



APPENDIX C Savannah River Site Spent Nuclear Fuel Management Program

Department of Energy Programmatic
Spent Nuclear Fuel Management
and
Idaho National Engineering Laboratory
Environmental Restoration and
Waste Management Programs
Final Environmental Impact Statement
Volume 1
Appendix C
Savannah River Site
Spent Nuclear Fuel Management Program
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1. INTRODUCTION

The U.S. Department of Energy (DOE) is engaged in two related decisionmaking pr concerning: (1) the transportation, receipt, processing, and storage of spent nucl DOE Idaho National Engineering Laboratory (INEL) which will focus on the next 10 ye (2) programmatic decisions on future spent nuclear fuel management which will empha years.

DOE is analyzing the environmental consequences of these spent nuclear fuel man actions in this two-volume Environmental Impact Statement (EIS). Volume 1 supports programmatic decisions that will have applicability across the DOE complex and desc purpose and need for this DOE action. Volume 2 is specific to actions at the INEL. which limits its discussion to the Savannah River Site (SRS) spent nuclear fuel man supports Volume 1 of the EIS. Other documents supporting Volume 1 focus on spent n management programs for the Hanford Site, INEL, Naval Nuclear Propulsion Program, a

As part of its planning process for this two-volume EIS, DOE issued an Implemen October 29, 1993. The organization of this document is consistent with the provisi the Implementation Plan and are outlined below:

- Chapter 2 contains background information related to the SRS and the framew environmental regulations pertinent to spent nuclear fuel management.
- Chapter 3 identifies spent nuclear fuel management alternatives that DOE co at the SRS, and summarizes their potential environmental consequences.
- Chapter 4 describes the existing environmental resources of the SRS that sp activities could affect.
- Chapter 5 analyzes in detail the environmental consequences of each spent n management alternative and describes cumulative impacts. The chapter also

information on unavoidable adverse impacts, commitment of resources, short-environment and mitigation measures.

2. BACKGROUND

The chapter contains an overview of the Savannah River Site (SRS) and a descriptive regulatory framework related to the actions that this document evaluates. In addition, it describes the U.S. Department of Energy (DOE) Spent Nuclear Fuel (SNF) Management Program as it relates to the SRS. Finally, it describes the representative sites located on the SRS that could be spent nuclear fuel facilities.

2.1 SRS Overview

The SRS is a key DOE facility for research on and processing of special nuclear materials. The U.S. Government built the Site in the early 1950s to produce the basic materials - plutonium-239 and tritium - used in the fabrication of nuclear weapons. The DOE Savannah River Operations Office manages the SRS, and Westinghouse Savannah River Company (WSRC) operates the Site under contract to DOE.

2.1.1 Site Description

The SRS occupies an area of approximately 310 square miles (800 square kilometers) in South Carolina, in a generally rural area about 25 miles (40 kilometers) southeast and 12 miles (19 kilometers) south of Aiken, South Carolina (Figure 2-1). The Site is on the southwestern border of the SRS, which includes portions of Aiken, Barnwell, and Colleton Counties. The average population density (1990 census data) in the six-county region around the Site is 140 people per square mile (54 per square kilometer); the largest population center is 2,595 people per square mile (1,002 per square kilometer) in the City of Augusta (Hawkins). Other population centers - Aiken, Allendale, Barnwell, and North Augusta, South Carolina - are within 22 miles (40 kilometers) of the Site. Three small towns - Jackson, New Ellenton, and Snelling, South Carolina - are adjacent to the SRS boundary to the northwest, north, and northeast, respectively. Based on 1990 U.S. Census Bureau data, the population within a 50-mile radius of the SRS is approximately 620,100 (Arnett et al. 1993).

The Site consists primarily of managed upland forest with some wetland areas. Wetlands occupy approximately 5 percent of the SRS land area. Access to the Site is limited to U.S. Highway 278, SRS Road 1, and the CSX Railroad corridor. Figure 2-1. National location of SRS. public transportation limited to through the U.S. Highway 278, SRS Road 1, and the CSX Railroad corridor.

The SRS contains 15 major production, service, and research and development (R&D) facilities. The SRS previously supported nuclear materials production and can support processing and management activities. Major SRS facilities include five nuclear reactors, two chemical processing plants, a fuel and target fabrication facility, the Defense Waste Processing Facility Replacement Tritium Facility, a heavy-water rework plant, and the Savannah River Technology Center (SRTC), formerly called the Savannah River Laboratory. In addition, the University of Georgia Research Foundation operates the Savannah River Ecology Laboratory (SREL) on the Site under contract to DOE. Under an interagency agreement, the U.S. Forest Service operates the River Forest Station, which manages the natural resources and secondary roads on the Site. Facilities are in defined areas scattered across the Site. Each area is identified as summarized in Table 2-1. Figure 2-2 shows the locations of the principal SRS facilities. The reactor, waste storage, and separations areas are at least 4 miles (6 kilometers) from the Site boundary.

The primary SRS facilities were related to the production of nuclear materials. The SRS manufactured fuel and target components for shipment to the SRS reactors. Original facilities operated five reactors; at present, all are in shutdown status. Shielded railroad cars transported irradiated fuel to the F- or H-Area Canyon for the recovery of nuclear materials. The separations processes dissolve irradiated components in acid, and extract and separate nuclear materials. In H-Area, additional processes extract other products from irradiated fuel.

DOE neutralizes and stores the high-level liquid radioactive waste generated by the SRS facilities in underground tanks. DOE plans to process this waste into a borosilicate glass waste form at the Defense Waste Processing Facility when that facility becomes operational, or in a waste form at the SRS until an offsite geological repository is available. [DOE has

Supplemental EIS related to Defense Waste Processing Facility operations (DOE 1994a) to the underground waste storage tanks, DOE has established a centrally located 196 (0.8-square-kilometer) site between F- and H-Areas, called E-Area, for the disposal radioactive waste and the storage of transuranic (TRU) radioactive waste and mixed radioactive waste. The Site also has a central sanitary landfill and buildings in

Table 2-1. Description of functions and principal facilities at SRS areas.

Area	Function	Principal facilities
A	Main DOE administration area, research laboratories	Main administration building, Savanna Technology Center, Savannah River Ecology Laboratory, powerhouse
B	Wackenhut Services, Inc., administration area (security)	Administration building, WSRC Engineer building, WSRC training buildings
C	One of five SRS reactors	C-Reactor, training facilities, cooling
D	Central powerhouse and heavy-water rework	Powerhouse, heavy-water rework facility
E	Waste disposal and storage	Solid Waste Disposal Facility
F	Process plutonium	F-Area Canyon, FB-Line, tank farm
G	Various support functions	Spread throughout the Site: railroad U.S. Forest Service installations
H	Process uranium and tritium	H-Area Canyon, HB-Line, Effluent Treatment Facility, tank farm, Receiving Basin Fuels, Consolidated Incineration Facility
K	One of five SRS reactors	K-Reactor, cooling basins, cooling towers
L	One of five SRS reactors	L-Reactor, cooling basins
M	Production of fuel and target assemblies	Slug and target production facilities treatment facility
N	Receiving	Central Shops
P	One of five SRS reactors	P-Reactor, cooling basins
R	One of five SRS reactors	R-Reactor, cooling basins
S	Process high-level radioactive waste	Defense Waste Processing Facility
TNX	Applied research and development	Analytical laboratory, Defense Waste Technology facilities, various mockup treatment facilities
Z	Waste treatment and handling	Saltstone facility

(N-Area) for the storage of nonradioactive hazardous wastes and mixed waste. DOE issued EIS on waste management activities at the SRS (DOE 1995a).

The Site contains facilities for processing support and for research and development include operational coal-fired powerhouses in A-, D-, and H-Areas that generate electricity. Figure 2-2. Location of principal SRS facilities (see Table 2-1). The largest powerhouses are in H-, and S-Areas through a 7-mile (11-kilometer) steam line. D-Area also contains a rework facility at which DOE purified the deuterium oxide (heavy water) used as the coolant in SRS reactors. TNX-Area facilities study chemical and waste processing production-scale equipment. Finally, A-Area facilities include the Savannah River Ecology Laboratory, and the DOE and Westinghouse Savannah River administrative offices.

The SRS employs approximately 20,000 people. Most of these employees work for Westinghouse Savannah River Company and its subcontractors. The remainder work for Savannah River Ecology Laboratory, Wackenhut Services, Inc., the U.S. Forest Service contractors.

2.1.2 Site History

The U.S. Atomic Energy Commission (AEC), a DOE predecessor agency, selected the site for the SRS in November 1950 after a study of more than 100 prospective sites. The selected E. I. du Pont de Nemours and Company, Inc., to build and operate the facility began in February 1951; the basic plant was completed in 1956 at a cost of \$1.1 billion. On October 3, 1952, operations began with the startup of a unit of the heavy plant. Criticality occurred in the first production reactor on December 28, 1953.

In 1972, the AEC designated the SRS as the nation's first National Environmental Laboratory. Through the years, scientists have performed a wide range of investigations on the flora, and fauna of the Site.

2.1.3 Mission

The historic mission of the SRS was to serve the national security interests of the United States by safely processing nuclear materials while protecting the health and safety of the public and protecting the environment. The SRS was responsible for producing tritium and other nuclear materials for national defense. At present, it supports the viability of recycling limited-life components. The SRS also produces isotopes for nonweapons and medical applications.

The SRS spent nuclear fuel mission is to manage DOE-owned spent fuel in a cost-effective manner that protects the safety of SRS workers, the public, and the environment. The goal of the program is the accurate quantification and characterization of DOE-owned spent nuclear fuel, assessment of spent nuclear fuel storage facilities, elimination of current spent nuclear fuel vulnerabilities, and identification of technologies and requirements for interim and ultimate disposition of spent nuclear fuel.

2.1.4 Management

The DOE Savannah River Operations Office manages the SRS; the Westinghouse Savannah River Company operates the Site under contract to DOE. Westinghouse assumed operational responsibility in April 1989 from E. I. du Pont de Nemours and Company, Inc., which operated the Site since 1951.

2.2 Regulatory Framework

This section summarizes the framework of environmental protection regulations that apply to spent nuclear fuel management at the SRS. The framework is based on Federal and State laws and one local ordinance, as discussed below. Volume 1 (Section 7.0) of this EIS provides additional information on the major Federal environmental regulations, Executive Orders, and DOE Orders that apply to spent nuclear fuel management alternatives.

2.2.1 Federal

The U.S. Environmental Protection Agency (EPA) has authorized South Carolina to implement most provisions of the Clean Air Act, Resource Conservation and Recovery Act, and Clean Water Act that apply to SRS spent nuclear fuel management. EPA Region IV has the lead responsibility for implementing Clean Air Act standards for radionuclide emissions from DOE facilities, imposing monitoring and approval requirements on SRS spent nuclear fuel management activities that could result in radionuclide emissions.

In addition, EPA Region IV has Resource Conservation and Recovery Act authority over radioactive hazardous (mixed) waste management, affecting wastes from spent nuclear fuel. EPA Region IV and the DOE Savannah River Operations Office have entered into a Federal Compliance Agreement on SRS mixed waste management.

The U.S. Army Corps of Engineers District Engineer for the Charleston District implements the Clean Water Act Section 404 and the Rivers and Harbors Act permitting program for SRS spent nuclear fuel construction activities that would affect U.S. waters.

In accordance with the Endangered Species Act, the SRS would consult with the U.S. Fish and Wildlife Service, Charleston Field Office on impacts that spent nuclear fuel construction could have on threatened and endangered species.

2.2.2 State

The South Carolina Department of Health and Environmental Control implements the State laws that would affect SRS spent nuclear fuel management activities:

- Pollution Control Act (nonradioactive emissions and discharges, and nonhazardous waste management)
- Hazardous Waste Management Act (nonradioactive hazardous waste management)
- Safe Drinking Water Act
- Groundwater Use Act
- Stormwater Management and Sediment Reduction Act

The U.S. Army Corps of Engineers District Engineer for the Charleston District

agreement with the South Carolina Department of Health and Environmental Control which department issues Clean Water Act Section 401 water quality certifications. The South Carolina Department of Health and Environmental Control also receives SRS reports in accordance with the Emergency Planning and Community Right-To-Know Act.

The South Carolina State Department of Archives and History includes the State Preservation Office. In accordance with the National Historic Preservation Act, the State Historic Preservation Officer on impacts that construction activities have on cultural resources.

2.2.3 Local

The only local requirement applicable to SRS spent nuclear fuel management is the County Sediment Control Ordinance, which would affect construction activities.

2.3 Spent Nuclear Fuel Management Program at the Savannah River Site

This EIS addresses the management of approximately 2,742 metric tons of heavy metal (3,023 tons) of spent nuclear fuel that would be stored at various locations within the DOE Complex over the next 40 years (1995-2035). At present, DOE has stored approximately 206.3 (227.4 tons), or about 8 percent of this material, at the SRS. The spent nuclear fuel at the SRS that DOE has included in the analyses in this document includes:

- 184.4 MTHM (203.3 tons) of Savannah River Defense Production [highly enriched (HEU) aluminum-clad fuels], including plutonium target material, and other fuels
- 4.6 MTHM (5.1 tons) of commercial spent fuel (primarily zirconium-clad)
- 11.9 MTHM (13.1 tons) of test and experimental reactor Zircaloy-clad fuel
- 5.4 MTHM (6.0 tons) of test and experimental reactor stainless steel-clad fuel

Spent nuclear fuel is currently stored in the Receiving Basin for Offsite Fuels, reactor disassembly basins, and in basins in F- and H-Canyons. Table 2-2 shows the fuel stored at these facilities.

Table 2-2. SRS Fuel Inventory by Facility.

Facility	Quantity (MTHM)
Receiving Basin for Offsite Fuel	60.73
L-Reactor Disassembly Basin	118.11
K-Reactor Disassembly Basin	3.32
P-Reactor Disassembly Basin	1.41
F-Canyon	22.63
H-Canyon	0.07
Total	206.27

Source: Wichmann (1995).

The F- and H-Area Canyons at the SRS are among the only remaining operable chemical separations facilities of their kind in the DOE Complex. Each canyon has an associated basin that serves as an interim staging area where reactor fuel bundles and targets await the Chemical Separations Process. The basins currently contain 13 reactor fuel assemblies (H-Area) and 13 clad targets (F-Area).

DOE has stored most of the remaining aluminum-clad spent nuclear fuel from SRS operations under water in concrete reactor storage basins. Three reactor disassembly and L-Reactors) contain reactor fuel and target material. These structures were built but were not intended for the prolonged storage of radioactive materials. Wet (underwater) storage is potentially viable for stainless steel-clad fuel elements, is not satisfactory for aluminum-clad fuels which are subject to corrosion and pitting.

In March 1992, chemical processing operations were suspended in the canyons to address a potential safety concern. The concern was subsequently addressed but prior to resuming processing, the Secretary of Energy directed that defense related chemical separations (reprocessing) be phased out at the SRS. Since the decision, DOE has determined that the disposition of nuclear material, including spent nuclear fuel, is subject to the Environmental Policy Act (NEPA) process. Non-safety related facility operations have continued with the exception of Pu-238 processing associated with the support of NASA missions.

As a result of these shut-downs, the canyons and the basins used for storage of and irradiated targets have a large inventory of in-process solutions and fuel and other materials. Some materials stored in the L- and K-Reactor disassembly basins have corroded, releasing materials into the pool water. DOE is preparing an environmental impact statement that

risks that these and other SRS materials represent to the public and workers and the near-term need for the actions to stabilize these materials to ensure continued safe (DOE 1995b). These actions would take place over the short-term (about 10 years), make programmatic decisions on disposition.

DOE stores other spent fuel in the Receiving Basin for Offsite Fuels (RBOF) on basin, which is in H-Area near the center of the Site, has been operating and receiving origin since 1964. This 15,000-square-foot (1,393-square-meter) facility consists of a basin, two storage basins, a repackaging basin, a disassembly basin, and an inspect basins and their interconnecting transfer canals hold about 500,000 gallons (1,893, Spent fuel elements arrive in lead-lined casks weighing from 24 to 70 tons (about 2 tons), which a crane lifts from a railroad car or truck trailer and places in the u 30 percent of the fuels in the Receiving Basin for Offsite Fuels consist of uranium steel or Zircaloy, which SRS facilities cannot process without modifications.

2.4 Vulnerabilities Associated with SRS Spent Nuclear Fuel

In August 1993, the Secretary of Energy commissioned a comprehensive baseline of the environmental, safety, and health vulnerabilities associated with the storage of the DOE complex. The purpose of this assessment was to determine the inventory and the Department's Reactor Irradiated Nuclear Material, which includes spent nuclear irradiated target material. The assessment also evaluated the condition of the fuel and identified the vulnerabilities and problems currently associated with these. Vulnerabilities in nuclear facilities are conditions or weaknesses that could lead to the public, unnecessary or increased exposure to workers, or release of radioactive environment. Loss of institutional controls, such as a cessation of facility funding facility maintenance and control, could cause some vulnerabilities.

Based on this evaluation process DOE released a report to the Secretary of Energy Fuel Working Group Report on Inventory and Storage of the Department's Spent Nuclear other Reactor Irradiated Nuclear Materials and Their Environmental, Safety and Health Vulnerabilities (i.e., "The Working Group Report," Volumes I, II, and III), to the December 7, 1993 (DOE 1993). This report identified over 100 vulnerabilities associated with fuel storage in the DOE complex, including 19 at the Savannah River Site. The report that five facilities and three burial grounds warranted priority attention from management unnecessary increases in worker radiation exposure and cost during cleanup. The Savannah L- and K-Reactor Disassembly Basins were among these facilities. The report grouped associated with each facility into three categories for management attention based on action should be initiated: less than 1 year, 1 to 5 years, and more than 5 years.

After issuing the Working Group Report, DOE developed a Plan of Action to address vulnerabilities, taking into consideration currently available resources for implementation. Action is a consolidation of individual action plans designed to address each spent vulnerability in a manner that reflects the DOE (1) sense of urgency, (2) concern for protection, (3) commitment to avoid or otherwise mitigate environmental impacts, and compatible long-term solutions.

The interim goal for the Savannah River Site reactor disassembly basins, pending the removal of the stored material, is the stabilization of basin conditions to reduce address known vulnerabilities. The long-term goal of the action plan is a safe storage of reactor-irradiated nuclear material within a 5-year period, consistent with safe and sound operations, including completion of appropriate NEPA review. These actions will mitigate the identified vulnerabilities while DOE pursues other courses of action.

The 19 vulnerabilities identified for the Savannah River Site now have complete (DOE 1994b, 1994c, 1994d). Table 2-3 lists SRS vulnerabilities by facility, tracking categorization, and Action Plan status.

DOE is currently implementing a number of the 19 Action Plans. These actions have been evaluated under the NEPA review process. The remaining corrective actions, those that are out through FY99, would also undergo NEPA review prior to implementation. Only one outstanding action, the construction of a dry storage facility, would likely require documentation (e.g., an EIS). The construction of such a facility is addressed in the EIS as part of the Decentralization, 1992/1993 Planning Basis, Regionalization, and alternatives. Construction of new facilities would require site-specific NEPA documentation. **Table 2-3.** SRS vulnerabilities by facility, vulnerability, tracking number, prior Action Plan status.

Site/Facility	Priority	Eight major	Less than
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Vulnerability Number		facilities with 1 year
Description		vulnerabilities
SRS/L-Reactor Disassembly Basin		y
SRS-01		
Potential unmonitored buildup of radionuclide or fissile materials in sand filters.		
SRS/L-Reactor Disassembly Basin		y
SRS-04		
Lack of authorization basis in operating the sand filter cleanup system for L-Area Disassembly Basin.		
SRS/Reactor Disassembly Basins		
SRS-05		
Corrosion of aluminum clad fuel, targets, and components.		
SRS/L-Reactor Disassembly Basins		y
SRS-06		
Cesium-137 activity level in L-Basin.		
SRS/L-Reactor Disassembly Basins		y
SRS-07		
Determine whether gas bubbles release is a potential hazard above the bucket storage area at L-Reactor.		
SRS/K-, L-, P-Reactors		y
SRS-08		
Lack of Reactor Authorization Basis.		
SRS/K-Reactor Disassembly Basins		y
SRS-09		
Corrosion of Mark 31 A and B target slugs in K and L disassembly basins.		
SRS/P-Reactor Disassembly Basins		y
SRS-10		
Hoist Rod Corrosion		
SRS/K-, L-Reactor Disassembly Basins		y
SRS-11		
Reactor Disassembly Basin Safety Analysis Envelope.		
SRS/L-Reactor Disassembly Basin		y
SRS-12		
Inadvertent flooding of L-Reactor Disassembly Basin.		
SRS/K-Reactor Disassembly Basin		y
SRS-13		
Inadvertent flooding of K-Reactor Disassembly Basin.		
SRS/P-Reactor Disassembly Basin		y
SRS-14		
Inadvertent flooding of P-Reactor Disassembly Basin.		
Table 2-3. (continued).		
Site/Facility		Priority
Vulnerability Number		Eight major
Description		facilities with less than
SRS/RBOF; P-, R-, L-, C-, R-Reactors		vulnerabilities 1 year
SRS-15 (NOTE: RBOF is a less than 1 year vulnerability)		y
Conduct of operations at reactor facilities and RBOF.		
SRS/Receiving Basin for Offsite Fuel (RBOF)		y
SRS-16		
Inadequate tornado protection at RBOF.		
SRS/Receiving Basin for Offsite Fuel (RBOF)		y
SRS-17		
Seismic vulnerability of RBOF.		
SRS/H-Area Canyon		
SRS-18		
Seismic vulnerability of H-Area Canyon.		
SRS/F-Area Canyon		
SRS-19		
Seismic vulnerability of F-Area Canyon.		

SRS/K-, L-, P-Reactor Disassembly Basins and RBOF	Y
SRS-20	
Inadequate leak detection system in the underground water-filled RINM storage basin.	
SRS/L-, K-, P-Reactor Disassembly Basins	Y
SRS-21	
Inadequate seismic evaluation and potential inadequacies of structures, systems, and components to withstand a design basis event.	

2.5 Representative Host Sites

DOE has identified two SRS areas as representative host sites for potential fac implementation of programmatic decisions on spent nuclear fuel management (Figure 2

- F- and H-Areas (considered together) for the modification or expansion of e new wet storage, and support facilities
- An undeveloped site for the construction of major new facilities, primarily Core Facility or dry storage vault.

Figure 2-3. Representative host sites on Savannah River Site. 2.5.1 F- and H-Areas

These two areas contain most of the current spent nuclear fuel facilities and o SRS, including the Receiving Basin for Offsite Fuels. Therefore, DOE would focus f under any of the alternatives in these areas as well, for cost-effectiveness and be would occur in areas that had been previously disturbed.

F- and H-Areas are about 2 miles (3.2 kilometers) apart near the center of the Site boundary is approximately 7.5 miles (12 kilometers) to the west. DOE uses the 5-mile (8-kilometer) radius of the two areas either for industrial purposes associa operations or as managed forest land. The closest facility to F- and H-Areas is th Waste Disposal Facility, which lies between the two areas (Figure 2-3). DOE uses t dispose of SRS solid low-level radioactive waste and to store TRU radioactive waste

The F-Area separations facilities occupy about 420 acres (1.7 square kilometers) were designed primarily for the recovery of plutonium-239 from irradiated and unirradiated materials. DOE used the F-Area Canyon to dissolve target materials and produce sol contained the various products extracted from fission products. Further processing products from solution to solid form for shipment off the Site. Large tanks in F-A liquid radioactive waste for future stabilization and disposal through the Defense Facility.

H-Area facilities occupy about 395 acres (1.6 square kilometers). The H-Area C irradiated fuel elements or target assemblies from reactors. Primary operations in of irradiated targets and fuel tubes, chemical and physical separation, and purific DOE stores high-level liquid waste in large tanks in H-Area, as in F-Area, for futu disposal through the Defense Waste Processing Facility.

2.5.2 Undeveloped Representative Host Site

DOE has selected an undeveloped representative host site for the construction o that F- or H-Area could not accommodate. This site is to the south and east of H-A SRS Road E and close to an existing railroad line, as shown in Figure 2-3. The SRS connections to existing electricity, water, and steam networks with minimal additio The use of this site would have the advantage of consolidating spent nuclear fuel-r F- and H-Areas and close to the center of the SRS.

This site is representative of many available areas on the SRS that could suppo fuel management activities. For example, DOE has identified a different representa possible construction of the Expanded Core Facility for the management of naval spe (see Appendix D of Volume 1 of this Environmental Impact Statement). DOE would con detailed siting analysis before implementing any programmatic decision at the SRS. assess, as necessary, the environmental consequences of the siting of any facilitie specific NEPA documentation.

3. SPENT NUCLEAR FUEL ALTERNATIVES

This chapter describes the five management alternatives for spent nuclear fuel U.S. Department of Energy (DOE) has evaluated for the Savannah River Site (SRS) as Volume 1 of this Environmental Impact Statement. These alternatives are:

1. No Action
2. Decentralization
3. 1992/1993 Planning Basis
4. Regionalization (with 2 subalternatives for the SRS)
5. Centralization (with 2 subalternatives for the SRS)

The activities covered by the alternatives range from maintaining the current inventory at the SRS without receiving any more shipments (Alternative 1), through keeping inventory and accepting or sending off some limited shipments (Alternatives 2 through 5). At the Site all DOE spent nuclear fuel and some from other sources (Alternative 5) examined an option for shipping all spent nuclear fuel at the SRS to another location (a variation of Alternatives 4 and 5). Table 3-1 summarizes the quantities of material received, shipped out, and ultimately managed at the SRS under the various alternatives. The chapter assessed the aluminum-clad spent nuclear fuel separately from nonaluminum-clad fuel (steel and Zircaloy) because the options for managing them at the Site could be different in Section 3.1.

The analytical approach used in this document produces estimates of consequences as large as or larger than any that could occur or be expected under the alternative comparison of the impacts of the principal technologies for managing spent nuclear fuel.

This chapter also provides an overview of the SRS management approach and describes the alternatives as they relate to the SRS (Sections 3.1 and 3.2). In addition, the chapter compares the potential environmental consequences of each alternative (Section 3.3).

Table 3-1. Quantities (MTHM) of spent nuclear fuel that would be received, shipped at the SRS under the five alternatives. a, b, c

Alternative	Fuel Type	Currently at SRS	Receive	Ship Out	Total SRS alt
1. No Action	Aluminum	184.40	0.00	0.00	184
	Nonaluminum	21.87	0.00	0.00	21
	Totals	206.27	0.00	0.00	206
2. Decentralization	Aluminum	184.40	11.02	0.00	195
	Nonaluminum	21.87	2.60	0.00	24
	Totals	206.27	13.62	0.00	219
3. 1992/1993 Planning Basis	Aluminum	184.40	13.69	0.00	198
	Nonaluminum	21.87	2.80	0.00	24
	Totals	206.27	16.49	0.00	222
4. Regionalization - A (by fuel type)	Aluminum	184.40	28.69	0.00	213
	Nonaluminum	21.87	0.00	(21.87)	0
	Totals	206.27	28.69	(21.87)	213
4. Regionalization - B (by location at SRS)	Aluminum	184.40	19.93	0.00	204
	Nonaluminum	21.87	30.42	0.00	52
	Totals	206.27	50.35	0.00	256
4. Regionalization - B (by location, elsewhere)	Aluminum	184.40	0.00	(184.40)	0.0
	Nonaluminum	21.87	0.00	(21.87)	0.0
	Totals	206.27	0.00	(206.27)	0.0
5. Centralization (at SRS)	Aluminum	184.40	28.69	0.00	2
	Nonaluminum	21.87	2,506.84	0.00	2,5
	Totals	206.27	2,535.53	0.00	2,7
5. Centralization (elsewhere)	Aluminum	184.40	0.00	(184.40)	0.0
	Nonaluminum	21.87	0.00	(21.87)	0.0
	Totals	206.27	0.00	(206.27)	0.0

a. To convert metric tons of heavy metal to tons, multiply by 1.1023.

b. Numbers may not sum due to rounding.

c. Source: Wichmann (1995).

3.1 SRS Management Approach

3.1.1 Management Options

DOE has evaluated three options for the management of spent nuclear fuel at the five alternatives considered for this EIS. These technical management options are storage of all fuels and the processing of aluminum-clad fuels. DOE could implement individually or in combination under any of the five alternatives. DOE would base or more of these technical management options on additional analysis, including a specific National Environmental Policy Act (NEPA) review based on this programmatic

3.1.1.1 Wet Storage. As described above in Section 2.3, the SRS currently maintains its

spent nuclear fuel in wet storage in the Receiving Basin for Offsite Fuels and severe wet storage under the 40-year interim management plan (except under the No Action alternative would require that DOE construct a new wet storage pool at the SRS and move all fuel. Prior to this transfer, DOE could place all the aluminum-clad fuel in stainless steel to further corrosion and breakdown of the fuel cladding. The stainless steel- and Zircaloy could also require canning. The SRS would monitor and maintain the water quality of the fuel in the storage pool throughout the interim management period.

Under this wet storage option, the spent nuclear fuel would be in an interim state that could require further treatment depending on the DOE decision on its ultimate disposition.

3.1.1.2 Dry Storage. DOE currently has no dry storage facilities for spent nuclear fuel at the

Site. Dry storage of SRS aluminum-clad fuels under this management plan would require development prior to the construction of a dry storage facility. Although such facilities exist at DOE sites and at commercial locations, DOE believes that the characteristics of SRS fuel are sufficiently different to require some research and development before the design of a facility for this fuel. DOE would cask all fuel before placing it into the dry storage facility. DOE also has to maintain and monitor the facility for the remainder of the 40-year management period.

As with wet storage, the dry storage option would place the spent fuel into an interim form that could require further treatment later depending upon DOE's decision on ultimate disposition.

3.1.1.3 Processing and Dry Storage. One method under this option would be for the SRS

to process existing aluminum-clad spent nuclear fuel through the existing separation process in the F- and H-Area Canyons, and place the nonaluminum-clad fuels and any future receipts. The process using existing capability would result in the generation of both separated products (e.g., uranium oxide), which would be stored on the site in existing facilities, and nonseparated products that would be placed in existing waste storage facilities for later conversion through the Defense Waste Processing Facility (DWPF). DOE would maintain and develop a dry storage facility containing the nonaluminum-clad spent fuel. Variations of this option are also possible, such as processing all the aluminum-clad fuel currently on the SRS received from elsewhere, or developing the capability at the SRS for processing for without chemical separations.

The process option selected for evaluation in this document is representative of processing options that might be employed, but is not necessarily the one that DOE would select. Detailed NEPA evaluations would be required to implement any spent nuclear fuel management option at the SRS.

3.1.2 Management Plan

Figure 3-1 summarizes DOE's overall plan for the interim management of aluminum-clad and nonaluminum-clad fuels at the SRS. This flowchart shows actions for all alternative management options, as explained in Section 3.2.1.

3.1.2.1 Aluminum-clad Fuels. Depending on the alternative and option selected, DOE could

(within constraints of mission commitments) consolidate some aluminum-clad fuel in

Basin for Offsite Fuels to take advantage of this facility's superior water quality aluminum-clad fuel into dry storage, wet storage, or initiate processing (Figure 3-process aluminum-clad fuel without any consolidation work. Before moving the fuel storage, DOE would place it in cans. DOE would hold the canned fuel or the stabilize processing in storage for the 40-year interim management period until it decided th

DOE would place aluminum-clad fuels received by the SRS from other locations in storage. DOE could not implement any of the options for aluminum-clad fuels, with processing using existing SRS capabilities, without a technology development effort

3.1.2.2 Nonaluminum-clad Fuels. DOE options for the management of nonaluminum-clad

fuels at the SRS are somewhat different, in that only dry or wet storage is considered. The processing of these fuels at the Site is not an option because the SRS does not have operational facilities capable of separating these materials. To improve aluminum-DOE could consolidate the nonaluminum-clad fuel inventory in a reactor basin where resistant stainless steel or Zircaloy cladding would be less susceptible to corrosion and remain there until DOE built new dry or wet storage facilities. DOE would then can move it into the new storage. DOE would place any nonaluminum-clad fuel received a completion of the new facilities directly into storage. The fuel would remain in t until DOE decided its ultimate disposition.

Figure 3-1. Diagram of how SRS would manage aluminum-clad and nonaluminum-clad f available.

3.2 Description of Alternatives

3.2.1 Overview

Table 3-2 compares actions under each of the five alternatives. These actions requirements for transportation, stabilization, facilities, and research and development address for each alternative. Transportation would include onsite movements as well shipment of spent fuel. The consideration of facilities addresses not only new ones required, but also the use of existing structures and capabilities such as the F- a SRS. Finally, each alternative would involve some level of research and development related to spent nuclear fuel interim management (e.g., stabilization, transportation ultimate disposition).

Alternative 1 (No Action) addresses only the interim wet storage option, while Alternatives 2 through 5 considers three options: dry storage, wet storage, and processing aluminum-clad fuels and placing the other fuels into storage. In addition, Alternative an option for the shipment of spent nuclear fuel off the SRS. This analytical approach relative impact of viable interim storage technologies for the range of alternatives considering for the SRS. However, this information is not sufficient to support the specific interim storage technology at the SRS because DOE has not completed site-specific and development for dry storage and wet storage methods or an evaluation of other options. In addition, the specific quantities of offsite fuel that DOE would manage are subject selection of an interim storage technology will be the subject of separate NEPA documentation to the SRS.

Figure 3-2 is a matrix showing the types of facilities that would be required for each alternative and option. The list includes those facilities already operating at the SRS (e.g., Offsite Fuels) as well as potential facilities (e.g., fuel characterization facilities) facilities in its evaluation of the consequences of each alternative, as described in the alternatives.

The alternatives described below address interim storage to 2035; further treatment of nuclear fuel would be necessary before DOE obtained a final disposable waste form. DOE does not address this additional treatment. However, DOE would carry out a full NEPA decision on final disposition of spent nuclear fuel.

Table 3-2. Actions required under each of the five alternatives at the SRS.

Alternative	Transportation	Stabilization
1. No Action	No shipments to or from the Site. Limit onsite transfers to those required for safe storage.	Place aluminum-clad fuel in wet storage if are badly corroded and in danger of cladding failure. Return fuel to wet storage.
2. Decentralization	Receive about 13.6 MTHM (15.0	Can aluminum-clad fuel

	tons) of aluminum-clad and nonaluminum-clad fuels. Limit onsite transfers to those required for safe storage, consolidation, and research and development. Later relocate fuels to new wet or dry storage facility or move aluminum-clad fuels to F- and H-Canyons for processing.	place them in wet or storage or process ex through F- and H-Cany Can stainless-steel a Zircaloy fuels and pl or dry storage.
3. 1992/1993 Planning Basis	Receive about 16.5 MTHM (18.2 tons) of aluminum-clad and nonaluminum-clad fuels. Limit onsite transfers to those required for safe storage, consolidation, and research and development. Later relocate fuels to new wet or dry storage facility, or move aluminum-clad fuels to F- and H-Canyon for processing.	Can aluminum-clad fue place them in wet or storage or process ex through F- and H-Cany Can stainless steel a Zircaloy fuels and pl or dry storage.
4. Regionalization - A (by fuel type at the SRS)	Receive about 28.7 MTHM (31.6 tons) of aluminum-clad fuel. Ship to Idaho National Engineering Laboratory about 21.9 MTHM (24.1 tons) of stainless steel and Zircaloy fuel. Relocate aluminum-clad fuels to Receiving Basin for Offsite Fuels, as necessary; then to new wet or dry storage facilities, or move aluminum-clad fuels to F- and H-Canyon for processing.	Can aluminum-clad fue place them in wet or storage; or process e fuel through F- and H-Canyons.
4. Regionalization - B (by location at the SRS)	Receive approximately 50.4 MTHM (55.6 tons) of spent fuel from other locations. Limit onsite transfers to those required for safe storage, consolidation, and research and development. Relocate fuels to new dry or wet storage facility or move aluminum-clad fuel to F- and H-Canyons for processing.	Can aluminum-clad fue place them in wet or storage; or process e aluminum-clad fuels t F- and H-Canyons and remaining fuel. Char and can fuel received offsite that is not i suitable for direct p into storage.
4. Regionalization - B (by location at another site)	Move all fuels to new characterization facility prior to shipment offsite. Ship out about 206.3 MTHM (227.4 tons) of spent fuel.	Characterize and can fuel prior to shipmen
5. Centralization (at the SRS)	Receive about 2,535.5 MTHM (2,794.9 tons) of spent fuel from offsite. Limit onsite transfers to those required for safe storage, consolidation, and research and development. Relocate fuels to new dry or wet storage facility or move aluminum-clad fuel to F- and H-Canyons for processing.	Can aluminum-clad fue place them in wet or storage; or process e aluminum-clad fuels t F- and H-Canyons and remaining fuels. Cha and can fuel received offsite that is not i suitable for direct p storage.
5. Centralization (at another site)	Move all fuels to new characterization facility prior to shipment offsite. Ship out about 206.3 MTHM (227.4 tons) of spent fuel.	Characterize and can fuel prior to shipmen

Figure 3-2. Types of facilities required for each alternative. 3.2.2 Alternative 1 - No Action

3.2.2.1 Overview. This alternative deals only with the minimum actions that DOE would

deem necessary for the continued safe and secure management of spent nuclear fuel. quo condition. Rather, across its complex of facilities, DOE would maintain spent to generation or current storage locations with no shipment between sites. Facility replacements and onsite fuel transfers would occur only to support safe and secure DOE would continue existing and new research and development activities for spent f management. Stabilization activities would be limited only to those minimum action spent nuclear fuel safely.

3.2.2.2 SRS Alternative 1 - Wet Storage. DOE would initiate the various SRS programs

and activities necessary to obtain optimum use of existing spent nuclear fuel facility storage of existing Site inventories totalling 206.3 metric tons (227.4 tons) of the following quantities:

- 184.4 MTHM (203.3 tons) of Savannah River Defense Production [highly enriched (HEU) aluminum-clad fuels], including plutonium target material, and other fuels
- 4.6 MTHM (5.1 tons) of commercial spent nuclear fuel (primarily zirconium-clad)
- 5.4 MTHM (6.0 tons) of test and experimental reactor stainless steel-clad fuel
- 11.9 MTHM (13.1 tons) of test and experimental reactor Zircaloy-clad fuel

The goal of this program would be to relocate some aluminum-clad fuels to the R for Offsite Fuels where precisely maintained water quality would prolong the storage types. In addition, DOE would relocate a portion of the stainless steel- and Zircaloy-clad reactor basin, where their more resistant cladding would maintain fuel containment period. These actions would be accomplished within the constraints of mission requirements.

The following describes one method that could be employed to improve the storage of aluminum-clad fuel. Variations of this plan that would involve only the use of existing facilities are also possible.

- Select a reactor basin for upgrading and for the interim storage of SNF.
- Relocate aluminum-clad fuels from the selected reactor basin to other on-site storage basins.
- Cleaning and repair of the basin chosen for upgrade to improve water quality.
- Consolidate fuels in the Receiving Basin for Offsite Fuels to the extent possible.
- After cleaning and renovating the selected reactor basin, move a portion of the Zircaloy-clad fuel assemblies now at the Receiving Basin for Offsite Fuels to the renovated reactor basin.
- Move the aluminum-clad fuels temporarily stored at other locations to the R for Offsite Fuels or the renovated reactor basin.

DOE will continue to place heavily corroded aluminum-clad fuel elements that pose a danger of cladding failure into containers in the wet pool as required to minimize corrosion throughout the pool. This action would be much simpler than canning the fuel and would occur under the other alternatives.

This alternative would require no new facilities. DOE would continue existing fuel-related research and development.

3.2.3 Alternative 2 - Decentralization

3.2.3.1 Overview. Under this alternative, DOE would maintain existing spent nuclear fuel in

storage at the current locations, and the SRS would receive some shipments of unenriched foreign fuel. This alternative differs from the No Action alternative by allowing development and upgrades. DOE could transport fuel on the Site for safety, fuel research and development activities. In addition, DOE could undertake actions it deemed though not essential, for safety and could perform spent nuclear fuel processing, transportation, and development.

3.2.3.2 SRS Options 2a, 2b, and 2c. DOE analyzed three options specific to the SRS for

this alternative: Option 2a deals with dry storage, Option 2b deals with wet storage, and Option 2c involves processing existing SRS aluminum-clad spent nuclear fuel and storing the reprocessed fuel.

The amount of spent fuel that the SRS would manage includes its current inventory, above for Alternative 1, plus:

- 11.0 MTHM (12.0 tons) of aluminum-clad fuel
- 1.1 MTHM (1.2 tons) of stainless steel-clad fuel
- 0.7 MTHM (0.8 ton) of Zircaloy-clad fuel
- 0.8 MTHM (0.9 ton) of other experimental fuel

Under this alternative, SRS would manage a total of about 219.9 MTHM (242.4 t) nuclear fuel. The SRS would receive spent fuel from research reactors as existing as new storage was constructed.

3.2.3.2.1 Option 2a - Dry Storage - Under this option, DOE would store existing SRS

inventories in wet pools while developing the technology and constructing the necessary facilities to examine, characterize, and can the fuels and transfer them to a new dry storage vault for final disposition.

The SRS would proceed with the fuel rearrangement plan described above for Alternative 1 to provide acceptable storage conditions to minimize failure of aluminum-clad material before its placement in a dry-storage container.

Placement in a dry-storage facility would require a technology development program capabilities to examine, characterize, and can aluminum-clad fuel elements before placement in a vault. In addition, the SRS would investigate technologies for the ultimate disposition of fuel. In addition to a dry storage facility, the SRS would build new fuel receiving and dry canning facilities.

3.2.3.2.2 Option 2b - Wet Storage - Under this option, DOE could rearrange existing

spent nuclear fuel as described above for Alternative 1 to provide interim wet storage while constructing new facilities.

SRS could also modify this rearrangement plan to accept shipments of spent fuel from offsite and place them directly into the Receiving Basin for Offsite storage. The new wet storage facilities required under this option would have the capability to examine and characterize fuels and to can deteriorating fuels in a vault for placement in the new pool. DOE would move all fuel to the new storage pool once complete. SRS would build new fuel receiving, characterization, and wet-canning facilities for a new wet storage pool. SRS would investigate technologies for the ultimate disposition of nuclear fuel.

3.2.3.2.3 Option 2c - Processing and Storage - Under this option, SRS would

process existing aluminum-clad spent nuclear fuel to consolidate and stabilize the storage in vaults, and would place the stainless steel- and Zircaloy-clad fuel and aluminum-clad fuel in dry storage.

The fuel would remain in the current wet pools while awaiting processing or the construction of new dry storage facilities. DOE would use existing facilities to process the aluminum-clad fuel to safe, stable, consolidated forms.

The new facilities that the SRS would require under this option would be similar to those described for dry storage (Option 2a), except they would be much smaller because the amount of fuel to be stored would be small: only about 11.0 MTHM (12.0 tons) of aluminum-clad and 0.8 MTHM (0.9 tons) of nonaluminum-clad fuel.

The SRS would investigate technologies required for the ultimate disposition of

3.2.4 Alternative 3 - 1992/1993 Planning Basis

3.2.4.1 Overview. This alternative assumes the continued transportation, receipt, processing,

and storage of spent nuclear fuel. Foreign and university research reactor spent nuclear fuel would be sent to the INEL and the SRS. DOE would assess the construction of new facilities to accommodate current and projected spent nuclear fuel storage requirements. This alternative would include activities related to the treatment of spent nuclear fuel, including research and development.

and pilot programs to support future decisions on its ultimate disposition.

3.2.4.2 SRS Options 3a, 3b, and 3c. DOE analyzed the same three options for this

alternative as for Alternative 2: dry storage (Option 3a), wet storage (Option 3b) of existing SRS aluminum-clad fuel and storing the remaining fuel (Option 3c). The would be somewhat greater than those for Alternative 2 because the options assume t would manage its present inventory (see Alternative 1) plus approximately:

- 13.7 MTHM (15.1 tons) of aluminum-clad fuel
- 1.3 MTHM (1.4 tons) of stainless steel-clad fuel
- 0.7 MTHM (0.8 ton) of Zircaloy-clad fuel
- 0.8 MTHM (0.9 ton) of other experimental fuel
- a small amount (<0.1 ton) of commercial nonaluminum-clad fuel

The total spent nuclear fuel managed would equal about 222.8 MTHM (245.6 tons). would receive shipments of fuel from other locations as existing space allowed and were completed.

3.2.4.2.1 Option 3a - Dry Storage - The Site would store current inventories in

existing wet pools while developing technology and constructing facilities necessary to characterize, and can the fuels and transfer them to a new dry storage vault to await disposition.

The actions that SRS would undertake under this option and the new facilities that would be the same as those described for Option 2a - Dry Storage under Alternative 2 (Decentralization) in Section 3.2.3.2.1.

3.2.4.2.2 Option 3b - Wet Storage - DOE could rearrange existing spent nuclear fuel

as described in Alternative 1 above to provide interim wet storage capacity while new facilities are developed.

The Site could also accept new shipments directly into the Receiving Basin for Offsite Fuel, as required. The actions that SRS would undertake under this option, and that would be constructed, would be the same as those described for Option 2b - Wet Storage under Alternative 2 (Decentralization) in Section 3.2.3.2.2.

3.2.4.2.3 Option 3c - Processing and Storage - Under this option, the SRS would

process existing aluminum-clad spent nuclear fuel and would place the stainless steel-clad fuel and new receipts of aluminum-clad fuel in storage as described for Option 3c under Alternative 2 (Decentralization) in Section 3.

2.3.2.3. The requirements for new facilities and for technology development would also be the same.

3.2.5 Alternative 4 - Regionalization

3.2.5.1 Overview. This alternative has two subalternatives. The first (Regionalization A)

would involve the distribution of existing and new spent nuclear fuel among DOE sites primarily on the similarity of fuel type, although DOE would also consider transportation, available processing capabilities, available storage capabilities, or a combination. Under this subalternative, SRS would receive all aluminum-clad fuel and would transfer its inventory of stainless steel- and Zircaloy-clad fuel to another DOE site. The SRS total of about 213.1 MTHM (234.9 tons) of spent fuel under the Regionalization A subalternative.

The second subalternative (Regionalization B) would require DOE to consolidate new spent fuel at two sites - one to the east of the Mississippi River and one to the west, depending on the location or generation site of the fuel. Under this alternative, DOE would receive all spent nuclear fuel in the east [approximately 256.6 MTHM (282.9 tons)] and transfer it to an offsite to the Oak Ridge Reservation in Tennessee. An additional option for the Eastern Regional Site is for DOE to construct an Expanded Core Facility at the site. This option is described in Appendix D of Volume 1 of this EIS.

Under either subalternative, DOE would undertake facility upgrades, replacement as appropriate. This alternative would include research and development and pilot current management and future decisions on spent fuel disposition.

3.2.5.2 SRS Options 4a, 4b, and 4c (Regionalization A). DOE analyzed three options

for the regionalization of fuels by fuel type: dry storage (Option 4a), wet storage processing of existing SRS aluminum-clad fuels and storing the remaining fuel (Option 4b). This subalternative assumes that the SRS would manage:

- Its current inventory of 184.4 MTHM (203.3 tons) of aluminum-clad fuels, plus
- Approximately 28.7 MTHM (31.6 tons) of research reactor aluminum-clad fuel from other sites

The SRS would ship to the Idaho National Engineering Laboratory approximately:

- 5.4 MTHM (6.0 tons) of stainless steel-clad fuel
- 4.6 MTHM (5.1 tons) of commercial nonaluminum-clad fuel
- 11.9 MTHM (13.1 tons) of Zircaloy-clad spent fuel

DOE would manage a total of about 213.1 MTHM (234.9 tons) of spent nuclear fuel under this subalternative. The site would receive shipments from other locations as they became available and as it shipped the nonaluminum-clad fuel.

3.2.5.2.1 Option 4a - Dry Storage - The actions that the SRS would undertake under

this option, and the new facilities to be constructed, would be the same as for the Option 2a - Dry Storage under Alternative 2 (Decentralization) in Section 3.

2.3.2.1.

This option would require an extensive research and development program to carefully examine, characterize, and test the SRS aluminum-clad fuel for dry storage.

3.2.5.2.2 Option 4b - Wet Storage - The SRS would carry out the same actions and

construct the same types of facilities under this option as it would for Option 2b Alternative 2 (Decentralization) as described in Section 3.

2.3.2.2. Research and development activities

would also be similar to those conducted under this Decentralization alternative, except not perform studies on nonaluminum-clad fuels.

