

308 - - - Q200002080007
Scientific Notebook # 236 (Continuation of
Notebook # 150)

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Notebook # 150)

G. R.

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150

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Ron Green
CNWRA #236

Ronald Green = ~~RH~~

CNWRA
CONTROLLED
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REFLUX CALCULATIONS

NOTE - THIS NOTEBOOK IS A CONTINUATION
OF WORK DESCRIBED IN NOTEBOOK #150.
THE PORTIONS OF NOTEBOOK #150 THAT
DISCUSS REFLUXING ARE PAGES: 259-263,
275-280, 282-284, 289-290.

8-14-97

This is for
George Rice
RH 10/15/99

NR THE FOLLOWING IS A BRIEF DESCRIPTION OF REFLUXING
AND THE EXPRESSIONS THAT ARE USED TO CALCULATE
ITS COMPONENTS.

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11/29/97

Calculating Reflux of Condensate to the Boiling Zone

Heat produced by the decay of spent fuel will cause waste package temperatures to exceed the boiling point of water. A portion of this heat may be consumed by vaporization of water dripping onto the packages, resulting in reduction of package temperature. A similar reduction in the temperature of the drift wall may be caused by vaporization of water in the surrounding rock. Water will vaporize as long as temperatures remain above boiling. The vapor will flow away from the boiling zone and condense where temperatures are below boiling. The condensate may then flow back to the boiling zone. This return of condensate to the boiling zone is called *refluxing*. A particular unit of water may participate in the reflux cycle many times. With every cycle, some portion of the refluxing water may escape and flow away from the heat source, possibly toward the water table.

Refluxing water may originate from two sources: 1) infiltration from ground surface, and 2) water boiled out of a dry-out zone in rock surrounding the waste package.

A method of calculating the amount of water that refluxes each year is presented below. However, it should be noted that some of the important variables that control refluxing are poorly constrained. Reliable estimates cannot be made until more precise values of these variables are obtained.

Reflux Derived From Infiltration

The amount of infiltration-derived water that refluxes in year 'N', is:

$$R_i = \sum_{j=0}^{N-1} \sum_{k=N}^{\infty} I_k (1-L_i)^j \quad \text{(Note, } j \text{ varies from } 0 \text{ to } N-1, k \text{ from } N \text{ to } 1)$$

And for a constant infiltration rate:

$$R_i = \sum_{j=0}^{N-1} I (1-L_i)^j$$

Where:

- I_k = amount of infiltration in year N [m]
- j, k = summation indices
- N = years since start of refluxing
- L_i = fraction of infiltration that escapes the reflux cycle each year

Note: For constant I , R_i converges to I/L_i .

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Reflux Derived From the Dry-Out Zone

The total amount of water vaporized from the dry-out zone and available for refluxing is:

$$D = (T)(n)(S - S_r)$$

Where:

- T = thickness of dry-out zone [m]
- n = porosity of rock
- S = liquid saturation
- S_r = residual saturation

As with refluxing infiltration, some portion of refluxing dry-out zone water may escape the cycle each year (L_D). In addition, dry-out zone condensate may take more or less than a year to participate in a reflux cycle. The number of years required for water to complete one reflux cycle is 'P'. This gives rise to two cases:

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DESCRIPTION OF REFLUXING (CONT)

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Case I, $P \geq 1.0$

The amount of dry-out zone water that refluxes in year 'N' is:

$$R_D = [(D) (P - L_D)^{N-1}] / P^N$$

Case II, $P < 1.0$

In this case, the amount of dry-out zone water that refluxes in a given year is:

$$R_D = \sum_{j=0}^{N-1} (1-L_D)^j D (1-L_D)^{1/P-1} (1-L_D)^{1/P(N-1)+j}$$

Total Reflux

The total amount of refluxing water derived from both infiltration and the dry-out zone in year 'N' is:

$$R_T = R_i + R_D$$

For Case I with a constant infiltration rate this is:

$$R_T = \sum_{j=0}^{N-1} (1-L_i)^j I + [(D) (P - L_D)^{N-1}] / P^N$$

For Case II with a constant infiltration rate:

$$R_T = \sum_{j=0}^{N-1} (1-L_i)^j I + \sum_{j=0}^{N-1} (1-L_D)^j D (1-L_D)^{1/P-1} (1-L_D)^{1/P(N-1)+j}$$

The predominant source of refluxing water may change with time. At early times, refluxing water may be dominated by water derived from the dry-out zone. At later times, water derived from infiltration may dominate. If water escapes the reflux cycle, all dry-out zone water will eventually be lost and the amount of refluxing water will stabilize to the value of $R_i (I/L_i)$. If no losses occur, the amount of refluxing water will grow at a rate equal to 'I'. The reflux cycle will stop once waste package temperatures drop below boiling.

Example Calculation

Calculate the amount of reflux occurring in year four. That is, four years after refluxing begins. Assume:

Infiltration Derived Reflux

- $I = 1 \times 10^{-3}$ m (constant)
- $L_i = 0.1$

Dry-Out Zone Derived Reflux

- $T = 20$ m
- $n = 0.15$
- $S = 0.9$
- $S_r = 0.0$

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DESCRIPTION OF REFLUXING (CONT)

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Then:

$$D = (20 \text{ m}) (0.15) (0.9 - 0.0) = 2.7 \text{ m}$$

- $L_D = 0.2$
- $P = 1/3$ (Case II)

In year 4, the amount of reflux due to infiltration and dry-out zone water is:

$$R_T = R_i + R_D = \sum_{j=0}^{N-1} (1-L_i)^j I + \sum_{j=0}^{N-1} (1-L_D)^j D (1-L_D)^{1/P-1} (1-L_D)^{1/P(N-1)+j}$$

$$= \sum_{j=0}^3 [(1 \times 10^{-3}) (1 - 0.1)^j] + \sum_{j=0}^3 2.7 (1 - 0.2)^{3+j}$$

$$= 1 \times 10^{-3} \text{ m} [(0.9)^0 + (0.9)^1 + (0.9)^2 + (0.9)^3] + 2.7 \text{ m} [(0.8)^0 + (0.8)^1 + (0.8)^2 + (0.8)^3]$$

$$= 1 \times 10^{-3} \text{ m} + 1 \times 10^{-3} \text{ m} [2.44] + 2.4 \text{ m} [0.327]$$

$$= 0.888 \text{ m}$$

NOTE: this result represents the amount of refluxing water, not water escaping the reflux cycle.

Derivation of Reflux Expressions

Infiltration Derived Reflux

Year	Infiltration	Reflux	Loss	Storage
1	I_1	I_1	$L_i I_1$	$I_1 - L_i I_1 = I_1 (1 - L_i)$
2	I_2	$I_2 + I_1 (1 - L_i)$	$L_i [I_2 + I_1 (1 - L_i)]$	$I_2 + I_1 (1 - L_i) - L_i [I_2 + I_1 (1 - L_i)]$ $= [I_2 (1 - L_i) + I_1 (1 - L_i)^2]$
3	I_3	$I_3 + [I_2 (1 - L_i) + I_1 (1 - L_i)^2]$	$L_i [I_3 + [I_2 (1 - L_i) + I_1 (1 - L_i)^2]]$	$I_3 + [I_2 (1 - L_i) + I_1 (1 - L_i)^2] - L_i [I_3 + [I_2 (1 - L_i) + I_1 (1 - L_i)^2]]$ $= [I_3 (1 - L_i) + [I_2 (1 - L_i)^2 + I_1 (1 - L_i)^3]]$

and so on ...

Thus, the amount of infiltration-derived water that refluxes in year four is:

$$R_i = I_4 + I_3 (1 - L_i) + I_2 (1 - L_i)^2 + I_1 (1 - L_i)^3$$

$$R_i = \sum_{k=0}^{N-1} \sum_{j=N-k}^{N-1} I_k (1 - L_i)^j \quad (\text{Note, } j \text{ varies from } 0 \text{ to } N-1, k \text{ from } N \text{ to } 1)$$

Or, if the infiltration rate is constant:

$$R_i = \sum_{j=0}^{N-1} (1 - L_i)^j I$$

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DESCRIPTION OF REFLEXION (CONCL)

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Dry-Out Zone Derived Reflux

Case II

For P = 1/3

Year	Cycle	Reflux	Loss	Storage
0	0	0	0	D
1	1	D	$L_0 D$	$D - L_0 D = D(1 - L_0)$
	2	$D(1 - L_0)$	$L_0 D(1 - L_0)$	$D(1 - L_0) - L_0 D(1 - L_0)$ $= D(1 - L_0)^2$
	3	$D(1 - L_0)^2$	$L_0 D(1 - L_0)^2$	$D(1 - L_0)^2 - L_0 D(1 - L_0)^2$ $= D(1 - L_0)^3$
2	1	$D(1 - L_0)^3$	$L_0 D(1 - L_0)^3$	$L_0 D(1 - L_0)^4$
	2	$D(1 - L_0)^4$	$L_0 D(1 - L_0)^4$	$L_0 D(1 - L_0)^5$
	3	$D(1 - L_0)^5$	$L_0 D(1 - L_0)^5$	

and so on ...

Thus, the amount of dry-out zone water that refluxes in year 2 is:

$$D[(1 - L_0)^3 + (1 - L_0)^4 + (1 - L_0)^5]$$

$$= 1 - e^{-\sum^5 D(1 - L_0)^{n+1}}$$

$$= R_0 = 1 - e^{-\sum^{1/P-1} D(1 - L_0)^{n/P(n-1)+1}}$$

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To: Sitakanta Mohanty

From: George Rice

Subject: TPA Code - Mass Balance for Reflux Module

Date: 8/21/97

Mass balance calculated as follows:

total reflux = total infiltration + dry-out water

Percent difference = $\frac{[\text{total reflux} - (\text{total infiltration} + \text{dry-out water})]}{(\text{total reflux} + \text{total infiltration} + \text{dry-out water})/2} \times 100$

Mass balances performed for three cases:

1. "Moderate" conditions: Mass balance difference = 0.06%
Thickness of dry-out zone = 20 m
Period = 100
Loss factor (infiltration) = 0.1
Loss factor (dry-out) = 0.1

2. Reflux forced to occur at early times: Mass balance difference = 4.1%
Thickness of dry-out zone = 100 m
Period = 1
Loss factor (infiltration) = 0.9
Loss factor (dry-out) = 0.9

3. Reflux forced to persist to late times: Mass balance difference = 0.9%
(run = 20,000 yrs)
Thickness of dry-out zone = 100 m
Period = 100
Loss factor (infiltration) = 0.01
Loss factor (Dry-out) = 0.01

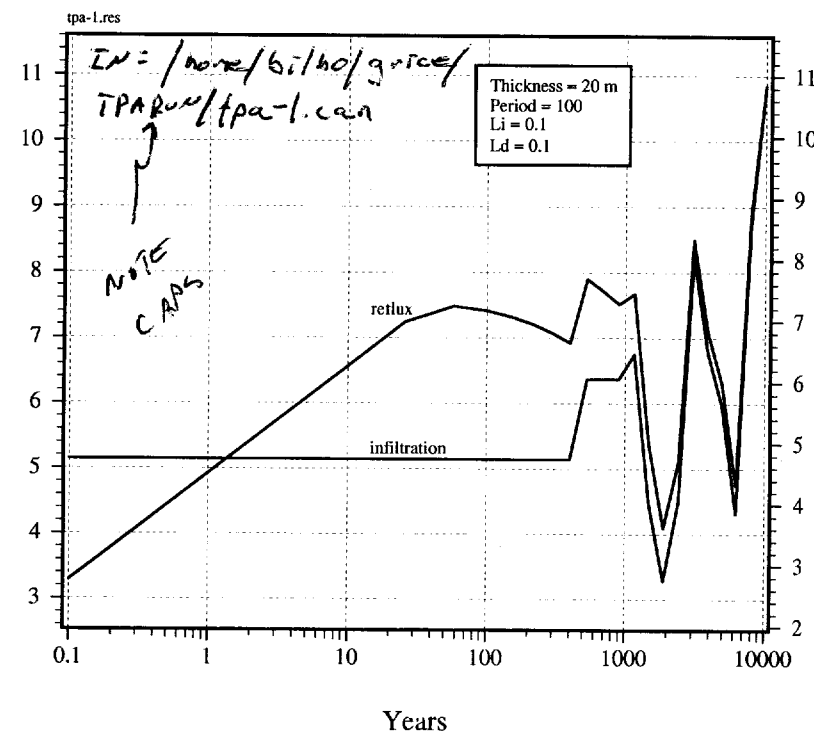
* Mass balance calculation can be improved by forcing TPA code to report output at earlier times.

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Case 1, TPA Code Test - Reflux Module

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TPA CODE OUTPUT: infilper.res - MODIFIED -
YEAR 0 → YEAR 0.1 SO RESULTS CAN BE PLOTTED
ON LOG SCALE. NEW NAME: tpa-1.res

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Input file tpa.inp as supplied with TPA Version 3.1beta4 Code.
Not a basecase dataset. Use only for beta testing.
TPA 3.1beta4, Job started: Tue Aug 26 07:39:45 1997
Subarea Averaged Infiltration/Deep Percolation Including
After Reflux and Diversion - Values for Each Vector

vector	time	avinfil	avreflux	avdivert
unitless	yr	mm/yr	mm/yr	mm/yr
1	0.1000000E+00	5.1448215E+00	2.7544821E+00	8.2634464E-01
1	2.5693704E+01	5.1448215E+00	6.9864341E+00	2.0959302E+00
1	5.8077611E+01	5.1448215E+00	7.2491623E+00	2.1747487E+00
1	9.8893734E+01	5.1448215E+00	7.1756778E+00	2.1527033E+00
1	1.5033768E+02	5.1448215E+00	7.0739401E+00	2.1221820E+00
1	2.1517675E+02	5.1448215E+00	6.9527686E+00	2.0858306E+00
1	2.9689880E+02	5.1448215E+00	6.8108273E+00	2.0432482E+00
1	3.9989989E+02	5.1448215E+00	6.6476912E+00	1.9943074E+00
1	5.2972070E+02	6.3738383E+00	7.6936522E+00	2.3080957E+00
1	6.9334463E+02	6.3738383E+00	7.4943494E+00	2.2483048E+00
1	8.9957344E+02	6.3738383E+00	7.2854446E+00	2.1856334E+00
1	1.1595007E+03	6.7496751E+00	7.4525303E+00	2.2357591E+00
1	1.4871086E+03	4.4886291E+00	4.9979532E+00	1.4993860E+00
1	1.9000200E+03	3.2858578E+00	3.6209015E+00	1.0862705E+00
1	2.4204465E+03	4.4947567E+00	4.7020430E+00	1.4106129E+00
1	3.0763831E+03	8.2302200E+00	8.3334861E+00	2.5000458E+00
1	3.9031145E+03	6.7801498E+00	6.8244343E+00	2.0473303E+00
1	4.9451126E+03	5.9622745E+00	5.9782781E+00	1.7934834E+00
1	6.2584292E+03	4.3152098E+00	4.3193102E+00	1.2957931E+00
1	7.9137110E+03	8.7454765E+00	8.7458956E+00	2.6237687E+00
1	1.0000000E+04	1.0847138E+01	1.0847239E+01	3.2541718E+00

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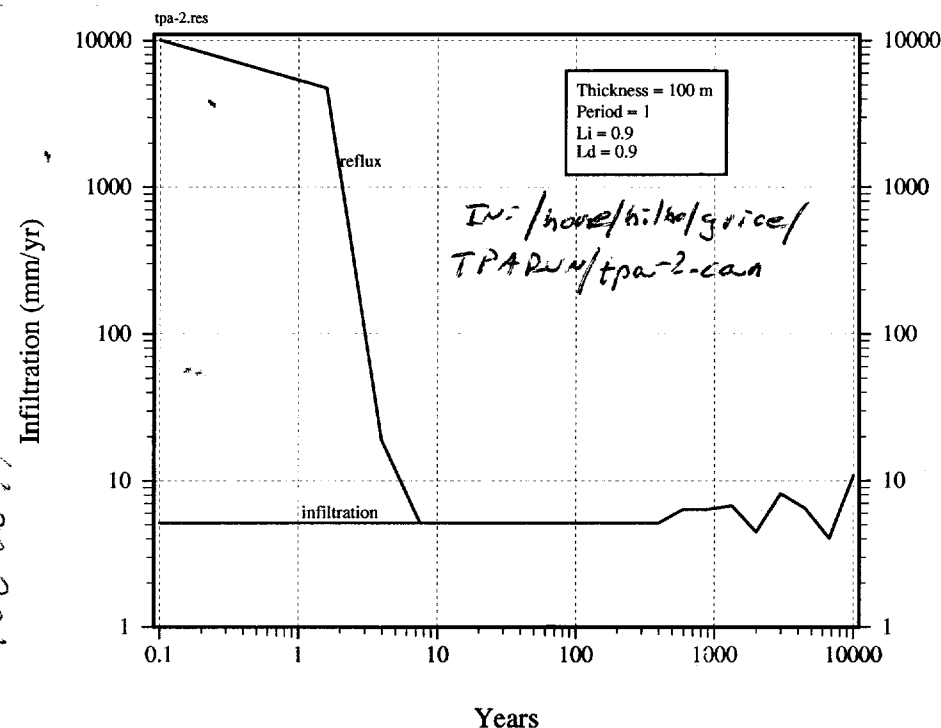
Reflux (mm/yr)

Infiltration (mm/yr)

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Case 2, TPA Code Test - Reflux Module

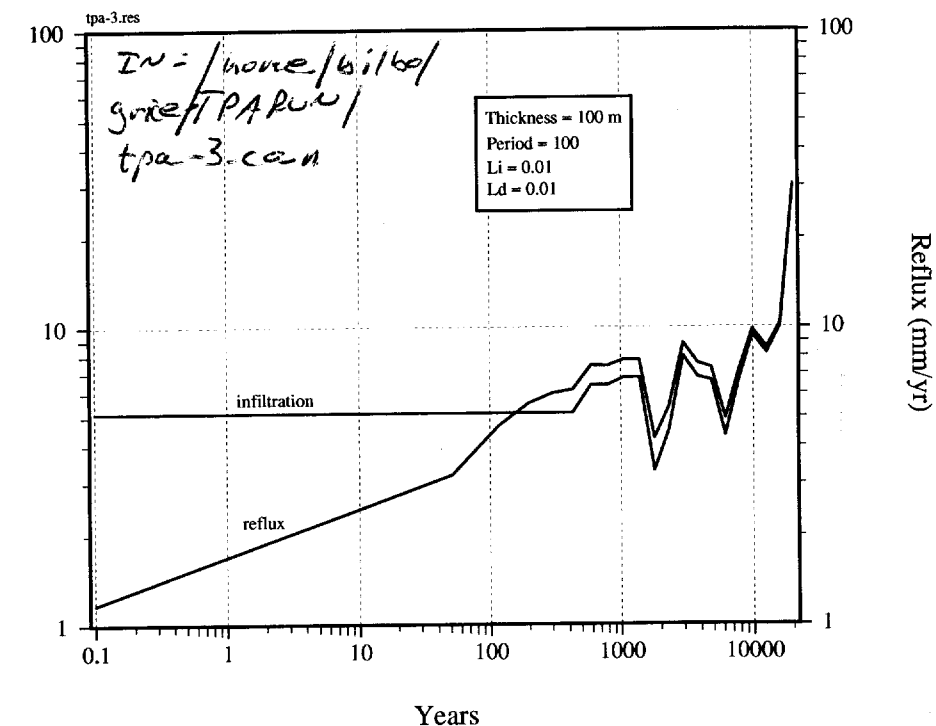


TPA output = infilper.res - modified for ϕ -
 from ϕ yrs to 0.1 yrs so it would plot on log
 scale - new name = tpa-2.res

Input file tpa.inp as supplied with TPA Version 3.1beta4 Code.
 Not a basecase dataset. Use only for beta testing.
 TPA 3.1beta4, Job started: Wed Aug 20 15:58:16 1997
 Subarea Averaged Infiltration/Deep Percolation Including
 After Reflux and Diversion - Values for Each Vector

vector unitless	time yr	avinfil mm/yr	avreflux mm/yr	avdivert mm/yr
IN:	1 0.1000000E+00	5.1448215E+00	1.0084630E+04	3.0253891E+03
/home/	1 1.5864169E+00	5.1448215E+00	4.7649273E+03	1.4294782E+03
hilko/grice/	1 3.9585937E+00	5.1448215E+00	1.8980492E+01	5.6941475E+00
TPARUN/	1 7.5057209E+00	5.1448215E+00	5.1503133E+00	1.5450940E+00
tpa-2.res	1 1.2809757E+01	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 2.0740907E+01	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 3.2600394E+01	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 5.0333941E+01	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 7.6850998E+01	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 1.1650208E+02	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 1.7579253E+02	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 2.6444982E+02	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 3.9701949E+02	5.1448215E+00	5.1448215E+00	1.5434464E+00
	1 5.9525154E+02	6.3738383E+00	6.3738383E+00	1.9121515E+00
	1 8.9166886E+02	6.3738383E+00	6.3738383E+00	1.9121515E+00
	1 1.3349031E+03	6.7496751E+00	6.7496751E+00	2.0249025E+00
	1 1.9976734E+03	4.4605153E+00	4.4573326E+00	1.3371998E+00
	1 2.9887169E+03	8.1609048E+00	8.1598405E+00	2.4479521E+00
	1 4.4706289E+03	6.4882750E+00	6.4876880E+00	1.9463064E+00
	1 6.6865391E+03	4.0380920E+00	4.0381627E+00	1.2114488E+00
	1 1.0000000E+04	1.0847138E+01	1.0847138E+01	3.2541414E+00

Case 3, TPA Code Test - Reflux Module



TPA CODE output = infilper.res - modified so
 that ϕ = 0.1 - allow to be plotted on
 log scale = tpa-3.res

Input file tpa.inp as supplied with TPA Version 3.1beta4 Code.
 Not a basecase dataset. Use only for beta testing.
 TPA 3.1beta4, Job started: Thu Aug 21 07:48:15 1997
 Subarea Averaged Infiltration/Deep Percolation Including
 After Reflux and Diversion - Values for Each Vector

vector unitless	time yr	avinfil mm/yr	avreflux mm/yr	avdivert mm/yr
IN:	1 0.1000000E+00	5.1448215E+00	1.1714482E+00	3.5143446E-01
/home/	1 5.1387409E+01	5.1448215E+00	3.1896084E+00	9.5688251E-01
hilko/grice/	1 1.1615522E+02	5.1448215E+00	4.6510457E+00	1.3953137E+00
TPARUN/	1 1.9778747E+02	5.1448215E+00	5.5381887E+00	1.6614566E+00
tpa-3.res	1 3.0067536E+02	5.1448215E+00	5.9811515E+00	1.7943454E+00
	1 4.3035349E+02	5.1448215E+00	6.1496777E+00	1.8449033E+00
	1 5.9379761E+02	6.3738383E+00	7.4130562E+00	2.2239168E+00
	1 7.9979978E+02	6.3738383E+00	7.4057906E+00	2.2217372E+00
	1 1.0594414E+03	6.7496751E+00	7.7570221E+00	2.3271066E+00
	1 1.3866893E+03	6.7496751E+00	7.7247380E+00	2.3174214E+00
	1 1.7991469E+03	3.2858578E+00	4.2215254E+00	1.2664576E+00
	1 2.3190014E+03	4.4947567E+00	5.3830236E+00	1.6149071E+00
	1 2.9742172E+03	7.9682058E+00	8.7995807E+00	2.6398742E+00
	1 3.8000400E+03	6.7801498E+00	7.5461336E+00	2.2638401E+00
	1 4.8408930E+03	6.5916447E+00	7.2812782E+00	2.1843834E+00
	1 6.1527663E+03	4.3152098E+00	4.9206021E+00	1.4761806E+00
	1 7.8062290E+03	6.6288966E+00	7.1455931E+00	2.1436779E+00
	1 9.8902252E+03	9.3661355E+00	9.7828989E+00	2.9348697E+00
	1 1.2516858E+04	8.1726389E+00	8.4933898E+00	2.5480170E+00
	1 1.5827422E+04	1.0014201E+01	1.0245078E+01	3.0735235E+00
	1 2.0000000E+04	3.0054835E+01	3.0206411E+01	9.0619232E+00

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NR

EXCEL SPREADSHEET

FOR CALCULATING
MASS BALANCE OF
TPA LVS - THIS
IS FOR CASE 1,
SEE PG 5.

