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**C. Lance Terry**  
Senior Vice President &  
Principal Nuclear Officer

Ref: 10 CFR 50.55a(3)(i)  
10 CFR 50.55a(g)(4)(iv)

CPSES-200301005  
Log # TXX-03159

September 11, 2003

U. S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
Washington, DC 20555

**SUBJECT: COMANCHE PEAK STEAM ELECTRIC STATION (CPSES)**  
**DOCKET NOS. 50-445 AND 50-446;**  
**RELIEF REQUEST C-2 FOR THE SECOND 10 YEAR ISI**  
**INTERVAL FOR UNIT 1 AND C-7 FOR THE FIRST**  
**10 YEAR ISI INTERVAL FOR UNIT 2 FROM 10 CFR 50.55a FOR**  
**THE PURPOSE OF INVOKING CODE CASE N-562-1.**  
**(UNIT 1 SECOND INTERVAL START DATE AUGUST 2000**  
**UNIT 2 FIRST INTERVAL END DATE: AUGUST 2004)**  
**(TAC NOS. MB7947 AND MB7948)**

**REFERENCE: TXU Energy Letter logged TXX-03046 dated March 5, 2003 from**  
**C. Lance Terry to the NRC**

Via the referenced letter TXU Generation Company LP (TXU Energy) requested relief from the ASME Code pursuant to 10CFR50.55a. After a review of the subject Relief Requests, the NRC staff requested additional information with respect to ASME Code Case N-562-1. TXU Energy is supplementing its request for relief from the ASME Code based on the additional information requested by the NRC staff. The changes are clearly identified by the revision bars in the attachment to this letter.

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This communication contains no new licensing basis commitments regarding CPSES.


TXU Energy requests approval of this relief request by September 30, 2003. The approval date was selected to allow use of this relief request during the seventh refueling outage for Unit 2, scheduled to start October 4, 2003. If you have any questions regarding this request, please contact Jack Hicks at (254) 897-6725.

Sincerely,

TXU Generation Company LP

By: TXU Generation Management Company LLC,  
Its General Partner

C. L. Terry  
Senior Vice President and Principal Nuclear Officer

By:   
Fred W. Madden  
Nuclear Licensing Manager

JCH/jch  
Attachment/Enclosure

c - T. P. Gwynn, Region IV  
W. D. Johnson, Region IV  
M. C. Thadani, NRR  
Resident Inspectors, CPSES  
Terry Parks, Chief Inspector, TDLR  
J.C. Hair ANII, CPSES

**TXU GENERATION COMPANY LP  
COMANCHE PEAK STEAM ELECTRIC STATION UNIT 1  
SECOND TEN-YEAR INTERVAL ISI RELIEF REQUEST NO. C-2  
AND UNIT 2 FIRST TEN YEAR INTERVAL FOR ISI RELIEF NO. C-7**

**PROPOSED USE OF SUBSEQUENT ASME CODE EDITION AND ADDENDA  
PURSUANT TO 10 CFR 50.55a(g)(4)(iv) AND INVOKING CODE CASE N-562-1**

**I. ASME System/Component(s) Affected:**

All ASME Class 3 Moderate Energy (i.e. less than or equal to 200°F or less than or equal to 275 psig maximum operating conditions) Carbon Steel Piping Systems.

**II. Applicable Code Edition and Addenda:**

ASME Code 1986 Edition (No Addenda), Section XI, IWD-4120 requires that the defect be removed or reduced in size in accordance with Article IWA.

**III. Proposed Subsequent Code Edition and Addenda and Code Case:**

TXU Energy proposes to use 1998 Edition, ASME Section XI IWA 4000 and invoke Code Case N-562-1, to repair the piping section or similar conditions found in other Class 3 piping during the corrosion monitoring program (CPSES procedure STA-730, "Corrosion Monitoring Program").