3.2.5.2.3 Option 4c - Processing and Storage - Under this option, the SRS would

process the existing aluminum-clad fuel as described for Option 2c - under Alternative 2 (Decentralization) and place the aluminum-clad fuel received from offsite into wet storage. The

requirements for new construction would be different than in Option 2c, in that dry storage would not be required because the nonaluminum-clad fuels would be shipped off site. The amount of aluminum-clad fuel to be received could be more readily stored in pools while developing new dry storage. Therefore, Option 4c would require DOE to construct a receiving, wet canning and wet storage facility to manage the fuel received after the operations are completed. These facilities would be much smaller than those required for the other alternatives.

3.2.5.3 SRS Options 4d, 4e, 4f, and 4g (Regionalization B). DOE analyzed the same

three options for the regionalization of spent fuel on the basis of geographic location alternatives: dry storage (Option 4d), wet storage (Option 4e), and processing of aluminum-clad fuel and storing the remaining fuel (Option 4f). In addition, it assumes shipping all SRS inventory offsite (Option 4g).

The amount of material that the SRS would manage if all the spent fuel in the EBR-II moved to the Site would total about 256.6 MTHM (282.9 tons). This would include the current inventory of about 206.3 MTHM (227.4 tons) as detailed in Section 3.2.2 plus:

- 19.9 MTHM (21.9 tons) of aluminum-clad fuel
- 26.7 MTHM (29.4 tons) of commercial nonaluminum-clad fuel

- 1.0 MTHM (1.1 ton) of stainless steel-clad fuel
- 1.3 MTHM (1.4 tons) of experimental Zircaloy-clad fuel
- 1.4 MTHM (1.5 tons) of other experimental fuel

The activities that DOE would have to undertake at the SRS, and the facilities to build, under the dry storage, wet storage, or processing options would be very similar required for the Decentralization alternative (Section 3.2.3). The difference would be the storage facilities would be somewhat greater because the amount of fuel to be managed [256.6 MTHM (282.9 tons) versus 219.9 MTHM (242.4 tons)]. In addition, DOE would conduct additional research and development on the other fuel types that SRS would use these options.

3.2.5.3.1 Option 4d - Dry Storage - The actions that the SRS would undertake under

this option, and the new facilities to be constructed, would be similar to those described in Option 2a - Dry Storage under Alternative 2 (Decentralization) in Section 3.

2.3.2.1. This option

would require an extensive research and development program into capabilities to evaluate and characterize, and can the SRS aluminum-clad fuel for dry storage.

3.2.5.3.2 Option 4e - Wet Storage - The SRS would carry out the same actions and

construct the same types of facilities under this option as it would for Option 2b Alternative 2 (Decentralization) as described in Section 3.

2.3.2.2. Research and development activities

would also be similar to those conducted under this Decentralization alternative.

3.2.5.3.3 Option 4f - Processing and Storage - Under this option, the SRS would

process the existing aluminum-clad fuel and place nonaluminum-clad fuel and aluminum received from offsite in dry storage as described for Option 2c - Processing with Alternative 2 (Decentralization).

The requirements for new facilities and for research and development would also be similar.

3.2.5.3.4 Option 4g - Shipment Off the Site - Under this option, the SRS would ship

its current inventory of about 206.

3 MTHM (227.4 tons) to the Oak Ridge Reservation. The activities and facilities required for this option are the same as those described below for Centralization alternative (Section 3.2.6.2.4).

3.2.6 Alternative 5 - Centralization

3.2.6.1 Overview. Under this alternative, DOE would collect all current and future spent

nuclear fuel inventories from DOE sites, the Navy, and other sources at a single location management until final disposition. DOE would construct new facilities at the center to accommodate the increased inventories. The originating sites would characterize and manage spent nuclear fuel before shipping. They would then close their spent fuel facilities and would include the centralization of activities related to the treatment of spent nuclear fuel research and development and pilot programs to support future decisions on its disposition.

3.2.6.2 SRS Options 5a, 5b, 5c, and 5d. DOE analyzed four options for this alternative.

Three deal with shipping all DOE spent nuclear fuel to the SRS for disposition and dry storage (Option 5a), wet storage (Option 5b), or by processing existing aluminum storing the remaining fuel (Option 5c). The fourth case involves the shipment of a Site to another location (Option 5d). Options 5a, 5b, and 5c concern the following

- 65.2 MTHM (71.7 tons) of naval fuel

- 213.1 MTHM (234.9 tons) of aluminum-clad fuel
- 2103.2 MTHM (2,318.4 tons) of Hanford defense fuel
- 27.6 MTHM (30.4 tons) of graphite fuel
- 156.5 MTHM (172.5 tons) of commercial nonaluminum-clad fuel
- 96.5 MTHM (106.4 tons) of experimental stainless steel-clad fuel
- 78.0 MTHM (86.0 tons) of Zircaloy-clad fuel
- 1.7 MTHM (1.9 tons) of other fuel types

DOE would manage a total of about 2,741.8 MTHM (3,022.3 tons) of spent nuclear SRS under the first three options. Options 5a and 5b would involve storing all the Option 5c would require processing the existing aluminum-clad fuel [184.4 MTHM (203 placing the remaining nonaluminum-clad SRS fuels and all fuel received from other 1 [2,557.4 MTHM (2,819.0 tons)] into dry storage. The SRS could accept shipments from sources and place them in storage as it built new facilities and transferred the on

Under Option 5d, shipments leaving the Site would amount to about 206.3 MTHM (2 which is equal to the inventory of spent nuclear fuel at the SRS under Alternative

3.2.6.2.1 Option 5a - Dry Storage - The actions that the SRS would undertake under

this option would be the same as those described for Option 2a - Dry Storage under (Decentralization) in Section 3.

2.3.2.1. However, the number and size of the new facilities needed to implement this centralization option would be much greater because of the larger volume of fuel the Site would manage. In addition, DOE would have to build a new Expanded Core Facility SRS to examine and characterize the naval fuels.

This option would require an extensive research and development program to examine, characterize, and can SRS and other fuel types before their placement in a DOE would also carry out research and development into other aspects of the management of spent fuels, including those related to its ultimate disposition.

3.2.6.2.2 Option 5b - Wet Storage - Under this option, DOE would undertake actions

similar to those described in Section 3.

2.3.2.2 for Option 2b - Wet Storage under Alternative 2. As with Option 5a (Dry Storage), the SRS would have to build major new facilities to manage the volume of fuel it would receive. DOE would also have to build a new Expanded Core Facility SRS. Research and development would be greatly expanded as well.

3.2.6.2.3 Option 5c - Processing and Storage - DOE would process the current

inventory of aluminum-clad spent fuel under this option in the same manner as described in the alternatives.

All other fuel onsite and all fuel received from elsewhere would be canned and placed in new dry storage facilities. The SRS would shut down the F- and H-Area separations processing the existing inventory of aluminum-clad fuel. Thereafter, any aluminum-clad fuel at the SRS would be placed in dry storage.

This option would require major new facilities, including a new Expanded Core Facility SRS. DOE would also conduct extensive research and development in spent fuel management.

3.2.6.2.4 Option 5d - Shipment Off the Site - DOE would consolidate and prepare

all spent nuclear fuel on the SRS for shipment to another DOE site; this would require the construction of a new fuel characterization facility.

Some fuels could require canning before shipment. SRS would use existing facilities to accomplish this. DOE would then close all SRS spent nuclear fuel facilities.

DOE would conduct research and development into methods of stabilizing, canning, and transporting aluminum-clad fuels, particularly that which is corroded or otherwise

3.3 Comparison of Alternatives

Table 3-3 summarizes the environmental consequences of the five alternatives. presents detailed descriptions of these consequences.

In general, the levels of impacts associated with Alternatives 1 through 4 would be approximately the same [e.g., about 206 to 257 MTHM (227 to 283 tons)] and would extend throughout the full 40-year management period. The lowest level of impact would occur under Option 4g or Option 5d (Regionalization or Centralization at another DOE would ship the SRS spent fuel off the Site well before the management period under Alternative 5, under which DOE would ship all spent nuclear fuel to the SRS, would have the greatest onsite impacts; the Site would have to manage approximately 2,741.8 MTHM (2,742 tons) of spent fuel.

Table 3-3. Comparison of impacts for the five alternatives.

ALTERNATIVE 1 - NO ACTION	
Option 1	
Wet Storage	
Land Use	No new facilities would be required.
Socioeconomics	No new operations jobs and only about 50 construction jobs would be created.
Cultural Resources	No new construction would be carried out. No impacts are anticipated.
Aesthetics and Scenic Resources	Facilities are in an existing industrial area not visible from public access roads or from off the Site. No impacts are anticipated. Emissions would not impact visibility.
Geology	No minerals of economic value are in affected area. No impacts are anticipated.
Air Resources	Emissions of criteria air pollutants and toxic air pollutants would be only a small fraction of air quality standards.
Water Resources	This option would not require use of additional surface water beyond the 75.7 billion liters (20 billion gallons) per year that the SRS withdraws at present.
	This option would not require withdrawals of additional groundwater beyond the 14.0 billion liters (3.7 billion gallons) per year the SRS uses. Activities related to this option currently use about 35.1 million liters (9.3 million gallons) of groundwater per year. Impacts would be minimal.
	No perennial streams or other surface waters would be affected.
	Accidental releases could contaminate shallow groundwater that is not a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.
Ecological Resources	Minor disturbance of wildlife due to traffic would occur.
	No wetlands or threatened or endangered species would be affected.
Noise	The only noise experienced by offsite populations would be generated by employee traffic and by truck and rail deliveries. There would be no change in traffic noise impacts.
Traffic and Transportation	This option would not increase site traffic.
	Number of LCFf, normal transport:
	Worker: 6.0×10^{-4}
	Public: 7.0×10^{-5}
Occupational and	Maximum LCFf probabilities:

Public Health and Safety (Radiological) Worker: 4×10^{-5}
 Offsite population: 4×10^{-14} (air)
 1×10^{-14} (water)

Annual LCFf incidences:
 Worker: 8×10^{-5}
 Offsite population: 2×10^{-9}

Table 3-3. (continued).

	Option 1 Wet Storage
Occupational and Public Health and Safety (Nonradiological) Utilities and Energy	Hazard index: Worker: 2×10^{-6} Maximally exposed individual: 2×10^{-7} Minimal changes in demand for electricity, steam, domestic water and wastewater treatment would occur. Current SRS capacities are adequate for these additions. Impacts would be minimal.
Materials and Waste Management	Annual average volume of waste generated (cubic meters)b: LLW: 400 TRU: 17 HLW: 0.4
Accidentsc	No impact on site waste management capacities. Greatest point estimate of riskd: Worker: Data not calculatede Colocated worker: 7.7×10^{-7} Maximally exposed individual: 1.6×10^{-7} Offsite population: 1.4×10^{-3}
a.	Not applicable.
b.	LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.
c.	Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.
d.	Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.
e.	The safety analysis reports from which information was extracted written before issuance of DOE Order 5480.23; previous orders di require the inclusion of workers.
f.	LCF = latent cancer fatalities.

Table 3-3. (continued).

	ALTERNATIVE 2 - DECENTRALIZATION		
	Option 2a	Option 2b	Option 2c
Land Use	Dry Storage Most new construction would be in parts of F- and H-Areas already dedicated to industrial use. Impacts would be minimal.	Wet Storage Same as Option 2a.	Processing Same as Option 2a.
Socioeconomic s	Operations jobs would be filled by current employees. A maximum of about 600 construction jobs would be	Same as Option 2a.	Operations jobs would be filled by current employees. A maximum of about 550 construction jobs would be

	created.		created.
Cultural Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Aesthetics and Scenic Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Geology	Same as Option 1.	Same as Option 1.	Same as Option 1.
Air Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Water Resources	New withdrawals of approximately 6.1 million liters (1.6 million gallons) per year of cooling water from Savannah River would be required. Impacts would be minimal.	New withdrawals of approximately 7.2 million liters (1.9 million gallons) per year of cooling water from Savannah River would be required. Impacts would be minimal.	New withdrawals of approximately 311 million liters (82.2 million gallons) per year of cooling water from Savannah River would be required. Impacts would be minimal.
	Additional groundwater withdrawals would total about 48.7 million liters (12.9 million gallons) per year. Impacts would be minimal.	Additional groundwater withdrawals would total about 50.6 million liters (13.4 million gallons) per year. Impacts would be minimal.	Same as Option 2a.
	No perennial streams or other surface waters would be affected.	No perennial streams or other surface waters would be affected.	No perennial streams or other surface waters would be affected.
	Accidental releases could contaminate shallow groundwater that is not used as a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.	Accidental releases could contaminate shallow groundwater that is not used as a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.	Accidental releases could contaminate shallow groundwater that is not used as a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.
Table 3-3. (continued).			
	Option 2a	Option 2b	Option 2c
	Dry Storage	Wet Storage	Processing
Ecological Resources	Small increase in traffic would cause slight increase in road kills and in disturbance of wildlife due to noise. Impacts would be minimal.	Same as Option 2a.	Small increases in traffic would cause small increase in road kills and in disturbance of wildlife due to noise. Impacts would be minimal.
	No wetlands or threatened or endangered species would be affected.	Same as Option 2a.	Same as Option 2a.
Noise	Only noise experienced by communities would be	Same as Option 2a.	Same as Option 2a.

	generated by employee traffic and by truck and rail deliveries.		
	Changes in traffic levels are expected to result in only very small changes in noise impacts.		
Traffic and Transportation	This option would increase site traffic slightly.	Same as Option 2a.	This option would increase site traffic slightly.
	Number of LCFg, normal transport: Worker: 1.0×10^{-3} Public: 1.2×10^{-4}		Number of LCFg, normal transport: Worker: 2.1×10^{-4} Public: 1.9×10^{-5}
Occupational and Public Health and Safety (Radiological)	Maximum LCFg probabilities: Worker: 3×10^{-5} Offsite population: 4×10^{-14} (air) 1×10^{-14} (water)	Maximum LCFg probabilities: Worker: 4×10^{-5} Offsite population: 5×10^{-14} (air) 2×10^{-14} (water)	Maximum LCFg probabilities: Worker: 6×10^{-5} Offsite population: 2×10^{-7} (air) 6×10^{-8} (water)
	Annual LCFg incidences: Worker: 7×10^{-5} Offsite population: 2×10^{-9}	Annual LCFg incidences: Worker: 8×10^{-5} Offsite population: 2×10^{-9}	Annual LCFg incidences: Worker: 3×10^{-2} Offsite population: 8×10^{-3}
Occupational and Public Health and Safety (Nonradiological)	Same as Option 1.	Same as Option 1.	Hazard index: Worker: 6×10^{-3} Maximally exposed individual: 5×10^{-4}
Utilities and Energy	Requirements would increase 3 to 7 percent above present levels. Current SRS capacities are adequate for these increases.	Same as Option 2a.	Very similar to Option 2a.
Materials and Waste Management	Annual average volume of waste generated (cubic meters)b: LLW: 400 TRU: 18 HLW: 0.4	Same as Option 2a.	Annual average volume of waste generated (cubic meters)b: LLW: 800 TRU: 19 HLW: 2.3c
	No impact on site capacities.		No impact on site capacities.
Table 3-3.	(continued).		
	Option 2a	Option 2b	Option 2c
	Dry Storage	Wet Storage	Processing
Accidentsd	Greatest point estimate of risk: Worker: Data not calculatedf Colocated worker: 1.6×10^{-6}	Greatest point estimate of risk: Worker: Data not calculatedf Colocated worker: 1.7×10^{-6}	Greatest point estimate of risk: Worker: Data not calculatedf Colocated worker: 7.7×10^{-7}

Maximally exposed individual: 3.3 x 10 ⁻⁷ Offsite population: 2.8 x 10 ⁻³	Maximally exposed individual: 3.5 x 10 ⁻⁷ Offsite population: 3.0 x 10 ⁻³	Maximally exposed individual: 1.6 x 10 ⁻⁷ Offsite population: 1.4 x 10 ⁻³
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- a. NA = not applicable.
- b. LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.
- c. High-level waste will be generated only during approximately the first 10 years.
- d. Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.
- e. Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.
- f. The safety analysis reports from which information was extracted were written before issuance of DOE Order 5480.23; previous orders require the inclusion of workers.
- g. LCF = latent cancer fatalities.

Table 3-3. (continued).

ALTERNATIVE 3 - 1992/1993 PLANNING BASIS			
	Option 3a Dry Storage	Option 3b Wet Storage	Option 3c Processing
Land Use	Same as Option 2a.	Same as Option 2a.	Same as Option 2a.
Socioeconomics	Same as Option 2a.	Operations jobs would be filled by current employees. A maximum of about 650 construction jobs would be created.	Same as Option 2c.
Cultural Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Aesthetics and Scenic Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Geology	Same as Option 1.	Same as Option 1.	Same as Option 1.
Air Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Water Resources	Same as Option 2a.	Same as Option 2b.	Same as Option 2c.
Ecological Resources	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Noise	Same as Option 2a.	Same as Option 2a.	Same as Option 2a.
Traffic and Transportation	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Occupational and Public Health and Safety (Radiological)	Same as Option 2a.	Same as Option 2b.	Same as Option 2c.
Occupational and Public Health and Safety (Nonradiological)	Same as Option 1.	Same as Option 1.	Same as Option 2c.
Utilities and Energy	Same as Option 2a.	Same as Option 2a.	Very similar to Option 2a.

Materials and Waste Management	Same as Option 2a.	Same as Option 2a.	Annual average volume of waste generated (cubic meters)a: LLW: 750 TRU: 19 HLW: 1.7b
Accidentsc	Greatest point estimate of riskd: Worker: Data not calculatede Colocated worker: 1.9×10^{-6} Maximally exposed individual: 4.0×10^{-7} Offsite population: 3.4×10^{-3}	Same as Option 3a.	No impact on site capacities. Greatest point estimate of riskd: Worker: Data not calculatede Colocated worker: 1.1×10^{-6} Maximally exposed individual: 2.3×10^{-7} Offsite population: 2.0×10^{-3}

- a. LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.
- b. High-level waste will be generated only during approximately the first 10 years.
- c. Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.
- d. Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.
- e. The safety analysis reports from which information was extracted written before issuance of DOE Order 5480.23; previous orders do require the inclusion of workers.

Table 3-3. (continued).

ALTERNATIVE 4 - REGIONALIZATION A (By Fuel Type)			
	Option 4a	Option 4b	Option 4c
	Dry Storage	Wet Storage	Processing
Land Use	Same as Option 2a.	Same as Option 2a.	Same as Option 2a.
Socioeconomics	Same as Option 3b.	Same as Option 3b.	Same as Option 2c.
Cultural Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Aesthetics and Scenic Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Geology	Same as Option 1.	Same as Option 1.	Same as Option 1.
Air Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Water Resources	Same as Option 2a.	Same as Option 2b.	Very similar to Option 2c.
Ecological Resources	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Noise	Same as Option 2a.	Same as Option 2a.	Same as Option 2a.
Traffic and Transportation	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Occupational and Public Health and Safety	Same as Option 2a.	Same as Option 2b.	Maximum LCFa probabilities: Same as Option 2c. Annual LCFa

(Radiologic
al)

incidences:

Worker: 3×10^{-2}

Offsite

population: 9×10^{-3}

Same as Option 2c.

Occupational and Public Health and Safety (Nonradiological)	Same as Option 1.	Same as Option 1.
Utilities and Energy	Very similar to Option 2a.	Same as Option 2a.
Materials and Waste Management	Same as Option 1.	Same as Option 1.

Very similar to Option 2a.

Annual average volume of waste generated (cubic meters)b:

LLW: 790

TRU: 18

HLW: 2.3c

No impact on site capacities.

Table 3-3. (continued).

	Option 4a Dry Storage	Option 4b Wet Storage	Option 4c Processing
Accidentsd	Greatest point estimate of risk: Worker: Data not calculatedf Colocated worker: 2.1×10^{-6} Maximally exposed individual: 4.4×10^{-7} Offsite population: 3.7×10^{-3}	Same as Option 3a.	Greatest point estimate of risk: Worker: Data not calculatedf Colocated worker: 1.3×10^{-6} Maximally exposed individual: 2.8×10^{-7} Offsite population: 2.4×10^{-3}

a. LCF = latent cancer fatalities.

b. LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.

c. High-level waste will be generated only during approximately the first 10 years.

d. Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.

e. Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.

f. The safety analysis reports from which information was extracted were written before issuance of DOE Order 5480.23; previous orders require the inclusion of workers.

Table 3-3. (continued).

	ALTERNATIVE 4 - REGIONALIZATION B (By Location)a		
	Option 4d Dry Storage	Option 4e Wet Storage	Option 4f Processing
Land Use	Same as Option 2a.	Same as Option 2a.	Same as Option 2a.
Socioeconomics	Operations jobs would be filled by current employees.	Operations jobs would be filled by current employees.	Same as Option 3b.
	A maximum of about 700 construction jobs would be	A maximum of about 800 construction jobs would be	

Cultural Resources	created. Same as Option 1.	created. Same as Option 1.	Same as Option 1.
Aesthetics and Scenic Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Geology	Same as Option 1.	Same as Option 1.	Same as Option 1.
Air Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Water Resources	Same as Option 2a.	Same as Option 2b.	Very similar to Option 2c.
Ecological Resources	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Traffic and Transportation	Same as Option 2a.	Same as Option 2a.	Same as Option 2c.
Occupational and Public Health and Safety (Radiological)	Maximum LCFe probabilities: Worker: 4×10^{-5} Offsite population: 5×10^{-14} (air) 2×10^{-14} (water) Annual LCFe incidences: Worker: 8×10^{-5} Offsite population: 2×10^{-9} Hazard index: Worker: 2×10^{-6} Maximally exposed individual: 3×10^{-7}	Maximum LCFe probabilities: Worker: 5×10^{-5} Offsite population: 6×10^{-14} (air) 2×10^{-14} (water) Annual LCFe incidences: Worker: 1×10^{-4} Offsite population: 2×10^{-9} Same as Option 4d.	Maximum LCFe probabilities: Worker: 7×10^{-5} Offsite population: 2×10^{-7} (air) 6×10^{-8} (water) Annual LCFe incidences: Worker: 3×10^{-2} Offsite population: 9×10^{-3} Hazard index: Worker: 8×10^{-3} Maximally exposed individual: 6×10^{-4}
Occupational and Public Health and Safety (Nonradiological)	Same as Option 2a.	Very similar to Option 2a.	Very similar to Option 2a.
Utilities and Energy Materials and Waste Management	Same as Option 1.	Same as Option 1.	Same as Option 4c.
Table 3-3.	(continued). Option 4d Dry Storage	Option 4e Wet Storage	Option 4f Processing
Accidentsb	Greatest point estimate of riskc: Worker: Data not calculatedd Colocated worker: 2.0×10^{-6} Maximally exposed individual: 4.1×10^{-7} Offsite population: 3.5×10^{-3}	Same as Option 4d	Greatest point estimate of riskc: Worker: Data not calculatedd Colocated worker: 1.2×10^{-6} Maximally exposed individual: 2.5×10^{-7} Offsite population: 2.1×10^{-3}
a.	Impacts for Option 4g, Ship Offsite, would be the same as for Option 5d as described in the last entry in this table.		
b.	Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.		
c.	Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.		
d.	The safety analysis reports from which information was extracted we		

written before issuance of DOE Order 5480.23; previous orders did not require the inclusion of workers.
e. LCF = latent cancer fatalities.

Table 3-3. (continued).

ALTERNATIVE 5 - CENTRALIZATION			
	Option 5a	Option 5b	Option 5c
Land Use	Dry Storage Most new construction would be in parts of F- and H-Areas already dedicated to industrial use. Additional maximum of 0.4 square kilometer (100 acres) would be converted from pine plantation to industrial use. Impacts would be minimal.	Wet Storage Same as Option 5a.	Processing Same as Option 5a.
Socioeconomics	Operations jobs would be filled by present employees. A maximum of about 2,550 construction jobs would be created.	Operations jobs would be filled by present employees. A maximum of about 2,700 construction jobs would be created.	Operations jobs would be filled by present employees. A maximum of about 2,550 construction jobs would be created.
Cultural Resources	No known historical, archeological, or paleontological resources are in areas to be affected. All areas are classified as having low or moderate probability of containing archeological site. Impact is unlikely.	Same as Option 5a.	Same as Option 5a.
Aesthetics and Scenic Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Geology	Same as Option 1.	Same as Option 1.	Same as Option 1.
Air Resources	Same as Option 1.	Same as Option 1.	Same as Option 1.
Water Resources	Same as Option 2a.	Same as Option 2b.	Same as Option 2c.
	Additional groundwater withdrawals would total about 67.7 million liters (17.9 million gallons) per year. Impacts would be minimal.	Additional groundwater withdrawals would total about 69.6 million liters (18.4 million gallons) per year. Impacts would be minimal.	Same as Option 5a.
	No perennial streams or other surface waters would be affected.	Same as Option 5a.	Accidental releases could contaminate shallow groundwater that is not used as

	Accidental releases could contaminate shallow groundwater that is not used as a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.	Accidental releases could contaminate shallow groundwater that is not used as a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.	a source for drinking water or domestic use. Releases would not affect surface streams or drinking water aquifers.
Table 3-3.	(continued).		
	Option 5a Dry Storage	Option 5b Wet Storage	Option 5c Processing
Ecological Resources	Same as Option 2a, plus	Same as Option 5a.	Same as Option 5a, plus
	Loss of up to 0.4 square kilometer (100 acres) of loblolly pine. Impacts would be minor.		Increased disturbance due to more worker traffic. Impacts would be minor.
Noise Traffic and Transportation	Same as Option 2a. Same as Option 2a.	Same as Option 2a. This option would increase site traffic by about 17 percent. Impacts would be small.	Same as Option 2a. Same as Option 2c.
		Number of LCFsg would be same as for Option 2b for normal transport.	
Occupational and Public Health and Safety (Radiological)	Maximum LCFg probabilities: Worker: 4×10^{-4} Offsite population: 5×10^{-13} (air) 2×10^{-13} (water)	Maximum LCFg probabilities: Worker: 5×10^{-4} Offsite population: 6×10^{-13} (air) 2×10^{-13} (water)	Maximum LCFg probabilities: Worker: 6×10^{-4} Offsite population: 2×10^{-7} (air) 6×10^{-8} (water)
	Annual LCFg incidences: Worker: 9×10^{-4} Offsite population: 2×10^{-8} Same as Option 1.	Annual LCFg incidences: Worker: 1×10^{-3} Offsite population: 3×10^{-8} Same as Option 1.	Annual LCFg incidences: Worker: 3×10^{-2} Offsite population: 9×10^{-3} Same as Option 2c.
Occupational and Public Health and Safety (Nonradiological)			
Utilities and Energy	Similar to Option 2a.	Similar to Option 2a.	Requirements for electricity would increase by about 17 percent. Other increases would be similar to Option 2c. Impacts would be minor.
Materials and Waste Management	Annual average volume of waste generated (cubic	Annual average volume of waste generated (cubic	Annual average volume of waste generated (cubic

	meters)b:	meters)b:	meters)b:
	LLW: 400	LLW: 400	LLW: 800
	TRU: 16	TRU: 20	TRU: 20
	HLW: 0	HLW: 2.3c	HLW: 2.3c
	No impact on site capacities.	No impact on site capacities.	No impact on site capacities.
Table 3-3.	(continued).		
	Option 5a	Option 5b	Option 5c
	Dry Storage	Wet Storage	Processing
Accidentsd	Greatest point estimate of risk:	Same as Option 5a.	Greatest point estimate of risk:
	Worker: Data not calculatedf		Worker: Data not calculatedf
	Colocated worker: 4.0 x 10 ⁻⁶		Colocated worker: 3.3 x 10 ⁻⁶
	Maximally exposed individual: 8.4 x 10 ⁻⁷		Maximally exposed individual: 6.8 x 10 ⁻⁷
	Offsite population: 7.2 x 10 ⁻³		Offsite population: 5.8 x 10 ⁻³
a.	NA = not applicable.		
b.	LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.		
c.	High-level waste will be generated only during approximately the first 10 years.		
d.	Data is provided as adjusted point estimates of risk by receptor gr to demonstrate a relative comparison of each alternative on an opti by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.		
e.	Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.		
f.	The safety analysis reports from which information was extrac written before issuance of DOE Order 5480.23; previous orders require the inclusion of workers.		
g.	LCF = latent cancer fatalities.		

Table 3-3. (continued).

	ALTERNATIVE 5 - CENTRALIZATION
	ALTERNATIVE 4 - REGIONALIZATION B
	Option 4g and Option 5db
	Ship Out
Land Use	Same as Option 1.
Socioeconomics	No new operations jobs and only about 200 constru jobs would be created.
Cultural Resources	Same as Option 1.
Aesthetics and Scenic Resources	Same as Option 1.
Geology	Same as Option 1.
Air Resources	Same as Option 1.
Water Resources	This option would require new withdrawals of approximately 3.0 million liters (790 thousand ga per year of cooling water from the Savannah River Impacts would be minimal.
	It also would require additional groundwater with of about 38.1 million liters (10.1 million gallon year. Impacts would be minimal.
	Impacts to surface water and groundwater would be similar to those from Option 1.
Ecological Resources	Same as Option 1.

Noise	Same as Option 2a.
Traffic and	NAA
Transportation	
Occupational and	Less than Option 1.
Public Health and	
Safety	
(Radiological)	
Occupational and	Same as Option 1.
Public Health and	
Safety	
(Nonradiological)	
Utilities and	Requirements would increase 2 to 6 percent above
Energy	levels during first 10 years. Current SRS capaci
	are adequate for these increases.
Materials and Waste	Annual average volume of waste generated initial
Management	years only (cubic meters)c:
	LLW: 400
	TRU: 18
	HLW: 0

Table 3-3. (continued).

	Option 4g and Option 5db
	Ship Out
Accidentsd	Greatest point estimate of risk:
	Worker: Data not calculatedf
	Colocated Worker:
	Option 4g: 8.1×10^{-7}
	Option 5d: 8.2×10^{-7}
	Maximally exposed individual:
	Option 4g: 1.7×10^{-7}
	Option 5d: 1.7×10^{-7}
	Offsite population:
	Option 4g: 1.4×10^{-3}
	Option 5d: 1.4×10^{-3}

- a. NA = not applicable.
- b. Impacts for Option 4g (Regionalization-B) are the same as for Option 5d.
- c. LLW = low-level waste; TRU = transuranic waste; HLW = high-level waste.
- d. Data is provided as adjusted point estimates of risk by receptor group to demonstrate a relative comparison of each alternative on an option-by-option basis. The adjusted values were taken from Tables 5-27 through 5-29.
- e. Units for adjusted point estimates of risk are given in terms of potential fatal cancers per year.
- f. The safety analysis reports from which information was extracted were written before issuance of DOE Order 5480.23; previous orders did not require the inclusion of workers.

4. AFFECTED ENVIRONMENT

4.1 Overview

This section describes the existing environment at the Savannah River Site (SRS) areas. Its purpose is to support the assessment of environmental consequences of actions regarding spent nuclear fuels described in Chapter 3. Chapter 5 describes consequences in detail.

4.2 Land Use

The SRS occupies an area of approximately 198,000 acres (800 square kilometers) South Carolina, in a generally rural area about 25 miles (40 kilometers) southeast of Aiken, which is bordered by the Savannah River to the southwest, includes portions of Barnwell, and Allendale Counties (Figure 2-1).

Land use on the SRS falls into three major categories: forest/undeveloped, water, and developed facilities. About 181,500 acres (735 square kilometers) of the SRS area (USDA 1991a). Approximately 90 percent of this undeveloped area is forested (Cummins 1952). In 1952, an interagency agreement between the U.S. Department of Energy [DOE, which includes the Atomic Energy Commission (AEC)] and the Forest Service, U.S. Department of Agriculture, established an SRS forest management program. In 1972, the AEC designated the SRS as a National Environmental Research Park (NERP); at present, approximately 14,000 acres (57 square kilometers, or 7 percent) of the SRS area are designated as "Set-Asides," areas specifically protected for environmental research activities that are coordinated either through the University of Georgia Savannah River Ecology Laboratory (SREL) or the Savannah River Technology Center (SRTC) (SRTC 1994). Administrative, production, and support facilities occupy approximately 5 percent of the SRS land area.

DOE is considering decisions that could affect the long-range land use of the SRS. Programmatic decisions on the reconfiguration of the nuclear weapons complex, spent nuclear fuel management strategies, and waste management and environmental restoration activities that are significant changes in the SRS mission are in the early stages of discussion. In the past, however, a Land Use Technical Committee consisting of representatives from DOE, Westinghouse Savannah River Company, and various stakeholder groups is evaluating alternative land uses and potential future uses. These activities are consistent with the guidelines for land use contained in DOE Order 4320.1B, "Site Development Planning," and in the Resource Conservation and Recovery Act (RCRA) and the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA).

Land use bordering SRS is primarily forest and agricultural. There is also a small area of open water and nonforested wetlands along the Savannah River valley. Incorporated areas are the only other significant use of land in the vicinity (Figure 4-1). None of the land in which the SRS is located has been zoned for any of the Site land. The only adjacent area is the Town of New Ellenton, which has two zoning categories for lands that border SRS development and residential development. The closest residences to the SRS boundary are within 200 feet (61 meters) of the Site perimeter to the west, north, and northeast.

Various industrial, manufacturing, medical, and farming operations are conducted surrounding the Site. Major industrial and manufacturing facilities in the area include plants producing polystyrene foam and paper products, chemical processing plants, a nuclear power plant. Farming is diversified in the region and includes crops such as watermelon, cotton, soybeans, corn, and small grains.

There is a wide variety of public outdoor recreation facilities in the SRS region. Federal outdoor recreation facilities include portions of the Sumter National Forest (75 kilometers) to the northwest of the Site, the Santee National Wildlife Refuge (80 kilometers) to the east, and the Clarks Hill/Strom Thurmond Reservoir, a U.S. Army Corps of Engineers impoundment (43 miles (70 kilometers) to the northwest). There are also county, and local parks in the region, most notably Redcliffe Plantation, Rivers Branch, Aiken County State Parks in South Carolina, and Mistletoe State Park in Georgia (HNF 1994).

The SRS is a controlled area with public access limited to through traffic on S Highway 125 (SRS Road A), U.S. Highway 278, SRS Road 1, and the CSX railway. The SRS does not contain any public recreation facilities. However, the SRS conducts controlled burns from mid-October through mid-December; hunters can also kill feral hogs during this time. Figure 4-1. Generalized land use at the Savannah River Site and vicinity. Figure 4-1 shows animal-vehicle accidents on SRS roads.

No on-site areas are subject to Native American treaty rights. The SRS does not include any prime farmland.

4.3 Socioeconomics

This section discusses baseline socioeconomic conditions within a region of approximately 90 percent of the SRS workforce lived in 1992. The SRS region of interest includes Aiken, Allendale, Bamberg, and Barnwell Counties in South Carolina, and Columbia and Wilkes Counties in Georgia (Figure 4-2).

4.3.1 Employment and Labor Force

The labor force living in the region of influence increased from about 150,550 between 1980 and 1990. In 1990, approximately 75 percent of the total labor force influence lived in Richmond and Aiken Counties. Assuming a constant unemployment rate, the regional labor force is likely to increase to approximately 257,000 by 1995.

Between 1980 and 1990, total employment in the region of influence increased from 199,161, an average annual growth rate of approximately 5 percent. Table 4-1 lists employment data for the six-county region of influence. As shown, by 1995 employment should increase 22 percent to approximately 242,000. The unemployment rates for 1990 were 7.3 percent and 4.7 percent, respectively (HNUS 1992a).

In 1990, employment at the SRS was 20,230 (DOE 1993a), representing 10 percent employment in the region of influence. In Fiscal Year 1992, employment at the SRS was approximately 15 percent to 23,351, with an associated payroll of more than \$1.1 billion. Planned budget reductions, Site employment could decline by as many as 4,200 jobs. As shown in Table 4-1, this would reduce Site employment to approximately 15,800 by 1995. **Table 4-1.** Forecast employment and population data for the Savannah River Site and influence.

Year	Labor Force (Region)	Employment (Region)	SRS Employment ^b	Population (Region)
1994	254,549	239,785	21,500	456,892
1995	256,935	242,033	20,000	461,705
1996	258,500	243,507	15,800	465,563
1997	260,680	245,561	15,800	468,665
1998	263,121	247,860	15,800	471,176
1999	265,694	250,284	15,800	473,186
2000	268,430	252,861	15,800	474,820
2001	271,265	255,532	15,800	476,179
2002	274,238	258,332	15,800	477,332
2003	277,318	261,234	15,800	478,340
2004	280,415	264,151	15,800	479,182

a. Source: HNUS (1993).

b. Sources: Turner (1994), Fiori (1995).

4.3.2 Personal Income

Personal income in the six-county region has doubled during the past two decades approximately \$3.4 billion in 1970 to almost \$6.9 billion by 1989 (in constant 1991 dollars). Together, Richmond and Aiken Counties accounted for 75.4 percent of the personal income in the region of influence in 1989, because these two counties provide most of the employment in the region. Personal income in the region is likely to increase 3 percent to approximately \$7.1 billion by 1995 and to almost \$8.2 billion by 2000 (HNUS 1992a).

4.3.3 Population

Between 1980 and 1990, the population in the region of influence increased 13 percent from 376,058 to 425,607. More than 88 percent of the 1990 population lived in Aiken (28 percent), Columbia (15.5 percent), and Richmond (44.6 percent) Counties. Table 4-1 also lists the region of influence forecast to 2004. According to census data, in 1990 the number of persons per household in the six-county region was 2.72, and the median age of the population was 31.2 years (HNUS 1992a).

4.3.4 Housing

From 1980 to 1990, the number of year-round housing units in the six-county region increased 23.2 percent from 135,866 to 167,356. In 1990, approximately 68 percent of the total were single-family units, 18 percent were multifamily units, and 14 percent were mobile homes. In the same year, the region had a 4.7-percent vacancy rate with 7,818 available unoccupied units. Of the available unoccupied units, 29 percent (2,267) were available for sale.

(5,551) were available for rent (HNUS 1992a).

4.3.5 Community Infrastructure and Services

Public education facilities in the six-county region include 95 elementary and schools and 25 high schools. Aside from the public school systems, 42 private secondary facilities are available to residents in the region (HNUS 1992a).

Based on a combined average daily attendance for elementary and high school students in the region of influence in 1988, the average number of students per teacher was 16. This ratio occurred in Barnwell County's District 29 high school, which had only 12 students (1988-1989) (HNUS 1992a).

The six-county region has 14 major public sewage treatment facilities with a combined capacity of 302.2 million liters (79.8 million gallons) per day. In 1989, these facilities operated at approximately 56 percent of capacity, with an average daily flow of 170 million gallons per day. Capacity utilization ranged from 45 percent in Aiken County to 84 percent in Barnwell County (HNUS 1992a).

There are approximately 120 public water systems in the region of influence. A county and municipal systems are major facilities, while the remainder serve individual water districts, trailer parks, and miscellaneous facilities. In 1989, the 40 major combined total capacity of 576.3 million liters (152.2 million gallons) per day. With a flow rate of approximately 268.8 million liters (71 million gallons) per day, these facilities were operating at 47 percent of total capacity in 1989. Facility utilization rates ranged from 34 percent in Allendale County to 84 percent in the City of Aiken (HNUS 1992a).

Eight general hospitals operate in the six-county region with a combined bed capacity of 2,433 (5.7 beds per 1,000 population). Four of the eight general hospitals are in Aiken, Allendale, Bamberg, and Barnwell Counties each have one general hospital. Columbia County has no hospital. In 1989, there were approximately 1,295 physicians serving the region, which represents a physician-to-population ratio of 3 to 1,000. This ratio ranged from 1.4 per 1,000 people in Aiken and Allendale Counties to 5.4 physicians per 1,000 people in Barnwell County (HNUS 1992a).

Fifty-six fire departments provide fire protection services in the region of influence. Seven of these are classified as municipal fire departments, but many provide protection outside municipal limits. The average number of firefighters in the region in 1988 was 1.6 per 1,000 people, ranging from 1.6 per 1,000 in Richmond County to 10.2 per 1,000 in Barnwell County (HNUS 1992a).

The county sheriff departments and municipal police departments provide most law enforcement services in the region of influence. In addition, state law enforcement agents are assigned to each county provide protection and assist county and municipal law enforcement. In 1988, the average ratio in the region of full-time police officers employed by local agencies per 1,000 population was 2.0. This ratio ranged from 1.4 per 1,000 in Aiken County to 2.5 per 1,000 in Richmond County (HNUS 1992a).

4.3.6 Government Fiscal Structure

This section discusses the fiscal structure of Aiken and Barnwell Counties because these counties would have the greatest potential for fiscal impacts from changes at SRS.

Public services provided by Aiken County are funded principally through the county general fund. In Fiscal Year 1988, revenues and expenditures of this fund were \$15.5 million and \$18 million, respectively. The current property tax rate is 55.8 mills for county general services and 8.0 mills for debt service. Long-term general obligation bond indebtedness was \$9.5 million at the end of Fiscal Year 1988, and reserve general obligation bond indebtedness was \$5.5 million. The assessed value of property in the county was \$182.5 million in Fiscal Year 1988 (HNUS 1992a).

Assuming revenues and expenditures increase in proportion to projected growth in employment and population, estimated revenues and expenditures for Aiken County over the period from Fiscal Year 1990 to Fiscal Year 2000 will be \$15.6 million to \$17.0 million (in dollars) (HNUS 1992a).

Public services provided by Barnwell County also are funded principally through the county general fund. In Fiscal Year 1988, revenues and expenditures of this fund were \$4.9 million and \$4.9 million, respectively. The property tax rate is 23.9 mills of assessed value. In Fiscal Year 1990 revenues were approximately \$4.5 million (HNUS 1992a).

4.4 Cultural Resources

4.4.1 Archeological Sites and Historic Structures

Field studies conducted under an ongoing program over the past two decades by the Carolina Institute of Archeology of the University of South Carolina, under contract consultation with the South Carolina State Historic Preservation Officer, have provided information about the distribution and content of archeological and historic resources. By the end of Fiscal Year 1992, approximately 60 percent of the Site had been examined. Archeological (historic and prehistoric) sites had been identified; these include 7350 historic components, some of which are mixed (i.e., contain elements of both). 53 have been determined to be eligible for the National Register of Historic Places. 21 of the 53 (40 percent) are historic sites, such as buildings, which are standing structures. These sites provide knowledge of the area's history. The remainder are primarily prehistoric sites and some are mixed (historic and prehistoric). Production facilities have been nominated for eligibility to the National Register for Historic Places, but no plans for such a nomination at this time (Brooks 1993; Brooks 1994). The existing production facilities are not likely to be eligible for the National Register, either because they lack architectural integrity, might not represent a particular architectural style, or do not fit the broad historic theme of the Manhattan Project and initial nuclear materials (DOE 1993a).

Archeologists have divided areas of the SRS into three sensitivity zones related to containing sites with multiple archeological components or dense or diverse artifact potential for eligibility to the National Register of Historic Places (SRARP 1989).

- Zone 1 is the zone of the highest archeological site density with a high probability of encountering large archeological sites with dense and diverse artifacts, and a high potential for nomination to the National Register of Historic Places.
- Zone 2 covers areas of moderate archeological site density that should contain a similar composition. Activities in this zone have a moderate probability of encountering archeological sites, but a low probability of encountering large sites with prehistoric components. All areas within the zone are conducive to site preservation. The zone has moderate potential for encountering sites that would be eligible for nomination to the National Register of Historic Places.
- Zone 3 covers areas of low archeological site density. Activities in this zone have a low probability of encountering archeological sites and virtually no chance of encountering sites with more than three prehistoric components; potential for site preservation is low. Some exceptions to this definition have been discovered in Zone 3, so some areas within the zone could be considered eligible for nomination to the National Register of Historic Places.

4.4.2 Native American Cultural Resources

In conjunction with 1991 studies related to a proposed New Production Reactor, an investigation of Native American concerns over religious rights in the Central Savannah River Area. During this study three Native American groups - the Yuchi Tribal Organization, the Council of Muskogee Creek, and the Indian People's Muskogee Tribal Town Confederacy - expressed concerns over sites and items of religious significance on the SRS. DOE has included these groups on its environmental mailing list and sends them documents about SRS activities (NUS 1991a).

Native American resources in the region include villages or townsites, ceremonial sites, cemeteries, and areas containing traditional plants for certain rituals. Villages contain a variety of sensitive features associated with different ceremonies and rituals. The Muskogee Creek tribes have expressed concerns that the area might contain several prehistoric sites used in tribal ceremonies (DOE 1993a).

4.4.3 Paleontological Resources

Invertebrate fossil remains occur within the McBean, Barnwell, and Congaree formations of the Eocene Age (54 million to 39 million years ago) on the SRS. Relatively large quantities of invertebrate fossils have been recorded for the McBean and Barnwell Formations. Re-

of fossil localities is difficult because the South Carolina Geological Survey has for, or registry of, important paleontological locations (DOE 1991b).

4.5 Aesthetics and Scenic Resources

The dominant aesthetic setting in the vicinity of the SRS consists mainly of a forest, with some limited residential and industrial areas. Because of the distance, the rolling terrain, normally hazy atmospheric conditions, and heavy vegetation, the SRS is generally visible from off the Site. The few locations that have views of some of the SRS are quite distant from the facility [5 miles (8 kilometers) or more].

SRS land is heavily wooded, and developed areas occupy only approximately 5 per cent of the total land area. The facilities are scattered across the SRS and are brightly lit. Reactors and principal processing facilities are large concrete structures as much as 30 meters high and usually collocated with lower administrative and support buildings. The facilities are visible in the direct line-of-sight when approaching them from the roads. A 500-foot cooling tower is located in K-Area. Otherwise, the heavily wooded area around the SRS road system and public highways that cross the Site limit views of the facilities.

4.6 Geology

The SRS is on the Upper Atlantic Coastal Plain of South Carolina, which consists of 366 meters (700 to 1,200 feet) of sands, clays, and limestones of Tertiary and Cretaceous sediments are underlain by sandstones of Triassic age and older metamorphic and igneous (Arnett et al. 1993). There are no known capable faults on the SRS or volcanic activity within 800 kilometers (500 miles) of the Site.

4.6.1 General Geology

The SRS is in the Coastal Plain physiographic province of western South Carolina approximately 32 kilometers (20 miles) southeast of the Fall Line, which separates the Coastal Plain provinces (Figure 4-3). The Coastal Plain province is underlain by a seaward-dipping and thickening unconsolidated and semiconsolidated sediments that extend from the Fall Line to the Continental Shelf (Figure 4-4).

In South Carolina, the Coastal Plain province is divided into the Upper Coastal Plain and Lower Coastal Plain. Subdivisions of the Coastal Plain in the State include the Aiken Congaree Sand Hills in the Upper Coastal Plain, and the Coastal Terraces in the Lower Coastal Plain. The Congaree Sand Hills trend along the Fall Line northeast and north of the Aiken Savannah and Congaree Rivers bound the Aiken Plateau, on which the SRS is located; extends from the Fall Line to the Coastal Terraces. The surface of the plateau is characterized by broad interfluvial areas with narrow steep-sided valleys. The plateau is drained, although poorly drained depressions (Carolina bays) do exist (DOE 1991b). The proximity of the SRS to the Piedmont province, it has more relief than areas that are near the coast, with onsite elevations ranging from 27 to 128 meters (89 to 420 feet) above sea level.

The sediments of the Atlantic Coastal Plain of South Carolina overlie a basement composed of Paleozoic crystalline and Triassic sedimentary rocks. These sediments extend seaward from the Fall Line and range in age from Late Cretaceous to Recent. The sediment sequence thickens from essentially zero at the Fall Line to more than 1,219 meters at the coast. Regional dip is to the southeast. Coastal Plain sediments underlying the SRS are clays and clayey sands, although occasional beds of clean sand, gravel, clay, or calcareous (Figure 4-5). Two clastic limestone zones occur within the Tertiary age sequence. The zones vary in thickness from about 0.6 meter (2 feet) to approximately 24 meters (80 feet). The clastic sediments are unconsolidated, but thin semiconsolidated beds also occur. Underlying sediments are dense crystalline igneous and metamorphic rock or younger sediments of the Triassic Period. The Triassic formations and older igneous and metamorphic are separated hydrologically from the overlying Coastal Plain sediments by a regional aquiclude (Appleton Confining System (Arnett et al. 1993). Section 4.8.2 contains a detailed hydrogeology on the SRS.

Figure 4-3. Location of the Savannah River Site in the southern United States. Figure 4-4. Generalized subsurface cross-section. Figure 4-5. Stratigraphy of the SRS region. 4.6.2

Geologic Resources

SRS construction activities have used clay, sand, and gravel to a limited extent. These materials are not of major economic value due to their abundance throughout the region. The SRS has been a major user of groundwater in the region, withdrawing about 33 million liters (gallons) per day. Section 4.8.2 describes the groundwater resources at the SRS.

