



**Pacific Gas and
Electric Company**

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September 12, 2003

PG&E Letter DCL-03-114

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555-0001

Docket No. 50-275, OL-DPR-80
Docket No. 50-323, OL-DPR-82
Diablo Canyon Units 1 and 2
Response to NRC Questions Regarding License Amendment Request 02-03,
"Spent Fuel Cask Handling"

Dear Commissioners and Staff:

By letter dated April 25, 2002, the Pacific Gas and Electric Company (PG&E) submitted an application for amendment to Facility Operating License Nos. DPR-80 and DPR-82, pursuant to 10 CFR 50.90. The License Amendment Request (LAR) submitted, for Nuclear Regulatory Commission (NRC) review and approval, proposed changes in the implementation of the Diablo Canyon Power Plant (DCPP) NUREG-0612 Control of Heavy Loads Program together with other analyses, design, and procedure changes required to implement a dry cask Independent Spent Fuel Storage Installation (ISFSI).

The NRC staff has recently asked an additional question related design modifications to the fuel handling building crane, which will allow handling and loading of Holtec International's (Holtec's) multi-purpose canisters and transfer cask in the DCPP 10 CFR 50 facilities. PG&E's response to this additional question is included in Enclosure 1.

This additional information does not affect the results of the safety evaluation and no significant hazards determination previously transmitted in PG&E Letter DCL-02-44, "License Amendment Request 02-03, Spent Fuel Cask Handling," dated April 15, 2002.

If you have any questions regarding this response, please contact Mr. Terence Grebel at (805) 545-4160.

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Document Control Desk
September 12, 2003
Page 2

PG&E Letter DCL-03-114

Sincerely,

A handwritten signature in black ink, appearing to read 'D H Oatley', written in a cursive style.

David H. Oatley
Vice President and General Manager

pns3/4998

Enclosures

cc: Edgar Bailey, DHS
Thomas P. Gwynn
David L. Proulx
Diablo Distribution
cc/enc: Girija S. Shukla

UNITED STATES OF AMERICA
NUCLEAR REGULATORY COMMISSION

**In the Matter of
PACIFIC GAS AND ELECTRIC COMPANY**

Diablo Canyon Power Plant Units 1 and 2

**Docket No. 50-275
Facility Operating License
No. DPR-80**

**Docket No. 50-323
Facility Operating License
No. DPR-82**

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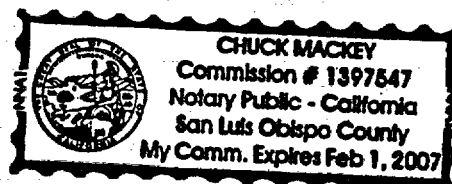
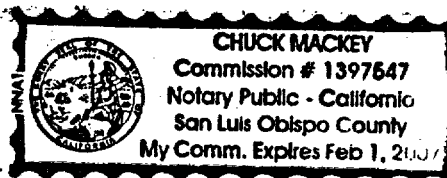
David H. Oatley, of lawful age, first being duly sworn upon oath, states that he is Vice President and General Manager – Diablo Canyon of Pacific Gas and Electric Company; that he is familiar with the content thereof; that he has executed this supplemental response to an additional NRC question regarding License Amendment Request 02-03, "Spent Fuel Cask Handling" on behalf of said company with full power and authority to do so; and that the facts stated therein are true and correct to the best of his knowledge, information, and belief.

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David H. Oatley
Vice President and General Manager

Subscribed and sworn to before me this 12th day of September 2003.

