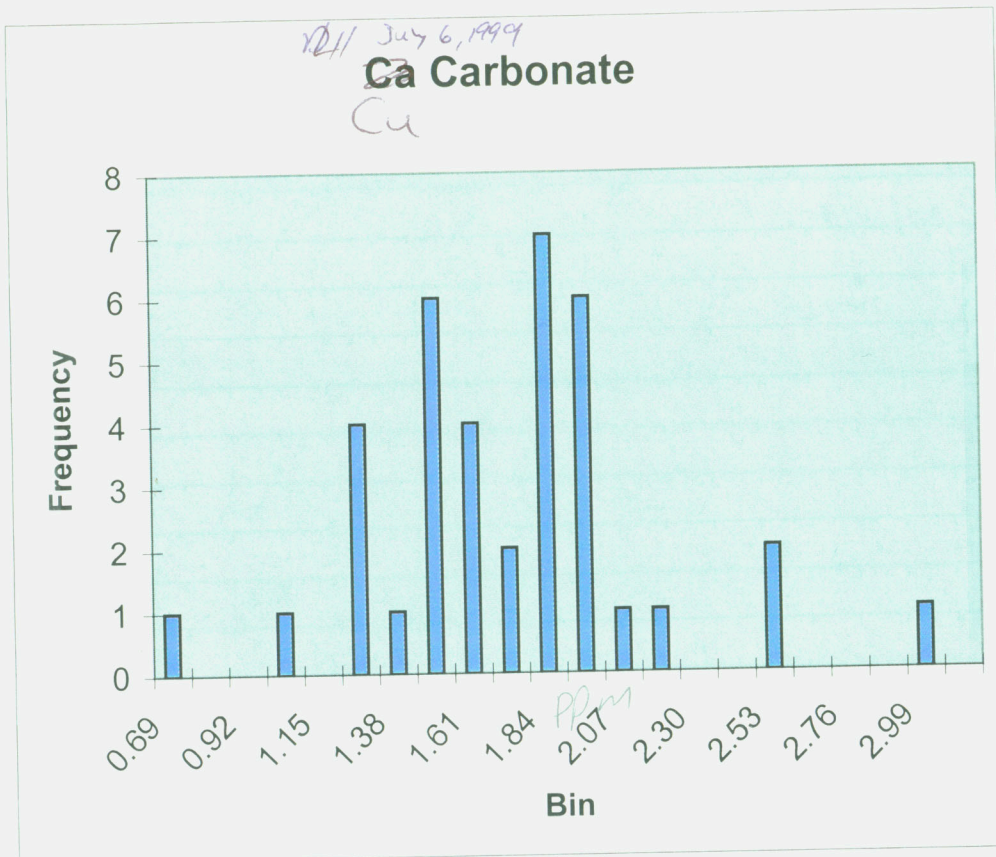
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37 data  $\text{CuCO}_3$

$\mu = 1.67$   
 $\sigma^2 = 0.183$   
 $\sigma = .428$   
 $\min = .69$   
 $\max = 2.99$

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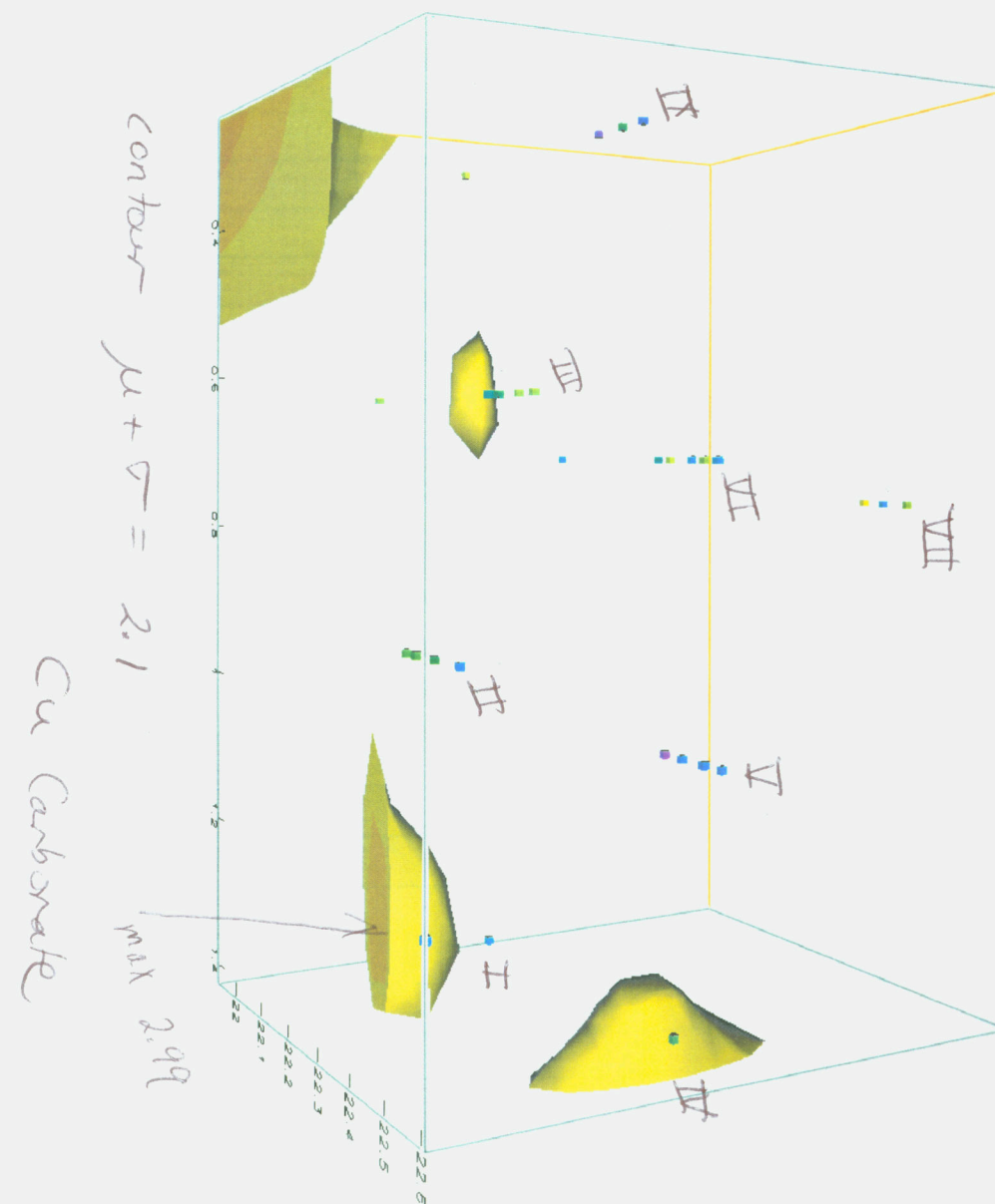
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AKOHH



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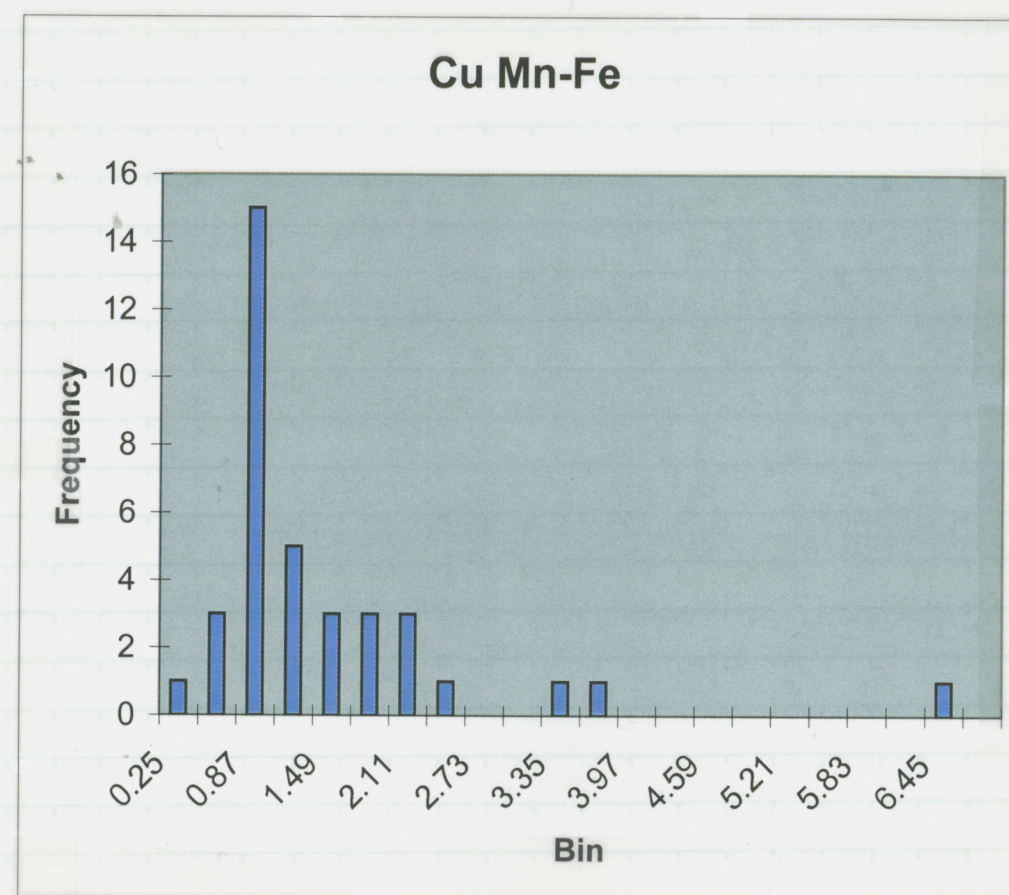
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Akrothri



37 data Cu (ppm, Fe-Mn oxide)

$$\mu = 1.25$$

$$\sigma^2 = 1.27$$

$$\sigma = 1.128$$

$$\min = 0.25$$

$$\max = 6.45$$

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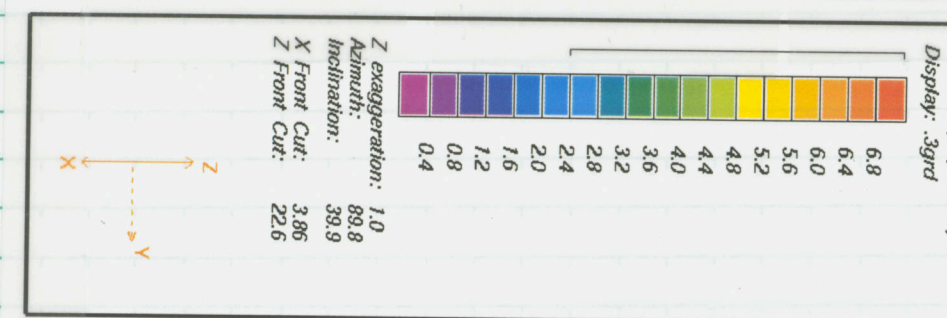
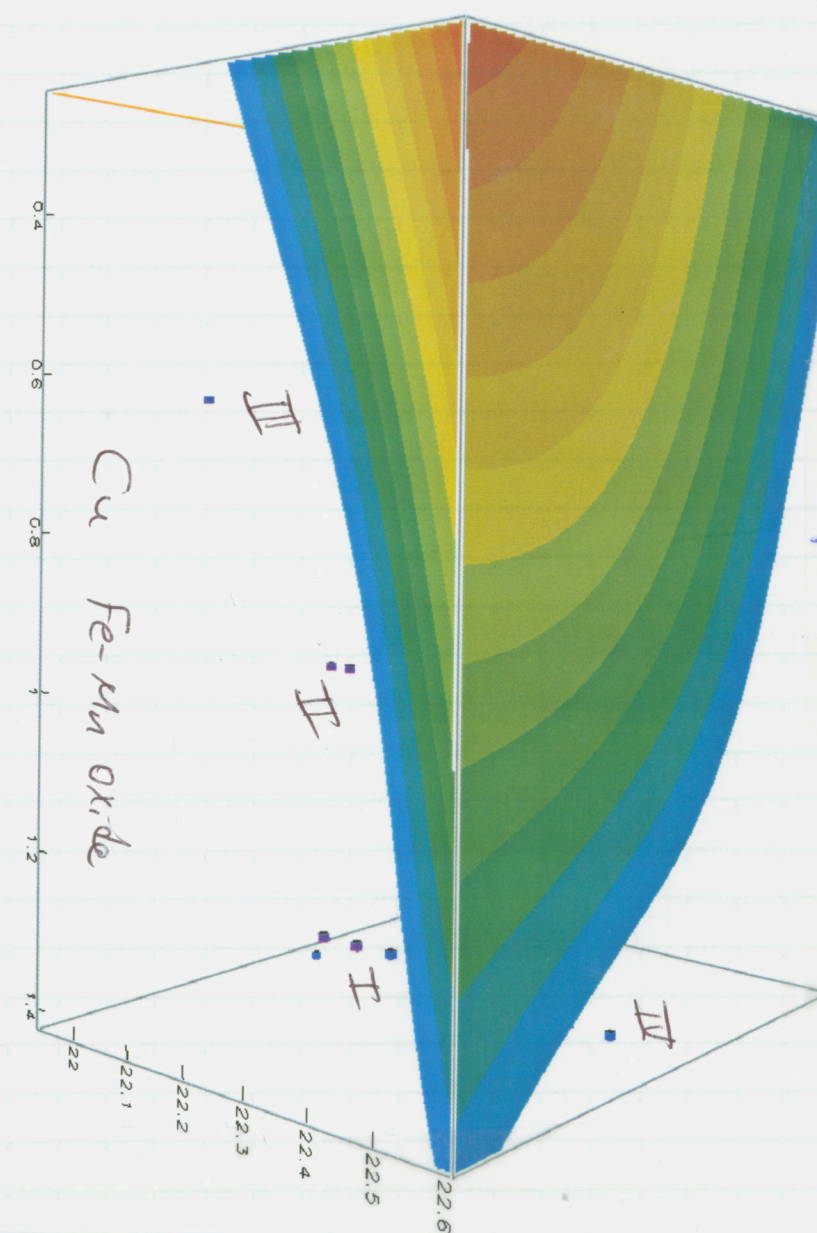
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Akrothri

 $\mu + \sigma \approx 2.4$  contour

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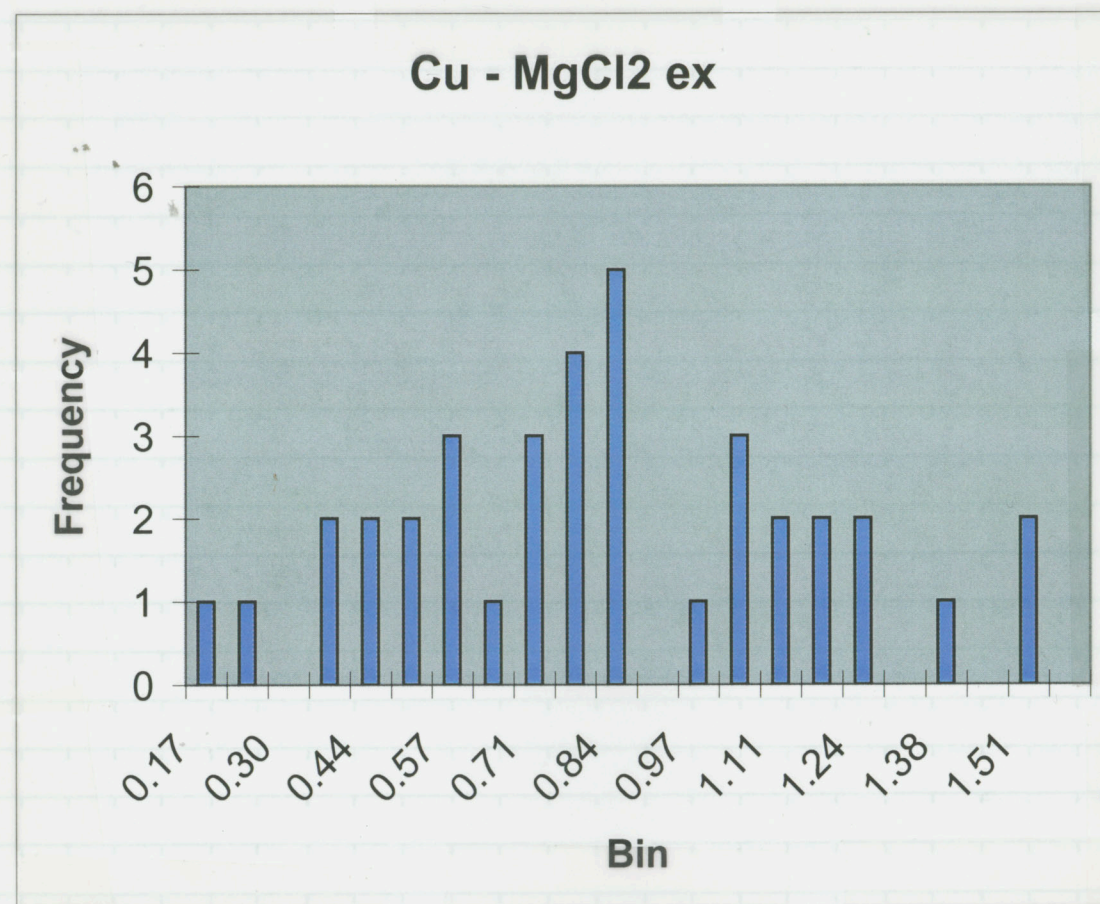
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Akrotri



$\mu = 0.79$   
 $\sigma^2 = .1176$   
 $\sigma = .343$   
 $\min = 0.17$   
 $\max = 1.51$

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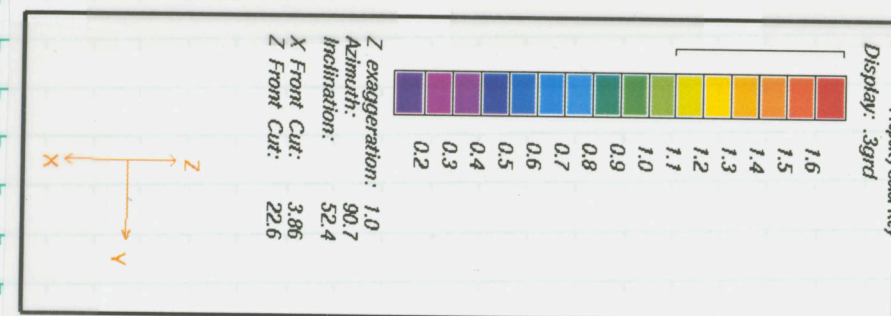
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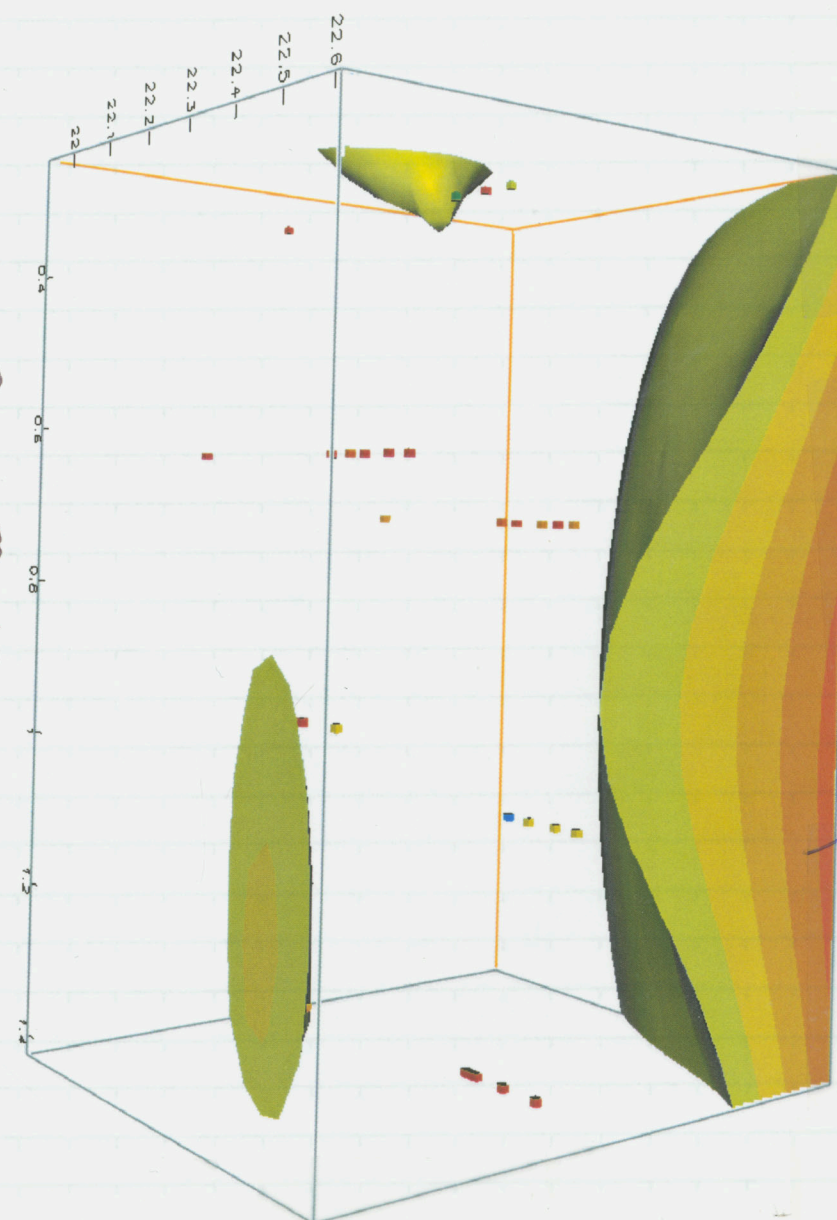
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Akrotri