4.6.3 Seismic and Volcanic Hazards

The closest offsite fault system of significance is the Augusta Fault Zone, approximately 40 kilometers (25 miles) from the SRS. In this fault zone, the Belair Fault has experienced recent movement, but it is not considered capable of generating major earthquakes. There is no conclusive evidence of recent displacement along any fault within 320 kilometers of the SRS, with the possible exception of the buried faults in the epicentral area of the earthquake at Charleston, South Carolina, approximately 145 kilometers (90 miles) from the SRS (WSRC 1994a). Faulting in the subsurface Coastal Plain sediments in the Charleston vicinity suggested, based on structure contour mapping of the Eocene-Oligocene unconformity, depth of about 30 to 61 meters (100 to 200 feet) below ground surface (WSRC 1994a). Because it is not known if these faults offset sediments younger than Eocene-Oligocene, faults cannot be related to modern earthquakes that occur at depths greater than about 1.2 miles. Figure 4-6 shows the geologic structures within 150 kilometers (95 miles) some of which are discussed above.

Several Triassic-Jurassic basins, 140 to 230 million years old, have been identified in the Coastal Plain province of South Carolina and Georgia. The Dunbarton Triassic basin, which is a portion of the SRS, was formed by fault movement resulting from extensional forces during the formation of the Atlantic Ocean. After the erosion of basin margins and infill of Triassic age sediments, possible movement of an opposite sense to that during basin formation occurred along the fault during the Late Cretaceous age. Geophysical data indicate on faults at the basement-Coastal Plain interface, with the exception of possible movement along the Pen Branch Fault up into the Tertiary (WSRC 1994a).

Figure 4-6. Geologic structures within 150 km of SRS (Source: DOE 1991b). Research on the central portion of the SRS (Snipes et al. 1993). This fault is probably a continuation of a boundary fault of the Triassic age Dunbarton basin and is interpreted as being at least a Cretaceous/Tertiary (144-1.6 million years) reactivation of that fault (WSRC 1994a). Displacements of the Coastal Plain sediments range from about 26 meters (85 feet) at the Basement/Cretaceous contact to about 9 meters (30 feet) in the shallower sediments. Based on the available data, there is no evidence to indicate that the Pen Branch fault is defined by the U.S. Nuclear Regulatory Commission (NRC). Under the NRC definition, capable if it has moved within the last 35,000 years, has had recurring movement within 500,000 years, is related to any earthquake activity, or is associated with another recent study (Snipes et al. 1993) examined a Quaternary light tan soil horizon in the SRS. The soil horizon, which has a thickness of 3 to 6 meters (10 to 20 feet), revealed no movement indicating that there has been no recent Pen Branch Fault activity. Figure 4-7 shows the Pen Branch Fault and other known or suspected faults within the Paleozoic and Tertiary (DOE 1991b).

Seismicity in the Coastal Plain of South Carolina occurs in three distinct seismic zones (WSRC 1994a): Middleton Place-Summerville, about 19 kilometers (12 miles) northwest of Charleston; Bowman, about 59 kilometers (37 miles) northwest of the Middleton Place-Summerville; and Adams Run, about 30 kilometers (19 miles) southwest of the Middleton Place-Summerville (WSRC 1994a). Of the distinct seismic zones within the Coastal Plain of the Charleston area has been and remains the most seismically active. The Charleston area is the most significant source of seismicity affecting the SRS, both in terms of maximum hazard and the number of earthquakes felt in the area (WSRC 1994a).

Tables 4-2 and 4-3 summarize the historic information on earthquakes that have occurred in the SRS region. Two notable earthquakes have occurred within 320 kilometers (200 miles) of the SRS. The first was a major earthquake in 1886 centered in the Charleston area about 145 kilometers (90 miles) from the Site; it had an estimated Richter magnitude of 6.8. DOE estimates that it would have felt a tremor with an estimated Modified Mercalli Intensity (MMI) of VI and an estimated peak horizontal acceleration of 10 percent of gravity, or 0.10g, due to the earthquake (WSRC 1994a). The second earthquake was the Union County, South Carolina, earthquake which had an estimated Richter magnitude of 6.0 and occurred about 160 kilometers (100 miles) from the SRS (WSRC 1994a). This earthquake, which is the closest significant event to the SRS (WSRC 1994a).

Figure 4-7. Geologic faults of the Savannah River Site. Table 4-2. Earthquakes

Date ^b	Location	Coordinates		Maximum Intensity	Distance from SRS (km) ^c
		Lat. (yN)	Long. (yW)		
1811 Jan 13	Burke Co., Ga.	33.2	82.2	V	55
1811-1812 (3 shocks)	New Madrid, Mo.	36.3	89.5	XI-XII	850
1875 Nov 02	Lincolnton, Ga.	33.8	82.5	VI	100
1886 Sep 02	Charleston, S.C.	32.9	80.0	X	145
1886 Oct 22	Charleston, S.C.	32.9	80.0	VII	155
1897 May 31	Giles Co., Va.	33.0	80.7	VIII	455
1913 Jan 01	Union Co., S.C.	34.7	81.7	VII-VIII	160
1920 Aug 01	Charleston, S.C.	33.1	80.2	VII	135
1972 Feb 03	Bowman, S.C.	33.5	80.4	V	115
1974 Aug 02	Willington, S.C.	33.9	82.5	VI	105
1974 Nov 22	Charleston, S.C.	32.9	80.1	VI	145

a. Source: DOE (1991b).

b. Based on Greenwich mean time.

c. Conversion factor: 1 kilometer = 0.6214 mile.

d. NA = data not available.

e. Estimated.

Table 4-3. Earthquakes in the SRS region with a Modified Mercalli Intensity greater than or equal to III.

Date ^b	Coordinates		Maximum Intensity	Distance from SRS (km) ^c	Reported Intensity
	Lat. (yN)	Long. (yW)			Estimate SRS
1811 Jan 13 ^d	33.2	82.2	V	55	III-IV
1853 May 20	34.0	81.2	VI	102	NA
1945 Jul 26	33.8	81.4	V	77	NA
1964 Mar 07	33.7	82.4	NA	85	NA
1964 Apr 20	33.8	81.1	V	96	NA
1968 Sep 22	34.1	81.5	IV	102	NA
1972 Aug 14	33.2	81.4	NA	27	NA
1974 Oct 28	33.8	81.9	IV	72	NA
1974 Nov 05	33.7	82.2	III	77	NA
1976 Sep 15	33.1	81.4	NA	25	NA
1977 Jun 05	3.1	81.4	NA	35	NA
1982 Jan 28	32.9	81.4	NA	40	NA
1985 Jun 08	33.2	81.7	III	Onsite	III
1988 Feb 17 ^f	33.6	81.7	III	45	NA
1988 Aug 05	33.1	81.4	NA	Onsite	II
1993 Aug 08	NA	NA	NA	NA	NA

a. Source: DOE (1991b).

b. Based on Greenwich mean time.

c. Conversion factor: 1 kilometer = 0.6214 mile.

d. Located in Burke County, Ga.

e. NA = data not available.

f. Located at Aiken, S.C.

The Charleston-area earthquake, produced an estimated intensity of II to III (MMI) at Aiken, which is approximately 19 kilometers (12 miles) north of the Site (DOE 1991b).

Two earthquakes have occurred on the SRS during recent years (see Figure 4-7). In 1985, onsite instruments recorded an earthquake with a Richter magnitude of 2.6 and about 1.0 kilometer (0.6 mile) (WSRC 1994a). The epicenter was just west of the C-Area. The ground acceleration from this event did not activate instrumentation in the real time limits of 0.002g. On August 5, 1988, an earthquake with a Richter magnitude of 2.7 depth of approximately 2.7 kilometers (1.7 miles) occurred (Stephenson 1988); earthquake magnitude 2.0 are normally detected only by specialized instrumentation. The epicenter was just northeast of K-Area. Although this event was not felt by workers on the SRS, it was recorded by sensors within 96 kilometers (60 miles) of the Site. A report on the Aiken earthquake (Stephenson 1988) also reviewed the latest earthquake history for the re-

predicts recurrence period of 1 year for a magnitude 2.0 event for the southeast Co. However, the report notes that historic data to calculate recurrence rates accurate workers did feel the effects of two other events that occurred in the area within the Richter magnitude 2.6 earthquake occurred in the City of Aiken, approximately 19 km (12 miles) north of the SRS on February 17, 1988. Reports indicate that this event occurred in the Aiken area and on the SRS (DOE 1991b). Most recently, a Richter magnitude 3.2 earthquake occurred on August 8, 1993, approximately 16 kilometers (10 miles) east of the City of Aiken, South Carolina. Residents reported feeling this earthquake in Aiken, New South Wales (immediately north of the SRS), North Augusta (approximately 40 kilometers [25 miles] north of the SRS), and the Site.

Based on seismic activity information in the past 300 years, this analysis does not predict earthquakes greater than a Richter magnitude 6.0, which corresponds to a Modified Mercalli of VII, to occur on the SRS. The design-basis earthquake for the SRS is a Modified Mercalli Intensity VIII event, which corresponds to a horizontal peak ground acceleration of 0.2g, current technology, as applied in various probabilistic evaluations of the seismic region, the 0.2g peak ground acceleration can be associated with a 2×10^{-4} annual exceedance (5,000-year return period). DOE Standards 1020 (DOE 1994a) and 1024 (DOE 1994b) summarize the results of recent seismic analyses at DOE sites and show that maximum ground accelerations for the Savannah River Site for 500 year, 1,000 year, 2,000 year, and 5,000 year seismic events are 0.10g, 0.13g, 0.18g, and 0.19g respectively. The seismic hazard presented in this EIS is for general seismic hazard comparisons across DOE sites. Seismic hazards for existing and new facilities should be evaluated on a facility-specific basis. DOE Orders and standards and site-specific standards.

Historically, DOE has generally selected the more conservative 0.20g as the peak ground acceleration for the 5,000 year seismic event when preparing safety analysis report impact statements for the SRS. For consistency with these existing analyses, this impact statement assumes 0.20g to be the peak horizontal ground acceleration that would be expected for the 5,000 year seismic event. Figure 4-8 shows seismic hazard curves for the SRS.

A number of paleoliquefaction sites have been identified in Beaufort County, South Carolina, some 50 miles (80 kilometers) southeast of the SRS, indicating a likelihood of prehistoric events outside of the currently-active Charleston seismic zone (Rajendran and Talwal 1992). There is no evidence to suggest that seismically-induced liquefaction of soils represents a hazard at the SRS. Weak subsurface zones are encountered occasionally during drilling. These are associated with carbonate materials and appear to be related to dissolution of these materials.

Engineering investigations have been conducted on granular soils underlying the Processing Facility [in S-Area just north of H-Area (see Figure 2-3)] to evaluate the potential for liquefaction under cyclic stresses of these soils (WSRC 1992b). These investigations indicate that the sands and clayey sands throughout the subgrade will not experience liquefaction leading to bearing capacity failures and will not develop cyclic mobility (significant accumulative deformations) under the safe shutdown earthquake with a peak horizontal ground acceleration of 0.20g (9.8 meters/second² or 32.1 feet/second²).

4.7 Air Resources

4.7.1 Meteorology and Climatology

The SRS collects wind data from instruments mounted on seven onsite 61-meter (200 feet) meteorological towers. Figure 4-9 shows a wind rose that represents annual wind direction and wind speeds for the SRS from 1987 through 1991. The maximum wind direction frequencies are from the northeast and west-southwest. The average wind speed for this 5-year period is 3.8 meters per second (8.5 miles per hour). Calm winds (less than 1 meter per second) occurred less than 10 percent of the time during the 5-year period. Seasonal wind speeds are shown in Figure 4-8. Seismic hazard curves for the SRS. Figure 4-9. Wind Rose. were generated at 3.4 meters per second (7.6 miles per hour) (WSRC 1994a).

The annual average temperature at the SRS is 18 degrees C (64 degrees F); monthly range from a low of 7 degrees C (45 degrees F) in January to a high of 27 degrees C (81 degrees F) in July. Relative humidity readings taken four times each day range from 36 percent in January to 98 percent in August (DOE 1991a).

The average annual precipitation at the SRS is approximately 122 centimeters (48 inches). Precipitation distribution is fairly even throughout the year, with the highest precipitation in summer [36.1 centimeters (14.2 inches)] and the lowest in autumn [22.4 centimeters (8.8 inches)]. Snowfall has occurred in the months of October through March, with the average annual snowfall of 1.5 centimeters (0.6 inches).

3.0 centimeters (1.2 inches). Large snowfalls are rare (DOE 1991a).

Winter storms in the SRS area occasionally bring strong and gusty surface winds high as 32 meters per second (72 miles per hour). Thunderstorms can generate winds high as 18 meters per second (40 miles per hour) and even stronger gusts. The fast speed recorded at Augusta between 1950 and 1986 was 37 meters per second (83 miles (DOE 1991a).

4.7.1.1 Occurrence of Violent Weather. The SRS area experiences an average of 56

thunderstorm days per year. From 1954 to 1983, 37 tornadoes were reported for a 1-latitude and longitude that includes the SRS (DOE 1991a). This frequency of occurrence to an average of about one tornado per year. The estimated probability of a tornado on the SRS is 7×10^{-5} per year (DOE 1991a). Since operations began at the SRS in confirmed tornadoes have occurred on or near the Site. They caused nothing more than with the exception of a tornado in October 1989 that caused considerable damage to an undeveloped southeastern sector of the SRS (WSRC 1994a).

From 1700 to 1992, 36 hurricanes occurred in South Carolina, resulting in an average of about one hurricane every 8 years. Three hurricanes were classified as major. about 160 kilometers (100 miles) inland, the winds associated with hurricanes have below hurricane force [i.e., equal to or greater than a sustained wind speed of 33. (75 miles per hour)] before reaching the SRS. Winds exceeding hurricane force have only once at SRS (Hurricane Gracie in 1959) (WSRC 1994a).

4.7.1.2 Atmospheric Stability. Based on measurements at onsite meteorological stations, the

atmosphere in the SRS region is unstable approximately 56 percent of the time, neutral the time, and stable about 21 percent of the time. On an annual basis, inversion occurs 21 percent of the time at the SRS (WSRC 1994a).

4.7.2 Nonradiological Air Quality

4.7.2.1 Background Air Quality. The SRS is in the Augusta (Georgia) - Aiken (South

Carolina) Interstate Air Quality Control Region (AQCR). This Air Quality Control Region designated as a Class II area, is in compliance with National Ambient Air Quality Standards for criteria pollutants. The criteria pollutants include sulfur dioxide, nitrogen dioxide, particulate matter (less than or equal to 10 microns), carbon monoxide, and lead (CFR 1993a). The closest nonattainment area to the SRS is the Atlanta, Georgia region, 233 kilometers (145 miles) to the west, which is in nonattainment of the standards.

The SRS will have to comply with Prevention of Significant Deterioration (PSD) requirements if there is a significant increase in emissions of criteria air pollutants modification at the Site (CFR 1993b). Development at the SRS has not yet triggered Significant Deterioration permitting requirements. If a permit were required, the address several requirements, including impacts on the air quality of Class I areas (6.2 miles) of the Site (CFR 1993b). The nearest Class I area to the SRS is the Congaree National Monument in South Carolina, approximately 73 kilometers (45 miles) to the Site. Therefore, a Prevention of Significant Deterioration permit, if required, does not have to address Class I areas.

4.7.2.2 Air Pollutant Source Emissions. The SRS utilized the 1990 comprehensive

emissions inventory data to establish the baseline year for showing compliance with air quality standards - calculating both maximum potential and actual emission rate compliance demonstration also included sources forecast for construction or operation (for which the SRS had obtained air quality construction permits through December 1991) based on its calculated emission rates for the sources on process knowledge, source operating capacity, material balance, and U.S. Environmental Protection Agency (EPA) Emission Factors (AP-42; EPA 1985).

4.7.2.3 Ambient Air Monitoring. At present, the SRS performs no onsite ambient air quality

monitoring. State agencies operate ambient air quality monitoring sites in Barnwell and Richland Counties. These areas, which include the SRS, are in attainment with National Ambient Air Quality Standards for sulfur dioxide, nitrogen oxides, carbon monoxide, particulate matter, and lead (CFR 1993a).

4.7.2.4 Atmospheric Dispersion Modeling. The SRS has performed atmospheric

dispersion modeling for criteria and toxic air pollutants for both maximum potential emissions for the base year 1990, using the EPA Industrial Source Complex Short Term model. The SRS used 1991 meteorological data collected at the Site meteorological stations model.

4.7.2.5 Summary of Nonradiological Air Quality. The SRS is in compliance with

National Ambient Air Quality Standards and with the gaseous fluoride and total suspended particulate standards required by South Carolina Department of Health and Environmental Control Regulation R.61-62.5, Standard 2, "Ambient Air Quality Standards" (AAQS) (see Table 4-4).

The SCDHEC has non-radiological air quality regulatory authority over the SRS. The SCDHEC determines SRS ambient air quality compliance based on SRS air pollutant concentrations modeled at the Site perimeter (excluding SC Highway 125, which crosses the southwest corner of the SRS).

The SRS is in compliance with SCDHEC Regulation R.61-62.5, Standard 8, "Toxic Air Pollutants," which regulates the emission of 257 toxic substances. The SRS has identified potential sources for 139 of the 257 regulated substances; the modeled results indicate that applicable Department of Health and Environmental Control standards (WSRC 1993a). SRS emissions of toxic air pollutants of concern related to the SRS spent nuclear fuel operation based on 1990 baseline data and the potential sources of air pollution permitted for operation in December 1992.

4.7.3 Radiological Air Quality

4.7.3.1 Background and Baseline Radiological Conditions. In the SRS region, airborne

radionuclides originate from natural resources (terrestrial or cosmic), worldwide nuclear power operations. The SRS maintains a network of air monitoring stations on and around the Site. Table 4-4. Estimated ambient concentration contributions of criteria air pollutant sources and sources planned for construction or operation through 1995 (-g/m3). ,b

Pollutantc	Averaging time	SRS Maximum Potential Concentration	Actual	Most stringent AAQSD (Federal or state)
SO ₂	Annual	18	10	80f
	24-hour	356	185	365f,g
	3-hour	1,210	634	1,300f,g
NO _x	Annual	30	4	100f
CO	8-hour	818	23	10,000f,g
	1-hour	3,553	180	40,000f,g
Gaseous fluorides (as HF)	12-hour	2.40	0.62	3.7e
	24-hour	1.20	0.31	2.9e
	1-week	0.6	0.15	1.6e
	1-month	0.11	0.03	0.8e
PM ₁₀	Annual	9	3	50f
	24-hour	93	56	150f
O ₃	1-hour	NA	NA	235f,g
TSP	Annual	20	11	75e
	geometric mean			
Lead	Calendar	0.0015	0.0003	1.5e

quarter
mean

- a. Source: WSRC (1994b).
 b. The contributions listed are the maximum values at the SRS boundary.
 c. SO₂ = sulfur dioxide; NO_x = nitrogen oxides; CO = carbon monoxide; PM₁₀ = particulate 10-m in diameter; TSP = Total Suspended Particulates, O₃ = Ozone.
 d. AAQS = Ambient Air Quality Standard.
 e. Source: SCDHEC (1976).
 f. Source: 40 CFR Part 50.
 g. Concentration not to be exceeded more than once a year.
 NA = Not available.

Table 4-5. Baseline 24-hour average modeled concentrations at the SRS boundary - the pollutants regulated by South Carolina from existing SRS sources and sources planned or operation through 1995 (yg/m³).

Pollutant ^b	Regulatory Limit	Maximum Potential Concentration ^c	Actual Concentration ^d	Maximum Potential Concentration ^e
Nitric acid	125	51	4.0	41
1,1,1-Trichloroethane	9,550	81	22	1
Benzene	150	32	31	21
Ethanolamine	200	<0.01	<0.01	<0.1
Ethyl benzene	4,350	0.58	0.12	<0.1
Ethylene glycol	650	0.20	0.08	<0.1
Formaldehyde	7.5	<0.01	<0.01	<0.1
Glycol ethers	Pending	<0.01	<0.01	-
Hexachloronaphthalene	1	<0.01	<0.01	<0.1
Hexane	200	0.21	0.072	<0.1
Manganese	25	0.82	0.10	3
Methyl alcohol	1,310	2.9	0.51	0.2
Methyl ethyl ketone	14,750	6.0	0.99	<0.1
Methyl isobutyl ketone	2,050	3.0	0.51	<0.1
Methylene chloride	8,750	10.5	1.8	<0.1
Naphthalene	1,250	0.01	0.01	<0.1
Phenol	190	0.03	0.03	<0.1
Phosphorus	0.5	<0.001	<0.001	<0.1
Sodium hydroxide	20	0.01	0.01	<0.1
Toluene	2,000	9.3	1.6	<0.1
Trichloroethylene	6,750	4.8	1.0	<0.1
Vinyl acetate	176	0.06	0.02	<0.1
Xylene	4,350	39	3.8	0.9

- a. Source: WSRC (1994b).
 b. Pollutants listed include compounds of interest regarding spent nuclear fuel.
 c. Maximum potential emissions from all SRS sources for 1990 plus maximum potential for sources permitted in 1991 and 1992.
 d. Actual emissions from all SRS sources plus maximum potential emissions for sources under construction through December 1992.
 e. AAQS = Ambient Air Quality Standard.
 determine concentrations of radioactive particulates and aerosols in the air (Arnet Table 4-6 lists average and maximum atmospheric radionuclide concentrations at the and background [160-kilometer (100-mile) radius] monitoring locations during 1991. the average concentrations of tritium in the atmosphere, as measured at on- and off locations.

Table 4-6. Radioactivity in air at SRS perimeter and at 160-kilometer (100-mile) radius

Location	Gross Alpha	Nonvolatile Beta	Sr-89, 90 ^b	Pu-238 ^b
Site perimeter				
Average	2.61x10 ⁻³	1.78x10 ⁻²	4.90x10 ⁻⁵	1.22x10 ⁻⁶
Maximum	1.07x10 ⁻²	4.63x10 ⁻²	5.11x10 ⁻⁴	1.94x10 ⁻⁵
Background (160-kilometer radius)				
Average	2.60x10 ⁻³	1.76x10 ⁻²	2.00x10 ⁻⁴	1.44x10 ⁻⁶

Maximum	9.31x10 ⁻³	5.26x10 ⁻²	2.08x10 ⁻³	2.39x10 ⁻⁵
a. Source: Arnett et al. (1992).				
b. Monthly composite.				
Table 4-7. Average atmospheric tritium concentrations on and around the Savannah R (pCi/m ³).				
Location	1991	1990	1989	
Onsite	250	430	640	
Site perimeter	21	32	37	
40-kilometer radius	11	12	14	
160-kilometer radius	8.5	8.8	9	
a. Source: Arnett et al. (1992).				

4.7.3.2 Sources of Radiological Emissions. Table 4-8 lists groups of facilities that

released radionuclides to the atmosphere in 1992; the facilities are grouped according to function that resulted in the release of radioactive materials.

Table 4-9 lists both the identified radionuclides that contributed to the SRS and the contribution of each radionuclide to the total site effective dose equivalent.

Table 4-8. Operational groupings and function of radionuclide sources.

Group	Function
Reactor Materials	Production of fuel and targets
Reactors	Irradiation of fuel and targets
Separations	Separation of useful radionuclides (other than tritium)
Analytical Laboratories	Process Control Laboratories
Tritium	Extraction, purification, and packaging
Waste Management	Management of radioactive waste
Savannah River Technology Center	Research and development to support SRS processes

4.8 Water Resources

4.8.1 Surface Water

The Savannah River bounds the SRS on its southwestern border for about 20 miles (32 kilometers), approximately 160 river miles (260 kilometers) from the Atlantic Ocean. River flow averages about 10,000 cubic feet (283 cubic meters) per second. River flow at the SRS averages about 3,960 cubic feet (112 cubic meters) per second to 71,700 cubic feet (2,030 cubic meters) per second.

Five upstream reservoirs - Jocassee, Keowee, Hartwell, Richard B. Russell, and Lake Lanier - minimize the effects of droughts and the impacts of low flow on downstream water and wildlife resources in the river.

At the SRS, a swamp occupies the floodplain along the Savannah River for a distance of approximately 10 miles (17 kilometers); the swamp is about 1.5 miles (2.5 kilometers) wide. A natural levee separates the river from the swampy floodplain. Figure 4-10 shows the floodplain of the Savannah River in the vicinity of the SRS as well as the floodplain tributaries draining the SRS. A 500-year floodplain map of the SRS has not been completed. It would be required prior to the siting of any spent nuclear fuel management facility with DOE regulations (CFR 1979). These regulations require DOE to evaluate the potential for flooding to proposed "critical actions" (for example, the storage of highly toxic materials), which it defines as those for which even a slight chance of flooding would be unacceptable.

The five principal tributaries to the river on the SRS are Upper Three Runs Creek, Middle Three Runs Creek, Pen Branch, Steel Creek, and Lower Three Runs Creek (Figure 4-10). These tributaries contribute about 10 percent of the total flow of the Savannah River at the SRS.

Table 4-9. Annual quantity of radionuclide emissions from the Savannah River Site.

Radionuclide	Annual Quantity (curies)	Percent of Total Site Dose
H-3 (oxide)	1.00x10 ⁵	98.0
Pu-239	7.45x10 ⁻⁴	0.6
U-235, 238	1.58x10 ⁻³	0.4
Pu-238	4.46x10 ⁻⁴	0.3
Ar-41	2.51x10 ²	0.3
I-129	3.50x10 ⁻³	0.2
Am-241, 243	1.13x10 ⁻⁴	0.1
Sr-89, 90 (Y-90)	2.03x10 ⁻³	0.02
Cm-242, 244	2.31x10 ⁻⁵	0.01
Cs-137 (Ba-137m)	2.50x10 ⁻⁴	0.01

C-14	1.86x10 ⁻¹	0.01
H-3 (elemental)	5.59x10 ⁴	<0.01
I-135	1.34x10 ⁻¹	<0.01
Kr-85	4.99x10 ¹	<0.01
I-131	9.99x10 ⁻⁵	<0.01
Ru-106 (Rh-106)	1.81x10 ⁻⁶	<0.01
I-133	1.15x10 ⁻³	<0.01
Co-60	3.60x10 ⁻⁷	<0.01
Xe-135	2.43x10 ⁻³	<0.01
Cs-134	3.75x10 ⁻⁸	<0.01
Ce-144 (Pr-144, 144m)	1.16x10 ⁻⁷	<0.01
Eu-154	3.44x10 ⁻¹³	<0.01
Eu-155	1.63x10 ⁻¹³	<0.01
Sb-125	7.27x10 ⁻¹⁵	<0.01
Zr-95 (Nb-95)	2.39x10 ⁻¹⁴	<0.01

a. Source: Arnett et al. (1993).

b. Includes emissions to the atmosphere and surface water.

Figure 4-10. Savannah River Site, showing major stream systems and facilities. a descends 50 to 200 feet (15 to 60 meters) before discharging into the river. The s historically have received varying amounts of effluent from various SRS operations, commercial sources of water. The natural flow of SRS streams ranges from less than (1 cubic meter) per second in smaller streams such as Pen Branch to 240 cubic feet per second in Upper Three Runs Creek.

4.8.1.1 SRS Streams. This section describes the pertinent physical and hydrologic properties

of Upper Three Runs Creek and Fourmile Branch, which are the streams closest to mos nuclear fuel management locations (Figure 4-10). These two streams are among the 1 SRS, and they border the areas where DOE is most likely to locate new spent nuclear

Upper Three Runs Creek is a large, cool [annual maximum temperature of 26.1 deg (79 degrees F)] blackwater stream in the northern part of the SRS. It drains an ar 210 square miles (545 square kilometers), and has an average discharge of 330 cubic meters) per second at the mouth of the creek. Upper Three Runs Creek is approximat (40 kilometers) long, with its lower 17 miles (28 kilometers) inside the boundaries creek receives more water from underground sources than the other SRS streams and, low conductivity, hardness, and pH values. Upper Three Runs Creek is the only majo the SRS that has never received thermal discharges.

Fourmile Branch is about 15 miles (24 kilometers) long and drains an area of ap 34 square miles (89 square kilometers). In its headwaters, Fourmile Branch is a sm stream that receives relatively few impacts from SRS operations. The water chemist headwater area of the creek is very similar to that of Upper Three Runs Creek, with nitrate concentrations, which are an order of magnitude higher than those in Upper (WSRC 1994a). These elevated nitrate concentrations are probably the result of gro and outcropping from the F- and H-Area seepage basins. In its lower reaches, Fourm broadens and flows through a delta formed by the deposition of sediments. Although through the delta is in one main channel, the delta has many standing dead trees, 1 cypress trees that provide structure and reduce the water velocity in some areas. delta, the creek flows in one main channel and most of the flow discharges into the River Mile 152 (kilometer 245), while a small portion of the creek flows west and e Creek, a small onsite tributary.

4.8.1.2 Surface Water Quality. The Savannah River, which forms the boundary between the

States of Georgia and South Carolina, supplies potable water to several users. Ups the river supplies domestic and industrial water needs for Augusta, Georgia, and No Carolina. The river also receives sewage treatment plant effluent from Augusta, Ge Augusta, Aiken, and Horse Creek Valley, South Carolina; and as described above from SRS operations via onsite stream discharges. Approximately 130 river-miles (210 ki downstream of the SRS, the river supplies domestic and industrial water needs for S and Beaufort and Jasper Counties in South Carolina through intakes located at about and River Mile 39. In addition, Georgia Power's Vogtle Electric Generating Plant w average of 1.3 cubic meters per second (46 cubic feet per second) for cooling and r of 0.35 cubic meters per second (12 cubic feet per second) of cooling tower blowdown

Urquhart Steam Generating Station at Beech Island, South Carolina withdraws approximately 265 cubic feet per second) for once-through cooling water.

The South Carolina Department of Health and Environmental Control regulates the properties and concentrations of chemicals and metals in SRS effluents under the National Discharge Elimination System (NPDES) program. This agency also regulates chemical water quality standards for SRS waters. On April 24, 1992, the agency changed the classification of the Savannah River and SRS streams from "Class B waters" to "Freshwaters." The definitions of Class B waters and Freshwaters are the same, but the Freshwaters classification imposes a more stringent set of water quality standards (Arnett et al. 1993). Tables 4-10 and 4-11 show the characteristics of SRS surface-water quality upstream and downstream, respectively, and contributions from SRS and possibly other sources. A comparison of these results with influences from SRS or other sources are not seriously degrading Savannah River water.

4.8.2 Groundwater Resources

4.8.2.1 Hydrostratigraphic Units. There are two hydrogeologic provinces in the subsurface

beneath SRS (WSRC 1994a). The first, referred to as the Piedmont hydrogeologic province (Figure 4-11), includes Paleozoic metamorphic and igneous basement rocks and Triassic mudstone, sandstone, and conglomerate contained within the Dunbarton Basin. The second, referred to as the Southeastern Coastal Plain hydrogeologic province, represents the major aquifer and consists of a wedge of unconsolidated Coastal Plain sediments of Late Cretaceous age (Figure 4-11). These two units are overlain by the vadose or unsaturated zone, which is the source of water to the Savannah River Site in 1990. ,b

Parameter	Unit of Measure	MCL c,d or DCGe	Existing Water Average
Aluminum	mg/L	0.05-0.2g	NCi
Ammonia	mg/L	NAj	0.1
Cadmium	mg/L	0.005g	NC
Calcium	mg/L	NA	NC
Cesium-137	pCi/L	120e	0.0088
Chemical oxygen demand	mg/L	NA	9.7
Chloride	mg/L	250h	7.8
Chromium	mg/L	0.1d	NC
Copper	mg/L	1.0d	NC
Dissolved oxygen	mg/L	>5	8.0
Fecal coliform	Colonies per 100/ml	1,000g	54
Gross alpha	pCi/L	15g	0.04
Iron	mg/L	0.3h	NC
Lead	mg/L	0.015g	NC
Magnesium	mg/L	NA	NC
Manganese	mg/L	0.05g	NC
Mercury	mg/L	0.002d	NC
Nickel	mg/L	0.1c	NC
Nitrite/Nitrate	mg/L	10g	0.32
Nonvolatile beta (dissolved)	pCi/L	50g	1.9
pH	pH Units	6.5-8.5g	Not reported
Phosphate	mg/L	N/A	0.09
Plutonium-238	pCi/L	1.6e	0.0006
Plutonium-239	pCi/L	1.2e	0.0005
Sodium	mg/L	NA	NC
Strontium-89	pCi/L	800e	0.23
Strontium-90	pCi/L	8c	0.09
Sulfate	mg/L	250h	7.8
Suspended solids	mg/L	NA	13
Temperature	Degrees Celsius	32.2k	18.0
Total dissolved solids	mg/L	500h	62
Tritium	pCi/L	20,000c	150
Zinc	mg/L	5h	NC

a. Source: Cummins et al. (1991).

b. Parameters are those for which DOE routinely measures as a regulatory requirement.

c. Maximum Contaminant Level (MCL), EPA National Primary Drinking Water Regulations

- d. Maximum Contaminant Level (MCL); South Carolina (1976).
- e. U.S. Department of Energy Derived Concentration Guides (DCGs) for Water (DOE 199 effective dose of 100 millirem per year; however, because drinking water MCL is percent of DCG.
- f. Average concentration of samples taken at downstream monitoring station. Maximum river potentially affected by site activities. Less than (<) indicates concentration
- g. Concentration exceeded water quality criteria; however, these criteria are listed and DOE DCGs are listed. Water Quality Criteria (WQCs) and secondary standards
- h. Secondary Maximum Contaminant Level (SMCL), EPA National Secondary Drinking Water
- i. NC = Not calculated due to insufficient number of samples.
- j. NA = None applicable.
- k. Shall not exceed weekly average of 32.2 degrees Celsius after mixing nor rise more temperature criterion mixing zone has been established.

Table 4-11. Water quality in the Savannah River below the confluence with Lower Tidal the Savannah River Site in 1990. ,b

Parameter	Unit of Measure	MCL c,d or DCGe	Existing Water Average
Aluminum	mg/L	0.05-0.2g	NCi
Ammonia	mg/L	NAj	0.1
Cadmium	mg/L	0.005g	NC
Calcium	mg/L	NA	NC
Cesium-137	pCi/L	120e	0.028
Chemical oxygen demand	mg/L	NA	9.8
Chloride	mg/L	250h	8
Chromium	mg/L	0.1d	NC
Copper	mg/L	1.0d	NC
Dissolved oxygen	mg/L	>5	7.7
Fecal coliform	Colonies per 100/ml	1,000g	54
Gross alpha	pCi/L	15g	0.08
Iron	mg/L	0.3h	NC
Lead	mg/L	0.015g	NC
Magnesium	mg/L	NA	NC
Manganese	mg/L	0.05h	NC
Mercury	mg/L	0.002d	NC
Nickel	mg/L	0.1c	NC
Nitrite/Nitrate	mg/L	10g	0.28
Nonvolatile beta (dissolved)	pCi/L	50g	2.1
pH	pH Units	6.5-8.5h	Not reported
Phosphate	mg/L	N/A	0.1
Plutonium-238	pCi/L	1.6e	0.0006
Plutonium-239	pCi/L	1.2e	0.0014
Sodium	mg/L	NA	NC
Strontium-89	pCi/L	800e	0.25
Strontium-90	pCi/L	8c	0.13
Sulfate	mg/L	250h	8.5
Suspended solids	mg/L	NA	12
Temperature	Degrees Celsius	32.2k	18.0
Total dissolved solids	mg/L	500h	63
Tritium	pCi/L	20,000c	900
Zinc	mg/L	5h	NC

a. Source: Cummins et al. (1991).

b. Parameters are those for which DOE routinely measures as a regulatory requirement

c. Maximum Contaminant Level (MCL), EPA National Primary Drinking Water Regulations

d. Maximum Contaminant Level (MCL); South Carolina (1976).

e. U.S. Department of Energy Derived Concentration Guides (DCGs) for Water (DOE 199 effective dose of 100 millirem per year; however, because drinking water MCL is percent of DCG.

f. Average concentration of samples taken at downstream monitoring station. Maximum river potentially affected by site activities. Less than (<) indicates concentration

g. Concentration exceeded water quality criteria; however, these criteria are listed and DOE DCGs are listed. Water Quality Criteria (WQCs) and secondary standards

h. Secondary Maximum Contaminant Level (SMCL), EPA National Secondary Drinking Water

i. NC = Not calculated due to insufficient number of samples.

j. NA = None applicable.

k. Shall not exceed weekly average of 32.2 degrees Celsius after mixing nor rise more temperature criterion mixing zone has been established.

Figure 4-11. Comparison of lithostratigraphy and hydrostratigraphy for the SRS or silty sand through which recharge takes place.

The sediments that make up the Southeastern Coastal Plain hydrogeologic province west-central South Carolina are grouped into three major aquifer systems divided by confining systems, all of which are underlain by the Appleton confining system (Figure 4-11). The Appleton system separates the Southeastern Coastal Plain hydrogeologic province from the Piedmont hydrogeologic province. Locally, each of the major aquifer systems contains aquifer and confining units. Figure 4-11 shows the regional lithostratigraphic subdivision of the province. The strata that form the three aquifer systems consist primarily of fine- to coarse-grained gravel and limestone deposited under relatively high energy conditions in fluvial environments (WSRC 1994a).

Figure 4-11 shows the current aquifer/aquitard terminology at the SRS. Aquifers, in ascending order, include the McQueen Branch, the Crouch Branch, and the Steed Pond. For comparison, the figure also includes the corresponding aquifer terminology used on the Georgia side of the Savannah River. These include the Midville, Dublin, and Floridan aquifer systems. In addition, the aquifers are separated by confining layers which include, in ascending order, the A and Meyers Branch confining systems (WSRC 1994a).

4.8.2.2 Groundwater Flow. Excellent quality groundwater is abundant in this region of

South Carolina from many local aquifer units. As a result, the South Carolina Department of Health and Environmental Control has classified all aquifers in the state as Class GB (South Carolina or U.S. Environmental Protection Agency (EPA) Class II, meaning that the aquifers contain resource-quality water, but are not the sole source of supply (South Carolina Class II aquifers) (DOE 1991b).

The main source of recharge to the vadose zone is rainfall. The annual precipitation is 48 inches (121.9 centimeters), with an estimated 16 inches (41 centimeters) designated as recharge at the center of the SRS, in bare and grass-covered areas (WSRC 1994a). The groundwater flow in the vadose zone is predominantly downward. However, given the presence of sand and clay that exist, there is significant lateral spread in some areas. In general, the thickness ranges from approximately 130 feet (40 meters) in the northernmost portion to 0 feet where the water table intersects wetlands, streams, or creeks.

The following discussion of groundwater flow in the Coastal Plain hydrogeologic province begins with the deepest aquifers at the SRS and proceeds to shallower units. It does so in the confining units because few hydraulic head measurements are available for them. For a good approximation, flow in aquitards is limited predominantly to vertical flow between them. The Midville or McQueen Branch aquifer (which has also been called the Middendorf, Cretaceous, the Tuscaloosa, and Aquifer IA) is highly transmissive and, therefore, is the primary production aquifer for much of the SRS. This aquifer flows horizontally, predominantly toward the Savannah River. In the past, groundwater production wells at the SRS were screened in the Midville (McQueen Branch) and Dublin (Crouch Branch) aquifers. In 1985 DOE committed the South Carolina Department of Health and Environmental Control to complete production in the McQueen Branch aquifer to minimize the potential for contamination to reach the surface spread in the deeper aquifers.

Flow in the Dublin or Crouch Branch aquifer (which has also been called the Bladwell, Tuscaloosa, the Upper Cretaceous, and Aquifer IB) is more complicated than flow in the McQueen Branch aquifer because of the apparent communication with Upper Three Runs Creek at the SRS. Nonetheless, horizontal flow in the Dublin (Crouch Branch) aquifer is predominantly toward the Savannah River. However, there is an upward vertical flow component near the river. Recharge to the Dublin-Midville aquifer system occurs in areas where the ground surface near the Fall Line (see Figure 4-3).

Horizontal flow in the Gordon aquifer (previously called the Congaree, the Tertius, or Aquifer II) is toward Upper Three Runs Creek and the Savannah River, depending on the location at the SRS. Both the river and Upper Three Runs Creek intercept this aquifer. The Gordon aquifer receives most of its recharge from groundwater that originates on the SRS.

Previous SRS studies have called the Upper Three Runs aquifer the "water table aquifer." They have defined it as both the Barnwell/McBean and water table aquifers in the central portion of the SRS where those aquifers were thought to be separated by a "tan clay." The Upper Three Runs is the shallowest aquifer at the SRS. The horizontal groundwater flow is generally to the surface-water feature that is in communication with the water table. Most SRS streams, including the Crouch Branch in the northeastern part of the Site, are in communication with the water table.

a "losing stream," meaning it provides, or "loses," water to the Upper Three Runs a the Upper Three Runs aquifer receives most of its recharge from precipitation. The aquifer is not a source of domestic or production water on the SRS because the lowe a more abundant supply of higher quality water (WSRC 1994a).

4.8.2.3 Groundwater Quality. The quality of groundwater in the principal hydrologic

systems beneath the SRS depends on both the source of the water and the inorganic a reactions that take place along its flowpath. Quality is strongly influenced by th composition and mineralogy of the enclosing geologic materials (WSRC 1994a).

In general, the quality of the groundwater in the Coastal Plain sediments at th surrounding areas is suitable for most domestic and industrial purposes. The water concentrations of total dissolved solids (TDS), ranging from less than 10 milligram 150 to 200 milligrams per liter. The pH values range from 4.9 to 7.7 (where the gr contact with limestone). Much of the groundwater is corrosive to metal surfaces du content and frequently low pH values. High dissolved iron concentrations can also some groundwater units. The SRS uses degasification and filtration processes to ra remove iron in domestic water supplies where necessary (WSRC 1994a).

Table 4-12 summarizes groundwater quality data from 85 existing waste sites on compared to drinking water standards; Table 4-13 lists similar information for sele constituents. The data in these tables are from ongoing monitoring programs on the EPA-accepted methods and guidelines for sampling and analysis are an integral part program. Several of the facilities discussed below have state-approved sampling an

The shallow aquifers beneath 5 to 10 percent of the SRS have been contaminated solvents, metals, tritium, or other constituents used or generated on the Site. Fi locations of facilities where the SRS monitors groundwater and areas with constitue drinking water standards in 1992; the concentrations shown on Figure 4-12 represent data from one monitoring well on at least one occasion at a given area. Contaminat the shallow aquifers, with one exception (see next paragraph). Most contaminated g SRS is beneath a few facilities; contaminants reflect the operations and chemical p facilities perform. For example, contaminants in the groundwater beneath A- and M-chlorinated volatile organics, radionuclides, metals, and nitrate. At F- and H-Are the groundwater include tritium and other radionuclides, metals, nitrate, chlorinat values much smaller than those found at A- and M-Areas, and sulfate. The groundwat Sanitary Landfill contains chlorinated volatile organics, radionuclides, and metals **Table 4-12.** Representative groundwater quality data for nonradioactive constituent Savannah River Site.

Parameter (Unit)	Standard	Maximum Value
Alkalinity (as CaCO ₃) (mg/L)	100	1,360b
pH (pH units)	8.5c	13b
Antimony (mg/L)	0.005	0.013
Arsenic (mg/L)	0.05	0.1
Beryllium (mg/L)	0.011d	0.0043
Cadmium (mg/L)	0.005c	0.34
Chromium (mg/L)	0.1c	0.82
Mercury (mg/L)	0.002c	0.12
Lead (mg/L)	0.015e	1.0
Nitrate-N (mg/L)	10c	278b
Sulfate (mg/L)	400c	73,500b
Pentachlorophenol (mg/L)	0.001c	0.0032
Lindane (mg/L)	0.0002c	0.00048
Carbon tetrachloride (mg/L)	0.005	0.43
1,2-Dichloroethane (mg/L)	0.005c	0.27
1,1,1-Trichloroethane (mg/L)	0.2c	0.21
1,1-Dichloroethylene (mg/L)	0.007c	0.15
Trichlorethylene (mg/L)	0.005c	147
Tetrachloroethylene (mg/L)	0.005c	101

a. Data compiled from 85 existing wastes sites (Arnett et al. 1993).

b. The elevated values for alkalinity and pH might be due to faulty well installati sulfate and nitrate values might be due to acid spills near wells.

c. National secondary drinking water regulations (CFR 1991).

d. National primary drinking water regulations (CFR 1974).

e. Action level at which providers of public drinking water apply treatment techniq

levels (CFR 1991).

Table 4-13. Representative groundwater data for radioactive constituents from the Site (pCi/liter).

Constituent	Standard ^b	Maximum Concentration
Gross alpha	15	2,700
Nonvolatile beta	50	19,000
Tritium	20,000	1.8 x 10 ⁸
Cesium-137	200	980
Cobalt-60	100	290
Iodine-129	1	72
Ruthenium-106	30	170
Total radium (radium-226 and radium-228)	5	50
Strontium-90	8	5,300

a. Source: Arnett et al. (1993).

b. National Primary Drinking Water Regulations (CFR 1974), (56 FR 33052).

beneath all the reactor areas except R-Area contains tritium, other nuclides, metal volatile organics. At R-Area, groundwater contaminants include radionuclides and groundwater beneath D-Area contains metals, radionuclides, sulfate, and chlorinated At TNX-Area, the groundwater contains chlorinated volatile organics, radionuclides, et al. 1993). None of these cases indicated the presence of groundwater contamination boundaries. With the ongoing and expanding "pump and treat" system at the A-/M-Area (Figure 4-12), concentrations in the volatile organic compound plume are likely to

Contamination of groundwater in a drinking water aquifer has been found in only small area north of A-Area, in the northwest portion of the site. In the early 1980s found low concentrations of trichloroethylene (11.7 microgram per liter) in water from well (53A) completed to the Dublin-Midville Aquifer System (formerly called the Tus Formation) in M-Area. The monitors found the contamination only at 430 and 480 feet (146 meters) in this well, which is 670 feet (204 meters) deep. The well is screened from 387 feet (118 meters) to the bottom. DOE concluded that the contamination is migrating down the outside well casing from soils near the surface that are contaminated with trichloroethylene. This contaminated water enters the well through screens set in

Figure 4-12. Groundwater contamination at the Savannah River Site. System (Du Pont) above Primary Drinking Water Standards in cretaceous zone (Dublin-Midville) well MS which is approximately 3,500 feet west of well 53A and 1,500 feet north of A-Area (1993).

4.8.2.4 Groundwater Use. The McQueen Branch aquifer, which becomes shallower toward

the Fall Line, forms the base for most municipal and industrial water supplies in Aiken County. Toward the coast, in Allendale and Barnwell Counties, this aquifer exists at increasing depths. As a consequence, the shallower Gordon aquifer supplies some municipal, in agricultural users (Arnett et al. 1993).

DOE has identified 56 major municipal, industrial, and agricultural groundwater withdrawals within 20 miles (32 kilometers) of the center of the SRS (DOE 1987a). The total pumpage is about 49 billion liters (13 billion gallons) per year. The SRS withdraws approximately 3.7 billion gallons of groundwater per year for domestic and industrial use.

4.9 Ecological Resources

The U.S. Government acquired the SRS in 1951. At that time, the Site was approximately two-thirds forested and one-third cropland and pasture (Dukes 1984). At present, approximately 90 percent of the SRS is forested. An extensive forest management program conducted at the Savannah River Forest Station, which is operated by the U.S. Forest Service, has converted pastures and croplands to pine plantations. With the exception of the SRS production areas, natural succession has reclaimed previously disturbed areas. Table 4-14 lists other than the land used for nuclear reactors and support facilities.

The SRS is important to maintaining the biodiversity of the region. Satellite imagery shows a circle of wooded habitat within a matrix of cleared uplands and narrow forest corridors. The SRS provides more than 734 square kilometers (181,000 acres) of forest cover broken only by unpaved secondary roads, transmission line corridors in various

succession, and a few paved primary roads. Carolina bays, the Savannah River swamp relatively intact longleaf pine-wiregrass communities provide important contributio biodiversity of the SRS and of the entire region.

Table 4-14. Land cover of undeveloped areas on the Savannah River Site.

Land cover types	Square kilometer	Percent of total
Longleaf pine	150	20
Loblolly pine	258	35
Slash pine	117	16
Mixed pine/hardwood	23	3
Upland hardwood	20	3
Bottomland hardwood	117	16
Savannah River swamp	49	7
Total	734	100.0

a. Source: USDA (1991a).

b. To convert square kilometers to acres, multiply by 247.1.

F- and H-Areas, located near the center of the SRS and approximately 1.6 kilome southeast of Upper Three Runs Creek, are heavily industrialized with little natural remaining inside the fenced areas. These areas are dominated by buildings, paved p gravelled construction areas, and laydown yards. While some grassed areas occur ar administration buildings and some vegetation is present along the ditches that drai majority of the site contains no vegetation. Wildlife is absent except for occasio brachyrhynchos) and nesting barn swallows (*Hirundo rustica*) around the buildings.