TPA Code Results
Mass Balance
Results From File 'infilper.res'

Reflux Parameters:
Thickness = 20 m
Porosity = 0.14
Initial Saturation = 0.9
Residual Saturation = 0.1
Period = 100
Li = 0.1
Ld = 0.1

Amount of reflux derived from vaporized dry-out zone water:

$$20m(0.14)(0.9 - 0.1) = 2240 \text{ mm}$$

Thus, For mass balance:

$$\text{Total Reflux} = \text{Total Infiltration} + 2240 \text{ mm}$$

ON P.C. IN:
C:/jonje/
memos/reflux/
tpa-1.xls

Time (yr)	avinfil mm/yr	avreflux mm/yr	total infil mm	total reflux mm
0	5.1448	2.7545	0	0
25.69	5.1448	6.9864	132.169912	125.121861
58.08	5.1448	7.2492	166.640072	230.5415542
98.89	5.1448	7.1757	209.959288	294.340085
150.3	5.1448	7.0739	264.494168	366.2815968
215.2	5.1448	6.9528	333.89752	455.166415
296.9	5.1448	6.8108	420.33016	562.24306
399.9	5.1448	6.6477	529.9144	693.11275
529.7	6.3738	7.6937	747.55714	930.715686
693.3	6.3738	7.4943	1042.75368	1242.3784
899.6	6.3738	7.2854	1314.91494	1524.52606
1160	6.7497	7.4525	1708.6797	1918.87458
1487	4.4886	4.998	1837.46205	2035.615675
1900	3.2859	3.6209	1605.43425	1779.80285
2420	4.4948	4.702	2022.982	2163.954
3076	8.2302	8.3335	4173.8	4275.644
3903	6.7801	6.8244	6206.75905	6267.79165
4945	5.9623	5.9783	6638.7904	6670.2067
6258	4.3152	4.3193	6747.17875	6760.3744
7914	8.7455	8.7459	10814.2596	10817.9856
10000	10.847	10.847	20434.9775	20435.3947

Totals

Thickness 20000
Porosity 0.14
Sat-Init 0.9
Sat-Resid 0.1

Dry-out:

2240

Mass

Balance: -42.792355 = -0.00061508

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NR

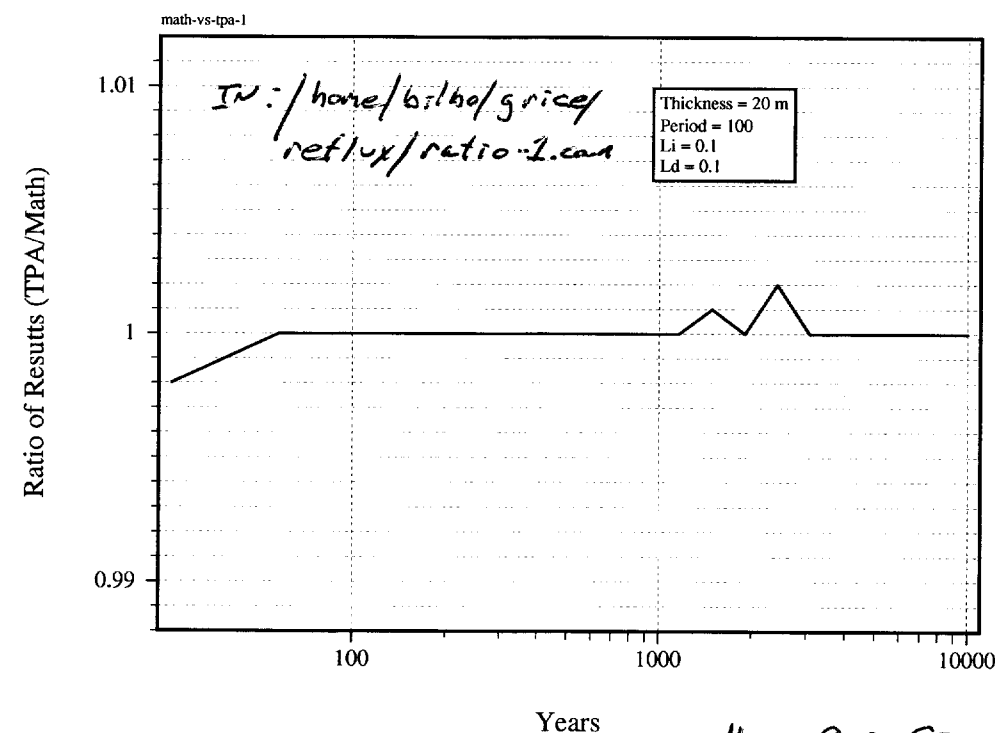
COMPARING REFLUX2 RESULTS - TPA CODE +
MATHEMATICA - FOR CASE 1 - PAGE 5.
MATHEMATICA FILE IS IN:
/home/bilbo/grice/reflux/test-tpa-1.xls

Comparison of reflux2 results obtained using Mathematica and the TPA code.
This comparison for "moderate" conditions (see page 5 of reflux notebook).

Time(yrs)	TPA Code	Mathematica	Ratio(TPA/Math)
26	6.986	6.997	0.998
58	7.249	7.249	1.000
215	6.953	6.953	1.000
400	6.648	6.648	1.000
900	7.285	7.285	1.000
1160	7.453	7.452	1.000
1487	4.998	4.995	1.001
1900	3.621	3.621	1.000
2420	4.702	4.694	1.002
3076	8.333	8.334	1.000
3903	6.824	6.825	1.000
4945	5.978	5.978	1.000
6258	4.319	4.319	1.000
7914	8.745	8.746	1.000
10000	10.85	10.85	1.000

NR 9-2-97

Reflux2 - TPA Code vs Mathematica, Case 1



NR 9-2-97

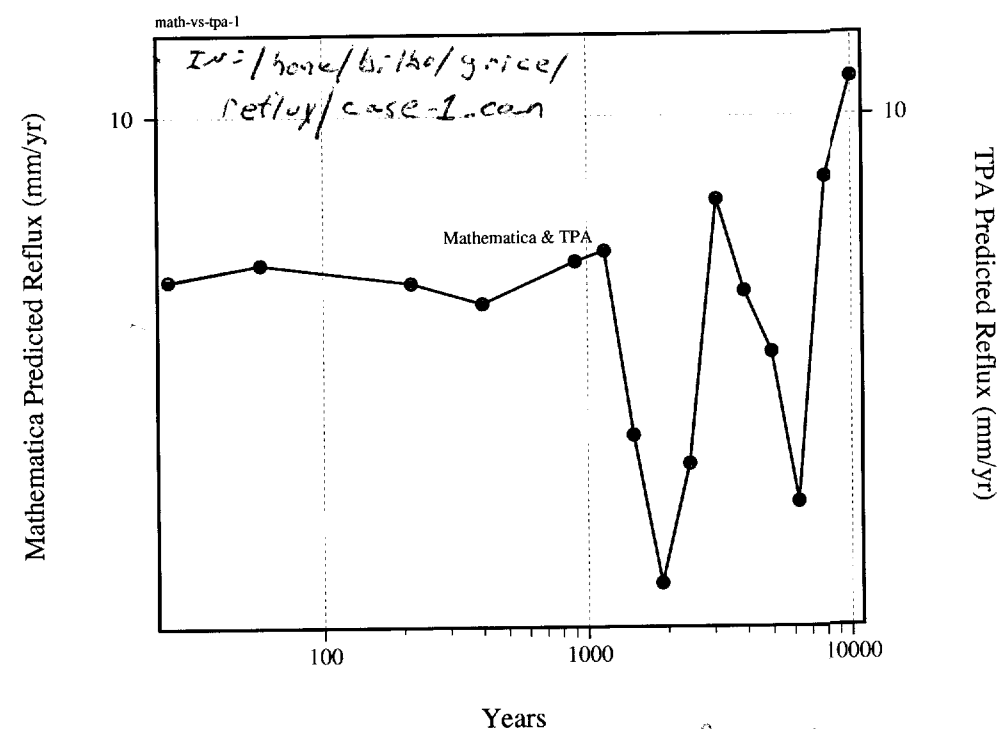
6x10⁻⁴

69550 - (67353 + 2240)
[69550 + 67353 + 2240] / 2

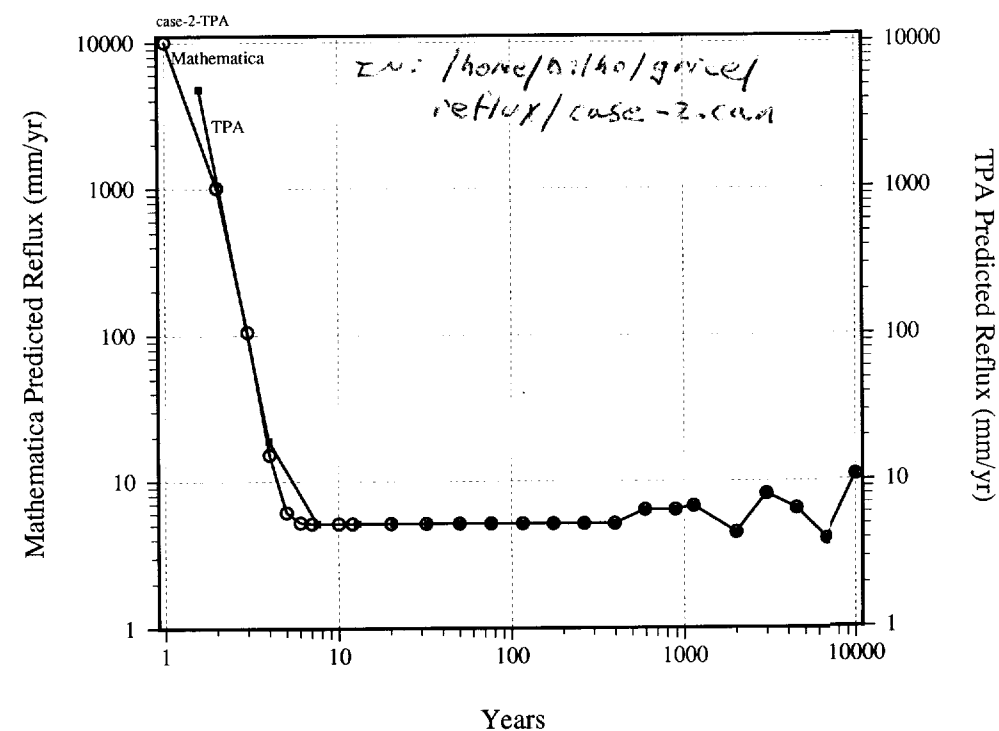
9-9-97

MR

Reflux2 - TPA Code vs Mathematica, Case 1



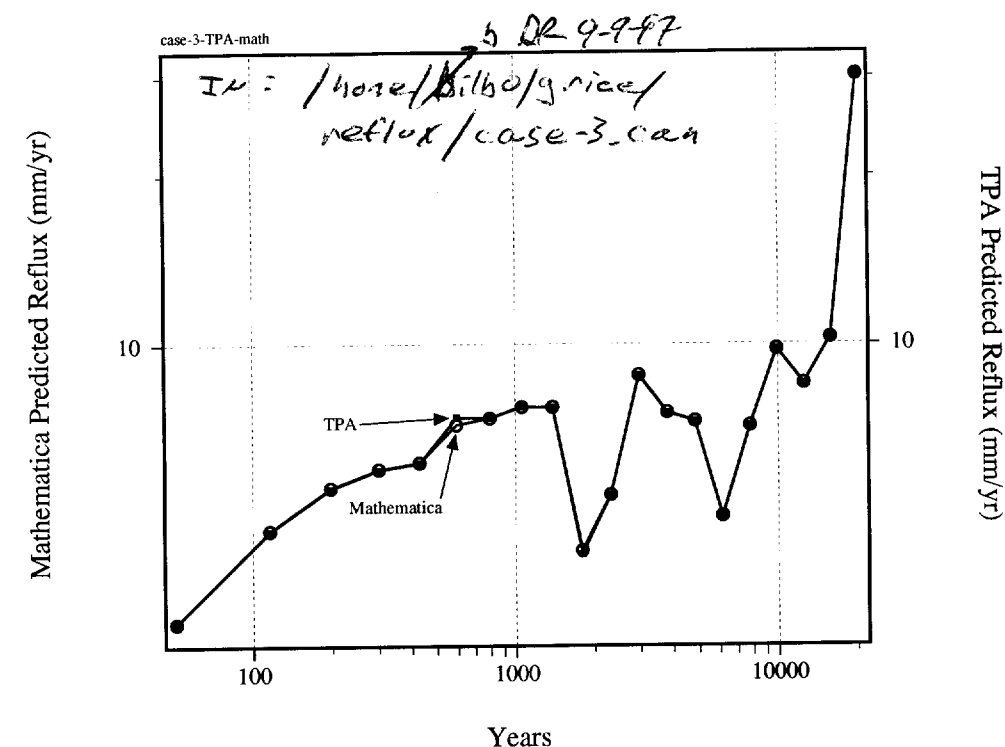
Reflux2 - TPA Code vs Mathematica, Case 2



9-9-97

MR

Reflux2 - TPA Code vs Mathematica, Case 3



9-11-97

MR

THE MATHEMATICA FILES USED TO PRODUCE
THE PLOTS ON THIS AND THE PREVIOUS PAGE ARE IN:
~~/home/sneezy/~~ MR 9-11-97
/home/bilbo/grice/reflux:

test-tpa-1.nb

test-tpa-2.nb

test-tpa-3.nb

MR 9-26-97

9-26-97

NR

TPA CODE - REFLUX2 SENSITIVITY ANALYSES

- VARYING REFLUX2 PARAMETERS [THICKNESS, PERIOD, LOSS-TO-FILL, LOSS-DAT] TO DETERMINE HOW LITTLE REFLUX WILL RESULT IN A RELEASE FROM THE WASTE PACKAGE.

ONLY VARYING REFLUX PARAMETERS - USING BASE CASE INPUT FROM TPA3-11 - ALSO USING EXECUTABLE COMMAND:

/solapps/cnwrk/tpa3-11/tpa.e. IN:
/home/bilbo/grise/tparun

NOTE - VOLCANO, SEISMO, AND FAULTS DO NOT APPEAR TO AFFECT RELEASES - COMPARE FILES SHOWN BELOW - BOTH USING tpa.inp FROM TPA3-11 - OUTPUTS ARE MODIFIED (ADDED HEADERS) cumrel.res files.

NR 9-26-97

Case 11:

Thickness = 500m
Period = 100
Li = 0.1
Ld = 0.1

Input file tpa.inp as supplied with TPA Version 3.1 Code.
Base case data set Rev 3.1.1 9/22/97
TPA 3.1, Job started: Thu Sep 25 13:34:22 1997
Cumulative Releases from EBS, UZ, and SZ by Nuclide
Summed Over All Subareas - Values for Each Vector

vector unitless	nuclide unitless	ebscumrl Ci	uzcumrl Ci	szcumrl Ci
1	Cm246	8.2554E-04	8.2330E-04	6.5119E-04
1	U238	1.5547E-04	1.5493E-04	1.2629E-04
1	Cm245	6.9455E-03	6.9258E-03	5.5470E-03
1	Am241	5.5657E-04	6.1891E-04	9.3470E-04
1	Np237	3.0061E-01	3.0039E-01	2.8086E-01
1	Am243	5.3941E-02	5.3786E-02	1.2038E-02
1	Pu239	1.1925E-02	1.1904E-02	1.2526E-02
1	Pu240	1.0244E-02	1.0219E-02	9.0347E-03
1	U234	5.7879E-04	5.7680E-04	4.7026E-04
1	Th230	3.2281E-02	3.2230E-02	2.6840E-02
1	Ra226	2.1031E-02	2.1040E-02	8.2178E-03
1	Pb210	2.0824E-02	2.0855E-02	8.0346E-02
1	Cs135	1.1387E-01	1.1384E-01	8.4619E-16
1	I129	3.4200E-02	3.4104E-02	3.1489E-02
1	Tc99	1.3786E+01	1.3747E+01	1.2450E+01
1	Ni59	1.9039E+00	1.8985E+00	1.3924E+00
1	Cl4	4.6033E-01	2.2725E-01	2.1348E-01
1	Se79	3.9441E-01	3.9335E-01	3.3591E-01
1	Nb94	5.6708E-04	5.6565E-04	3.6040E-04
1	Cl36	1.3250E-02	1.3213E-02	1.2418E-02

NR 9-26-97

NR 9-26-97

Case 13:

Thickness = 500m
Period = 100
Li = 0.1
Ld = 0.1

With seismo, faulto, and volcano

Input file tpa.inp as supplied with TPA Version 3.1 Code.
Base case data set Rev 3.1.1 9/22/97
TPA 3.1, Job started: Thu Sep 25 14:09:35 1997
Cumulative Releases from EBS, UZ, and SZ by Nuclide
Summed Over All Subareas - Values for Each Vector

vector unitless	nuclide unitless	ebscumrl Ci	uzcumrl Ci	szcumrl Ci
1	Cm246	8.2554E-04	8.2330E-04	6.5119E-04
1	U238	1.5547E-04	1.5493E-04	1.2629E-04
1	Cm245	6.9455E-03	6.9258E-03	5.5470E-03
1	Am241	5.5657E-04	6.1891E-04	9.3470E-04
1	Np237	3.0061E-01	3.0039E-01	2.8086E-01
1	Am243	5.3941E-02	5.3786E-02	1.2038E-02
1	Pu239	1.1925E-02	1.1904E-02	1.2526E-02
1	Pu240	1.0244E-02	1.0219E-02	9.0347E-03
1	U234	5.7879E-04	5.7680E-04	4.7026E-04
1	Th230	3.2281E-02	3.2230E-02	2.6840E-02
1	Ra226	2.1031E-02	2.1040E-02	8.2178E-03
1	Pb210	2.0824E-02	2.0855E-02	8.0346E-02
1	Cs135	1.1387E-01	1.1384E-01	8.4619E-16
1	I129	3.4200E-02	3.4104E-02	3.1489E-02
1	Tc99	1.3786E+01	1.3747E+01	1.2450E+01
1	Ni59	1.9039E+00	1.8985E+00	1.3924E+00
1	Cl4	4.6033E-01	2.2725E-01	2.1348E-01
1	Se79	3.9441E-01	3.9335E-01	3.3591E-01
1	Nb94	5.6708E-04	5.6565E-04	3.6040E-04
1	Cl36	1.3250E-02	1.3213E-02	1.2418E-02

NR 9-26-97

FOR THE BASECASE INPUT IN TPA3-11, THE SMALLEST AMOUNT OF REFLUX WATER THAT RESULTS IN A RELEASE FROM THE EBS IS ^{0.1-0.647} ~~WHEN~~ THE AMOUNT CORRESPONDING TO A THICKNESS OF 357"

NR 9-29-97

Case 27:

Thickness = 315m
Period = 200
Li = 0.1
Ld = 0.1

Input file tpa.inp as supplied with TPA Version 3.1 Code.
Base case data set Rev 3.1.1 9/22/97
TPA 3.1, Job started: Fri Sep 26 15:31:39 1997
Cumulative Releases from EBS, UZ, and SZ by Nuclide
Summed Over All Subareas - Values for Each Vector

vector unitless	nuclide unitless	ebscumrl Ci	uzcumrl Ci	szcumrl Ci
1	Cm246	1.5665E-05	2.0437E-06	0.0000E+00
1	U238	2.4817E-06	3.2434E-07	7.5370E-12
1	Cm245	1.4653E-04	1.9131E-05	0.0000E+00
1	Am241	1.1000E-05	1.7868E-06	0.0000E+00
1	Np237	6.7626E-03	8.8381E-04	3.9537E-05
1	Am243	1.1309E-03	1.4764E-04	0.0000E+00
1	Pu239	2.5588E-04	3.3484E-05	1.8737E-06
1	Pu240	1.9324E-04	2.5222E-05	1.3822E-06
1	U234	9.2293E-06	1.2062E-06	2.8009E-11
1	Th230	1.9545E-03	2.5542E-04	2.7588E-16
1	Ra226	1.5254E-03	1.9967E-04	0.0000E+00
1	Pb210	1.5193E-03	1.9913E-04	1.6956E-07
1	Cs135	6.5981E-03	8.6104E-04	0.0000E+00
1	I129	5.5586E-04	7.2650E-05	1.8469E-05
1	Tc99	2.2437E-01	2.9322E-02	3.6192E-03

NR 9-29-97

9-29-97

SEE PREVIOUS PAGE.