Contour  $\mu + \sigma \approx 1.1$   
 Cu MgCl<sub>2</sub> exchange



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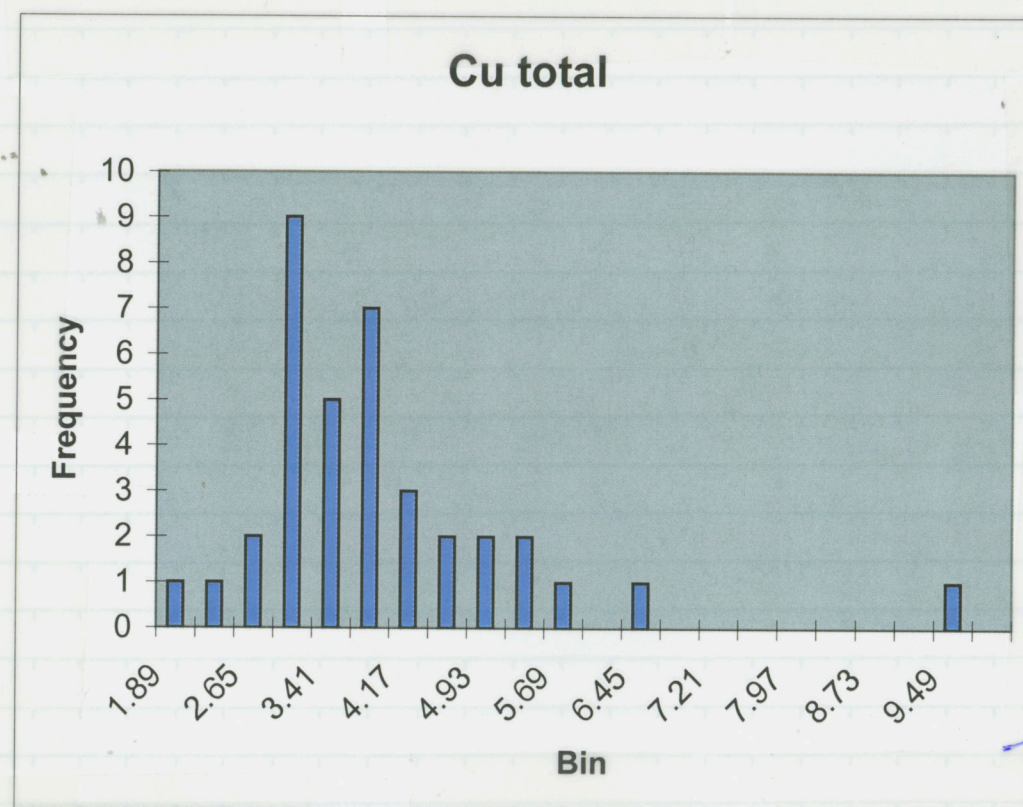
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Akrotiri



$$\mu = 3.71$$

$$\sigma^2 = 1.76$$

$$\sigma = 1.326$$

$$\min = 1.89$$

$$\max = 9.49$$

throw out

9.49 datum

$$\mu = 3.55$$

$$\sigma^2 = .83$$

$$\sigma = .91$$

$$\min = 1.89$$

$$\max = 6.09$$

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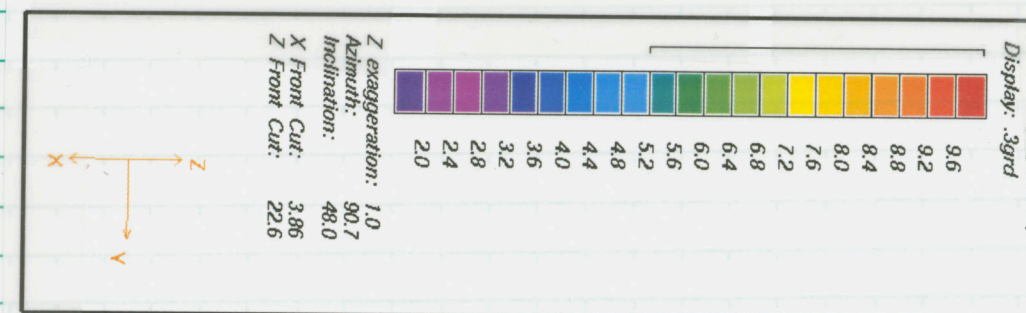
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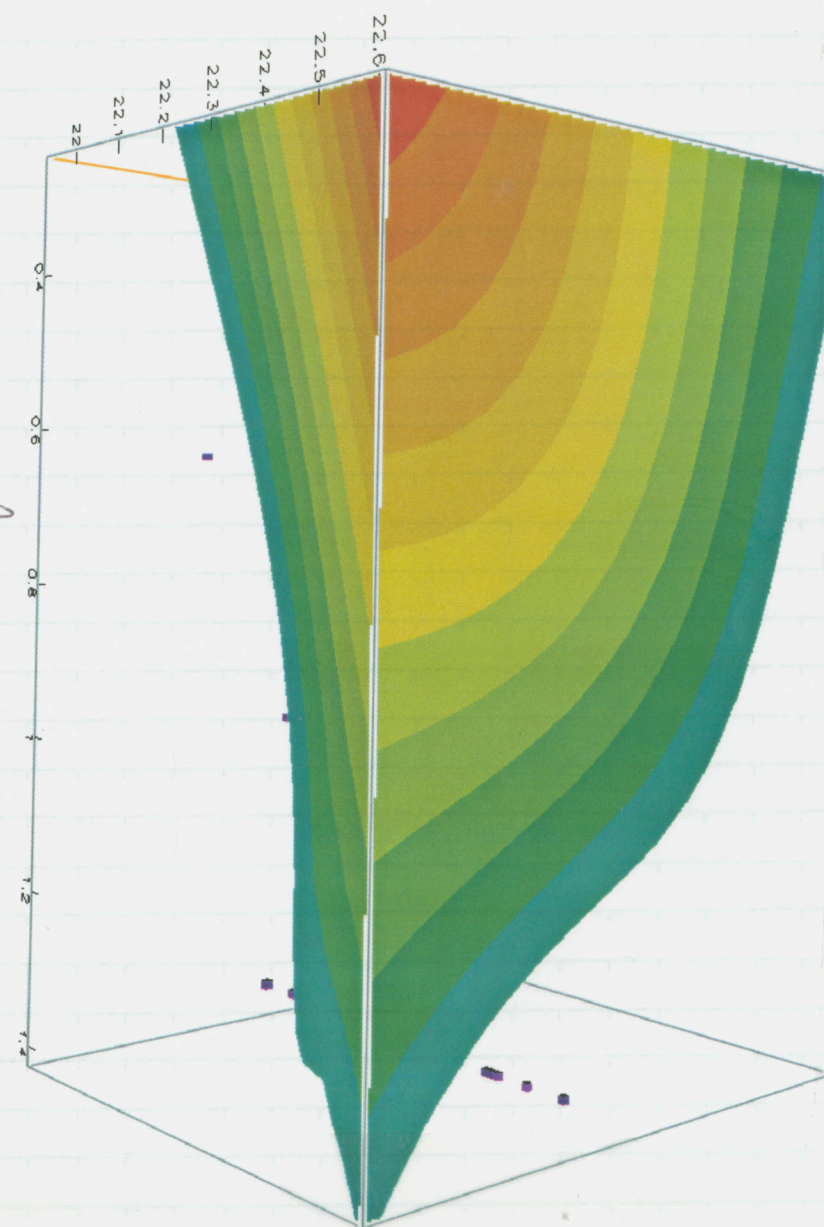
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Akrotiri



Cu total

$\mu + \sigma \approx 5.0$  (5.2) cm bsw



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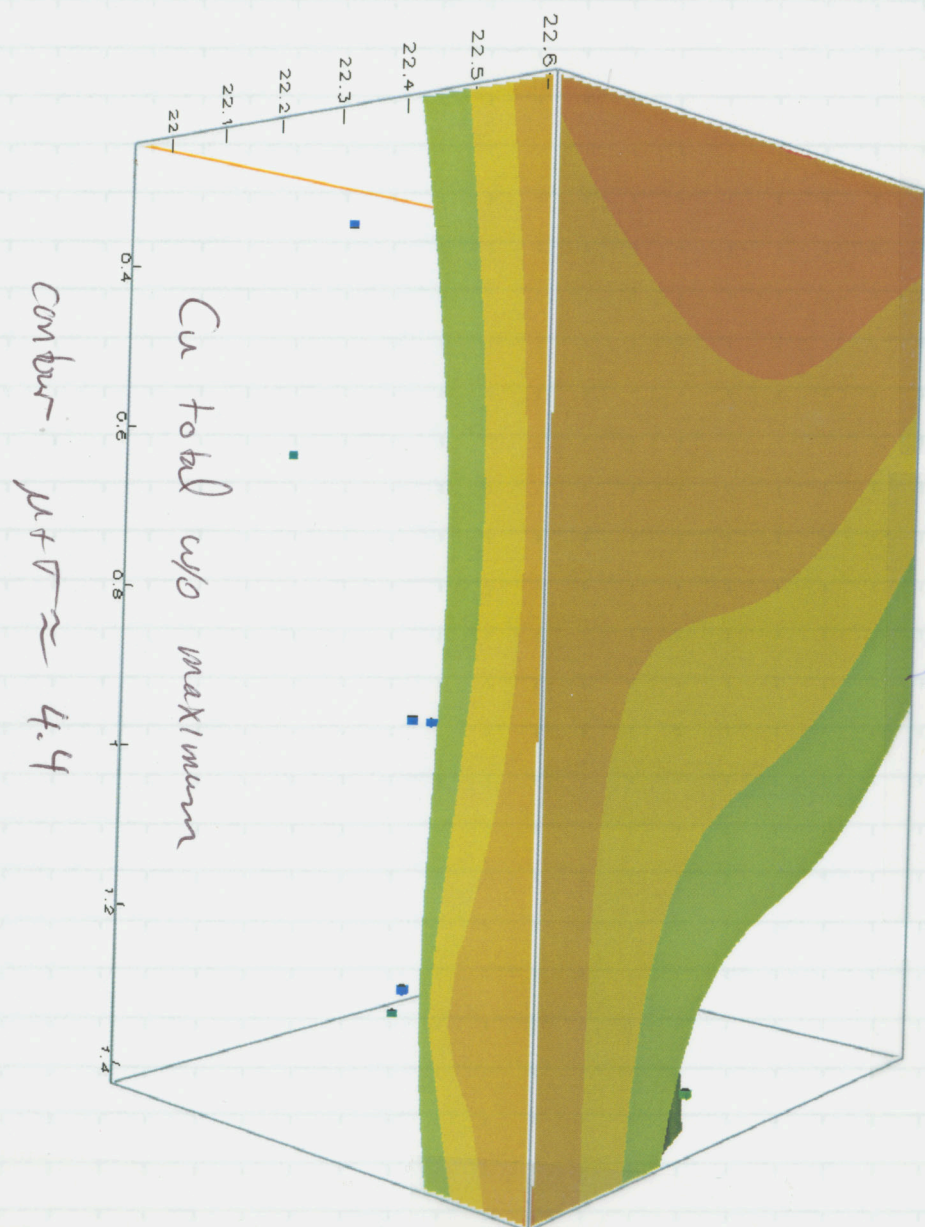
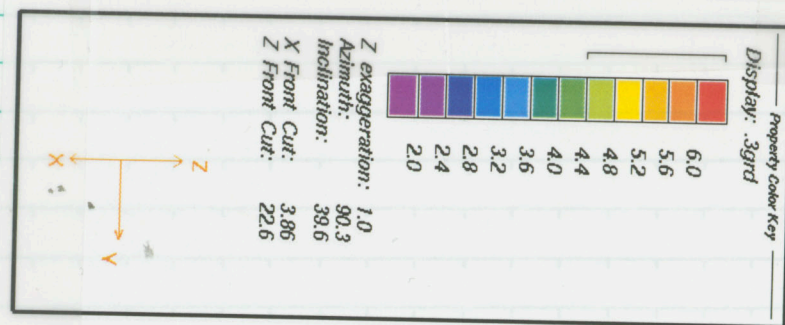
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Akrotiri

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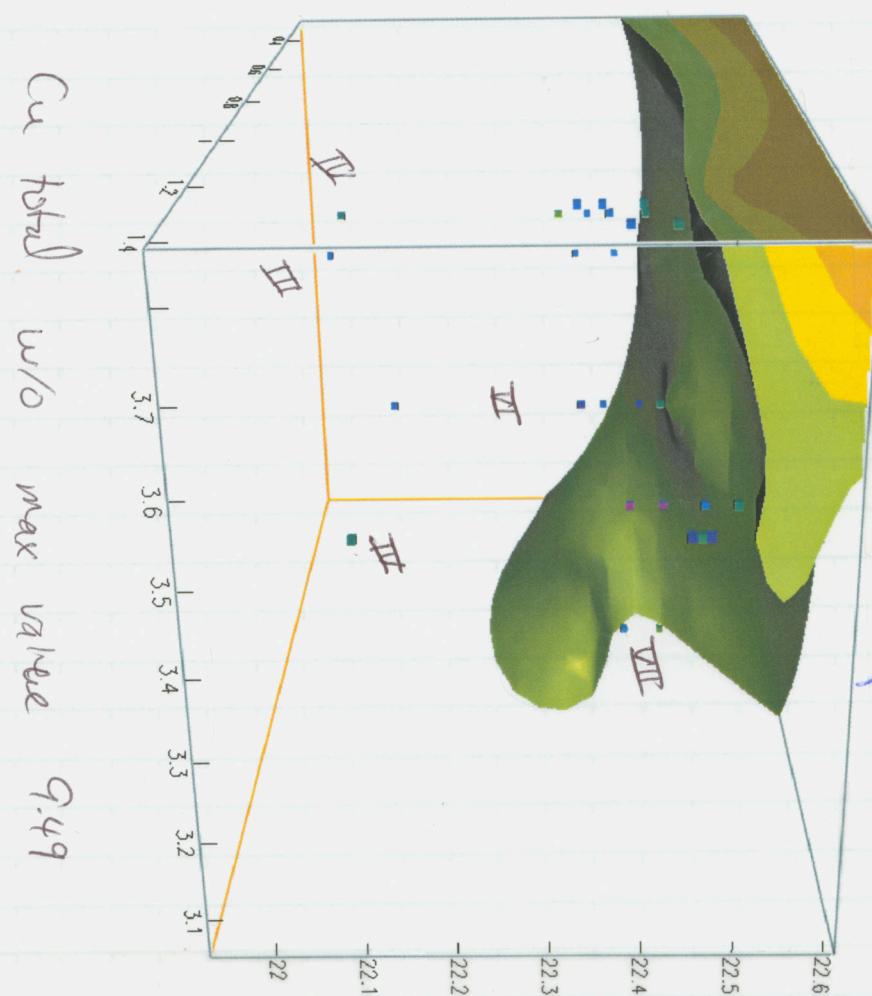
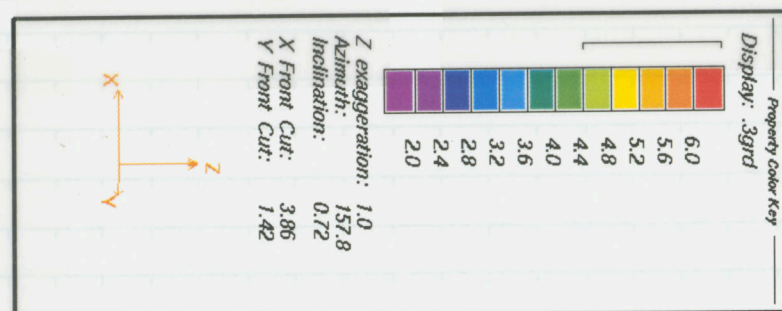
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Akrotiri

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The redacted material is from the following reference:

Hughson, D.L., L. Browning, W.M. Murphy, and R. Green. "An Archeological Site at Akrotiri, Greece, as a Natural Analog for Radionuclide Transport: Implications for Validity of Performance Assessments." Proceedings of the Scientific Basis for Nuclear Waste Management XXIII. D. Shoosmith and R. Smith, eds. Materials Research Society. 1999.

Paper due circa Oct 1, 1999 according to Bill Murphy.

1D & 3D models w/ parameters & BC variations

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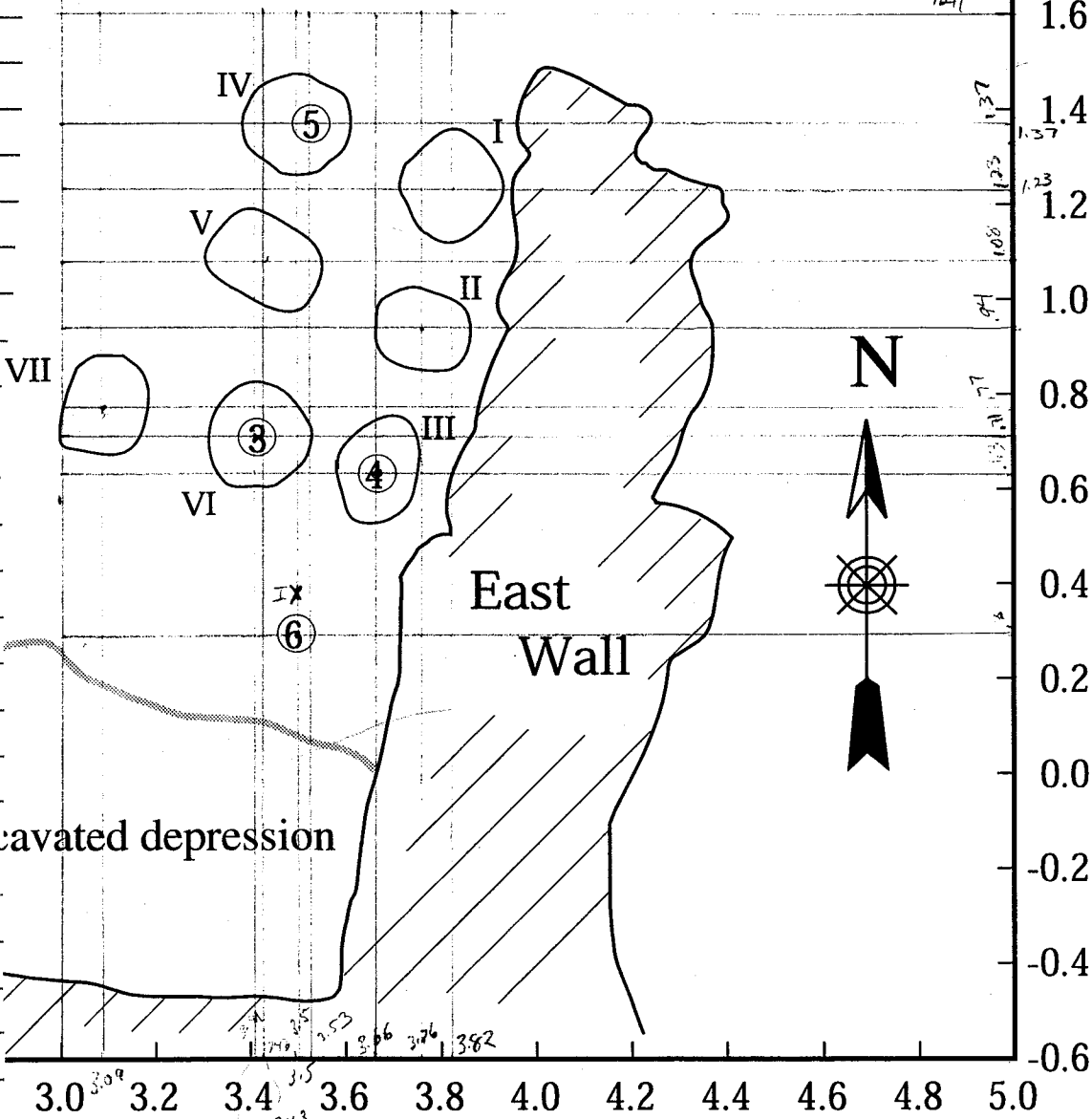
TITLE

ENFE - Akrotiri

From F

HOLE	X	Y	m Z elev topo	cm Δ paired corals	ref
I	3.82	1.23	22.55	4.5 22.51	18.05
II	3.76	0.94	22.52	6.0 22.46	16.52
III	3.66	0.63	22.49	2.0 22.47	20.49
IV	3.53	1.37	22.59	3.5 22.56	19.09
V	3.43	1.08	22.54	2.0 22.52	20.54
VI	3.41	0.71	22.50	0 22.5	22.50
VII	3.09	0.77	22.50	0 22.5	22.50
IX	3.5	0.3	22.47	3.0 22.44	19.47

20p  
8/24/00  
Woul.  
20p  
8/24/00



Location EW (m)

Location NS (m)

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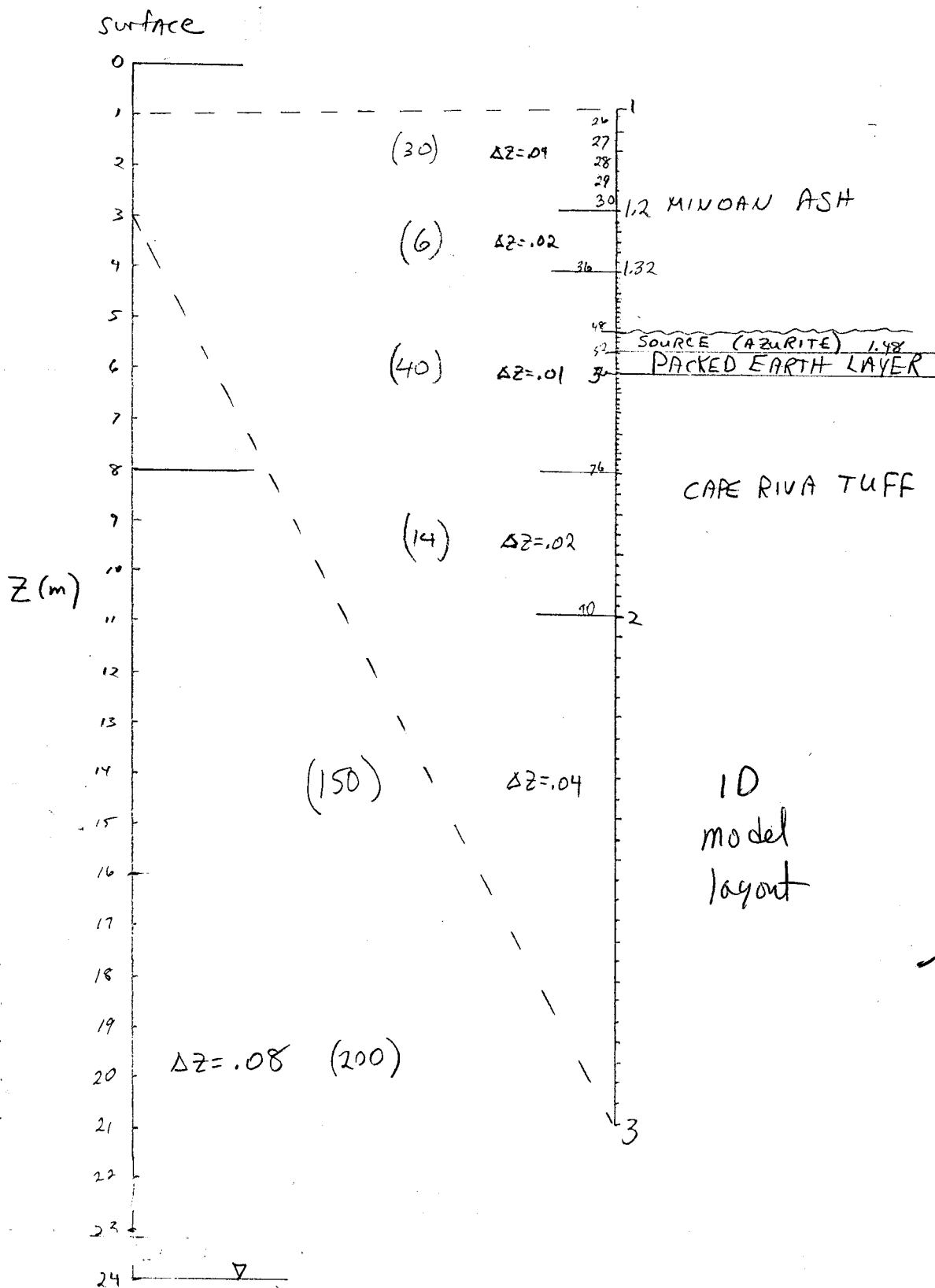
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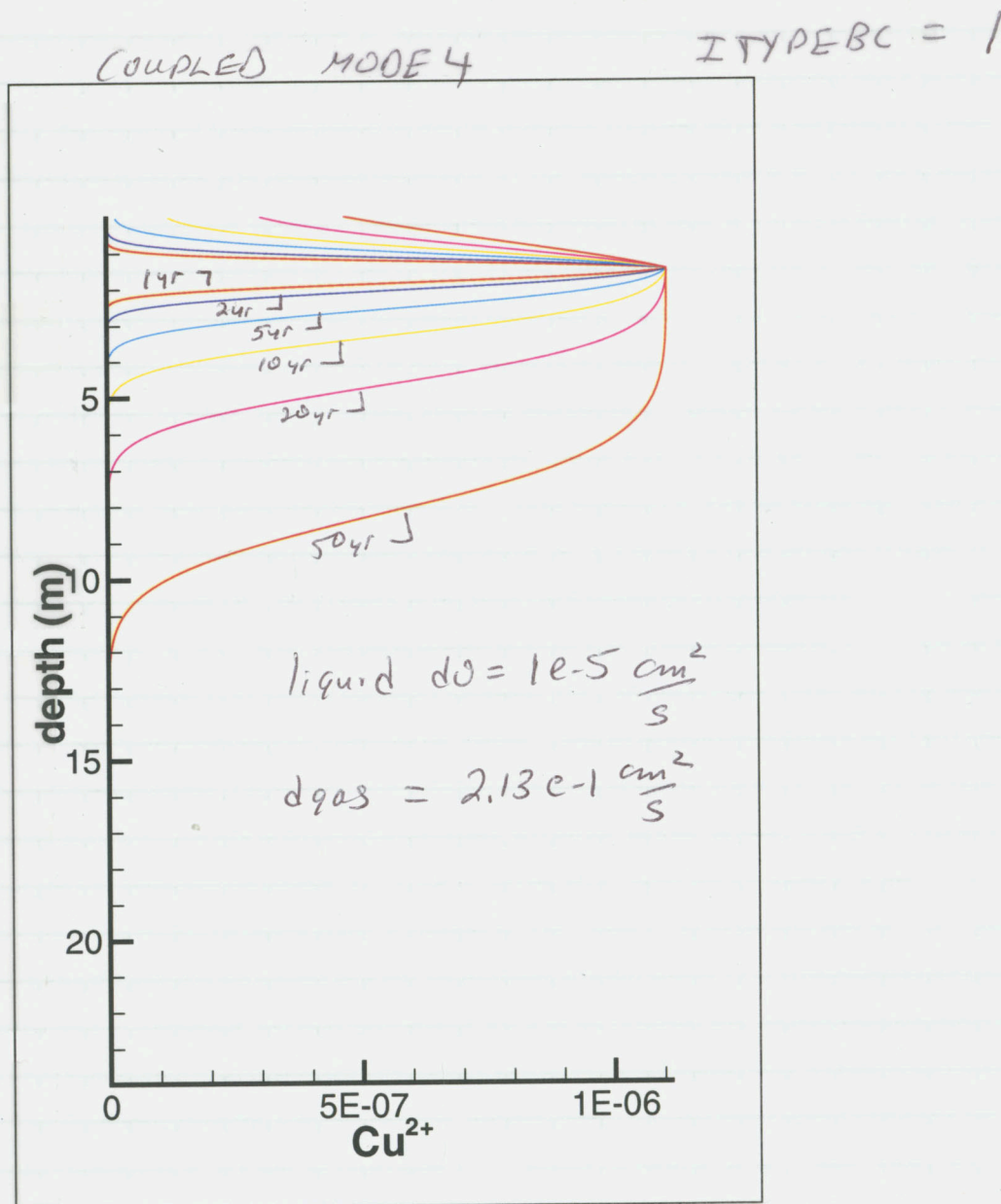
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Problems found with itypebc = 5 & reported to  
S Poulter Aug 2, 1999.  $S_g$  at bc adjusted by  
trial & error to give  $\sim 10.5 \frac{mm}{yr}$  infiltration