Figure 2-3 shows the location of a representative host site at the SRS for pote fuel activities. F- and H-Areas (and developed areas immediately adjacent to them) spent nuclear fuel management facilities, while the undeveloped area south and east be used for the construction of new facilities that F- and H-Areas could not accomm undeveloped area, which was 98 percent cleared fields in 1951, is now almost comple the most part with 5- to 40-year-old upland pine stands that are actively managed b River Forest Station. Most of these stands are loblolly pine (*Pinus taeda*), but th of slash pine (*P. elliotii*), upland hardwoods (predominantly oaks and hickories), hardwoods (most commonly sweetgum, *Liquidambar styraciflua*, and yellow poplar, *Liri tulipifera*) associated with two small Carolina bays located south of H-Area. The a lies in the Fourmile Branch watershed, while the area east of H-Area is in the McQu tributary of Upper Three Runs Creek) watershed. Neither area is likely to contain endangered species or their habitats.

The general area of the representative host site contains suitable habitat for feral hogs as well as other faunal species common to the mixed pine/hardwood forest Carolina. Additional wildlife species found in the area include gray squirrel (*Sci squirrel* (*S. niger*), wild turkey (*Meleagris gallopovo*), cottontail rabbit (*Sylvilag* (*Procyon lotor*), bobcat (*Felix rufus*), and gray fox (*Urocyon cinereoargenteus*).

4.9.1 Terrestrial Ecology

The SRS is near the transition area between the oak-hickory-pine forest and the forest. As a consequence, species typical of both associations occur (Dukes 1984). farming, fire, soil features, and topography have strongly influenced existing SRS

A variety of vascular plant communities occurs in the upland areas (Dukes 1984) scrub oak communities occur on the drier, sandier areas. Longleaf pine (*Pinus palu* (*Quercus laevis*), bluejack oak (*Q. incana*), blackjack oak (*Q. marilandica*), and dwa (*Q. margaretta*) dominate these communities, which typically have understories of wi stricta) and huckleberry (*Vaccinium* sp.). Oak-hickory communities occur on more fe uplands; characteristic species are white oak (*Q. alba*), post oak (*Q. stellata*), so (*Q. falcata*), mockernut hickory (*Carya tomentosa*), pignut hickory (*C. glabra*), and an understory of sparkleberry (*Vaccinium arboreum*), holly (*Ilex* sp.), greenbriar (*S poison ivy* (*Rhus radicans*).

The removal of human residents in 1951 and the subsequent restoration of forest provided the wildlife of the SRS with excellent habitat. Furbearers such as gray f opossum (*Didelphis virginiana*), bobcat, beaver (*Castor canadensis*), and otter (*Lutr relatively common throughout the Site. Game species such as gray squirrel and fox white-tailed deer* (*Odocoileus virginianus*), cottontail rabbit, and wild turkey are Savannah River Ecology Laboratory has conducted numerous studies of reptile and amp

the wetlands and adjacent uplands of the SRS.

DOE allows carefully regulated public hunting for white-tailed deer and feral h on most of the SRS to reduce the incidence of animal/vehicle collisions and maintain populations within the carrying capacity of the range. SRS personnel monitor all animals from the Site for contamination before releasing them to the hunters (WSRC 1992a).

Before releasing any animal to a hunter, SRS technicians perform field analyses at the hunt site. In 1992, hunters collected 1,519 deer and 168 hogs. The maximum field measurement for deer was 22.4 picocuries per gram; the average was 6.4 picocuries (Arnett et al. 1993). For hogs, the maximum value was 22.9 picocuries per gram and 3.5 picocuries per gram. The field technicians determine estimated doses from consumption of venison and pork and make this information available to the hunters.

In 1992, the estimated maximum dose received by a hunter was 49 millirem per year for this unique hypothetical maximum dose, which was for a hunter who harvested eight hogs, is the assumption that the hunter consumed the entire edible portion of each additional hypothetical model involved a hunter whose total meat consumption for that year of SRS deer [81 kilograms (179 pounds) per year] (Arnett et al. 1993). Based on these low-probability assumptions and on the average concentration of cesium-137 (6.4 picocuries harvested on the SRS), the estimated potential maximum dose from this pathway is 26 percent of the annual 100-millirem DOE Derived Concentration Guide. Although a percentage of this hypothetical dose is probably due to cesium-137 from worldwide fallout, the estimated total contains this background cesium-137 for conservatism.

4.9.2 Wetlands

The SRS has extensive, widely distributed wetlands, most of which are associated with floodplains, creeks, and impoundments. In addition, approximately 200 Carolina bay sites (Shields et al. 1982; Schalles et al. 1989).

The southwestern SRS boundary adjoins the Savannah River for approximately 32 kilometers (20 miles). The river floodplain supports an extensive swamp, covering about 49 square miles (12,148 acres) of the Site; a natural levee separates the swamp from the river. This swamp existed in the late 1800s. At present, the swamp forest consists of second-growth bald cypress (*Taxodium distichum*), black gum (*Nyssa sylvatica*), and other hardwood species (Workman and McLeod 1990; USDA 1991a).

Five major streams drain the SRS and eventually flow into the Savannah River. These floodplains are characterized by bottomland hardwood forests or scrub-shrub wetlands in succession. Dominant species include red maple (*Acer rubrum*), box elder (*A. negundo*), water tupelo (*Nyssa aquatica*), sweetgum, and black willow (*Salix nigra*) (Workman and McLeod 1990).

Carolina bays are unique wetland features of the southeastern United States. These wetland habitats are dispersed throughout the uplands of the SRS. The approximately 200 bays exhibit extremely variable hydrology and a range of plant communities from herbaceous to forested wetlands (Shields et al. 1982; Schalles et al. 1989). SRS scientists have studied bays extensively, particularly in relation to the construction of the Defense Waste Management Facility (DWPF; SREL 1980).

4.9.3 Aquatic Ecology

The aquatic resources of the SRS have been the subject of intensive study for more than 30 years. Research has focused on the flora and fauna of the Savannah River and those portions of the river that drain the Site. Section 4.8.1.1 describes those portions of the Site where spent nuclear fuel management activities could affect. In addition, several monographs (Dahlberg and Scott 1971; Bennett and McFarlane 1983), the eight-volume Comprehensive Cooling Water Study (Du Pont 1987), and three EISs (DOE 1984; DOE 1987b; DOE 1990) evaluated operations of SRS production reactors describe the aquatic biota and aquatic resources of the SRS.

4.9.4 Threatened and Endangered Species

Threatened, Endangered, and Candidate Plant and Animal Species of the Savannah River (HNUS 1992b) describes threatened, endangered, and candidate plant and animal species known to occur or that might occur on the SRS. Table 4-15 lists these species.

The following Federally listed endangered animals are known to occur on the SRS Savannah River adjacent to the Site: the red-cockaded woodpecker (*Picoides borealis*), bald eagle (*Haliaeetus leucocephalus*), the wood stork (*Mycteria americana*), and the sturgeon (*Acipenser brevirostrum*) (HNUS 1992b). Researchers have found one Federal endangered plant species, the smooth coneflower (*Echinacea laevigata*), on the Site, **Table 4-15**. Threatened, endangered, and candidate plant and animal species of the

Common Name (Scientific Name)	Status
Animals	
Rafinesques (= Southeastern) big-eared bat (<i>Plecotus rafinesquii</i>)	FC2
Loggerhead Shrike (<i>Lanius ludovicianus</i>)	FC2
Bachman's sparrow (<i>Aimophila aestivalis</i>)	FC2
Carolina crawfish (= Gopher) frog (<i>Rana areolata capito</i>)	FC2
Southern hognose snake (<i>Heterodon simus</i>)	FC2
Northern pine snake (<i>Pituophis melanoleucus melanoleucus</i>)	FC2
Bald eagle (<i>Haliaeetus leucocephalus</i>)	E
Wood stork (<i>Mycteria americana</i>)	E
Red-cockaded woodpecker (<i>Picoides borealis</i>)	E
American alligator (<i>Alligator mississippiensis</i>)	T/SA
Shortnose sturgeon (<i>Acipenser brevirostrum</i>)	E
Plants	
Smooth coneflower (<i>Echinacea laevigata</i>)	E
Bog spice bush (<i>Lindera subcoriacea</i>)	FC2
Boykin's lobelia (<i>Lobelia boykinii</i>)	FC2
Loose watermilfoil (<i>Myriophyllum laxum</i>)	FC2
Nestronia (<i>Nestronia umbellula</i>)	FC2
Awed meadowbeauty (<i>Rhexia aristosa</i>)	FC2

Key: E = Federal endangered species.

T/SA = Threatened due to Similarity of Appearance.

FC2 = Under review (a candidate species) for listing by the Federal government listed Category 2 species, and several state listed species (Knox and Sharitz 1990) SRS is implementing strategies for the protection of these species.

F- and H-Areas and the representative host site contain no habitat suitable for Federally listed threatened or endangered species found on the SRS. The Southern wood stork feed and nest near wetlands, streams, and reservoirs, and thus would not host site, a densely forested upland area. Shortnose sturgeon, typically residents and estuaries, have never been collected in Fourmile Branch or any of the tributary River that drain the SRS.

Red-cockaded woodpeckers prefer open pine forests with mature trees (older than foraging and nesting. The pines of the undeveloped host site are 5 to 40 years old woodpeckers probably would not forage or nest in the area.

The Red-cockaded Woodpecker Management Standards and Guidelines, Savannah River (USDA 1991b) describes the SRS management strategy for the red-cockaded woodpecker. significant element of this management strategy is the conversion of slash (and some a designated red-cockaded woodpecker management area to longleaf pine, with a harvest 120 years.

4.10 Noise

The major noise sources at the SRS occur primarily in developed operational areas various facilities, equipment, and machines (e.g., cooling towers, transformers, steam vents, paging systems, construction and materials-handling equipment, and vehicle noise sources outside the operational areas consist primarily of vehicles and rail. Previous studies have assessed noise impacts of existing SRS operational activities (1991b; DOE 1990; DOE 1993a). These studies concluded that, because of the remote SRS operational areas, there are no known conditions associated with existing onsite adversely affect individuals at offsite locations. Some disturbance of wildlife at the SRS as a result of operational and construction activities.

Existing SRS-related noise sources of importance to the public are those resulting from transportation of people and materials to and from the Site. These sources include vehicles, helicopters, and freight trains. In addition, a portion of the air cargo using commercial air transport through the airports at Augusta, Georgia, and Columbia, South Carolina, are attributable to SRS operations.

The States of Georgia and South Carolina and the counties in which the SRS is located

established any regulations that specify acceptable community noise levels with the County. A provision of the Aiken County Nuisance Ordinance limits daytime and night frequency band (Aiken County 1991).

During a normal week in 1995, about 20,000 employees are likely to travel to the site in private vehicles from surrounding communities. Both government-owned and private vehicles deliver materials at the Site. Most private vehicles and trucks traveling to a day use South Carolina Highways (SC) 125 and 19. The contribution of SRS operation volumes along SC 125 and SC 19, especially during peak traffic periods, affects noise in the towns of New Ellenton and Jackson and the City of Aiken.

Noise measurements taken during 1989 and 1990 along SC 125 in the Town of Jackson point about 15 meters (50 feet) from the roadway indicate that the 1-hour equivalent traffic ranged from 48 to 72 decibels (A-weighted). The estimated day/night average along this route was 66 decibels for summer and 69 decibels for winter. Similarly, measurements along SC 19 in the town of New Ellenton at a point about 15 meters (50 feet) from the roadway indicate that the 1-hour equivalent sound level from traffic ranged from 53 to 67 decibels for summer and 68 decibels for winter (NUS 1990). Employment at the SRS has increased slightly since 1990, potentially causing small increases in traffic noise, especially during peak traffic periods (approximately between 6:30 and 8:30 a.m. and between 3:30 and 5:30 p.m., corresponding to major shift changes). Because some residences and at least two schools are within these routes, some annoyance to members of the public residing along these highways is based on the relationship between the day/night average sound level and the "percent exceedance" (Schultz 1978; Fidell et al. 1989; FICON 1992).

Noise sources from rail transport include diesel engines, wheel-track contact, and whistle-warnings at rail crossings.

4.11 Traffic and Transportation

4.11.1 Regional Infrastructure

The SRS is surrounded by a system of Interstate highways, U.S. highways, state highways, and railroads. The regional transportation networks service the four South Carolina counties (Allendale, Bamberg, and Barnwell) and two Georgia counties (Columbia and Richmond) about 90 percent of SRS commuter traffic (HNUS 1992a). Two major railroads - CSX Transportation and Norfolk Southern Corporation - also serve the SRS vicinity. Although barge traffic on the Savannah River, neither the SRS nor commercial shippers normally use barges. This section describes the regional transportation infrastructure.

4.11.1.1 Regional Roads. Two Interstate highways serve the SRS area. Interstate 20 (I-20)

I-20 provides a primary east-west corridor and I-520 links I-20 with parts of Augusta, Georgia. U.S. Highways 1 and 25 are principal north-south routes and U.S. 78 provides east-west. Several other highways - U.S. 221, U.S. 301, U.S. 321, and U.S. 601 - provide additional routes in the region.

Several state routes provide direct access to the SRS. Running northwest/southwest, SC 19 provides access to the Site from the north by SC 19, from the northeast by SC 39, and from the east by SC 64.

U.S. 278 bisects the northern part of the SRS and is available to public access. The SRS maintains barricades at site entries and exits on SC 125 to control public access, although it is generally open to unrestricted public travel. The public also has access to Road 1. All other site roads have restricted access.

4.11.1.2 Regional Railroads. Norfolk Southern serves Augusta and Savannah, Georgia, as

well as Columbia and Charleston, South Carolina. CSX serves the same locations and

4.11.2 SRS Infrastructure

The SRS transportation infrastructure consists of more than 143 miles (230 kilometers) of primary roads, 1,200 miles (1,931 kilometers) of unpaved secondary roads, and 103 kilometers of

(64 miles) of railroad track (WSRC 1993b). These roads and railroads provide various SRS facilities and to offsite transportation linkages. Figure 4-14 shows primary roadways and access points. Figure 4-15 shows the SRS railway system.

4.11.2.1 SRS Roads. Two major public highways traverse the Site: SC 125 and U.S. 278.

SC 125 connects Allendale, South Carolina, to Augusta, Georgia, by crossing the Site northwest-to-southeast direction. U.S. 278 also connects Augusta and Allendale, but approximately follows the northern and eastern SRS boundaries.

Figure 4-13. Regional transportation infrastructure. Figure 4-14. Major SRS roads from SC 125; three limited access from SC 19, SC 39, and SC 64; and two limited access areas of the administrative complex near the northern SRS boundary (A-Area).

In general, the primary SRS roadways are in good condition and are smooth and free of potholes. Typically, wide, firm shoulders border roads that are either straight or turns. Intersections are well marked for both traffic and safety identification and are cleared of trees and brush that might obstruct a driver's view of oncoming traffic. The side of the roadways offer protection at appropriate locations from dropoffs or other vehicles. In general, the roadways are lighted only at gate areas and near major facilities. There are two overpasses, one at the cloverleaf intersection of Roads 2 and C, and the other where Road C overpasses the CSX railroad tracks in the southern part of the Site. The 60 bridge has been inspected and evaluated for safe loading, with some bridges rated as high as 2 tons) under controlled conditions. The steepest roadway gradient is on Road C at the Upper Three Runs Creek, where the road drops more than 100 feet (30 meters) in about 0.4 kilometer). At the base of the dropoff is a bridge over the creek and an immediate road. This area presents a relatively hazardous roadway condition.

In general, heavy traffic occurs early in the morning and late in the afternoon as surrounding communities commute to and from the Site. During working hours, official logging trucks constitute most of the traffic. At any time, as many as 60 logging trucks might be operating on the Site, with an annual average of about 25 trucks. Table 4-16 provides data on traffic counts for various roads and access points around the Site.

4.11.2.2 SRS Railroads. Railroads on the Site include both CSX tracks and SRS rolling stock and tracks.

Two routes of the CSX distribution system run through the Site: one from Florence, South Carolina, and Augusta, Georgia, and a line between Yemassee, South Carolina, and Augusta, Georgia. The two lines join on the Site just south of Lake (Figure 4-15). CSX discontinued service on the line from the SRS junction to Florence.

The 64 miles (103 kilometers) of SRS railroads are well maintained. The rails are in good condition, and the track lines are clear of vegetation and debris. Signaling is provided on both sides. Intersections of railroads and roadways are marked by flashing lights where appropriate.

Table 4-16. SRS traffic counts - major roads.

Measurement point	Date	Direction	Day Total	Peak	Peak time	Average speed (mph)
Road 2 between Roads C and D	2-23-93	East	3,031	800	1530	47
	4-21-93	West	3,075	864	0630	NA
Road 4 between Roads E and C	12-9-92	East	1,624	352	1530	NA
	12-9-92	West	1,553	306	0615	NA
Road 8 at Pond C	2-23-92	East	634	274	1530	58
	2-23-92	West	662	331	0615	56
Road C between landfill and R12-16-92	12-16-92	North	6,931	2,435	1530	53
	12-16-92	South	6,873	2,701	0630	58
Road C north of Road 7	1-20-93	North	742	288	0630	53
	1-20-93	South	763	223	1530	54
Road D	9-29-93	North	1,779	218	1500	43
	9-29-93	South	1,813	220	0845	52
Road E at E-Area	8-25-93	North	3,099	669	1530	35
	8-25-93	South	3,054	804	0630	38
Road F at Upper Three Runs Cr	2-2-93	North	3,239	1,438	1530	53
	2-2-93	South	3,192	1,483	0630	51

H-Area Exit 12-2-92 Outbound 2,181 406 1530 12
 a. Source: Swygert (1993).
 b. Number of vehicles in peak hour.
 c. Start of peak hour.
 d. mph = miles per hour; to convert to kilometers per hour multiply by 1.6093.
 e. NA = data not available.

The SRS rail classification yard is east of P-Reactor. This eight-track facility handles rail cars. Deliveries of SRS shipments occur at two onsite rail stations at the F-Area and Dunbarton. From these stations, an SRS engine moves the railcars to the appropriate facility. The Ellenton station, which is on the main Augusta-Yemassee line, is the main point. The Dunbarton station, which is on the discontinued portion of the Augusta-Yemassee line, receives less use.

4.12 Occupational and Public Radiological Health and Safety

The sources of radiation exposure to individuals consist of natural background cosmic, terrestrial, and internal body sources; radiation from medical diagnostic and therapeutic practices; and radiation from manmade sources, including consumer and industrial product facilities, and weapons test fallout.

All radiation doses discussed in this document are effective dose equivalents (equivalents weighted for biological effect and summed to yield a whole-body dose equivalent same risk as irradiation of individual organs) as defined by the International Commission on Radiological Protection, Publication 26 (ICRP 1977), unless specifically identified (thyroid dose, bone dose).

Natural background radiation contributes about 83 percent of the annual dose of radiation received by an average member of the population within 50 miles (80 kilometers) of the Site. On national averages, medical exposure accounts for 14 percent of the annual dose, doses from weapons test fallout, consumer and industrial products, and air travel account for approximately 3 percent (Arnett et al. 1993).

4.12.1 Occupational Health and Safety

SRS maintains a network of air monitoring stations on and around the Site to determine concentrations of radioactive particulates and aerosols in the air (Arnett et al. 1993). Table 4-18 lists average and maximum concentrations of tritium in atmospheric moisture for the F- and H-Areas, SRS boundary, and background monitoring locations.

Gamma radiation levels measured by thermoluminescent dosimeters in 1992 at the Site perimeters averaged 70 and 74 millirem per year, respectively. Gamma radiation levels, background (terrestrial and cosmic) radiation, measured at the Site perimeter in 1992 averaged a dose of 35 millirem per year (Arnett et al. 1993).

Table 4-17. Radioactivity in air at the Savannah River Site and vicinity (pCi/m³).

Location	Gross Alpha	Nonvolatile Beta	SR-89,90b
F-Area			
Average	1.80x10 ⁻³	1.94x10 ⁻²	0.62x10 ⁻⁴
Maximum	3.55x10 ⁻³	5.56x10 ⁻²	6.02x10 ⁻⁴
H-Area			
Average	1.80x10 ⁻³	1.93x10 ⁻²	2.69x10 ⁻⁴
Maximum	4.24x10 ⁻³	5.39x10 ⁻²	2.83x10 ⁻³
Site perimeter			
Average	1.80x10 ⁻³	2.30x10 ⁻²	0.13x10 ⁻⁴
Maximum	4.04x10 ⁻²	4.95x10 ⁻²	4.54x10 ⁻⁴
Background (100-mile radius)			
Average	1.67x10 ⁻³	1.73x10 ⁻²	0.49x10 ⁻⁴
Maximum	3.83x10 ⁻³	4.37x10 ⁻²	6.89x10 ⁻⁴

a. Arnett et al. (1993).

b. Monthly composite.

Table 4-18. Tritium measured in air at the Savannah River Site (pCi/cc).

Location	Average	Maximum
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F-Area	8.67x10 ⁻⁵	2.98x10 ⁻⁴
H-Area	0.99x10 ⁻³	6.77x10 ⁻³
Site boundary	2.65x10 ⁻⁵	1.03x10 ⁻⁴
Background (100-mile radius)	8.32x10 ⁻⁶	1.08x10 ⁻⁵

a. Arnett (1993).

Soil samples from uncultivated areas provide a measure of the quantity of particulate deposited from the atmosphere. Table 4-19 lists maximum measurements of radionuclides for 1992 at F- and H-Areas, SRS boundary, and background [100-mile (160-kilometer)-monitoring locations. The SRS measured elevated concentrations of plutonium-238 and around F- and H-Areas, reflecting releases from these areas. From 1955 through 1992 atmospheric plutonium releases from the F- and H-Areas were approximately 0.7 curies of plutonium-238 and 3 curies of plutonium-239 (Arnett et al. 1992; 1993).

The SRS workers investigated for purposes of assessing occupational radiation exposure the group of involved workers assigned to F- and H-Area facilities. The investigation facilities because they process materials with radiological characteristics similar to the SRS.

Table 4-19. Maximum radioactivity concentrations in soil at the Savannah River Site

Location	Sr-90	Cs-137	Pu-238	Pu-239
F-Area	2.16x10 ⁻²	7.19x10 ⁻¹	4.03x10 ⁻¹	5.31x10 ⁻¹
H-Area	2.89x10 ⁻²	8.22x10 ⁻¹	2.13x10 ⁻²	5.54x10 ⁻²
Site perimeter	(b)	4.84x10 ⁻¹	2.19x10 ⁻³	1.36x10 ⁻²
Background (100-mile radius)	1.46x10 ⁻²	(b)	2.34x10 ⁻⁴	1.93x10 ⁻²

a. Arnett et al. (1992).

b. None detected.

analyzed in this EIS. The dosimetry results for these two involved worker groups are because they depict occupational impacts that are directly relevant to each alternative investigation selected two dosimetry periods of record for this analysis: 1983 - 1987 and 1988 - 1992. The earlier 5-year period included times when materials processing was occurring at a rate accelerated in comparison with recent years. The later period includes processing activities that reflect near-term DOE mission initiatives.

Tables 4-20 and 4-21 list the involved worker dosimetry data for 1983 - 1987 and 1988 - 1992, respectively. This analysis adapted these data from monitoring data statistics (Matheny 1994b) for operations, maintenance, laboratory, and health protection personnel at the F- and H-Area Canyons and the associated B-Line facilities. The calculated individual fatal cancer attributable to each facility's collective worker dose are approximately 0.01 and 0.02, respectively. Similarly, the highest calculated probabilities attributable to average individual worker doses are approximately 0.01 and 0.02, respectively. The analysis estimated these health effects using risk coefficients (DOE 1993).

4.12.2 Public Health and Safety

Table 4-22 summarizes the major sources of exposure for the population within 50 miles (80 kilometers) of the SRS and for the Savannah River water-consuming population in Jasper Counties, South Carolina, and Port Wentworth, Georgia. Most of the sources, background dose and medical dose, are independent of the presence of the SRS.

Atmospheric releases of radioactive material to the environment from SRS operations in 1992 resulted in an average dose of approximately 0.02 millirem per year to individuals living near the SRS.

Table 4-20. Annual involved worker doses, 1983 - 1987.

Facility	Average Worker Dose (rem)	Total Collective Worker Dose (person-rem)
H-Canyon	0.41	36.28
HB-Line	0.49	21.84
F-Canyon	0.48	87.25
FB-Line	0.74	124.68

Facilities Average 0.53

Facilities Total NA

NA

270.05

NA = Not applicable.

Table 4-21. Annual involved worker doses, 1993.

Facility	Average Worker Dose (rem)	Total Collective Worker Dose (person-rem)
H-Canyon	0.17	11.07

HB-Line	0.24	21.97
F-Canyon	0.22	9.16
FB-Line	0.24	51.16
Facilities Average	0.22	NA
Facilities Total	NA	93.36

NA = Not applicable.

Table 4-22. Major sources of radiation exposure to the public in the vicinity of the Site.

Source of Exposure	Dose to average individual (mrem/yr)	P
Natural background radiation	315	8
Medical radiation	54	1
Consumer and industrial products, fallout, air travel	10	3
Savannah River Site operations	0.22	0.0
Grand Total	380	1

a. Arnett et al. (1993).

(80-kilometer)-radius population. The collective effective dose equivalent due to from 1992 SRS operations to the population of 620,100 within 50 miles (80 kilometer approximately 6.4 person-rem per year. Atmospheric releases of tritium accounted for 90 percent of the offsite population dose; tritium is the only radionuclide of SRS routinely detected in offsite air (Cummins et al. 1991; Arnett et al. 1992, 1993). average annual atmospheric tritium concentrations in the vicinity of SRS for the year 1992.

Table 4-23. Average atmospheric tritium concentrations in the vicinity of the Savannah River Site (pCi/m³).

Location	1992	1991	1990
Onsite	340	250	430
Site perimeter	27	21	32
25-mile radius	11	11	12
100-mile radius	8.3	8.5	8.8

a. Arnett et al. (1993).

From 1990 to 1992, the calculated maximum individual average annual dose from releases to a hypothetical individual residing at the SRS boundary was 0.12 millirem (Cummins et al. 1991; Arnett et al. 1992, 1993).

In general, liquid releases of tritium account for more than 99 percent of the introduced into the Savannah River from SRS activities (Arnett et al. 1993). The collective annual dose to the maximally exposed individual resulting from liquid releases from 0.21 millirem (Cummins et al. 1991; Arnett et al. 1992, 1993). From 1990 to 1992, 1 radioactive material to the environment from SRS operations resulted in an average millirem per year and 0.05 millirem per year to downstream consumers of drinking water at Beaufort-Jasper and Port Wentworth water treatment plants, respectively. These doses to Beaufort-Jasper river-water-consuming population of about 51,000 and the current Port Wentworth river-water-consuming population of about 20,000 would yield a collective effective dose to these populations of approximately 3 person-rem per year (Cummins et al. 1991; Arnett et al. 1993).

The SRS analyzes samples from other environmental media that onsite releases might provide a pathway for radiation exposure to the public and Site employee samples of milk, food products, drinking water, wildlife, rainwater, soil, sediment. The 1992 SRS Environmental Report (Arnett et al. 1993) describes the sampling program locations, and monitoring results for each of these media.

Major nuclear facilities within 50 miles (80 kilometers) of the SRS include a landfill site operated by Chem-Nuclear Systems, Inc., near the eastern SRS boundary in South Carolina, and the Georgia Power Company Alvin W. Vogtle Electric Generating Plant, located on the Savannah River from the SRS. Plant Vogtle began commercial operation in 1987, and is controlled to meet U.S. Nuclear Regulatory Commission requirements.

4.13 Utilities and Energy

This section describes SRS electricity consumption, water consumption, fuel usage, and industrial wastewater treatment. Table 4-24 contains information on the current utility items at SRS.

Table 4-24. Current capacities and usage of utilities and energy at SRS.

ELECTRICITY

Consumption	659,000 megawatt hour
Load	75 megavolt-amperes
Peak Demand	130 megavolt-amperes
Capacity	340 megavolt-amperes

WATER

Groundwater usage	12,490 million liters
Surface water usage (cooling)	75,700 million liters

FUEL

Oil	28.4 million liters (
Coal	210,000 metric tons (
Gasoline	4.7 million liters (1

WASTEWATER

Domestic capacity	3.97 million liters (
Domestic load	1.89 million liters (
Industrial capacity ^{a,b}	1.64 million liters (
Industrial load ^a	44,000 liters (11,580

a. F/H Effluent Treatment Facility only.

b. Design capacity; permitted capacity is about 67 percent of this value.

4.13.1 Electricity

The SRS purchases electric power from the South Carolina Electric and Gas Company through three purchased power-line interconnects to the SRS transmission grid. The annual power consumption for the SRS was approximately 659,000 megawatt-hours. The was 75 megavolt-amperes and the peak demand was about 130 megavolt-amperes. South Electric and Gas sources can supply as much as 340 megavolt-amperes to the SRS grid direct connections. The SRS generating station in D-Area can produce an additional 80 megavolt-amperes capacity, although that plant currently produces only process s transmission grid that would provide power to any spent nuclear fuel facilities con 145 kilometers (90 miles) of 115-kilovolt lines, four switching stations, and 15 su service to all major production areas provides parallel redundant capacity to ensur availability and reliability (WSRC 1993c).

4.13.2 Water Consumption

Groundwater from a deep confined aquifer supplies domestic and process water fo through approximately 100 production wells. The aquifer system sustains single wel 10.2 million liters (2.7 million gallons) per day. Current usage from this source liters (3.7 billion gallons) per year (DOE 1990). The SRS withdraws cooling water from the Savannah River at an annual rate of about 75.7 billion liters (20 billion (WSRC 1993c).

4.13.3 Fuel Consumption

Fuels consumed at SRS include oil, coal, and gasoline. SRS facilities and equi approximately 28.4 million liters (7.5 million gallons) of oil each year. This tot No. 6 oil, and No. 2 oil. The SRS burns coal and some waste oils in the D-Area pow produce steam for Site facilities. Current coal usage is about 208,655 metric tons year. SRS vehicles use approximately 4.7 million liters (1.24 million gallons) of Under the provisions of the Energy Policy Act of 1992, natural gas will replace gas within the next 10 years. At that time, SRS usage of natural gas would be approxim cubic meters (429 million cubic feet) per year. At present, the SRS consumes no na (WSRC 1993c).

4.13.4 Wastewater Treatment

By 1995, the SRS Centralized Sanitary Wastewater Treatment Facility will proces

domestic effluent on the Site. This centrally located facility has a design capacity (1.05 million gallons) per day. Once operational, the plant will use about 50 percent. In addition, five smaller sanitary treatment plants serve more remote areas of the spent nuclear fuel management would use the centralized facility.

The F/H Effluent Treatment Facility (ETF), which decontaminates routine process accidental radioactive releases from operations, treats industrial wastewater in the area where the spent fuel management activities would occur.

Effluent Treatment Facility process operations performed on the waste liquids include neutralization (adjusts pH), submicron filtration (removes suspended solids), active absorption (removes dissolved organic chemicals), reverse osmosis membrane deionization (removes salts), ion exchange (removes heavy metals), and evaporation (separates radionuclide condensate). This facility releases two different streams. The treated water stream is analyzed to ensure that it meets discharge requirements and then is released to Upp Creek via a permitted outfall. The waste concentrate (i.e., bottoms from the evaporation) is transferred to the H-Area waste tank farm for treatment and disposal in the Z-Area.

The design capacity for the Effluent Treatment Facility is approximately 600 million gallons per year. The maximum permitted treatment capacity is about 400 million (105.7 million gallons) per year. Under normal operating conditions, the facility treats 16,000 cubic meters (26 million gallons) of liquid waste per year (WSRC 1993d).

The influent water load to processes discharging to the permitted outfall includes 54 million liters (54 million gallons) per year of F-Area Canyon process wastewater, 132 million (32 million gallons) per year of H-Area Canyon process wastewater, 34 million liter gallons) per year from the F-Area collection and retention basins, 34 million liter gallons) per year from the H-Area collection and retention basins, 68 million liters (18 million) of Effluent Treatment Facility acid, caustic, flush and rinse water, and similar wastewater from SRS facilities.

4.14 Materials and Waste Management

The historic national defense mission of the SRS has resulted in the generation of radioactive waste, transuranic waste, low-level radioactive waste (low-activity and hazardous waste, mixed waste (radioactive and hazardous combined), and sanitary waste (nonhazardous, nonradioactive solid waste). This section discusses the treatment, management, and disposal of waste at the SRS. Section 4.13 discusses domestic and industrial wastewater treatment.

DOE is preparing an environmental impact statement on Waste Management at the Savannah River Site (DOE 1995). The purpose of the EIS is to provide a basis for DOE to select a strategic approach to managing present and future SRS waste generated as a result of operations, environmental restoration activities, transition from nuclear production and decontamination and decommissioning programs. The Waste Management EIS will support project-level decisions on the operation of specific treatment, storage, and disposal near term (10 years or less). In addition, the EIS will provide a baseline for waste management activities and a basis for the evaluation of the specific waste management alternatives. The Waste Management EIS will not include management of spent nuclear fuel which is discussed in this document.

DOE treats and stores waste generated from onsite operations in waste management facilities located primarily in E-, F-, H-, N-, S-, and Z-Areas (Figure 4-16). These facilities include the H-Area Effluent Treatment Facility, the High-Level Waste Tank Farms, and the Solid Waste Facility. The Defense Waste Processing Facility is nearly operational and the Consolidated Incineration Facility is under construction. The SRS places sanitary and inert waste in Sanitary Landfill and the Burma Road Landfill, respectively.

DOE continues to reduce the amount of waste generated and disposed of at the SRS through waste minimization and treatment programs. DOE accomplishes waste minimization by reducing the volume, toxicity, or mobility of waste before storing or disposing of it. These activities include more intensive surveying, waste segregation, and use of administrative and engineering controls.

The waste that DOE presently stores on the SRS includes high-level, transuranic waste, mixed waste and some low-level waste. The Site stores high-level waste in underground storage tanks that have received South Carolina Department of Health and Environmental Control in accordance with wastewater permits, and manages them in accordance with Clean Water Act, Resource Conservation and Recovery Act, and DOE requirements. The SRS stores transuranic mixed waste on storage pads in accordance with South Carolina Department of Health and Environmental Control requirements and DOE Orders. Hazardous and mixed waste is placed in permitted or approved storage units.

Figure 4-16. Waste management facilities at the Savannah River Site. storage in

storage buildings.

Figure 4-17 shows the high-level liquid waste management process at the SRS. F shows the process for handling all other forms of solid waste at the Site.

Table 4-25 is a forecast of annual waste generation for all waste forms except high-level waste (WSRC 1994c). The volumes listed do not include waste related to and decommissioning because DOE has not yet completed the planning of these activities. Section 5.14 discusses potential consequences of spent nuclear fuel activities as alternative interim storage and treatment scenarios.

4.14.1 High-Level Waste

The SRS generated high-level waste from the recovery of nuclear materials from target processing in the F- and H-Areas. It is stored in 50 underground tanks. The other radioactive waste effluents (primarily low-level radioactive waste such as aqueous including purge water from storage basins for irradiated reactor fuel or fuel element waste is stored to permit the decay of short-lived radionuclides and allow separation from soluble waste. Evaporators concentrate soluble waste to reduce original volume immobilize it as crystallized salt by successive evaporations of the liquid supernatant the evaporator overheads in cesium removal columns before transferring them to the Effluent Treatment Facility. The SRS processes the sludge and salt to prepare them for the Defense Waste Processing Facility (high-level waste), when it becomes operational at the Z-Area Saltstone Facility (low-level waste). DOE has prepared a Supplemental Defense Waste Processing Facility operations (DOE 1994d).

By December 31, 1991, DOE had stored approximately 127.9 million liters (33.8 million cubic feet) of high-level radioactive waste on the Site. Estimates of current tank capacity and forecasts should be available in 1995. In general, however, due to a number of factors important of which has been the extended outage of the evaporators, the estimated inventory in the high-level tanks is greater than 90 percent of existing capacity (WSRC 1994d). DOE is constructing a replacement high-level waste tank evaporator to augment or replace existing evaporators.

Figure 4-17. Flow diagram for high-level radioactive waste. Figure 4-18. Flow

Waste Type	FY94	FY95	FY96
Transuranic	670	860	760
Low-Level			
Low-Activity	21,350	17,680	17,970
Intermediate-Level	940	580	740
Hazardous	140	130	100
Mixed	120	130	110

a. Source: WSRC (1994c).

b. To convert cubic meters to cubic feet, multiply by 35.314.

4.14.2 Transuranic Waste

At present, DOE uses three methods of retrievable storage for transuranic waste at the time of generation. Transuranic waste generated before 1974 is buried in approximately 120 belowgrade concrete culverts in the Solid Waste Disposal Facility. Transuranic waste from 1974 to 1985 is stored on five concrete pads and one asphalt pad that have been approximately 1.2 meters (4 feet) of native soil. DOE stores waste generated since 1985 on 13 additional concrete pads that are not covered with soil. Pads 1 through 17 are in Status approved by the South Carolina Department of Health and Environmental Control. Pads 18 through 19, which are not required to have interim status, to manage nonhazardous wastes only.

The SRS stores wastes containing 10 to 100 nanocuries per gram of transuranic material. Transuranic waste until it can complete Site-specific radiological performance assessments provide disposal limits for transuranic isotopes. SRS transuranic waste inventories include both transuranic waste and the 10- to 100-nanocuries-per-gram transuranic waste.

At the end of 1993, the SRS had approximately 9,900 cubic meters (350,000 cubic feet) of transuranic waste in storage (WSRC 1994e). Based on the 1994-to-1996 average annual waste forecast, the Site generates approximately 760 cubic meters (27,000 cubic feet) of waste annually. Transuranic mixed waste (transuranic and hazardous combined) accounts for approximately 110 cubic meters (3,900 cubic feet) of this volume (WSRC 1994c). DOE is providing available storage space for transuranic mixed waste to alleviate any storage capacity constraints.

4.14.3 Mixed Low-Level Waste

The SRS mixed waste program consists primarily of providing safe storage until treatment and disposal facilities are available. The current volume of mixed low-level waste at the Site is 1,700 cubic meters (60,000 cubic feet) (WSRC 1994e). Based on the 1994-to-1996 average generation forecast, the Site generates approximately 118 cubic meters (4,170 cubic feet) of low-level waste annually (WSRC 1994c). DOE is evaluating available storage space to determine when the SRS will exceed its capacity. However, DOE is constructing a Consolidated Facility in H-Area, which will treat mixed, hazardous, and low-level waste. When it is operational, existing inventory will be reduced and more storage capacity will become available.

4.14.4 Low-Level Waste

The SRS packages low-level waste for disposal on the Site in accordance with the waste's estimated surface dose rate. The Site places low-activity waste in carbonaceous waste deposits in an Engineered Low-Level Trench (ELLT). The trenches are several acres and 6 meters (20 feet) deep and have sloped sides and floor, allowing drainage to a collection system. When the trenches are full, DOE backfills and covers them with at least 1.8 meters of soil. The Site packages intermediate-level wastes according to the waste form and disposes of them in trenches. DOE will store long-lived wastes, such as resins, until the Long-Lived Waste Building, currently under construction, becomes operational. This building will provide space for DOE to develop treatment and disposal technologies.

The SRS is developing a new disposal facility, known as the E-Area Vault (EAV). The vault will include vaults for low-activity waste, intermediate-level non-tritium waste, and tritium waste.

Based on the 1994-to-1996 average annual generation forecast, the Site generates 19,000 cubic meters (671,400 cubic feet) of low-activity waste and 750 cubic meters (26,500 cubic feet) of intermediate-level waste annually. DOE expects that the Consolidated Incineration Facility will begin operations by the second quarter of Fiscal Year 1996; this facility will be capable of annually processing as much as 15,850 cubic meters (560,000 cubic feet) of boxed waste and approximately 186 cubic meters (6,600 cubic feet) of hazardous and mixed waste.

4.14.5 Hazardous Waste

DOE stores hazardous wastes generated at various SRS facilities in buildings in the N-Areas, and on the Solid Waste Storage Pads. The Resource Conservation and Recovery Act regulates these wastes.

The inventory of hazardous waste in storage at the SRS is about 1.6 million kilograms (3,500,000 pounds), occupying a volume of about 2,430 cubic meters (86,000 cubic feet) (WSRC 1994e). Based on the 1994-to-1996 average annual generation rate forecast, the Site generates approximately 124 cubic meters (4,370 cubic feet) of hazardous waste annually (WSRC 1994c).

4.14.6 Sanitary Waste

The SRS disposes of most of its solid sanitary waste in onsite landfills, the most of which began operation in 1985. Current disposal operations include the Interim Sanitary Landfill. Thirty trucks per work day arrive at this facility carrying approximately 18,125 kilograms of waste that, after compaction, occupies approximately 115 cubic meters (150 cubic feet) of space. The recent implementation of SRS paper and aluminum can recycling programs and the removal of office waste off the Site in a commercial landfill has increased the projected life of the landfill to the fourth quarter of 1996 (WSRC 1994e).

DOE also maintains an inert material landfill on the Site near Burma Road. This landfill is used for demolition and construction debris. DOE is evaluating the construction of a new Solid Waste Landfill or the use of a commercial landfill.

4.14.7 Hazardous Materials

The SRS 1993 Tier II emergency and hazardous chemical inventory lists 205 reports of hazardous materials.

substances present on the Site in excess of the 10,000-pound (4,536-kilogram) threshold (WSRC 1994f). The number and the total weight of any hazardous chemicals used on site daily in response to use. The annual Superfund Amendments and Reauthorization Act for the SRS include listings of hazardous materials used or stored on the Site during

5. ENVIRONMENTAL CONSEQUENCES

5.1 Overview

This chapter discusses the potential environmental consequences for each spent management alternative described in Chapter 3. The representative host site locations in Chapter 2, are the F- and H-Areas and an undeveloped site close to H-Area. These sites are representative of available areas that could support spent fuel management missions. Based on facility characteristics, this chapter analyzes representative consequences in terms of attributes of the potential host areas and the Savannah River Site (SRS) at large, in Chapter 4. Table 3-2 compares the environmental consequences of each alternative. Impacts associated with the construction and operation of a Navy Expanded Core Facility are discussed in this chapter, but are included in Appendix D of Volume 1 of this Environmental Impact

5.2 Land Use

Overall environmental impacts on land use by any of the alternatives would be small. The U.S. Department of Energy (DOE) would construct most new facilities in F- and H-Areas already dedicated to industrial use and which previous activities have disturbed. For the undeveloped representative host site near H-Area would probably be necessary on construction of a dry storage vault.

The Centralization Alternative (Alternative 5), under which DOE would transfer spent fuel to the SRS, would result in the greatest changes in land use. Under this alternative, DOE would dedicate between 70 and 100 acres (0.3 and 0.4 square kilometer) for use in spent fuel management; the exact location and size of the area affected would depend on whether DOE uses the wet storage, dry storage, or processing option. Of this affected area, approximately 100 acres (0.4 square kilometer) would change from managed pine forest to industrial use.

DOE would retain under its control any lands supporting the spent nuclear fuel management program for the life of the project. No alternative would require the acquisition of additional land.

5.3 Socioeconomics

Socioeconomic consequences resulting from the implementation of any of the alternatives relate primarily to changes in employment within the region of influence (ROI). DOE conducted an analysis in the following section on estimated employment and population data for the SRS region. For the nuclear fuel alternative, as listed in Table 5-1. The population within the region is estimated to be approximately 462,000. The labor force will be about 257,000 people and about 242,000 will be employed.

DOE expects the employment level at the Site to decline from about 20,000 (in 1994) to 15,800 (in 2004) as the SRS mission is redefined. This anticipated decline would be offset by the jobs created by the spent nuclear fuel management activities. Therefore, no alternative would require additional operations employees because the SRS could fill positions through the reassignment of existing workers. Consequently, this analysis does not estimate employment impacts from construction activities. Given the natural variation in construction employment levels, the analysis could not accurately determine the reassignment of construction workers. As a result, this assessment analyzed the maximum potential employment. It assumes that all construction employment would represent new jobs that in-migrating workers would fill.

DOE estimated total employment impacts using the Regional Input-Output Modeling technique developed by the U.S. Bureau of Economic Analysis for the SRS region of influence. This analysis also analyzed changes in population based on historic data that indicate that 90 people live in the six-county region.

5.3.1 Potential Impacts

Table 5-1 lists direct increases in construction employment for each alternative corresponding change in population. As listed, potential impacts to socioeconomic smallest under Alternative 1 (No Action) and would be greatest under Option 5b (Cen Storage). Therefore, Option 5b provides the bounding case for maximum potential im socioeconomic resources.

Table 5-1. Direct construction employment and total population changes by alternat

Alternative	1995a	1996a	1997a	1998a	1999a	2000	2001
Alternative 1-	50	50	50	50	50	50	50
Employment	200	150	150	100	100	100	100
Population							
Option 2a-	50	50	50	50	50	200	400
Employment	200	150	150	100	100	850	1,550
Population							
Option 2b-	50	50	50	50	50	200	400
Employment	100	150	150	100	100	850	1,550
Population							
Option 2c-	50	50	50	50	50	200	350
Employment	200	150	150	100	100	700	1,350
Population							
Option 3a-	50	50	50	50	50	200	400
Employment	200	150	150	100	100	850	1,550
Population							
Option 3b-	50	50	50	50	50	200	400
Employment	200	150	150	100	100	800	1,600
Population							
Option 3c-	50	50	50	50	50	200	350
Employment	200	150	150	100	100	700	1,350
Population							
Option 4a-	50	50	50	50	50	200	400
Employment	200	150	150	100	100	800	1,600
Population							
Option 4b-	50	50	50	50	50	200	400
Employment	200	150	150	100	100	800	1,600
Population							
Option 4c-	50	50	50	50	50	200	350
Employment	200	150	150	100	100	700	1,350
Population							
Option 4d-	50	50	50	50	50	300	500
Employment	200	200	150	150	150	1,100	1,900
Population							
Option 4e-	50	50	50	50	50	250	500
Employment	200	200	150	150	150	1,000	2,000
Population							
Option 4f-	50	50	50	50	50	200	450
Employment	200	200	150	150	150	850	1,700
Population							
Option 4g-	50	50	50	50	50	100	150
Employment	200	150	150	100	100	250	500
Population							
Alternative	1995a	1996a	1997a	1998a	1999a	2000	2001
Option 5a-	50	50	50	50	50	900	1,750
Employment	200	150	150	100	100	3,500	6,800
Population							
Option 5b-	50	50	50	50	50	1,000	1,900
Employment	200	150	150	100	100	3,850	7,450
Population							
Option 5c-	50	50	50	50	50	900	1,750
Employment	200	150	150	100	100	3,500	6,800
Population							

Option 5d- Employment Population	50 200	50 150	50 150	50 100	50 100	100 250	150 500
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a. Construction is related to renovation of reactor basin and Receiving Basin for Table 5-2 lists indirect employment and corresponding population changes associated with construction phase activities under Option 5b. As listed, the number of full-time jobs required to support the implementation of this option from 1995 to 2004 would range from approximately 50 to 2,700. When added to the indirect employment of 1,600 jobs in 2002, the total employment impact in the region would be approximately 4,300 employees. **Table 5-2.** Estimated increases in employment and population related to construction under Option 5b, from 1995 to 2004. ROI refers to the six-county region of influence.

Factor	1995	1996	1997	1998	1999	2000
Direct employment	50	50	50	50	50	1,000
Secondary employment	30	30	30	30	30	600
Total employment change	80	80	80	80	80	1,600
% Change in ROI labor force	0.03	0.03	0.03	0.03	0.03	0.54
% Change in ROI employment	0.03	0.03	0.03	0.03	0.03	0.57
Population change (in region)	200	150	150	100	100	3,850
% Change in ROI population	0.04	0.03	0.03	0.02	0.02	0.81

Assuming in-migrating workers filled all jobs, the regional labor force and employment would increase by 1.4 percent and 1.5 percent, respectively. These changes would be temporary and have an adverse impact on the region. After 2004, employment would gradually decline to a constant level of about 50 jobs.

Based on historic data, approximately 90 percent of new employees would live within the six-county region of influence. Assuming each new employee represented one household, there would be approximately 10,550 additional people in the peak year (2002). These changes would be temporary and would represent an estimate of increase in baseline population levels. Given this minor change in population, DOE expects impacts on the demand for community resources and services such as housing, schools, health care, and fire protection to be negligible.

Because all the other alternatives would require fewer employees, they would require fewer changes than those listed in Table 5-2, and would have no adverse impacts on socioeconomic resources in the region of influence.