AR 9-29-97

Case 29:

Thickness = 310m
 Period = 200
 Li = 0.1
 Ld = 0.1

Input file tpa.inp as supplied with TPA Version 3.1 Code.
 Base case data set Rev 3.1.1 9/22/97
 TPA 3.1, Job started: Fri Sep 26 15:54:05 1997
 Cumulative Releases from EBS, UZ, and SZ by Nuclide
 Summed Over All Subareas - Values for Each Vector

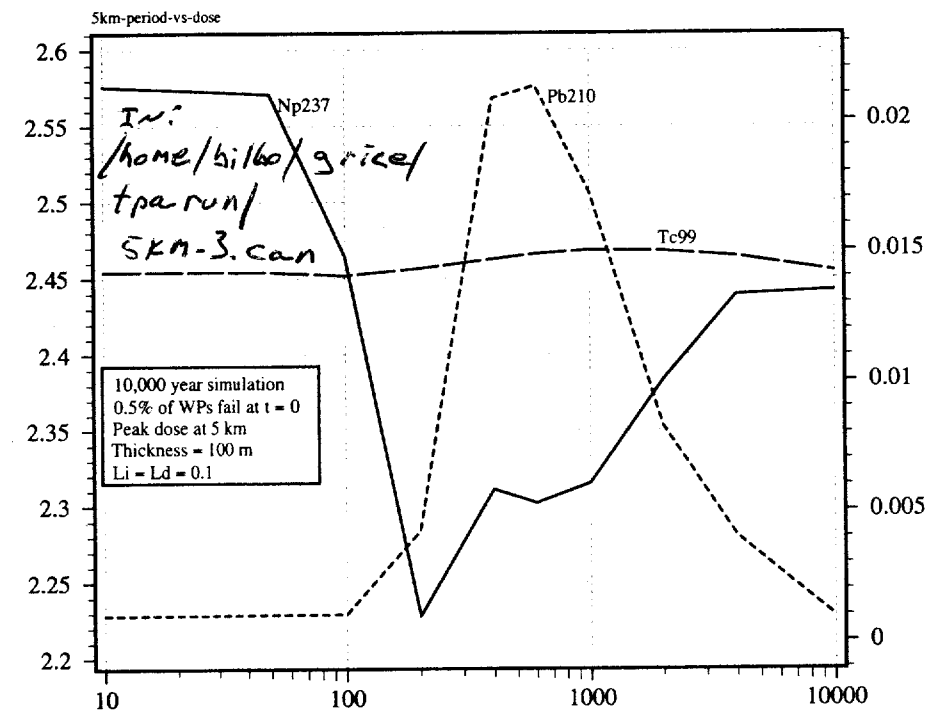
vector unitless	nuclide	ebsumrl Ci	uzsumrl Ci	szsumrl Ci
1	Cm246	0.0000E+00	0.0000E+00	0.0000E+00
1	U238	0.0000E+00	0.0000E+00	0.0000E+00
1	U235	0.0000E+00	0.0000E+00	0.0000E+00
1	Am241	0.0000E+00	0.0000E+00	0.0000E+00
1	Np237	0.0000E+00	0.0000E+00	0.0000E+00
1	Am243	0.0000E+00	0.0000E+00	0.0000E+00
1	Pu239	0.0000E+00	0.0000E+00	0.0000E+00
1	Pu240	0.0000E+00	0.0000E+00	0.0000E+00
1	U234	0.0000E+00	0.0000E+00	0.0000E+00
1	Th230	0.0000E+00	0.0000E+00	0.0000E+00
1	Ra226	0.0000E+00	0.0000E+00	0.0000E+00
1	Pb210	0.0000E+00	0.0000E+00	0.0000E+00
1	Cs135	0.0000E+00	0.0000E+00	0.0000E+00
1	I129	0.0000E+00	0.0000E+00	0.0000E+00
1	Tc99	0.0000E+00	0.0000E+00	0.0000E+00
1	N159	0.0000E+00	0.0000E+00	0.0000E+00
1	C14	0.0000E+00	0.0000E+00	0.0000E+00
1	Se79	0.0000E+00	0.0000E+00	0.0000E+00
1	Nb94	0.0000E+00	0.0000E+00	0.0000E+00
1	C136	0.0000E+00	0.0000E+00	0.0000E+00

AR 9-29-97

10-7-97

AR

TPA Code Sensitivity to Reflux Period



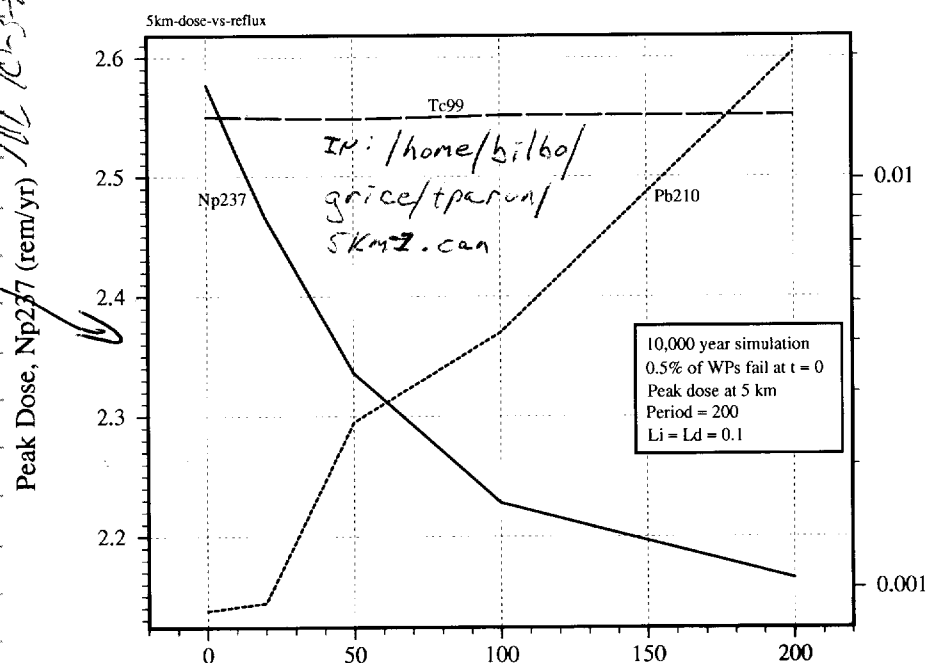
Peak Dose, Pb210 & Tc99 (rem/yr)

10-3-97

NOW USING NEW INPUT FILE - CHANGES RESULTS

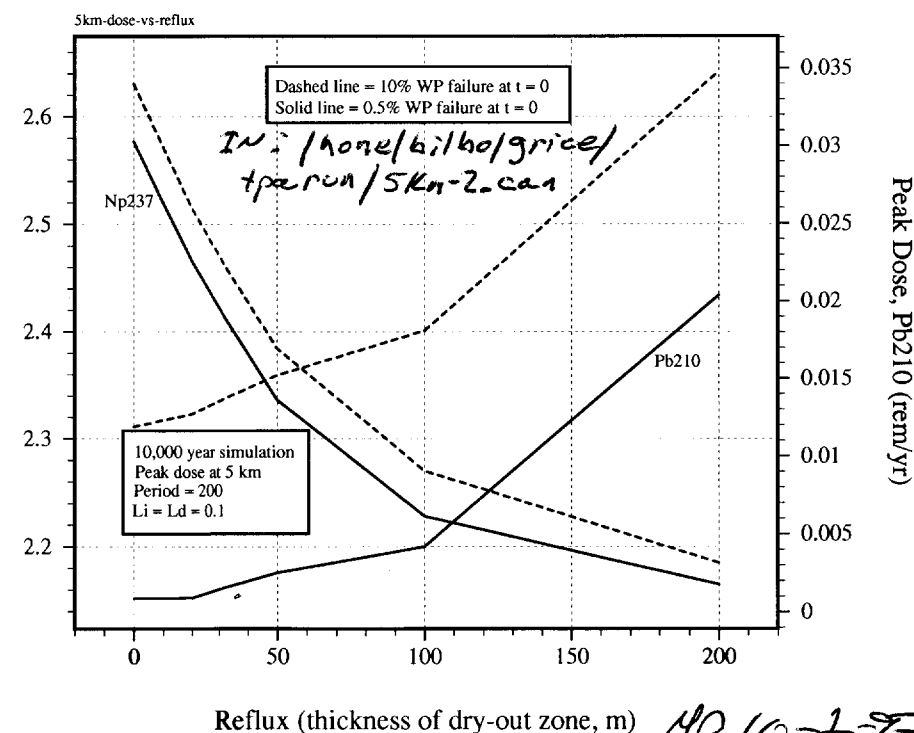
FROM HERE ON, INPUT FILE IS: tpa.inp.meanvalues.1

TPA Code Sensitivity, Reflux vs Peak Dose



Peak Dose, Pb210 & Tc99 (rem/yr)

TPA Code Sensitivity to WP Failure at t = 0



Peak Dose, Pb210 (rem/yr)

NOTE - THE OUTPUT FILES FROM WHICH
 THESE AND THE FOLLOWING 3 PLOTS WERE
 GENERATED ARE F.M. /home/bilbo/
 grice/tpa.run/npkdose-1.through
 npkdose-31.

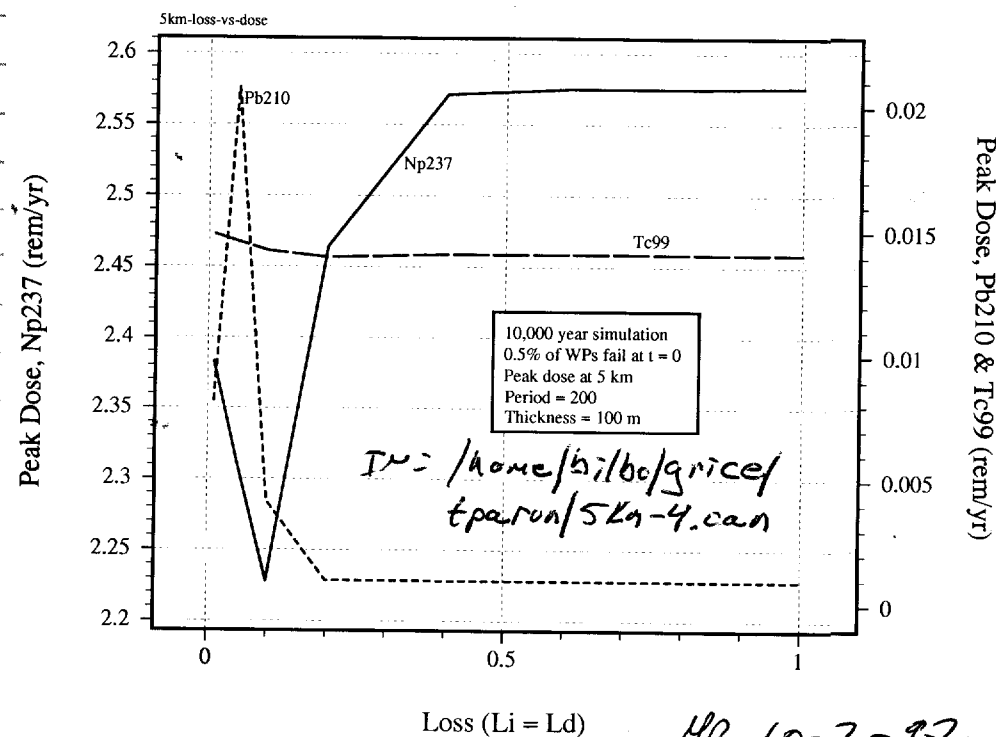
AR 10-7-97

AR 10-7-97

10-7-97

JR

TPA Code Sensitivity to Reflux Loss Parameters



JR 10-7-97

10-9-97

JR

RUNNING 100 REALIZATIONS OF REFLUX 1:

CHANGING CONSTANTS TO VARIABLES:

LENGTH OF REFLUX ZONE - UNIFORM - 10m - 200m

PERCHEN BUCKET VOLUME - UNIFORM - 0.2 - 0.8

ALSO - FaultFactor + FowFactor MADE CONSTANTS, 1.0 + 0.05, RESPECTIVELY.

SUBAREA WET REMAINS UNIFORM DISTRIBUTION

BUT VERY NARROW: 0.5 TO 0.50001 -

PROGRAM WON'T RUN IF IT IS A CONSTANT.

RUN FOR 20,000 YRS - LOOK @ 5 KM

EXCEPT AS NOTED ABOVE, INPUT FILE SAME AS: tpa.inp. manual values.

JR 10-7-97

700 RS

10-10-97

JR

- RUN (TPA CODE) STARTED YES TO WHAT CRASHED - MESSAGE ON SCREEN:

"logical unit 29 named 'diagnostic.out'

CORE DUMPED

istatus = ne.0

istatus = 54("release.e>release.out")

istatus = 34304

- NOTE - 12 REALIZATIONS WRITTEN TO OUTPUT FILE "infilper.res"

BUT - THE FILE "100 SAMPLES PARAMS" CONTAINS INFO ON 100 REALIZATIONS! - SIX VALUES FOR EACH VECTOR.

BUT - FILE "gwpldos.res" ONLY CONTAINS OUTPUT FOR 12 VECTORS (REALIZATIONS)

- RE-RUN SAME INPUT - SEE WHAT HAPPENS

THIS RUN IS IN: /home/bilbo/grice/tparun

REFLUX2:

RUNNING 100 REALIZATIONS FOR 20,000 YEARS - LOOKING AT DOSE AT 5 KM. CHANGED FAULTFACTOR, FOWFACTOR, + SUBAREA WET TO CONSTANTS: 1.0, 0.05, + 0.5; RESPECTIVELY. TO DO SO - HAD TO COMMENT OUT REFERENCES TO CORRELATIONS IN ~ LAST 30 LINES OF tpa.inp.

IR: /home/bilbo/grice/tparun2

REFLUX2 PARAMETERS:

REFLUX2 THICKNESS - UNIFORM - 10.0 - 200.0m

REFLUX2 PERIOD - UNIFORM - 1.0 - 100

REFLUX2 LOSS I - UNIFORM - 0.0 - 1.0

REFLUX2 LOSS D - UNIFORM - 0.0 - 1.0

10-13-97

NR

BOTH REFLEX1 + REFLEX2 RUN SUCCESSFULLY.
HOWEVER - THE SP.TPE FILE FOR REFLEX2
LESTS 2 REFLEX1 PARAMETERS AS VARIABLES
THIS SHOULDN'T OCCUR - WILL DISCUSS
w/ S. I. TAKHTA MONDAY.

- RE-RUNNING REFLEX2 WITH REFLEX2 PARAMETERS
CONSTANT OUT.

10-14-97

NR

- REFLEX2 RUN - RUN SUCCESSFULLY - NOW RUNNING
IND-TECH RUN FOR 10,000 YRS

OUTPUT OF SUCCESSFUL RUNS PUT INTO FILES
OF FORM:

REFLEX2 - 20ky - 5km - *.res
REFLEX1 - 20ky - 5km - *.res

IN: /home/bilbo/grice/tparun2 + tparun,
RESPECTIVELY.

NEW RUN: REFLEX2 - SAME AS ABOVE BUT
RUN FOR 100,000 YRS; ELMTE BASED 20 KM.

NOTE - FOR RUN DISCUSSION OF THIS &
PREVIOUS MAGES:

Run of Sisyphus
Factor = constant = 1.0
FOR FACTOR = constant = 0.05
SUB RUN WGT = constant = 0.5

IN: /sisyphus/home/bilbo/grice/tpatester

10-15-97

NR

NOTE - 10,000 yr REFLEX2 RUN STARTED YESTERDAY DID
NOT WRITE TO MOST *.res FILES - RUNNING IT
AGAIN.

10-16-97

AR

NEW RUN - REFLEX2, 100,000 yr @ 20km
IN: /home/bilbo/grice/tparun

10-17-97

NR

→ DONE

COMPLETED RUN WITH ALL VARIABLES HELD
CONSTANT EXCEPT THICKNESS OF DRY-OUT
ZONE FOR REFLEX2 - PURPOSE - NRC (SOFF
POHLE etc.) ASKED TO SEE EFFECT OF
REFLEX PARAMETERS ON AMOUNT OF WATER
PASSING THROUGH REPOSITORY KORTEN.

IN:

/home/bilbo/grice/rflx-vs-div

FILES NAMED: reflex2-period-*

NOTE - MISNAMED - SHOULD BE CALLED THICKNESS

RUNNING NEW TPA RUN ON SISYPHUS - SAME AS ABOVE EXCEPT
ALL VARIABLES HELD CONSTANT EXCEPT PERIOD FOR
REFLEX2. IN:

/home/bilbo/grice/rflx-vs-div

10/20/97

NR

100,000 YEAR RUNS @ 20km DONE FOR REFLEX1 +
REFLEX2. REFLEX2 OUTPUT IS:

/home/bilbo/grice/tpatester. FILES CALLED:
reflex2-100ky-20km-*.res.

OUTPUT GIVING
AMOUNT OF WATER
THAT RUNS TO THE
REPOSITORY
IN: RUN2.TPE

NAME CHANGE: RUN FOR REFLEX2 WHERE ALL
VARIABLES HELD CONSTANT - OUTPUT NOW
CALLED:
reflex2-THICKNESS-*.res, etc

RUN WHERE ALL HELD CONSTANT EXCEPT PERIOD
reflex2-PERIOD-*.res

IN: /home/bilbo/grice/rflx-vs-div

OUTPUT GIVING
VALUES OF
'INDIVAR' FROM
infilper.res to
raw3.txt.

10/20/97

MR

- Now TPA CODE SENSITIVITY RUN -
ALL VARIABLES HELD CONSTANT EXCEPT
LOSS FOR REFLUX2. IN:
/home/bilbo/grice/rlx-vs-div

10-26-97

MR

Re; Run WITH ONLY LOSS VARYING (DRY-OUT-ZONE LOSS)

RUN COMPLETED, OUTPUT SAVED AS:

reflux2-lossd-*.res IN:

/home/bilbo/grice/rlx-vs-div

Now RUN STARTED - REFLUX1 WITH ONLY
LENGTH OF REFLUX ZONE VARYING, IN:

/home/bilbo/grice/tparun

"ardivent" values from infilper.res IN
FILE RAW4.txt.

10-22-97

MR

RUN WITH ONLY LOSS VARYING (INFILTRATION LOSS) COMPLETED
OUTPUT SAVED AS:

reflux2-lossi-*.res IN:

/home/bilbo/grice/rlx-vs-div. 'ardivent' values
from infilper.res IN RAW5.txt.

10-27-97

MR

REFLUX1 RUNS - OUTPUT IN:

~~home/sa~~ /home/bilbo/grice/tparun

RUN FOR 20,000 YRS, OUTPUT @ 5 KM DOWN SEAPORT:

"reflux1-20ky-5km-*.res"

100,000 YRS, 20 KM:

"reflux1-100ky-20km-*.res"

RUNS VARYING ONLY ONE REFLUX PARAMETER AT A TIME:

VARYING ONLY LENGTH - ALL OTHER TPA CODE PARAMETERS = CONSTANT:
"reflux1-length-*.res", raw6.txt

10-22-97

MR

RUN VARYING ONLY PERCHED BUCKET VOLUME:
"reflux1-bucket-*.res", raw7.txt

RUN VARYING ONLY MAXIMUM FLUX:

"reflux1-flux-*.res", raw8.txt

REFLUX2 RUNS - OUTPUT IN:

/home/bilbo/grice/tparun2 AND:

/home/bilbo/grice/rlx-vs-div

NOTE - ALL OUTPUT

NOW IN DIRECTORY

...tparun2.

OUTPUT IN ... tparun2:

RUN FOR 20,000 YRS, 5 KM:

reflux2-20ky-5km-*.res

RUN FOR 10,000 YRS, 5 KM:

reflux2-10ky-5km-*.res

RUN FOR 100,000 YRS, 20 KM:

reflux2-100ky-20km-*.res

RUN WHERE ONLY THICKNESS VARIED - ALL OTHER
PARAMETERS HELD CONSTANT:

reflux2-thickness-*.res

RUN WHERE ONLY PERIOD VARIED:

reflux2-period-*.res

RUN WHERE ONLY LOSS - DRYOUT ZONE VARIED:

reflux2-lossd-*.res

RUN WHERE ONLY LOSS - INFILTRATION VARIED:

reflux2-lossi-*.res

MR

10-27-97

10-27-97

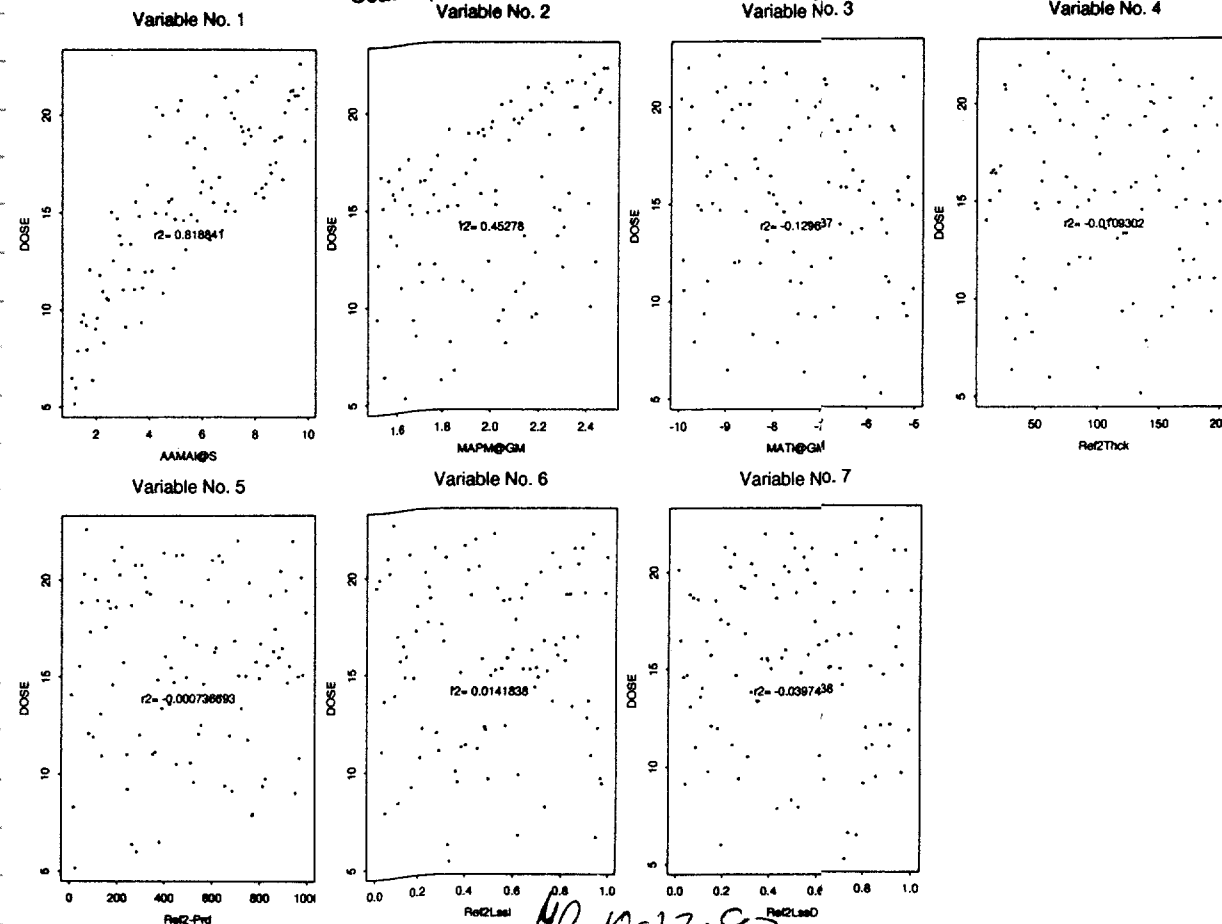
MR

THE PLOT BELOW, AND THE PLOTS ON THE FOLLOWING PAGES ARE RESULTS OF TPA CODE SENSITIVITY RUNS. THE RESULTS OF THE RUNS ARE IN THE DIRECTORIES SPECIFIED ON PAGES 20+21.