Relief is requested from removing defects and repairing in accordance with the design specification or the original construction code for internal wall thinning or pitting resulting from conditions such as, but not limited to, microbiological corrosion; cavitation induced pitting; erosion/corrosion and/or localized pitting corrosion.

The ASME Section XI Code Committee recognized that an alternative existed for internal wall thinning of Class 3 piping systems which have experienced degradation mechanisms such as flow-assisted corrosion (FAC) and/or microbiological corrosion that would provide an acceptable repair configuration. This alternative repair technique involves the application of additional weld metal on the exterior of the piping system, which restores the wall thickness requirement. Code Case N-562-1 was approved by the ASME Section XI Code Committee on July 30, 1998. However, it has not been incorporated into NRC Regulatory Guide 1.147 (or Draft Guide (DG) 1091) and thus is not presently available for application at nuclear power plants.

This code case is denoted in NRC Draft Guide (DG)-1112 with the comment that, "[N]either the ASME Code or the Code Case have criteria for determining the rate or extent of degradation or the repair or the surrounding base metal. Reinspection requirements are not provided to verify structural integrity since the root cause may not be mitigated."

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**PROPOSED USE OF SUBSEQUENT ASME CODE EDITION AND ADDENDA  
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CONT.**

In response to this concern, the TXU Energy plans to implement Code Case N-562-1 through the industry standard NSAC-202L-R2, "Recommendations for an Effective Flow Accelerated Corrosion (FAC) Program," for calculating the wear rates, forecasting remaining life, and conducting inspections of FAC degradation at CPSES, Units 1 and 2. This is proceduralized in STA-730, "Corrosion Monitoring Program."

Pursuant to 10 CFR 50.55a(a)(3)(i), relief is requested to use Code Case N-562-1 on the basis that the proposed alternative will provide an acceptable level of quality and safety. This relief request applies to ASME Class 3 moderate energy piping system (i.e., less than or equal to 200°F and/or less than or equal to 275 psig maximum operating conditions) carbon steel piping.

**IV. Basis of Using Subsequent Code Editions and Addenda and Code Case:**

A number of alternatives (e.g., Generic Letter GL 90-05 "Guidance for Performing Temporary Non-Code Repair of ASME Code Class 1, 2, and 3 Piping", Code Cases N-513 "Evaluation Criteria for Temporary Acceptance of Flaws in Class 3 Piping, Section XI, Division 1" and N-523-1 "Mechanical Clamping Devices for Class 2 and 3 Piping, Section XI, Division 1") are currently available and approved by the NRC for evaluating and repairing of piping wall thinning and pitting (including through wall leaks). Nonetheless, these alternatives have limitations and do not always encompass the specific situations that arise from a piping leak.

While the guidance provided by GL 90-05 and Code Case N-513 could be used to evaluate and accept the leaking condition, if the structural integrity of the piping can be ascertained, the leak would most likely continue to increase in size over time and would pose more significant housekeeping difficulties. On the other hand, if the flaw exceeds the acceptance criteria provided by GL 90-05 or Code Case N-513, an emergency code repair (which may include up to full piping replacement of the affected sections) would be warranted. Therefore this would pose a significant hardship on plant operations to isolate and drain the affected piping sections (some of which are not isolable and would require extended plant shutdown). For that reason, TXU Energy requests that relief be granted to use a weld overlay in lieu of a code weld repair on Class 3 moderate energy piping. This would provide additional insurance that an unscheduled plant shutdown could be avoided.

Code Case N-562-1 provides an additional alternative to the IWA-4000 requirements for the repair of internal piping system defects or degradation. Please note that the ASME XI Code Committee determined that such a weld overlay would restore the minimum piping wall thickness at the flawed location and would ensure that an adequate level of quality and

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safety is maintained.

The primary purpose for implementing this alternate repair method (installation of a weld overlay) is to avoid the need to extend an outage to perform code repair and possibly piping replacement. It also allows for adequate time to perform additional evaluation of adjacent piping so that pipe replacement can be properly identified and scheduled to reduce impact on system availability, increase safety of plant operations, and reduce cost for replacement materials and labor.