5.4 Cultural Resources

A Programmatic Memorandum of Agreement (SRARP 1989) between the DOE Savannah River Operations Office, the South Carolina State Historic Preservation Office, and the Aiken County Historic Preservation, ratified on August 24, 1990, is the instrument for the management of cultural resources at the SRS. DOE uses this memorandum to identify cultural resources, assess eligibility for the National Register of Historic Places, and develop mitigation measures in consultation with the State Historic Preservation Officer. DOE would implement the terms of the memorandum for all activities needed to support spent nuclear fuel management.

The potential for adverse impacts on cultural resources would be smallest under the No Action alternative and would be greatest under Alternative 5 (Centralization). Any facilities constructed in F- and H-Areas, north of Road E (Alternatives 1-5), would be in Zones 2 and 3. Section 4.4 describes these zones. The undeveloped representative area east of H-Area (Alternative 5) is in Sensitivity Zone 3. Although there are no known sites in the area, it has never been surveyed. Surveying being conducted near F-Area Road C and west of Road 4 along Upper Three Runs Creek has recorded some historic prehistoric sites. However, DOE expects no impacts in F- and H-Areas due to their industrial development. Until DOE has determined the precise locations of facilities for any of the alternatives, it cannot predict impacts on cultural resources in the undeveloped area (Sassaman 1994). However, DOE would mitigate, through avoidance or removal, impact on potentially significant resources that future site surveys might discover.

5.5 Aesthetic and Scenic Resources

None of the alternatives for spent nuclear fuel management at the SRS would have consequences on scenic resources or aesthetics. Most new construction would be in both of which are already dedicated to industrial use. New construction on the und which would occur primarily under Alternative 5, would be adjacent to H-Area in an industrialized portion of the SRS. In all cases, new construction would not be visible from public access roads on the Site. No alternative would produce emissions to which would be visible or would indirectly reduce visibility.

5.6 Geologic Resources

The SRS contains no unique geologic features or minerals of economic value. The anticipates no impacts to geologic resources at the SRS from any of the spent nuclear management alternatives.

Other sections in this chapter consider the relationships of the Site's specific region's historic and analyzed seismicity to the local environment and to SRS spent related structures and facilities. Section 5.8 discusses the consequences of analyzing both surface-water and groundwater resources. Section 5.15 describes estimates of both the probability of and the consequences from a wide range of seismic events, and regional historically documented earthquakes to postulated lower probability, high events.

The accident analyses in this chapter, which DOE based on information from appropriate analysis reports for applicable facilities, address the frequency and consequences of earthquakes, as well as postulated less likely, but more damaging, seismic events. The consequences from seismic challenges to the facilities and structures up to 0.2 acceleration.

5.7 Air Quality Consequences

The SRS is in compliance with both Federal and state ambient air quality standards and toxic air pollutants. As shown in the following tables, the predicted incremental impacts would not contribute to exceeding either the National Ambient Air Quality Standards or South Carolina's Ambient Air Quality Standards.

DOE performed analyses using computer models in order to assess the potential air impacts of operations under each of the spent nuclear fuel management alternatives. This section describes the results of these analyses. All the concentrations discussed below are estimations based on results from the ISC2 and FDM models for nonradiological pollutants. MAXIGASP- and POPGASP SRS-climatology-specific models for radionuclides. The analyses assume that facility operations would result in both radiological and nonradiological impacts. This section assesses construction impacts qualitatively in relation to the land area to be disturbed under each alternative.

Nonradiological Emissions. DOE analyzed the potential incremental impacts of 65 substances for which it expects releases to the atmosphere during the normal operation of fuel facilities. The nonradiological releases evaluated for each alternative include 65 pollutants and 23 toxic pollutants. DOE selected the toxic substances for analysis anticipated chemical usage at the proposed spent nuclear fuel facilities to the list of pollutants in the South Carolina Air Pollution Regulations (SCDHEC 1976). The SRS potential emissions of the listed toxic chemicals that DOE anticipates would be used in nuclear fuel activities. The following subsections discuss the results for both criteria and toxic pollutants. Tables 5-3 and 5-4 list the estimated maximum incremental concentrations of pollutants at the Site boundary, while Tables 5-5 and 5-6 contain the incremental releases of pollutants.

Radiological Emissions. DOE evaluated the potential radiological releases to the atmosphere from spent fuel management at the SRS using existing Site historical operations information and the actual 1993 emissions data from the Receiving Basin for Offsite Fuels (WSRC). Table 5-3. Estimated incremental air quality impacts at the Savannah River Site for criteria pollutants ($\mu\text{g}/\text{m}^3$).

Pollutantb	Averaging Time	Regulatory Standardc	Maximum Potential Concentration	Actual Concen
CRITERIA POLLUTANTS (-g/m3)				
Carbon monoxide	8-hour	10,000	818	23
	1-hour	40,000	3,553	180
Ozone (as VOC)	1-hour	245	N/Ad	N/Ad
Nitrogen oxides	Annual	100	30	4
	geometric mean			
Particulate matter (<10-m)	Annual	50	9	3
	24-hour	150	93	56
Total suspended particulates (TSP)	Annual	75	20	11
Sulfur dioxide	Annual	80	18	10
	24-hour	365	356	185
	3-hour	1,300	1,210	634
Lead	Calendar quarter mean	1.5	<0.01	<0.01
Gaseous Fluorides (as HF)	1-month	0.8	0.11	0.03
	1-week	1.6	0.6	0.15
	24-hour	2.9	1.20	0.31
	12-hour	3.7	2.40	0.62

Table 5-3. (continued).

Pollutantb	Averaging Time	Regulatory Standardc	Maximum Potential Concentration	Actual Concen
CRITERIA POLLUTANTS (-g/m3)				
Carbon monoxide	8-hour	10,000	818	23
	1-hour	40,000	3,553	180
Ozone (as VOC)	1-hour	245	N/Ad	N/Ad
Nitrogen oxides	Annual	100	30	4
	geometric mean			
Particulate matter (<10-m)	Annual	50	9	3
	24-hour	150	93	56
Total suspended particulates (TSP)	Annual	75	20	11
Sulfur dioxide	Annual	80	18	10
	24-hour	365	356	185
	3-hour	1,300	1,210	634
Lead	Calendar quarter mean	1.5	<0.01	<0.01
Gaseous Fluorides (as HF)	1-month	0.8	0.11	0.03
	1-week	1.6	0.6	0.15
	24-hour	2.9	1.20	0.31
	12-hour	3.7	2.40	0.62

Table 5-3. (continued).

	Averaging Time	Regulatory Standardc	Maximum Potential Concentration	Ac Co
CRITERIA POLLUTANTS (-g/m3)				

Carbon monoxide	8-hour	10,000	818	23
	1-hour	40,000	3,553	18
Ozone (as VOC)	1-hour	245	N/Ad	N/
Nitrogen oxides	Annual	100	30	4
	geometric mean			
Particulate matter (<10-m)	Annual	50	9	3
	24-hour	150	93	56
Total suspended particulates (TSP)	Annual	75	20	11
Sulfur dioxide	Annual	80	18	10
	24-hour	365	356	18
	3-hour	1,300	1,210	63
Lead	Calendar	1.5	<0.01	<0
	quarter mean			
Gaseous Fluorides (as HF)	1-month	0.8	0.11	0.
	1-week	1.6	0.6	0.
	24-hour	2.9	1.20	0.
	12-hour	3.7	2.40	0.

- = No impact.

a. Maximum modeled ground-level concentration at SRS perimeter unless higher offsite

b. Major pollutants of concern regarding spent nuclear fuel management activities.

c. Most stringent Federal and state regulatory standards (CFR 1991a), (SCDHEC 1976)

d. Measurement data currently unavailable.

e. Maximum operational air pollutant emissions projected for baseline year 1995. C plus maximum potential emissions for sources permitted through December 1992.

Table 5-4. Estimated incremental air quality impacts at the Savannah River Site for toxic pollutants (-g/m³).

Pollutant ^b	Averaging Time	Regulatory Standard ^c	Maximum Potential Concentration	Actual Concentration ^d
TOXIC POLLUTANTS (-g/m ³)				
Nitric acid	24-hour	125	51	6.7
1,1,1,- Trichloroethane	24-hour	9,550	81	22
Benzene	24-hour	150	32	31
Ethanolamine	24-hour	200	<0.01	<0.01
Ethyl benzene	24-hour	4,350	0.58	0.12
Ethylene glycol	24-hour	650	0.20	0.08
Formaldehyde	24-hour	7.5	<0.01	<0.01
Glycol ethers	24-hour	+	<0.01	<0.01
Hexachloronaphthalene	24-hour	1.0	<0.01	<0.01
Hexane	24-hour	200	0.21	0.07
Manganese	24-hour	25	0.82	0.10
Methyl alcohol	24-hour	1,310	2.9	0.51
Methyl ethyl ketone	24-hour	14,750	6.0	0.99
Methyl isobutyl ketone	24-hour	2,050	3.0	0.51
Methylene chloride	24-hour	515	10.5	1.8
Naphthalene	24-hour	1,250	0.01	0.01
Phenol	24-hour	190	0.03	0.03
Phosphorus	24-hour	0.5	<0.001	<0.001
Sodium hydroxide	24-hour	20	0.01	0.01
Toluene	24-hour	2,000	9.3	1.6
Trichloroethylene	24-hour	6,750	4.8	1.0
Vinyl acetate	24-hour	176	0.06	0.02
Xylene	24-hour	4,350	39	3.8

Table 5-4. (continued).

Pollutant ^b	Averaging Time	Regulatory Standard ^c	Maximum Potential Concentration	Actual Concentration ^d
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TOXIC POLLUTANTS (-g/m3)

Nitric acid	24-hour	125	51	6.7
1,1,1,- Trichloroethane	24-hour	9,550	81	22
Benzene	24-hour	150	32	31
Ethanolamine	24-hour	200	<0.01	<0.01
Ethyl benzene	24-hour	4,350	0.58	0.12
Ethylene glycol	24-hour	650	0.20	0.08
Formaldehyde	24-hour	7.5	<0.01	<0.01
Glycol ethers	24-hour	+	<0.01	<0.01
Hexachloronapthalene	24-hour	1.0	<0.01	<0.01
Hexane	24-hour	200	0.21	0.07
Manganese	24-hour	25	0.82	0.10
Methyl alcohol	24-hour	1,310	2.9	0.51
Methyl ethyl ketone	24-hour	14,750	6.0	0.99
Methyl isobutyl ketone	24-hour	2,050	3.0	0.51
Methylene chloride	24-hour	515	10.5	1.8
Naphthalene	24-hour	1,250	0.01	0.01
Phenol	24-hour	190	0.03	0.03
Phosphorus	24-hour	0.5	<0.001	<0.001
Sodium hydroxide	24-hour	20	0.01	0.01
Toluene	24-hour	2,000	9.3	1.6
Trichloroethylene	24-hour	6,750	4.8	1.0
Vinyl acetate	24-hour	176	0.06	0.02
Xylene	24-hour	4,350	39	3.8

Table 5-4. (continued).

Pollutant ^b	Averaging Time	Regulatory Standard ^c	Maximum Potential Concentration	Actual Concentration ^d
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TOXIC POLLUTANTS (-g/m3)

Nitric acid	24-hour	125	51	6.7
1,1,1,- Trichloroethane	24-hour	9,550	81	22
Benzene	24-hour	150	32	31
Ethanolamine	24-hour	200	<0.01	<0.01
Ethyl benzene	24-hour	4,350	0.58	0.12
Ethylene glycol	24-hour	650	0.20	0.08
Formaldehyde	24-hour	7.5	<0.01	<0.01
Glycol ethers	24-hour	+	<0.01	<0.01
Hexachloronapthalene	24-hour	1.0	<0.01	<0.01
Hexane	24-hour	200	0.21	0.07
Manganese	24-hour	25	0.82	0.10
Methyl alcohol	24-hour	1,310	2.9	0.51
Methyl ethyl ketone	24-hour	14,750	6.0	0.99
Methyl isobutyl ketone	24-hour	2,050	3.0	0.51
Methylene chloride	24-hour	515	10.5	1.8
Naphthalene	24-hour	1,250	0.01	0.01
Phenol	24-hour	190	0.03	0.03
Phosphorus	24-hour	0.5	<0.001	<0.001
Sodium hydroxide	24-hour	20	0.01	0.01
Toluene	24-hour	2,000	9.3	1.6
Trichloroethylene	24-hour	6,750	4.8	1.0
Vinyl acetate	24-hour	176	0.06	0.02
Xylene	24-hour	4,350	39	3.8

- No impact.

+ Not available.

a. Maximum modeled ground-level concentration at SRS perimeter unless higher offsite b. Major pollutants of concern regarding spent nuclear fuel.

c. Most stringent Federal and state regulatory standards (CFR 1991a), (SCDHEC 1976)

d. Maximum operational air pollutant emissions projected for baseline year 1995. C 1990 plus maximum potential emissions for sources permitted through December 199

Table 5-5. Incremental air quality pollutant emission rates related to spent nuclear
Baseline Alternatives

Pollutant	Maximum Design Capacity	Actual ^b	No Action	D
CRITERIA POLLUTANTS (TONS PER YEAR)			1	2
NOx	2.22x10 ⁴	2.62x10 ³	-	6
Particulates				
TSP	3.62x10 ³	9.80x10 ²	-	4
PM10	2.66x10 ³	4.97x10 ²	-	2
CO	6.77x10 ³	1.99x10 ²	-	1
SO ₂	6.42x10 ⁴	6.68x10 ³	1.6x10 ⁻³	4
Gaseous Fluorides	2.14x10 ⁻²	1.07x10 ⁻²	-	-
Ozone (as VOC)	N/Ac	N/Ac	-	6
CRITERIA POLLUTANTS (TONS PER YEAR)			Regionalization A	
			4a	4
NOx	2.22x10 ⁴	2.62x10 ³	8.5x10 ⁰	8
Particulates				
TSP	3.62x10 ³	9.80x10 ²	6.0x10 ⁻²	6
PM10	2.66x10 ³	4.97x10 ²	1.45x10 ¹	1
CO	6.77x10 ³	1.99x10 ²	2.0x10 ⁰	2
SO ₂	6.42x10 ⁴	6.68x10 ³	5.5x10 ⁻²	5
Gaseous Fluorides	2.14x10 ⁻²	1.07x10 ⁻²	-	-
Ozone (as VOC)	N/Ac	N/Ac	8.5x10 ⁻¹	8

Table 5-5. (continued).

Pollutant	Maximum Design Capacity	Actual ^b	Alternatives	
CRITERIA POLLUTANTS (TONS PER YEAR)			Centralization	
			5a	
NOx	2.2x10 ⁴	2.6x10 ³	5.6x10 ¹	5
Particulates				
TSP	3.62x10 ³	9.8x10 ²	2.1x10 ⁰	2
PM10	2.66x10 ³	4.97x10 ²	1.4x10 ⁰	1
CO	6.77x10 ³	1.99x10 ²	2.7x10 ¹	2
SO ₂	6.42x10 ⁴	6.68x10 ³	8.1x10 ⁰	8
Gaseous Fluorides	2.14x10 ⁻²	1.07x10 ⁻²		
Ozone (as VOC)	N/Ac	N/Ac	4.6x10 ⁰	4

a. Source: WSRC (1994a).

b. Maximum operational air pollutant emissions projected for baseline year 1995. C year 1990 plus maximum potential emissions for sources permitted through December 1990.

c. Emissions data currently unavailable.

- No proposed incremental emissions.

Table 5-6. Incremental air quality pollutant emission rates related to spent nuclear fuel processing alternatives.

Pollutant	Maximum Design Capacity	Actual ^b	No Action	Decentral
TOXIC POLLUTANTS (TONS PER YEAR)			1	2a
Nitric Acid	1.13x10 ³	2.56x10 ⁰	5.1x10 ⁻²	5.1x10 ⁻²
1,1,1-Trichloroethane	8.0x10 ¹	N/Ac	-	-
Benzene	2.9x10 ¹	4.48x10 ⁰	-	-
Ethanolamine	2.21x10 ⁻²	5.35x10 ⁻³	1.46x10 ⁻³	1.46x10 ⁻³
Ethyl Benzene	2.56x10 ⁰	1.07x10 ⁰	-	-
Ethylene Glycol	6.83x10 ⁻¹	4.17x10 ⁻¹	2.25x10 ⁻²	2.25x10 ⁻²
Formaldehyde	4.55x10 ⁻²	4.8x10 ⁻⁴	3.6x10 ⁻⁶	3.6x10 ⁻⁶

Glycol Ethers	4.36x10 ⁻³	1.99x10 ⁻⁴	4.06x10 ⁻³	4.06x10 ⁻³
Hexachloronaphthalene	<0.01	NAC	3.65x10 ⁻⁵	3.65x10 ⁻⁵
Hexane	3.54x100	2.22x10 ⁻¹	3.28x10 ⁻³	3.28x10 ⁻³
Manganese	2.84x10 ⁻¹	3.43x10 ⁻¹	-	-
Methyl Alcohol	6.62x10 ⁻¹	3.46x10 ⁻¹	6.84x10 ⁻²	6.84x10 ⁻²
Methyl Ethyl Ketone	6.41x100	3.17x100	2.19x10 ⁻³	2.19x10 ⁻³
Methyl Isobutyl Ketone	8.25x100	2.25x100	-	-
Methylene Chloride	1.53x100	1.19x100	-	-
Naphthalene	7.22x10 ⁻²	3.08x10 ⁻²	5.84x10 ⁻⁴	5.84x10 ⁻⁴
Phenol	8.07x10 ⁻²	1.37x10 ⁻²	-	-
Phosphorus	2.97x10 ⁻³	1.65x10 ⁻⁴	-	-
Sodium Hydroxide	1.26x10 ⁻¹	1.26x10 ⁻¹	-	-
Toluene	3.91x100	7.66x10 ⁻¹	5.0x10 ⁻²	5.0x10 ⁻²
Trichloroethylene	2.52x101	9.8x100	-	-
Vinyl Acetate	4.38x10 ⁻²	5.9x10 ⁻³	-	-
Xylene	1.46x103	1.22x101	1.58x10 ⁻¹	1.58x10 ⁻¹

Table 5-6. (continued).

	Baseline		Alternatives	
Pollutant	Maximum Design Capacity	Actualb	Regionalization A	
			4a	4b
TOXIC POLLUTANTS (TONS PER YEAR)				
Nitric Acid	1.1x103	2.6x100	5.1x10-2	5.1x
1,1,1-Trichloroethane	8.0x101	NAC	-	-
Benzene	2.9x101	4.5x100	-	-
Ethanolamine	2.2x10-2	5.4x10-3	1.5x10-3	1.5x
Ethyl Benzene	2.6x100	1.1x100	-	-
Ethylene Glycol	6.8x10-1	4.2x10-1	2.3x10-2	2.3x
Formaldehyde	4.6x10-2	4.8x10-4	3.6x10-6	3.6x
Glycol Ethers	4.4x10-3	2.0x10-4	4.1x10-3	4.1x
Hexachloronapthalene	<0.01	NAC	3.7x10-5	3.7x
Hexane	3.5x100	2.2x10-1	3.3x10-3	3.3x
Manganese	2.8x10-1	3.4x10-1	-	-
Methyl Alcohol	6.6x10-1	3.5x10-1	6.8x10-2	6.8x
Methyl Ethyl Ketone	6.4x100	3.2x100	2.2x10-3	2.2x
Methyl Isobutyl Ketone	8.3x100	2.3x100	-	-
Methylene Chloride	1.5x100	1.2x100	-	-
Naphthalene	7.2x10-2	3.1x10-2	5.8x10-4	5.8x
Phenol	8.1x10-2	1.4x10-2	-	-
Phosphorus	3.0x10-3	1.7x10-4	-	-
Sodium Hydroxide	1.3x10-1	1.3x10-1	-	-
Toluene	3.9x100	7.7x10-1	5.0x10-2	5.0x
Trichloroethylene	2.5x101	9.8x100	-	-
Vinyl Acetate	4.4x10-2	5.9x10-3	-	-
Xylene	1.5x103	1.2x101	1.6x10-1	1.6x

Table 5-6. (continued).

Pollutant	Maximum Design Capacity	Actualb	Alternatives	
			Centralization 5a	5b
TOXIC POLLUTANTS (TONS PER YEAR)				
Nitric Acid	1.1x103	2.6x100	5.1x10-2	5.1x
1,1,1-Trichloroethane	8.0x101	NAC	-	-
Benzene	2.9x101	4.5x100	-	-
Ethanolamine	2.2x10-2	5.4x10-3	1.5x10-3	1.5x
Ethyl Benzene	2.6x100	1.1x100	-	-
Ethylene Glycol	6.8x10-1	4.2x10-1	2.3x10-2	2.3x
Formaldehyde	4.6x10-2	4.8x10-4	3.6x10-6	3.6x

Glycol Ethers	4.4x10 ⁻³	2.0x10 ⁻⁴	4.1x10 ⁻³	4.1x
Hexachloronapthalene	<0.01	NAC	3.7x10 ⁻⁵	3.7x
Hexane	3.5x100	2.2x10 ⁻¹	3.3x10 ⁻³	3.3x
Manganese	2.8x10 ⁻¹	3.4x10 ⁻¹	-	-
Methyl Alcohol	6.6x10 ⁻¹	3.5x10 ⁻¹	6.8x10 ⁻²	6.8x
Methyl Ethyl Ketone	6.4x100	3.2x100	2.2x10 ⁻³	2.2x
Methyl Isobutyl Ketone	8.3x100	2.3x100	-	-
Methylene Chloride	1.5x100	1.2x100	-	-
Naphthalene	7.2x10 ⁻²	3.1x10 ⁻²	5.8x10 ⁻⁴	5.8x
Phenol	8.1x10 ⁻²	1.4x10 ⁻²	-	-
Phosphorus	3.0x10 ⁻³	1.7x10 ⁻⁴	-	-
Sodium Hydroxide	1.3x10 ⁻¹	1.3x10 ⁻¹	-	-
Toluene	3.9x100	7.7x10 ⁻¹	5.0x10 ⁻²	5.0x
Trichloroethylene	2.5x101	9.8x100	-	-
Vinyl Acetate	4.4x10 ⁻²	5.9x10 ⁻³	-	-
Xylene	1.5x103	1.2x101	1.6x10 ⁻¹	1.6x

a. Source: WSRC (1994a).

b. Maximum operational air pollutant emissions projected for baseline year 1995. C year 1990 plus maximum potential emissions for sources permitted through December 1995.

c. NA= Emissions data currently unavailable.

- No proposed incremental emissions.

consist of about 2 y 10⁻⁷ curies per year of cesium-137. Releases from dry storage these alternatives would be somewhat less. For Alternative 5 where SRS would manage MTHM (3,020 tons) of spent fuel (versus about 206 to 257 MTHM [227 to 283 tons] for alternatives), the atmospheric releases of cesium-137 would be proportionally higher.

DOE used actual emissions from F- and H-Areas during 1985 and 1986, a period when it was processing material through the separations facilities at close to maximum capacity. These releases represent potential releases from spent nuclear fuel management activities. DOE believes that the releases during this period, and their emission rates, represent maximum emissions under any of the alternatives (Table 5-7). The results of the analyses are presented in Section 5.12. Section 5.15 presents the human health consequences are discussed in Section 5.12. Section 5.15 presents the consequences of accidents.

Construction Emissions. Potential impacts to air quality from construction activities include fugitive dust from the clearing of land, as well as exhaust emissions from (e.g., earth-moving vehicles, diesel generators). The amount of dust produced would depend on the land area disturbed for the new facilities, all of which would be located near the Site. The areas affected by each alternative would be as follows:

- No Action - 0 acres
- Decentralization, 1992/1993 Planning Basis and Regionalization A (by fuel treatment) - 9 acres
- Regionalization B (by location) - 7 to 11 acres
- Centralization - 70 to 100 acres
- Shipping fuel offsite - 1 acre

DOE anticipates that overall construction impacts to air quality would be minimal in duration (6 months to 3 years). The SRS sitewide compliance with state and Federal air quality standards would not be affected by any construction-related activities associated with fuel management.

Table 5-7. Estimated maximum annual emissions (in curies) of radionuclides to the environment from spent nuclear fuel management activities.

Radionuclide Annual Emissions^{a,b}

Tritium (elemental)	1.88x10 ^{5,c}
Cesium-134	3.60x10 ⁻⁴
Cesium-137	4.07x10 ⁻³
Curium-244	2.00x10 ⁻⁴
Cerium-141	1.83x10 ⁻³
Cerium-144	3.11x10 ⁻²
Americium-241	2.27x10 ⁻⁴
Cobalt-60	4.00x10 ⁻⁶
Plutonium-238	1.28x10 ⁻³
Plutonium-239	4.01x10 ⁻⁴
Strontium-90	1.39x10 ⁻²

Rubidium-103	7.25x10 ⁻³
Uranium-235	2.00x10 ⁻³
Osmium-185	3.60x10 ⁻⁴
Niobium-95	2.89x10 ⁻²
Selenium-75	1.52x10 ⁻⁵
Zirconium-95	1.68x10 ⁻²
Rubidium-106	5.12x10 ⁻³
Krypton-85	6.80x10 ⁵
Carbon-14	2.80x10 ¹

a. Source: Hamby (1993).

b. Source terms are taken from 1985/86 F-/H-Area releases.

c. Historically, less than 10 percent of the atmospheric tritium releases have been operations in the F-/H-Area Canyons.

5.7.1 Alternative 1 - No Action

The SRS would not process any spent nuclear fuel under the No Action alternative. Baseline emissions would continue (Tables 5-3, 5-4, 5-5, 5-6 and 5-7). DOE would not build new facilities under this alternative.

5.7.2 Alternative 2 - Decentralization

Atmospheric emissions under two of the Decentralization options (dry storage and wet storage) would be similar to those for No Action. Those from the processing of the spent fuel would be of somewhat higher concentrations (Tables 5-3, 5-4, 5-5, 5-6 and 5-7). They would originate from existing facilities involved in the management of spent fuel under the alternative as well as new ones that DOE would construct (Figure 3-2).

5.7.3 Alternative 3 - 1992/1993 Planning Basis

Emissions to the atmosphere would be similar to those for Alternative 2 because the amount of fuel managed would be similar [223 and 220 MTHM (246 and 243 tons), Alternative 3 and Alternative 2 respectively] and the facilities required would be the same (Figure 3-2).

5.7.4 Alternative 4 - Regionalization

Regionalization A (by fuel type). Atmospheric emissions would be similar to those for Alternative 2 because of the similarity in volumes of fuel managed [213 and 220 MTHM (243 tons), respectively] and in the facilities involved (Figure 3-2).

Regionalization B (by location). Emissions would be somewhat higher than for Alternative 2 for both dry and wet storage options if the SRS receives all the eastern portion of the country, because the Site would manage about 20 percent more spent nuclear fuel. Atmospheric emissions from processing would not change from those under other alternatives because the amount of aluminum-clad fuel involved would be the same. Facility requirements would be similar (Figure 3-2).

Shipping all of the current SRS inventory off the Site (Option 4g) would result in emissions to the atmosphere of any of the options under this alternative. These results are from the characterization and canning of the fuel prior to shipment.

5.7.5 Alternative 5 - Centralization

The atmospheric emissions resulting from centralizing all the spent nuclear fuel would be the greatest of all the alternatives. The Site would manage about 2,740 MTHM (310 tons) of fuel. Releases from storage activities for centralization would be proportionally greater than for other alternatives where the SRS would manage about 206 to 257 MTHM (227 to 283 tons) of fuel. However, emissions from processing under Alternative 5 would be similar to those for other alternatives because the same amount of aluminum-clad fuel would be processed. The facilities required under all three options would be similar in function (Figure 3-2).

larger capacity than for other alternatives.

Shipping all the SRS fuel to another site (Option 5d) would result in the lowest atmospheric releases of any alternative, similar to those under Regionalization B,

5.8 Water Quality and Related Consequences

SRS use of surface-water and groundwater resources under any of the alternative substantially increase the volumes currently used for process, cooling, and domestic. Table 5-8 summarizes the groundwater and surface water usage requirements for each option, and compares them to current SRS usages.

The Centralization Alternative (Option 5c), under which DOE would transfer all fuel to the SRS, would result in the largest amount of water use [approximately 378 (100 million gallons) per year], which is a small amount compared to current SRS use of approximately 89.7 billion liters (23.7 billion gallons) per year. This represents approximately 0.4 percent above current usage. Therefore, DOE anticipates that water of the alternatives would have minimal impact on the water resources of the Site.

The impact on water quality of the operation of any of the alternatives would be minimal. Existing SRS treatment facilities could accommodate all new spent fuel-related domestic wastewater streams. The expected total SRS flow volumes would still be well within capacities of the Site treatment systems. Because these plants would continue to meet Pollutant Discharge Elimination System limits and reporting requirements, DOE expects the water quality of the receiving streams. The increased cooling water flows would discharge permit limits and would have minimal impacts on the receiving water.

Each of the alternatives would contribute to the very small releases of radionuclides from SRS operations discharge to the surface water through federally permitted wastewater treatment. Table 5-8. Annual groundwater and surface water usage requirements for each alternative.

Alternative	Groundwater Usage per Year	Surface Water Usage per Year	Total
Current SRS Usage	14.0 billion liters	75.7 billion liters	89.7
No Action			
Option 1 - Wet Storage	35.1 million liters	None	35.1 m
Decentralization			
Option 2a - Dry Storage	48.7 million liters	6.1 million liters	54.8 m
Option 2b - Wet Storage	50.6 million liters	7.2 million liters	57.8 m
Option 2c - Processing	48.7 million liters	310.8 million liters	359.5
Planning Basis			
Option 3a - Dry Storage	48.7 million liters	6.1 million liters	54.8 m
Option 3b - Wet Storage	50.6 million liters	7.2 million liters	57.8 m
Option 3c - Processing	48.7 million liters	310.8 million liters	359.5
Regionalization - A			
Option 4a - Dry Storage	48.7 million liters	6.1 million liters	54.8 m
Option 4b - Wet Storage	50.6 million liters	7.2 million liters	57.8 m
Option 4c - Processing	47.6 million liters	308.8 million liters	356.5
Regionalization - B			
Option 4d - Dry Storage	48.7 million liters	6.1 million liters	54.8 m
Option 4e - Wet Storage	50.6 million liters	7.2 million liters	57.8 m
Option 4f - Processing	48.7 million liters	310.8 million liters	356.5
Option 4g - Ship Out	38.1 million liters	3.0 million liters	41.1 m
Centralization			
Case 5a - Dry Storage	67.7 million liters	6.1 million liters	73.8 m
Case 5b - Wet Storage	69.6 million liters	7.2 million liters	76.8 m
Case 5c - Processing	67.7 million liters	310.8 million liters	378.5
Case 5d - Ship Out	38.1 million liters	3.0 million liters	41.1 m

a. Source: WSRC (1994b).

b. To convert liters to gallons, multiply by 0.26418.

c. First 10 years only.

Table 5-9 summarizes the estimated maximum amounts of radioactivity that could be released from the Savannah River in liquid effluents from normal spent nuclear fuel management activities. Actual liquid releases from F- and H-Area during 1985 and 1986 to estimate potential releases could occur during spent fuel management activities. DOE believes the isotopes and during this period are representative of releases that could occur during processing alternatives. This is because 1985 and 1986 represent periods when the F- and H-Area facilities operated at or near peak capacity to process spent nuclear fuel. Estimates

or dry storage would be less than these amounts. Consequently, the estimated releases Table 5-9 represent the upper limit of liquid radiological releases that DOE expects from spent nuclear fuel management activities.

Radionuclide	Annual Release ^{a,b}
Tritium	1.3×10^4 , ^c
Strontium-90	2.4×10^{-1}
Iodine-129	2.2×10^{-2}
Cesium-137	1.1×10^{-1}
Plutonium-239	7.0×10^{-3}

a. Source: Hamby (1993).

b. Source terms are taken from 1985/86 F-/H-Area releases.

c. Less than 1 percent of this quantity was from processing operations in F-/H-Area

nuclear fuel management activities. The consequences to human health due to these are discussed in Section 5.12, Occupational and Public Health and Safety.

Construction of new facilities under any alternative would require amounts of water to be only a very small percentage of the current daily water use at the SRS. Good engineering measures would prevent sediment runoff or spills of fuel or chemicals. Therefore, construction activities should have no impact on surface or groundwater quality at the Site.

DOE also analyzed the potential impacts of accidents in F- and H-Areas on surface and groundwater quality. The analysis evaluated two types of accidental releases: one to the surface (e.g., overflow of a wet storage pool) and another directly to the subsurface (e.g., pool liner). Because pool water could contain some radionuclides, but would not contain harmful chemicals, the following evaluation addresses only the consequences of radionuclide releases.

A release of pool water onto the ground from the Receiving Basin for Offsite Fuel would not flow directly into any stream or other surface-water body. The building is surrounded by an earthen berm immediately to the south. A channelized drainage system approximately 244 meters (800 feet) west of the basin building and passes through a railroad line and Road E before emptying into a tributary of Fourmile Branch about 1,650 feet from the Receiving Basin. The grading at the Site would contain a small area of overflowing the basin in the immediate area of the building. In the unlikely event that the drainage ditch to the west, DOE could contain the water by blocking existing culverts through which the drainage ditch passes. After containing the spilled water, DOE would remove and properly dispose of it. DOE would design and construct new facilities to contain pools in a manner that would confine any overflow or other surface release of pool water. DOE believes that there will be no direct release to surface water from spills of pool water at an existing or potential facility.

An overflow from a pool could reach the groundwater by slowly flowing downward through the unsaturated zone until it reached the water table, which is 9 to 50 feet below the grade in the F- and H-Areas. Overflow water would take several years to reach the water table, based on a vertical velocity of between 0.9 and 2.1 meters (3 to 7 feet per year) (1987). As discussed in the following paragraphs, once in the groundwater, a plume of water would take years to reach either the closest surface-water bodies, Fourmile Branch to the south or Runs Creek to the north.

DOE has calculated the travel times of groundwater in the F- and H-Areas based on information on the hydraulic conductivity, the hydraulic gradient, and the effective porosity in this area (WSRC 1993a) and on the use of Darcy's Law. Water would take between 1 to 10 years to travel 1.6 kilometers (1 mile) toward Fourmile Branch or Upper Three Runs Creek. Estimates of travel time agree with values obtained from the results of DOE modeling performed on the F- and H-Areas (Geotrans 1993; appended to WSRC 1993a). The reason for the wide range of potential travel time is that the hydraulic conductivity of the aquifer is highly variable and can vary in the same aquifer by several orders of magnitude. This slow movement through the subsurface, either vertically through the unsaturated zone or horizontally through the aquifer, would facilitate the removal of radionuclides from the spill plume through natural processes. These include radioactive decay, trapping of particulates in the soil, adsorption by the soil (Hem 1989). DOE believes that travel time of a contaminant through the subsurface in the F- or H-Area or in the adjacent representative host site would be long enough that radionuclides would reach Fourmile Branch, Upper Three Runs Creek, or any other surface water by this route. For the same reasons, no radioactive contaminants introduced into the ground in these areas would move off the Site in groundwater.

DOE does not believe that releases of radionuclides such as those described above would affect SRS drinking-water sources that lie in deep aquifers under the Site. These aquifers

hundred feet below the ground surface, and a number of thick aquifers and aquitards from the water table aquifer (see Section 4.8). In addition to the distances and confining layers, vertical flow in the intervening stratified sedimentary aquifers to horizontal flow. Radionuclide contamination of offsite drinking water sources unlikely given the depth of their source aquifers, the distances involved, and the contaminants in the soils, as described above.

DOE also evaluated a second kind of unintentional release in the F- or H-Area, the subsurface from a breach in a storage pool during routine operations. The anal 19-liter (5-gallon)-per-day leak as a result of secondary containment or piping failure in the wet storage and fuel transfer facility (Creed 1994). The analysis assumed would go undetected for 1 month, a conservative assumption given the sensitivity of equipment that these new facilities would require. The reliability and sensitivity devices would be equal to or superior to those required by the U.S. Nuclear Regulatory Commission (NRC 1975) for spent nuclear fuel storage facilities in commercial nuclear power plants. Spent nuclear fuel storage pools (whether fuel unloading pools or storage basins) require detection monitoring devices, pool water level monitors, and radiation monitors locally and in a continuously staffed central location. Constant process monitoring facility design (including double-walled containment of vessels and piping) would a DOE to limit operational releases from new wet storage facilities, including fuel unloading basins, to near zero.

To provide a common basis for analysis of spent nuclear fuel alternatives at the Y-12 DOE developed a generic infrastructure design for a hypothetical spent nuclear fuel storage facility (Creed 1994). This design includes proposed criteria for temporary wet storage basins, fuel unloading pools, and transfer canals.

Based on the design criteria in Hale (1994), a leak from one of these basins in the F- or H-Area could result in the introduction of radionuclide-contaminated water in depths as much as 13.4 meters (44 feet) below grade. Such a release would go directly to the water table aquifer or to the unsaturated zone above it, depending on the depth of the release. The processes governing the slow plume movement (i.e., the hydraulic conductivity gradient, and effective porosity of aquifers in the F- and H-Areas) and the process attenuation of contaminants and radionuclides (i.e., radioactive decay, trapping of soil, ion exchange in the soil, and adsorption to soil particles) described in the Y-12 design would also prevent or mitigate impacts to surface- or groundwater resources from the release. There could be localized contamination of groundwater in the surface aquifer in the vicinity of the storage facilities. This aquifer is not used as a source of drinking water. radionuclide contamination of deeper confined aquifers that are sources of onsite drinking water could occur from a release of this type. And, as noted earlier, these wet storage basins would be equipped with state-of-the-art leak detection devices, pool level monitors, and that would limit and mitigate any subsurface releases.

5.8.1 Alternative 1 - No Action

5.8.1.1 Option 1 - Wet Storage. During operations under this alternative, current levels of

water usage would not change. Nor would changes occur in thermal discharges from the quantity or quality of radioactive and nonradioactive wastewater effluents.

The viable accidents under this alternative would be a release of pool water on the surface or a breach of the liner of the wet storage basins in which the spent nuclear fuel is stored. As discussed above, radionuclides in the released water would enter the water table aquifer but would not reach any surface-water or any drinking water aquifer on or off the SRS. The SRS contains no toxic or hazardous chemicals. Therefore, accidental releases from the wet storage basins would have minimal impacts on surface- and groundwater resources.

Spills of chemicals would not reach surface- or groundwater due to existing process design and environmental controls, and to rapid containment and cleanup.

5.8.2 Alternative 2 - Decentralization

Operations under either the dry or wet storage option for the Decentralization alternative would increase Site water usage by less than 0.1 percent above current levels. Processing of spent nuclear fuel would increase by about 0.4 percent. Release of nonradioactive and radioactive materials to the surface would increase only slightly and would be well within discharge permit limits and DOE does not expect any releases to groundwater during normal operations. Overall impacts to water resources would be minimal.

water quality would be minimal.

Impacts to water resources due to accidental releases onto the ground or into the aquifer would also be minimal as explained above. Potential contamination would be limited to the aquifer.

5.8.3 Alternative 3 - 1992/1993 Planning Basis

DOE expects that the impacts to water resources under the dry storage, wet storage, and processing cases for this alternative would be similar to those described for the same cases under Alternative 2, Decentralization. Overall impacts would be minimal.

5.8.4 Alternative 4 - Regionalization

DOE expects that the impacts to water resources under the three options for regionalization (Regionalization A) would be similar to those described for the same options under Alternative 2, Decentralization. Regionalization B (by geographic location) would have somewhat greater impacts than those for Alternative 2 because the SRS would have to manage MTHM (41 tons) of spent fuel. In either case, overall impacts would be minimal. For shipping all SRS fuel to Oak Ridge Reservation, impacts to water resources would be similar to those for Option 5d - Centralization.

5.8.5 Alternative 5 - Centralization

The first three options for this alternative - dry storage (Option 5a), wet storage (Option 5c) - assume that DOE would transfer all spent nuclear fuel to the management. The impacts of operations to water resources under these options would be similar in nature to the impacts for the same options under Alternative 2, Decentralization, as described in Section 5.8.2. However, the extent of the impacts would be greater because the number of facilities that DOE would construct and operate and the quantities of fuel it would manage would be larger than those for any other alternative. Even so, DOE expects the overall impacts to water resources to be minor. For example, the total volume of water that the SRS would use for construction, cooling, processing, and domestic use under any of these three options would be approximately 378.5 million liters (100 million gallons) per year. This requirement represents approximately 0.4 percent of the 89.7 billion liters (23.7 billion gallons) that the SRS uses annually.

Similarly, DOE believes that the overall impacts of accidents under any of these three options would be minor, even though the number and size of the facilities would be greater than for any other alternative. Radionuclides released during an accident would not contaminate surface water or any drinking water aquifer. However, surface aquifer resources would be contaminated in the area of any release.

For Option 5d (shipping the spent nuclear fuel off the Site), impacts to water resources would be smaller than those for any other alternative or option. DOE would have to build on the Site (for fuel characterization) and the spent fuel would remain at SRS only for the final management period. Overall impacts would be minimal.

5.9 Ecology

DOE expects that construction impacts, which would include loss of some wildlife and land clearing, would be greatest under the Centralization Alternative. Dry Storage Representative impacts from operations would include disturbance and displacement of wildlife by movement and noise of personnel, equipment, and vehicles; however, these impacts would be minor under all the proposed alternatives. Construction and operation would not disturb sensitive habitat, nor would they affect any wetland areas. Releases of radionuclides into the environment from any of the proposed alternatives would be small and would not be expected to accumulate in aquatic or terrestrial ecosystems or measurably affect the health of animal communities.

5.9.1 Alternative 1 - No Action

Under this alternative, DOE could refurbish or modify existing wet storage facilities to confine any activity to these facilities. As a consequence, DOE expects no impacts on ecological resources. Impacts of operations under this alternative would be minimal, limited disturbance of animals by vehicular traffic.

5.9.2 Alternative 2 - Decentralization

5.9.2.1 Option 2a - Dry Storage. This option would require some new construction, but any

construction activity would occur either within the boundaries of F- and H-Areas, which are heavily developed, or adjacent to them. As a result, this construction would have no impacts on ecological resources. There would be no impacts to wetlands, threatened or endangered species (such as the eastern wild turkey), or other species (such as wood warblers and vireos). Impacts of operations under this option would be some minor disturbance of animals by slight increases in vehicular traffic. No endangered, or candidate species occur in the area of operations. Species likely to be killed by vehicles (e.g., cotton rat, gray squirrel, opossum, and white-tailed deer) are ubiquitous in the area. Overall impact to ecological resources would be minimal.

5.9.2.2 Option 2b - Wet Storage. Construction impacts would be similar to those described

for dry storage (Option 2a). Impacts of operations under this option would also be described for dry storage (Option 2a). Overall impacts to ecological resources would be minimal.

5.9.2.3 Option 2c - Processing and Storage. Construction and operations impacts for this

option would also be similar to those for dry storage (Option 2a). Overall impacts would be minimal.

5.9.3 Alternative 3 - 1992/1993 Planning Basis

Both construction and operational impacts for the three options under this alternative are similar to those described for Alternative 2 - Decentralization. Overall impacts would be minimal.

5.9.4 Alternative 4 - Regionalization

Under the Regionalization A alternative, impacts to ecological resources would be described for Alternative 2. Impacts due to the Regionalization B options would be due to the larger volume of spent fuel that the SRS would manage. Overall impacts would be minimal, however.

The smallest impacts would occur under Option 4g because DOE would ship all spent fuel off the Site.

5.9.5 Alternative 5 - Centralization

5.9.5.1 Option 5a - Dry Storage. The discussion that follows assumes that any facility

development would take place in an area that does not contain any pristine wetlands, timber, threatened and endangered species, or designated critical habitat. More specifically, the upland areas south and east of H-Area are dominated by planted pine (primarily loblolly) stands, the discussion of impacts assumes that any facility development in support of fuel management would take place in an area of 5- to 40-year-old pines. Finally, it is assumed that any facility development would require a site-specific National Environmental Review as required under 10 CFR Part 1021 and in accordance with the Council on Environmental Quality's NEPA implementing regulations (CFR 1991b).

The proposed interim dry storage facility and support facilities, requiring approximately 0.28 square kilometers (70 acres) to 0.4 square kilometers (100 acres) of land, would be located on the Site.

somewhere within the largely wooded roughly 2.8 square kilometer (700-acre) area so H-Area west of F-Road, and north of Fourmile Branch. This area has a number of advantages: it would be relatively easy to connect with existing utilities (gas, water, minimize the amount of supporting infrastructure (e.g., railroad spurs, access road lines) that would have to be built; and it would enable DOE to consolidate spent nuclear management activities in an area that has been altered many times over the years by 1951) and timber management activities (after 1951).

Construction activities would result in the clearing of as much as approximately 1 kilometer (100 acres) of planted 5- to 40-year-old loblolly or slash pine for new undeveloped representative host site south and east of H-Area. This land clearing would involve a relatively small number of loggers and heavy equipment operators, but probably would displace birds and larger, more mobile animals from the area. Some smaller, less mobile animals such as turtles, toads, lizards, mice, and voles, probably would be killed. Aside from the 0.4 square kilometer (70-100 acres) of planted pines that provide habitat for a limited number of reptiles, birds, and mammals, construction impacts would be minor.

Any land clearing and timber harvesting conducted on the undeveloped host site would be carefully planned and conducted according to widely accepted Best Management Practices to prevent erosion and soil loss and to prevent impacts to downgradient wetlands and streams. DOE policy is to achieve "no net loss" of wetlands. DOE has issued a guidance document titled "Mitigation of Wetlands Impacts at the Savannah River Site (DOE 1992)", for project purposes forth a practical approach to wetlands protection that begins with avoidance of impacts, moves to minimization of impacts (if avoidance is impossible), and requires compensation (wetlands restoration, creation, enhancement, or acquisition) in the event that impacts are avoided.

In the event that new facility development was required, DOE would perform preconstruction surveys to ensure that its activities would not affect threatened and endangered species habitats. To the extent practicable, land clearing and timber harvesting would be scheduled for the year when songbirds and game birds were not nesting or rearing young. In South Carolina, songbirds nest, rear, and fledge young from March to September (Sprunt and Chamberlain 1970). Quail, dove, and wild turkey in the region normally nest and fledge young during the summer (Sprunt and Chamberlain 1970).

No threatened or endangered plants or animals are known to be present in the area under consideration for development. Construction activities probably would not affect the Carolina bays lying in the east-central portion of the undeveloped host site. Construction would not affect plant and animal diversity locally or regionally, because the managed slash pine stands that would be removed are not unique, nor do they provide habitat for sensitive, unusual, or Federally listed plant or animal species.

Impacts of operations under this option would be similar to, but slightly greater than those described for Option 2a. Overall impacts to ecological resources would be minor.

5.9.5.2 Option 5b - Wet Storage. Construction impacts under this option would be less than

those described for Option 5a because less land area would be required for new facility operations under this case would be similar to those described for Option 5a. Overall impacts to ecological resources would be minor.

5.9.5.3 Option 5c - Processing and Storage. Construction impacts under this case would

be similar to those described for Option 5a. This case would require the largest number of acres in all the cases under consideration. It would result in more noise, more traffic, and a level of disturbance to terrestrial wildlife (specifically reptiles, songbirds, and mammals) accustomed to feeding, foraging, perching, hunting, nesting, or denning in the area. Animals would be driven from the area permanently, while others probably would be displaced to the increased noise and activity levels, and would return to the area. Overall impacts to ecological resources would be minor.

5.9.5.4 Option 5d - Shipment off the Site. Construction impacts under this case would be

smaller than those for any other alternative, excluding Alternative 1 - No Action. Under this case would also be minimal, limited to some minor disturbances of animal traffic. Overall impacts to ecological resources would be minimal.

5.10 Noise

As described in Section 4.10, noises generated on the SRS do not travel off the site and affect the general population. Therefore, SRS noise impacts for each alternative would be the noise resulting from the transportation of personnel and materials to and from the SRS and from the nearby communities and from onsite sources that could affect some wildlife near the SRS. The analysis would address the effects of noise on wildlife near spent nuclear fuel management facilities for each alternative in a project-specific NEPA evaluation.

Transportation noises would be a function of the size of the workforce (i.e., a larger workforce would produce increased employee traffic and corresponding increases in truck and rail and a decreased workforce would produce decreased employee traffic and corresponding decreases in deliveries). The analysis of traffic noise took into account railroad and major roadways that provide access to the SRS. DOE does not expect the number of vehicles per day in the region and through the Site to change as a result of any of the alternatives. Some trains could be dedicated to the transport of spent nuclear fuel. Rail shipment of spent nuclear fuel, regardless of the alternative, would not substantially increase the rail traffic through the SRS. Therefore, vehicles used to transport employees and personnel on the SRS would be the principal sources of community noise impacts. This analysis used the day-night average sound level (DNL) to assess community noise, as suggested by the Environmental Protection Agency (EPA 1974; 1982) and the Federal Interagency Committee on Noise (FICON 1992). The analysis based its estimate of the change in day-night average sound level from the baseline on the projected changes in employment and traffic levels for each alternative. The analysis also considered the combination of construction and operation of the SRS. The traffic noise analysis considered SC 125 and SC 19, both of which provide access to the SRS. Changes in noise level below 3 decibels would not be likely to result in a community reaction (FICON 1992).