THESE RESULTS WERE PLOTTED USING Splus.

Scatter plots of Data vs. Dose: Reflux2, 20 ky, 5 km

MR 10-27-97

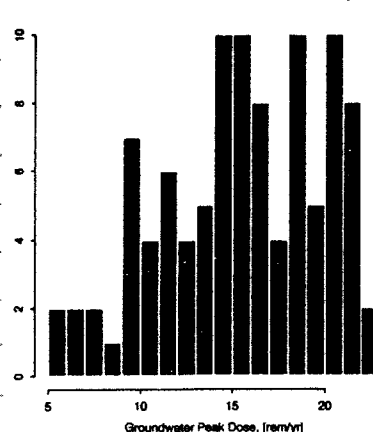


MR 10-27-97

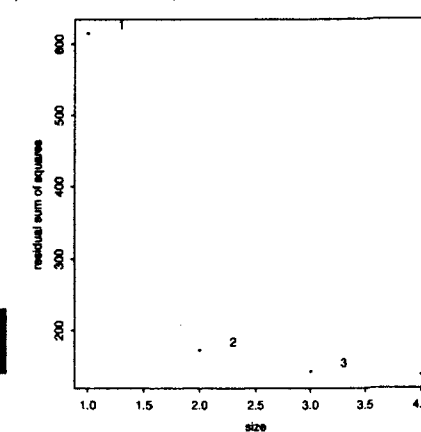
MR 10-27-97

REFLUX2, 20ky, 5km

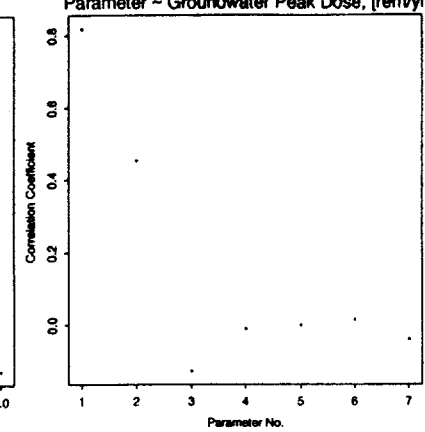
Distribution of Groundwater Peak Dose, [rem/y]



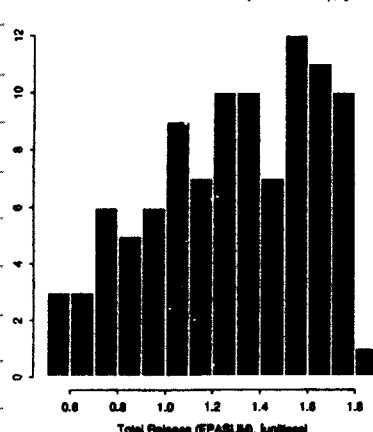
Stepwise Reduction in Error



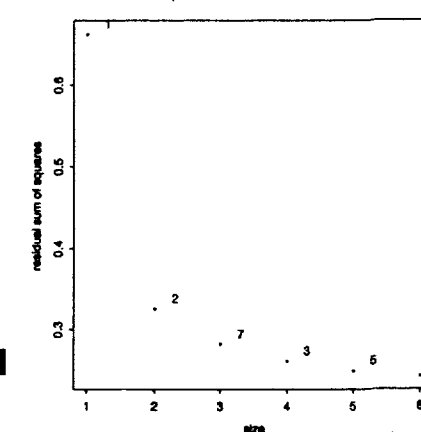
Correlation Coefficients Parameter ~ Groundwater Peak Dose, [rem/y]



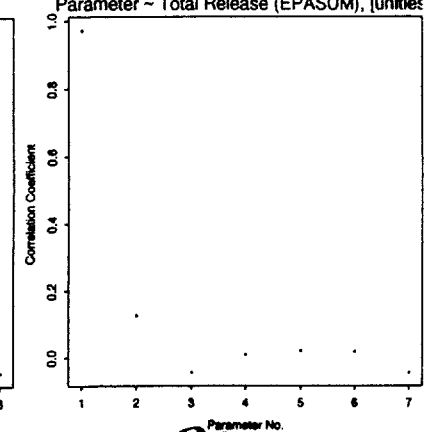
Distribution of Total Release (EPASUM), [unitless]



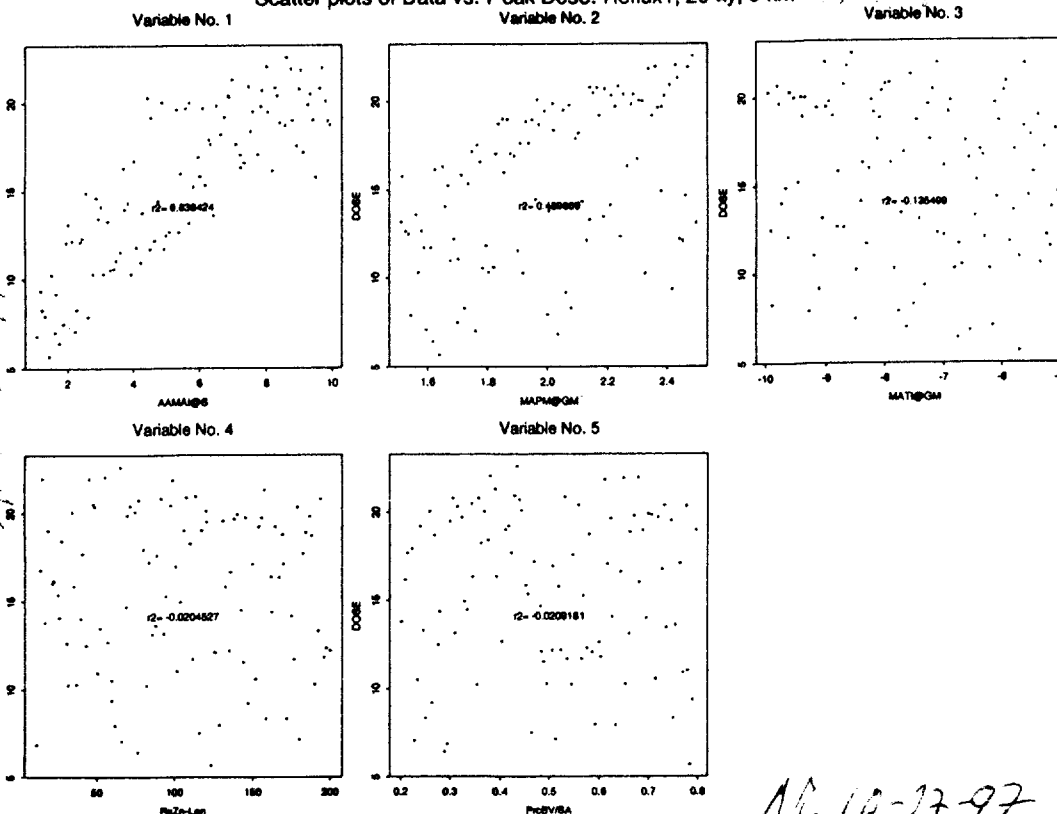
Stepwise Reduction in Error



Correlation Coefficients Parameter ~ Total Release (EPASUM), [unitless]



Scatter plots of Data vs. Peak Dose: Reflux1, 20 ky, 5 km

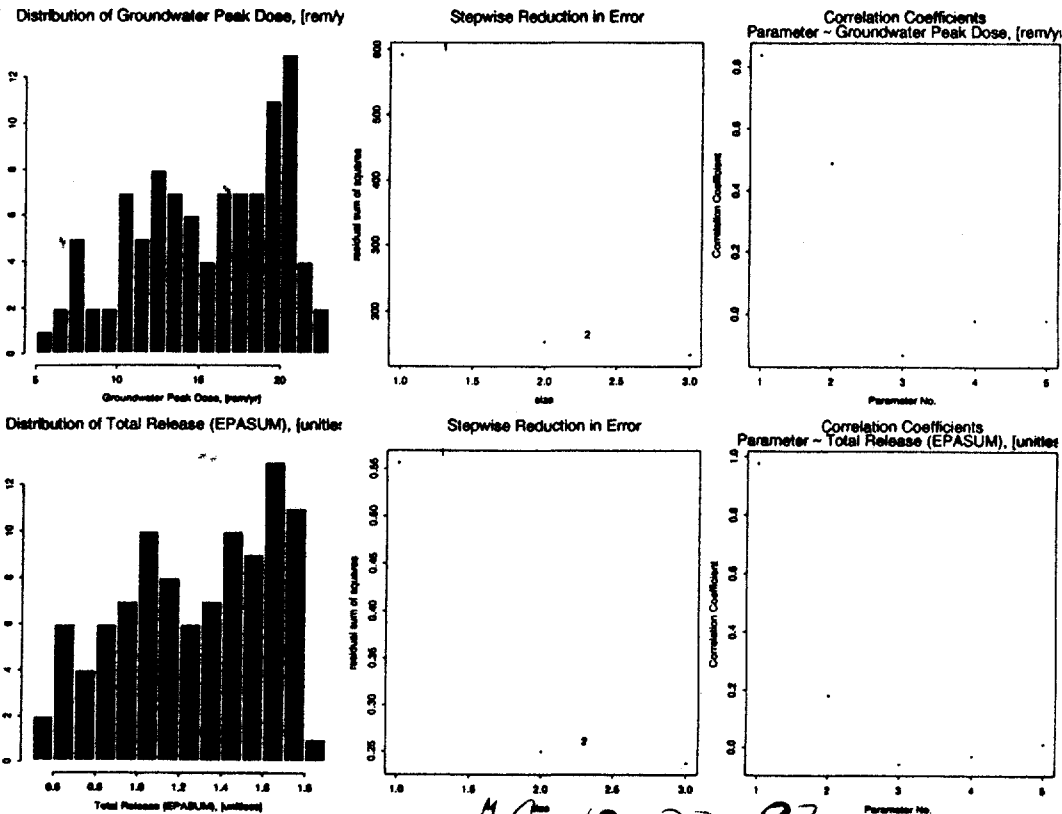


6-6-01-01-01

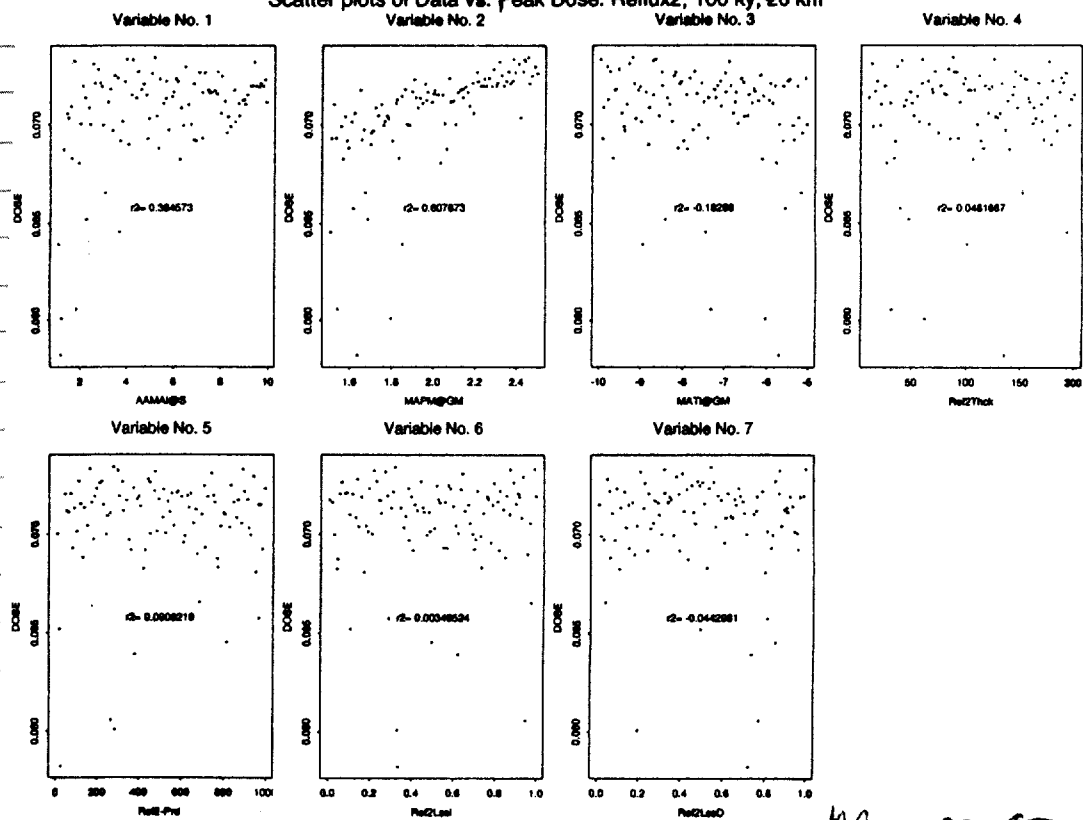
MR 10-27-97

10-27-97

NR 10-97-27
Kerfuz, 20K, 20 km



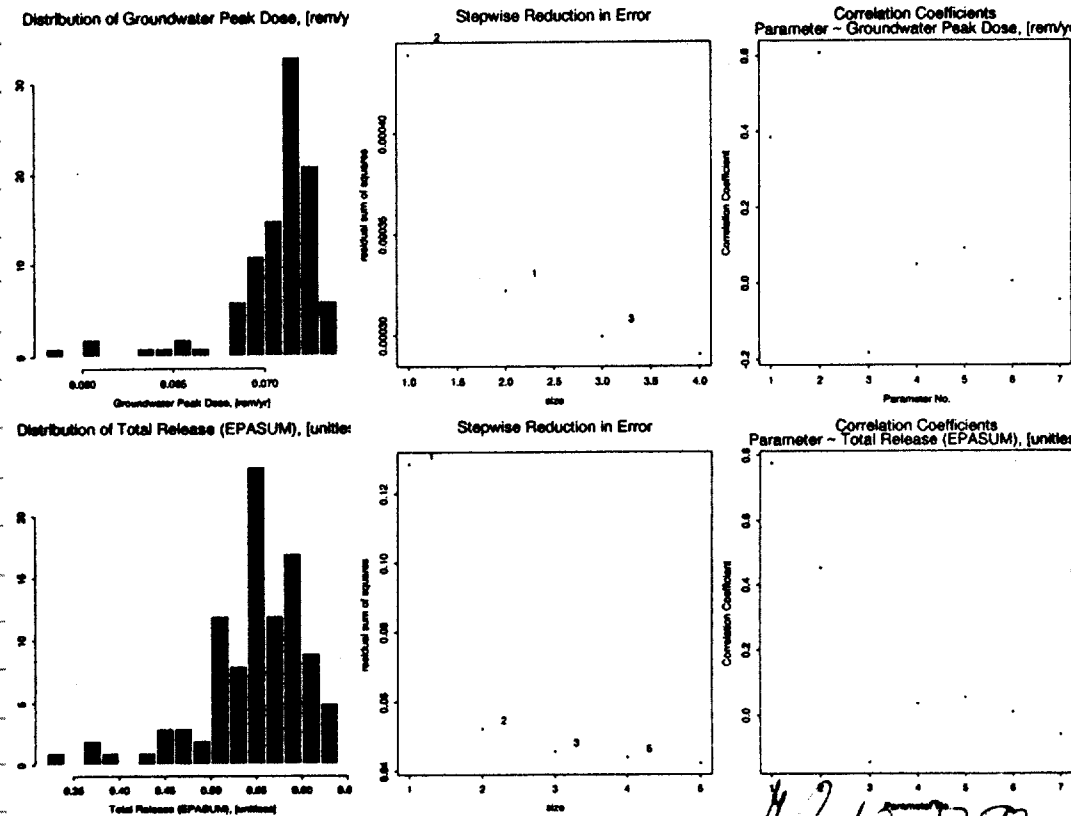
Scatter plots of Data vs. Peak Dose: Reflux2, 100 ky, 20 km



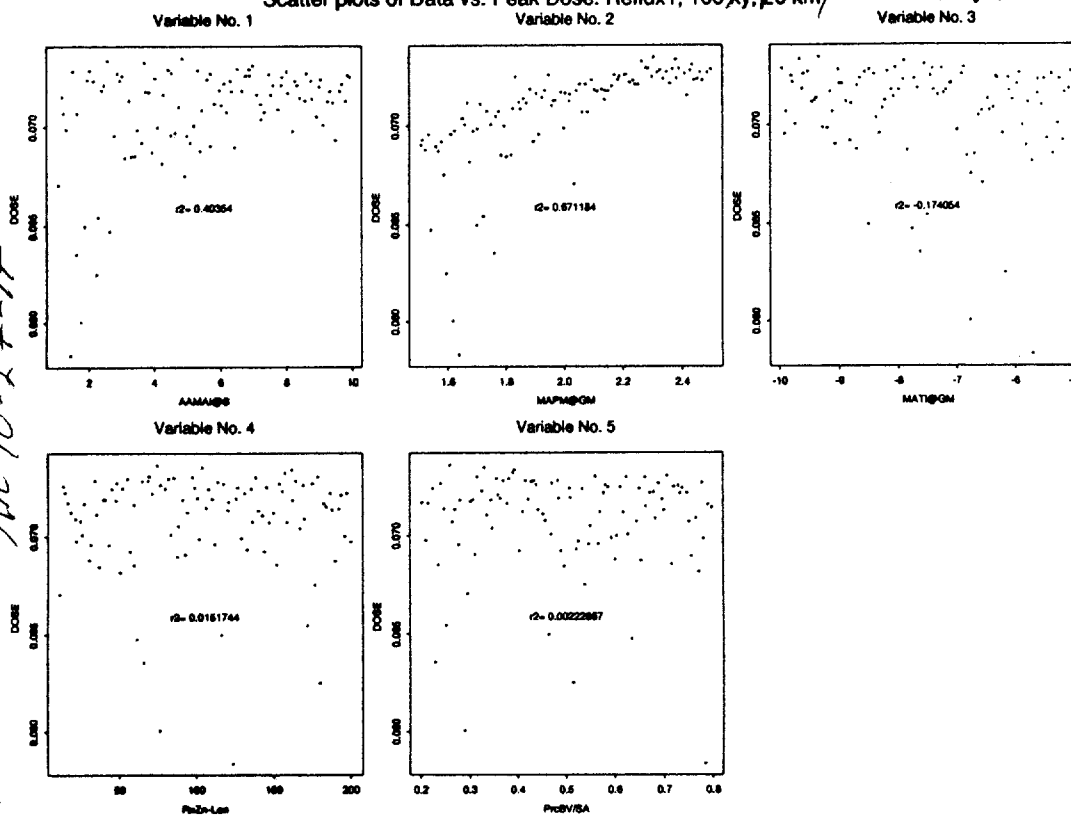
NR 10-27-97

Reflux2, 100K, 20 km NR 10-27-97

10-27-97



Scatter plots of Data vs. Peak Dose: Reflux1, 100 ky, 20 km

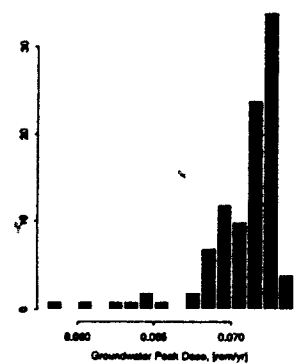


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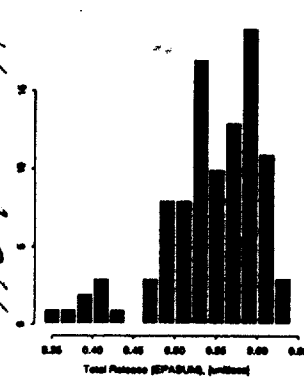
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NR

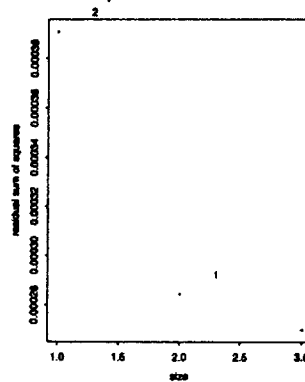
Distribution of Groundwater Peak Dose, (rem/yr)



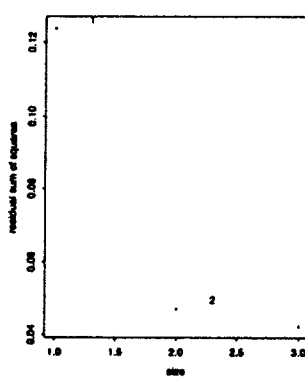
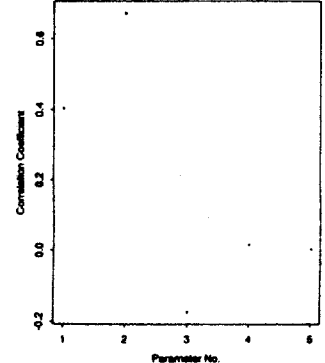
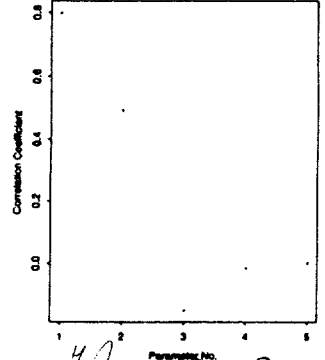
Distribution of Total Release (EPASUM), (unitless)