Additionally, TXU Energy is proposing the following restrictions on the use of the Code Case N-562-1, to assure that the use of the Code Case will provide an acceptable alternative pursuant to 10 CFR 50.55a(a)(3)(i):

- The scope of the alternative repair techniques in Relief Request C-2 for Unit 1 and C-7 for Unit 2 is limited to repairs of ASME Class 3 moderate energy (i.e., less than or equal to 200° F and/or less than or equal to 275 psig maximum operating conditions) carbon steel plant service water piping systems.
- Repairs are limited to internal thinning or pitting caused by general localized corrosion, such as microbiological corrosion; cavitation induced pitting; erosion/corrosion and/or localized pitting corrosion; but excluded are conditions involving corrosion-assisted cracking or any other form of cracking.
- TXU Energy will evaluate the use of Code Cases N-513 "Evaluation Criteria for Temporary Acceptance of Flaws in Class 3 Piping, Section XI, Division 1," or N-523 "Mechanical Clamping Devices for Class 2 and 3 Piping, Section XI, Division," or N-597 "Requirements for Analytical Evaluation of Pipe Wall Thinning, Section XI, Division 1", prior to use of Code Case N-562-1, for the identified Class 3 moderate energy (i.e., less than or equal to 200° F and/or less than or equal to 275 psig maximum operating conditions) piping system repairs resulting from phenomenon such as flow-assisted corrosion and/or microbiological corrosion. When engineering evaluation determines that the aforementioned guidance or code cases are not suitable, the repair technique described in Code Case N-562-1 may be utilized for the particular defect or degradation being resolved.
- The repair will be considered to have a maximum service life of one fuel cycle.
- The SMAW, GTAW processes may be used for these repairs on piping that is empty; however, only the SMAW process may be used on water backed piping. This process,

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SMAW, may only be used on water backed piping with the special requirements as stated in Code Case N-562-1.

- An evaluation of the degradation mechanism will be performed to determine the reexamination schedule to be performed over the life of the repair.
- The provisions for implementing these alternative repair techniques will be addressed in CPSES Repair and Replacement Program Procedure.
- Weld repairs will not be performed on surfaces that are wet or exposed to water, such as those from small leaks in the piping system.
- The initial re-inspection of the weld overlay and its surrounding areas will be performed within a period of no greater than 6 months.

TXU will implement Code Case N-562-1 through the industry standard NSAC-202L-R2, "Recommendations for an Effective Flow Accelerated Corrosion (FAC) Program," for calculating wear rates, forecasting remaining life, and conducting inspections of FAC degradation at CPSES, Units 1 and 2.

Therefore, the proposed alternative is justified per 10CFR50.55a(a)(3)(i) as the proposed repair will provide an acceptable level of quality and safety.

**V. Duration of Proposed Alternative:**

This relief is requested for the Comanche Peak Steam Electric Station Unit 1, second 10-year interval, and for Unit 2 first 10-year interval.

Granting of this relief request will not have an impact on plant quality or safety and will not adversely impact the health and safety of the public.

**VI. Precedents:**

- 1) Southern Nuclear Operation Company's Hatch Plant, Units 1 and 2 (Reference SER dated May 31, 2000, TAC Nos. MA6123 and MA 6124).
- 2) Entergy Nuclear Northeast's James A. Fitzpatrick Plant (Reference SER dated November 14, 2002, TAC NO. MB3750)

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Approval Date: July 30, 1998  
See Numeric Index for expiration  
and any reaffirmation dates.

Case N-562-1  
Alternative Requirements for Wall Thickness  
Restoration of Class 3 Moderate Energy Carbon  
Steel Piping  
Section XI, Division 1

**Inquiry:** As an alternative to replacement or internal weld repair, what requirements may be applied for wall thickness restoration of Class 3 moderate-energy carbon steel piping systems that have experienced internal wall thinning or pitting from conditions such as, but not limited to, flow-assisted corrosion and microbiological corrosion?