DOE projects no new employment due to operations for any of the alternatives. Construction jobs may be required but overall SRS employment would not exceed the 1995 levels, except for Alternatives 5a, 5b, and 5c. The maximum Site employment of about 1,000 would occur in 1995 for all alternatives except 5a, 5b, and 5c for which the peak would be in 2002 due to a peak in construction employment. The general decrease in employment could result in some decrease in vehicle trips to and from the Site. There would be a decrease in truck trips per day to and from the Site carrying spent nuclear fuel under any of the alternatives. An increase in truck trips would not result in a perceptible increase in traffic noise to the SRS. The day-night average sound level along SC 125 and SC 19 and other access roads would probably decrease slightly except in the peak construction years under Alternative 5c, as a result of the overall decrease in employment levels at the SRS after 1995. The change in the community reaction to noise along these routes. Consequently, no mitigation is necessary.

5.11 Traffic and Transportation

This section discusses the consequences of both the onsite transportation of spent nuclear fuel and the increased traffic patterns due to construction activities at the SRS. Traffic patterns for spent nuclear fuel facilities will remain at or below current Site levels because construction activities will be drawn from the existing SRS workforce. The consequences of the spent nuclear fuel between the SRS and other DOE sites are described in Appendix I of the Volume 1 Environmental Impact Statement (EIS).

5.11.1 Traffic

Traffic impacts would be bound by Alternative 5b (Centralization - Wet Storage) which would result in the greatest number of additional construction workers (and vehicles) on site. As a measure of traffic flow, a traffic count was estimated for each road to and from the SRS. The highest traffic could be experienced at SC 19 and SC 230 intersections during peak hours. However, construction vehicles in support of spent nuclear fuel construction activities would represent only 17 percent (HNUS 1994) of the total traffic flow. Therefore, the change in level of service for Alternative 5b would be minimal.

5.11.2 Transportation

This section discusses the potential radiological consequences due to incident and accidents during transport. All SRS onsite shipments are carried out by rail.

5.11.2.1 Onsite Spent Nuclear Fuel Shipments. DOE based the number of fuel

shipments on the amount and type of spent nuclear fuel stored at various SRS locations. The amount of spent nuclear fuel at each location or disposition specified in the spent nuclear fuel alternatives. The number of shipments from each location was determined by dividing the amount of spent nuclear fuel at each location by the capacity of the shipping cask. Individual shipments from the various locations were summed to obtain the total number of shipments for each alternative (HNUS 1994).

Onsite shipments are those that originate and terminate at the SRS. Movements of spent nuclear fuel within functional areas (e.g., H-Area or F-Area) are operational transfers, not shipments; therefore, this analysis does not consider them.

5.11.2.2 Incident-Free Transportation Analysis. Under each alternative, DOE analyzed

incident-free (normal transport) radiological impacts to transport vehicle crews and the general public from onsite rail shipments. The analysis calculated occupational radiation doses to transport vehicle crew members (four locomotive operators). Because the general public has no immediate access to areas where the SRS would transport spent nuclear fuel, the analysis assumed that any general public dose is to escorted individuals on the Site waiting at any of the entrances at the time a fuel shipment passed. The analysis calculated radiological doses to them using the Riskind (Yuan et al. 1993) computer code. The results are presented in Table 5-10.

The magnitude of incident-free consequences depends on the dose rate on the exterior of the transport vehicle, the exposure time, and the number of people exposed. For each alternative, the analysis assumed the external dose rate 2 meters (6.6 feet) from the shipping cask per hour (HNUS 1994), which is the SRS procedurally-allowed maximum dose rate during shipments. Actual receptor dose rates would depend on receptor distance from the shipment [5 meters (16.4 feet) for the general public]. The duration of exposure would depend on vehicle speed and the number of shipments. In addition, occupational exposure time would depend on the distance of each shipment.

The analysis calculated health effects measured as the number of latent cancer fatalities by multiplying the resultant occupational and general public doses by risk factors of 5×10^{-4} latent cancer fatalities per person-rem (DOE 1993a), respectively.

Table 5-10 summarizes the collective doses (person-rem) and health effects (latent cancer fatalities) associated with the incident-free onsite shipment of spent nuclear fuel by alternative.

Option	Occupational (person-rem)	General Public (person-rem)	Number of LCFs Occupational
No Action			
Option 1b - Wet Storage	1.5x100	1.4x10 ⁻¹	6.0x10 ⁻⁴
Decentralization			
Option 2a - Dry Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 2b - Wet Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 2c - Processing	5.3x10 ⁻¹	3.7x10 ⁻²	2.1x10 ⁻⁴
Planning Basis			
Option 3a - Dry Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 3b - Wet Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 3c - Processing	5.3x10 ⁻¹	3.7x10 ⁻²	2.1x10 ⁻⁴
Regionalization			
Option 4a - Dry Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 4b - Wet Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 4c - Processing	5.3x10 ⁻¹	3.7x10 ⁻²	2.1x10 ⁻⁴
Option 4d - Dry Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 4e - Wet Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 4f - Processing	5.3x10 ⁻¹	3.7x10 ⁻²	2.1x10 ⁻⁴
Option 4g - Ship Out	NAb	NAb	NAb

Centralization

Option 5a - Dry Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 5b - Wet Storage	2.5x100	2.3x10 ⁻¹	1.0x10 ⁻³
Option 5c - Processing	5.3x10 ⁻¹	3.7x10 ⁻²	2.1x10 ⁻⁴
Option 5d - Ship Out	NAb	NAb	NAb

a. LCF = latent cancer fatality.

b. NA = not applicable.

doses and latent cancer fatalities for members of the public would be approximately than those for the occupational worker. The data indicate that the lowest collective latent cancer fatality would be associated with the Processing option under the Dec Planning Basis, Regionalization, and Centralization alternatives.

5.11.2.3 Transportation Accident Analysis. DOE analyzed radiological impacts from

potential accidents to both the onsite maximally exposed individual (MEI), and offsite general public from onsite rail shipments. The analysis calculated doses using the (et al. 1993) computer code with site-specific meteorology, demographics, and spent fuel was calculated using site-specific rail accident rates and accident probabilities.

The magnitude of accident consequence would depend on the amount of radioactive material which the individual(s) was exposed, the exposure time, and the number of people exposed. The analysis assumed that the maximum reasonably foreseeable amount of radioactive material of spent fuel shipped on the SRS was released (HNUS 1994). The assumed duration of each receptor was 2 hours. The assumed maximally exposed individual was an SRS worker downwind of the accident at distances of 50 and 100 meters (164 and 330 feet).

The analysis calculated offsite exposure using both rural and suburban population census data. The rural and suburban population densities have an average of 6 persons per kilometer and 244 persons per square kilometer, respectively. The west-northwest has the highest population density within 80 kilometers (50 miles) of the SRS.

The analysis used site-specific meteorology at the 50th and 95th percentile to estimate consequences. Joint probability includes both the event frequency and the probability of reasonably foreseeable type of accident occurring.

The analysis calculated health effects measured as the number of latent cancer fatalities by multiplying the resultant occupational and general public doses by the risk factors of 5×10^{-4} latent cancer fatalities per person-rem (DOE 1993a), respectively. Risk was calculated by multiplying the resultant doses by the joint probability of 1×10^{-4} (HNUS 1994).

Tables 5-11 and 5-12 summarize the collective doses and associated latent cancer fatalities postulated onsite rail accidents with subsequent releases of radioactive material. The dose consequences of an accidental release of radioactive material was assessed under typical 50th percentile meteorological conditions (i.e., those that would result in percent of the time, respectively). In all cases the estimated number of latent cancer fatalities is low.

5.11.3 Onsite Mitigation and Preventative Measures

All onsite shipments must be in compliance with DOE Savannah River Directive Instruction 5480.3, "Safety Requirements for the Packaging and Transportation of Hazardous Substances, and Hazardous Wastes." DOE, DOE-SR, or the Nuclear Regulatory Commission (NRC) must approve packages used for onsite shipments with a certificate of approval. **Table 5-11.** Impacts on maximally exposed individual from spent nuclear fuel transportation on the Savannah River Site.

Dose Percentile	Distance (meters)	Dose to MEIa (rem)	Number of LCFsb per year	Risk
50 percent	100	0.16	6.4×10^{-5}	1.6×10^{-3}
95 percent	50	0.37	1.5×10^{-4}	3.7×10^{-3}

a. MEI = maximally exposed individual.

b. LCF = latent cancer fatality.

Table 5-12. Impacts on offsite population from spent nuclear fuel transportation at the Savannah River Site.

Population Density Category	Dose Percentile	Offsite Population Dose (person-rem)	Number of LC per year
Rural	50th	1.7	8.7×10^{-4}
Rural	95th	7.1	3.6×10^{-3}

Suburban	50th	5.2	2.6x10 ⁻³
Suburban	95th	21.3	1.1x10 ⁻²

a. LCF = latent cancer fatality.

compliance. If DOE or NRC has not certified an onsite package as Type B, the shipping administrative controls and site-mitigating circumstances that will ensure package administrative and emergency response considerations must provide sufficient controls would not result in loss of containment, shielding, or criticality; or the uncontrolled radioactive material would not create a hazard to the health and safety of the public.

In the event of an accident, SRS has established an emergency management program that incorporates activities associated with emergency planning, preparedness, and

5.12 Occupational and Public Health and Safety

5.12.1 Radiological Health

This human health effects analysis relied principally on data on F- and H-Area operations documented for the 1985, 1986, and 1993 operating years (Marter 1986; 1987; WSRC 1987). Therefore, that these emissions represent conservative estimates as to the emission from spent nuclear fuel management activities at the SRS. This air and surface-water information defined the source terms for the baseline evaluation (No Action alternative effects discussed in this section). To estimate health effects, this analysis defined groups:

- The F- and H-Area workers assigned to F- and H-Area operations involving nuclear materials
- The F- and H-Area workers assigned to the Receiving Basin for Offsite Fuels operations
- The maximally exposed individual residing at the SRS boundary
- The projected 1994 offsite population of 628,200 persons residing within an (50-mile) radius of F- and H-Areas
- The maximally exposed individual potentially affected by SRS surface-water
- The approximate offsite population of 65,000 persons whom SRS surface-water could affect.

With the exception of the worker group, this analysis calculated exposures for receptor groups using the baseline source terms as input data to automated atmospheric transport, human intake, and human dosimetry models configured for routine use (Hamby 1994). The analysis estimated worker exposures using averaged dosimetry data for F- and H-Area workers from 1983 through 1987 and Receiving Basin for Offsite Fuels 1993 (Matheny 1994), corrected for an assumed occupancy factor of 0.25 (i.e., a worker potentially exposed during one-quarter of his/her shift). This correction was applied to data only. At the SRS, the waterborne exposure pathway does not exist for the worker because Site drinking water is drawn from deep aquifers unaffected by any radiological contamination.

The analysis developed incremental receptor group exposure estimates (millirem per year; effective dose equivalent) based on spent fuel quantities for each of alternatives (i.e., Alternatives 2 through 5) and their options by applying calculations of heavy metal (MTHM) for each alternative and option compared to the No Action alternative. DOE used these ratios as incremental scaling factors to estimate exposures under each alternative. The calculation of the MTHM ratios used the data presented in Table 3-1. Table 5-13 lists the exposure estimate calculations. Since these incremental exposures include control effective dose equivalent from existing (No Action) spent fuel management at the SRS, health effects for each alternative can be estimated as the difference between the incremental exposure and the No Action exposure.

The analysis calculated the potential health effects expressed in the exposed receptor groups consistent with risk determination guidance issued by the DOE Office of NEPA Oversight (1993a) and International Commission on Radiological Protection Publication 60 (ICRP 1991). For exposed individuals and populations, the potential health effect (detriment) of interest is cancer. For exposed individuals, this analysis presents the health effect as the maximum probability for detriment expression; for exposed populations, it presents the annual detriment incidence. For completeness, it also provides the "project life" (i.e., incidence as the annual incidence multiplied by 40). Table 5-14 (worker) and Table 5-15 (exposed individual and offsite population) summarize the health effects calculation.

The Centers for Disease Control and Prevention is conducting a comprehensive review of historic offsite doses associated with SRS operations. The results of this investigation will be available in the future.

available.

5.12.2 Nonradiological Health

DOE used the operations air quality data listed in Tables 5-3, 5-4, 5-5 and 5-6 WSRC 1994a) to evaluate health impacts associated with potential exposure to the compound classes: criteria pollutants and toxic pollutants. The analysis evaluate receptor locations: (1) a worker in S-Area and (2) a maximally exposed individual boundary. However, it was unnecessary to postulate an intake of criteria pollutant by these receptors because airborne concentration standards are available for these

Tables 5-3 and 5-4 list 8 criteria pollutants and 23 toxic compounds. The toxic classified as carcinogens and noncarcinogens consistent with Environmental Protection Agency carcinogenicity group (weight of evidence) designations published in the Integrated Table 5-13. Incremental radioactive contaminant annual exposure summary.

Onsite Workersa

Alternative	(mrem/ year)c	(person- rem/ year)
No Action - Wet Storage (Option 1)	100	0.2
Decentralization - Dry Storage (Option 2a)	83	0.2
Decentralization - Wet Storage (Option 2b)	104	0.2
Decentralization - Processing (Option 2c)	145	70
Planning Basis - Dry Storage (Option 3a)	84	0.2
Planning Basis - Wet Storage (Option 3b)	105	0.2
Planning Basis - Processing (Option 3c)	147	71
Regionalization A - Dry Storage (Option 4a)	83	0.2
Regionalization A - Wet Storage (Option 4b)	103	0.2
Regionalization A - Processing (Option 4c)	148	76
Regionalization B - Dry Storage (Option 4d)	105	0.2
Regionalization B - Wet Storage (Option 4e)	131	0.3
Regionalization B - Processing (Option 4f)	175	74
Regionalization B - Ship Out (Option 4g)	<100	<0.2
Centralization - Dry Storage (Option 5a)	1,102	2.2
Centralization - Wet Storage (Option 5b)	1,377	2.8
Centralization - Processing (Option 5c)	1,422	79
Centralization - Ship Out (Option 5d)	<100	<0.2

a. Insignificant digits are displayed for comparison purposes only.

b. MEI = maximally exposed individual.

c. The DOE administrative dose limit is 2,000 mrem (DOE 1994a).

d. Data is provided separately for the air and water exposure pathways because the co-located.

Table 5-14. Incremental fatal cancer incidence and maximum probability for workers

Alternative	Annual Incidencea	40-Year Incidence
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No Action - Wet Storage (Option 1)	8x10 ⁻⁵	3x10 ⁻³
Decentralization - Dry Storage (Option 2a)	7x10 ⁻⁵	3x10 ⁻³
Decentralization - Wet Storage (Option 2b)	8x10 ⁻⁵	3x10 ⁻³
		-3
Decentralization - Processing (Option 2c)	3x10 ⁻²	1
Planning Basis - Dry Storage (Option 3a)	7x10 ⁻⁵	3x10 ⁻³
Planning Basis - Wet Storage (Option 3b)	8x10 ⁻⁵	3x10 ⁻³
		-3
Planning Basis - Processing (Option 3c)	3x10 ⁻²	1
Regionalization A - Dry Storage (Option 4a)	7x10 ⁻⁵	3x10 ⁻³
Regionalization A - Wet Storage (Option 4b)	8x10 ⁻⁵	3x10 ⁻³
		-3
Regionalization A - Processing (Option 4c)	3x10 ⁻²	1
Regionalization B - Dry Storage (Option 4d)	8x10 ⁻⁵	3x10 ⁻³
Regionalization B - Wet Storage (Option 4e)	1x10 ⁻⁴	4x10 ⁻³
		-3
Regionalization B - Processing (Option 4f)	3x10 ⁻²	1
Regionalization B - Ship Out (Option 4g)	<8x10 ⁻⁵	<3x10 ⁻³
Centralization - Dry Storage (Option 5a)	9x10 ⁻⁴	4x10 ⁻²
Centralization - Wet Storage (Option 5b)	1x10 ⁻³	4x10 ⁻²
		-2
Centralization - Processing (Option 5c)	3x10 ⁻²	1
Centralization - Ship Out (Option 5d)	<8x10 ⁻⁵	<3x10 ⁻³

a. Number of latent fatal cancers over a lifetime which could be attributed to one nuclear fuel management activities.

System (IRIS) data base (DOE 1994b). For purposes of health effects analysis, carc compounds designated Group A (human carcinogens), Group B1 (probable human carcinog evidence in human studies), Group B2 (probable human carcinogen, inadequate evidenc from human studies), and Group C (possible human carcinogen). Using this designati 23 toxic compounds are carcinogens: benzene (Group A), formaldehyde (Group B1), an chloride (Group B2).

Carcinogen health effects are expressed as the incremental probability of an in developing cancer, assuming a lifetime (70 years) of exposure to the carcinogen. D risk (slope) factors published in IRIS (Integrated Risk Information System) to obta (risk per concentration) needed to calculate incremental probability. Carcinogens incomplete or unavailable carcinogen assessment data) information listed in the Int Information System data base precluded a quantitative risk assessment; this analysi noncarcinogens.

Table 5-15. Incremental fatal cancer incidence and maximum probability for the max individual and offsite population (air and water pathways).

Alternative	Population Annual Incidencea	Population 40-Year Incidence
No Action - Wet Storage (Option 1)		
Air	2x10 ⁻⁹	7x10 ⁻⁸
Water	3x10 ⁻¹⁰	1x10 ⁻⁸
Decentralization - Dry Storage (Option 2a)		
Air	2x10 ⁻⁹	6x10 ⁻⁸
Water	2x10 ⁻¹⁰	9x10 ⁻⁹
Decentralization - Wet Storage (Option 2b)		
Air	2x10 ⁻⁹	8x10 ⁻⁸
Water	3x10 ⁻¹⁰	1x10 ⁻⁸
Decentralization - Processing (Option 2c)		
Air	7x10 ⁻³	0.3
Water	1x10 ⁻³	4x10 ⁻²
Planning Basis - Dry Storage (Option 3a)		
Air	2x10 ⁻⁹	6x10 ⁻⁸
Water	2x10 ⁻¹⁰	9x10 ⁻⁹
Planning Basis - Wet Storage (Option 3b)		
Air	2x10 ⁻⁹	8x10 ⁻⁸
Water	3x10 ⁻¹⁰	1x10 ⁻⁸
Planning Basis - Processing (Option 3c)		
Air	7x10 ⁻³	0.3
Water	1x10 ⁻³	4x10 ⁻²

Regionalization A - Dry Storage (Option 4a)		
Air	2x10 ⁻⁹	6x10 ⁻⁸
Water	2x10 ⁻¹⁰	9x10 ⁻⁹
Regionalization A - Wet Storage (Option 4b)		
Air	2x10 ⁻⁹	8x10 ⁻⁸
Water	3x10 ⁻¹⁰	1x10 ⁻⁸
Regionalization A - Processing (Option 4c)		
Air	8x10 ⁻³	0.3
Water	1x10 ⁻³	5x10 ⁻²
Regionalization B - Dry Storage (Option 4d)		
Air	2x10 ⁻⁹	8x10 ⁻⁸
Water	3x10 ⁻¹⁰	1x10 ⁻⁸
Regionalization B - Wet Storage (Option 4e)		
Air	2x10 ⁻⁹	1x10 ⁻⁷
Water	4x10 ⁻¹⁰	1x10 ⁻⁸
Regionalization B - Processing (Option 4f)		
Air	8x10 ⁻³	0.3
Water	1x10 ⁻³	5x10 ⁻²
Regionalization B - Ship Out (Option 4g)		
Air	<2x10 ⁻⁹	<7x10 ⁻⁸
Water	<3x10 ⁻¹⁰	<1x10 ⁻⁸

Table 5-15. (continued).

Alternative	Population Annual Incidencea	Population 40-Year Incidence
Centralization - Dry Storage (Option 5a)		
Air	2x10 ⁻⁸	8x10 ⁻⁷
Water	3x10 ⁻⁹	1x10 ⁻⁷
Centralization - Wet Storage (Option 5b)		
Air	3x10 ⁻⁸	1x10 ⁻⁶
Water	4x10 ⁻⁹	2x10 ⁻⁷
Centralization - Processing (Option 5c)		
Air	8x10 ⁻³	0.3
Water	1x10 ⁻³	5x10 ⁻²
Centralization - Ship Out (Option 5d)		
Air	<2x10 ⁻⁹	<7x10 ⁻⁸
Water	<3x10 ⁻¹⁰	<1x10 ⁻⁸

a. Number of latent fatal cancers over a lifetime that could be attributed to one management activities.

This analysis evaluated noncarcinogenic and priority pollutant compound health hazard quotients to obtain a hazard index. The hazard quotient is the ratio of com or dose to a Reference Concentration (RfC) or Dose (RfD) (EPA 1989). The regulator in this analysis was the more stringent of the following: (1) Occupational Safety Administration (OSHA) 8-hour permissible exposure limit (PEL), (2) American Confere Governmental Industrial Hygienists (ACGIH) threshold limit value (TLV), or (3) Stat Carolina air quality standards. The use of the noncancer hazard index assumed a le (i.e., RfC) below which adverse health effects are unlikely. The hazard index is n probability; therefore it cannot be interpreted as such.

Table 5-16 summarizes nonradiological health effects attributable to atmospheric toxic and criteria pollutant compounds. Because no hazard index value would exceed adverse health effects are unlikely under any alternative.

5.12.3 Industrial Safety

This section describes the following measures of impact for workplace hazards: reportable injuries and illnesses and (2) fatalities in the work force. This analy injury/illness and fatality incidence rates for construction workers separately bec Table 5-16. Nonradiological annual incremental health effects summary.

Alternative	Worker Cancer Probabilitya	Worker Hazard Index
No Action - Wet Storage (Option 1)	Insufficient data	2x10 ⁻⁶

Decentralization - Dry Storage (Option 2a)	Insufficient data	2x10 ⁻⁶
Decentralization - Wet Storage (Option 2b)	Insufficient data	2x10 ⁻⁶
Decentralization - Processing (Option 2c)	Insufficient data	6x10 ⁻³
Planning Basis - Dry Storage (Option 3a)	Insufficient data	2x10 ⁻⁶
Planning Basis - Wet Storage (Option 3b)	Insufficient data	2x10 ⁻⁶
Planning Basis - Processing (Option 3c)	Insufficient data	6x10 ⁻³
Regionalization A - Dry Storage (Option 4a)	Insufficient data	2x10 ⁻⁶
Regionalization A - Wet Storage (Option 4b)	Insufficient data	2x10 ⁻⁶
Regionalization A - Processing (Option 4c)	Insufficient data	6x10 ⁻³
Regionalization B - Dry Storage (Option 4d)	Insufficient data	2x10 ⁻⁶
Regionalization B - Wet Storage (Option 4e)	Insufficient data	2x10 ⁻⁶
Regionalization B - Processing (Option 4f)	Insufficient data	8x10 ⁻³
Regionalization B - Ship Out (Option 4g)	Insufficient data	2x10 ⁻⁶
Centralization - Dry Storage (Option 5a)	Insufficient data	2x10 ⁻⁶
Centralization - Wet Storage (Option 5b)	Insufficient data	2x10 ⁻⁶
Centralization - Processing (Option 5c)	Insufficient data	6x10 ⁻³
Centralization - Ship Out (Option 5d)	Insufficient data	2x10 ⁻⁶

a. Insufficient data exists in the IRIS data base to perform a quantitative inhalat
b. MEI = maximally exposed individual.

more hazardous nature of construction work. Table 5-17 lists the incidence of inju
fatalities for construction and non-construction workers. These data are for the h
year (i.e., maximum hours worked in any year from 1994 through 2035, assuming 2,000
worker) (WSRC 1994b). This analysis used the average occupational injury/illness a
incidence rates experienced by DOE and its contractors from 1988 through 1992 to ca
incidence of industrial hazards listed in Table 5-17 (DOE 1993b).

Table 5-17. Incremental industrial hazard maximum annual incidence summary.

Alternative	Construction Injuries and Illnesses	Construction Fatalities
No Action - Wet Storage (Option 1)	92	<1
Decentralization - Dry Storage (Option 2a)	71	<1
Decentralization - Wet Storage (Option 2b)	71	<1
Decentralization - Processing (Option 2c)	66	<1
Planning Basis - Dry Storage (Option 3a)	71	<1
Planning Basis - Wet Storage (Option 3b)	82	<1
Planning Basis - Processing (Option 3c)	66	<1
Regionalization A - Dry Storage (Option 4a)	82	<1
Regionalization A - Wet Storage (Option 4b)	82	<1

Regionalization A - Processing (Option 4c)	66	<1
Regionalization B - Dry Storage (Option 4d)	89	<1
Regionalization B - Wet Storage (Option 4e)	102	<1
Regionalization B - Processing (Option 4f)	82	<1
Regionalization B - Ship Out (Option 4g)	22	<1
Centralization - Dry Storage (Option 5a)	316	1
Centralization - Wet Storage (Option 5b)	337	1
Centralization - Processing (Option 5c)	316	1
Centralization - Ship Out (Option 5d)	22	<1

5.13 Utilities and Energy

The existing capacities and distribution systems at the SRS for electricity, steam, and domestic wastewater treatment are adequate to support any of the five alternatives. This section summarizes estimates of the annual requirements for electricity, steam, and domestic wastewater treatment for each alternative and case, and compares them to current SRS usage of Table 5-8 lists information on water usage by alternative. The utility and energy Table 5-18. Estimates of annual electricity, steam, and domestic wastewater treatment for each alternative. ,b

Alternative	Electricity Usage (megawatt hours per year)	Steam (kilowatt hours per year)
Current SRS Usage	659,000	1.7
1. No Action		
Option 1 - Wet Storage	1,400	11.
2. Decentralization		
Option 2a - Dry Storage	19,400	16.
Option 2b - Wet Storage	22,400	14.
Option 2c - Processing	56,400	19.
3. 1992/1993 Planning Basis		
Option 3a - Dry Storage	19,400	16.
Option 3b - Wet Storage	22,400	14.
Option 3c - Processing	56,400	19.
4. Regionalization - A		
Option 4a - Dry Storage	24,400	16.
Option 4b - Wet Storage	27,400	14.
Option 4c - Processing Regionalization - B	67,400	16.
Option 4d - Dry Storage	24,400	16.
Option 4e - Wet Storage	27,400	14.
Option 4f - Processing	56,400	19.
Option 4g - Ship Out	11,400	11.
5. Centralization		
Option 5a - Dry Storage	44,400	16.

Option 5b - Wet Storage	47,400	14.
Option 5c - Processing	110,400	19.
Option 5d - Ship Out	11,400	11.

a. Source: WSRC (1994b).

b. Water requirements are shown in Table 5-8.

c. To convert kilograms to pounds, multiply by 2.2046.

d. To convert liters to gallons, multiply by 0.26418.

the alternatives represent a small percentage of current requirements. No new gene facilities would be necessary; connections to existing networks would require only Increases in SRS fuel consumption would be minimal because overall activity on the increase due to changes in the SRS mission and the general reduction in employment overall impacts of any of the alternatives on the SRS utilities and energy resource

The smallest increase in demand would result from the No Action alternative, wh similar to current spent nuclear fuel-related requirements at the SRS. The largest due to the centralization of spent nuclear fuel at the SRS (Alternative 5). Altern a maximum additional electrical demand of about 110,400 megawatt-hours annually (Op an increased steam consumption of about 19.1 million kilograms (42.1 million pounds (Option 5c). Water requirements would also be greatest under this Alternative (Tab withdrawals of Savannah River water for cooling purposes would reach about 310.8 mi (82.1 million gallons) and groundwater usage for domestic and processing purposes w approximately 69.6 million liters (18.4 million gallons). The volume of domestic w treatment would range from approximately 35 to 70 million liters (9 to 18 million g This additional water usage amounts to an increase of about 10 percent over current requirements.

Among the three management options, processing would result in the greatest inc on utilities and energy in comparison to either the dry or wet storage options. In storage would be similar in their requirements of these resources.

5.14 Materials and Waste Management

This section discusses potential impacts of the management of materials and was with the implementation of alternatives identified for spent nuclear fuel managemen 5.12 (Air Quality and Occupational and Public Health and Safety, respectively) disc hazardous and toxic materials as they relate to routine operations and accidents.

DOE has projected rates and volumes of waste and impacts of waste generation at level, transuranic, and high-level wastes for each of the alternatives for spent nu Table 5-19 summarizes the estimated annual average and total volume of these three each alternative would produce during a 40-year management period. The discussion Table 5-19. Annual average and total volume (cubic meters)d of radioactive wastes each alternative during the 40-year interim management period.

Alternative	Low-level wasteb		Transuranic waste	
	Average	Total	Average	T
1. No Action				
Option 1 - Wet Storage	400	16,000	17	7
2. Decentralization				
Option 2a - Dry Storage	400	16,000	18	7
Option 2b - Wet Storage	400	16,000	18	7
Option 2c - Processing	800	32,000	19	7
3. 1992/1993 Planning Basis				
Option 3a - Dry Storage	400	16,000	18	7
Option 3b - Wet Storage	400	16,000	18	7
Option 3c - Processing	750	30,000	19	7
4. Regionalization - A				
Option 4a - Dry Storage	400	16,000	17	7
Option 4b - Wet Storage	400	16,000	17	7
Option 4c - Processing	790	31,600	18	7
4. Regionalization - B				
Option 4d - Dry Storage	400	16,000	17	7
Option 4e - Wet Storage	400	16,000	17	7
Option 4f - Processing	790	31,600	18	7
Option 4g - Ship Out	400	4,000	18	1
5. Centralization				

Option 5a - Dry Storage	400	16,000	16	6
Option 5b - Wet Storage	400	16,000	20	8
Option 5c - Processing	800	32,000	20	8
Option 5d - Ship Out	400	4,000	18	1

a. Based on WSRC (1994b).

b. Source: WSRC (1994c).

c. Figures are for the initial 10-year period when most processing would be complete.
d. To convert cubic meters to cubic yards multiply by 1.307.

below also identifies the impacts that the waste produced by spent nuclear fuel act on the existing SRS capacity to manage each waste type.

DOE has not developed estimates of low-level mixed, hazardous, or solid sanitary spent nuclear fuel management activities at the SRS could generate, although it is these activities would produce these waste types only in limited quantities. Further, Section 5.14.2 related to the impacts of spent fuel management wastes on the SRS would not include considerations of wastes that will result from Site cleanup because assessment activities are still underway and will undergo NEPA review as part of the SRS Waste Environmental Impact Statement (DOE 1995).

Volume 1 of this spent nuclear fuel EIS provides information concerning the major environmental laws and regulations, Executive Orders, and DOE Orders that apply to prevention at the Savannah River Site. The DOE views source reduction as the first pollution prevention program, followed by an increased emphasis on recycling. Source reduction reduces the waste management burden while eliminating the potential for future liability. Recycling and using recycled materials will conserve resources and landfill space. Incineration and disposal are considered only when prevention or recycling is not possible or practical. In creating a Savannah River Site waste minimization program (the precursor of the SRS prevention program) in 1990, the amounts of wastes of all types (excluding low-level wastes, a by-product of environmental restoration activities) generated have decreased, and reductions in hazardous and mixed wastes (Hoganson and Miles 1994).

5.14.1 Alternative Comparison

The first four alternatives would generate similar amounts of radioactive waste activities that produce the wastes would be similar under each of the alternatives. Low-level and transuranic wastes would be generated during the first part of the 40-year period while DOE was transferring existing inventory and renovating the Receiving Building, Fuel Storage Basins, and a reactor basin. The characterization and canning of the current inventory for placement into storage would also result in some waste generation. Once in storage, activities would produce only small amounts of radioactive waste for the rest of the period.

The dry- and wet-storage options would both produce about 16,000 cubic meters (11,964 cubic yards) of low-level waste and between 640 cubic meters (836 cubic yards) and 800 cubic meters (1,046 cubic yards) of transuranic waste during the 40-year management period. Both would generate small amounts of high-level waste. The processing of the existing aluminum-clad fuels (the third option under each alternative) would generate all low-level and high-level wastes in appreciably greater volumes, and transuranic wastes in greater volumes.

Alternative 5 (excluding the Ship Out option) could result in somewhat larger volumes of radioactive waste than the other four alternatives. However, any increase in waste is directly proportional to the larger amounts of fuel that would be managed on the Site. The originating sites would characterize and can their fuel prior to shipment so that it can be shipped directly into storage at the SRS. Therefore, the radioactive wastes produced during the Site would come from the initial fuel transfer and pool renovations and from the canning of small amounts of new fuel. The processing of existing aluminum-clad fuels would produce the same types and volumes of waste as for the other alternatives.

The option for shipping the SRS inventory off the Site for regionalization or storage elsewhere would also result in the production of some radioactive waste. This would require characterization and canning prior to shipment and would generate the smallest volume of waste of any alternative action: 4,000 cubic meters (5,228 cubic yards) of low-level waste and 235 cubic yards of transuranic waste. This waste would be produced only during the first 10 years of the management period.

5.14.2 Impact on the SRS Waste Management Capacity

The impact of spent nuclear fuel activities on SRS waste management capacities minimal because the Site could accommodate the waste with existing and planned radi storage and disposal facilities. DOE would transfer high-level waste to the F/H Ta volume reduction and then to the Defense Waste Processing Facility (DWPF) for convey borosilicate glass form suitable for prolonged storage. The SRS would use the Cons Incineration Facility, once operational, to treat the low-level waste. This facility permitted capacity [105,500 cubic meters (137,889 cubic yards) per year] to treat the volume of these materials. However, actual through-put volume is dependent upon variables and waste characteristics. The F/H Effluent Treatment Facility would treat waste. This facility has sufficient design process capacity [598 million liters (1 year)] to treat the anticipated volumes of these materials. DOE would manage the transfer with existing and planned storage capacity.

5.15 Accident Analysis

Operations involving the receipt, handling, processing, or storing of spent nuclear involve radioactive materials or toxic chemicals. These materials would be received, transferred between facilities, disposed of on the Site, and shipped off the Site. In circumstances, these materials could be involved in an accident.

An accident is a series of unexpected or undesirable events initiated by equipment error, or a natural phenomenon such as severe weather, earthquake, or volcanism. That cause the release of either radioactive or chemically toxic materials inside a facility environment.

This section summarizes analyses of possible accidents involving spent nuclear fuel at the SRS. To provide a perspective on potential accidents, this section summarizes analyses associated with spent nuclear fuel activities that have occurred at the SRS (historical reviews previous accident analyses for Site operations. This section uses the results of analyses as a baseline for determining the impacts for the alternatives that involve each alternative, this section discusses the accidents with the largest point estimates (radiological impacts in terms of potential fatal cancers x frequency of the initial

The facilities considered for each alternative are either existing facilities for which safety analyses were used, or new facilities (WSRC 1994b) for which existing safety analyses were substituted by evaluating the type of accident(s) that could be postulated to occur at the projected function of the facility. Two facilities that contain very small amounts of spent nuclear fuel, Buildings 331-M and 773-A, were not included in this analysis because they were analyzed for the major facilities would bound the consequences of possible accident locations.

This section addresses historic accidents, facility radiological accidents, chemical accidents, and secondary impacts. Section 5.11 addresses onsite transportation accidents.

5.15.1 Historic Accidents at the Savannah River Site

Impacts from accidents can involve fatalities, injuries, or illness. Fatalities (immediate) such as in construction accidents or latent (delayed) such as an increase in cancers due to radiation exposure. Section 5.12 addresses worker injuries, illness for increased cancer risk anticipated from normal operations of the facilities. No accidents have dominated impacts to workers at the SRS (Durant et al. 1987); impacts to the public from historic SRS accidents have been negligible.

The SRS has maintained an operational event data base on its facilities since the 1950s. The data base currently contains approximately 450,000 entries including data on the Reprocessing Offsite Fuel, the principal wet storage pool facility at the SRS; and both F-and H- this EIS, DOE reviewed the data base to identify historic spent nuclear fuel-related accidents. Fuel cutting events, fuel handling events, and various liquid releases from fuel management over the 40-year operating history of the SRS were examined. The purpose of the data base review was to provide an historic perspective on the types of accidents that have occurred at the SRS. Events representative of fuel failures include higher than expected contamination of fuel storage basin water and evidence of fuel canister cracking at a weld. Fuel handling accidents are due in large part to crane operator errors or crane and handling equipment failures. These historical events provided a basis for the selection of representative accidents for the spectrum of spent nuclear fuel management activities. No significant offsite impacts

from these historic occurrences.

5.15.2 Potential Facility Accidents

The SRS spent nuclear fuel alternatives have the potential for radiological accidents (Attachment A, Table A-2) that could affect the health and safety of workers and the concerns and characteristics that are common to these accidents would be common regardless of whether the cause were a natural phenomenon or human error. For health effects to occur, there must be a release of hazardous material to, or an increase in radiation levels in the environment. The released material must be transported to locations frequented by large quantities of hazardous materials that reach locations where people are and the way people are important factors in the determination of health effects.

A number of studies have investigated the ways in which radioactivity reaches the human body, how it is absorbed and retained, and the resulting health effects. The International Commission on Radiological Protection has made specific recommendations for estimating these health effects (ICRP 1991). This organization is the recognized body for establishing standards for workers and the public from the effects of radiation exposure. Health effects include acute effects (up to and including death) and latent effects, including cancers and genetic damage. The SRS-developed computer code, AXAIR89Q, estimates potential radiation doses to maximum individuals or population groups from accidental releases of radionuclides.

The AXAIR89Q code is a highly automated site-specific environmental dispersion code for postulated airborne releases. The environmental dispersion models used are described in Regulatory Guide 1.145 (NRC 1983). The exposure pathways considered in the AXAIR89Q code include inhalation of radionuclides and gamma irradiation from the radioactive plume.

Doses from the inhalation of radionuclides in air depend on the amount of radioactivity released, the dispersion factor; the physical, chemical, and radiological characteristics of the radionuclides; various biological parameters such as breathing rate and biological half-life. The code uses a conservative breathing rate of 12,000 cubic meters (424,000 cubic feet) per day. Dose commitment factors used in the environmental dosimetry code, as described in this section, are from Internal Dose Conversion Factors for Calculation of Dose to the Public (NRC 1983).

External gamma radiation doses from the traveling plume depend on the spatial distribution of the radionuclides in the air, the energy of the radiation, and the extent of shielding. The code takes no credit for shielding in calculating doses. The code calculates gamma doses using a nonuniform Gaussian model, which has more realistic modeling than doses from the conventional uniform semi-infinite plume model.

In addition to using the worst sector, 99.5 percentile meteorology, conservative meteorology, and taking no credit for shielding, the AXAIR89Q code also takes no credit for the rise from stack releases. Therefore, the offsite maximum individual doses calculated provide conservative bounding estimates of radiological consequences to exposed individuals and populations from postulated accidental atmospheric releases.

AXAIR89Q has been validated for compliance to accepted standards for such software. Attachment A, Accident Analysis, discusses AXAIR89Q and its predecessor, AXAIR. When used in conjunction with models for predicting health effects, the results from AXAIR89Q can be compared with other site-specific codes such as RSAC-5, because both codes provide relative concentrations based on the guidance provided in NRC Regulatory Guide 1.145.

This section summarizes the potential for radiological accidents and their consequences under each alternative. Attachment A describes the methodology and assumptions used in the assessment; describes radiological accident scenarios in more detail; provides source term estimates used to estimate the doses and impacts for each alternative and case; and lists factors that the DOE decisionmaker can apply to the source term or dose for each facility and case.

DOE assessed the potential impacts from a selected spectrum of radiological releases ranging from low (1×10^{-6} event per year) to high (more than 1 event per year) frequency of occurrence, along with the associated impacts (doses and potential latent fatal cancer risk). The accidents used as references are attributed to individual facilities and processes (see Attachment A, Table A-3), not to specific cases or alternatives. A comparison of alternatives depending on which facilities support a specific case or process is shown in Figure 5-1, a flowchart for the preparation of accident analysis information. No accidents occurred because existing documentation adequately supports a quantitative or qualitative assessment of potential impacts, as required by the National Environmental Policy Act of 1969. The postulated radiological accidents associated with spent nuclear fuel at the SRS and the highest point estimate of risk to the public within 80 kilometers (50 miles) of the SRS is a 1.4×10^{-3} latent fatal cancer per year. The estimated dose to the same population

including natural background sources, would be about 19,000 person-rem per year (DO could cause about nine latent fatal cancers per year in the same population. For p background radiation sources would result in approximately 6,000 times the risk as largest consequence accident postulated in this EIS for the various spent nuclear f alternatives.

DOE did not quantitatively analyze the potential health effects for SRS workers meters (328 feet) from radiological accidents. Computer codes used to calculate ra experience potentially large errors as a source disperses throughout a building. H carry out a qualitative evaluation of the potential radiological effects to SRS wor vicinity of an accident related to spent fuel management. DOE estimates that the c accident for the most part would result in higher than normal radiation doses. How would occur except in the event of an inadvertent criticality in FB-Line, where up may result. This evaluation is discussed in more detail in Section A.2.6.2 of Atta

5.15.2.1 Alternative 1 - No Action. This alternative identifies the minimum actions deemed

necessary for continued safe and secure management of spent nuclear fuel at the SRS Chapter 3, this is not a status quo condition. Spent nuclear fuel would be maintai defueling or current storage locations with minimal facility upgrade or equipment r local transport would occur. SRS activities required to safely store spent nuclear This alternative would require SRS to place corroded and pitted fuel elements in ca spread of material into the pool. DOE estimated potential radiological accident im occur under this alternative using existing DOE-approved safety analyses for the in

Figure 5-1. Accident analysis process. spent nuclear fuel at SRS facilities. As under this alternative would consist of existing facilities, including necessary up interim wet storage. In addition, Attachment A, Table A-4, provides a reference ac associated with these facilities for this alternative. Attachment A, Table A-2, li the source terms considered in analyzing potential accidents under this alternative estimated frequencies. Table 5-20 lists the accident scenario with the highest poin the general public. Table 5-21 compares the potential radiological accidents and h interim wet storage (Option 1) of spent nuclear fuel for the No Action alternative. **Table 5-20.** Highest point estimates of risk among receptor groups (Option 1).

	Receptor Groups	Pop
	Maximally Exposed	
	Offsite Individual	
Overall Point Estimate of Riska	1.6x10 ⁻⁷ (Fuel Assembly Breach)	1.4
a. Units of latent fatal cancers per year.		

5.15.2.2 Alternative 2 - Decentralization. Accident assessments considered for this

alternative include those considered for the No Action alternative for wet storage assessments for the dry storage (Option 2a) of spent nuclear fuel and for the proce (Option 2c). Option 2c (processing) assumes the use of existing facilities to diss further stabilize spent nuclear fuel. For cases that include some treatment (e.g., nuclear fuel, such treatment is referred to as "stabilization," not processing. Th various types to be considered would include those quantities from the production r research fuel, foreign research reactor fuel, and fuel transported for safety or re

5.15.2.2.1 Option 2a - Dry Storage - DOE estimated potential radiological accident

impacts that could occur in this case using existing DOE-approved safety analysis r DOE by Westinghouse Savannah River Company for vault storage of special nuclear mat existing facilities.

DOE has not incorporated the technology to support interim dry storage of spent nuclear fuel at the SRS. To provide a basis for evaluating the potential impacts f case, this assessment used data from existing safety analyses for special nuclear m facilities and extrapolated these data to apply to spent nuclear fuel. DOE also co accidents associated with wet storage, at least in the near term, because the spent currently in wet storage. Similarly, this assessment includes fuel handling accide transition phase (i.e., until fuel is in interim dry storage). As indicated in Att **Table 5-21.** Radioactive release accidents and health effects for spent nuclear fue

Alternative (by case)	Accident Scenario	Frequency (per year)
1. No Action		
Option 1 Wet Storage	A1 Fuel Assembly Breach	1.6x10 ⁻¹
	A4 Material Release (Adjacent Facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
2. Decentralization		
Option 2a Dry Storage	A1 Fuel Assembly Breach	1.6x10 ⁻¹
	A3 Material Release (Dry Vault)	1.4x10 ⁻³
	A4 Material Release (Adjacent Facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
Option 2b Wet Storage	A1 Fuel Assembly Breach	1.6x10 ⁻¹
	A4 Material Release (Adjacent Facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
Option 2c Processing	A1 Fuel Assembly Breach	1.6x10 ⁻¹
	A2 Material Release (Processing)	2.6x10 ⁻¹
Option 2c (continued)	A3 Material Release (Dry Vault)	1.4x10 ⁻³
	A4 Material Release (Adjacent Facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A6 Criticality in Processing	1.4x10 ⁻⁴
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid Discharge (internal)	1.1x10 ⁻³
3. 1992/1993 Planning Basis		
Option 3a Dry Storage	Same as Option 2a for Decentralization	
Option 3b Wet Storage	Same as Option 2b for Decentralization	
Option 3c Processing	Same as Option 2c for Decentralization	
4. Regionalization - A		
Option 4a Dry Storage	Same as Option 2a for Decentralization	
Option 4b Wet Storage	Same as Option 2b for Decentralization	
Option 4c Processing	Same as Option 2c for Decentralization	

4. Regionalization - B

Option 4d Dry Storage	Same as Option 2a for Decentralization
Option 4e Wet Storage	Same as Option 2b for Decentralization
Option 4f Processing	Same as Option 2c for Decentralization
Option 4g Shipping Out	Same as Option 1 for No Action

5. Centralization

Option 5a Dry Storage	Same as Option 2a for Decentralization
Option 5b Wet Storage	Same as Option 2b for Decentralization
Option 5c Processing	Same as Option 2c for Decentralization
Option 5d Shipping Out	Same as Option 1 No Action

a. The safety analysis reports from which information was extracted for these accidents
 b. The safety analysis reports from which information was extracted for these accidents
 colocated workers.

c. Units for point estimates of risk are given in potential latent fatal cancers per

d. ICRP 60 risk factor for the general public (5.0×10^{-4} fatal cancer per year) was

e. ICRP 60 risk factor for workers (4.0×10^{-4} fatal cancer per year) was used to determine

the facilities required under this alternative would consist of existing and new facilities to

support the safe handling, stabilization, and dry storage of spent nuclear fuel. This

identifies a potential accident spectrum associated with these facilities for this

Table A-2, lists the references for the source terms considered in analyzing potential

this alternative case, as well as the estimated frequency of occurrence for each accident

lists the potential radiological accidents and health effects associated with dry storage

fuel for the Decentralization alternative. For the transition period of wet to dry

lists the accident scenario with the highest overall point estimate of risk to the

Table 5-22 lists the accident scenario with the highest point estimate of risk (after

general public when the fuel had been moved from wet storage (after approximately 1

placed in interim dry storage. This indicates a substantial reduction in risk (more

magnitude) when fuel handling events are no longer potential accident initiators.

Table 5-22. Highest point estimates of risk among receptor groups (Option 2a).

	Receptor Groups	Population
	Maximally Exposed	
	Offsite Individual	
Overall Point Estimate of Risk	1.6×10^{-7} (Fuel Assembly Breach)	1.4×10^{-3} Breach)
Transitioned to Dry Storage	1.5×10^{-12} (Dry Vault Material Release)	4.9×10^{-9} Release)
Point Estimate of Risk		

a. Units of latent fatal cancers per year.

5.15.2.2.2 Option 2b - Wet Storage - DOE estimated potential radiological accident

impacts that could occur under this case using existing DOE-approved safety analysis amendments submitted to DOE by Westinghouse Savannah River Company for existing wet facilities.

As indicated in Attachment A, Table A-4, the facilities (modules as defined in the 1994b and Figure 3-2) would consist of existing facilities and specific upgrades to safe interim wet storage. In addition, Table A-4 identifies the reference accident with these facilities for this option. Attachment A, Table A-2, lists the references considered in analyzing potential accidents under this alternative option, as well as frequency of occurrence for each accident. Table 5-21 lists the radiological accident consequences of the wet storage (Option 2b) of spent nuclear fuel for the Decentralization. **Table 5-23 lists the accident scenario with the highest point estimate of risk to the wet pool storage options, there are no transition phases.**

Table 5-23. Highest point estimates of risk among receptor groups (Option 2b).

	Receptor Groups	Population
	Maximally Exposed	
	Offsite Individual	
Overall Point Estimate of Risk	1.6×10^{-7} (Fuel Assembly Breach)	1.4×10^{-3} Breach)

Breach)

Breach)

a. Units of latent fatal cancers per year.