Stepwise Reduction in Error



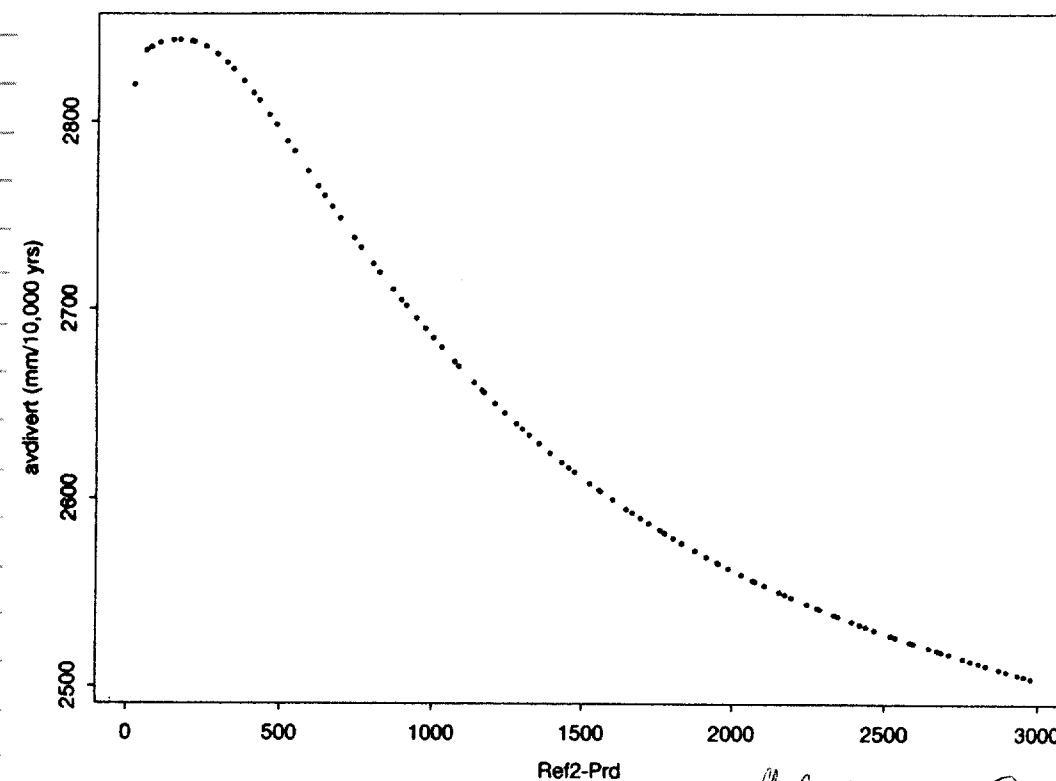
Stepwise Reduction in Error

Correlation Coefficients
Parameter ~ Groundwater Peak Dose, (rem/yr)Correlation Coefficients
Parameter ~ Total Release (EPASUM), (unitless)

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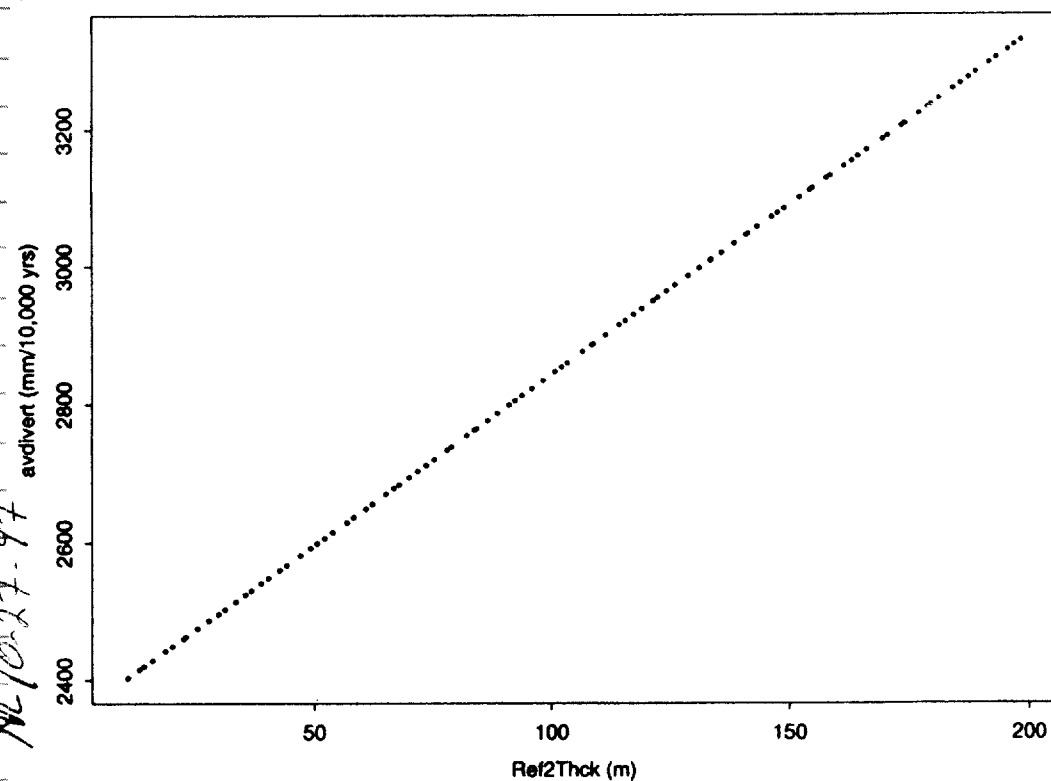
NR

Effect of Reflux2 parameter 'Ref2-Prd' on avdivert



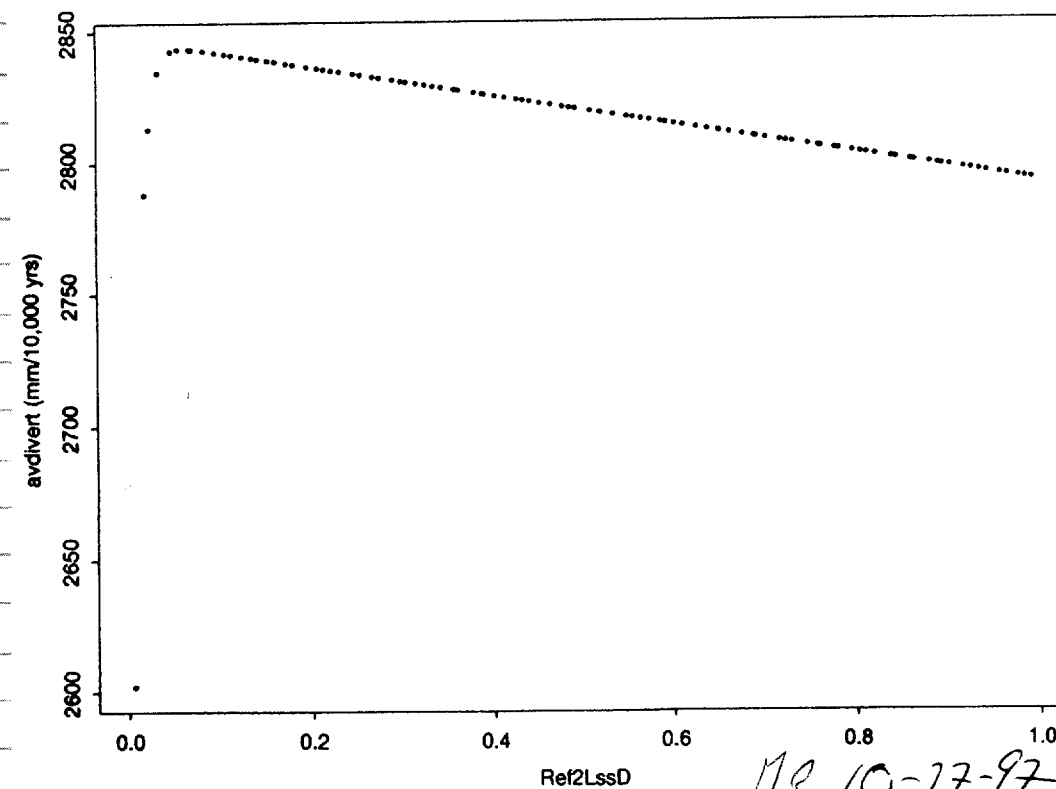
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Effect of Reflux2 parameter 'Ref2Thck' on avdivert



NR 10-27-97

Effect of Reflux2 parameter 'Ref2LssD' on avdivert



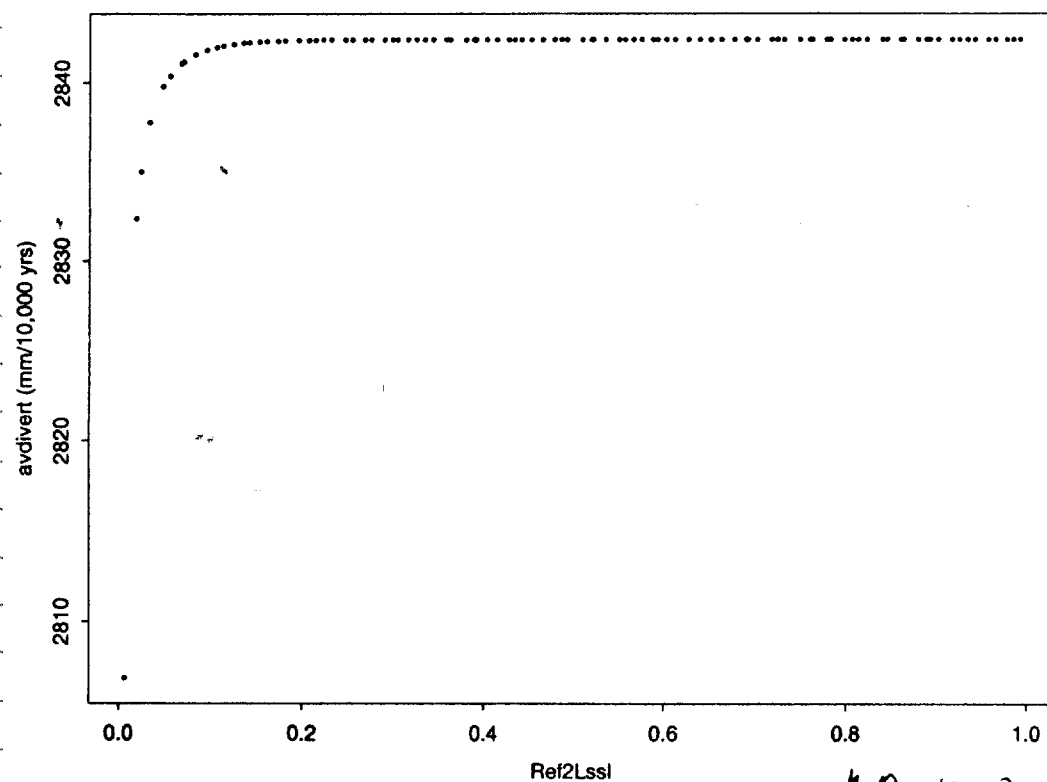
NR 10-27-97

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NR

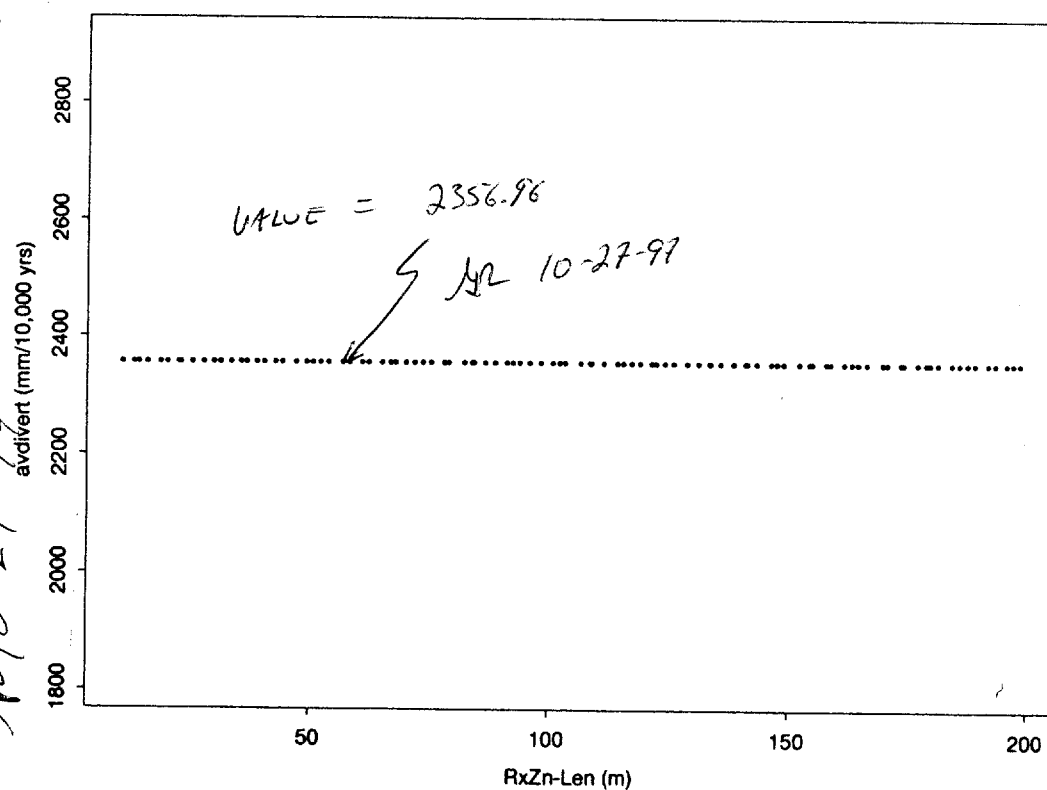
NR 10-27-97

Effect of Reflux2 parameter 'Ref2Lssl' on avdivert



NR 10-27-97

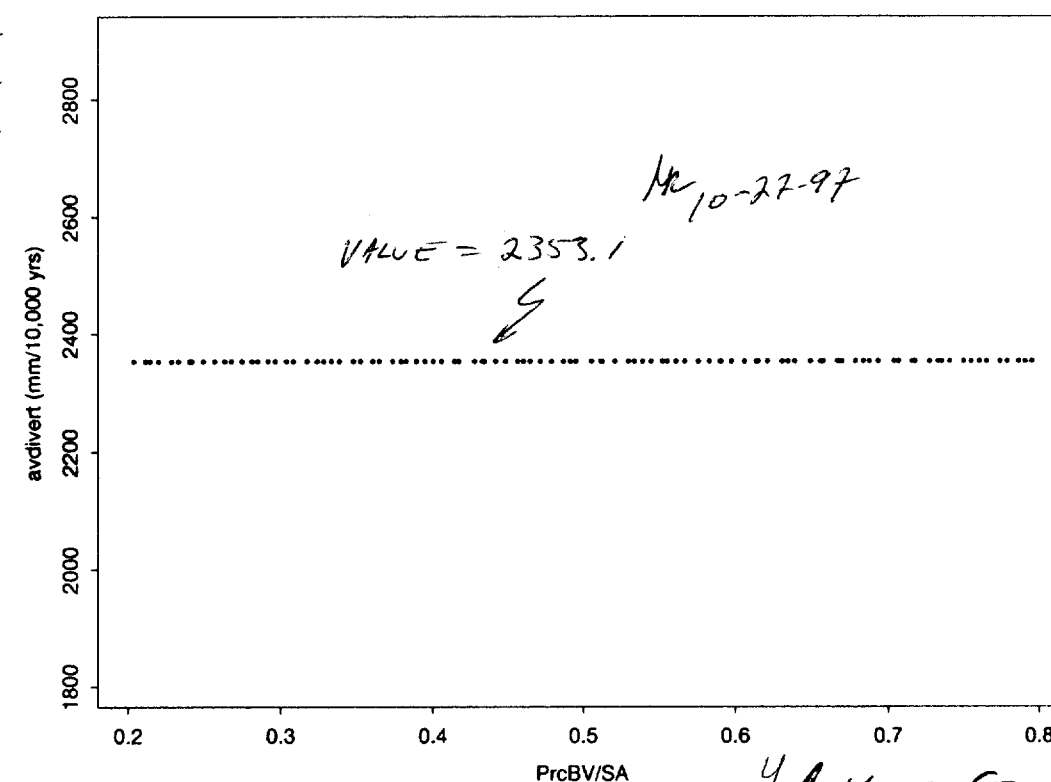
Effect of Reflux1 parameter 'RxZn-Len' on avdivert



NR 10-27-97

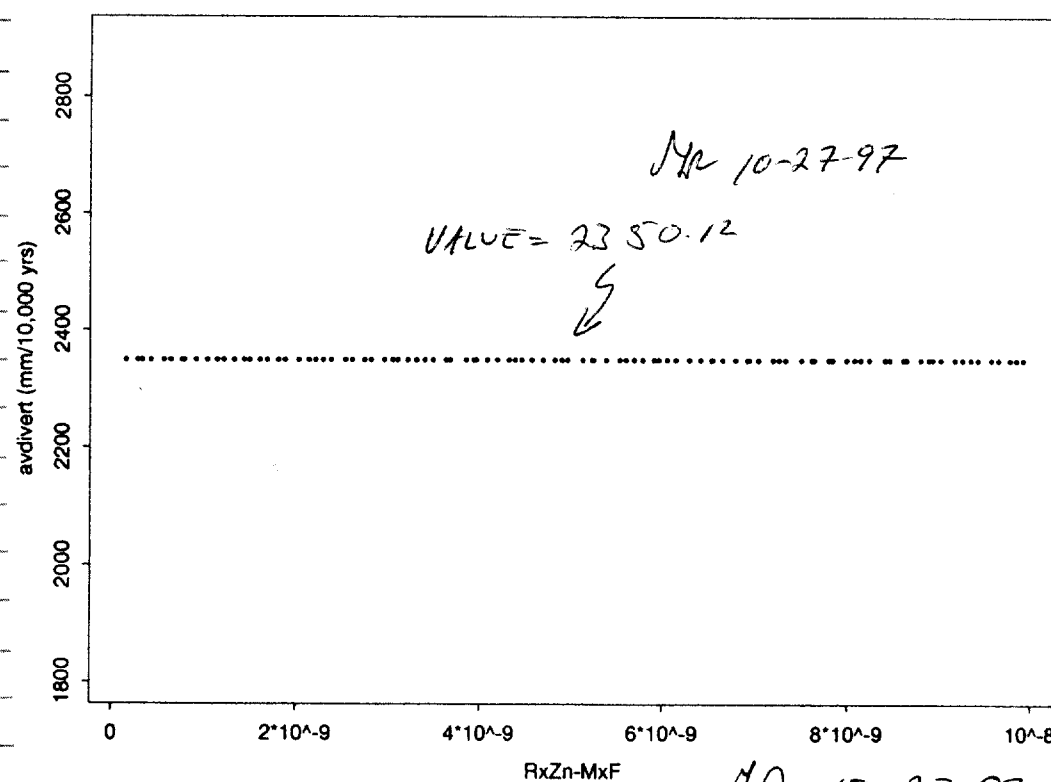
NR 10-27-97

Effect of Reflux1 parameter 'PrcBV/SA' on avdivert



NR 10-27-97

Effect of Reflux1 parameter 'RxZn-MxF' on avdivert



NR 10-27-97

11-12-97

RUNNING THE TPA CODE WITH TEMPERATURE-HUMIDITY TABLES GENERATED BY METRA.

3 METRA RUNS WERE PERFORMED:

"1.0-old.dat", "5.5-old-1.dat", and "10.0-old-1.dat"

THESE RUNS IN: /home/bilbo/grice/3d/oldbase

THE TEMPERATURE & HUMIDITY OUTPUT PRODUCED BY METRA WAS CONVERTED TO THE FORM REQUIRED BY THE TPA CODE USING THE FORTRAN PROGRAM "tmp-rh-1.f" - THIS IS A SLIGHT MODIFICATION OF A CODE WRITTEN BY RUI CHEN.

FORTRAN CODE, 11-12-97

THE METRA RESULTS AND TRANSFORMED OUTPUT ARE IN: /home/bilbo/grice/testcode

THE OUTPUT IN THE FORM REQUIRED BY THE TPA CODE IS:

"1-old-t-rh", "5.5-old-t-rh", and "10-old-t-rh"

THE TPA RUNS THEMSELVES WERE DONE IN: /home/bilbo/grice/tparun

THE OUTPUT IS IN THE FILES:

*-old-t-rh-gupkds
*-old-t-rh-npkdset
*-old-t-rh-nelguys
*-old-t-rh-wpsfail
*-old-t-rh-cunrel

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2-18-98

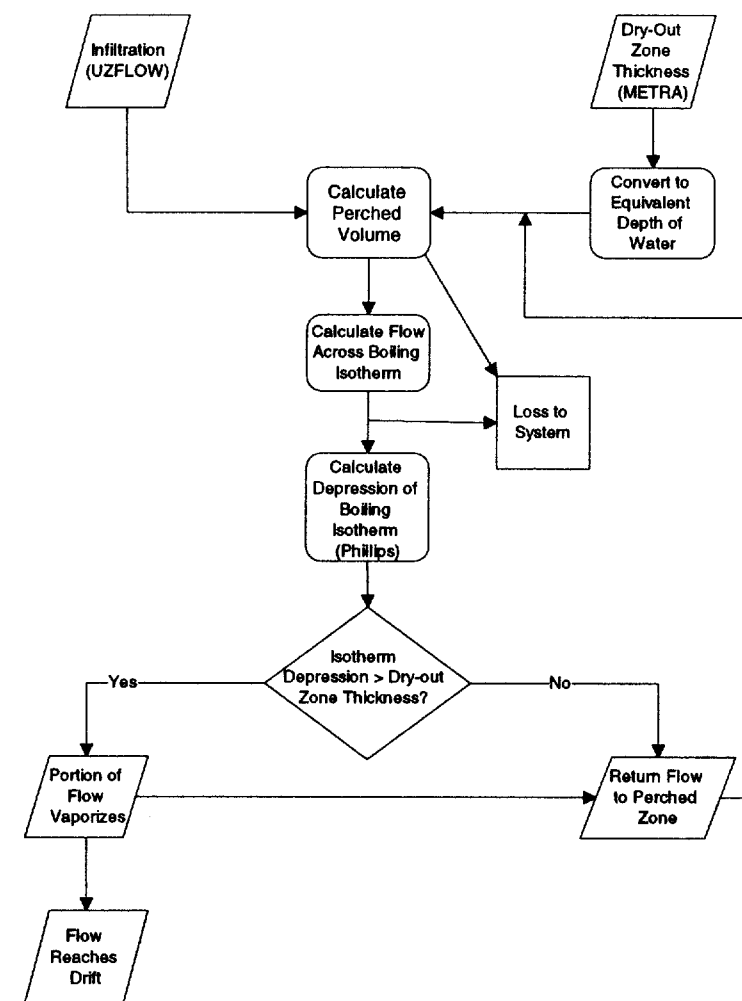
11/2

NEW REFLUX SUBROUTINE TO BE INCORPORATED INTO NEXT VERSION OF TPA CODE. THIS IS MEANT TO REPLACE REFLUX2 AND REFLUX1 MODULES.