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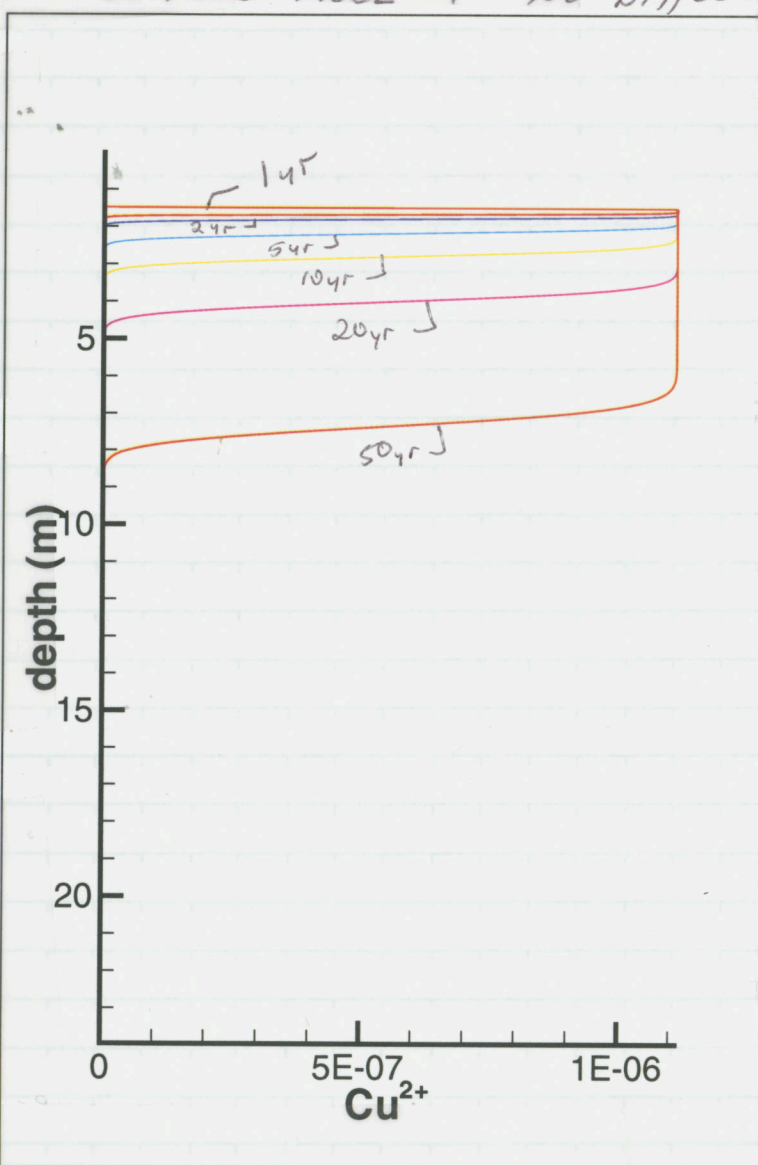
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COUPLED MODE 4 NO DIFFUSION

0 aqueous  
& gaseous  
diffusion

$$q_z \approx 10.5 \frac{\text{mm}}{\text{yr}}$$

$$\phi = .52 \quad S_e = .18 = \frac{\theta}{\phi} \quad \theta = 9.36e-2$$

$$v = \frac{q}{\theta} = \frac{10.5 \frac{\text{mm}}{\text{yr}}}{9.36e-2} = 112 \frac{\text{mm}}{\text{yr}} \quad @ 50 \text{ yr} = 5.6 \text{ m}$$

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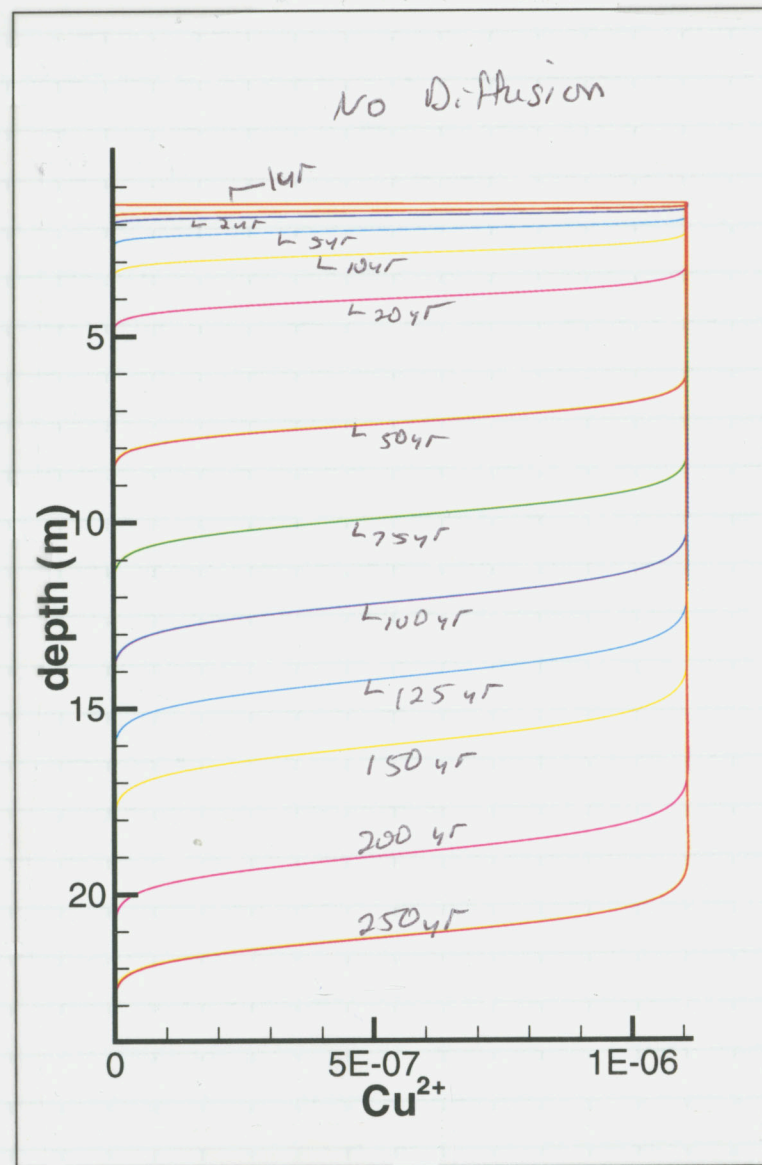
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Aug 2, 1999

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No Diffusion



10.5 mm/yr

infiltration

with  
advective  
transport  
alone

10.5 mm/yr  
flux,  
plane  
will  
arrive  
at the  
water  
table  
in about  
300 years

using base  
case properties

~ dhuqson/multiFlo/murphy/akrotiri/10/inputfiles/

multi.1 masin.1

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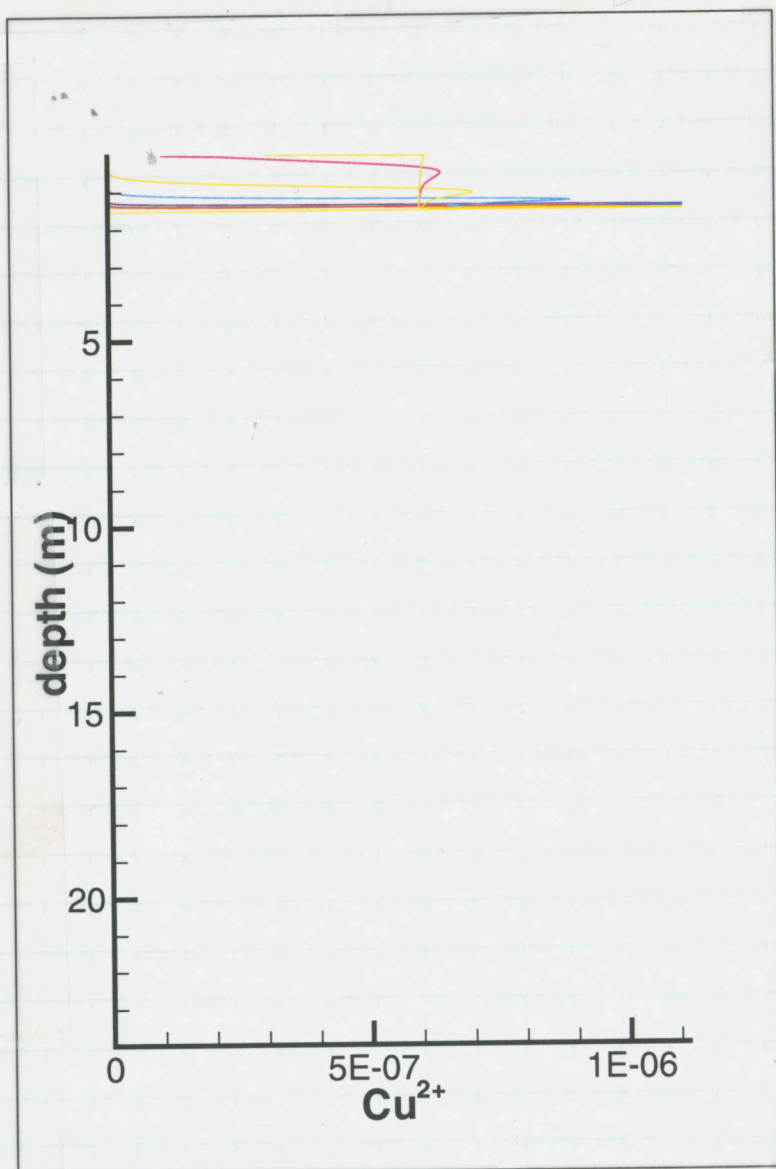
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$S_g$  at top  
 $BC = 0.9$

$S_l = 0.10$

Results in  
 upward  
 liquid flux  
 of  
 $\sim -4.75 \frac{\text{mm}}{\text{yr}}$

Agrees  
 diffusion

$D_d = 0$

Simulation  
 to ~~20~~  
 250 years

ECP  
 8/24/00

THE quality of  
 this page is now  
 improved.

ECP  
 8/24/00

Note

Murphy et al (1998) represent infiltration @  $15 \frac{\text{cm}}{\text{yr}} = 150 \frac{\text{mm}}{\text{yr}}$

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Sg Top BCFlux in top layer

0.43

10.6 mm/yr

② 25°C

0.40

15.0 mm/yr

0.30

47.0 mm/yr

0.20

205.0 mm/yr

0.10

4811.0 mm/yr

mean annual precip = 32 cm/yr = 320 mm/yr

Est mean annual infiltration = 150 mm/yr ?

~~Est~~ mean annual temp = 17°C

ECP 8/24/2000

Sg at Top BCFlux in top layer

② 17°C

0.4

12.4 mm/yr

0.3

38.8 mm/yr

0.2

169.6 mm/yr

0.1

3463.2 mm/yr

0.19

209 mm/yr

0.18

263 mm/yr

0.17

342.1 mm/yr

0.16

466 mm/yr

0.15

680.8 mm/yr

0.14

1129.5 mm/yr

0.13

2808.4 mm/yr

0.10

3379.0 mm/yr

0.09

-3.75 mm/yr

0.095

-4 mm/yr

0.05

-5 mm/yr approx

② 17°C

25°C @ TOP 17°C @ bottom

Use  
as initial  
condition

0.12

16429 mm/yr

≈ 4.5 mm/day

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Hellenic National Meteorological Service  
Climatological Data Base

Lat N 36.25 Long E 25.26 1974-1991

Mon	Total mm	Max 24 hr	Avg monthly Total
Jan	59.4	47.6	13.2
Feb	60.2	58.5	13.38
Mar	53.2	114.5	11.8
Apr	15.0	41.0	3.3
May	3.6	21.6	0.8
Jun	.9	4.0	0.2
Jul	.0	0.8	0
Aug	.1	2.0	0.22
Sep	5.6	64.4	1.24
Oct	19.9	40.2	4.42
Nov	50.1	46.3	11.1
Dec	52.7	33.0	11.7

320.7

Unlikely to be < 10 mm/yr infiltration

Simulated precipitation model did not work ~  
flooding, pt errors, terrible mass balance, etc.

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TITLE

ENFE AKROTIRI

3D model setup

Bottom BC from 1D model  
for  $S_g = 0.41$  at TOP BC  $q_{in} = 11.03 \frac{mm}{yr}$

1D model at depth 4.5 m

$P = 101170 Pa$   $T = 17^\circ C$   $S_l = 0.1836$

$= 0.186 @ 4.98 m$

Grid size  $12 \times 9 \times 30 = 3240$

Run for 2 days trying to get initial condition  
steady state. Reached 0.8 years

3D model has impossibly long run times.

try 2D model at slice through 3D. ECP  
ECP 8/24/00 These were not worked, but I realize now that this helps. 8/24/00

Go to File multi. 11mm initialized to ~ 10.6 mm/yr  
infiltration on type 5 pc

Results with 20 mm/yr at 130 mm/yr show lots  
of  $Ca^{2+}$  below packed earth ~ to 4.5m z  
at 10 yrs.

Re try using initialization flux at ~ 1.4 mm/yr

Step to ~ 15 mm/yr for transport.

Results in  $Ca^{2+}$  at 4.5m z in ~ 50 years

Retry initializing to hydrostatic

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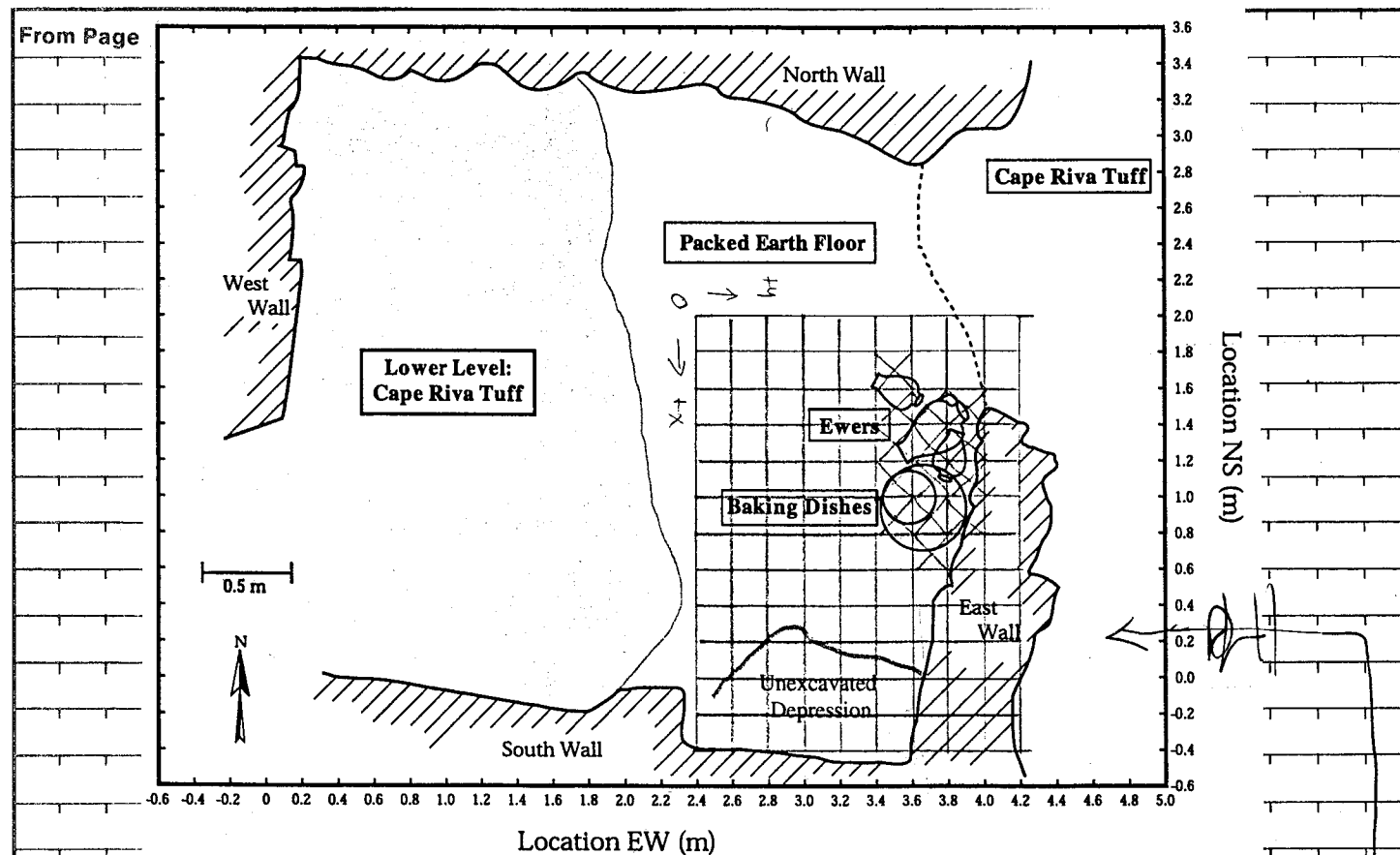
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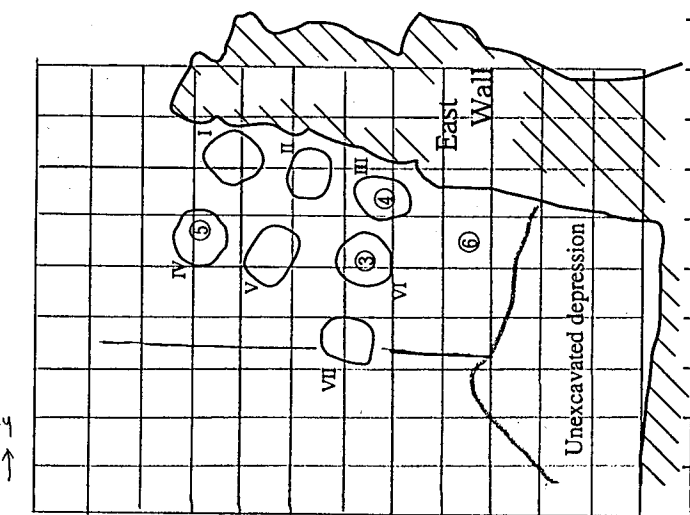
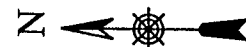
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Location NS (m)

1.6 1.4 1.2 1.0 0.8 0.6 0.4 0.2 0.0 -0.2 -0.4 -0.6



0 → +x

Source term  
in blocks  
marked X

Relation of  
sampling holes  
to grid  
& coordinates

X = 2 m N  
y = 2.4 m W  
is origin

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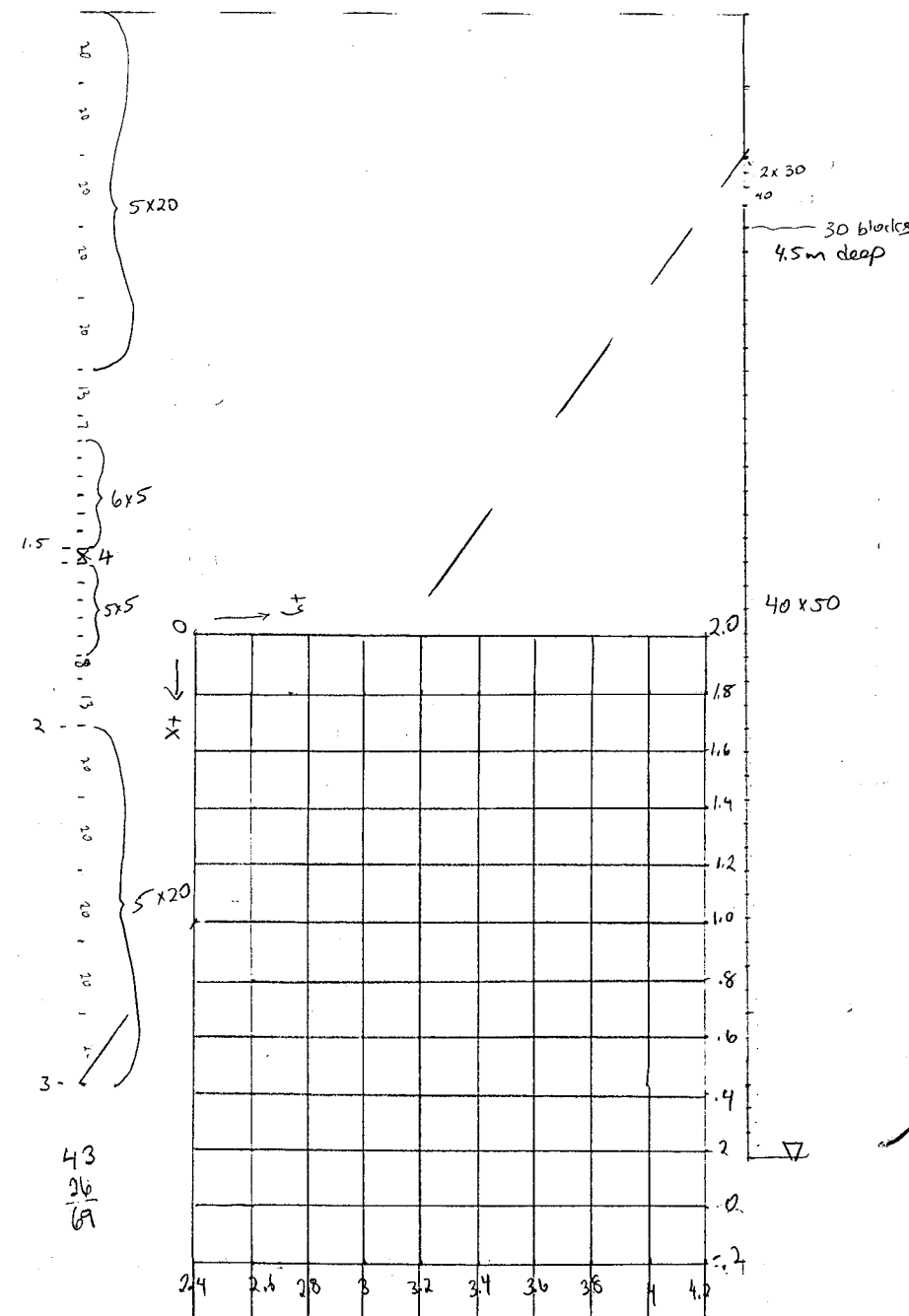
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3D model discretization



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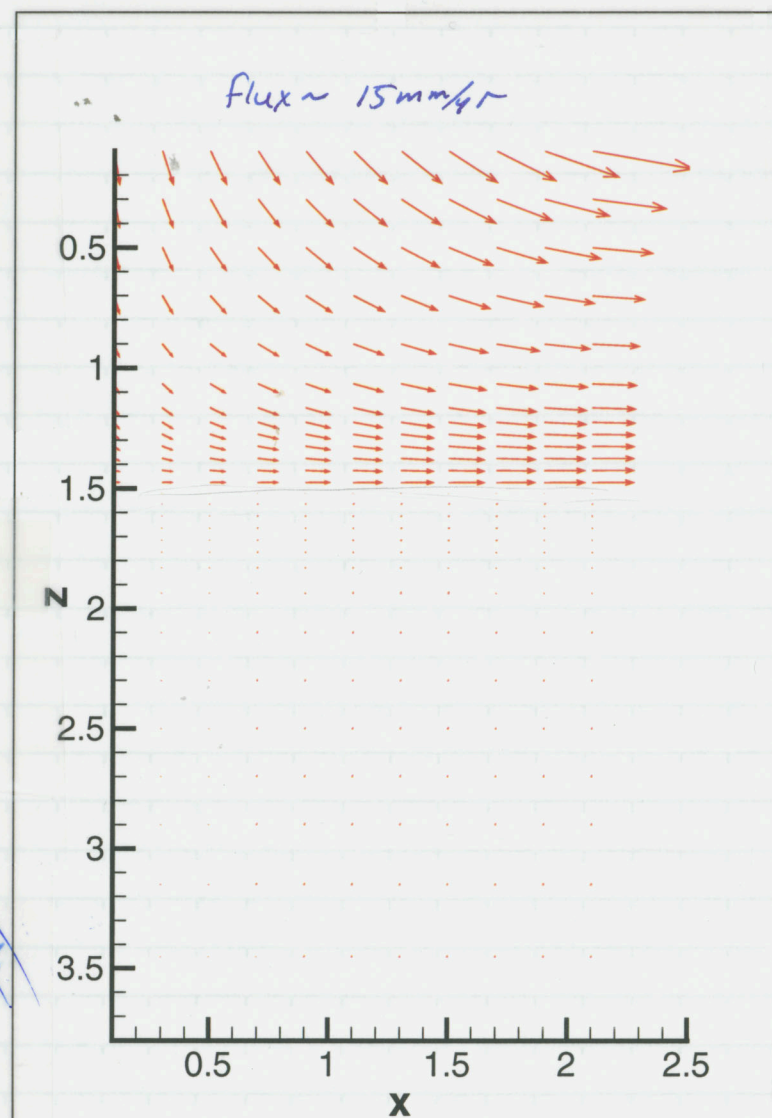
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No-flow on  
left sideLarge block  
reservoir on  
right side  
(prescribed state)Initial cond  
close to  
hydrostaticFlux on top  
set to 15 mm/yrZ vel slightly  
less ~ 13. mm/yrshows the  
diversion  
capacity of  
the packed  
earth layerSlope  $\angle$   
set to  $16^\circ$   
sloping south

Graphs on following page show  $\text{Cu}^{+2}$  transport  
due to advection only. Aquem's Diffusion set  
to zero. No  $\text{Cu}^{+2}$  below packed earth in 500 yrs.