5.15.2.2.3 Option 2c - Processing and Storage - Processing for the SRS is defined

as the operation of the separations facilities in F- or H-Areas.

The H-Area facilities were designed to recover uranium and plutonium from spent production reactor fuel, and the F-Area facilities were designed to recover plutonium.

DOE estimated potential radiological accident impacts that could occur under the existing DOE-approved safety analysis reports submitted to DOE by Westinghouse Savannah Company for processes and for vault storage of special nuclear material from existing facilities. DOE also considered radiological accidents associated with wet storage, because the special nuclear material is currently in wet storage. Similarly, it included fuel handling accidents throughout the phase (i.e., until special nuclear material is in interim dry storage). As indicated in Table A-4, the facilities required under this option would consist of existing and new facilities necessary to support safe handling and processing of spent nuclear fuel into special nuclear material for dry storage. In addition, Table A-4 identifies the reference accident spectrum for this case. Attachment A, Table A-2, lists the references for the studies used in analyzing potential accidents under this alternative case, as well as the estimated occurrence for each accident. Table 5-21 lists the radiological release accidents associated with the processing of spent nuclear fuel to special nuclear material for the Decentralization alternative. Table 5-24 lists the accident scenario with the highest overall point estimate of risk for the public from the transition period of wet spent fuel storage into processing for special nuclear material. When the fuel had been processed from wet storage to special nuclear material and placed in interim dry storage, Table 5-24 lists the accident scenario with the highest point estimate of risk to the general public. This indicates a substantial reduction in risk (in magnitude) when fuel handling events and processing events are no longer potential. **Table 5-24.** Highest point estimates of risk among receptor groups (Option 2c).

	Receptor Groups	
	Maximally Exposed	
	Offsite Individual	Population
Overall Point Estimate of Risk	1.6x10 ⁻⁷ (Fuel Assembly Breach)	1.4x10 ⁻³ (Breach)
Transitioned to Dry Storage Point Estimate of Risk	1.5x10 ⁻¹² (Dry Vault Material Release)	4.9x10 ⁻⁹ (Release)

a. Units of latent fatal cancers per year.

For this option, DOE assumes it could not process some fuel clad in stainless steel into special nuclear material and, therefore, would dry-store it as fuel. The technology of nonaluminum-clad fuel has been demonstrated and is assumed to pose no greater risk than the monitored dry storage of special nuclear material.

5.15.2.3 Alternative 3 - 1992/1993 Planning Basis. Because this alternative would be

consistent with the status quo at the SRS, existing documents contain sufficient information to examine its accident analysis impacts. The SRS would continue to receive the spent nuclear fuel designated for the Site, and DOE would complete facilities already planned to accommodate existing inventory and the spent nuclear fuel receipts. This alternative would require the use of facilities already used to support the cases discussed in the Section 5.15.2.2. The amount of fuel ultimately stored because this alternative assumes the fuel beyond that shipped to the SRS under the Decentralization alternative.

5.15.2.3.1 Option 3a - Dry Storage - DOE estimated potential radiological accident

impacts that could occur under this case using existing DOE-approved safety analysis reports for storage from existing facilities and the study discussed for Option 2a.

DOE also considered

radiological accidents associated with wet storage, at least in the near term, because the special nuclear material is currently in wet storage. Similarly, it included fuel handling accidents throughout the phase (i.e., until the fuel is in interim dry storage). As indicated in Attachment A, the facilities required under this option would consist of existing and new facilities necessary to support the safe handling and stabilization of spent nuclear fuel for dry storage. In addition,

identifies the reference accident spectrum associated with these facilities for this Table A-2, lists the authorization basis references for the source terms considered potential accidents under this option, as well as the estimated frequency of occurrence accident. Table 5-21 lists the radiological release accidents and health effects of spent nuclear fuel for the 1992/1993 Planning Basis alternative. For the entire pe scenarios with the highest point estimates of risk to the general public would be for Option 2a, as listed in Table 5-22.

5.15.2.3.2 Option 3b - Wet Storage - DOE estimated potential radiological accident

impacts that could occur under this case using existing DOE-approved safety analysis amendments submitted to DOE by Westinghouse Savannah River Company for wet storage existing facilities.

As indicated in Attachment A, Table A-4, the facilities required under this option would consist of existing facilities and upgrades necessary to support safe interim addition, Table A-4 identifies the reference accident spectrum associated with this option. Attachment A, Table A-2, lists the references for the source terms considered potential accidents under this option, as well as the estimated frequency of occurrence accident. Table 5-21 lists the radiological release accidents and health effects of (Option 3b) of spent nuclear fuel for the 1992/1993 Planning Basis alternative. The with the highest point estimate of risk to the general public would be the same as as listed in Table 5-23.

5.15.2.3.3 Option 3c - Processing and Storage.

Table 5-21 lists the radioactive release accidents and health effects for the processing of spent nuclear fuel for the processing is complete, the accident scenario with the highest point estimate of risk associated with the storage of special nuclear materials, as discussed for Option 2 Table 5-24.

5.15.2.4 Alternative 4 - Regionalization. This alternative comprises Regionalization A and

Regionalization B subalternatives. Under the Regionalization A subalternative (Option 4c), the SRS would receive all aluminum-clad fuel from the other sites considered it would transfer its existing inventory of stainless steel- and Zircaloy-clad fuel to appropriate. These proposed activities would reflect current and past activities, information and analyses are available to enable the scaling or other extrapolation accident impacts. The total amount of spent nuclear fuel to be managed under Regionalization would be slightly less than that for Alternatives 2 and 3; the decisionmaker could adjust the estimated point estimate of risk by the use of an appropriate adjustment discussed in Attachment A, Section A.2.9.

Under the Regionalization B subalternative (Options 4d, 4e, 4f, and 4g), the SRS would store all existing and new spent nuclear fuel east of the Mississippi River. The decisionmaker would change in spent nuclear fuel inventories to adjust the estimated point estimate of appropriate adjustment (scaling) factor, as discussed in Attachment A, Section A.2. of this evaluation, Option 4g (Section 5.15.2.4.7) assumes that DOE would ship all the spent nuclear fuel to the Oak Ridge Reservation.

5.15.2.4.1 Option 4a - Dry Storage - This case is similar to Option 2a, with the

exception of the quantity and type of fuel to be stored. As with Option 2a, this assessment evaluated existing analyses; the point estimates of risk are the same as those for Option 2a.

5.15.2.4.2 Option 4b - Wet Storage - This case is similar to Option 2b, with the

exception of a slightly smaller quantity of fuel to be stored. As with Option 2b, this assessment evaluated existing analyses, and the point estimates of risk are the same as those

5.15.2.4.3 Option 4c - Processing and Storage - For this option, the accident

analysis evaluation is similar to Option 2c.

DOE assumes that it could process spent nuclear fuel associated with regionalization at SRS with existing facilities, because they are d aluminum-clad fuel. However, the small amount of aluminum-clad fuel received after processing options are completed would be placed in wet storage.

5.15.2.4.4 Option 4d - Dry Storage - The accident analysis evaluation for this option

is similar to that for Option 2a, with the exception of the increased inventories a stored.

5.15.2.4.5 Option 4e - Wet Storage - The accident analysis evaluation for this option

is similar to that for Option 2b, with the exception of the increased inventories a stored.

5.15.2.4.6 Option 4f - Processing and Storage - For this option, the accident

analysis evaluation is similar to Option 2c.

DOE assumes that it could process all the current SRS aluminum-clad spent nuclear fuel with existing facilities. However, all receipts o will be placed in dry storage as discussed for Option 4d.

5.15.2.4.7 Option 4g - Shipping Off Site - This option assumes that DOE would

characterize the fuel and ship it all off the Site.

Thus, the potential radiological accidents considered are the same as those for Alternative 1.

5.15.2.5 Alternative 5 - Centralization. This alternative for the SRS would involve fuel

types and new facilities beyond those considered for any other alternative. For in alternative, the SRS would receive spent nuclear fuel from the U.S. Navy. One of t that would be necessary to support this type of spent nuclear fuel is the Expended Volume 1, Appendix D, includes a detailed accident analyses for this proposed facil SRS-specific parameters.

This alternative would bound the maximum number of spent nuclear fuel-related a scenarios that DOE could expect at the SRS, due to the number of new facilities at have to accommodate the diversity and the increased amount of the fuel to be manage decisionmaker could use this maximum amount of spent nuclear fuel to adjust the est the use of an appropriate scaling factor, as discussed in Attachment A, Section A.2 purposes of this evaluation, Option 5d (Section 5.15.2.5.4) assumes that DOE would the Site to another DOE facility.

5.15.2.5.1 Option 5a - Dry Storage - The major difference in dry storage facilities

between this alternative and the others would be the addition of a facility for Nav and the large quantity of spent fuel shipped to the SRS from the Hanford Site.

DOE estimated

potential radiological accident impacts that could occur under this option using DO analysis reports submitted to DOE by Westinghouse Savannah River Company for vault existing facilities at the SRS and the study discussed for Option 2a. In addition, radiological accidents associated with wet storage, at least in the near term, beca nuclear fuel is currently in wet storage. Similarly, it included fuel handling acc transition phase (i.e., until fuel is in interim dry storage). As indicated in Att the facilities required under this option would consist of existing and new facilit

support the safe handling and stabilization of spent nuclear fuel for dry storage. Table A-4 identifies the reference accident spectrum associated with these facilities. Attachment A, Table A-2, lists the references for the source terms considered in an accidents under this option, as well as the estimated frequency of occurrence for each. Table 5-21 compares the radiological release accidents and health effects for the dry nuclear fuel for the Centralization alternative. From the transition period of wet accident scenario with the highest point estimate of risk to the general public would be that for Option 2a, as listed in Table 5-22. When the fuel had been moved from wet (approximately 25 years) and placed in interim dry storage, the accident scenario would estimate of risk to the population would be the same as the Option 2a dry storage p

5.15.2.5.2 Option 5b - Wet Storage - The accident analysis evaluation for this option

is similar to that for Option 2b, with the exception of the amount and type of fuel

5.15.2.5.3 Option 5c - Processing and Storage - For this option, the accident

analysis evaluation is similar to Option 2c.

DOE assumes that it could process the current SRS

aluminum-clad spent nuclear fuel with existing facilities. However, the SRS would not store fuel in dry storage, as discussed for Option 5a.

5.15.2.5.4 Option 5d - Shipping Off Site - This option assumes that DOE would

perform the characterization of the fuel at the SRS, and then would ship all fuel off site. Thus,

the potential radiological accidents considered are the same as those for the No Action

5.15.3 Chemical Hazard Evaluation

For toxic chemicals, several government agencies recommend the quantification of chemical releases as threshold values of concentrations in air or water that cause short-term effects on human health. The health consequences of human exposure to toxic chemicals are not as well understood as those for radiation. Thus, the potential health effects from toxic chemicals are more subject to uncertainty than those for radioactive materials.

This section provides a quantitative discussion for an analyzed chemical accident at the Receiving Basin for Offsite Fuel facility and qualitative discussions addressing chemical hazards at each of the other existing SRS facilities involved in the receipt, processing, and transport of spent nuclear fuel.

5.15.3.1 Receiving Basin for Offsite Fuel. The maximum reasonably foreseeable chemical

hazard accident for the Receiving Basin for Offsite Fuel would involve the release of vapor following the complete reaction of a drum of target cleaning solution (13.4 p with sodium nitrite (WSRC 1993b)). The initiator for this accident is a leak from a drum of the target cleaning solution and involves multiple failures or maloperations with a probability comparable to that of a natural phenomena accident. Table 5-25 shows the estimated release of nitrogen dioxide vapor that an individual at the SRS boundary and a maximally exposed worker could receive.

Table 5-25. Results of analyzed chemical accident.

Receptor Group	Frequency (per year)	NO ₂ Conc (mg/m ³)
Maximally Exposed Offsite Individual	1.0 x 10 ⁻³	0.083
Colocated Worker	1.0 x 10 ⁻³	0.64

To determine the potential health effects from this bounding chemical accident assessment was to compare the resulting airborne concentrations of nitrogen dioxide at various distances against Emergency Response Planning Guideline (ERPG) values, where available. Since there were no ERPG values available for nitrogen dioxide, the assessment substituted toxicity values as follows:

- For Emergency Response Planning Guideline 1, the assessment substituted the

values/time-weighted average (TLV/TWA) values (ACGIH 1987). The time-weighted average is the average concentration for a normal 8-hour workday and a 40-h from which nearly all workers could receive repeated exposure, day-after-day adverse effect.

- For Emergency Response Planning Guideline 2, the assessment substituted level of concern (LOC) values [equal to 0.1 of the immediately dangerous to life or health (IDLH) value; - see below]. The level of concern value is the concentration of a substance in the air above which there could be serious irreversible health effects as a result of a single exposure for a relatively short period of time (EPA 1990).
- For Emergency Response Planning Guideline 3, the assessment substituted immediately dangerous to life or health values. This value is the maximum concentration a person could escape within 30 minutes without a respirator and without exposure impairment of escape or irreversible side effects (NIOSH 1990).

These values as they apply to nitrogen dioxide are as follows:

- Time-weighted average value = 5.6 milligrams per cubic meter
- Level of concern value = 9.4 milligrams per cubic meter
- Immediately dangerous to life or health value = 94.0 milligrams per cubic meter

5.15.3.2 Reactor Basins. There are no postulated chemical accidents for the reactor basins

that would cause an impact to an individual at the SRS boundary or a colocated worker.

5.15.3.3 H-Area. There are no postulated chemical accidents for the H-Area Canyon that

would cause an impact to an individual at the SRS boundary or a colocated worker. DOE performed an accident analysis for the H-Area Canyon facility workers that indicate potential injuries due to chemical contamination or exposure to hazardous vapors at or above the level of concern exposure limit (Du Pont 1983a). The analysis does not project exposure vapors at or above the immediate danger to life and health level to occur.

The probability that a worker could be accidentally exposed to any of the hazards identified in Attachment A, Table A-14, is bounded by a frequency of 2.8×10^{-2} per year (Du Pont 1983a). The most likely injury is an acid burn to the skin.

The probability for exposure to hazardous vapors at or above the level of concern is 8.5×10^{-1} per year (Du Pont 1983a). The potential for chemical uptakes and for depend on the safety measures taken before the exposure, the duration of the exposure and mitigating actions taken after the exposure.

5.15.3.4 F-Area. There are no postulated chemical accidents for the F-Area Canyon that

would cause an impact to an individual at the SRS boundary or a colocated worker. DOE performed an accident analysis for the F-Area Canyon facility workers that indicate potential injuries due to chemical contamination or exposure to hazardous vapors at or above the level of concern exposure limit (Du Pont 1983b). The analysis does not project exposure vapors at or above the immediate danger to life and health level to occur.

The probability that a worker could be accidentally exposed to any one of the hazards identified in Attachment A, Table A-15, is bounded by a frequency of 1.2×10^{-2} per year (Du Pont 1983b). The most likely injury is an acid burn to the skin.

The probability for exposure to hazardous vapors at or above the level of concern is 3.2×10^{-1} per year (Du Pont 1983b). The potential for chemical uptakes and for depend on the safety measures taken before the exposure, the duration of the exposure and mitigating actions taken after the exposure.

5.15.4 Secondary Impacts

The primary focus of the accident analysis is to determine the magnitude of the postulated accident scenarios on public and worker health and safety. However, DOE chemical and radiological accidents can also adversely affect the surrounding environment (secondary impacts). Accordingly, DOE has qualitatively evaluated each of the eight accident scenarios considered in this analysis for potential secondary impacts. The paragraphs discuss the results of the evaluation, and Table 5-26 summarizes expected impacts for each accident scenario.

5.15.4.1 Biotic Resources. With the exception of a direct discharge of disassembly basin

water to an onsite stream, DOE does not expect radiological contamination resulting analyzed accidents to reach any onsite or offsite surface water. DOE previously evaluated a direct discharge of disassembly basin water (DOE 1990) and believes that impacts on biotic resources would be minor. Therefore, the impacts on aquatic biota from any of the accidents would be minor. Small areas of minor surface contamination likely would be outside the industrialized area of a postulated accident. Terrestrial biota in or near the containment area could be exposed to small quantities of radioactive materials and ionizing radiation until the area could be decontaminated. DOE believes that the impacts on biotic resources from the accidents would be minor.

5.15.4.2 Water Resources. DOE expects no adverse impacts on water quality from any of

the postulated accident scenarios. Accident A7 (External Spill/Liquid Discharge) would have the most significant impact. With the exception of the reactor disassembly building and configuration of existing or potential facilities would prevent a direct release of contaminated water to surface water. However, contamination of the surface aquifer release would be likely. The processes governing the slow plume movement and attenuation of contaminants described in Section 5.8 would prevent the contamination from reaching groundwater resources. Similarly, radionuclide contamination of onsite or offsite groundwater resources would be minor.

Table 5-26. Qualitative summary of expected secondary impacts.

Accident Scenario	Accident Description	Environmental or social factor		Economic Impacts
		Biotic Resources	Water Resources	
A1	Fuel assembly breach	No adverse effects on biota expected.	No adverse effects expected to surface or groundwater resources.	Limited economic impacts are expected. Any required cleanup could be handled by existing work.
A2	Material release (processing)	Same as A1.	Same as A1.	Same as A1.
A3	Material release (dry vault)	Same as A1.	Same as A1.	Same as A1.
A4	Material release (adjacent facility)	Same as A1.	Same as A1.	Same as A1.
A5	Criticality in water	Same as A1.	Same as A1.	Same as A1.
A6	Criticality during processing	Same as A1.	Same as A1.	Same as A1.
A7	External spill/liquid discharge	Same as A1.	Surface-water table contamination expected in area of the release. No adverse effects expected to surface-water or drinking water aquifers.	Same as A1.
A8	Internal spill/liquid discharge	Same as A1.	No adverse impact to water resources. The spill is expected to be contained entirely within the building structure.	Same as A1.

water sources would be unlikely. DOE evaluated the effects of a direct discharge of water on water resources (DOE 1990) and believes that impacts on water resources would be minor.

5.15.4.3 Economic Impacts. DOE expects limited economic impacts as a result of any of

the postulated accidents. Any cleanup required would be localized, and the existing equipment could perform it. Contamination should be contained within a small area boundaries for all eight postulated accident scenarios. The existing workforce could perform required cleanup.

5.15.4.4 National Defense. None of the postulated accidents would affect the DOE national

defense mission. Spent nuclear fuel management activities do not involve the production needed for national defense.

5.15.4.5 Environmental Contamination. DOE expects that none of the postulated accident

scenarios would result in large areas of contamination. Local contamination is likely from an accident, but in all scenarios should be contained within the SRS boundaries. Contamination outside the immediate area of the accident is unlikely to require cleanup of a small area inside the Site boundary. Impacts in all cases should be minimal.

5.15.4.6 Endangered Species. There are no Federally listed threatened or endangered

species habitats in the immediate vicinity of existing or potential spent nuclear fuel processing facilities (see Section 4.9.4). None of the postulated accident scenarios would result in large areas of surface contamination outside the immediate facilities, and DOE does not expect adverse impacts to surface water. Therefore, none of the postulated accident scenarios would impact threatened or endangered species.

5.15.4.7 Land Use. No accident scenario should result in large areas of contamination, nor

would the impacts be irreversible. DOE expects no change in land use.

5.15.4.8 Treaty Rights. The environmental impacts of each of the accident scenarios should

be contained within the SRS boundaries. Because there are no Native American or public lands within the site boundaries, treaty rights would not be affected.

5.15.5 Adjusted Point Estimate of Risk Summary

The accident scenarios described in Section 5.15.2 differ only slightly between alternatives. These scenarios did not account for variations in spent nuclear fuel onsite operational transfers) and spent fuel storage inventories across the alternatives. For a realistic comparison across alternatives, DOE developed adjustment factors to adjust consequences, depending on the specific circumstance of each alternative. Attachment A.2.9, provides the methodology and justifications used to develop adjustment factors. This section provides the adjusted point estimates of risk for each accident scenario receptor group to demonstrate a relative comparison of each alternative on a case-by-case basis. Tables 5-27, 5-28, and 5-29 summarize the adjusted point estimates of risk for each accident scenario receptor group, the general population to 80 kilometers, and the colorado

5.16 Cumulative Impacts

The Savannah River Site (SRS) contains major U.S. Department of Energy (DOE) and other facilities, unrelated to spent nuclear fuel, that would continue to operate through the spent nuclear fuel management program. The activities associated with these existing facilities produce environmental consequences that this document has included in the baseline conditions (Chapter 4) against which it assesses the consequences of the spent nuclear fuel management program. Impacts of both the construction and operation of SRS spent nuclear fuel facilities

cumulative with the impacts of existing and planned facilities unrelated to spent n

This cumulative impact assessment considered the incremental and synergistic effect of operation of the Defense Waste Processing Facility, which is nearing completion, an Incineration Facility, which is under construction, when appropriate and when data example, the Air Quality analysis factored in emissions from these two facilities with potential impacts of operations of spent nuclear fuel facilities. The small volume (treated sanitary wastes) currently entering the environment from the Defense Waste Facility, on the other hand, were considered part of the Water Quality baseline. The alone facilities scheduled to be built in the near future on the SRS are the Savannah Laboratory Conference Center and the new Centralized Sanitary Wastewater Treatment number of other planned facilities have not been factored into the cumulative impact final funding approval has not been received or because decisions on these facilities

Table 5-27. Adjusted point estimates of risk for the maximally exposed offsite individual

		Decentralization			
		No Action			
Accident Description	Attributed	Option 1	Option 2a	Option 2b	Option 0
A1 - Fuel Assembly Breach	Adjusted Health Effects ^a	1.0x10 ⁻⁶	1.0x10 ⁻⁶	1.0x10 ⁻⁶	1
	Adjusted Annual Frequency	1.6x10 ⁻¹	3.3x10 ⁻¹	3.5x10 ⁻¹	1
	Adjusted Point Estimate of Risk ^b	1.6x10 ⁻⁷	3.3x10 ⁻⁷	3.5x10 ⁻⁷	1
A2 - Processing release	Adjusted Health Effects ^a	(c)	(c)	(c)	3
	Adjusted Annual Frequency	(c)	(c)	(c)	2
	Adjusted Point Estimate of Risk ^b	(c)	(c)	(c)	9
A3 - Dry vault release	Adjusted Health Effects ^a	(c)	1.1x10 ⁻⁹	(c)	1
	Adjusted Annual Frequency	(c)	1.4x10 ⁻³	(c)	1
	Adjusted Point Estimate of Risk ^b	(c)	1.6x10 ⁻¹²	(c)	1
A4 - Adjacent facility release	Adjusted Health Effects ^a	3.0x10 ⁻⁶	3.0x10 ⁻⁶	3.0x10 ⁻⁶	3
	Adjusted Annual Frequency	2.4x10 ⁻³	5.0x10 ⁻³	5.3x10 ⁻³	2
	Adjusted Point Estimate of Risk ^b	7.2x10 ⁻⁹	1.5x10 ⁻⁸	1.6x10 ⁻⁸	7
A5 - Criticality in water	Adjusted Health Effects ^a	1.5x10 ⁻⁶	1.5x10 ⁻⁶	1.5x10 ⁻⁶	1
	Adjusted Annual Frequency	3.1x10 ⁻³	6.4x10 ⁻³	6.8x10 ⁻³	3
	Adjusted Point Estimate of Risk ^b	4.7x10 ⁻⁹	9.7x10 ⁻⁹	1.0x10 ⁻⁸	4
A6 - Criticality during processing	Adjusted Health Effects ^a	(c)	(c)	(c)	3
	Adjusted Annual Frequency	(c)	(c)	(c)	1
	Adjusted Point Estimate of Risk ^b	(c)	(c)	(c)	5
A7 - External spill/liquid	Adjusted Health Effects ^a	2.7x10 ⁻⁶	2.8x10 ⁻⁶	2.8x10 ⁻⁶	2

discharge A8 - Internal spill/liquid discharge	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2
	Adjusted Point Estimate of Risk _b	5.4x10 ⁻¹⁰	5.4x10 ⁻¹⁰	5.4x10 ⁻¹⁰	5
	Adjusted Health Effects _a	1.2x10 ⁻¹³	1.2x10 ⁻¹³	1.2x10 ⁻¹³	1
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹	1.1x10 ⁻¹	1
	Adjusted Point Estimate of Risk _b	1.3x10 ⁻¹⁴	1.3x10 ⁻¹⁴	1.3x10 ⁻¹⁴	1

Table 5-27. (continued).

Accident Description	Attribute _a	Regionalization - B	
		Option 4d	Option 4e
A1 - Fuel Assembly Breach	Adjusted Health Effects _a	1.0x10 ⁻⁶	1.0x10 ⁻⁶
	Adjusted Annual Frequency	4.1x10 ⁻¹	4.1x10 ⁻¹
	Adjusted Point Estimate of Risk _b	4.1x10 ⁻⁷	4.1x10 ⁻⁷
	Adjusted Health Effects _a	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)
A2 - Processing release	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
A3 - Dry vault release	Adjusted Annual Frequency	1.4x10 ⁻⁹	(c)
	Adjusted Point Estimate of Risk _b	1.4x10 ⁻³	(c)
	Adjusted Annual Frequency	2.0x10 ⁻¹²	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
A4 - Adjacent facility release	Adjusted Annual Frequency	3.0x10 ⁻⁶	3.0x10 ⁻⁶
	Adjusted Point Estimate of Risk _b	6.2x10 ⁻³	6.2x10 ⁻³
	Adjusted Annual Frequency	1.9x10 ⁻⁸	1.9x10 ⁻⁸
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
A5 - Criticality in water	Adjusted Annual Frequency	1.5x10 ⁻⁶	1.5x10 ⁻⁶
	Adjusted Point Estimate of Risk _b	8.0x10 ⁻³	8.0x10 ⁻³
	Adjusted Annual Frequency	1.2x10 ⁻⁸	1.2x10 ⁻⁸
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
A6 - Criticality during processing	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)

A7 - External spill/liquid discharge	Estimate of Riskb		
	Adjusted Health Effectsa	3.5x10 ⁻⁶	3.5x10 ⁻⁶
	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴
A8 - Internal spill/liquid discharge	Adjusted Point Estimate of Riskb	7.0x10 ⁻¹⁰	7.0x10 ⁻¹⁰
	Adjusted Health Effectsa	1.6x10 ⁻¹³	1.6x10 ⁻¹³
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹
	Adjusted Point Estimate of Riskb	1.7x10 ⁻¹⁴	1.7x10 ⁻¹⁴

- a. Units for adjusted health effects are given in terms of potential fatal cancers.
b. Units for adjusted point estimates of risk are given in terms of potential fatal
c. The accident scenario is not included in the spectrum of potential accidents for
d. Adjustment factors were calculated using March 1994 data and information. In-pr
to these factors by more than 10 percent.

Table 5-28. Adjusted point estimates of risk for the colocated worker (radiologica

Accident Description	Attribute	No Action Option 1	Decentralization Option 2a	Option 2b	O 2
		4.8x10 ⁻⁶	4.8x10 ⁻⁶	4.8x10 ⁻⁶	4
A1 - Fuel Assembly Breach	Adjusted Health Effectsa				
	Adjusted Annual Frequency	1.6x10 ⁻¹	3.3x10 ⁻¹	3.5x10 ⁻¹	1
	Adjusted Point Estimate of Riskb	7.7x10 ⁻⁷	1.6x10 ⁻⁶	1.7x10 ⁻⁶	7
A2 - Processing release	Adjusted Health Effectsa	(c)	(c)	(c)	3
	Adjusted Annual Frequency	(c)	(c)	(c)	2
	Adjusted Point Estimate of Riskb	(c)	(c)	(c)	9
A3 - Dry vault release	Adjusted Health Effectsa	(c)	(d)	(c)	(
	Adjusted Annual Frequency	(c)	(d)	(c)	(
	Adjusted Point Estimate of Riskb	(c)	(d)	(c)	(
A4 - Adjacent facility release	Adjusted Health Effectsa	2.0x10 ⁻⁵	2.0x10 ⁻⁵	2.0x10 ⁻⁵	2
	Adjusted Annual Frequency	2.4x10 ⁻³	5.0x10 ⁻³	5.3x10 ⁻³	2
	Adjusted Point Estimate of Riskb	4.8x10 ⁻⁸	1.0x10 ⁻⁷	1.1x10 ⁻⁷	4
A5 - Criticality in water	Adjusted Health Effectsa	5.6x10 ⁻⁵	5.6x10 ⁻⁵	5.6x10 ⁻⁵	5
	Adjusted Annual Frequency	3.1x10 ⁻³	6.4x10 ⁻³	6.8x10 ⁻³	3
	Adjusted Point Estimate of Riskb	1.7x10 ⁻⁷	3.6x10 ⁻⁷	3.8x10 ⁻⁷	1
A6 - Criticality during	Adjusted Health Effectsa	(c)	(c)	(c)	1

processing	Adjusted Annual Frequency	(c)	(c)	(c)	1
	Adjusted Point Estimate of Risk _b	(c)	(c)	(c)	1
A7 - External spill/liquid discharge	Adjusted Health Effects _a	3.0x10 ⁻⁵	3.1x10 ⁻⁵	3.1x10 ⁻⁵	3
	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2
	Adjusted Point Estimate of Risk _b	6.0x10 ⁻⁹	6.2x10 ⁻⁹	6.2x10 ⁻⁹	6
A8 - Internal spill/liquid discharge	Adjusted Health Effects _a	8.0x10 ⁻¹⁵	8.3x10 ⁻¹⁵	8.3x10 ⁻¹⁵	8
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹	1.1x10 ⁻¹	1
	Adjusted Point Estimate of Risk _b	8.8x10 ⁻¹⁶	9.2x10 ⁻¹⁶	9.2x10 ⁻¹⁶	9

Table 5-28. (continued).

		Regionalization - B	
Accident Description	Attribute	Option 4d	Option 4e
A1 - Fuel Assembly Breach	Adjusted Health Effects _a	4.8x10 ⁻⁶	4.8x10 ⁻⁶
	Adjusted Annual Frequency	4.1x10 ⁻¹	4.1x10 ⁻¹
	Adjusted Point Estimate of Risk _b	2.0x10 ⁻⁶	2.0x10 ⁻⁶
	Adjusted Health Effects _a	(c)	(c)
A2 - Processing release	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)
A3 - Dry vault release	Adjusted Point Estimate of Risk _b	(c)	(c)
	Adjusted Health Effects _a	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)
A4 - Adjacent facility release	Adjusted Health Effects _a	2.0x10 ⁻⁵	2.0x10 ⁻⁵
	Adjusted Annual Frequency	6.2x10 ⁻³	6.2x10 ⁻³
	Adjusted Point Estimate of Risk _b	1.2x10 ⁻⁷	1.2x10 ⁻⁷
	Adjusted Health Effects _a	5.6x10 ⁻⁵	5.6x10 ⁻⁵
A5 - Criticality in water	Adjusted Annual Frequency	8.0x10 ⁻³	8.0x10 ⁻³
	Adjusted Point Estimate of Risk _b	4.5x10 ⁻⁷	4.5x10 ⁻⁷
	Adjusted Health Effects _a	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)

during processing	Health Effects ^a		
	Adjusted Annual Frequency	(c)	(c)
	Adjusted Point Estimate of Risk ^b	(c)	(c)
A7 - External spill/liquid discharge	Adjusted Health Effects ^a	3.9x10 ⁻³	3.9x10 ⁻³
	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴
	Adjusted Point Estimate of Risk ^b	7.8x10 ⁻⁷	7.8x10 ⁻⁷
A8 - Internal spill/liquid discharge	Adjusted Health Effects ^a	1.0x10 ⁻¹⁴	1.0x10 ⁻¹⁴
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹
	Adjusted Point Estimate of Risk ^b	1.2x10 ⁻¹⁵	1.2x10 ⁻¹⁵

- a. Units for adjusted health effects are given in terms of potential fatal cancers.
b. Units for adjusted point estimates of risk are given in terms of potential fatal
c. The accident scenario is not included in the spectrum of potential accidents for
d. The safety analyses from which information was extracted for these accidents were require the inclusion of colocated workers.

Table 5-29. Adjusted point estimates of risk for the general population - 80 kilom

Accident Description	Attribute	No Action Decentralization		
		Option 1	Option 2a	Option 2b
A1 - Fuel Assembly Breach	Adjusted Health Effects ^a	8.5x10 ⁻³	8.5x10 ⁻³	8.5x10 ⁻³
	Adjusted Annual Frequency	1.6x10 ⁻¹	3.3x10 ⁻¹	3.5x10 ⁻¹
	Adjusted Point Estimate of Risk ^b	1.4x10 ⁻³	2.8x10 ⁻³	3.0x10 ⁻³
	Adjusted Health Effects ^a	(c)	(c)	(c)
A2 - Processing release	Adjusted Annual Frequency	(c)	(c)	(c)
	Adjusted Point Estimate of Risk ^b	(c)	(c)	(c)
	Adjusted Health Effects ^a	(c)	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)	(c)
A3 - Dry vault release	Adjusted Health Effects ^a	(c)	3.6x10 ⁻⁶	(c)
	Adjusted Annual Frequency	(c)	1.4x10 ⁻³	(c)
	Adjusted Point Estimate of Risk ^b	(c)	5.0x10 ⁻⁹	(c)
	Adjusted Health Effects ^a	(c)	(c)	(c)
A4 - Adjacent facility release	Adjusted Annual Frequency	2.5x10 ⁻²	2.5x10 ⁻²	2.5x10 ⁻²
	Adjusted Annual Frequency	2.4x10 ⁻³	5.0x10 ⁻³	5.3x10 ⁻³

	Adjusted Point Estimate of Risk _b	6.0x10 ⁻⁵	1.2x10 ⁻⁴	1.3x10 ⁻⁴
A5 - Criticality in water	Adjusted Health Effects _a	4.4x10 ⁻³	4.4x10 ⁻³	4.4x10 ⁻³
	Adjusted Annual Frequency	3.1x10 ⁻³	6.4x10 ⁻³	6.8x10 ⁻³
	Adjusted Point Estimate of Risk _b	1.4x10 ⁻⁵	2.8x10 ⁻⁴	3.0x10 ⁻⁴
A6 - Criticality during processing	Adjusted Health Effects _a	(c)	(c)	(c)
	Adjusted Annual Frequency	(c)	(c)	(c)
	Adjusted Point Estimate of Risk _b	(c)	(c)	(c)
A7 - External spill/liquid discharge	Adjusted Health Effects _a	9.0x10 ⁻³	9.4x10 ⁻³	9.4x10 ⁻³
	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2.0x10 ⁻⁴
	Adjusted Point Estimate of Risk _b	1.8x10 ⁻⁶	1.9x10 ⁻⁶	1.9x10 ⁻⁶
A8 - Internal spill/liquid discharge	Adjusted Health Effects _a	1.0x10 ⁻⁹	1.0x10 ⁻⁹	1.0x10 ⁻⁹
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹	1.1x10 ⁻¹
	Adjusted Point Estimate of Risk _b	1.1x10 ⁻¹⁰	1.1x10 ⁻¹⁰	1.1x10 ⁻¹⁰

Table 5-29. (continued).

		Regionalization - B		
Accident Description	Attribute	Option 4d	Option 4e	Op 4
A1 - Fuel Assembly Breach	Adjusted Health Effects _a	8.5x10 ⁻³	8.5x10 ⁻³	8.
	Adjusted Annual Frequency	4.1x10 ⁻¹	4.1x10 ⁻¹	2.
	Adjusted Point Estimate of Risk _b	3.5x10 ⁻³	3.5x10 ⁻³	2.
	Adjusted Health Effects _a	(c)	(c)	2.
A2 - Processing Release	Adjusted Annual Frequency	(c)	(c)	3.
	Adjusted Point Estimate of Risk _b	(c)	(c)	8.
	Adjusted Health Effects _a	4.6x10 ⁻⁶	(c)	4.
A3 - Dry vault Release	Adjusted Annual Frequency	1.4x10 ⁻³	(c)	1.
	Adjusted Point Estimate of Risk _b	6.4x10 ⁻⁴	(c)	6.

A4 - Adjacent Facility Release	Riskb			
	Adjusted Health Effectsa	2.5x10 ⁻²	2.5x10 ⁻²	2.
	Adjusted Annual Frequency	6.2x10 ⁻³	6.2x10 ⁻³	3.
	Adjusted Point Estimate of Riskb	1.6x10 ⁻⁴	1.6x10 ⁻⁴	9.
A5 - Criticality in water	Adjusted Health Effectsa	4.4x10 ⁻³	4.4x10 ⁻³	4.
	Adjusted Annual Frequency	8.0x10 ⁻³	8.0x10 ⁻³	4.
	Adjusted Point Estimate of Riskb	3.5x10 ⁻⁵	3.5x10 ⁻⁵	2.
	Adjusted Health Effectsa	(c)	(c)	4.
A6 - Criticality during processing	Adjusted Annual Frequency	(c)	(c)	1.
	Adjusted Point Estimate of Riskb	(c)	(c)	7.
	Adjusted Health Effectsa	1.2x10 ⁻²	1.2x10 ⁻²	1.
	Adjusted Annual Frequency	2.0x10 ⁻⁴	2.0x10 ⁻⁴	2.
A7 - External spill/liquid discharge	Adjusted Point Estimate of Riskb	2.4x10 ⁻⁶	2.4x10 ⁻⁶	2.
	Adjusted Health Effectsa	1.3x10 ⁻⁹	1.3x10 ⁻⁹	1.
	Adjusted Annual Frequency	1.1x10 ⁻¹	1.1x10 ⁻¹	1.
	Adjusted Point Estimate of Riskb	1.4x10 ⁻¹⁰	1.4x10 ⁻¹⁰	1.
A8 - Internal spill/liquid discharge	Adjusted Health Effectsa			
	Adjusted Annual Frequency			
	Adjusted Point Estimate of Riskb			
	Adjusted Health Effectsa			

- a. Units for adjusted health effects are given in terms of potential fatal cancers
b. Units for adjusted point estimates of risk are given in terms of potential fatal cancers
c. The accident scenario is not included in the spectrum of potential accidents for

unresolved DOE policy issues. For example, this cumulative impact assessment does not address long-term reconfiguration issues. Table 5-30 presents a summary of cumulative impacts with the various spent fuel management alternatives.

5.16.1 Land Use

The land committed to spent nuclear fuel management activities at the SRS would be most part, within existing onsite industrial compounds or undeveloped onsite areas consistent with the continued mission of the Site. Under two of the alternatives - Regionalization by and Centralization (at SRS) - a new Expanded Core Facility could be required to examine and characterize spent nuclear fuels from naval installations east of the Mississippi. One has been proposed for the Expanded Core Facility, one in the approximate center of the site at the old Allied General Nuclear Services facility (or "Barnwell Nuclear Fuel Plant") off Road G (and near SRS Barricade 4) just east of and adjacent to the Site.

Previously-undeveloped land committed to new spent nuclear fuel facilities (except the Expanded Core Facility) would be limited to a maximum of approximately 100 acres (0

kilometer). Depending on the location chosen, an additional 30 acres (0.1 square k required for a new Expanded Core Facility. Thus, a maximum of 130 acres (0.5 squar could be converted from woodlands or old fields to industrial facilities and suppor under the bounding options, Option 5a (Centralization - Dry Storage) and Option 5c Processing). Any site used for the support of spent nuclear fuel activities would control. With the exception of the Barnwell Nuclear Fuel facility, which the Navy from Allied General Nuclear Services for an offsite Expanded Core Facility, DOE wou any additional land from the public domain for SRS spent nuclear fuel management fa

Ground was broken for the new Savannah River Ecology Laboratory Conference Cent 1994. The new facility will occupy a 70-acre area, but only 5 to 10 acres will be for the new conference center, parking areas, and an access road. The remaining 60 managed as a nature study area and preserve. Thus, the Savannah River Ecology Labo Conference Center will require conversion of 5 to 10 acres of planted pines or pine (depending on the exact location of the building) to light-industrial/public use.

Table 5-30. Cumulative impacts associated with construction and operation of spent alternatives at Savannah River Site.

ALTERNATIVE 1 - NO ACTION

	Option 1 Wet Storage
Land Use	No new land committed to new use.
Socioeconomics	A maximum of 50 new jobs created annually duri jobs created during operation.
Air Resources	Site emissions would not exceed any air qualit lists cumulative Site nonradioactive releases
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cu maximally exposed individual at the Site bound rem.
Materials and Waste Management	High-Level: Current generation levels Transuranic: Current generation levels Low-Level: Current generation levels Mixed: Current generation levels Hazardous: Current generation levels Sanitary: Current generation levels

ALTERNATIVE 2 - DECENTRALIZATION

	Option 2a Dry Storage	Option 2b Wet Storage	Option 2c Processing
Land Use	Small amount of land (<10 acres) committed to new use.	Small amount of land (<10 acres) committed to new use.	Small amount of (<10 acres) comm new use.
Socioeconomics	Construction jobs: 600 peak Operation: No new jobs	Construction jobs: 600 peak Operation: No new jobs	Construction jobs: 550 peak Operation: No ne
Air Resources	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions w exceed any air q standard. Table lists cumulative nonradioactive r the SRS boundary
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.	Radioactive airb releases, expres cumulative dose maximally expose individual at th boundary, would rem.
Materials and Waste Management	High-Level: No change Transuranic: 6% increase Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb	High-Level: No change Transuranic: 6% increase Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb	High-Level: 475% incr Transuranic: 12% inc Low-Level: 100% Mixed: No change Hazardous: No ch Sanitary: No cha

ALTERNATIVE 3 - 1992/1993 PLANNING BASIS

	Option 3a	Option 3b	Option 3c
Land Use	Dry Storage Small amount of land (<10 acres) committed to new use.	Wet Storage Small amount of land (<10 acres) committed to new use.	Processing Small amount of (<10 acres) comm new use.
Socioeconomics	Construction jobs: 600 peak Operation: No new jobs	Construction jobs: 650 peak Operation: No new jobs	Construction jobs: 550 peak Operation: No ne
Air Resources	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions w exceed any air q standard. Table lists cumulative nonradioactive r the SRS boundary
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airb releases, expres cumulative dose maximally expose individual at th boundary, would rem.
Materials and Waste Management	High-Level: No change Transuranic: 6% increase Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb	High-Level: No change Transuranic: 6% increase Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb	High-Level: 325% incr Transuranic: 12% inc Low-Level: 87.5% Mixed: No change Hazardous: No ch Sanitary: No cha

ALTERNATIVE 4 - REGIONALIZATION

	Option 4a	Option 4b	Option 4c
Land Use	Dry Storage Small amount of land (<10 acres) committed to new use.	Wet Storage Small amount of land (<10 acres) committed to new use.	Processing Small amount of (<10 acres) comm new use.
Socioeconomics	Construction jobs: 650 peak Operation: No new jobs	Construction jobs: 650 peak Operation: No new jobs	Construction jobs: 550 peak Operation: No ne
Air Resources	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions w exceed any air q standard. Table lists cumulative nonradioactive r the SRS boundary
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airb releases, expres cumulative dose maximally expose individual at th boundary, would rem.
Materials and Waste Management	Option 4a Dry Storage High-Level: No change Transuranic: No change Low-Level: No change Mixed: No changea	Option 4b Wet Storage High-Level: No change Transuranic: No change Low-Level: No change Mixed: No changea	Option 4c Processing High-Level: 475% incr Transuranic: 6% Low-Level: 97.5% Mixed: No change Hazardous: No ch

	Hazardous: No changea Sanitary: No changeb Option 4d Dry Storage	Hazardous: No changea Sanitary: No changeb Option 4e Wet Storage	Sanitary: No cha Option 4f Processing
Land Use	Approximately 40 acres committed to new use.	Approximately 35 acres committed to new use.	Approximately 35 committed to new
Socioeconomics	Construction jobs: 910 peak Operation: No new jobs	Construction jobs: 910 peak Operation: No new jobs	Construction jobs: 860 peak Operation: No ne
Air Resources	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site nonradioactive releases at the SRS boundary.	Site emissions w exceed any air q standard. Table lists cumulative nonradioactive r the SRS boundary
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0x10 ⁻⁵ rem.	Radioactive airb releases, expres cumulative dose maximally expose individual at th boundary, would rem.
Materials and Waste Management	High-Level: No change Transuranic: No change Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb Option 4g Ship Out	High-Level: No change Transuranic: No change Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb	High-Level: 475% incr Transuranic: 6% Low-Level: 97.5% Mixed: No change Hazardous: No ch Sanitary: No cha
Land Use	Less than one acre of land committed to new use.		
Socioeconomics	Construction jobs: 200 peak Operation: No new jobs		
Air Resources	Site emissions would not exceed any air quality standard. Table 5-cumulative site nonradioactive releases at the SRS boundary.		
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a ma exposed individual at the Site boundary, would be (less than) <9.0x		
Materials and Waste Management	High-Level: Reduced volume of waste produced Transuranic: 6% increase Low-Level: No change Mixed: No changea Hazardous: No changea Sanitary: No changeb		
ALTERNATIVE 5 - CENTRALIZATION			
	Option 5a Dry Storage	Option 5b Wet Storage	Option 5c Processing
Land Use	100-130 acres of land committed to new use.	70-80 acres of land committed to new use.	100-130 acres of committed to new
Socioeconomics	Construction: 2,550 peak Operation: No new jobs	Construction: 2,700 peak Operation: No new jobs	Construction: 2, Operation: No ne
Air Resources	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site	Site emissions would not exceed any air quality standard. Table 5-31 lists cumulative Site	Site emissions w exceed any air q standard. Table lists cumulative nonradioactive r

Occupational and Public Health and Safety	nonradioactive releases at the SRS boundary. Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.	nonradioactive releases at the SRS boundary. Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.	the SRS boundary Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.
Materials and Waste Management	High-Level: Reduced volume of waste produced Transuranic: Reduced volume of waste produced Low-Level: No change Mixed: No change Hazardous: No change Sanitary: No change Option 5d Ship Out	High-Level: 475% increase Transuranic: 18% increase Low-Level: No change Mixed: No change Hazardous: No change Sanitary: No change	High-Level: 475% increase Transuranic: 18% increase Low-Level: 100% Mixed: No change Hazardous: No change Sanitary: No change
Land Use	Less than one acre of land committed to new use.		
Socioeconomics	Construction: 200 peak Operation: No new jobs		
Air Resources	Site emissions would not exceed any air quality standard. Table 5 cumulative Site nonradioactive releases at the SRS boundary.		
Occupational and Public Health and Safety	Radioactive airborne releases, expressed as cumulative dose to a maximally exposed individual at the Site boundary, would be 9.0×10^{-5} rem.		
Materials and Waste Management	High-Level: Reduced volume of waste produced Transuranic: 6% increase Low-Level: No change Mixed: No change Hazardous: No change Sanitary: No change		

a. Not expected to change; no analysis conducted.

b. Not expected to change; based on projected employment levels at SRS.

Construction on the new Centralized Sanitary Wastewater Treatment Facility is scheduled to begin in 1994 and should be completed in 1995. This new facility will be built approximately 1 mile south of F-Area on Burma Road. Building the central facility will require clearing approximately 6 acres of planted pines. An 18 mile trunkline/collection system will also be required, using existing transmission line and steam line rights-of-way to the extent possible. This trunkline will be located in the northwest quadrant of the SRS, and will connect the new Centralized Sanitary Wastewater Treatment Facility to A-Area, F-/H-Areas, and C-Area.

Depending on the spent nuclear fuel management alternative chosen, a total of 150 acres of SRS land could be cleared and converted to facilities and infrastructure as a result of spent nuclear fuel management (including an Expanded Core Facility), construction of the Savannah River Ecology Laboratory Conference Center, and completion of the Centralized Sanitary Wastewater Treatment Facility. This represents less than 0.1 percent of the undeveloped land on the SRS, and will have minimal cumulative impact on long-term land use locally and regionally.

5.16.2 Socioeconomics

There would be minimal cumulative impacts on the socioeconomic resources of the SRS region from any spent fuel management alternative. The greatest

change in employment would occur under the Centralization Alternative, which would include construction and operation of an Expanded Core Facility at SRS. Construction of an Expanded Core Facility would require an estimated 850 additional employees in the peak year (1999), while operation of the facility would add a maximum of approximately 500 full-time jobs. DOE anticipates that overall employment on the Site will decline during the first 5 years of the spent fuel management period and will stabilize thereafter as the SRS mission changes. Workers who might otherwise lose their jobs could be employed by SRS in spent fuel program activities. Therefore, DOE expects little or no direct increase in employment due to the program. The Site would fill any new jobs from the existing regional labor force.