FLOWCHART OF NEW REFLUX MODULE. THIS IS FOLLOWED BY BOTH THE FORTRAN CODE AND THE EXCEL WORKSHEET PROVIDED ON THE PROCEEDING PAGES.

11/2 2-18-98

Reflux Calculation
for one Time Step



11/2 2-18-98

2-20-98

REFLUX CODE - VERSION OF 2-18-98

PROGRAM REFLUX1_98

* By GRice January - February, 1998

* NOTE: this is a stand-alone program. Thus, it uses files and
 * contains subroutines that will not be included in the final version.
 * The final version will be a subroutine of the TPA code.

* The OUTPUT of this program is 'reachDrift': the amount of water
 * that reaches the drift each year. The program reads two inputs:
 * infiltration and dry-out zone thickness as they vary with time.

```
REAL Qm3PerYrinSA(100000), SAarea, thickness(100000)
REAL interpQm3PerYrinSA(100000), interpThick(100000)
INTEGER ntim, nthick, iSA, timestep(100000), tim(100000)
INTEGER interp_tim(100000)
REAL MPrs_TSw, initSat, residSat
REAL equivThick(100000), perchedVol(100000)
REAL reachDrift(100000), loss(100000)
```

* Parameters:

cellLength = length of unit cell holding one waste package. Units = m.
 cellWidth = width of unit cell holding one waste package. Units = m.
 delEqTh = change in equivThick each year. Units = m.
 delT = Thermal gradient in vicinity of boiling isotherm. CNWRA
 experiment (Green et al.) indicated value of - 700. Units = none.
 depress = distance boiling isotherm depressed by flow of water. Units = m
 equivThick = Water equivalent of interpThick. Units = m.
 h = enthalpy of phase change. Units = J/kg
 initSat = initial saturation of TSW matrix. Units = none
 interpQm3PerYrinSA = Interpolated values of Qm3PerYrinSA created by interpolation
 subroutine (maplist). Units = m³/yr
 interp_tim = array in which times go from 1 to end (e.g., 10000 years) in increments
 one year. Created to allow interpolater (subroutine maplist) to create
 interpolated values of infiltration (interpQm3PerYrinSA). Units = none
 interpThick = Interpolated values of thickness created by interpolation
 subroutine (maplist). Units = m
 iSA = subarea (SA) number currently being evaluated. Passed from main.
 kRock = Thermal conductivity of rock. Units = W/m-K
 MPrs_TSw = matrix porosity of repository horizon - Topopah Springs tuff (TSw).
 Units = none.
 n2 = number of years for which interpolated values of Qm3PerYrinSA
 and dry-out zone thickness (interpQm3PerYrinSA and interp_thick) will
 be produced. Number of years in interp_tim.
 nthick = number of values in table that gives thickness of dry-out zone vs time
 ntim = number of times in ntim array. Passed from main.
 perchedVol = Volume of water perched above dry-out zone
 per unit cell (waste package). Units = m³.
 Q = Steady flowrate, a function of perched volume. Flow that crosses boiling
 isotherm. Units = m³/s
 Qm3PerYrinSA = water infiltrating from ground surface in a given year. Calculated
 by UZFLOW and passed from main. Units = m³/yr
 reachDrift = amount of perched water that reaches the drift each year.
 Units = m³/yr.

residSat = residual saturation of TSW matrix. Units = none
 rhoLiq = density of water at boiling isotherm. Units = kg/m³
 SAarea = area of subarea currently being evaluated. Passed from subroutine
 gsarea. Units = m².
 shed1Fact = fraction of perchedVol that disappears from system each year. Mechanism
 causing disappearance not specified.
 shed2Fact = fraction of 'Q' that disappears from system each year. Mechanism
 causing disappearance not specified.
 thickness = Thickness of dry-out zone above waste package. Read from file
 'dry_thick.dat'. Units = m
 tim = array containing times for which reflux is calculated. Passed from main
 program. Units = years
 vaporize = amount of water that crosses boiling isotherm but
 vaporizes before reaching drift. Units = m³/s.

Dr: /hone/bi/ko/
 grice/refluxcode/
 reflux1_98.f

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REFLUX CODE (cont)

```
OPEN(12, FILE = 'out')
OPEN(22, FILE = 'uzflow.res')
OPEN(24, FILE = 'stop.1')
OPEN(25, FILE = 'dry_thick.dat')
```

```
ntim = 8
nthick = 20
n2 = 20
```

```
MPrs_TSw = 0.14
initSat = 0.90
residSat = 0.00
```

* Subroutine to read timestep, tim, and Qm3PerYrinSA and thickness from files uzflow.res
 * and dry_thick.dat. It then calls a subroutine that interpolates
 * the infiltration and thickness data so that there are
 * n2 years of values for infiltration and thickness.
 * This subroutine also calls the subroutine that converts Qm3PerYrinSA
 * from m³/yr to m/yr.

```
CALL INTERPOLATE (ntim, timestep, tim, Qm3PerYrinSA, n2,
& interp_tim, interpQm3PerYrinSA, nthick, thickness,
& interpThick, iSA)
```

* Subroutine that calculates the amount of water perched above the dry-out zone.
 * The sources of this water are infiltration and water vaporized from the
 * dry-out zone. Also calls subroutines that calculate losses to system and
 * depression of boiling isotherm (Phillips).

```
CALL PERCHED_VOL (n2, interpQm3PerYrinSA, interpThick,
& MPrs_TSw, initSat, residSat, equivThick, perchedVol,
& reachDrift, loss)
```

* Write results to file 'out'

```
WRITE(12,101)
101 FORMAT(1x, ' I', 3x, 'reachDrift')
```

DO 20 I = 1, n2

```
WRITE(12,102) I, reachDrift(I)
102 FORMAT(1x, I3, 3x, F10.6)
```

20 CONTINUE

```
CLOSE (UNIT = 12)
CLOSE (UNIT = 22)
CLOSE (UNIT = 24)
CLOSE (UNIT = 25)
```

STOP

END

```
*****-72
*****-72
```

```
SUBROUTINE INTERPOLATE (ntim, timestep, tim, Qm3PerYrinSA, n2,
& interp_tim, interpQm3PerYrinSA, nthick, thickness,
& interpThick, iSA)
```

```
INTEGER ntim, nthick, n2
REAL Qm3PerYrinSA(ntim), SAarea, thickness(nthick)
REAL interpQm3PerYrinSA(n2), interpThick(n2)
INTEGER interp_tim(n2), iSA, timestep(n2), tim(ntim)
```

* Subroutine to read timestep, tim, and Qm3PerYrinSA lists from data file uzflow.res
 * This subroutine also calls the interpolating subroutine and the subroutine that
 * converts Qm3PerYrinSA from m³/yr to m/yr.

```
CALL uzflow_reader (ntim, timestep, tim, Qm3PerYrinSA,
& n2, interp_tim, interpQm3PerYrinSA)
```

* Subroutine that reads thickness of dry-out zone from data file. Also calls
 * interpolating subroutine

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MR

NEW REFLUX CODE (CONT)

```
CALL thickness_reader ( nthick, timestep, tim, thickness,
& n2, interp_tim, interpThick)
```

```
RETURN
END
```

```
*****
*****
```

```
SUBROUTINE uzflow_reader (ntim, timestep, tim, Qm3PerYrinSA,
& n2, interp_tim, interpQm3PerYrinSA )
```

```
REAL tim(ntim), Qm3PerYrinSA(ntim), interpQm3PerYrinSA(100000)
REAL interp_tim(100000)
INTEGER timestep(ntim), n2
```

```
5 FORMAT(I3, X, f5.1, X, f5.4)
```

```
DO 10 I = 1, ntim
```

```
READ(22, 5) timestep(I), tim(I), Qm3PerYrinSA(I)
```

```
10 CONTINUE
```

```
* Subroutine that converts UZFLOW output from m^3/yr to m/yr.
```

```
CALL convertUZ (ISA, ntim, Qm3PerYrinSA)
```

```
* Create interp_tim array with n2 years.
```

```
DO 20 I = 1, n2
```

```
interp_tim(I) = I
```

```
20 Continue
```

```
* CALL subroutine to interpolate values of Qm3PerYrinSA for n2 years.
* This subroutine provided by Sitakanta Mohanty.
```

```
CALL maplist (ntim, tim, Qm3PerYrinSA,
& n2, interp_tim, interpQm3PerYrinSA)
```

```
RETURN
END
```

```
*****
*****
```

```
SUBROUTINE thickness_reader ( nthick, timestep, tim, thickness,
& n2, interp_tim, interpThick )
```

```
INTEGER nthick, timestep(nthick), n2
REAL tim( nthick), thickness(nthick),
& interpThick(100000)
REAL interp_tim(100000)
```

```
5 FORMAT(I3, f7.1, f7.1)
```

```
DO 10 I = 1, nthick
```

```
READ(25, 5) timestep(I), tim(I), thickness(I)
```

```
10 CONTINUE
```

```
* Create interp_tim array with n2 years.
```

```
DO 20 I = 1, n2
```

```
interp_tim(I) = I
```

```
20 Continue
```

```
* CALL subroutine to interpolate values of thickness for n2 years.
* This subroutine provided by Sitakanta Mohanty.
```

```
*
```

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MR

REFLUX CODE (CONT)

```
CALL maplist ( nthick, tim, thickness,
& n2, interp_tim, interpThick)
```

```
RETURN
END
```

```
-----
c-----
subroutine maplist(n1, x1, y1, n2, x2, y2)
c-----
```

```
c map data in first list into second list
c given the first set of {x,y}, and the second set of {x}, find the
c second set of {y}
```

```
c
c n1 = input, integer, dimension of first array lists
c x1[n1] = input, double precision, array of x-values in first list
c y1[n1] = input, double precision, array of y-values in first list
c n2 = input, integer, dimension of second array lists
c x2[n2] = input, double precision, array of x-values in second list
c y2[n2] = output, double precision, array of y-values in second list
c values of y2 based on linear interpolation to of first list
c
```

```
* implicit double precision (a-h,o-z)
```

```
dimension x1(n1), y1(n1)
dimension x2(n2), y2(n2)
```

```
external ainterl
```

```
if( n1 .le. 0 ) then
```

```
print *, ' '
print *, ' ***** Error in maplist <<<*** '
print *, ' n1 .le. 0 '
print *, ' n1 = ', n1
print *, ' x1 = ', x1
print *, ' y1 = ', y1
print *, ' n2 = ', n2
print *, ' x2 = ', x2
print *, ' y2 = ', y2
INCLUDE 'stop.i'
```

```
elseif( n2 .le. 0 ) then
```

```
print *, ' '
print *, ' ***** Error in maplist <<<*** '
print *, ' n2 .le. 0 '
print *, ' n1 = ', n1
print *, ' x1 = ', x1
print *, ' y1 = ', y1
print *, ' n2 = ', n2
print *, ' x2 = ', x2
print *, ' y2 = ', y2
INCLUDE 'stop.i'
```

```
elseif( n1 .eq. 1 ) then
```

```
do k = 1, n2
y2(k) = y1(1)
enddo
else
do k = 1, n2
y2(k) = ainterl( n1, x1, y1, x2(k) )
enddo
endif
```

```
return
end
```

```
-----
function ainterl( n, t, v, tin )
c-----
```

```
c LINEAR interpolation in list of {time, value} data
c to find value at given time.
```

```
c
c n = input, integer, length of array values
c t[n] = input, double precision, array of times,
c assumed to be in ascending order
c v[n] = input, double precision, array of values
c tin = input, double precision, time at which interpolated
c value of "v" is requested
c ainterl = output, double precision, interpolated value
c if tin < t(1), then ainterl = v(1)
```

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MR

REFLUX CODE (CONT)

```
CALL maplist ( nthick, tim, thickness,
& n2, interp_tim, interpThick)
```

```
RETURN
END
```

```
-----
c-----
subroutine maplist(n1, x1, y1, n2, x2, y2)
c-----
```

```
c map data in first list into second list
c given the first set of {x,y}, and the second set of {x}, find the
c second set of {y}
```

```
c
c n1 = input, integer, dimension of first array lists
c x1[n1] = input, double precision, array of x-values in first list
c y1[n1] = input, double precision, array of y-values in first list
c n2 = input, integer, dimension of second array lists
c x2[n2] = input, double precision, array of x-values in second list
c y2[n2] = output, double precision, array of y-values in second list
c values of y2 based on linear interpolation to of first list
c
```

```
* implicit double precision (a-h,o-z)
```

```
dimension x1(n1), y1(n1)
dimension x2(n2), y2(n2)
```

```
external ainterl
```

```
if( n1 .le. 0 ) then
```

```
print *, ' '
print *, ' ***** Error in maplist <<<*** '
print *, ' n1 .le. 0 '
print *, ' n1 = ', n1
print *, ' x1 = ', x1
print *, ' y1 = ', y1
print *, ' n2 = ', n2
print *, ' x2 = ', x2
print *, ' y2 = ', y2
INCLUDE 'stop.i'
```

```
elseif( n2 .le. 0 ) then
```

```
print *, ' '
print *, ' ***** Error in maplist <<<*** '
print *, ' n2 .le. 0 '
print *, ' n1 = ', n1
print *, ' x1 = ', x1
print *, ' y1 = ', y1
print *, ' n2 = ', n2
print *, ' x2 = ', x2
print *, ' y2 = ', y2
INCLUDE 'stop.i'
```

```
elseif( n1 .eq. 1 ) then
```

```
do k = 1, n2
y2(k) = y1(1)
enddo
else
do k = 1, n2
y2(k) = ainterl( n1, x1, y1, x2(k) )
enddo
endif
```

```
return
end
```

```
-----
function ainterl( n, t, v, tin )
c-----
```

```
c LINEAR interpolation in list of {time, value} data
c to find value at given time.
```

```
c
c n = input, integer, length of array values
c t[n] = input, double precision, array of times,
c assumed to be in ascending order
c v[n] = input, double precision, array of values
c tin = input, double precision, time at which interpolated
c value of "v" is requested
c ainterl = output, double precision, interpolated value
c if tin < t(1), then ainterl = v(1)
```

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NR

REFLUX CODE (CON-7)

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```

c
c
c      if tin > t(n), then ainterl = v(n)
c
c      implicit double precision (a-h,o-z)
c      dimension t(n)
c      dimension v(n)
c
c      if( n .le. 0 ) then
c      print *, ' '
c      print *, ' ***>>> Error in ainterl <<<*** '
c      print *, ' n = ', n
c      INCLUDE 'stop.i'
c      elseif( n .eq. 1 ) then
c      ainterl = v(1)
c      return
c      elseif( tin .le. t(1) ) then
c      ainterl = v(1)
c      return
c      elseif( tin .ge. t(n) ) then
c      ainterl = v(n)
c      return
c      else
c      do k = 2, n
c      if( tin .lt. t(k) ) then
c      denom = (t(k)-t(k-1))
c      if( denom .lt. 1.0d-30 ) denom = 1.0d-30
c      frac = (tin - t(k-1))/ denom
c      ainterl = v(k-1) + frac*(v(k)-v(k-1))
c      return
c      endif
c      enddo
c      print *, ' '
c      print *, ' ***>>> Error in ainterl <<<*** '
c      print *, ' should never get here '
c      print *, ' n = ', n
c      print *, ' tin = ', tin
c      do i = 1, n
c      write(*,100) i, t(i), v(i)
c100  format( 'i,t,v= ', 3e13.4 )
c      enddo
c      INCLUDE 'stop.i'
c      end

```

```

*****
*****

```

```

SUBROUTINE convertUZ (ISA, ntim, Qm3PerYrinSA)

```

```

REAL SAarea, Qm3PerYrinSA(ntim)
INTEGER ISA, ntim

```

```

CALL gsarea (ISA, SAarea)

```

```

DO 10 I=1, ntim

```

```

    Qm3PerYrinSA(I) = Qm3PerYrinSA(I) / SAarea

```

```

10 CONTINUE

```

```

RETURN
END

```

```

*****
*****

```

```

SUBROUTINE gsarea (ISA, SAarea)

```

```

REAL SAarea
INTEGER ISA

```

```

SAarea = 1.0

```

```

RETURN
END

```

```

*****
*****

```

```

SUBROUTINE PERCHED_VOL (n2, interpQm3PerYrinSA,
* interpThick, MPrs_TSw, initSat, residSat,
* equivThick, perchedVol, reachDrift, loss)

```

REFLUX CODE (CON-7)

NR 2-20-98

```

INTEGER n2
REAL interpQm3PerYrinSA(n2), interpThick(n2)
REAL perchedVol(n2), cellWidth, cellLength, cellArea
REAL MPrs_TSw, initSat, residSat, equivThick(n2)
REAL maxThick, delEqTh(100000), loss(100000)
REAL reachDrift(n2)

```

```

cellWidth = 22.0
cellLength = 19.0
cellArea = cellWidth * cellLength

```

```

*
* The equivalent thickness of water perched above the dry-out zone is
* a function of the maximum dry-out zone thickness. When the dry-out zone
* thickness decreases, the maximum amount (minus losses calculated below)
* derived from the dry-out zone remains perched and available to flow toward
* the drift.
*

```

```

DO 10 I=1, n2

```

```

    IF(interpThick(I) .GT. maxThick) THEN
        maxThick = interpThick(I)
    ENDIF

```

```

    equivThick(I) = maxThick * (MPrs_TSw * (initSat
        - residSat))

```

```

    IF (I .GT. 1) THEN
        delEqTh(I) = equivThick(I) - equivThick(I-1)
        IF (delEqTh(I) .LT. 0.0) THEN
            delEqTh(I) = 0.0
        ENDIF
    ENDIF

```

```

10 CONTINUE

```

```

DO 20 I=1, n2

```

```

*
* Calculate volume of water perched above the dry-out zone. After the
* first year, losses are subtracted from the amount perched.
*

```

```

IF (I .EQ. 1) THEN
    perchedVol(I) = (interpQm3PerYrinSA(I)
        + equivThick(I)) * cellArea
ELSE
    CALL LOSSES (I, n2, perchedVol, interpThick, loss,
        reachDrift)

```

```

    perchedVol(I) = perchedVol(I-1) + ((interpQm3PerYrinSA(I)
        + delEqTh(I)) * cellArea) - loss(I)

```

```

20 CONTINUE

```

```

RETURN
END

```

```

*****
*****

```

```

SUBROUTINE LOSSES (I, n2, perchedVol, interpThick, loss,
    reachdrift)

```

```

INTEGER I, n2
REAL perchedVol(n2), loss(n2), shed1(100000), shed2(100000)
REAL interpThick(n2), reachDrift(n2), shed1Fact
REAL vaporize(100000)

```

```

shed1Fact = 0.01

```

```

*
* Shed1 is a loss to the system (mechanism undefined) that
* occurs every year.
*

```

```

shed1(I) = perchedVol(I-1) * shed1Fact

```

```

*
* Shed2, vaporize, and reachDrift are functions of flow beyond
* the boiling isotherm (Q). No flow occurs the first year.
*

```

NR 2-20-98

NR 2-20-98

NR 2-20-98

2-20-98

MR

REFLUX CODE (CONCL)

```
shed2(1) = 0.0
vaporize(1) = 0.0
reachDrift(1) = 0.0
```

```
IF(I .GT. 1) THEN
```

- * Call subroutine that calculates 3D depression of boiling isotherm at long times with steady-state flow rate. One year assumed to be long time.
- * Governing equation from O.M. Phillips, "The Infiltration of a Liquid Finger Down a Fracture into Superheated Rock", for CNWRA, 1994

```
CALL PHILLIPS_3D (I, n2, interpThick, perchedVol,
reachDrift, shed1, shed2, vaporize)
ENDIF
```

- * Total amount of water lost to system:

```
loss(I) = shed1(I) + shed2(I) + reachDrift(I)
```

```
RETURN
END
```

```
*****72
*****72
```

```
SUBROUTINE PHILLIPS_3D (I, n2, interpThick, perchedVol,
reachDrift, shed1, shed2, vaporize)
```

```
INTEGER I, n2
REAL interpThick(n2), perchedVol(n2), reachDrift(n2),
depress(100000), Q(100000), kRock, shed2Fact,
shed1(n2), shed2(n2), vaporize(n2)
```

- * Calculate amount of water that flows across the boiling isotherm. It depends on the amount of water that was perched the previous year.

```
Q(I) = ((perchedVol(I-1)-shed1(I)) / (86400 * 365)) * 0.01
```

```
rhoLiq = 958
h = 2.432E+06
kRock = 2.1
delt = 100.0
```

- * Calculate depression of boiling isotherm.

```
depress(I) = SQRT( (rhoLiq * Q(I) * h) / (kRock * delt) )
```

```
shed2Fact = 0.01
shed2(I) = Q(I)*shed2Fact
```

- * Calculate amount of flow (Q) that reaches the drift. Flow reaches drift only if the boiling isotherm is depressed more than the thickness of the dry-out zone. Amount of flow reaching drift is reduced by amount that vaporizes in transit and by an undefined loss: shed2. Shed2 (like shed1) represents water that leaves the system. It is lost even if no flow reaches the drift.