**Reply:** It is the opinion of the Committee that areas of Class 3 moderate energy (i.e., less than or equal to 200°F or and less than or equal to 275 psig maximum operating conditions) carbon steel piping experiencing internal thinning or pitting may have the wall thickness restored externally by means of a weld-deposited carbon or low-alloy steel reinforcement on the outside surface of the piping in accordance with the following requirements. Excluded from these provisions are conditions involving corrosion-assisted cracking or any other form of cracking.

1.0 GENERAL REQUIREMENTS

(a) The wall thickness restoration shall be performed in accordance with a Repair/Replacement Plan satisfying the requirements of IWA-4150.<sup>1</sup>

(b) The wall thickness restoration shall meet the requirements of IWA-4000,<sup>2</sup> except as stated in this Case.

(c) If the minimum required thickness of deposited weld metal necessary to satisfy the requirements of para. 3.0 is greater than the nominal thickness for the size and schedule of the piping, the provisions of this

Case shall not apply. In addition, the total thickness of filler metal applied over multiple repairs shall not exceed the original nominal thickness of the piping.

2.0 INITIAL EVALUATION

The material beneath the surface to which the weld overlay is to be applied shall be evaluated to establish the existing average wall thickness and the extent and configuration of degradation to be reinforced by the weld overlay. Consideration shall be given to the cause of degradation. The extent of degradation in the piping, and the effect of the repair on the piping, shall be evaluated in accordance with IWA-4160.<sup>3</sup>

3.0 DESIGN

3.1 General Design Requirements

(a) Unless otherwise established by theoretical or experimental analysis, or by proof testing as provided for in para. 3.3 or para. 3.4, the full thickness of the weld overlay shall extend a distance of at least  $s$  in each direction beyond the area predicted, over the design life of the restoration to infringe upon the required thickness.<sup>4</sup>

where

$$s = \frac{2}{3} \sqrt{R t_{\text{nom}}}$$

$R$  = outer radius of the component

$t_{\text{nom}}$  = nominal wall thickness of the component

Edges of the weld overlay shall be tapered to the existing piping surface at a maximum angle ("α" in Fig. 1) of 45 deg. Final configuration of the reinforcement shall permit the examinations and evaluations required herein, including any required preservice or inservice examinations of encompassed or adjacent welds.

<sup>1</sup>IWA-4140 in the 1989 Edition with the 1991 Addenda through 1995 Edition. IWA-4130 (Repair Program) in the 1989 Edition with the 1990 Addenda and earlier Editions and Addenda.

<sup>2</sup>IWA-4000/7000 and IWC/TWD-4000/7000, as applicable, in the 1989 Edition with the 1990 Addenda and earlier Editions and Addenda.

<sup>3</sup>IWA-4150 in the 1989 Edition with the 1991 Addenda through 1995 Edition. IWA-4130 (Repair Program) in the 1989 Edition with the 1990 Addenda and earlier Editions and Addenda.

<sup>4</sup>Design thickness as prescribed by the Construction Code.

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(b) The thickness shall be sufficient to maintain required thickness for the predicted life of the repair, and, except for the tapered edges, the overlay shall have a uniform thickness.

(c) The tensile strength of the weld filler metal for the reinforcement shall be at least that specified for the base metal to which it is applied.

(d) The predicted maximum degradation of the overlaid piping and the overlay over the design life of the restoration shall be considered in the design. The predicted degradation of the piping shall be based upon in-situ inspection and established data for similar base metals. If the weld overlay is predicted to become exposed to the corroding medium, the predicted degradation of the overlay shall be based upon established data for base metals or weld metals with similar chemical composition to that of the filler metal used for the weld overlay.