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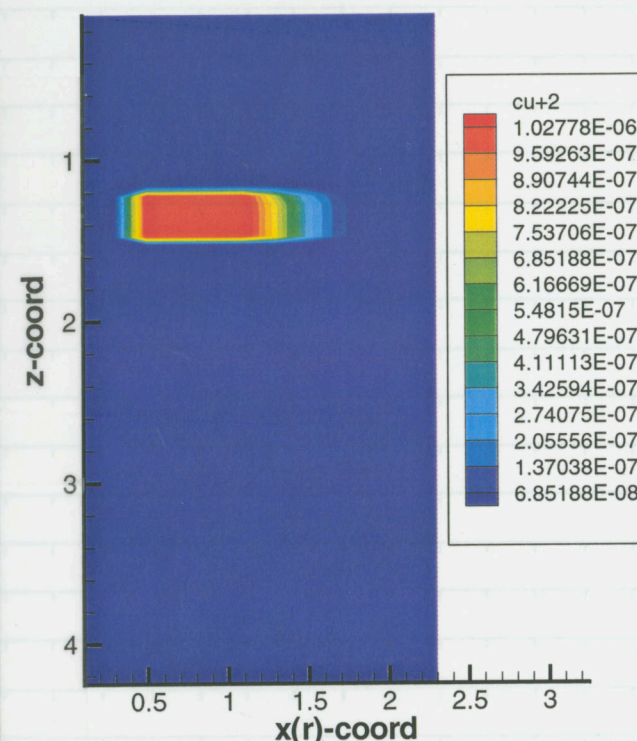
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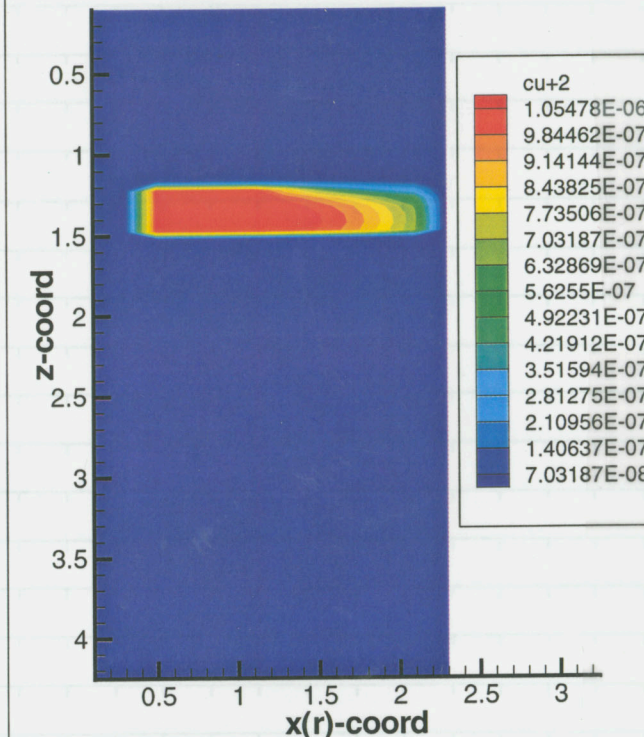
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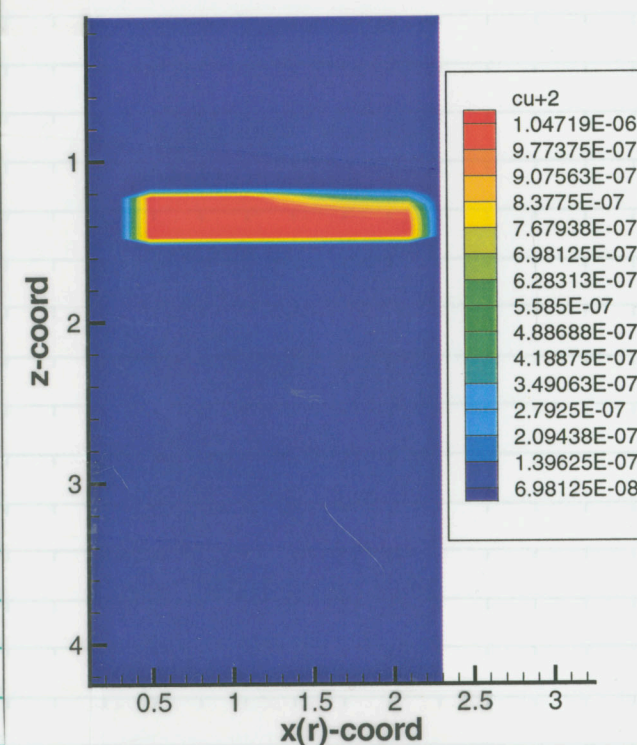
1 year



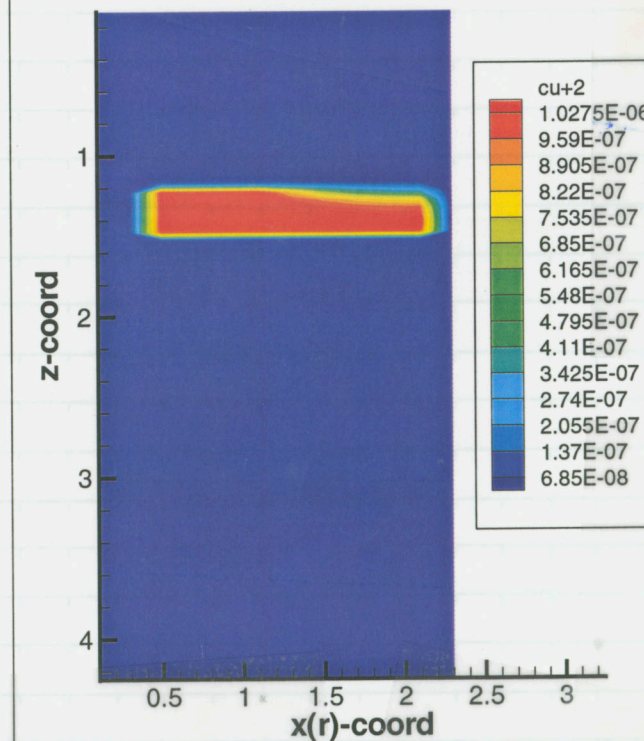
5 year



10 year



500 year



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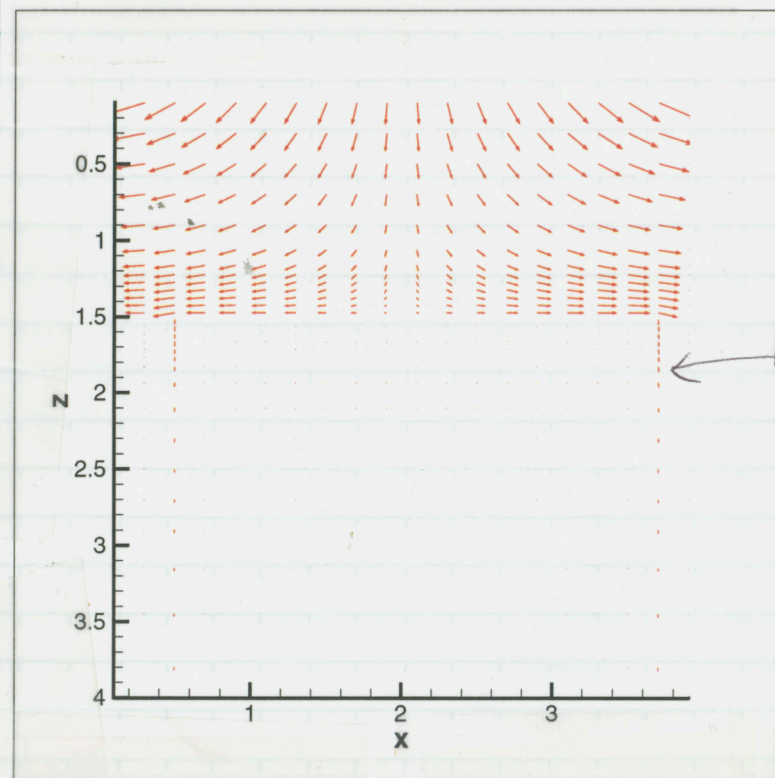
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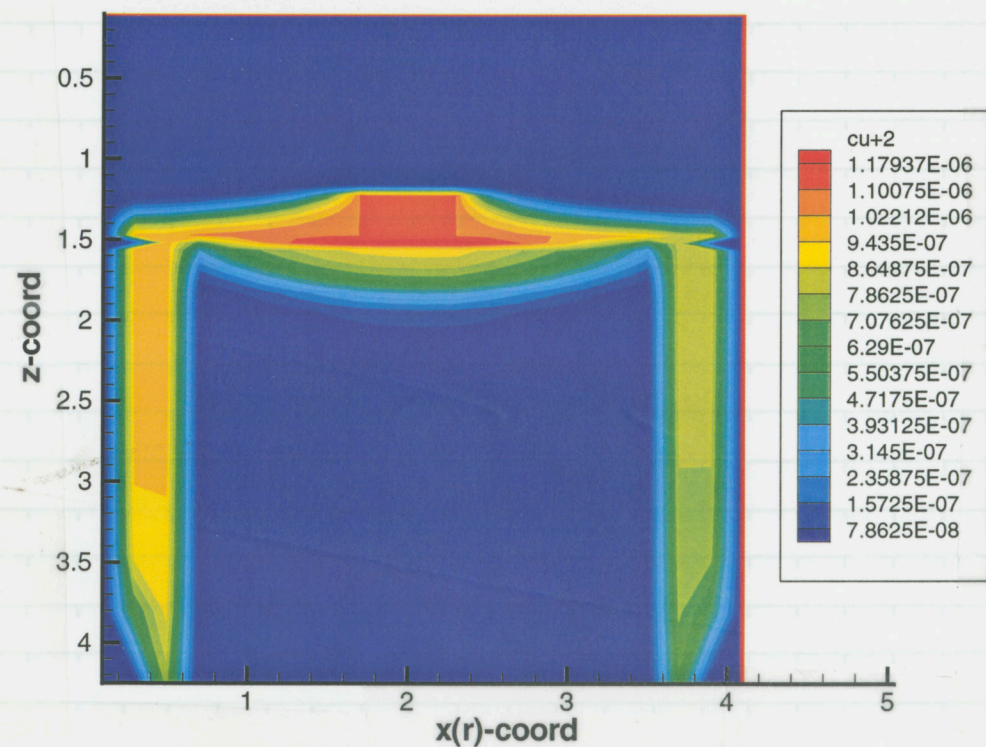
From Page No.



Initialized to nearly hydrostatic. The 15 mm/yr infiltration to steady state ~ prescribed state BC right and left with high  $K$  zones for fracture conduits. BC dominate this model & give rise to diversion above the contact.

Numerical diffusion results from resident velocities

500 years, 15mm/yr infiltration, no diffusion



1 to 10 mm/yr in the supposed hydrostatic initial condition prior to flux at the top.

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TITLE

ENFE Akrotiri

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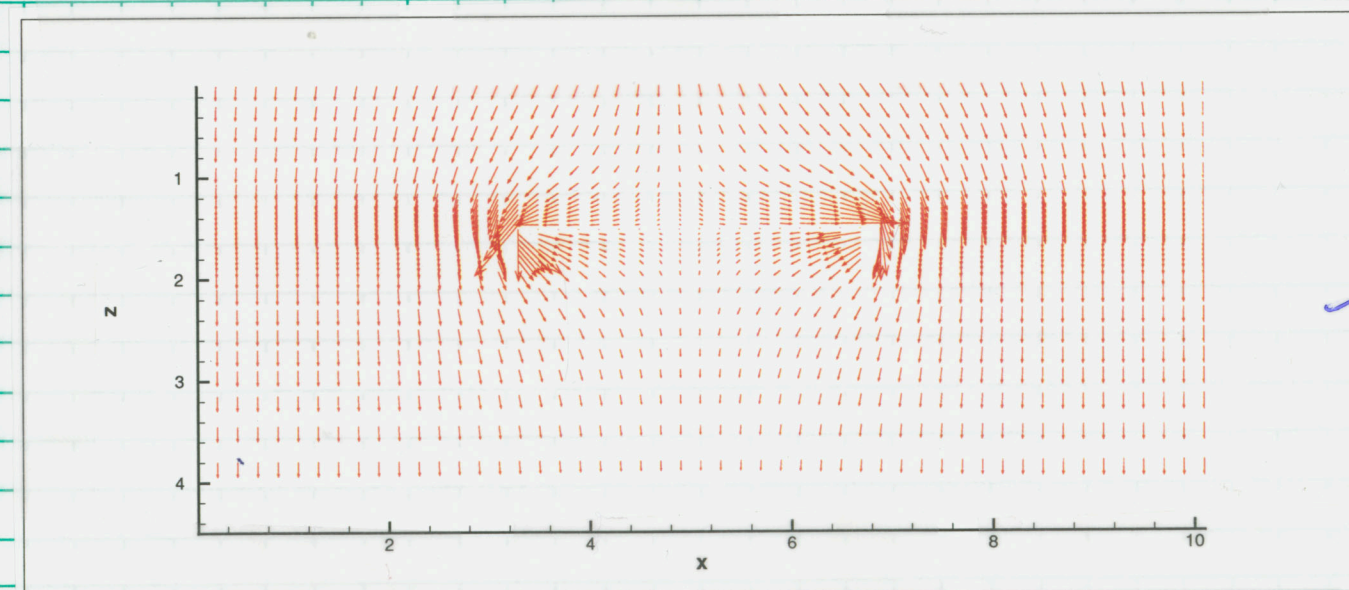
Previous page input file saved as  
~dhughson/multiflo/murphy/akrotiri/20/inputfiles  
multi.1 and masin.1

Need to widen model domain to move BC farther away.

52 columns at 0.2 m wide - same depth 4.5 m

Picked center in middle 12 cols  
Ash on Cape Riva otherwise

No flow bc left and right  
~ 15 mm/yr infiltration



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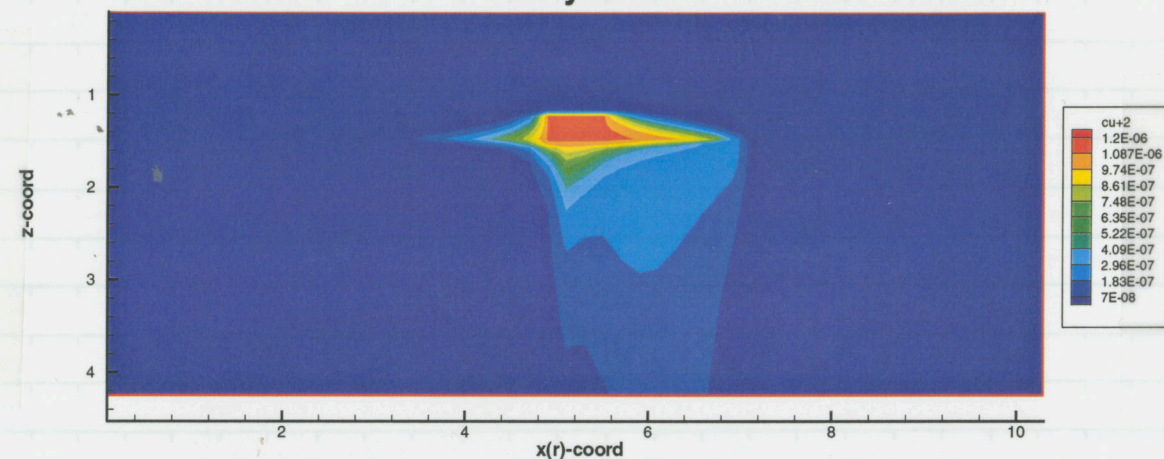
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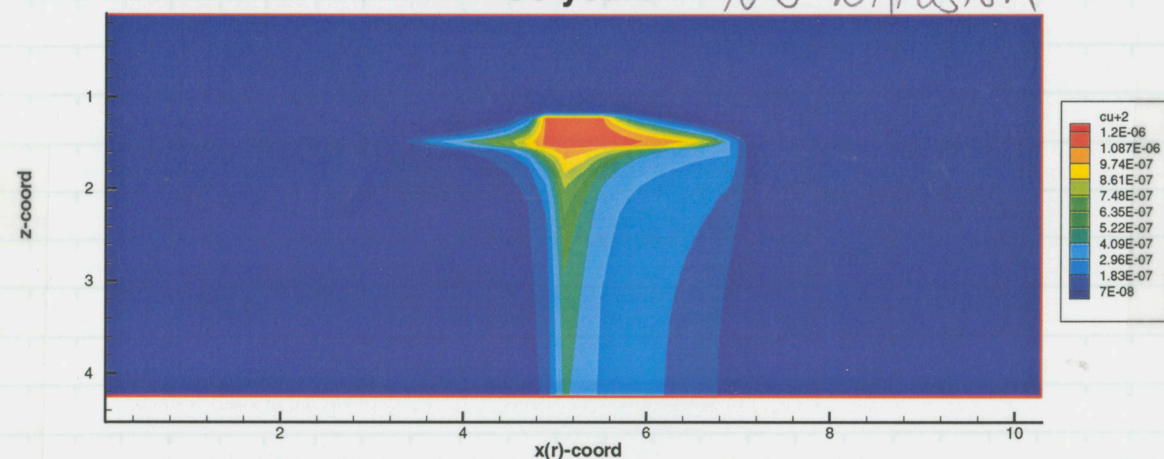
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25 years

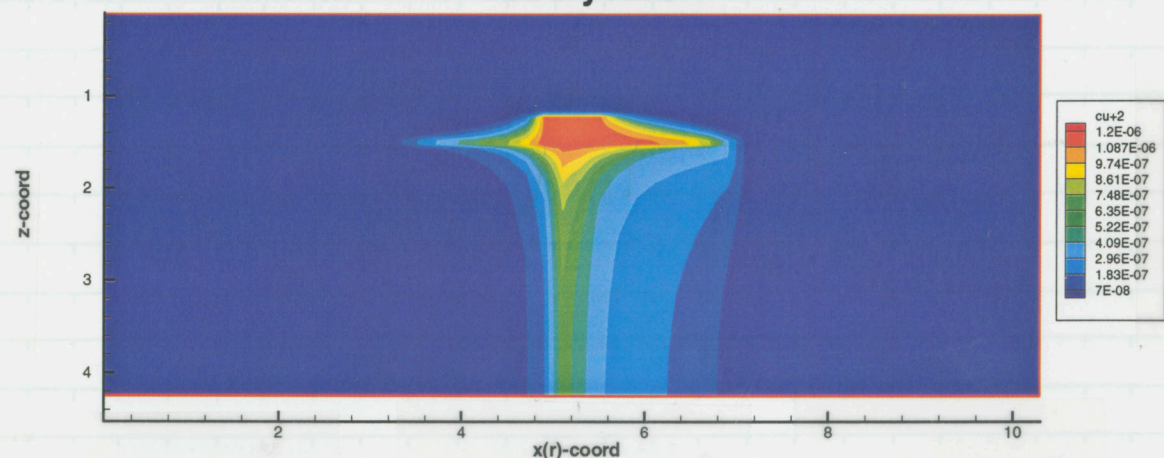


50 years

NO Diffusion



500 years



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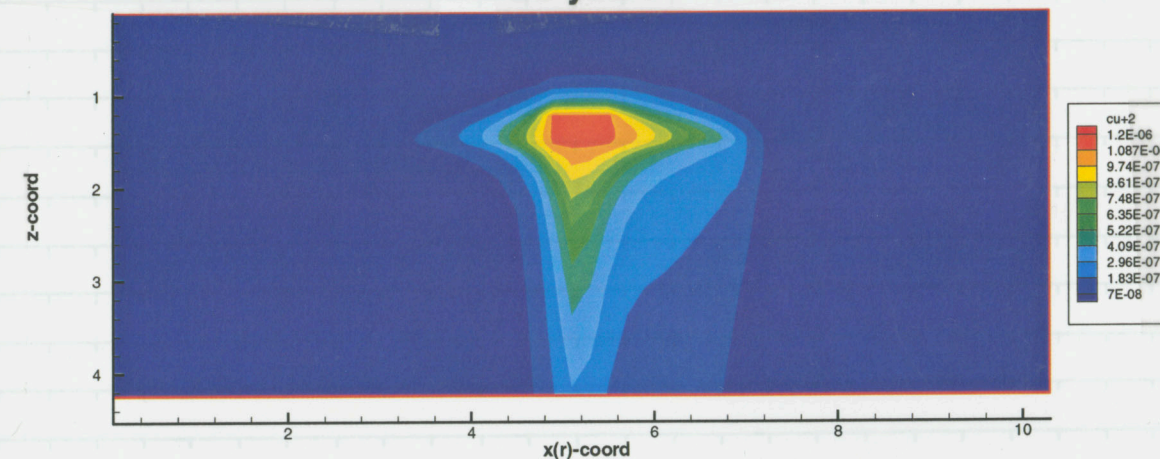
Aug 12  
1999

TITLE

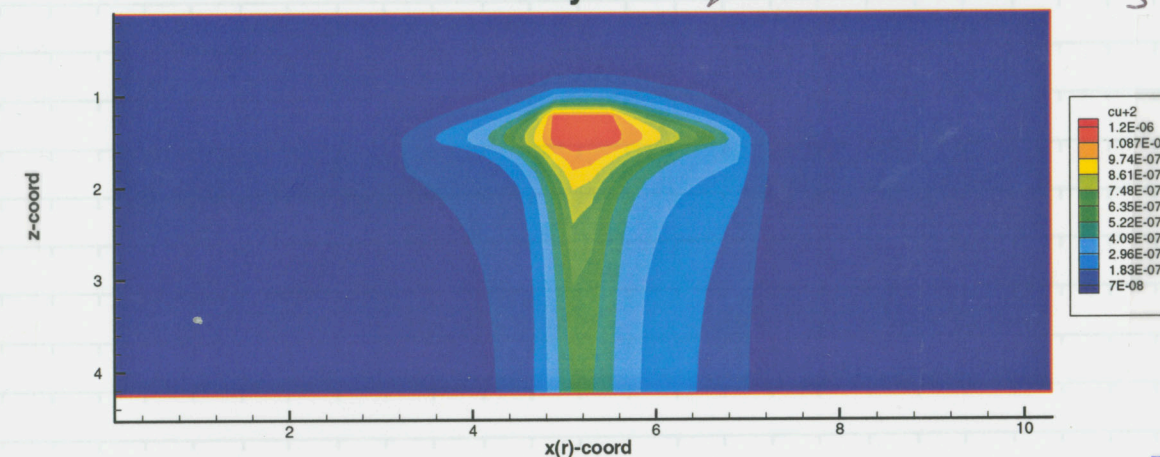
ENFE - AKroti

From Page No.