```
IF(depress(I) .GT. interpThick(I)) THEN
vaporize(I) = (interpThick(I)/depress(I)) * Q(I)
reachDrift(I) = (Q(I)- shed2(I) - vaporize(I)) * 86400 * 365
shed2(I) = shed2(I) * 86400 * 365
ELSE
reachDrift(I) = 0.0
shed2(I) = shed2(I) * 86400 * 365
ENDIF
```

```
RETURN
END
```

2-20-98

MR

EXCEL CODE USED TO CHECK RESULTS OF FORTRAN CODE:

MR 2-20-98

New Reflux 2/98 Incorporating Dry-out Zone Thickness and Depression of Boiling Isotherm				
Year	Infiltration (m)	Thickness (m)	Thick Diff (m)	Max Fact
1	0.003	5	5	1.00
2	0.003	10	5	1
3	0.003	100	90	1
4	0.004	80	-20	0
5	0.005	60	-20	0
6	0.004	20	-40	0
7	0.003	2	-18	0
8	0.003	2	0	0
9	0.003	2	0	0
10	0.003	2	0	0
11	0.003	2	0	0
12	0.003	2	0	0
13	0.0035	2	0	0
14	0.004	2	0	0
15	0.0045	2	0	0
16	0.005	2	0	0
17	0.004	2	0	0
18	0.003	1	-1	0
19	0.002	1	0	0
20	0.001	0	-1	0

EXCEL WORKSHEET ON W2BLOG 51 TO: W2BLOG 51 TO: C/JOSE 2-98/ REFLUX 2-98/ NEW REFLUX 2-98/

Step 1
Calculate volume of water perched above dry-out zone
This depends on infiltration and dry-out zone thickness
as well as values calculated in steps 2 and 4.

Year	Porosity	Saturation	Add Eqv - Thick (m)	Unit Area (m ²)	Perched Vol (m ³)
1	0.14	0.9	0.63	418	284.594
2	0.14	0.9	0.63	418	528.5159
3	0.14	0.9	11.34	418	5262.573
4	0.14	0.9	0	418	5211.098
5	0.14	0.9	0	418	5160.581
6	0.14	0.9	0	418	5110.116
7	0.14	0.9	0	418	5033.663
8	0.14	0.9	0	418	4958.55
9	0.14	0.9	0	418	4884.754
10	0.14	0.9	0	418	4812.25
11	0.14	0.9	0	418	4741.014

Step 2
Calculate first loss to system and volume of flow crossing
boiling isotherm

Year	Perched Vol (m ³)	First Loss Factor	Q Factor	First Loss (m ³ /yr)	Q (m ³ /yr)
1	284.594	0.01	0.01	2.84594	0
2	528.5158652	0.01	0.01	5.285159	2.819481
3	5262.572581	0.01	0.01	52.62573	5.212507
4	5211.097861	0.01	0.01	52.11098	52.09047
5	5160.580984	0.01	0.01	51.60581	51.58987
6	5110.116478	0.01	0.01	51.10116	51.08955

MR 2-20-98

* SEE NOTE ON PAGE 42
MR 2-24-98

MR 2-20-98

2-20-98

Me

7	5033.062508	0.01	0.01	50.33663	50.59015	
8	4958.550050	0.01	0.01	49.5855	49.83328	
9	4884.753997	0.01	0.01	48.84754	49.08965	
10	4812.250016	0.01	0.01	48.1225	48.35908	
11	4741.01419	0.01	0.01	47.41014	47.64128	
12	4671.023053	0.01	0.01	46.71023	46.93604	
13	4602.462586	0.01	0.01	46.02463	46.24313	
14	4535.30657	0.01	0.01	45.35307	45.56438	
15	4469.529292	0.01	0.01	44.69529	44.89954	
16	4405.105537	0.01	0.01	44.05106	44.24834	
17	4341.383575	0.01	0.01	43.41384	43.61054	
18	4267.26704	0.01	0.01	42.67267	42.9797	
19	4194.17211	0.01	0.01	41.94172	42.24824	
20	4111.126085	0.01	0.01	41.11126	41.5223	

Step 3
Calculate distance doiling isotherm depressed
(Phillip's 3-D Method)

Year	Q (m ³ /s)	rhoLq (kg/m ³)	h (J/kg)	Therm K Rock (W/m-K)	Delta T (K/m)	Depress (m)
1	0	958	2.43E+06	2.1	100	0
2	8.30632E-08	958	2.43E+06	2.1	100	0.959973
3	1.65288E-07	958	2.43E+06	2.1	100	1.354175

4	1.65200E-08	958	2.43E+06	2.1	100	4.281227
5	1.63580E-08	958	2.43E+06	2.1	100	4.260237
6	1.62004E-08	958	2.43E+06	2.1	100	4.239529
7	1.6042E-08	958	2.43E+06	2.1	100	4.218758
8	1.5802E-08	958	2.43E+06	2.1	100	4.18708
9	1.55662E-08	958	2.43E+06	2.1	100	4.155722
10	1.53340E-08	958	2.43E+06	2.1	100	4.124683
11	1.51069E-08	958	2.43E+06	2.1	100	4.093957
12	1.48833E-08	958	2.43E+06	2.1	100	4.063543
13	1.46638E-08	958	2.43E+06	2.1	100	4.033436
14	1.44484E-08	958	2.43E+06	2.1	100	4.003726
15	1.42375E-08	958	2.43E+06	2.1	100	3.974409
16	1.40311E-08	958	2.43E+06	2.1	100	3.945482
17	1.38288E-08	958	2.43E+06	2.1	100	3.916944
18	1.36288E-08	958	2.43E+06	2.1	100	3.88851
19	1.33982E-08	958	2.43E+06	2.1	100	3.855189
20	1.31668E-08	958	2.43E+06	2.1	100	3.822014

Step 4
Compare dry-out zone thickness with isotherm
depression. If thickness less than depression, Q (minus
loss and fraction that vaporizes) reaches drift.
Otherwise, Q (minus loss) returned to perched zone -
added to perched volume.

Year	Second Loss Factor	Second Loss (m ³ /yr)	Thick (m)	Depress (m)	IF - Result	Vaporize (m ³ /yr)	Reach Drift (m ³ /yr)
1	0	0	5	0	0	0	0
2	0.01	0.028195	10	0.959973	0	0	0
3	0.01	0.052125	100	1.354175	0	0	0
4	0.01	0.520995	80	4.281227	0	0	0
5	0.01	0.515899	80	4.260237	0	0	0
6	0.01	0.510898	20	4.239529	0	0	0
7	0.01	0.505902	2	4.218758	1	23.98344	26.10082
8	0.01	0.498333	2	4.18708	1	23.80335	25.53158
9	0.01	0.490896	2	4.155722	1	23.62508	24.97367
10	0.01	0.483591	2	4.124683	1	23.44862	24.42685
11	0.01	0.476413	2	4.093957	1	23.27395	23.89091
12	0.01	0.46936	2	4.063543	1	23.10105	23.36563
13	0.01	0.462431	2	4.033436	1	22.92989	22.8508
14	0.01	0.455644	2	4.003726	1	22.76099	22.34775
15	0.01	0.448995	2	3.974409	1	22.59432	21.85622
16	0.01	0.442483	2	3.945482	1	22.42988	21.37598
17	0.01	0.436105	2	3.916944	1	22.26784	20.9068
18	0.01	0.429797	1	3.88851	1	11.063	31.4000
19	0.01	0.422462	1	3.855189	1	10.95828	30.8655
20	0.01	0.415223	0	3.822014	1	0	41.10708

EXCEL RESULTS - COMPARE WITH
FORTRAN RESULTS ON
FOLLOWING PAGE.

2-20-98

Me

1 1.0 0.003
2 3.0 0.003
3 5.0 0.005
4 7.0 0.003
5 12.0 0.003
6 16.0 0.005
7 18.0 0.003
8 20.0 0.001

FORTRAN CASE
INFILTRATE
INPUT

Me 2-20-98
Me 2-20-98

1 1.0 5.0
2 2.0 10.0
3 3.0 100.0
4 4.0 80.0
5 5.0 60.0
6 6.0 20.
7 7.0 2.
8 8.0 2.0
9 9.0 2.0
10 10.0 2.0
11 11.0 2.0
12 12.0 2.0
13 13.0 2.0
14 14.0 2.0
15 15.0 2.0
16 16.0 2.0
17 17.0 2.0
18 18.0 1.0
19 19.0 1.0
20 20.0 0.0

FORTRAN CASE
THICKNESS
INPUT

1 reachDrift
2 0.000000
3 0.000000
4 0.000000
5 0.000000
6 0.000000
7 26.100811
8 25.531572
9 24.973656
10 24.426840
11 23.890903
12 23.365627
13 22.850798
14 22.347736
15 21.856205
16 21.375971
17 20.906790
18 31.496881
19 30.865484
20 41.107059

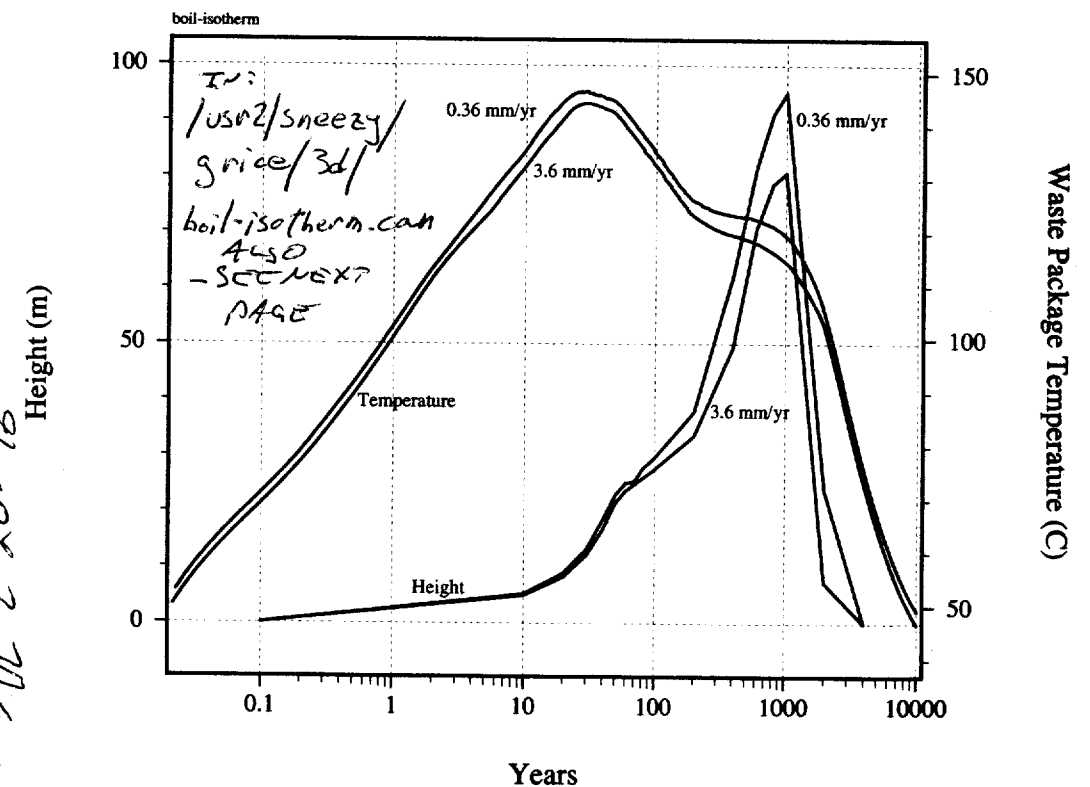
UNITS =
M³/YR

FORTRAN CASE
RESULTS. COMPARE
W/ EXCEL RESULTS
ON PREVIOUS PAGE

Me 2-20-98

METRA OUTPUT - THICKNESS OF DRY-OUT ZONE

Height of Boiling Isotherm (100 C) Above Waste Package



2-20-98

RESULTS OF METEOR RUNS

MR 2-20-98

Height of boiling isotherm above waste package for 3.6 mm/yr and 0.36 mm/yr infiltration rates. Power = 83 kW/acre. Data from runs "3d-3.6-3.dat" and "3d-0.36.dat". Top of waste depth = 343.4 m.

Time	3.6	0.36
.1	0	0
10	4.9	5.2
20	8.2	8.9
30	12.1	13.2
40	16.7	18.5
50	21.5	23
60	23.7	25.1
70	24.9	25.4
80	25.9	27.6
100	27.6	29.7
200	33.6	37.9
400	49.5	62.3
600	70.7	81.7
800	78.7	91.4
1000	80.7	95.1
2000	7.3	23.9
4000	0	0

TW:

1 usd 2/sneez/price/3d/
boil-isotherm

MR 2-20-98

2-24-98

NOTE:

VAPORIZATION SHOULD BE CALCULATED AFTER THE LOSS (SHED2) IS DEDUCTED FROM THE FLOW (Q). OTHERWISE, THE SUBSEQUENT VALUE (REACHDRIFT) MAY BECOME NEGATIVE. (ESPECIALLY WHEN DEPRESS ~ THICKNESS)

THE FORTRAN CODE HAS BEEN CORRECTED BY ALTERING THE LINE TO READ:

$$VAPORIZE(I) = (INTERATHICK(I) / DEPRESS(I))$$

$$* (Q(I) - SHED2(I))$$

THE EXCEL CODE HAS ALSO BEEN CORRECTED

3-13-98

MR

MODIFICATION TO NEW REFLUX CODE
(CALLING IT REFLUX3) - MASS BALANCE
SUBROUTINE:

MASS BALANCE SUBROUTINE ADDED TO REFLUX3 CODE:

MR 3-13-98

```

*****
SUBROUTINE MASS_BALANCE (n2, interpQm3PerYrinSA, equivThick,
6      cellArea, perchedVol, reachDrift,
6      loss, massBal)

INTEGER I, n2
REAL interpQm3PerYrinSA(n2), equivThick(n2), cellArea
REAL perchedVol(n2), reachDrift(n2), loss(n2)
REAL totIn(100000), totOut(100000), delStore(100000)
REAL delEqTh(100000), massBal(n2), relError(100000)

* Summ mass entering system

totIn(1) = (interpQm3PerYrinSA(1) + equivThick(1)) * cellArea

DO 10 I=2, n2
  delEqTh(I) = equivThick(I) - equivThick(I-1)

  IF (delEqTh(I) .LT. 0.0) THEN
    delEqTh(I) = 0.0
  ENDIF

  totIn(I) = (interpQm3PerYrinSA(I) + delEqTh(I)) * cellArea
  + totIn(I-1)
10 CONTINUE

* Summ mass leaving system

totOut(1) = loss(1)

DO 20 I=2, n2
  totOut(I) = loss(I) + totOut(I-1)
20 CONTINUE

totIn - totOut should equal perchedVol

DO 30 I=1, n2
  delStore(I) = totIn(I) - totOut(I)
  massBal(I) = delStore(I) - perchedVol(I)
  relError(I) = massBal(I) / ((totIn(I) + totOut(I)) / 2)
30 CONTINUE

WRITE(21, 101)
101 FORMAT(1x, 4x, 'I', 15x, 'totIn', 12x, 'totOut', 10x, 'perch',
6      15x, 'massBal', 8x, 'relError')

DO 40 I=1, n2
  WRITE(21, 102) I, totIn(I), totOut(I), perchedVol(I),
6      massBal(I), relError(I)
102 FORMAT(1x, 15, 3x, 5(6x, F12.6))
40 CONTINUE