(e) The effect of weld overlay application on interior coating shall be addressed in the Repair/Replacement Plan (Repair Program).

3.2 Design

The design of weld overlays not prequalified by paras. 3.3, 3.4, or 3.5 shall be in accordance with the applicable requirements of the Construction Code or ND-3100 and ND-3600 (including Appendix II), and shall consider the weld overlay as an integral portion of the piping or component upon which it is applied (not as a weld). The allowable stress values of the base metal shall apply to the design of the deposited weld metal. The following factors shall be considered, as applicable, in the design and application of the reinforcement:

(a) The shrinkage effects, if any, on the piping.

(b) Stress concentrations caused by application of the overlay or resulting from existing and predicted piping internal surface configuration.

3.3 Proof Test Qualification as a Piping Product

As an alternative to design, the configuration of weld overlays may be qualified by performance of proof testing of a mockup in accordance with the following requirements:

(a) A satisfactory mockup burst test shall qualify the design or configuration for application in the same orientation on the same type of item, and the same location on fittings, when the following conditions are satisfied (see Fig. 1):

(1) the base metal is of the same P-No. and Group Number when impact properties are applicable, as the base metal tested;

(2) the specified minimum tensile strength of the item does not exceed that specified for the base metal tested;

(3) the average thickness of the overlay areas is at least the thickness of the mockup plug,  $u$ ;

(4) the overlap on the full thickness of base metal,  $s$ , is at least that of the mockup;

(5) the transition angle at the outer edges of the overlay,  $\alpha$ , is not greater than that of the mockup;

(6) the overlay surface finish is similar to or smoother than that tested;

(7) the maximum proportionate axial dimension,  $L/D$ , is not more than that tested;

(8) the maximum proportionate circumferential dimension,  $C/D$ , is not more than that tested;

(9) the nominal diameter is not less than one-half nor more than two times the diameter tested;

(10) the nominal thickness/diameter ratio,  $t/D$ , is not less than one-half nor more than three times the  $t/D$ , ratio tested.

(b) The mockup base shall consist of new base material of similar configuration, or type of item, as the item to be overlaid. A rounded-corner segment of the base material shall be removed to represent the maximum proportionate size (axial dimension of  $L$  and circumferential dimension of  $C$ ) and location of thinning or pitting to be compensated for by the weld overlay. A plug of the same base metal and of uniform thickness  $u$ , which shall not exceed the smallest average thickness on which the overlays will be permanently applied, shall be full-penetration welded around the opening and flush with the outside surface of the piping. Alternatively, an equivalent volume of base metal may be removed from the inside surface of the mockup by machining or grinding, without need for welding in a closure plug.

(c) The mockup weld overlay shall be applied in accordance with the design or specified configuration using the specified weld filler metal. Maximum section thickness at the overlaid opening (weld metal plus base metal plug,  $u + w$ ) shall not exceed 87½% of the nominal thickness of the piping.

(d) Straight pipe equivalent to a minimum of one pipe diameter, or one-half diameter for piping over NPS 14, shall be provided (butt-welded to the mockup, if necessary) beyond both ends of the overlay. The piping shall be capped and the completed mockup assembly shall be thoroughly vented and hydrostatically



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pressure tested to bursting. To qualify the design for general application within the limits of para. 3.3(a), burst pressure shall not be less than:

$$P = \frac{2S_{act}}{D_o}$$

where

$P$  = minimum acceptable burst pressure, psi

$t$  = minimum specified thickness (excluding manufacturing tolerance) of the base metal being tested, in.

$S_{act}$  = reported actual tensile strength of the base metal being tested, psi

$D_o$  = outside diameter of the pipe, in.