Notary Public
State of California
County of San Luis Obispo



DCPP FHB Crane Auxiliary Lift NUREG-0612 Appendix C Conformance Matrix

NUREG-0612 Appendix C NUREG-0554 Guidelines Section	Guidance	DCPP Auxiliary Lift Conformance Results
(1)	"The allowable stress limits should be identified and be conservative enough to prevent permanent deformation of the individual structural members when exposed to maximum load lifts."	Conformant. The FHB Crane Auxiliary Lift meets the basic allowable stresses from AISE No. 6 (used to design the existing crane) as follows: Bearing = 0.70Fy; Bending (fully supported) = 0.55 Fy; Shear = 0.33 Fy; Tension = 0.55Fy. These stress limits preclude permanent deformation of the material [ref. PG&E Letter DCL-03-047, RAI Question 1-3, 1-4].
(2)	"The minimum operating temperature of the crane should be determined from the toughness properties of the structural materials that are stressed by the lifting of the load."	Conformant. The FHB Crane, an indoor crane located near the ceiling of the Fuel Handling Building in a conditioned environment, is not susceptible to low temperature operating conditions. Minimum operating temperature is not a concern for this application.
(3)	"The crane should be capable of stopping and holding the load during a seismic event equal to a Safe Shutdown Earthquake (SSE) applicable to that facility."	N/A. FHB crane, structure, and supporting runway and building superstructure are seismically qualified at full rated load [ref. PG&E Letter DCL-03-047, RAI Question 2-1 Table 2-1-1]. The specific seismic evaluation of the FHB crane was reviewed and accepted by NRC [ref. DCPD SSER (NUREG-0675) No. 9, June 1980]. The building structure review is presented in the DCPD FSAR Update [ref. Sections 3.7 and 3.8.2]. The seismically-qualified main hoist of the FHB crane always carries the load during crane operations. The auxiliary lift can be loaded only by a non-seismic failure of the main hoist system. Thus, the auxiliary lift structure itself does not require seismic qualification since the transfer of load to it from the main hoist constitutes the single failure in the system [ref. PG&E Letter DCL-02-044, Section 4.2.1 and PG&E Letter DCL-03-047, RAI 1-3, 1-4, 1-7].

DCPP FHB Crane Auxiliary Lift NUREG-0612 Appendix C Conformance Matrix

NUREG-0612 Appendix C NUREG-0554 Guidelines Section	Guidance	DCPP Auxiliary Lift Conformance Results
(4)	"Automatic controls and limiting devices should be designed so that component or system malfunction will not prevent the crane from stopping and holding the load safely."	<p>Conformant.</p> <p>The auxiliary lift is positioned by processing weight sensing signals from the main hoist system and comparing them with weight applied to the auxiliary lift structure. Using direction or travel input from the main hoist, the auxiliary lift adjusts vertical position to maintain a slight preload on the interconnecting rigging. No active movement of the auxiliary lift beam is required at the instant of load transfer from the main hoist. By maintaining proper position with respect to the main hoist load block, the lift is ready to receive a load transfer. Any failure of the auxiliary lift to maintain position would be annunciated to the crane operator and stop hoisting operations. Crane electrical systems will use applicable logic to stop crane operation in a fail-safe mode (i.e., de-energized control component states). Electrical devices for protection of the auxiliary lift will be independent from those of the main hoist [ref. PG&E Letter DCL-03-047, RAI Question 1-6].</p> <p>The FHB Crane Auxiliary Lift basic design does not allow for the load to overhaul the lift drive system. The mechanical design of the screw jack thread geometry does not allow the screw jack shaft to rotate under an applied load on the traveling nut from the lower lifting beam. In addition, there is an electromechanical holding brake (typically mounted on the end of the drive motor) for the screw jack. Though the auxiliary lift structure is free to pivot in the lateral directions, to preclude any side loading of the auxiliary lift, the crane control system will be modified to restrict the crane to single axis operation during use of the auxiliary lift. A diverse, master (crane and aux. lift) "all stop" function will also be added to aid the crane operator upon apparent crane malfunction to assure the crane stops and holds the load safely. Lastly, load measuring to sense and preclude load hang-up conditions will stop crane motion to assure the crane stops and holds the load safely [ref. PG&E Letter DCL-03-047, RAI Question 2-1 Table 2-1-1].</p>