RETURN
END
*****

```

MR 3-13-98

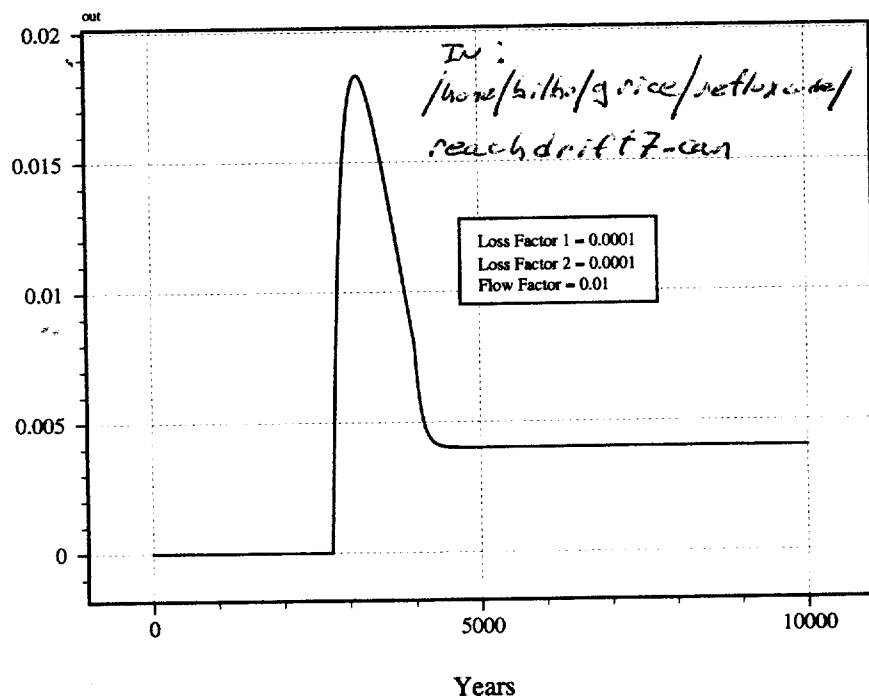
MR 3-16-98

3-16-98

MR

NEW REFLUX - RESULTS + MASS BALANCE
 MR 3-16-98
New Reflux

Flow Reaching Drift (m/yr)



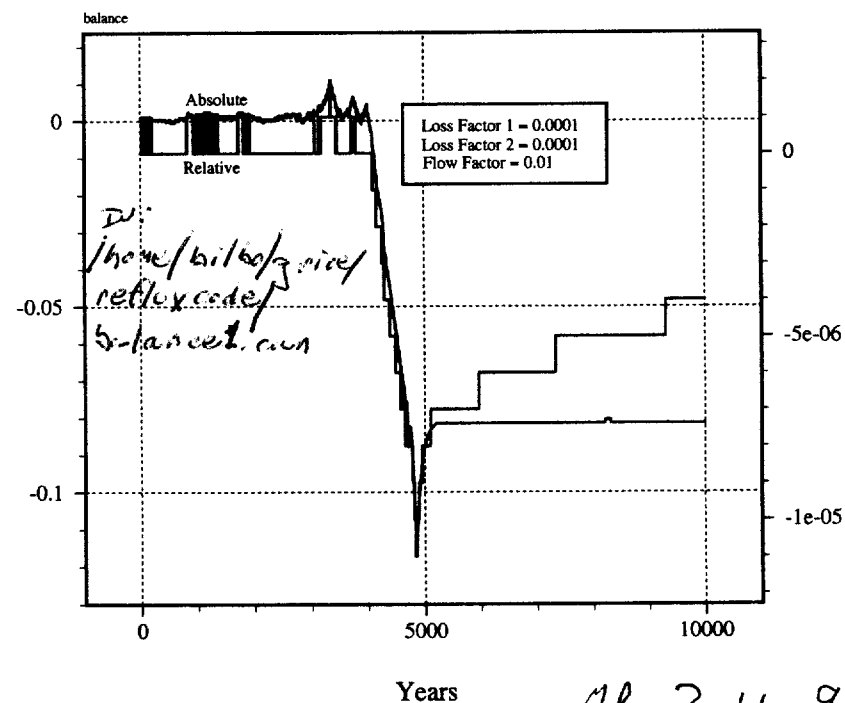
MR 3-16-98

REFLUX3 Mass Balance

MR 3-16-98

NOTE - SEE
 PAGE 52 -
 THE DOUBLE
 PRECISION OF
 THE TPA CODE
 (CUSTOMER
 STAFF HAD
 ELDI WATERS
 ERRORS IN
 TOGETHER

MR 7-13-98

Absolute Error (totIn-totOut-Store [m³])

MR 3-16-98

Relative Error (Absolute Error/(totIn+totOut)/2)

6-29-98

MR

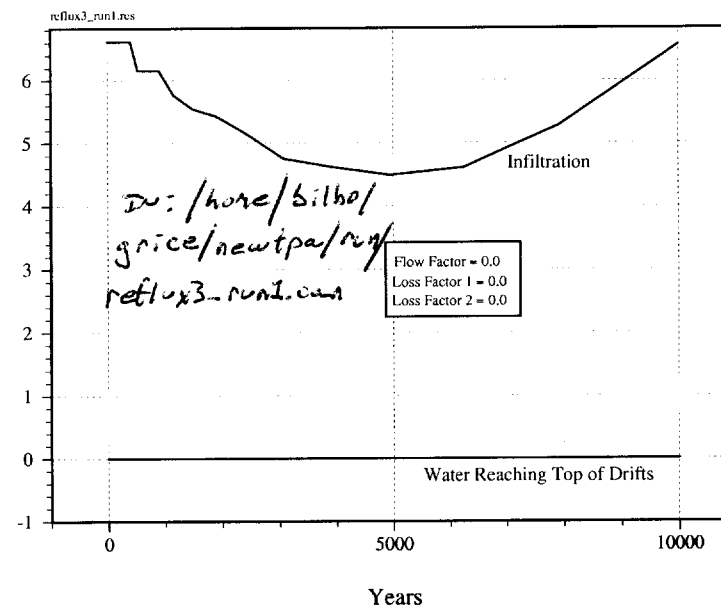
TESTING TPA CODE VERSION OF REFLUX3 -
 ARE RESULTS REASONABLE?

TEST #1: NO WATER PERMITTED TO LEAVE SYSTEM -
 FLOW AND LOSS FACTORS SET TO ZERO.

TPA Code REFLUX3 Results

MR 6-29-98

Flux (mm)



MR 6-29-98

TEST #1 RESULTS AS EXPECTED - NO WATER LEAVES
 SYSTEM.

TEST #2: NO DRY-OUT ZONE - ONLY WATER IS
 SYSTEM COMES FROM INFILTRATION:

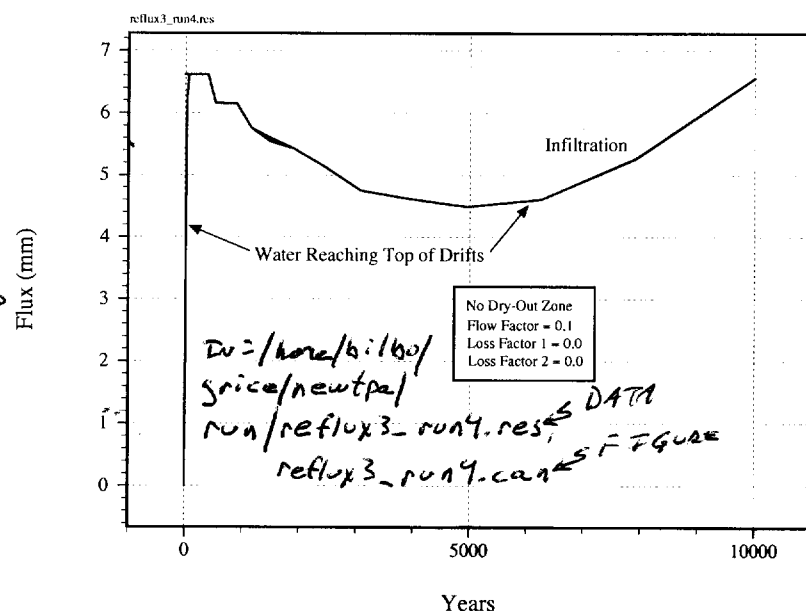
MR 6-29-98

6-29-98

MR

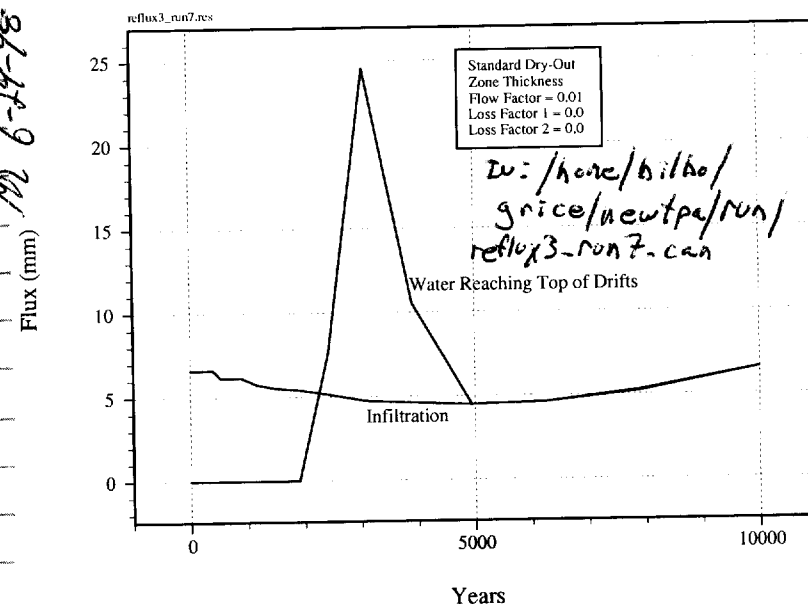
TPA Code REFLUX3 Results

MR 6-29-98



TEST #2 RESULTS AS EXPECTED: WITH NO WATER FROM DRY-OUT ZONE AND NO LOSSES, ALL INFILTRATION PASSES THROUGH SYSTEM AND WATER SOON REACHES DRIFTS AT INFILTRATION RATE. TIME THAT WATER REACHING DRIFTS + INFILTRATION RATE BECOME EQUAL DEPENDS ON FLOW FACTOR.

TEST #3 - TO COMPARE WITH TESTS #'S 4 + 5!
TPA Code REFLUX3 Results

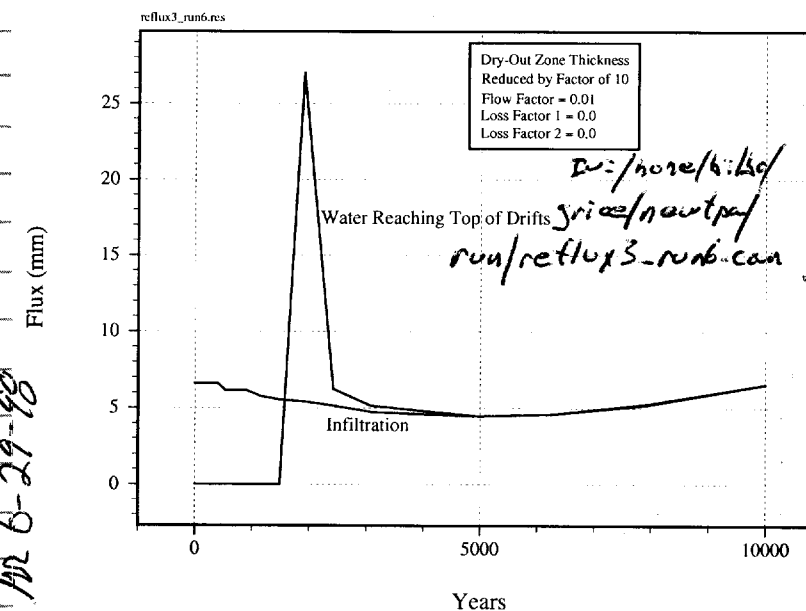


6-29-98

MR

TEST #4 - SAME AS #3 BUT DRY-OUT ZONE THICKNESS REDUCED BY FACTOR OF 10.
REDUCED

TPA Code REFLUX3 Results



RESULTS AS EXPECTED - AMOUNT OF WATER RETAINING IN DRIFTS IS REDUCED BY AMOUNT THAT VOLUME OF DRY-OUT ZONE WATER IS REDUCED: THAT REMAINS

REDUCTION IN DRY-OUT ZONE WATER (TOTAL VOLUME):

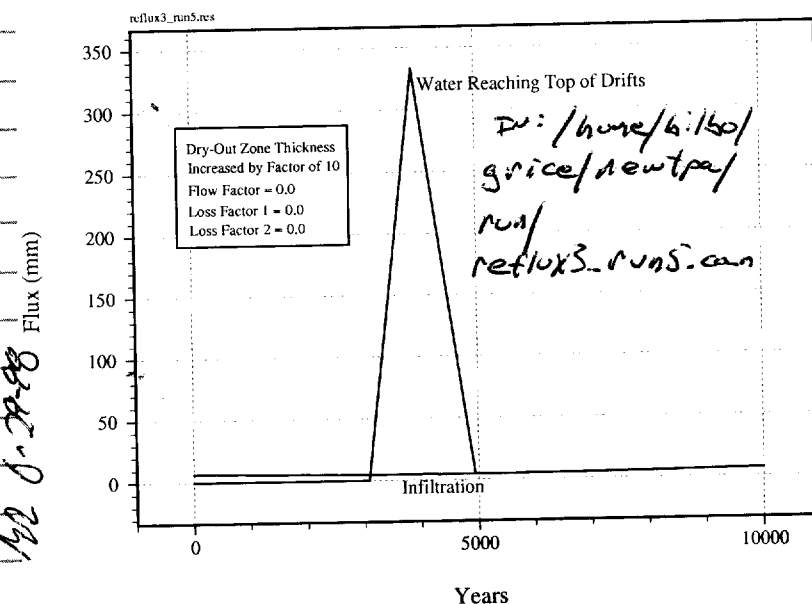
$$\underbrace{(80.7 - 8.07)}_{\text{SEE P42 (m)}} \underbrace{(0.14)}_{\text{POROSITY}} \underbrace{(0.9)}_{\text{INIT SAT}} \underbrace{(418)}_{\text{AREA OF UNIT CELL (m}^2\text{)}} \text{ m}^3$$

TEST #5 - SAME AS #3 BUT WITH DRY-OUT ZONE THICKNESS INCREASED BY A FACTOR OF 10.

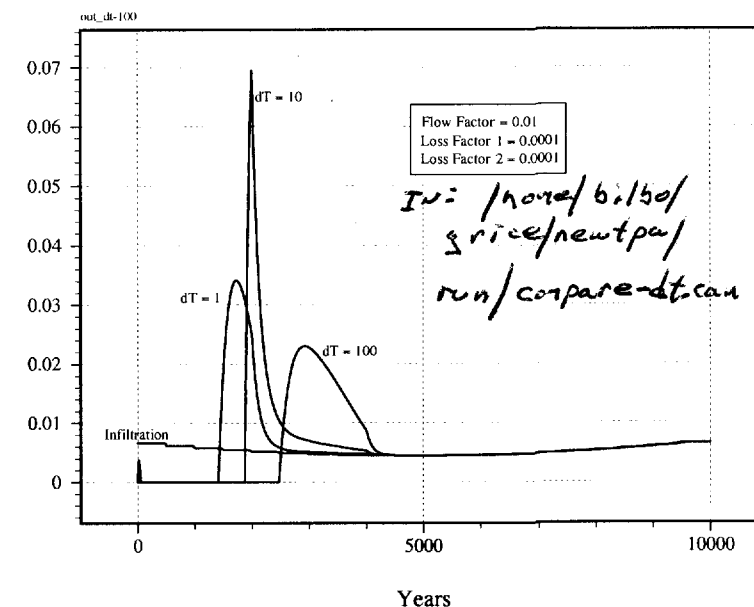
6-29-98

MR

TPA Code REFLUX3 Results

7-2-98
MR

REFLUX3: Effect of Tempertaure Gradient

7-2-98
MR

TEST #5 RESULTS AS EXPECTED - TOTAL AMOUNT OF WATER REACHING DRIFTS IS INCREASED BY AMOUNT VOLUME OF WATER CONTRIBUTED BY DRY-OUT ZONE IS INCREASED.

7-7-98

MR

RESULTS OF MULTIPLE TPA RUNS (REANALYZATIONS) TPA CODE AUTOMATICALLY CHANGING VARIABLES.

July 7, 1998

REFLUX3 Variables for NFENV table

constant	WPUnitCellWidth[m]	Width (m) of waste package unit cell	22.5	TRW Environmental Safety Systems, Inc. (1995)
loguniform	FractionOfCondensateRemoved	Fraction of water in condensation zone that is removed from system each year	1.0e-8 - 1.0	TEF team best estimate
loguniform	FractionOfCondensateTowardRepositoryRemoved	Fraction of water flowing from condensation zone toward repository that is removed from system each year	1.0e-8 - 1.0	TEF team best estimate
uniform	FractionOfCondensateTowardRepository	Fraction of water in condensation zone that flows toward repository each year	0 - 1	TEF team best estimate
constant	DensityOfWaterAtBoiling[kg/m ³]	Density of water at boiling point (97 C, kg/m ³)	960.5	Handbook of Chemistry and Physics (62 nd Edition)
constant	EnthalpyOfPhaseChangeForWater[J/kg]	Enthalpy change, boiling water (J/kg)	2.4E+6	Handbook of Chemistry and Physics (62 nd Edition)
uniform	TemperatureGradientInVicinityOfBoilingIsotherm[K/m]	Temperature gradient across boiling isotherm (K/m)	1 - 100	MULTIFLOW runs, laboratory-scale experiments

projname\reflux3\reflux3table1.doc

INCREASE:

(807M - 80.7M) (0.14) 0.9 (418M)

SEE PG
42

POROSITY

AREA OF
UNIT CELLINITIAL
SATURATIONNEW REFLUX3
VARIABLES IN
TPA CODE.

7-2-98

MR

RESULTS OF REFLUX3 RUNS THAT EXAMINE SENSITIVITY TO TEMPERATURE GRADIENT IN EXPRESSION DEVELOPED BY PHILLIPS (1996)

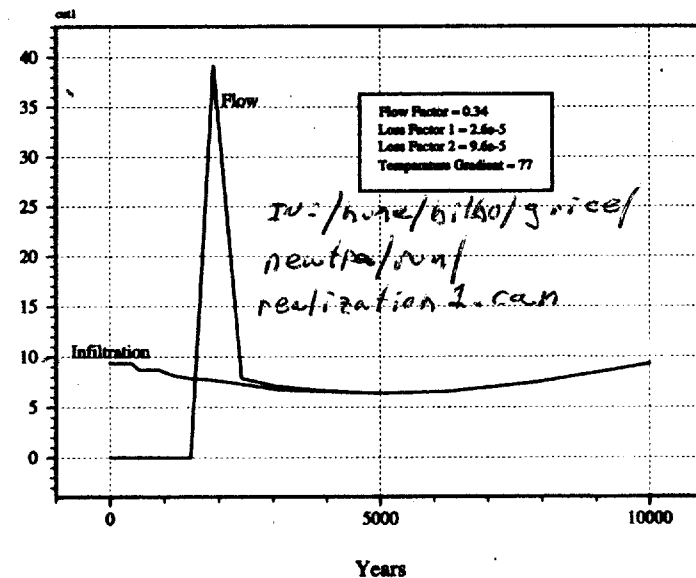
MR
7-2-986-2-98
MR
7-2-98
MR7-2-98
MR

MR 7-7-98

7-7-98

MD

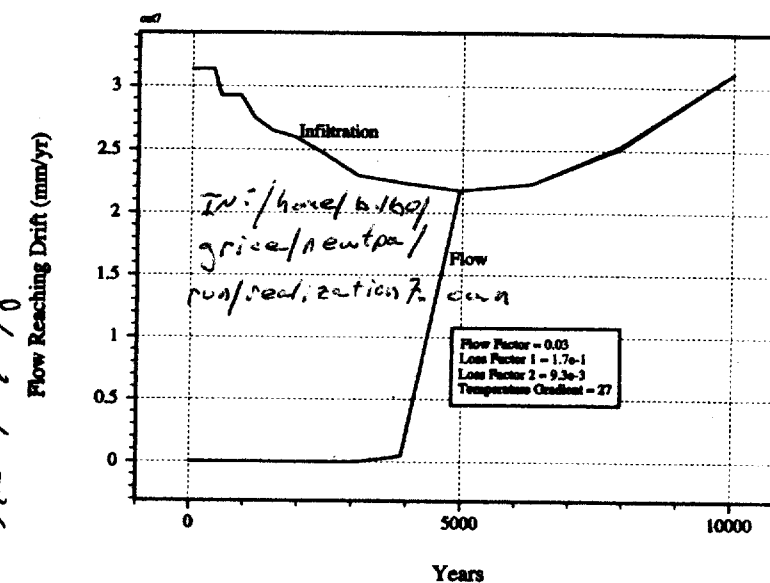
REFLUX3 - Realization 1



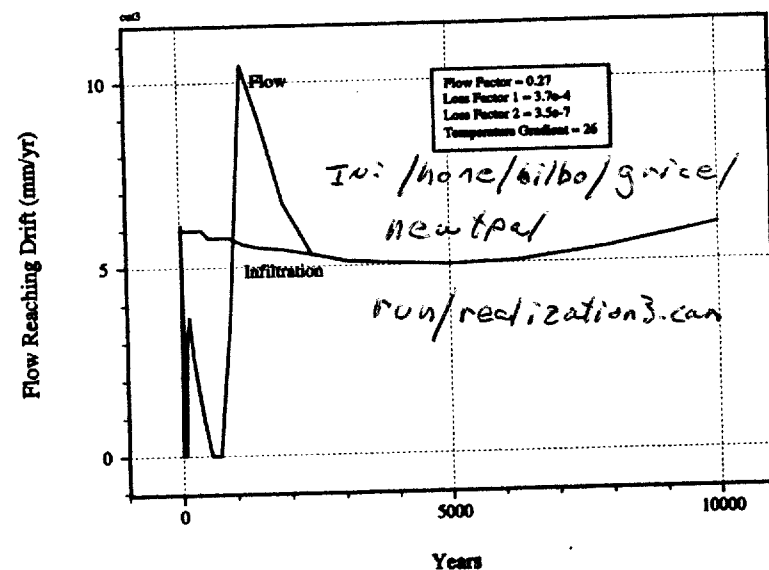
7-7-98

MD

REFLUX3 - Realization 7



REFLUX3 - Realization 3

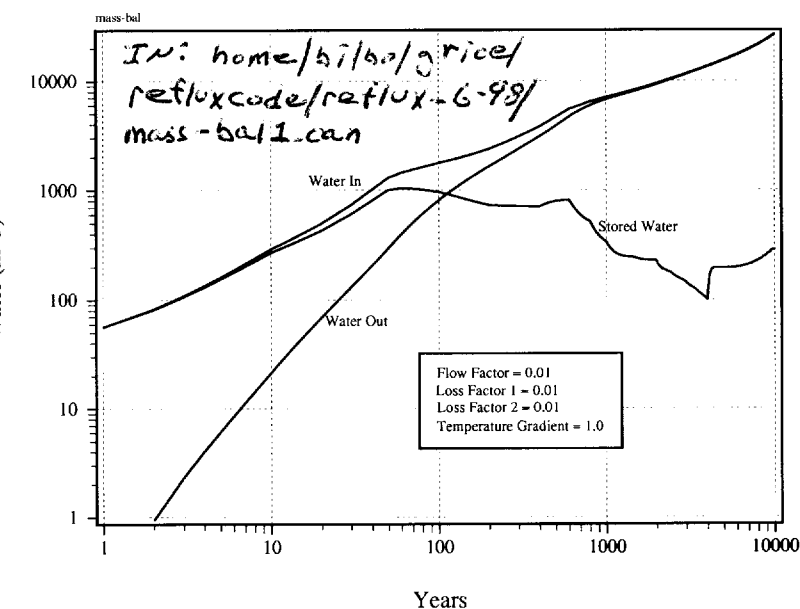


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MD

REFLUX3 MASS BALANCE - RESULTS OF
STAND-ALONE VERSION.

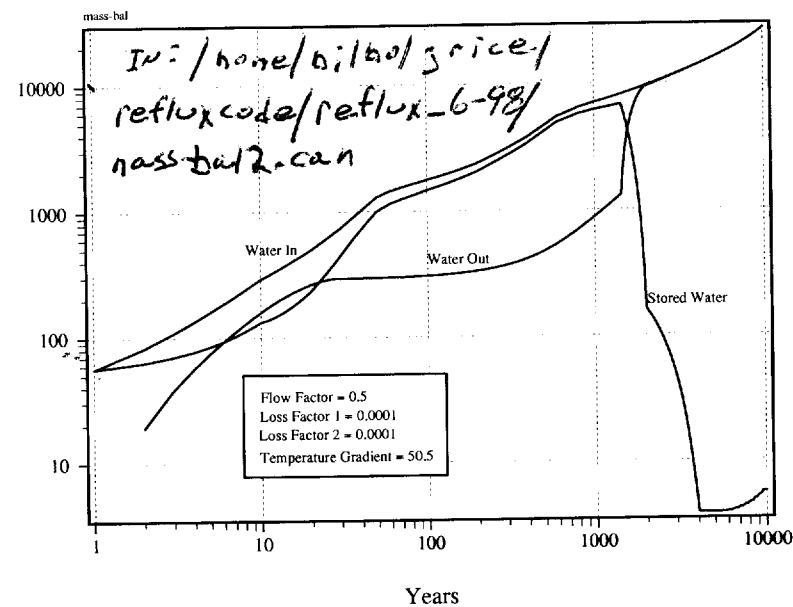
REFLUX3 Mass Balance



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MR

REFLUX3 Mass Balance



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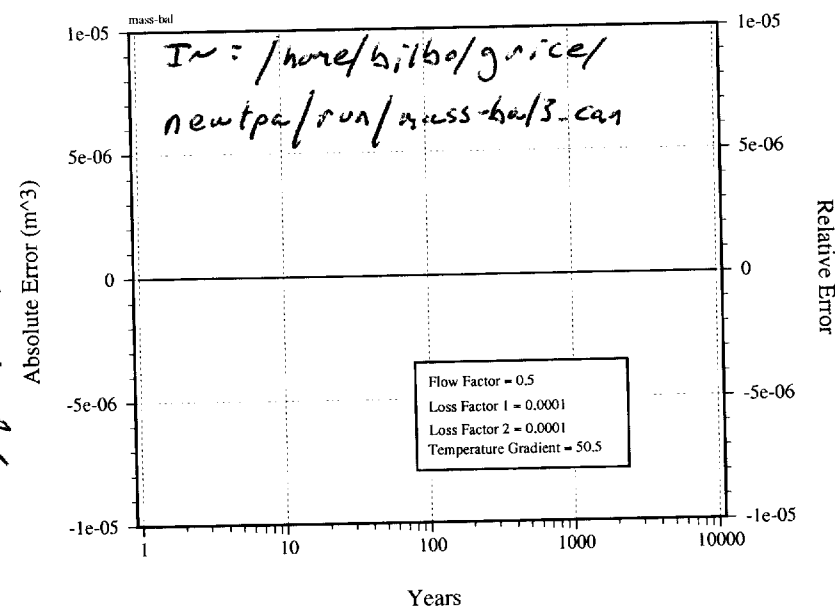
Years

7-13-98

MR

NOTE - THE FOLLOWING RUN DONE WITH THE
CURRENT TPA CODE - DOUBLE PRECISION.

REFLUX3 Mass Balance

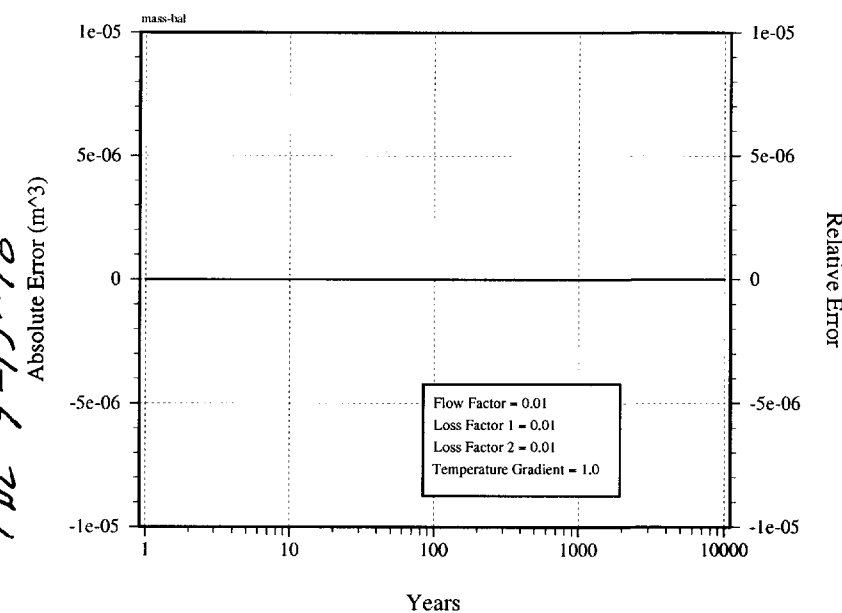


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SEE NOTE ABOVE - ALSO SEE NOTE ON Pg 44.

REFLUX3 Mass Balance



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Final Entry:

This notebook appears to comply
with QAP-001.

E. C. Pen
2/8/2008