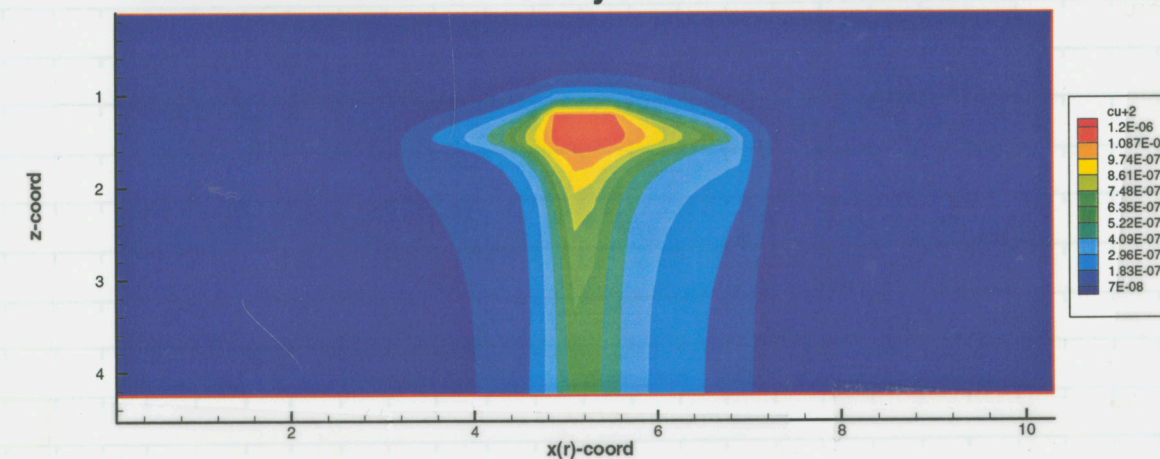
25 years



50 years

Aquifers Diffusion  $7.5E-6 \frac{cm^2}{s}$ 

500 years



To Page No.

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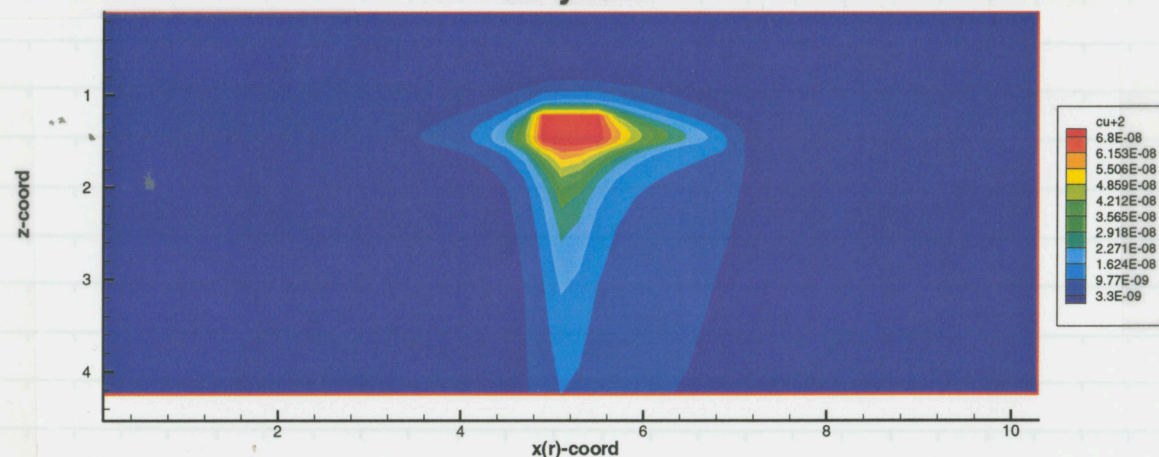
Date

Aug 13  
1999

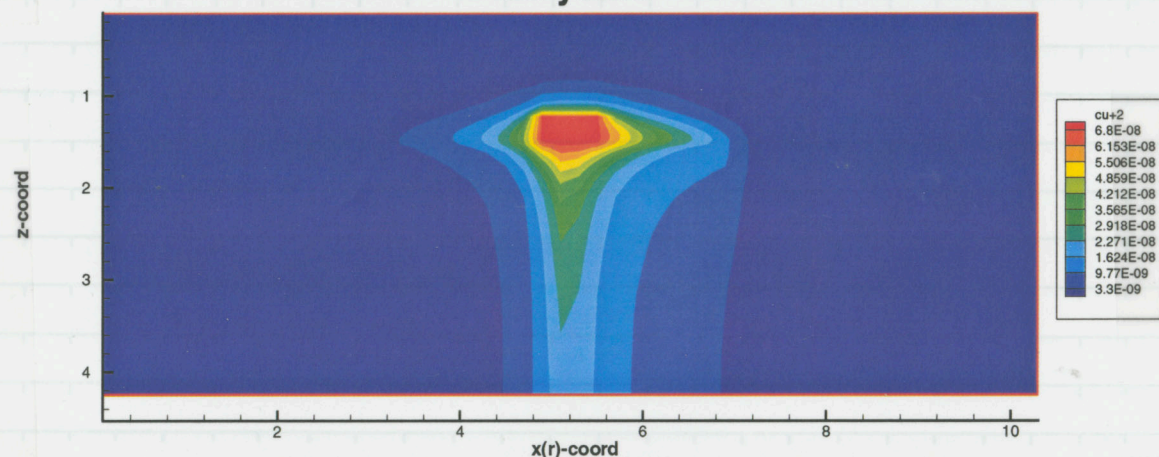


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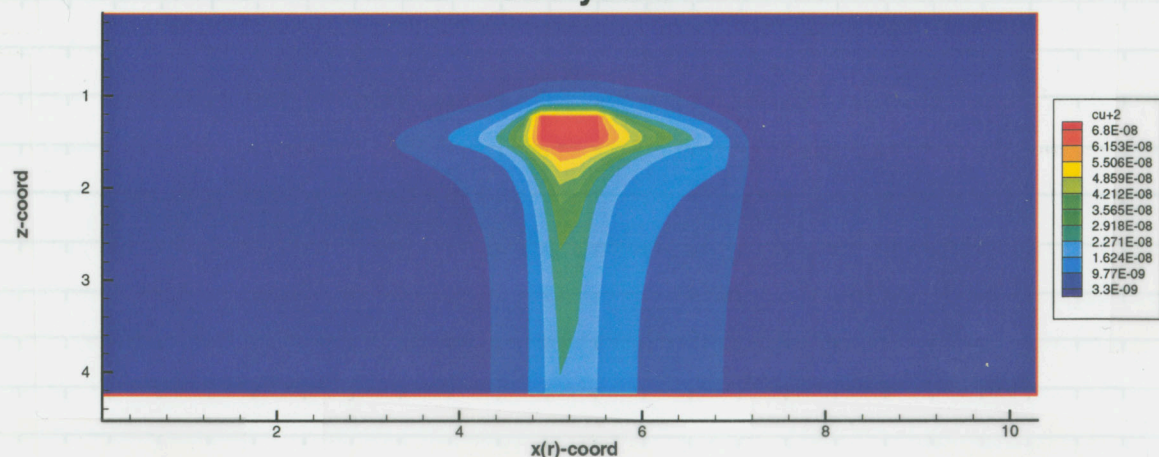
25 years



50 years



500 years



To Page No.

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Aug 16  
1999

TITLE

ENFE Akrotri

From Page No.

Using mineral atacamite as the source instead of azurite results in  $\text{Cu}^{2+}$  concentration reduction but same general shape. But undersaturated  
 ~ dhughson/multiFlo/murphy/akrotri/20/inputfiles/multi.2 masin.2

Potential Evaporation Hamon [1963] from Federer et al. WRR 32(7) p 2319 1996

$$PE = \frac{715.5 \Delta e^*}{T_m + 273.2}$$

$\Delta$  Day length days

$e^*(T)$  saturated vapor press at  $T$  kPa

$T_m$  = mean air Temp for day  $^{\circ}\text{C}$

From CRC  $\approx 72^{\text{nd}}$  ed

8/24/2000  
 This date is now  
 4x better. 8/24/00

Lauren reworked the constraints & aqueous species so that atacamite is closer to equilibrium with the water around the source.

This results in peak concentrations going up about 3 orders of magnitude but plume is about the same shape.

Plot on page 49 input file saved as

~ dhughson/multiFlo/murphy/akrotri/20/inputfiles/masin.3 multi.3

To Page No.

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Date

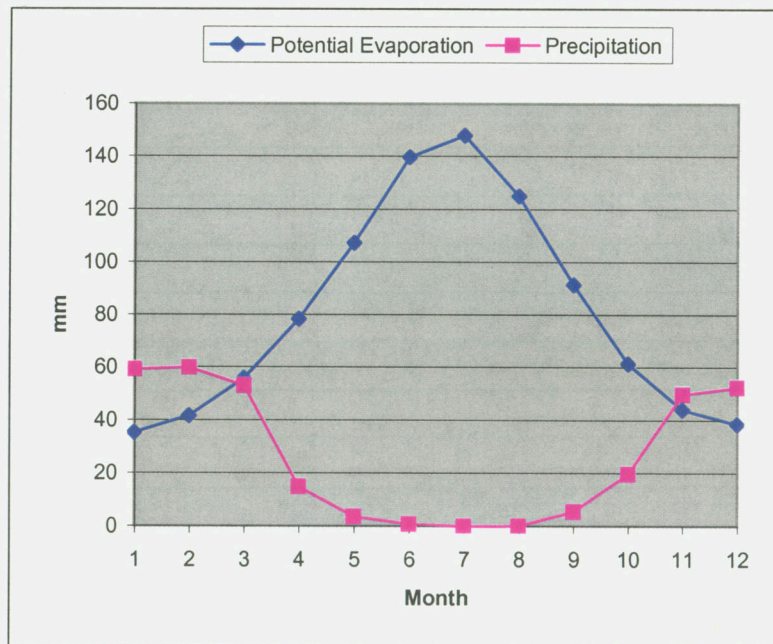
Aug 20  
1999



From Page No. \_\_\_\_\_

Method of Hamon (1963)

Month	Mean T	vap press	day length	PE	Total Prec
Jan	11.2	1.3309	0.348395	35.48204	59.4
Feb	11.2	1.3309	0.409893	41.74532	60.2
Mar	12.7	1.4693	0.5	55.92263	53.2
Apr	15.5	1.76205	0.590107	78.38326	15
May	19.1	2.2119	0.651605	107.3106	3.6
Jun	23.3	2.8628	0.66497	139.73	0.9
Jul	25.4	3.2466	0.625958	148.1172	0
Aug	24.8	3.1322	0.546955	125.1141	0.1
Sep	22.6	2.7441	0.453045	91.4669	5.6
Oct	19.1	2.2119	0.374042	61.59961	19.9
Nov	15.4	1.7508	0.33503	44.23284	50.1
Dec	12.6	1.4598	0.348395	38.72789	52.7



To Page No. \_\_\_\_\_

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Date \_\_\_\_\_

Aug 16  
1999

HELLENIC NATIONAL METEOROLOGICAL SERVICE  
DIVISIONS II-III/STAT. CLIMAT. SECTION  
CLIMATOLOGICAL DATA BASE

STATION 9HPA 744

LATITUDE N 36.25 DEGR LONGITUDE E 25.26 DEGR ALTITUDE OF BARM. 36.50 METERS

DATCLIM MET. PAR.59

MONTH	PRESS (M.S.L.)	PERIOD 1974-1991					REL HUM.	AV. CLOUD.	PRECIPITATION (IN MM)	
		T E M P	E R A T U R E	ABS MAX	ABS MIN	TOTAL MAX 24H				
JANUARY	1018.0	11.2	9.1	21.8	1.0	59.4	71.4	4.6	47.6	
FEBRUARY	1015.9	11.2	9.2	22.0	1.0	60.2	70.7	4.7	58.5	
MARCH	1014.6	12.7	10.2	25.6	1.6	53.2	72.4	4.1	114.5	
APRIL	1012.9	15.5	12.5	28.4	6.6	15.0	69.8	3.5	41.0	
MAY	1013.0	19.1	15.7	32.6	9.0	3.6	67.7	2.7	21.6	
JUNE	1011.6	23.3	19.6	39.0	12.0	.0	62.5	1.1	4.0	
JULY	1010.1	25.4	21.8	39.4	13.6	.0	59.9	.3	.8	
AUGUST	1010.2	24.8	21.6	36.6	16.0	.1	61.8	.4	2.0	
SEPTEMBER	1013.7	22.6	19.4	35.0	10.4	5.6	65.5	1.0	64.4	
OCTOBER	1016.6	19.1	16.4	33.8	10.0	19.9	70.1	2.6	40.2	
NOVEMBER	1016.8	15.4	13.1	27.4	.8	50.1	72.1	3.8	46.3	
DECEMBER	1016.6	12.6	10.0	22.2	.0	52.7	71.6	4.4	33.0	

MONTH	CLIMADINES		N	U	M	B	E	R	O	F	D	A	Y	S	W	I	T	H	TEMPERATURE		W	I
	(C	8/8)																	MIN	MAX		
	0-1.5	1.6-6.4	6.5	8.0	PREC.	RAIN	SNOW	THUND.	HAIL	ST	GND	FOG	DEW	H.FROST	LE	0.0	LE	0.0			GE	68
JANUARY	2.3	23.8	4.8		9.4	9.1	.0	1.2	.1	.1	.1	.0	.4	.0	.0	.0	.0	.0	.0	8.2		
FEBRUARY	1.9	21.4	4.0		9.4	8.9	.4	1.3	.0	.1	.1	.1	1.1	.0	.2	.0	.0	.0	.0	8.3		
MARCH	5.5	20.5	5.0		7.2	6.9	.2	1.7	.1	.0	.0	.2	1.1	.0	.0	.0	.0	.0	.0	6.8		
APRIL	7.8	19.4	2.8		4.6	4.5	.0	.5	.0	.0	.0	.1	.5	.0	.0	.0	.0	.0	.0	5.0		
MAY	12.2	17.3	1.5		1.8	1.6	.0	.2	.0	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	2.7		
JUNE	22.1	7.8	.1		.6	.6	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	2.6		
JULY	28.9	2.0	.1		.4	.4	.0	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	3.8		
AUGUST	28.3	2.7	.1		.1	.1	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	2.6		
SEPTEMBER	23.2	6.4	.3		.9	.9	.0	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0	.0	.0	3.1		
OCTOBER	13.0	16.2	1.8		3.9	3.7	.0	.6	.0	.0	.0	.1	.9	.0	.0	.0	.0	.0	.0	4.3		
NOVEMBER	5.3	21.6	3.2		7.2	7.2	.0	1.4	.0	.0	.0	.2	1.5	.0	.0	.0	.0	.0	.0	5.5		
DECEMBER	3.2	22.9	4.8		10.2	9.4	.0	1.5	.1	.0	.0	.1	.9	.0	.1	.0	.0	.0	.0	8.3		

To Page No.

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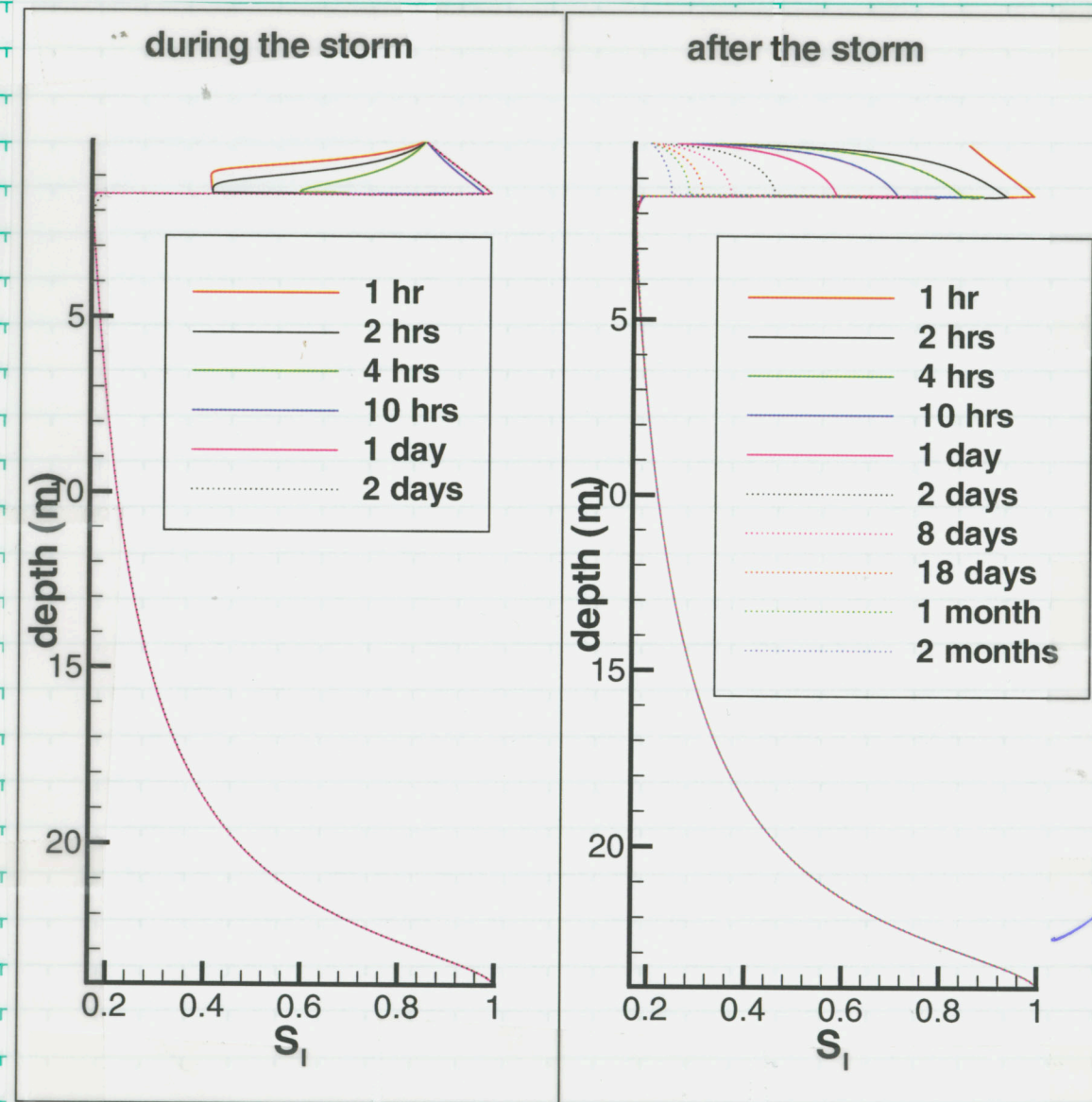
Date

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From Page No.

Suppose Initial hydrostatic  $\sim S_p$  at surface  $\sim 0.4$ .  
 2 day rain causes surface  $S_p = 0.85$ . After  
 rain, sun comes out & dries soil to  $S_p = 0.2$



Water goes below packed earth after 1 day of rain  
 but dries out to hydrostatic  $S_i = 0.4$  between 2  
 and 8 days

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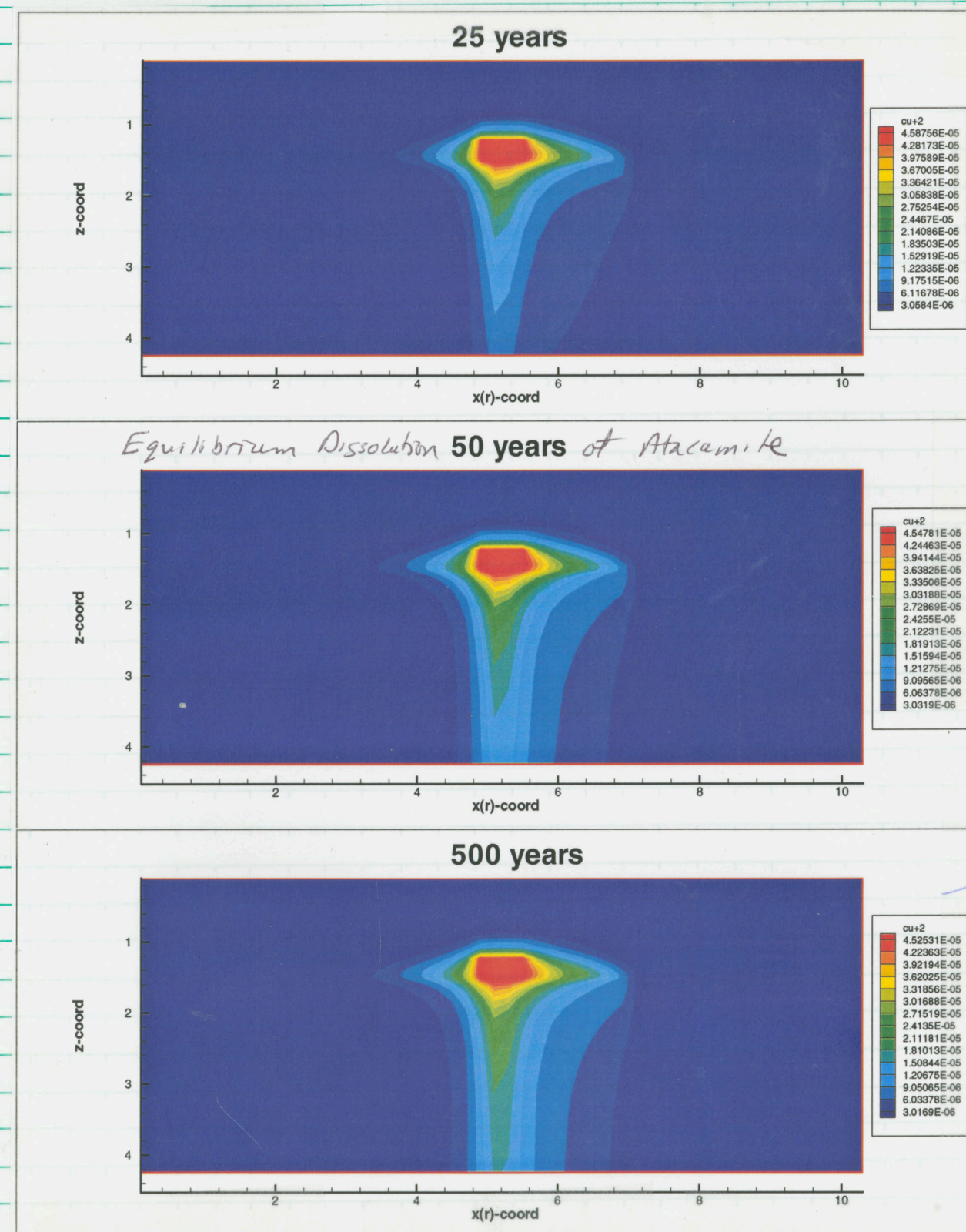
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ENFE - Akrotiri

From Page No.



~ dhuighson/multiflo/murphy/akrotiri/20/ inputfiles/ masin.4 8/ part: 4

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From Page No.