(e) If flexibility analysis was required by the original Construction Code, the effect of the weld overlay shall be reconciled with the original analysis. In this case, for rectangular-shaped overlays on piping designed to ND-3650 and aligned parallel or perpendicular to the axis of the piping, unless a lower stress intensification factor (SIF or  $I$ ) is established, an SIF ( $I$ ) of 2.1 shall be applied for overlays on straight pipe and adjacent welds; a stress multiplier of 1.7 shall be applied to the SIF ( $I$ ) for standard elbows; and an SIF ( $I$ ) of 2.1 shall be applied for tees and branch connections when the toe of the overlay is not less than  $2\frac{1}{2}\sqrt{R_{nom}}$  from any branch reinforcement in Fig. 1.

#### 3.4 Proof Test Qualification for Specific Applications

As an alternative to design by analysis or proof test qualification as a piping product, the design or configuration of weld overlays may be qualified for limited service conditions using the provisions of ND-6900. "Proof Tests to Establish Design Pressure," except that component hydrostatic testing is not required (other than as required by FWA-4000<sup>3</sup>). The mockups shall be fabricated and tested in accordance with the provisions of para. 3.3(b), (c), and (d), and shall be applied in accordance with the provisions and conditions of para. 3.3(a). The provisions of para. 3.3(e) shall be met.

#### 3.5 Frequalified Design

Application of weld overlays on straight pipe, portions of tees not less than  $2\frac{1}{2}\sqrt{R_{nom}}$  from any branch reinforcement in Fig. 1 standard elbows, and associated welds to correct limited degradation shall be exempt from the requirements of para. 3.2 through para. 3.4,

provided all of the following conditions are satisfied in Fig. 1:

(a) All of the requirements of para. 3.1 apply.

(b) The provisions of para. 3.3(e) shall be met.

(c) The full thickness of weld overlay shall not exceed a maximum axial length of the greater of six in. or the outside diameter of the piping.

(d) The finished overlay shall be circular, oval, full-circumferential, or rectangular in shape.

(1) For each repair, the maximum dimension compensated by a circular overlay shall not exceed  $\frac{1}{2}$  the nominal outside diameter of the piping.

(2) Rectangular overlays shall be aligned parallel with or perpendicular to the axis of the piping, and corners shall be rounded with radii not less than the overlay thickness.

(3) For oval overlays, the end radii shall not be less than  $\frac{1}{4}\sqrt{R_{nom}}$ , and the axis of the overlay shall be aligned parallel with or perpendicular to the axis of the piping.

(e) The distance between toes of adjacent overlays shall not be less than  $t_{nom}$ .

#### 4.0 Water-backed Applications

(a) Manual application of overlays on water-backed piping shall be restricted to P-No. 1 base materials. Welding of such overlays shall use the SMAW process and low-hydrogen electrodes. In addition, the surface examination required in para. 6.0 shall be performed no sooner than 48 hours after completion of welding. For such overlays consideration should be given to using a temper bead technique similar to that described in FWA-4650.<sup>3</sup>

(b) Piping with wall thickness less than the diameter of the electrode shall be depressurized before welding.

#### 5.0 INSTALLATION

(a) The entire surface area to which the weld overlay is to be applied shall be examined using the liquid penetrant or magnetic particle method, with acceptance criteria in accordance with ND-2500/5300 for the product form (base metal or weld) involved.

(b) If through-wall repairs are required to satisfy the acceptance criteria, or result from application of the

<sup>3</sup>FWA-4340 in the 1989 Edition with the 1991 Addenda through the 1993 Edition. FWE-4200 in the 1986 Edition with the 1988 Addenda through the 1989 Edition with the 1990 Addenda. FWE-4320 in the 1986 Edition with the 1987 Addenda and earlier Editions and Addenda.

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weld overlay, they shall be accomplished by sealing with weld metal using a qualified weld procedure suitable for open-root welding. This weld shall be examined in accordance with para. 5.0(a). In addition, the first layer of overlay over the repaired area shall be examined in accordance with para. 5.0(a).