DCPP FHB Crane Auxiliary Lift NUREG-0612 Appendix C Conformance Matrix

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(5)	"Design of the wire rope reeving system should include dual wire ropes."	<p>N/A.</p> <p>The FHB Crane Auxiliary Lift operates in parallel with the wire rope-reeved main hoist but does not use a wire rope reeving system to hold its load [ref. PG&E Letter DCL-02-044, LAR Figure 5]. The slings between the auxiliary lift and the cask lift yoke are designed as non-redundant devices to a minimum overall safety factor of 10 [ref. PG&E Letter DCL-03-047, RAI 1-4]. The auxiliary lift is never fully loaded under normal operating conditions where its movement parallels the main hoist lower block. Therefore, the amount of operational wear on the auxiliary lift components is not expected to be of concern. Load holding functions of the lift structure when demanded are assured by mechanical design features as described in (4) above. The maximum calculated stress in the main hoist wire rope, based on the efficiency of the single path reeving, weight of the lower block assembly in addition to the crane rated load is 1/6 of the manufacturer's specified breaking strength [ref. DCPD FSAR Update Section 9.1.4.2.1.3].</p>
(6)	"Sensing devices should be included in the hoisting system to detect such items as overspeed, overload, and overtravel and cause the hoisting action to stop when limits are exceeded."	<p>Conformant.</p> <p>The FHB Crane Auxiliary Lift mechanical thread design does not allow an overspeed condition found in rope-reeved systems. The auxiliary lift will include sensing devices in its control system to preclude overload (motor current, load cell measurement) and overtravel (motor encoder position, travel limit sensors). Upon an additional crane operating condition as postulated by the Guidance of this section, plant crane operating and maintenance procedures will prescribe steps to begin troubleshooting and restoration of hoist and lift functions as applicable.</p>

DCPP FHB Crane Auxiliary Lift NUREG-0612 Appendix C Conformance Matrix

NUREG-0612 Appendix C NUREG-0554 Guidelines Section	Guidance	DCPP Auxiliary Lift Conformance Results
(7)	"The reeving system should be designed against the destructive effects of 'two-blocking.'"	<p>Conformant.</p> <p>The FHB Crane Auxiliary Lift will use redundant travel limit devices to preclude a "two-block" event between its upper and lower cross members and stop all hoist and lift operations if tripped. The FHB Crane main hoist control system currently has two redundant upper limit devices that preclude a two-block event. These devices would be modified to preclude a two-block event between the lower block and the auxiliary lift lower lifting beam due to the reduced vertical headroom under the trolley to mount the auxiliary lift.</p>
(8)	"The hoisting drum(s) should be protected against dropping should its shafts or bearings fail."	<p>N/A.</p> <p>The FHB Crane Auxiliary Lift does not use a hoisting drum [ref. PG&E Letter DCL-02-044, LAR Figure 5; PG&E Letter DCL-02-047, Figure 1-5-1]. The worm gear inside the screw jack drive housing is captured by the base of the housing and the baseplate on the auxiliary lift to which the screw jack assembly is mounted. The minimum factor of safety reported from the manufacturer for the load bearing components of each screw jack assembly of the lift is 7 to yield and 9 to ultimate [ref. PG&E Letter DCL-03-047, RAI 1-4]. Therefore a pullout of the screw jack threads is highly unlikely. There is no credible malfunction of the lift that could cause the top block pin to fail because the moving components of the auxiliary lift do not have the capability to apply driven forces onto the trolley to which the lift is mounted.</p>
(9)	"Safety devices such as limit switches provided to reduce the likelihood of a malfunction should be in addition to those normally provided for control of maloperation or operator error."	<p>Conformant.</p> <p>The control system for the FHB Crane Auxiliary Lift and main hoist will use additional, independent devices to provide control signals for determining if the lift is outside its normal expected range of operation [ref. PG&E Letter DCL-02-044, Section 4.2.1].</p>
(10)	"The crane system should be given a cold proof test if material toughness properties are not known."	<p>Conformant.</p> <p>See results for Section (2) above.</p>