Table 3: Stratigraphic Unit Upper Contacts and Unit Thicknesses for the USW SD-7 Drill Hole  
(-- not present in this hole, or otherwise not identified)

Lithostratigraphic Unit	Abbreviation	Depth to Upper Contact (ft)	Apparent thickness (ft)	Tops from Stratigraphic Compendium (ft)
Tiva Canyon Tuff (Tpc) — 277.9 ft thick <sup>1</sup>				
Crystal-poor middle nonlithophysal zone	Tpcmn	50.1 <sup>1</sup>	24.7 <sup>1</sup>	50.2
lower nonlithophysal subzone	Tpcpml	50.1 <sup>1</sup>	24.7 <sup>1</sup>	
Crystal-poor lower lithophysal zone	Tpcpl	74.8	120.2	140.0
Crystal-poor lower nonlithophysal zone	Tpcpln	195.0	100.4	195.2
hackly subzone	Tpcplnh	195.0	60.8	
columnar subzone	Tpcplnc	255.8	39.6	
Crystal-poor vitric zone ("shardy base")	Tpcpv	295.4	32.6	295.0
moderately welded subzone	Tpcpv2	295.4	21.0	

Geology of Drill Hole USW SD-7

Table 3: Stratigraphic Unit Upper Contacts and Unit Thicknesses for the USW SD-7 Drill Hole  
(Continued)

Lithostratigraphic Unit	Abbreviation	Depth to Upper Contact (ft)	Apparent thickness (ft)	Tops from Stratigraphic Compendium (ft)
nonwelded subzone	Tpcpv1	316.4	11.6	
Pre-Tiva Canyon Tuff bedded tuff	Tpcb4	328	2.5	326.0
Yucca Mountain Tuff (Tpy) — not present			0.0	
Pre-Yucca Mountain Tuff bedded tuff	Tpyb3	330.5 <sup>2</sup>	0.0 <sup>2</sup>	
Pah Canyon Tuff (Tpp) — 14.5 ft thick		345 <sup>2</sup>	14.5 <sup>2</sup>	
Pre-Pah Canyon Tuff bedded tuff	Tppb2	357 <sup>2</sup>	1.5 <sup>2</sup>	
Topopah Spring Tuff (Tpt) — 1005.5 ft thick				
Crystal-rich vitric zone	Tptrv	358.5 <sup>2</sup>	29.8	366.0
nonwelded subzone	Tptrv1	358.5 <sup>2</sup>	22.5	366.0
moderately welded subzone	Tptrv2	381	6.2	
densely welded subzone	Tptrv3	387.2	1.1	387.0
Crystal-rich nonlithophysal zone	Tptrn	388.3	99.5	393.0
Crystal-rich lithophysal zone	Tptrl	--	0.0	--
Crystal transition interval		473.2-487.8	14.8	
Compositional transition		472.2-532.0	59.8	
Crystal-poor upper lithophysal zone	Ttpul	487.8	194.7	490.0
Crystal-poor middle nonlithophysal zone	Ttpmn	682.5	120.8	640.0
Crystal-poor lower lithophysal zone	Ttppl	803.3	216.7	829.0
Crystal-poor lower nonlithophysal zone	Ttppln	1020.0	171.4	1020.0
Crystal-poor vitric zone	Ttpv	1191.4	172.6	1182.1
densely welded subzone	Ttpv3	1191.4	83.1	1182.1
moderately welded subzone	Ttpv2	1274.5	20.5	1274.6
nonwelded subzone	Ttpv1	1295.0	69.0	
Pre-Topopah Spring Tuff bedded tuff	Ttpb1	1364 <sup>2</sup>	41 <sup>2</sup>	1357.0
Calico Hills Formation (Tac) — 221.2 ft thick				
unit 3	Tac3	1405 <sup>2</sup>	88.3 <sup>2</sup>	1381.0
unit 2	Tac2	1493.3	30.5	
unit 1	Tac1	1523.8	43.4	
bedded tuff unit	Tacbt	1567.2	43.1	
basal sandstone unit	Tacbs	1610.3	15.9	
Prow Pass tuff (Tcp) — 554.0 ft				
unit 4	Tcp4	1626.2	28.8	
unit 3	Tcp3	1655.0	182.8	
unit 2	Tcp2	1837.8	40.2	
unit 1	Tcp1	1878.5	289.0	
bedded tuff unit	Tcpbt	2167.5	12.7	
Bullfrog Tuff (Tcb) — 417.8 ft				
unit 4	Tcb4	2180.2	37.8	
unit 3	Tcb3	2218.0 <sup>1</sup>	260.0 <sup>1</sup>	

10 Geology of the USW SD-7 Drill Hole, Yucca Mountain, Nevada

Table 3: Stratigraphic Unit Upper Contacts and Unit Thicknesses for the USW SD-7 Drill Hole  
(Continued)

Lithostratigraphic Unit	Abbreviation	Depth to Upper Contact (ft)	Apparent thickness (ft)	Tops from Stratigraphic Compendium (ft)
unit 2	Tcb2	2478.0 <sup>1</sup>	3.5 <sup>1</sup>	
unit 1	Tcb1	2481.5	97.9	
tuffaceous sandstone unit	Tcbts	2579.4	18.6	
Tram Tuff (Tct) — 77.1 ft <sup>1</sup>				
upper ash-flow unit		2598.0	77.1 <sup>1</sup>	

<sup>1</sup> Entire unit not penetrated; partial thickness only.<sup>2</sup> Extremely poor core recovery in this general interval makes it impossible to determine exact contacts, or in some cases, the presence/absence of units; contacts have been inferred through interpretation of petrophysical logs. See geologic log sheets in Appendix B for interpretation and detailed descriptions of available evidence.<sup>3</sup> Fault contact; partial thickness only.Drill hole: UE-25 UZ #16  
Data Tracking Number: GS931208314211.047

Zones of welding (W)

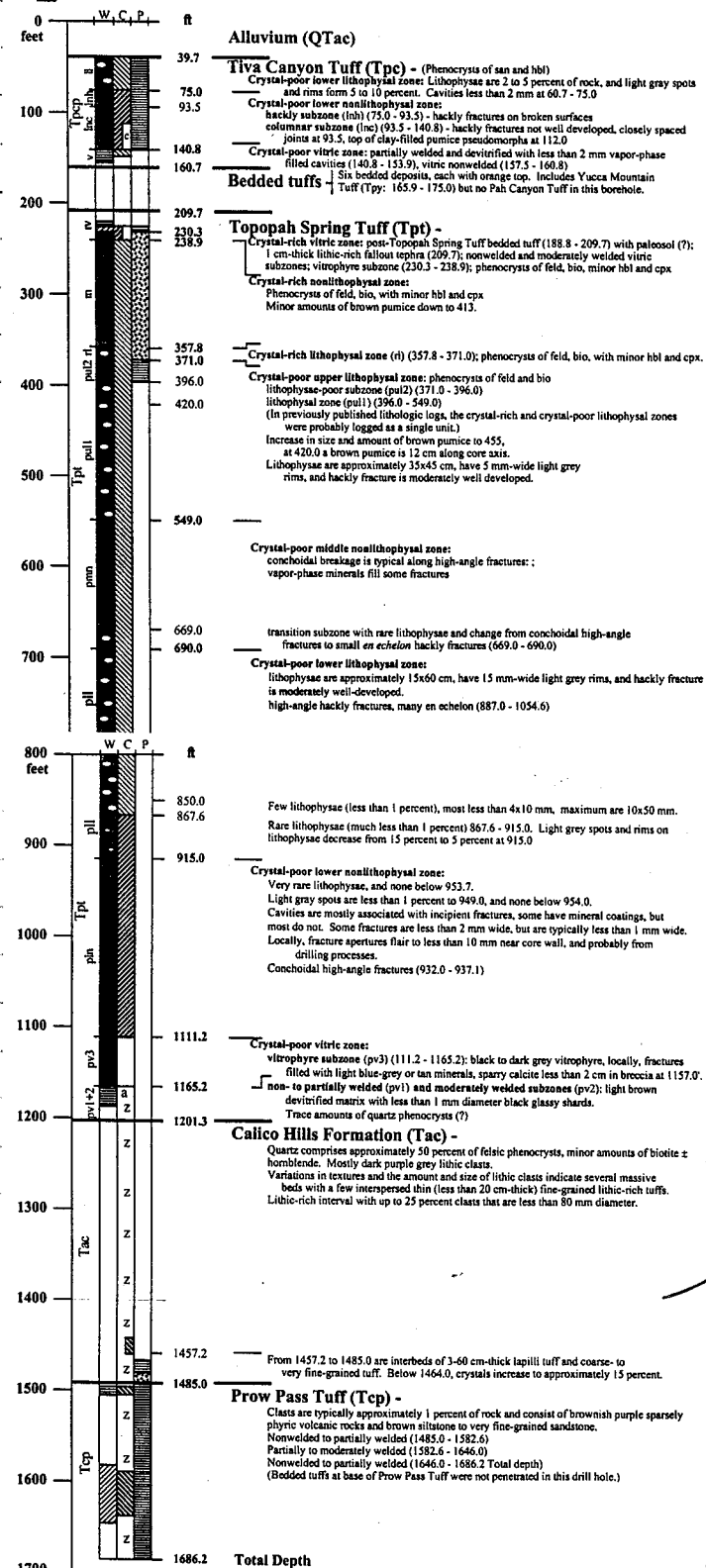
- ☒ Moderately to Densely (o-lithophysae)  
☒ Partially to Moderately  
☒ Non-to Partially  
☐ Nonwelded

Zones of crystallization (C)

- ☒ Devitrified / Devit. + vapor-phase mins.  
☒ Vitric / Vitric + vapor-phase mins.  
☒ Altered (a) / to clay (c) / to zeolite (z)

Phenocryst content (P)

- ☒ greater than 10 percent  
☒ 5 - 10 percent  
☐ less than 5 percent



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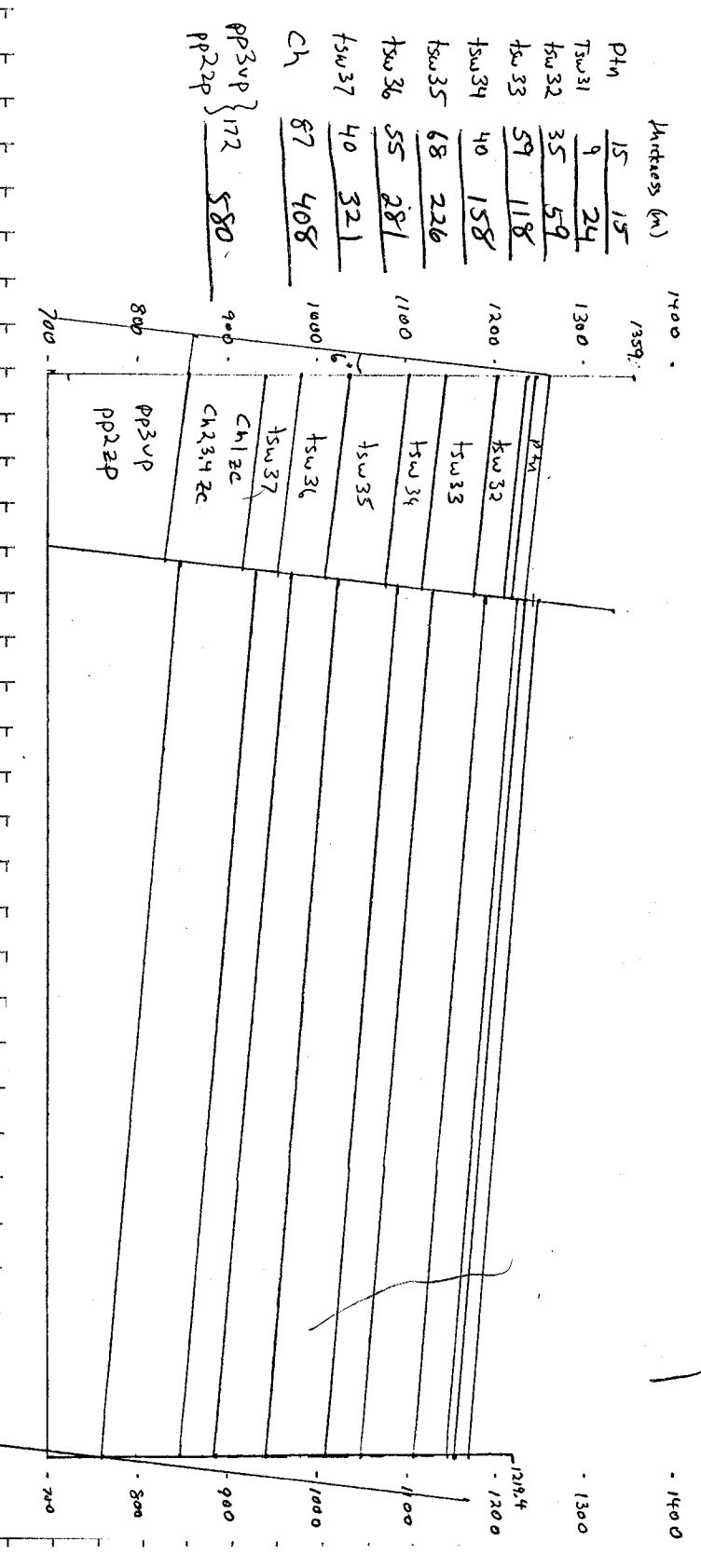
Recorded by

Date

Sept 1, 1999

From Page No.

Rattman, Christopher A. & Dale A. Engstrom, Geology of the USW SD-7  
 Drill Hole, Yucca Mountain, Nevada, Sandra Report SM096-1474  
 UC-814, Sept. 1996 Sandra Rattman, Albuquerque NM  
 Geslin, Jeffrey K., Thomas C. Meyer, & David C. Buesch, Summary of  
 Hydrologic Logging of New and Existing Boreholes at Yucca Mountain,  
 Nevada, Aug 1993 to Feb 1994 US Geological Survey Open-File  
 Report 94-342, Denver CO 1995



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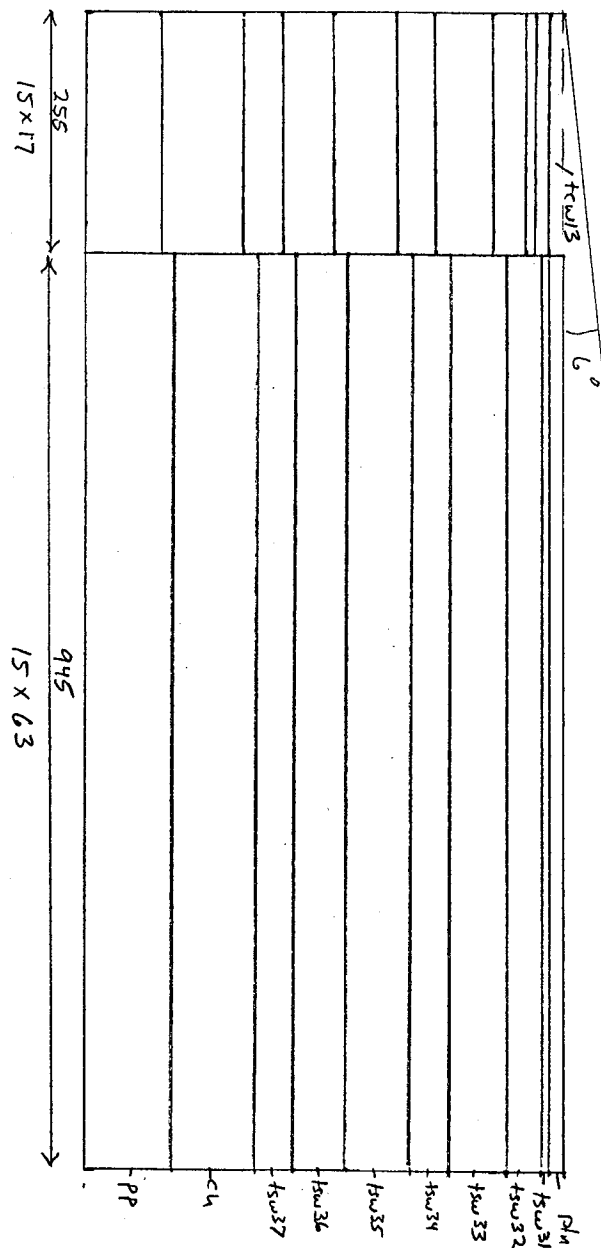
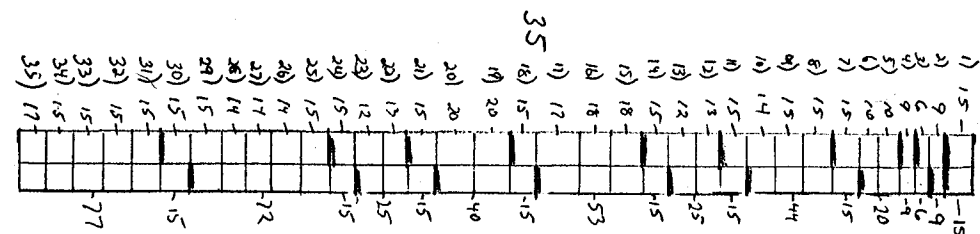
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Sept 1  
1999

TITLE

ENFE Akrotiri

From Page No.

Check on MULTIFLO 1-D simulations using SWMS-3D

Minean Ash

$$K_s = 1.7e-4 \frac{m}{s} \quad \rightarrow = 14.688 \frac{m}{day}$$

$$K_s = \frac{R \rho_g}{\mu}$$

$$R = \frac{K_s \mu}{\rho_g} = \frac{1.7e-4 \frac{m}{s} \cdot 0.1119 \frac{g}{cm^3} \cdot \frac{100 cm}{m}}{998.3 \frac{kg}{m^3} \cdot \frac{1000 g}{kg} \cdot \frac{9.8 m}{s^2}} = 1.944e-11 m^2$$

$$\alpha = .4904 m^{-1} \frac{m^3}{s^2} = 5.01e-5 Pa^{-1}$$

$$n = 1.4 \quad A = 1 - \frac{1}{n} \quad m = \frac{1}{1-n} \quad m = 1 - \frac{1}{n} = .2857$$

$$S_r = .02 \quad \phi = .6 \quad \theta_r = S_r \phi = .012$$

$$K_d = .0027 \frac{m^3}{kg} \cdot \frac{kg}{1000 g} = 2.7e-6 \frac{m^3}{g}$$

Packed Earth

$$K_s = 1.0e-7 \frac{m}{s} = 8.64e-3 \frac{m}{d}$$

$$R = 1.144e-14 m^2 \quad n = 1.13 \quad m = .0115$$

$$\alpha = 2.7 m^{-1} = 2.76e-4 Pa^{-1} \quad S_r = 0.1 \quad \phi = .3 \quad \theta_r = .03$$

$$K_d = 0.45 \frac{m^3}{kg} = 4.5e-4 \frac{m^3}{g}$$

$$Cape Riva \quad K_s = 1.5e-4 \frac{m}{s} = 12.96 \frac{m}{d}$$

$$R = 1.716e-11 m^2 \quad n = 1.7 \quad m = .4118$$

$$\alpha = .6865 m^{-1} = 7.02e-5 Pa^{-1} \quad S_r = .02 \quad \phi = .52 \quad \theta_r = .0104$$

$$K_d = .0027 \frac{m^3}{kg} = 2.7e-6 \frac{m^3}{g}$$

To Page No.

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Invented by

Recorded by

Date

Sept 17  
1999



From Page No. EQ 3/6 Run  $\text{Cu}^{2+}$  in Equilibrium with Atacamite =  $4.67 \times 10^{-5}$  moles/kg

1-D MULTIFLO RUN TO 30 years 15 cm/yr recharge  
no sorption

In the source term blocks  $\text{Cu}^{2+} = 4.829 \times 10^{-5}$  moles/kg

$\frac{C}{C_0} = 0.5$  Front at  $z = 17.1$  m here's error in SE causing the  
Transport distance  $17.1 - 1.48 = 15.62$  m all Sept 21/99 results

1-D SWMS-3D Run to 30 years 15 cm/yr recharge  
no sorption

Source term B.C.  $4.67 \times 10^{-5} \frac{\text{mole}}{\text{kg}}$   $\frac{\text{kg}}{1000 \text{ g}}$   $\frac{998.3 \text{ kg}}{\text{m}^3}$   $\frac{1000 \text{ g}}{\text{kg}}$   $\frac{63.546 \text{ g}}{\text{mole}}$   
 $= 2.96 \text{ g/m}^3$  EDP 8/24/00 I HAVE NOW increased the quality of this record. EDP 8/21/00

$\text{Cu}_2\text{Cl}(\text{OH})_3$  Atacamite

$\frac{2(63.546)}{35.453}$  Murphy  $(15 \text{ cm}) (\text{m}^2) (\frac{100 \text{ cm}}{\text{m}})^2 1 \times 10^{-5} \text{ mole L}$   $\frac{3600 \text{ y}}{1000 \text{ cm}^3}$   
 $\frac{3(15.9994)}{3(1.0079)}$   
 $= 5.4 \text{ mole Cu} = 576.6 \text{ g Atacamite per sq meter}$

$213.55 \text{ g/mole}$   $(15 \text{ cm}) (\text{m}^2) (\frac{100 \text{ cm}}{\text{m}})^2 (\frac{1.9983 \text{ g}}{\text{cm}^3}) (\frac{\text{kg}}{1000 \text{ g}}) (4.67 \times 10^{-5} \frac{\text{mole}}{\text{kg}}) 3570 \text{ yr}$   
 $= 25 \text{ mole Cu} = 2669 \text{ g Atacamite per sq meter}$

Source Footprint  $4(1.2 \text{ m})(1.2 \text{ m}) = 1/6 \text{ m}^2 = 427 \text{ g Atacamite}$

To Page No.

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Date

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Date

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D11

Sept 22  
1999

From Page No. Final Vol. Fraction from mult flo at 3600 y

0.002 block vol  $\text{m}^3$   
Initial Volume fraction of atacamite

0.1	0.1	0.1	0.1
0.1	0.1	0.1	0.1
0.1	0.1	0.1	0.1
0.1	0.1	0.1	0.1
0.1	0.1	0.1	0.1
0.1	0.1	0.1	0.1

56.8  $\text{cm}^3/\text{mole}$  213.545 g/mole  
Initial mass in place

751.919	751.919	751.919	751.919
751.919	751.919	751.919	751.919
751.919	751.919	751.919	751.919
751.919	751.919	751.919	751.919
751.919	751.919	751.919	751.919
751.919	751.919	751.919	751.919

Final volume fraction 1.5 cm/yr infiltration

0.09888	0.09956	0.099561	0.099518
0.099374	0.1	0.1	0.099996
0.099375	0.1	0.1	0.099998
0.099375	0.1	0.1	0.099999
0.099377	0.1	0.1	0.1
0.099334	0.099982	0.09989	0.099993

final mass in place

743.4975	748.6106	748.6181	748.2948
747.212	751.919	751.919	751.8889
747.2195	751.919	751.919	751.904
747.2195	751.919	751.919	751.9115
747.2346	751.919	751.919	751.919
746.9112	751.7837	751.0919	751.8664

Final volume fraction 15 cm/yr infiltration

0.091857	0.096945	0.096631	0.096049
0.094748	0.1	0.1	0.099994
0.094721	0.1	0.1	0.099998
0.094693	0.1	0.1	0.099999
0.094666	0.1	0.1	0.1
0.094529	0.099925	0.099949	0.099964

final mass in place

690.6902	728.9479	726.5869	722.2107
712.4282	751.919	751.919	751.8739
712.2252	751.919	751.919	751.904
712.0147	751.919	751.919	751.9115
711.8117	751.919	751.919	751.919
710.7815	751.3551	751.5355	751.6483

mass loss 43.52107

8.421493	3.308444	3.300924	3.62425
4.707013	0	0	0.030077
4.699494	0	0	0.015038
4.699494	0	0	0.007519
4.684455	0	0	0
5.007781	0.135345	0.827111	0.052634

mass loss 340.8599

61.22877	22.97113	25.33215	29.70832
39.49079	0	0	0.045115
39.6938	0	0	0.015038
39.90434	0	0	0.007519
40.10736	0	0	0
41.13749	0.563939	0.383479	0.270691