(c) Overlay weld metal shall be deposited using a groove-welding procedure qualified in accordance with Section IX and the Construction Code, Section X and Section III, or IWA-4610 and either IWA-4620 or IWA-4650.<sup>6</sup> The qualified minimum thickness specified in the weld procedure does not apply to the weld overlay or associated base metal repairs.<sup>7</sup>

(d) The surface of the weld overlay shall be prepared by machining or grinding, as necessary, to permit performance of surface and volumetric examinations required by para. 6.0. For ultrasonic examination, a surface finish of 250 RMS or better is required.

6.0 EXAMINATION

(a) The completed weld overlay shall be examined using the liquid penetrant or magnetic particle method and shall satisfy the surface examination acceptance criteria for welds of the Construction Code or ND-5300.

(b) The weld overlay, including the existing piping upon which it is applied, shall be examined to verify acceptable wall thickness.

<sup>6</sup>IWA-4300 and either IWA-4310 or IWA-4340 in the 1989 Edition with the 1991 Addenda through 1993 Edition, IWA-4310 or IWE-4200 in the 1986 Edition with the 1988 Addenda through 1989 Edition with the 1990 Addenda, IWB-4320 or IWE-4320 in the 1986 Edition with the 1987 Addenda or earlier Editions and Addenda.

<sup>7</sup>Exception to IWA-4000.

(c) Weld overlays shall be volumetrically examined as base metal repairs when required by the Construction Code, except as follows:

(1) Weld overlays not exceeding 10 in.<sup>2</sup> surface area are exempt from volumetric examination.

(2) Other weld overlays shall be exempt from volumetric examination when the finished applied thickness ( $w$  in Fig. 1) does not exceed:

(a)  $\frac{1}{8}t$  for  $t \leq \frac{3}{4}$  in.

(b)  $\frac{1}{4}$  in. for  $\frac{3}{4}$  in.  $< t \leq 2\frac{1}{2}$  in.

(c) The lesser of  $\frac{3}{8}$  in. or 10% of  $t$  for  $t > 2\frac{1}{2}$  in.

where

$t$  = finished full-section thickness of compensated area (e.g.,  $w + n$ , in Fig. 1)

When volumetric examination is required, the full volume of the finished overlay, excluding the tapered edges, but including the volume of base metal required for the design life of the overlay, shall be examined using either the ultrasonic or radiographic method, and shall, to the depth at the surface of the existing piping, satisfy the acceptance criteria for weldments of the Construction Code or ND-5300. The volume of the existing piping, beneath the weld overlay, taken credit for in the design, shall satisfy the volumetric acceptance criteria of ND-2500/5300 for the product form, or IWA-3000.<sup>8</sup>

(d) Follow-up inspection shall be scheduled as necessary to confirm any design assumptions relative to rate or extent of future degradation.

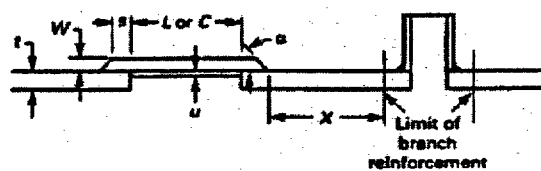
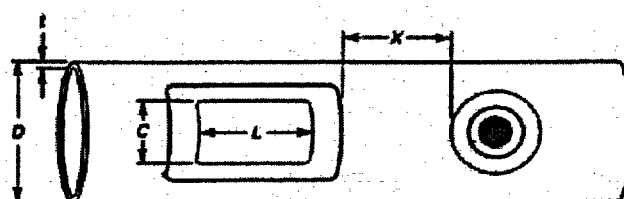
7.0 DOCUMENTATION

Use of this Case shall be documented on an NIS-2 Form.

<sup>8</sup>IWA-3000 and IWB-3514 in the 1989 Edition with the 1990 Addenda and earlier Editions and Addenda.

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$$X \geq 2\frac{1}{2}\sqrt{R_{t, \text{nom}}}$$

FIG. 1