7.832066

D11

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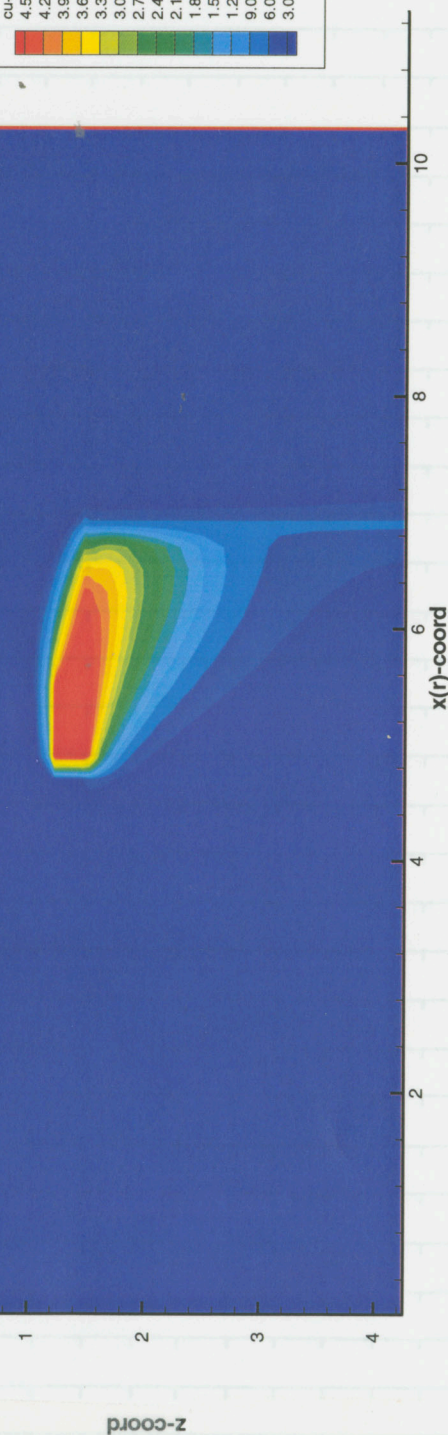
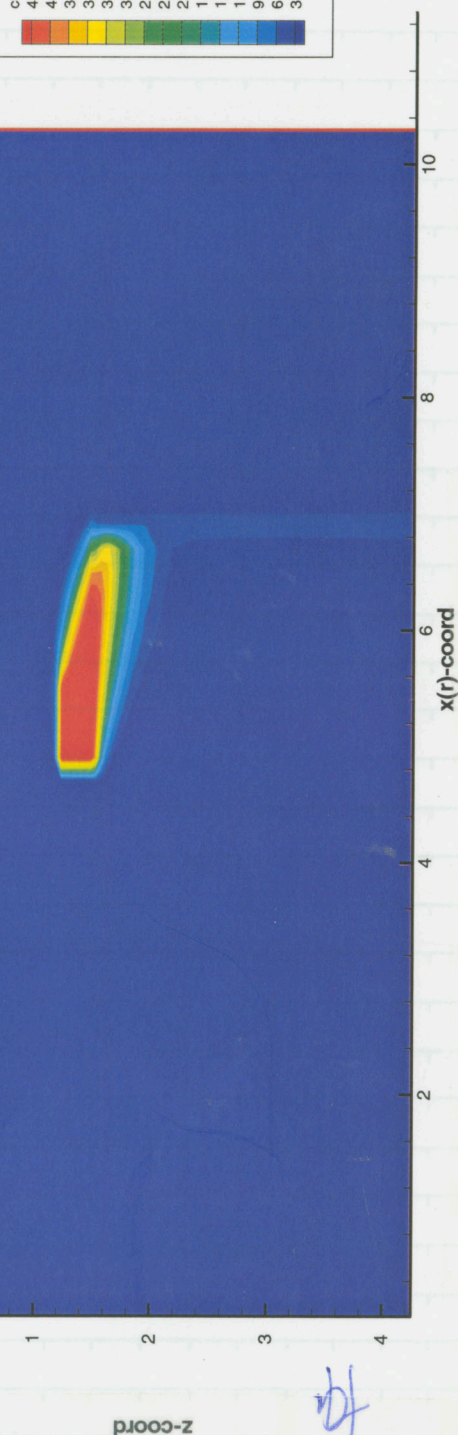
Recorded by

D11

Sept 23  
1999



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Cu<sup>2+</sup> at 3600 yr with 1.5cm/yr infiltrationCu<sup>2+</sup> at 3600 yr with 15cm/yr infiltration

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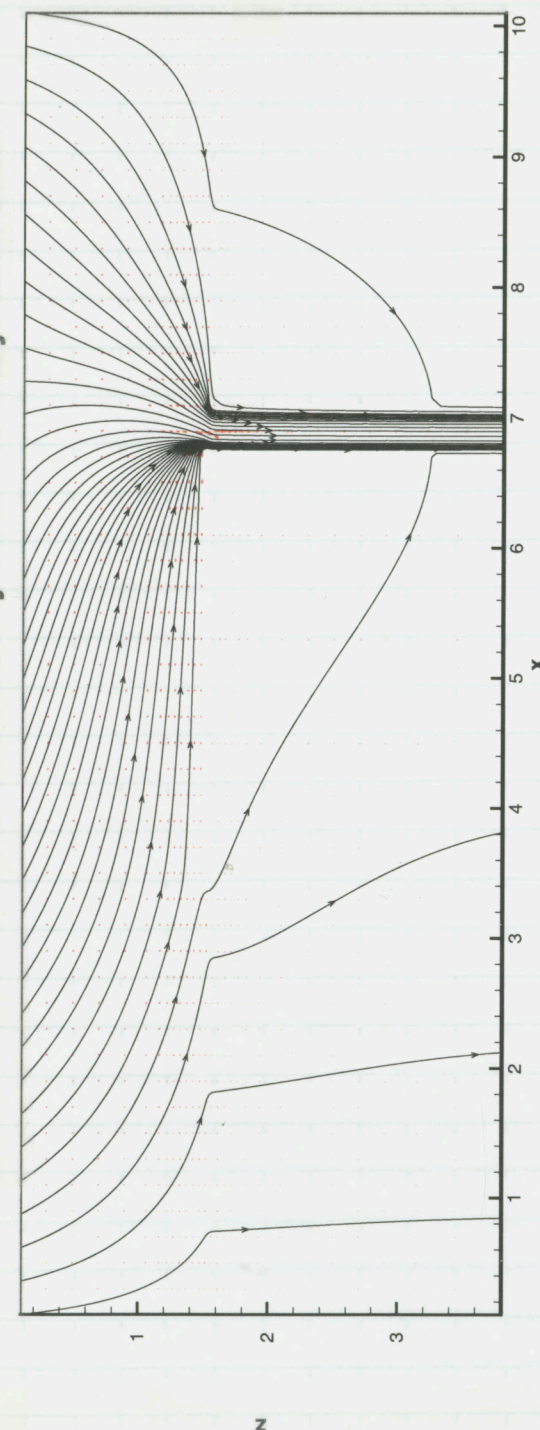
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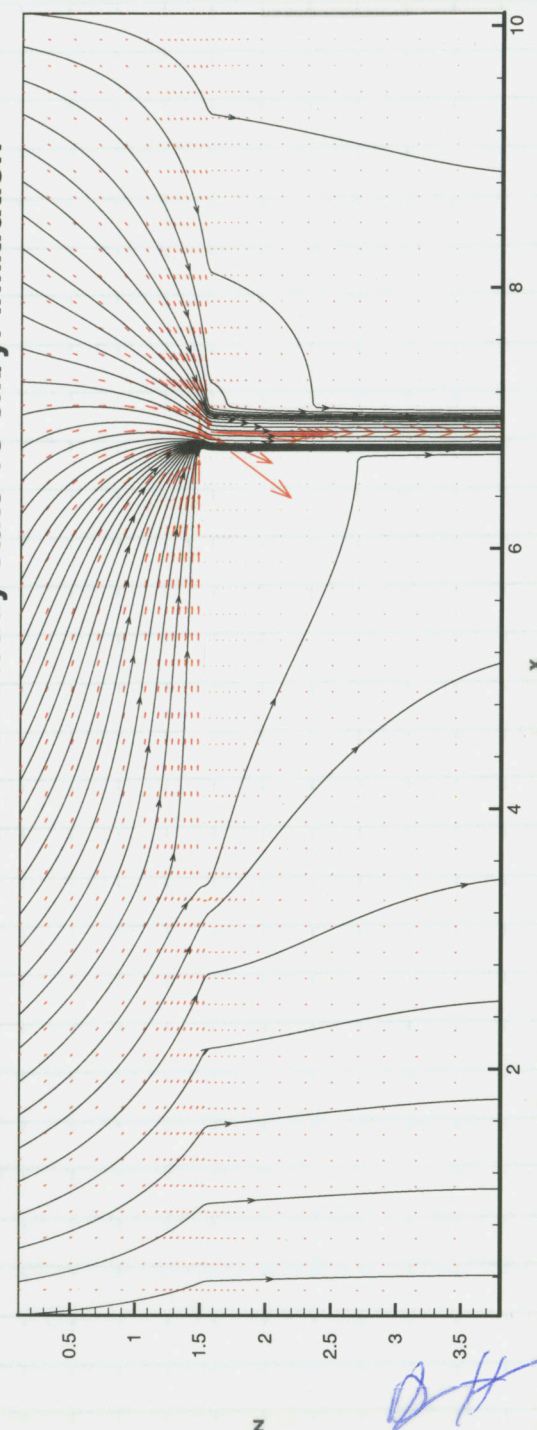
ENFE Akrotiri

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flux vectors and streamlines steady state 1.5 cm/yr infiltration



flux vectors and streamlines steady state 15 cm/yr infiltration



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Hughson, D.L., L. Browning, W.M. Murphy, and R. Green. "An Archeological Site at Akrotiri, Greece, as a Natural Analog for Radionuclide Transport: Implications for Validity of Performance Assessments." Proceedings of the Scientific Basis for Nuclear Waste Management XXIII. D. Shoesmith and R. Smith, eds. Materials Research Society. 1999.

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		Recorded by <i>DH</i>	<i>Oct 28 1999</i>	

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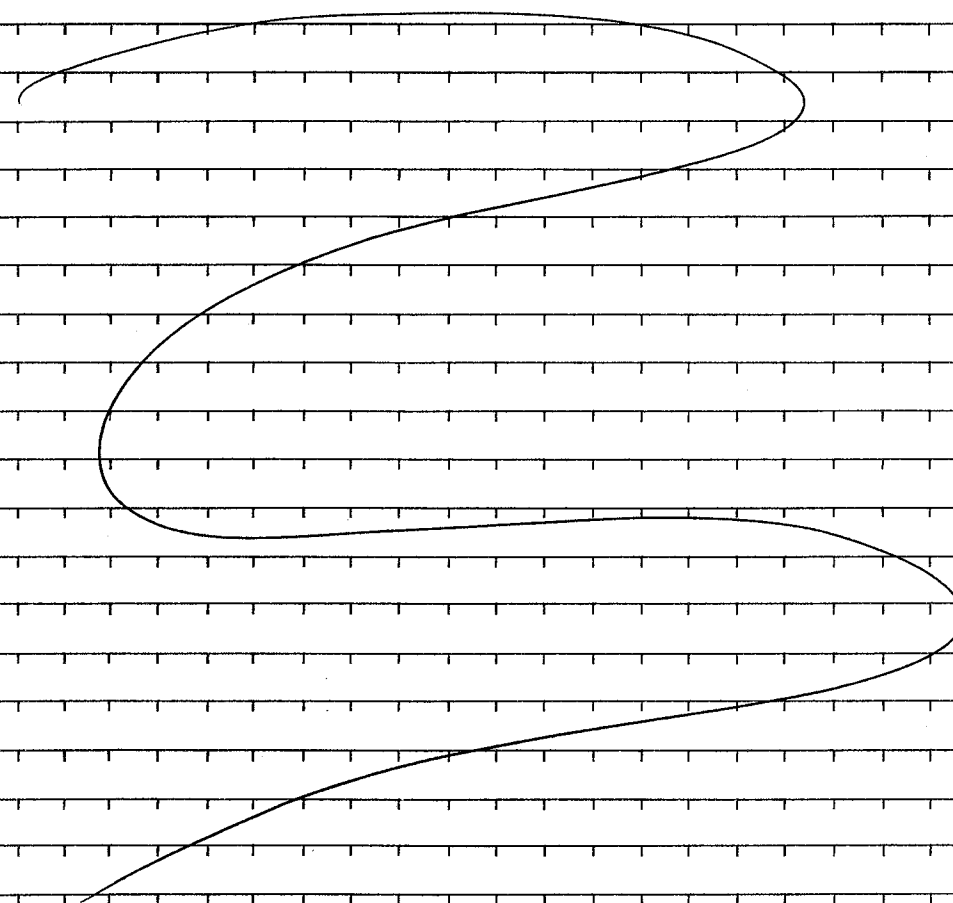
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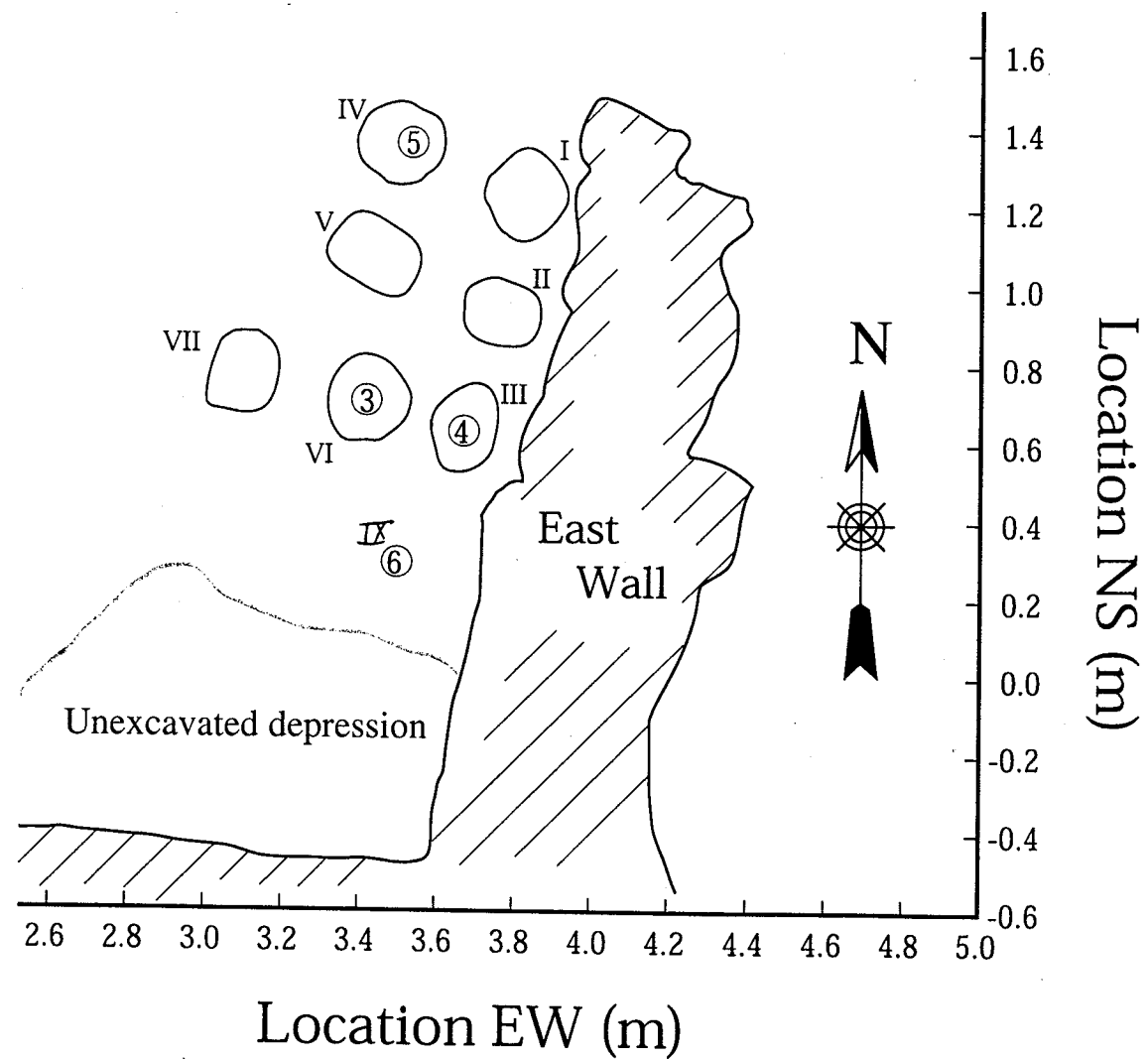
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2000

Following pages are some  
odds & ends of graphs  
& diagrams that I used  
but did not paste into  
this notebook in sequence





From Page No.



Location EW (m)

Sample Hole Locations

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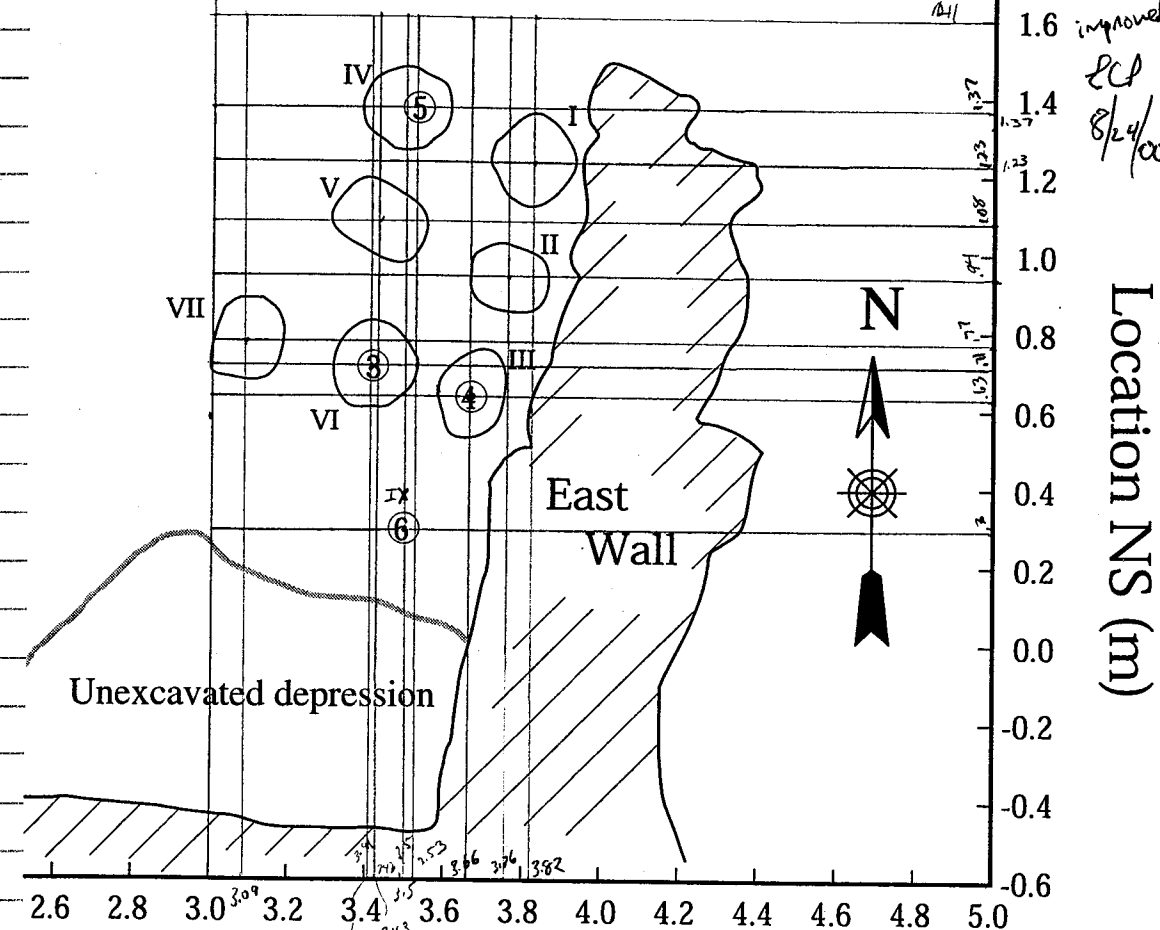
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HOLE	X	Y	m Elev. top	cm Δ paked earth	Ref
I	3.82	1.23	22.55	4.5 22.51	18.05
II	3.76	0.94	22.52	6.0 22.46	16.52
III	3.66	0.63	22.49	2.0 22.47	20.49
IV	3.53	1.37	22.59	3.5 22.56	19.09
V	3.43	1.08	22.54	2.0 22.52	20.54
VI	3.41	0.71	22.50	0 22.5	22.50
VII	3.09	0.77	22.50	0 22.5	22.50
IX	3.5	0.3	22.47	3.0 22.44	19.47



Location EW (m)

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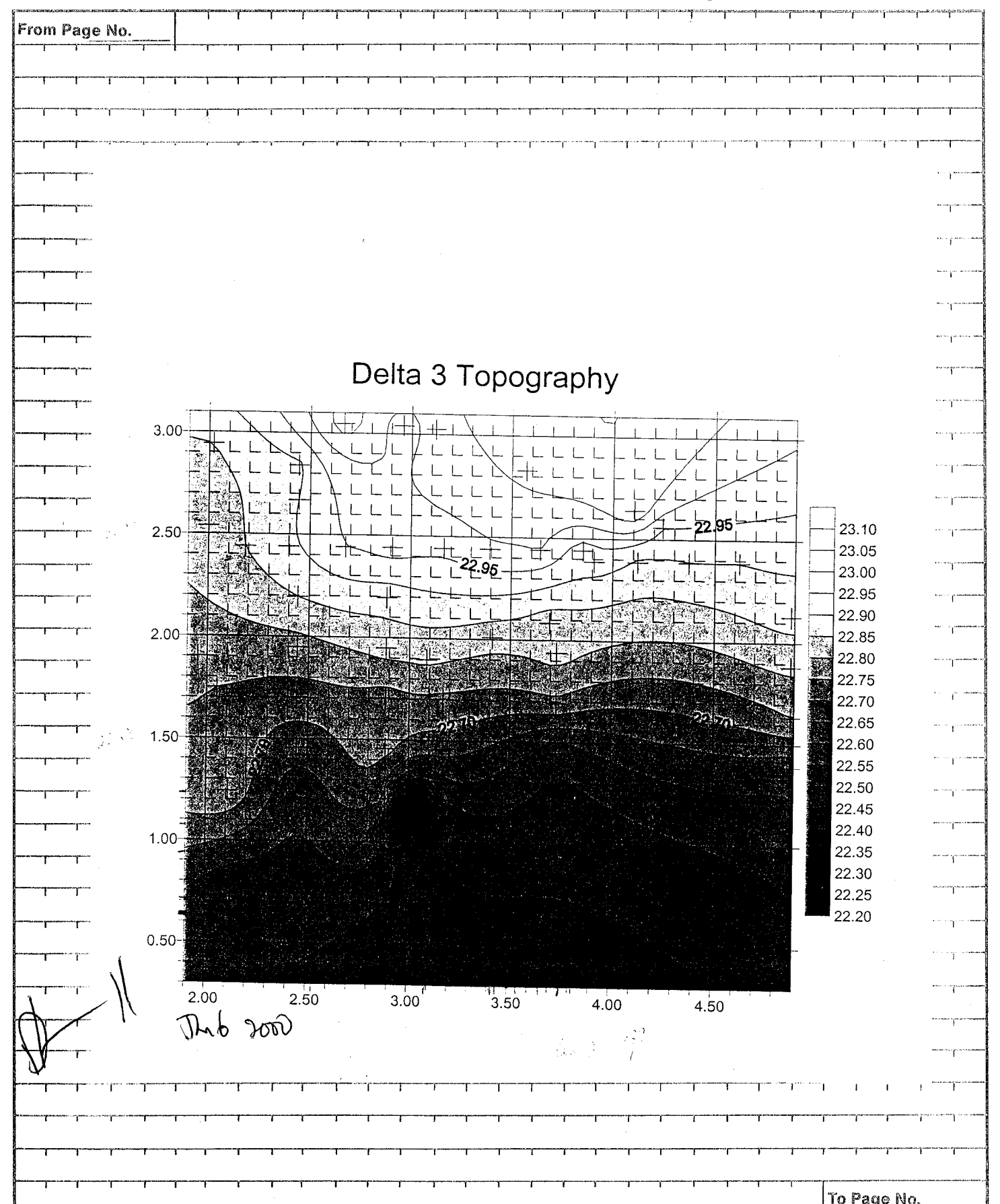
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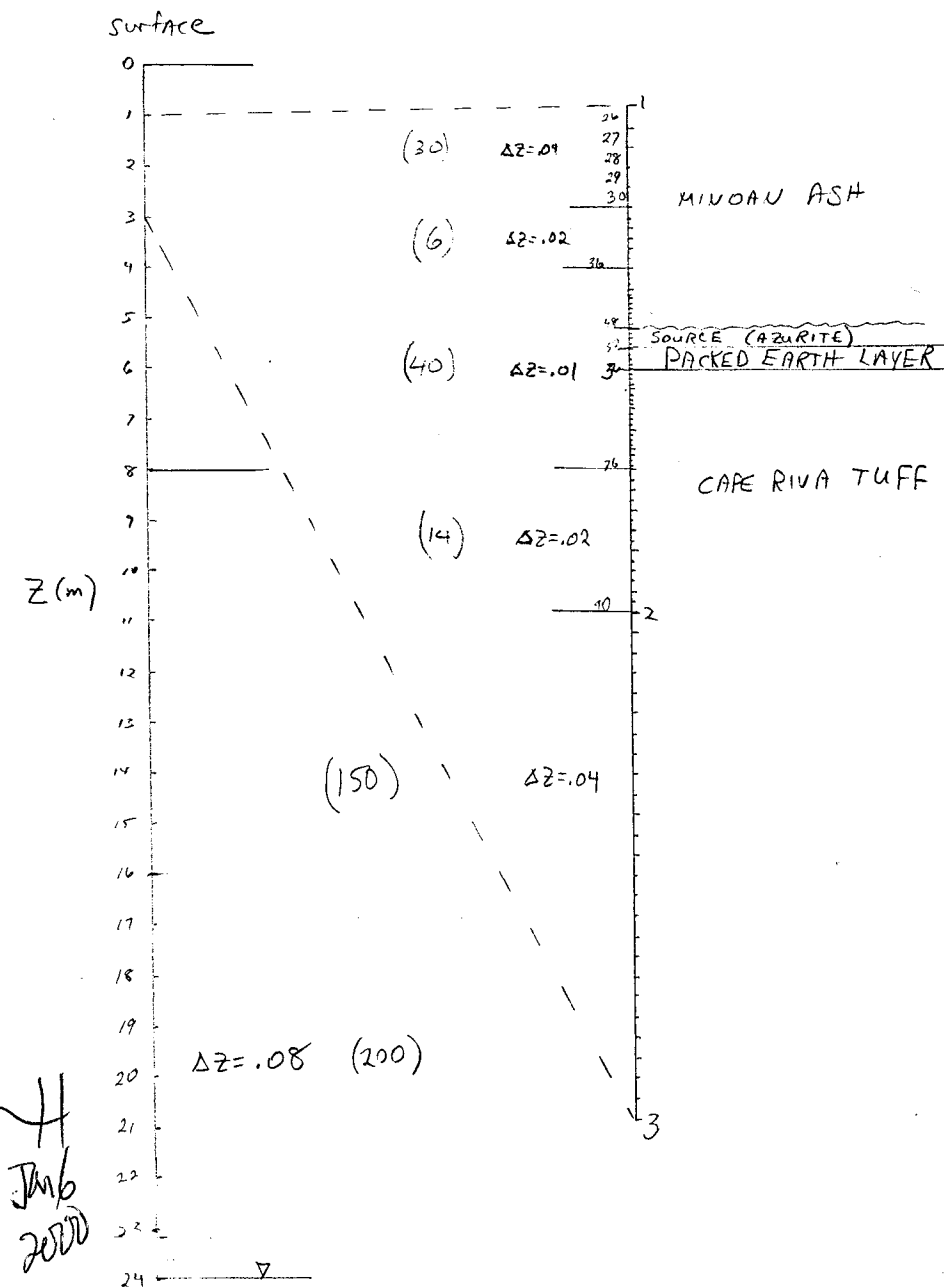
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1-D Grid

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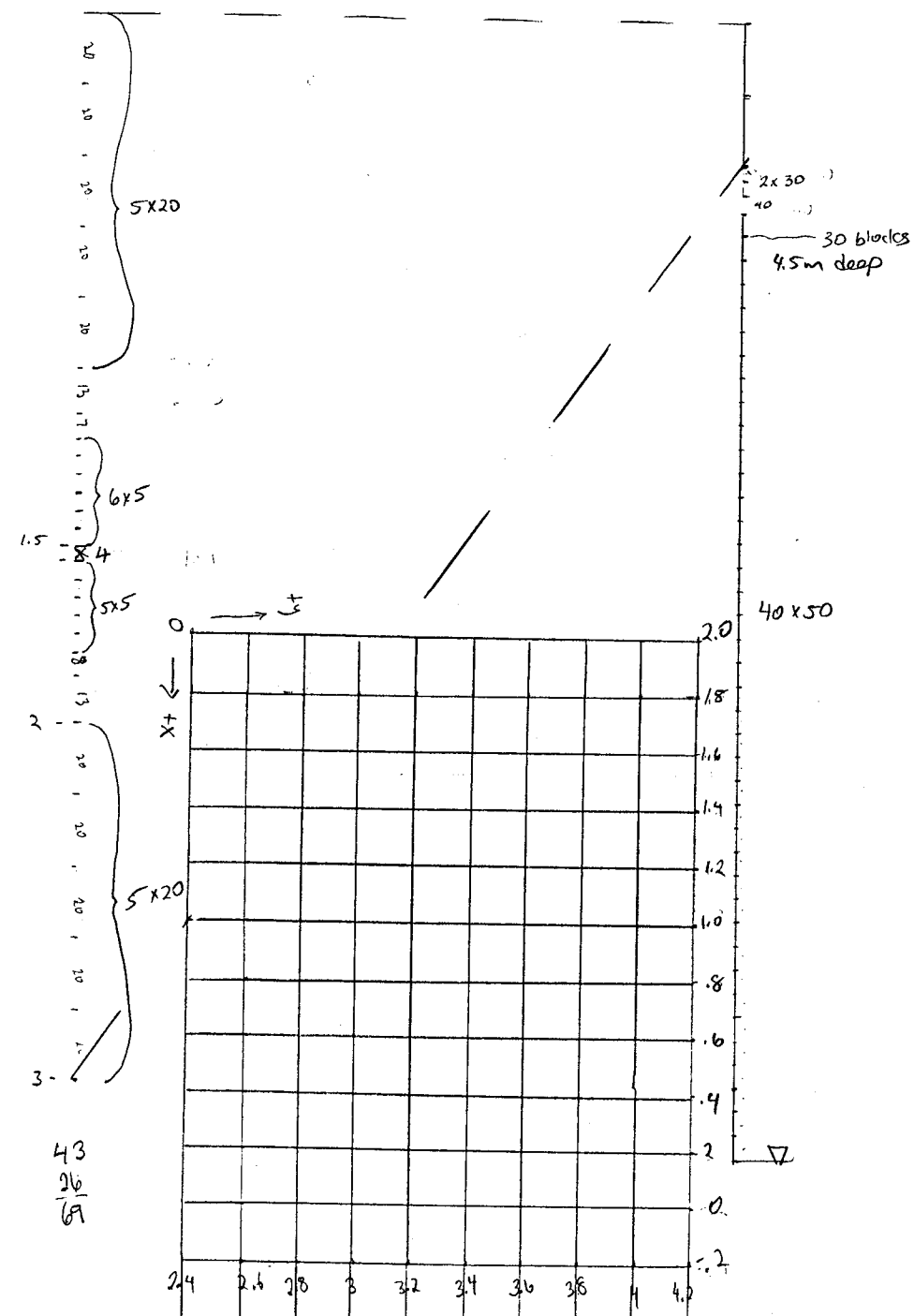
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Debra.30

## --- Distribution of Aqueous Species ---

Species	Molality	Log molality	Log gamma	Log activity
Na+	9.9494E-03	-2.0022	-0.0487	-2.0509
Cl-	7.7363E-03	-2.1115	-0.0465	-2.1580
HCO3-	1.7033E-03	-2.7687	-0.0450	-2.8138
SO4--	4.7220E-04	-3.3259	-0.1852	-3.5111
O2(aq)	2.5149E-04	-3.5995	0.0012	-3.5983
SiO2(aq)	1.0016E-04	-3.9993	0.0000	-3.9993
K+	9.9750E-05	-4.0011	-0.0502	-4.0513
Ca++	9.5246E-05	-4.0212	-0.1816	-4.2028
Mg++	9.3063E-05	-4.0312	-0.1719	-4.2032
CO2(aq)	3.3879E-05	-4.4701	0.0012	-4.4689
NaSO4-	2.0095E-05	-4.6969	-0.0450	-4.7420
NaHCO3(aq)	1.9474E-05	-4.7106	0.0000	-4.7106
CO3--	1.0890E-05	-4.9630	-0.1796	-5.1426
NaCl(aq)	1.0330E-05	-4.9859	0.0000	-4.9859
MgSO4(aq)	4.9827E-06	-5.3025	0.0000	-5.3025
CaSO4(aq)	2.4961E-06	-5.6027	0.0000	-5.6027
HSiO3-	1.2390E-06	-5.9069	-0.0450	-5.9520
CaHCO3+	1.1991E-06	-5.9211	-0.0487	-5.9698
MgHCO3+	1.1681E-06	-5.9325	-0.0487	-5.9812
OH-	1.1253E-06	-5.9487	-0.0465	-5.9953
CaCO3(aq)	9.5888E-07	-6.0182	0.0000	-6.0182
NaHSiO3(aq)	4.4223E-07	-6.3544	0.0000	-6.3544
MgCO3(aq)	4.2971E-07	-6.3668	0.0000	-6.3668
MgCl+	3.5696E-07	-6.4474	-0.0487	-6.4961
NaCO3-	2.3227E-07	-6.6340	-0.0450	-6.6791
KSO4-	2.3031E-07	-6.6377	-0.0450	-6.6827
CaCl+	9.8246E-08	-7.0077	-0.0487	-7.0564
KCl(aq)	1.9776E-08	-7.7039	0.0000	-7.7039
H+	1.1027E-08	-7.9576	-0.0424	-8.0000
NaOH(aq)	1.4261E-09	-8.8459	0.0000	-8.8459
CaOH+	9.9028E-10	-9.0042	-0.0487	-9.0529
CaCl2(aq)	6.8806E-10	-9.1624	0.0000	-9.1624
HSO4-	3.2590E-10	-9.4869	-0.0450	-9.5320
KOH(aq)	3.0802E-11	-10.5114	0.0000	-10.5114
H2SiO4--	1.6810E-11	-10.7744	-0.1852	-10.9596
HCl(aq)	1.4859E-11	-10.8280	0.0000	-10.8280
H6(H2SiO4)4--	3.5216E-14	-13.4533	-0.1852	-13.6384
KHSO4(aq)	1.7835E-15	-14.7487	0.0000	-14.7487
ClO-	9.6927E-20	-19.0136	-0.0450	-19.0586
H4(H2SiO4)4----	6.4707E-20	-19.1890	-0.7494	-19.9384
HClO(aq)	3.2404E-20	-19.4894	0.0000	-19.4894
CuCl2-	7.2636E-21	-20.1388	-0.0450	-20.1839
H2SO4(aq)	2.9379E-21	-20.5320	0.0000	-20.5320
Cu+	2.2887E-21	-20.6404	-0.0487	-20.6891
CuCl3--	4.4771E-22	-21.3490	-0.1852	-21.5342
HO2-	8.7859E-23	-22.0562	-0.0450	-22.1013
Mg4(OH)4++++	1.4711E-24	-23.8324	-0.7310	-24.5633
ClO3-	1.6933E-25	-24.7713	-0.0450	-24.8163
ClO4-	9.6124E-26	-25.0172	-0.0465	-25.0637
ClO2-	1.5162E-29	-28.8193	-0.0450	-28.8643
HSO5-	2.8072E-31	-30.5517	-0.0450	-30.5968
HClO2(aq)	2.0207E-34	-33.6945	0.0000	-33.6945
Formate	1.6788E-44	-43.7750	-0.0450	-43.8201
H2(aq)	4.9110E-45	-44.3088	0.0012	-44.3077
S2O8--	7.3134E-48	-47.1359	-0.1852	-47.3211
Formic acid(aq)	8.5693E-49	-48.0671	0.0000	-48.0671
SO3--	7.0619E-49	-48.1511	-0.1852	-48.3363

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HSO3-	8.2069E-50	-49.0858	-0.0450	-49.1309
CO(aq)	1.9289E-51	-50.7147	0.0000	-50.7147
H2SO3(aq)	7.5325E-56	-55.1231	0.0000	-55.1231
SO2(aq)	5.3641E-56	-55.2705	0.0000	-55.2705
S2O6--	3.4867E-73	-72.4576	-0.1852	-72.6428
Formaldehyde(aq)	1.6297E-94	-93.7879	0.0000	-93.7879
S2O5--	1.2768E-103	-102.8939	-0.1852	-103.0791
Methanol(aq)	4.7741E-124	-123.3211	0.0000	-123.3211
S2O4--	1.2715E-136	-135.8957	-0.1852	-136.0809
HS-	2.6012E-143	-142.5848	-0.0465	-142.6314
H2S(aq)	2.2716E-144	-143.6437	0.0000	-143.6437
S--	4.1564E-148	-147.3813	-0.1852	-147.5665
Methane(aq)	1.7440E-148	-147.7585	0.0000	-147.7585
S2O3--	6.6133E-150	-149.1796	-0.1852	-149.3648
Acetate	7.3237E-154	-153.1353	-0.0450	-153.1803
NaCH3COO(aq)	4.6280E-156	-155.3346	0.0000	-155.3346
MgCH3COO+	8.7965E-157	-156.0557	-0.0487	-156.1044
HS2O3-	4.9462E-157	-156.3057	-0.0450	-156.3508
CaCH3COO+	3.9491E-157	-156.4035	-0.0487	-156.4522
Acetic acid(aq)	3.7748E-157	-156.4231	0.0000	-156.4231
KCH3COO(aq)	3.1954E-158	-157.4955	0.0000	-157.4955
CuCH3COO(aq)	2.8866E-174	-173.5396	0.0000	-173.5396
S3O6--	5.5477E-182	-181.2559	-0.1852	-181.4411
Acetaldehyde(aq)	1.0020E-201	-200.9991	0.0000	-200.9991
Ethyne(aq)	9.6393E-223	-222.0160	0.0000	-222.0160
Ethanol(aq)	1.0610E-235	-234.9743	0.0000	-234.9743
Ethylene(aq)	3.6324E-240	-239.4398	0.0000	-239.4398
S2--	2.4588E-254	-253.6093	-0.1852	-253.7945
Ethane(aq)	2.9042E-264	-263.5370	0.0000	-263.5370
Propanoate	1.4920E-267	-266.8262	-0.0450	-266.8713
Propanoic acid(aq)	1.0246E-270	-269.9895	0.0000	-269.9895
S4O6--	7.1122E-275	-274.1480	-0.1852	-274.3332
Ca(CH3COO)2(aq)	3.7119E-309	-308.4304	0.0000	-308.4304
Mg(CH3COO)2(aq)	3.0033E-309	-308.5224	0.0000	-308.5224
Na(CH3COO)2-	1.4094E-309	-308.8510	-0.0450	-308.8960
Acetone(aq)	1.2489E-310	-309.9035	0.0000	-309.9035
K(CH3COO)2-	7.1805E-312	-311.1438	-0.0450	-311.1889
Propanal(aq)	0.0000E+00	-314.1329	0.0000	-314.1329
Cu(CH3COO)2-	0.0000E+00	-326.7042	-0.0450	-326.7492
1-Propyne(aq)	0.0000E+00	-331.6680	0.0000	-331.6680
1-Propanol(aq)	0.0000E+00	-348.6065	0.0000	-348.6065
1-Propene(aq)	0.0000E+00	-350.9024	0.0000	-350.9024
S3--	0.0000E+00	-359.9154	-0.1852	-360.1006
Propane(aq)	0.0000E+00	-377.5380	0.0000	-377.5380
Butanoate	0.0000E+00	-381.0009	-0.0450	-381.0459
Butanoic acid(aq)	0.0000E+00	-384.2227	0.0000	-384.2227
Ethylacetate(aq)	0.0000E+00	-392.9382	0.0000	-392.9382
S5O6--	0.0000E+00	-395.9206	-0.1852	-396.1058
2-Butanone(aq)	0.0000E+00	-423.7923	0.0000	-423.7923
Butanal(aq)	0.0000E+00	-429.6637	0.0000	-429.6637
1-Butyne(aq)	0.0000E+00	-445.8355	0.0000	-445.8355
1-Butanol(aq)	0.0000E+00	-463.4483	0.0000	-463.4483
1-Butene(aq)	0.0000E+00	-465.2530	0.0000	-465.2530
S4--	0.0000E+00	-466.4415	-0.1852	-466.6267
n-Butane(aq)	0.0000E+00	-491.5946	0.0000	-491.5946
Pentanoate	0.0000E+00	-495.0657	-0.0450	-495.1108
Pentanoic acid(aq)	0.0000E+00	-498.2656	0.0000	-498.2656
2-Pentanone(aq)	0.0000E+00	-538.0989	0.0000	-538.0989
Phenol(aq)	0.0000E+00	-543.0657	0.0000	-543.0657
Pentanal(aq)	0.0000E+00	-543.5012	0.0000	-543.5012
1-Pentyne(aq)	0.0000E+00	-559.9881	0.0000	-559.9881
S5--	0.0000E+00	-573.1874	-0.1852	-573.3726
Benzene(aq)	0.0000E+00	-575.3968	0.0000	-575.3968
1-Pentanol(aq)	0.0000E+00	-576.3109	0.0000	-576.3109

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1-Pentene(aq)	0.0000E+00	-579.4277	0.0000	-579.4277
o-Phthalate	0.0000E+00	-586.1704	-0.1852	-586.3556
Na(o-Phthalate)-	0.0000E+00	-587.6614	-0.0450	-587.7065
Ca(o-Phthalate)(aq)	0.0000E+00	-588.1383	0.0000	-588.1383
H(o-Phthalate)-	0.0000E+00	-588.9025	-0.0450	-588.9476
o-Phthalic acid(aq)	0.0000E+00	-593.9976	0.0000	-593.9976
n-Pentane(aq)	0.0000E+00	-605.7210	0.0000	-605.7210
Hexanoate	0.0000E+00	-609.2330	-0.0450	-609.2780
Hexanoic acid(aq)	0.0000E+00	-612.4182	0.0000	-612.4182
2-Hexanone(aq)	0.0000E+00	-652.0904	0.0000	-652.0904
Hexanal(aq)	0.0000E+00	-657.6832	0.0000	-657.6832
1-Hexyne(aq)	0.0000E+00	-674.2362	0.0000	-674.2362
Toluene(aq)	0.0000E+00	-686.7127	0.0000	-686.7127
1-Hexanol(aq)	0.0000E+00	-691.0867	0.0000	-691.0867
1-Hexene(aq)	0.0000E+00	-693.4118	0.0000	-693.4118
n-Hexane(aq)	0.0000E+00	-719.9909	0.0000	-719.9909
Heptanoate	0.0000E+00	-723.3344	-0.0450	-723.3795
Heptanoic acid(aq)	0.0000E+00	-726.4244	0.0000	-726.4244
2-Heptanone(aq)	0.0000E+00	-766.1845	0.0000	-766.1845
Heptanal(aq)	0.0000E+00	-772.7375	0.0000	-772.7375
1-Heptyne(aq)	0.0000E+00	-788.5208	0.0000	-788.5208
Ethylbenzene(aq)	0.0000E+00	-800.9021	0.0000	-800.9021
1-Heptanol(aq)	0.0000E+00	-806.2362	0.0000	-806.2362
1-Heptene(aq)	0.0000E+00	-807.5279	0.0000	-807.5279
n-Heptane(aq)	0.0000E+00	-834.0850	0.0000	-834.0850
Octanoate	0.0000E+00	-837.4285	-0.0450	-837.4735
Octanoic acid(aq)	0.0000E+00	-840.2985	0.0000	-840.2985
2-Octanone(aq)	0.0000E+00	-880.2785	0.0000	-880.2785
Octanal(aq)	0.0000E+00	-886.1939	0.0000	-886.1939
1-Octyne(aq)	0.0000E+00	-902.6736	0.0000	-902.6736
n-Propylbenzene(aq)	0.0000E+00	-914.7616	0.0000	-914.7616
1-Octanol(aq)	0.0000E+00	-920.1104	0.0000	-920.1104
1-Octene(aq)	0.0000E+00	-921.7832	0.0000	-921.7832
n-Octane(aq)	0.0000E+00	-948.2230	0.0000	-948.2230

\*\*\*\*\*

Version level= 7.2 (xcon3)  
EQ3NR input file name= Debra.3i

Akrotiri Water Composition  
Computations by Lauren Browning 6-29-99

Temperature (C) | 25.00 | Density(gm/cm3) | 1.00000

Total Dissolved Salts | | mg/kg | mg/l | \*not used

Electrical Balancing on | Cl- | code selects | not performed |

SPECIES	BASIS SWITCH/CONSTRAINT	CONC/ETC	UNITS OR TYPE
redox		-7	Logf02
H+		8.0	pH
Ca++		1e-4	molality
Mg++		1e-4	molality
Na+		0.01	molality
SiO2(aq)	Quartz		mineral
HCO3-	CO2(g)	-3	log fugacity
Cl-		1e-2	molality
K+		1e-4	molality
SO4--		5e-4	molality
Cu+		1e-20	molality

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Step # 40 Xi = 0.4000

Temperature = 25.0 C Pressure = 1.013 bars

pH = 6.077 log fO<sub>2</sub> = -0.800

Eh = 0.8577 volts pe = 14.4995

Ionic strength = 0.009563

Activity of water = 0.999687

Solvent mass = 1.000039 kg

Solution mass = 1.000672 kg

Solution density = 1.013 g/cm<sup>3</sup>

Chlorinity = 0.008968 molal

Dissolved solids = 633 mg/kg sol'n

Reactants	moles remaining	moles reacted	grams reacted	cm <sup>3</sup> reacted
Atacamite	3.000	2.000	854.3	113.6

Minerals in system	moles	log moles	grams	volume (cm <sup>3</sup> )
Atacamite	1.999	0.301	854.0	113.6
Malachite	0.0001840	-3.735	0.04068	0.01009
Tenorite	0.001985	-2.702	0.1579	0.02426
(total)		854.2	113.6	

Aqueous species	molality	mg/kg sol'n	act. coef.	log act.
Na+	0.009419	216.4	0.9038	-2.0699
Cl-	0.008955	317.3	0.9011	-2.0931
CO <sub>2</sub> (aq)	0.0009392	41.31	1.0000	-3.0273
HCO <sub>3</sub> -	0.0005607	34.19	0.9038	-3.2952
O <sub>2</sub> (aq)	0.0002003	6.405	1.0000	-3.6983
SiO <sub>2</sub> (aq)	9.998e-005	6.003	1.0000	-4.0001
Cu <sup>++</sup>	4.673e-005	2.967	0.6803	-4.4977
NaCl(aq)	1.148e-005	0.6705	1.0000	-4.9400
CuCO <sub>3</sub> (aq)	8.138e-006	1.005	1.0000	-5.0895
NaHCO <sub>3</sub> (aq)	6.152e-006	0.5165	1.0000	-5.2110
CuOH+	2.165e-006	0.1743	0.9038	-5.7084
H+	9.151e-007	0.0009217	0.9154	-6.0769
CuCl+	7.764e-007	0.07681	0.9038	-6.1539
CO <sub>3</sub> --	4.240e-008	0.002543	0.6693	-7.5470
HSiO <sub>3</sub> -	1.473e-008	0.001135	0.9038	-7.8758
OH-	1.337e-008	0.0002273	0.9025	-7.9183

(only species &gt; 1e-8 molal listed)

Mineral saturation states

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log Q/K

log Q/K

Malachite	0.0000 sat	Cristobalite(alp)	-0.5513
Tenorite	0.0000 sat	Coesite	-0.8108
Atacamite	0.0000 sat	Cristobalite(bet)	-0.9948
Quartz	-0.0008	SiO <sub>2</sub> (am)	-1.2865
Ice	-0.1388	Diopase	-2.4215
Tridymite	-0.1723	Chrysocolla	-2.5586
Chalcedony	-0.2720		

(only minerals with log Q/K &gt; -3 listed)

Gases fugacity log fug.

O <sub>2</sub> (g)	0.1585	-0.800
CO <sub>2</sub> (g)	0.02765	-1.558
H <sub>2</sub> O(g)	0.02597	-1.586
HCl(g)	3.345e-015	-14.476
Cl <sub>2</sub> (g)	6.463e-022	-21.190
H <sub>2</sub> (g)	7.038e-042	-41.153
CO(g)	6.078e-047	-46.216
Cu(g)	6.972e-075	-74.157
Na(g)	1.168e-076	-75.932
CH <sub>4</sub> (g)	5.412e-144	-143.267
C(g)	3.581e-188	-187.446
Si(g)	5.589e-221	-220.253
C <sub>2</sub> H <sub>4</sub> (g)	1.167e-234	-233.933

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This notebook has been prepared in accordance with applicable quality assurance procedures. The content is sufficient to allow a technically qualified person to replicate the studies described herein.

Gordon Wittinger

5/25/2000

FINAL FINAL (?) ENTRY:

I HAVE reviewed THIS notebook AND find it in compliance with QAP-001. I HAVE improved the quality of THIS notebook by retroactively adding my initials AND TODAY'S DATE in various places. There is sufficient information in THIS notebook so THAT another qualified individual could repeat the Activity.

E.C. Pen  
8/24/2000

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