5.16.3 Air Quality

Table 5-31 compares the cumulative emissions of nonradioactive pollutants from the SRS, including those from the proposed spent nuclear fuel alternatives, to the pertinent regulatory standards. The values provided are the maximum concentrations that would occur at ground level at the Site boundary. Not all maximum concentrations would occur at the same location.

Table 5-31. Total maximum ground-level concentrations (yg/cubic meter) of criteria and toxic air pollutants at SRS boundary resulting from normal operations and spent nuclear fuel management alternatives. ,b

Emissions	Averaging Time	
	Option a Dry Storage	Option b Wet Storage
Criteria Pollutants		
NOx	An4 (4%)	4 (4%)
SOx	An10 (12%) 24185.0 (50%)	10 (12%) 185.0 (50%)
PM10	3-634 (49%) An3 (6%) 2456.0 (37%)	634 (49%) 3 (6%) 56.0 (37%)
TSP	An11 (17%)	11 (17%)
Ozone (as VOC)	1-N/Ad	N/Ad
Gaseous	1-0.03 (4%)	0.03 (4%)
fluoride (as	1-0.15 (9%)	0.15 (9%)
HF)	240.31 (11%) 120.62 (17%)	0.31 (11%) 0.62 (17%)
Lead	An<0.01 (<1%)	<0.01 (<1%)
CO	8-23.1 (0.2%) 1-181 (0.4%)	23.1 (0.2%) 181 (0.4%)
Toxic Pollutants		
Nitric acid	246.7 (5%)	6.7 (5%)
1,1,1-Trichloroethane	2422 (0.2%)	22 (0.02%)
Benzene	2431 (21%)	31 (21%)
Ethanolamine	24<0.01 (<0.1%)	<0.01 (<0.1%)
Ethylbenzene	240.12 (<0.1%)	0.12 (<0.1%)
Ethylene glycol	240.08 (<0.1%)	0.08 (<0.1%)
Formaldehyde	24<0.01 (<0.1%)	<0.01 (<0.1%)
Glycol ethers	24<0.01 N/A	<0.01 N/A
Hexachloronapht halene	24<0.01 (<1%)	<0.01 (<1%)
Hexane	240.07 (<0.1%)	0.07 (<0.1%)
Manganese	240.10 (0.4%)	0.10 (0.4%)
Methanol	240.51 (<0.1%)	0.51 (<0.1%)
Methyl ethyl ketone	240.99 (<0.1%)	0.99 (<0.1%)
Methyl isobutyl ketone	240.51 (<0.1%)	0.51 (<0.1%)
Methylene	241.8 (0.3%)	1.8 (0.3%)

chloride		
Napthalene	240.01 (<0.1%)	0.01 (<0.1%)
Phenol	240.03 (<0.1%)	0.03 (<0.1%)

Table 5-31. (continued).

Emissions	Averaging Time	Alternatives 1 through 4	
		Option a Dry Storage	Option b Wet Storage
Phosphorus		24<0.001 (<0.2%)	<0.001 (<0.2%)
Sodium hydroxide		240.01 (<0.1%)	0.01 (<0.1%)
Toluene		241.6 (8%)	1.6 (8%)
Trichloroethene		241.0 (0.3%)	1.0 (0.3%)
Vinyl acetate		240.02 (<0.1%)	0.02 (<0.1%)
Xylene		243.81 (<0.1%)	3.81 (<0.1%)

Alternative 5 - Centralization

Emissions	Averaging	Alternative 5 - Centralization			
	Time	Option 5a Dry Storage	Option 5b Wet Storage	Option 5c Processing	Option 5d Ship Out
Criteria Pollutants					
NOx		Ann4 (4%)	4 (4%)	15.1 (15%)	4 (4%)
SOx		Ann10 (12%)	10 (12%)	10 (12%)	10 (12%)
		24-185.0 (50%)	185.0 (50%)	185.5 (52%)	185.0 (50%)
		3-h634.5 (49%)	634.5 (49%)	637.5 (49%)	634 (49%)
PM10		Ann3 (6%)	3 (6%)	3 (6%)	3 (6%)
		24-56.0 (37%)	56.0 (37%)	56.4 (38%)	56.0 (37%)
TSP		Ann11 (17%)	11 (17%)	11 (17%)	11 (17%)
Ozone (as VOC)		1-hN/Ad	N/Ad	N/Ad	N/Ad
Gaseous fluoride (as HF)		1-m0.03 (4%)	0.03 (4%)	0.05 (6%)	0.03 (4%)
		1-w0.15 (9%)	0.15 (9%)	0.25 (16%)	0.15 (9%)
		24-0.31 (11%)	0.31 (11%)	0.41 (14%)	0.31 (11%)
		12-0.62 (17%)	0.62 (17%)	1.02 (28%)	0.62 (17%)
Lead		Ann<0.01 (<1%)	<0.01 (<1%)	<0.01 (<1%)	<0.01 (<1%)
CO		8-h24 (0.2%)	24 (0.2%)	28.1 (0.3%)	23.1 (0.2%)
		1-h187 (0.5%)	187 (0.5%)	217 (0.5%)	181 (0.4%)
Toxic Pollutants					
Nitric acid		24-6.7 (5%)	6.7 (5%)	7.7 (6%)	6.7 (5%)
1,1,1-Trichloroethane		24-22 (0.2%)	22 (0.02%)	22 (0.2%)	22 (0.2%)
Benzene		24-31 (21%)	31 (21%)	31 (21%)	31 (21%)
Ethanolamine		24-<0.01 (<0.1%)	<0.01 (<0.1%)	<0.01 (<0.1%)	<0.01 (<0.1%)
Ethylbenzene		24-0.12s (<0.1%)	0.12 (<0.1%)	0.12 (<0.1%)	0.12 (<0.1%)
Ethylene glycol		24-0.08s (<0.1%)	0.08 (<0.1%)	0.08 (<0.1%)	0.08 (<0.1%)
Formaldehyde		24-<0.01 (<0.1%)	<0.01 (<0.1%)	<0.01 (<0.1%)	<0.01 (<0.1%)
Glycol ethers		24-<0.01 (N/A)	<0.01 (N/A)	<0.01 (N/A)	<0.01 (N/A)
Hexachloronapht halene		24-<0.01 (<1%)	<0.01 (<1%)	<0.01 (<1%)	<0.01 (<1%)

Table 5-31. (continued).

Emissions	Averaging Time	Alternative 5 - Centralization			
		Option 5a Dry Storage	Option 5b Wet Storage	Option 5c Processing	Option 5d Ship Out
Hexane		24-0.07s (<0.1%)	0.07 (<0.1%)	0.11 (<0.1%)	0.07 (<0.1%)

Manganese	24-0.10 (0.4%)	0.10 (0.4%)	0.10 (0.4%)	0.10 (0.4%)
Methanol	24-0.51s ($<0.1\%$)	0.51 ($<0.1\%$)	0.51 ($<0.1\%$)	0.51 ($<0.1\%$)
Methyl ethyl ketone	24-0.99s ($<0.1\%$)	0.99 ($<0.1\%$)	0.99 ($<0.1\%$)	0.99 ($<0.1\%$)
Methyl isobutyl ketone	24-0.51s ($<0.1\%$)	0.51 ($<0.1\%$)	0.51 ($<0.1\%$)	0.51 ($<0.1\%$)
Methylene chloride	24-1.8 (0.3%)	1.8 (0.3%)	1.82 (0.4%)	1.8 (0.3%)
Napthalene	24-0.01s ($<0.1\%$)	0.01 ($<0.1\%$)	0.01 ($<0.1\%$)	0.01 ($<0.1\%$)
Phenol	24-0.03s ($<0.1\%$)	0.03 ($<0.1\%$)	0.03 ($<0.1\%$)	0.03 ($<0.1\%$)
Phosphorus	24- <0.001 ($<0.2\%$)	<0.001 ($<0.2\%$)	<0.001 ($<0.2\%$)	<0.001 ($<0.2\%$)
Sodium hydroxide	24-0.01s ($<0.1\%$)	0.01 ($<0.1\%$)	0.01 ($<0.1\%$)	0.01 ($<0.1\%$)
Toluene	24-1.6 (8%)	1.6 (8%)	2.0 (10%)	1.6 (8%)
Trichloroethene	24-1.0 (0.3%)	1.0 (0.3%)	1.0 (0.3%)	1.0 (0.3%)
Vinyl acetate	24-0.02s ($<0.1\%$)	0.02 ($<0.1\%$)	0.02 ($<0.1\%$)	0.02 ($<0.1\%$)
Xylene	24-3.81s ($<0.1\%$)	3.81 ($<0.1\%$)	3.85 ($<0.1\%$)	3.81 ($<0.1\%$)

a. Source: WSRC (1994a).

b. Numbers in parentheses indicate the percentage of the regulatory standard that each concentration represents.

c. No standard for this chemical.

d. Measurement data currently unavailable.

The data demonstrate that, even with the emissions from the spent nuclear fuel management activities, releases of toxic air pollutants from the SRS would be only a small fraction of the regulatory standards. Therefore, DOE anticipates no cumulative impact.

The releases of some criteria air pollutants by SRS operations would approach regulatory standards. Site sulfur dioxide emissions would reach about 50 percent of both the 24-hour and 3-hour limits under all alternatives. In addition, the emissions of particulates less than 10 microns (PM10) would approach a concentration equal to about 38 percent of the standard. However, the contribution to both these pollutants concentrations made by spent nuclear fuel-related activities would be small, as explained in Section 5.7.

The SRS evaluated the cumulative impact of airborne radioactive releases in terms of cumulative dose to a maximally exposed individual at the Site boundary. Table 5-32 lists the results of this

Table 5-32. Annual cumulative health effects to workers and offsite population due to SRS radioactive releases during incident-free operations.

	Worker				Offsite Population Maximally Exposed Individual		
	Average Individual Dose ^a	Fatal Cancer ^b	Total Collective Dose ^c	Fatal Cancer ^b sd	Dose ^a	Fatal Cancer ^b	Total Collect ^c
Alternative 1 - No Action							
Option 1 Wet Storage	3.2x10 ⁻¹	1.3x10 ⁻⁴	9.4x10 ¹	3.7x10 ⁻²	9.0x10 ⁻⁵	4.5x10 ⁻⁸	8.9x100
Alternative 2 - Decentralization							
Option 2a Dry Storage	3.0x10 ⁻¹	1.2x10 ⁻⁴	9.4x10 ¹	3.7x10 ⁻²	9.0x10 ⁻⁵	4.5x10 ⁻⁸	8.9x100
Option 2b Wet Storage	3.2x10 ⁻¹	1.3x10 ⁻⁴	9.4x10 ¹	3.7x10 ⁻²	9.0x10 ⁻⁵	4.5x10 ⁻⁸	8.9x100
Option 2c	3.6x10 ⁻¹	1.5x10 ⁻⁴	1.6x10 ¹	6.5x10 ⁻²	4.4x10 ⁻⁵	2.2x10 ⁻⁷	2.6x101

Processing	1	4	2	2	4			
Alternative 3 - 1992/1993 Planning Basis								
Option 3a	3.0x10-	1.2x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Dry	1	4	1	2	5			
Storage								
Option 3b	3.2x10-	1.3x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Wet	1	4	1	2	5			
Storage								
Option 3c	3.7x10-	1.5x10-	1.6x10	6.6x10-	4.5x10-	2.2x10-7	2.6x101	
Processing	1	4	2	2	4			
Alternative 4 - Regionalization								
Option 4a	3.0x10-	1.2x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Dry	1	4	1	2	5			
Storage								
Option 4b	3.2x10-	1.3x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Wet	1	4	1	2	5			
Storage								
Option 4c	3.7x10-	1.5x10-	1.7x10	6.8x10-	4.7x10-	2.3x10-7	2.7x101	
Processing	1	4	2	2	4			
Option 4d	3.2x10-	1.3x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Dry	1	4	1	2	5			
Storage								
Option 4e	3.5x10-	1.4x10-	9.4x10	3.7x10-	9.0x10-	4.5x10-8	8.9x100	
Wet	1	4	1	2	5			
Storage								
Option 4f	4.0x10-	1.6x10-	1.7x10	6.8x10-	4.7x10-	2.3x10-7	2.6x101	
Processing	1	4	2	2	4			
Option 4g	<3.2x1	<1.3x10	<9.4x1	<3.7x1	<9.0x1	<4.5x10	<8.9x1	
Ship Out	0-1	-4	01	0-2	0-5	-8	00	

Table 5-32. (continued).

Worker

	Worker				Offsite Population		
	Average		Total		Maximally		Total
	Individual		Collective		Exposed		
	Dosea	Fatal Cancers b	Dosec	Fatal Cancer sd	Dosea	Fatal Cancers b	
Alternative 5 - Centralization							
Option 5a	1.3	5.3x10-	9.6x10	3.8x10-	9.0x10-	4.5x10-8	8.9x100
Dry		4	1	2	5		
Storage							
Option 5b	1.6	6.4x10-	9.6x10	3.8x10-	9.0x10-	4.5x10-8	8.9x100
Wet		4	1	2	5		
Storage							
Option 5c	1.6	6.6x10-	1.7x10	6.9x10-	4.7x10-	2.3x10-7	2.7x101
Processing		4	2	2	4		
Option 5d	<3.2x1	<1.3x10	<9.4x1	<3.7x1	<9.0x1	<4.5x10	<8.9x1
Ship Out	0-1	-4	01	0-2	0-5	-8	00

a. Dose in rem.

b. Probability of fatal cancer.

c. Dose in person-rem.

d. Incidence of excess fatal cancers.

analysis. The highest dose would be 4.7×10^{-1} millirem, which would occur under the processing options of Alternatives 4 and 5. This dose is below the regulatory standard (CFR 1994) of 10 millirem.

Airborne emissions from the two-unit Vogtle Electric Generating Plant (approximately 10 miles southwest of the center of the SRS near Waynesboro, Georgia) were reported to have delivered an MEI total body dose of 1.14×10^{-3} millirem during 1992 (Georgia Power Company 1993). Since the SRS and Plant Vogtle are essentially proximal to the same 80 kilometer population, the ratio of SRS population and MEI doses was used as an estimator of the population dose due to Plant Vogtle emissions. Using this approach, the population dose attributable to Vogtle was estimated to have been about 8.3×10^{-2} person-rem

in 1992. Adding (1) the population dose from Plant Vogtle, (2) the total collective offsite population dose from all SRS activities in 1992 (both air and water source terms), and (3) the highest projected collective dose from spent nuclear fuel management activities (Options 4c and 5c) yields a total cumulative dose of 27.083 person-rem from all SRS sources and Plant Vogtle, which is only 0.3 percent higher than the dose from SRS alone. Note that the doses in Table 5-32 ("Total Collective Dose, Offsite Population") represent the sum of (2) and (3) above.

5.16.4 Water Resources

Approximately 82.1 million gallons per year of Savannah River water would be required for the two most water-intensive options, Option 4f (Regionalization at SRS - Processing) and Option 5c (Centralization - Processing). Because either of these options would probably require construction of an Expanded Core Facility, this facility's projected surface water usage of 2.5 million gallons per year was factored into the cumulative impacts analysis. Thus, the two options with the highest surface water usage, both of which would require as much as 84.6 million gallons, represent approximately 0.4 percent of the current (baseline) SRS surface water usage of 20 billion gallons per year (see Table 5-8).

Operational impacts to surface water quality under any of the spent nuclear fuel management options examined would be minimal. Existing SRS treatment facilities could accommodate all new spent nuclear fuel-related domestic and process wastewater streams. Expected wastewater flows would be well within the design capacities of existing (or planned upgrades of) Site treatment systems. Sanitary wastewater from new spent nuclear fuel facilities would be routed to the new Centralized Sanitary Wastewater Treatment Facility. Liquid radioactive wastes would presumably be sent to the F-/H-Area Effluent Treatment Facility. Treated nonradioactive liquid releases from the new spent nuclear fuel facilities would likely be discharged to Upper Three Runs Creek or Fourmile Branch.

Water quality in the Savannah River downstream of the SRS is adequate to good, with most parameters analyzed showing values below state and Federal Maximum Contaminant Levels or DOE Derived Concentration Guides. Iron, present in soils in the region, is the only constituent of surface waters that routinely exceeds MCLs. Spent nuclear fuel management activities are not expected to result in higher concentrations of iron downstream of the SRS. As noted earlier, in Section 5.16, construction on the new Centralized Sanitary Wastewater Treatment Facility is scheduled to begin in 1994 and should be completed in 1995. The new Centralized Sanitary Wastewater Treatment Facility will replace 14 aging sanitary wastewater facilities with a single state-of-the-art facility which will treat sanitary wastes by an extended aeration-activated sludge process. Chlorine will not be used to treat sanitary wastes in the new facility. Use of non-chemical ultraviolet light disinfection systems will eliminate the use and handling of 32,000 gallons of sodium hypochlorite and 59,000 gallons of sodium sulfite per year. Eliminating these chemicals will essentially eliminate the potential for toxic chemical releases from the wastewater treatment process.

Operation of the new Centralized Sanitary Wastewater Treatment Facility and closure of the old A-, B-, S-Area, and Naval Fuel sanitary wastewater facilities would also eliminate wastewater discharges to Upper Three Runs Creek, the stream on the SRS least degraded by past operations. Treated effluent from the new Centralized Sanitary Wastewater Treatment Facility will discharge to Fourmile Branch. Overall stream quality in Fourmile Branch is expected to improve because the effluent from the new facility will be cleaner than the effluent from the old package plants in C-, F-, and H-Areas that presently discharge to Fourmile Branch. As a result, the cumulative effect of the new spent nuclear fuel management facilities (any alternative considered) and new Centralized Sanitary Wastewater Treatment Facility will probably be a net improvement in water quality in two SRS streams, Upper Three Runs Creek and Fourmile Branch, and may result in better water quality downstream in the Savannah River as well.

Sanitary wastewater from the new Consolidated Incineration Facility will be routed to the new Centralized Sanitary Wastewater Treatment Facility; there will be no direct process wastewater drains to the environment. Liquid wastes will be collected in storage tanks and periodically trucked to a permitted hazardous/mixed waste treatment and disposal facility. Sanitary wastes from the new Savannah River Ecology Laboratory Conference Center will be piped to a septic tank-drain field system and would not impact surface water in the area.

Sanitary wastes produced during construction of the Expanded Core Facility would be treated through the use of portable chemical toilets or through an existing wastewater treatment facility. Depending on the location chosen by DOE and the Navy for the new Expanded Core Facility, sanitary wastes from operation of the ECF would either be treated in an existing wastewater treatment facility (most likely the new Centralized Sanitary Wastewater Facility) or a new treatment facility designed to handle the facility's wastewater capacity. No process wastes from operation of the Expanded Core Facility will be discharged to the environment.

5.16.5 Occupational and Public Health and Safety

Table 5-32 summarizes the cumulative health effects of incident-free SRS operations, including those projected for the spent nuclear fuel alternatives. The table lists potential cancer fatalities for workers and the public due to radiological exposures to airborne and waterborne releases from the Site. In addition, the table provides the (airborne) dose to the hypothetical maximally exposed individual in the offsite population. The evaluation used 1992 as the baseline year for normal operations, because it is the last year for which the SRS has complete information. DOE believes that this year gives a realistic depiction of current operational releases of radionuclides. The assessment added the estimated releases from each spent fuel alternative to this baseline to determine the cumulative impacts listed in Table 5-32.

5.16.6 Waste Management

The analysis of cumulative impacts of SRS waste management activities takes as its starting point the assumption that waste generation under the No Action Alternative represents the baseline condition for the entire Savannah River Site. Waste generation levels associated with the other proposed spent nuclear fuel management alternatives (see Table 5-19) thus represent positive and negative deviations from this baseline. Cumulative effects of the proposed spent nuclear fuel alternatives on the volume of low-level waste, transuranic waste, and high-level waste produced under each of the proposed alternatives are presented in Table 5-30.

In addition to baseline waste generation and wastes generated by spent nuclear fuel management activities, environmental restoration and cleanup activities are expected to become an increasingly important part of the DOE mission at the SRS in the future. These remediation activities are expected to produce large quantities of radioactive, hazardous, and mixed wastes. It is estimated that approximately 22,000 cubic meters (28,754 cubic yards) of low-level waste, 366,000 cubic meters (478,362 cubic yards) of hazardous waste, 82,000 cubic meters (107,174 cubic yards) of mixed wastes, and 900 cubic meters (1,176 cubic yards) of transuranic wastes would be produced by environmental restoration activities at the SRS over the 1995-2024 period (DOE 1995). Decontamination and decommissioning activities are expected to generate approximately 109,000 cubic meters (142,463 cubic yards) of low-level waste, 32,000 cubic meters (41,824 cubic yards) of hazardous waste, 95,000 cubic meters (124,165 cubic yards) of mixed wastes, and 4,000 cubic meters (5,228 cubic yards) of transuranic wastes over the same 30-year period (DOE 1995). High-level radioactive waste would not be generated by environmental restoration or decontamination and decommissioning activities.

5.17 Unavoidable Adverse Environmental Impacts

The construction and operation of facilities related to any of the five alternatives at the Savannah River Site (SRS) would result in some adverse impacts to the environment. Changes in project design and other measures could eliminate, avoid, or reduce most of these to minimal levels. The following paragraphs identify adverse impacts that mitigation could not reduce to minimal levels or avoid altogether.

The generation of some fugitive dust during construction would be unavoidable, but would be controlled by water and dust suppressants. This would occur under Alternatives 2 to 5, but greatest generation of dust would occur under Alternative 5 (excluding the offsite shipping option). Similarly, construction activities would result in some minor, yet unavoidable, noise impacts from heavy equipment, generators, and vehicles.

The maximum loss of habitat would involve the conversion of 70 to 100 acres (0.28 to 0.4 square kilometer) of managed pine forest to industrial land use; this would occur under Alternative 5 if DOE moved all spent nuclear fuel to the SRS.

The amount of radioactivity that normal operation of the spent nuclear fuel facilities would release under four of the five alternatives (Alternatives 1 to 4) would be a small fraction of the 1992 operational releases at the SRS and would be well below applicable regulatory standards.

For the alternative having the most impact (Alternative 5 - Centralization), DOE has calculated that the maximum probability for latent fatal cancer for the maximally exposed member of the public would be about 3 times higher than that calculated for 1992 at the SRS. For latent fatal cancer incidence in the offsite population, this comparison indicates an increase of about 2 times, but the number of cancers calculated is less than one.

The only socioeconomic impacts of the proposed spent nuclear fuel management facilities would be temporary increases in employment and expenditures in the region of influence during the construction phase. These would be unavoidable beneficial impacts.

5.18 Relationship Between Short-Term Use of the Environment and the

Maintenance and Enhancement of Long-Term Productivity

Implementation of any of the proposed alternatives would result in some short-term resource demands (e.g., fuel, construction materials, and labor) and would, under certain alternatives (notably the Centralization Alternative), reduce the natural productivity of a relatively small tract of land (less than .07 percent of total SRS area) currently committed to timber production. Depending upon the precise location selected for facility development, a small amount of marginal-to-good wildlife habitat (see Sections 4.9 and 5.9) would also be lost when the area is cleared, graded, and committed to facilities and supporting infrastructure. However, these short-term resource losses and land-use restrictions provide a basis for improved productivity and utility over the long term at the SRS because consolidating all spent nuclear fuel at a few onsite locations would free for other uses those locations presently committed to spent fuel management. On a national scale, the interim management plan described in this EIS would have the same impact of making locations throughout the DOE complex available for other long-term uses.

5.19 Irreversible and Irretrievable Commitments of Resources

The irreversible and irretrievable commitment of resources resulting from the construction and operation of facilities related to the spent nuclear fuel alternatives would involve materials that could not be recovered or recycled or that would be consumed or reduced to unrecoverable forms. The construction and operation of spent nuclear fuel facilities at the SRS would consume irretrievable amounts of electrical energy, fuel, concrete, sand, gravel, and miscellaneous chemicals. Other resources used in construction would probably

not be recoverable. These would include finished steel, aluminum, copper, plastics, and lumber. Most of this material would be incorporated in foundations, structures, and machinery. Construction and operation of facilities for spent nuclear fuel management would also require the withdrawal of water from surface- and groundwater sources, but most of this water would return to onsite surface streams or the Savannah River after use and treatment.

The Centralization alternative (Option 5c - Processing) would consume the greatest amount of electricity of any of the alternatives, about 110,400 megawatt-hours. The Processing option (excluding Option 4c, Regionalization by fuel type) would have the highest requirements for coal to produce steam, approximately 2,580 metric tons (2,843 tons) annually. The Centralization alternative (except Option 5d where all spent fuel would be shipped off the site) would involve the greatest irretrievable consumption of other resources, such as construction materials, chemicals, gases, and operating supplies. However, this demand would not constitute a permanent drain on local resources or involve any material that is in short supply in the region.

5.20 Potential Mitigation Measures

This section summarizes measures that DOE could use to avoid or reduce impacts to the environment caused by spent nuclear fuel management activities at the SRS. DOE would determine the extent to which any mitigation would be necessary and the selection of which measures would be implemented during a detailed site-specific NEPA review tiered from this Programmatic EIS. Consequently, the following sections in this chapter address impact avoidance and mitigation in general terms and describe typical measures that the SRS could implement. In addition, the analyses described in this appendix indicate that the environmental consequences of spent fuel management would be minimal in most environmental media.

5.20.1 Pollution Prevention

DOE is committed to comply with Executive Order 12856, "Federal Compliance with Right-to-Know Laws and Pollution Prevention Requirements"; Executive Order 12780, "Federal Acquisition, Recycling and Waste Prevention"; and applicable DOE Orders and Guidance Documents in planning and implementing pollution prevention at the SRS. The pollution prevention program at the Site was initiated in 1990 as a waste minimization program. Currently, the program consists of four major initiatives: solid waste minimization; source reduction and recycling of wastewater discharges; source reduction of air emissions; and potential procurement of products manufactured from recycled materials. Since 1991, the waste of all types generated at the SRS has decreased, with greatest reductions in hazardous and mixed wastes. These reductions are attributable primarily to material substitutions.

All spent fuel management activities at the SRS would be subject to the Site pollution prevention program. Implementation of the program plan would minimize the amount of waste generated by these activities.

5.20.2 Socioeconomics

Spent nuclear fuel activities would have minimal impact on the socioeconomic environment in the region of influence because most employees would be drawn from the existing site workforce. The minor impacts of immigrating construction workers could be minimized by DOE possibly informing local communities and county planning agencies as to scheduling of construction activities.

5.20.3 Cultural Resources

A Programmatic Memorandum of Agreement (SRARP 1989) between the DOE Savannah River Operations Office, the South Carolina State Historic Preservation Office, and the Advisory Council on Historic Preservation, ratified on August 24, 1990, is the instrument for the management of cultural resources at the SRS. DOE uses this memorandum to identify cultural resources and develop mitigation plans for affected resources in consultation with the State Historic Preservation Officer. DOE would comply with the terms of the memorandum for all measures needed to support spent nuclear fuel management at the Site. For example, DOE would survey sites prior to disturbance and could reduce impacts to any potentially-significant cultural resources discovered through avoidance or removal. Any artifacts discovered would be protected from further disturbance and the elements until removed.

DOE conducted an investigation of Native American concerns over religious rights in the Central Savannah River Valley in conjunction with studies in 1991 related to a New Production Reactor. During this study, three Native American groups expressed concern over sites and items of religious significance on the SRS (see Section 4.4.2). DOE has included these organizations on its environmental mailing list, solicits their comments on NEPA actions of the Site, and sends them documents about SRS environmental activities, including those related to these SNF management considerations. These Native American groups would be consulted on any actions that may follow subsequent site-specific environmental reviews.

5.20.4 Geology

DOE expects that there would be no impacts to geologic resources at the SRS under any alternative evaluated in this EIS. Potential soil erosion in areas of ground disturbance would be minimized through sound engineering practices such as implementing controls for stormwater runoff (e.g., sediment barriers), slope stability (e.g., rip-rap placement), and wind erosion (e.g., covering soil stockpiles). Re-landscaping would minimize soil loss after construction was completed. These measures would be included in a site-specific Storm Water Pollution Prevention Plan that the SRS would prepare prior to initiating any construction.

5.20.5 Air Resources

DOE would meet applicable standards and permit limits for all radiological and non-radiological releases to the atmosphere. In addition, the SRS would follow the DOE policy of maintaining radiological emissions to levels "as low as reasonably achievable" (ALARA). ALARA is an approach to radiation protection to control or manage exposures (both individual and collective) and releases of radioactive material to the environment as low as social, technical, economic, practical, and public policy considerations permit. ALARA is not a dose limit, but rather a process that has as its objectives the attainment of dose levels as far below the applicable limits as practicable.

5.20.6 Water Resources

DOE would minimize the potential for adverse impacts on surface water during construction through the implementation of a stormwater pollution prevention plan that details controls for erosion and sedimentation. The plan would also establish measures for prevention of spills of fuel and chemicals and for rapid containment and cleanup.

DOE could minimize water usage during both construction and operation of facilities by instituting water conservation measures such as instructing workers in water conservation (e.g., turn off hoses when not in use), installing flow restrictors, and using self-closing hose nozzles.

5.20.7 Ecological Resources

DOE does not anticipate that any of the spent fuel alternatives would impact any wetlands on the Site. In any case, DOE and SRS policy is to achieve "no net loss" of wetlands. Pursuant to this goal, DOE has issued a guidance document, Information for Mitigation of Wetlands Impacts at the Savannah River Site (DOE 1992), for project planners that puts forth a practical approach to wetlands protection that begins with avoidance of impacts (if possible), moves to minimization of impacts (if avoidance is impossible), and requires compensatory measures (wetlands restoration, creation, or acquisition) in the event that impacts cannot be avoided.

The analysis in this EIS indicates that there are no threatened and endangered species or sensitive habitats in the areas considered as representative of potential sites for spent nuclear fuel activities at the SRS. However, DOE would perform site-specific predevelopment surveys to ensure that development of new facilities would not impact any of these biological resources.

5.20.8 Noise

DOE anticipates that noise impacts both on and off the Site would be minimal. DOE does not foresee noise impacts from spent nuclear fuel management that would warrant mitigation measures beyond those consistent with good construction, engineering, operations, and management practices.

5.20.9 Traffic and Transportation

DOE has a system of onsite buses operating at the SRS. The Site would evaluate the need for upgrades or changes in service that might be required for the spent nuclear fuel management activities and would make changes, as necessary.

DOE would manage changes in traffic volume or patterns during construction through such measures as designating routes for construction vehicles, providing workers with safety reminders, and upgrading onsite police traffic patrols, if necessary.

5.20.10 Occupational and Public Health and Safety

The DOE program for maintaining radiological emissions to levels "as low as reasonably achievable" (ALARA) described in Section 5.20.5 above will minimize any impacts to workers and the public due to atmospheric releases. Likewise, the Site Pollution Prevention Plan and emergency preparedness measures will enhance safety both on and off the Site.

5.20.11 Utilities and Support Services

The utilities and support services at the SRS are sufficient to meet the requirements of any of the alternatives for the spent fuel management at the Site. Impacts on these services would be minimal. No mitigation measures would be required.

5.20.12 Accidents

The SRS has in place emergency action plans that would be activated in the case of an accident. These plans contain both onsite provisions (e.g., evacuation plans, response teams, medical and fire response, training and drills, communications equipment) and offsite arrangements (e.g., response

plans for medical and fire agencies, coordination with local and state agencies, communication plans). The SRS plans would be updated to include any new facilities or activities related to spent nuclear fuel management that would involve the Site. The execution of the plans in response to an accident would mitigate adverse effects both on the Site and in the surrounding areas.

ATTACHMENT A: ACCIDENT ANALYSIS

ATTACHMENT A: ACCIDENT ANALYSIS

A.1 Accident Evaluation Methodologies and Assumptions

The potential for facility accidents and the magnitude of their consequences is a factor in the evaluation of the spent nuclear fuel alternatives addressed in this EIS. The following discusses health risk issues:

- Would accidents at any of the Savannah River Site (SRS) facilities that the Department of Energy (DOE) could build for spent nuclear fuel management activities pose health risks to workers or the general public?
- Could alternative locations or facilities for the spent nuclear fuel alternatives pose public or worker health risks? Smaller risks could arise from such factors as isolation of the facility from the public, a reduced frequency of such external initiators as seismic events or aircraft crashes, reduced inventory, and proper management.

Guidance for the implementation of Council on Environmental Quality (CEQ) regulations (CFR 1986), as amended (51 FR 15625), requires the evaluation of impacts that would be caused by the probability of occurrence but high consequences if they did occur; this EIS, therefore, evaluates the potential for facility accidents to the extent feasible.

A.1.1 Radiological Accident Evaluation Methodology

The alternatives considered in this EIS provide an opportunity to incorporate new technology in new facilities, processes, and operations that would minimize the potential risk to the health and safety of plant workers and the public. Modifications and improvements to existing facilities would be used to mitigate accident consequences from existing facilities or reduce the likelihood of accidents.

Under normal circumstances, DOE would develop accident scenarios and calculate consequences using safety analyses, mitigation features, and design details on proposed designs. However, the preliminary design information for the proposed facilities during the preparation of this EIS does not contain sufficient detail to permit quantitative analyses. Therefore, for each spent nuclear fuel alternative, DOE has evaluated the proposed facilities for the type of radiological accidents it has determined to be most likely to occur.

The radiological accident types fell into four categories: (1) fuel damage, (2) nuclear criticalities, and (3) liquid spills or discharges. For each accident type, DOE used reference accidents by examining DOE-approved safety analysis reports (SARs) and other documentation (e.g., previous EISs). In addition, DOE considered accidents from other sources for their possible impacts related to spent nuclear fuel. DOE extracted the overall reference accident from the appropriate source, rather than attempting to calculate frequencies for all possible initiators; that is, DOE did not use the specific probability of a magnitude earthquake to determine the frequency of a criticality or spill, given the frequency of earthquakes. If multiple initiators could lead to one of the reference accidents, the frequency of the initiators could lead to one of the reference accidents, DOE used the frequency of the initiators, generally providing conservative results. For example, Offsite Fuel has a number of potential release initiators that could result in a criticality, as listed in Table A-1. As listed, a number of incidents, all of which have assigned frequencies, can contribute to the initiation of an uncontrolled criticality. Table A-1. Potential release initiators at the Receiving Basin for Offsite Fuel.

Natural Phenomena	External Events	Operations Induced Events	Criticality Events
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Temperature Extreme	Aircraft Crash	Fuel Cutting	Fuel Bundli
Snow	Helicopter Crash	Spill at Hose Rack	Cask Loadin
Rain	Surface Vehicle Crash	Fuel Rupture in Storage	Fuel Identi
			Problem
Lightning		Fire and Explosion	Fuel Move
Tornado		Fuel Near Basin Surface	Dropped Fue
Earthquake		Spills and Leaks	Crane or Ho
Meteorite Impact		Resin Regeneration	Cask Immers
		Facility Waste to Cell	

This evaluation results in qualitative comparisons for proposed facilities base that the facility function is similar to one already analyzed. In addition, an ide not considered in each safety analysis report for existing SRS facilities because t prepared over several years in accordance with requirements in effect at the time. includes a comparison of the similarities of possible facilities to an existing fac selection of reference accidents, and several tables containing data to support a c estimates of risk.

The qualitative comparison supports the National Environmental Policy Act (NEPA that the decisionmaker can assess the relative risk from each alternative at SRS an

A.1.1.1 Notable Accident Initiators. While there are many different types of accident

initiators of various frequencies that could lead to an accident, three notable ini earthquakes, and aircraft crashes - require additional discussion due to the public importance of these initiators and the public's familiarity with these types of ini

Because there has never been an uncontrolled criticality accident at the SRS, D historic experience related to the initiators to estimate the frequency for a criti Receiving Basin for Offsite Fuel. Storage basins for spent nuclear fuel have excel From 1945 through 1980, there were 40 known criticality accidents worldwide, none o occurred in a fuel storage facility. From 1975 to 1980, there were, conservatively storage basins in operation around the world, and no criticality incidents occurred assumes that the upper frequency limit for a criticality event is 3.1×10^{-3} per ye This figure is applicable to the extent that the storage basins and the operations similar to those of the Receiving Basin for Offsite Fuel. However, the frequency f criticality event was determined through a detailed fault tree analysis, as referen analysis report, to be an overall calculated limit of 1.4×10^{-4} per year. This va implementation of new administrative controls or equipment.

The SRS is in an area that has a relatively low seismic frequency. Based on th recorded seismic activity, an earthquake with a Richter magnitude greater than 6.0, to a Modified Mercalli Intensity Scale (MMI) of VII, would not be likely at the SRS basis earthquake for the SRS is a MMI VIII event with a corresponding horizontal pe acceleration of 0.2g. Based on current technology, as applied in various probabili the seismic hazard in the SRS region, the 0.2g peak ground acceleration can be asso 2×10^{-4} annual probability of exceedance (5,000-year return period). There are fo Receiving Basin for Offsite Fuel to which an earthquake of intensity MMI VIII or gr contribute:

- Deformation of the storage racks leading to a criticality incident.
- Derailment of the 100-ton (91-metric-ton) crane into the storage basin with of the storage rack leading to criticality.
- Damage to the basin walls leading to the release of contaminated basin wate
- Rupture of a waste tank or pipe in the Resin Regeneration Facility leading contaminated liquids.

An aircraft crash into a spent nuclear fuel facility is of concern because it c radioactive release of materials from the stored spent nuclear fuel. Appendix D co crash probability analysis based on the examination of large civilian and military airspace within a 10-mile (16-kilometer) radius of the SRS. It does not include th of general aviation aircraft because aircraft of this type generally do not possess attain sufficiently high velocities to produce a serious radiological threat in the into an area containing spent nuclear fuel. The analysis did not evaluate crash pr likelihood of occurrence of less than 10^{-7} per year because they would not signific the risk. This was the case for spent nuclear fuel facilities located at the SRS.

A.1.1.2 Use of DOE-Approved Safety Documents. The NEPA guidance issued by the

DOE Office of NEPA Oversight, dated May 1993, recommends that accident impact analysis "reference Safety Assessments and Safety Analysis Reports, if available." This is the primary basis used to develop the approach used in the accident analysis section of Appendix D. Several relevant safety analysis reports as well as previously published analysis reports are the primary source of information on reasonably foreseeable accident potential to cause a release of hazardous materials. These reports are required for nuclear materials facilities with operations that potentially pose a significant hazard to personnel, offsite populations, or the environment. The referenced safety analysis approval/draft submittal dates encompass a range from 1983 to 1993. The 1983 safety analysis was supplemented by a 1993 addendum; the next oldest safety analysis report was approved in 1985.

A.1.2 Chemical Hazard Evaluation Methodology

This analysis reviewed the appropriate safety analyses to assess the degree to which chemical accidents were addressed. It found that each of the safety analyses addressed chemical accidents in a qualitative manner. To provide a quantitative discussion of chemical hazards, the analysis used a separate risk assessment (WSRC 1993c) for the storage risk of offsite releases from the Receiving Basin for Offsite Fuel to determine a bounding chemical accident. The analysis also reviewed chemical inventories (see Section A.3) for the existing spent nuclear fuel facilities at the Savannah River Site Tier Two Emergency and Hazardous Chemical Inventory Report (W 1994a) to determine the facilities total chemical inventory. This chemical inventory was screened using the EPA's "List of Lists" (EPA 1990).

A.1.3 SRS Emergency Plan

The SRS emergency plan (WSRC 1993b) defines appropriate response measures for the management of emergencies (e.g., accidents) involving the Site. It incorporates a description of the entire process designed to respond to and mitigate the consequences of emergencies that could cause activation of all or portions of this plan include:

- Events (operational, transportation, etc.) with the potential to cause releases beyond the limits of hazardous materials.
- Events such as fires, explosions, tornadoes, hurricanes, earthquakes, dam failures, etc., that could affect safety systems designed to protect site and offsite environment.
- Events such as bomb threats, hostage situations, etc., that reduce the security of the Site.
- Events created by proximity to other facilities, such as the Vogtle Electric Plant, a commercial nuclear powerplant located across the Savannah River from the Site.

For radiological emergencies, protective actions in this plan are designed to keep offsite exposures As Low As Reasonably Achievable (ALARA). This is accomplished by time spent in the vicinity of the hazard, keeping as far from the hazard as possible, and the advantage of available shielding. Protective actions that could be used on the Site during an emergency include remaining indoors, sheltering, evacuation, and relocation. For an actual or projected radiological release, appropriate protective actions for on-site personnel have been determined based on trigger points called Protective Action Guides (PAGs).

A.1.4 General Assumptions

This assessment applied the following key assumptions to examine existing accidents and to relate these analyses to the spent nuclear fuel alternatives.

- When a referenced accident scenario is used for a possible new facility, DOE assumes the new facility close to an existing referenced facility performing a similar function, resulting in consequences and health effects similar to the existing facility. An exception could be the proposed Expanded Core Facility which Appendix D analyzes separately.
- For existing facilities to be modified, portions of the facility to be decommissioned, or new facilities to be added, potential accident initiators resulting from construction activities would be bounded by the referenced accident scenarios.
- Type 2 High Enriched Uranium fuel, the dominant type currently in storage on the SRS, would provide a reference source term for other fuel types (i.e., Mark 1).

- Spent nuclear fuel acceptance criteria would specify that all fuel must be indefinite suspension in air with no melting.
- The total frequency of an event (e.g., criticality) could be used to determine of risk, regardless of the type or specific frequencies of the individual components.
- Adjustment (scaling) factors could be applied to reflect a best engineering of relative risk between the various alternatives.
- The point estimate of risk for a given accident scenario would be representative could, for the purposes of this programmatic EIS, represent a similar accident new facilities that perform similar functions.
- Reference accidents would be attributed to a facility based on its function or dry material storage) regardless of whether the facility currently exists design, or is in the conceptual design phase.
- Possible new facilities would be designed to pose no greater risk to the workers than existing facilities with similar functions.

This evaluation takes no credit for the upgraded design requirements for the proposed. Such facilities should have improved reliability or mitigative features and, therefore, aggregate frequency of accidents. Therefore, the application of values from existing reports would provide conservative results. In addition, the evaluation makes no attempt to discriminate among similar existing facilities that might have slightly different frequencies of occurrence or source terms (i.e., an FB-Line event frequency was applied to HB-Line processing facilities).

For most accidents, the evaluation did not quantify consequences for workers. The analysis reports from which information was extracted for the reference accidents were the issuance of DOE Order 5480.23 (DOE 1992); previous applicable Orders did not require inclusion of worker doses. The historic record indicates that DOE facilities have a good record. Figure A-1 compares the rate of worker fatalities in the DOE complex (DOE average rates compiled by the National Safety Council for various industry groups). Because the DOE worker accident fatality rate compares favorably to rates from such as agriculture and construction and is slightly less than trade and services group quantitative data regarding accident impacts to radiological workers should not impact the decisionmaking process. The discussion presented in Volume 1 adequately addresses impacts to close-in workers (i.e., those directly involved in the activity or near the accident).

A.1.4.1 Receptor Group Assumptions. To ensure comparative results, the evaluation

assessed the measures of impacts among four receptor groups:

- Worker. An individual located 100 meters (328 feet) in the worst sector of the site location where the release occurs.
- Colocated Worker. An individual located 640 meters (2,100 feet) in the worst sector of the facility location where the release occurs.

Figure A-1. Comparison of fatality rates among workers in various industry groups.
Site boundary from the facility location where the release occurs.

- Offsite Population to 80 Kilometers. The collective sum of individuals located within the 80-kilometer (50-mile) radius of the SRS.

As noted above, the worker is 100 meters (328 feet) from the facility where the release occurs. This is because information quantifying accident impacts (i.e., dose and health effects) less than 100 meters from an accidental release of radionuclides is unavailable. For accident scenarios considered in Appendix C of this EIS, there is some risk of work at distances closer than 100 meters. Furthermore, the safety analyses from which the extracted information for the accident scenarios often did not include any discussion of impacts as a result of potential accidents. DOE Orders published before DOE 5480.2 did not require the inclusion of worker doses. However, Section A.2.6.2 includes a discussion regarding accident impacts for the worker at less than 100 meters (328 feet) for radiological accident scenarios.

A.1.4.2 Code Assumptions. DOE's application of the AXAIR and AXAIR89Q (a validated

version) dose estimation models is acceptable for projecting health effects from accidents. Comparing the results to results from other similar codes (RSAC-5 and GENII) used in the AXAIR is a Gaussian model based on the methodology outlined in NRC Regulatory Guide (NRC 1983). AXAIR contains a meteorological data file specific to SRS that provide calculated doses for the radiological consequences of atmospheric releases. AXAIR includes the following specific functions:

- Performs both environmental transport and radiation dosimetry calculations
- Bases environmental transfer models on NRC Reg Guide 1.145 guidelines
- Includes exposure pathways for inhalation of radionuclides and gamma radiation radioactive plume
- Calculates gamma shine doses using a non-uniform Gaussian model
- Uses worst sector and 99.5-percentile meteorology

Doses calculated with this code should bound the radiological consequences for atmosphere postulated.

A.1.4.3 Criticality Assumptions. An estimate of the consequences of a criticality incident

requires an estimate of the number of fissions that might occur. While U.S. Nuclear Commission (NRC) Regulatory Guide 3.34 specifies 1×10^{19} fissions as the upper ten experience, the SRS analyses are based on mean values, to the extent possible, for Criticality incidents have produced from 10^{14} to 4×10^{19} fissions with a mean of 2×10^{17} incidents involving fissile solutions and a mean of 5×10^{17} fissions for incidents a consequence, two accident scenarios (Table A-2) address criticality - the wet pool and the processing criticality scenario. For the wet pool criticality scenario, the systems (5×10^{17}) is assumed to apply to the source term used to determine the accident consequences, while the processing criticality scenario assumes that the mean value (2×10^{18}) was applied to the source term to determine accident consequences.

A.2 Radiological Accident Scenarios

A.2.1 Selection of Reference Accidents

To support the examination of both existing and proposed facilities, this evaluation spectrum of potential accident types. To develop a meaningful spectrum of potential evaluation posed the following question:

"What could be done to spent nuclear fuel that would result in a radiological consequence to the receptor groups?"

In determining the answer to this question, the following four general types of events (1) fuel damage, (2) material releases, (3) criticalities, and (4) liquid spills or applicable safety analysis reports for the SRS facilities that the spent nuclear fuel likely to affect generated more than 20 accidents involving the transport, receipt, storage of spent nuclear fuel. A consolidation and subsequent "binning" of these accident type reflects an appropriate range of case-specific reference accidents.

Table A-2. Reference radiological accidents considered for spent nuclear fuel activity

Name and Reference	Reference for Source Term/Dose	C
A1. Fuel Assembly Breach Reference Accident: RBOF fuel cutting	Tables 1-3 DPSTSA-200-10-3, Addendum 1	1
A2. Material Release (Processing) Reference Accident: F-Canyon Uncontrolled Reaction	Meehan 1995	2
A3. Material Release (Dry Vault) Reference Accident: PSF release	Table 5-9 DPSTSA-200-10-19	1
A4. Material Release (Adjacent Facility) Reference Accident: Release of Waste Tank Activity to Cell	Tables 1-3 DPSTSA-200-10-3, Addendum 1	2
A5. Criticality in Water Reference Accident: RBOF criticality	Tables 1-3 DPSTSA-200-10-3, Addendum 1	3
A6. Criticality During Processing Reference Accident: FB-Line	WSRC-RP-93-1102	1
A7. Spill/Liquid Discharge (External) Reference Accident: Direct discharge of water from K-Reactor disassembly basin	Figure 3 Meehan 1994	2
A8. Spill/Liquid Discharge (Internal) Reference Accident: RBOF hose rack	Tables 1-3 DPSTSA-200-10-3,	1

spill

Addendum 1

The fuel damage event (type 1 accident) considered was physical damage or breach assembly. Three material (type 2 accidents) releases were considered; they represent events that could occur during processing from medium energetic events, those that could occur from storage of special nuclear materials, and those that could occur from an adjacent facility (type 3 accidents) can have different dose impacts and can occur with different frequencies on the physical or chemical characteristics of the material and the surroundings. Events - in water and during processing - represent these accident scenarios. The considered a dry criticality accident scenario bounded by the wet pool criticality and bounded by the processing criticality accident in terms of number of fissions a discharges and spills (type 4 accidents) were considered - discharges of pool or bath contain tritium, cesium, and other radioactive constituents from the fuel in the pool spills of slightly contaminated liquids inside a facility during fuel handling, spray unloading (internal spill).

These eight typical accidents form the set of accidents for the selection of a set. Each type has been assigned an alphanumeric designator, which is listed below and in this document:

- Type 1 - Fuel damage
 - A1 - Fuel assembly breach
- Type 2 - Material releases
 - A2 - Processing release
 - A3 - Dry vault release
 - A4 - Adjacent facility release
- Type 3 - Criticalities
 - A5 - Criticality in water
 - A6 - Criticality during processing
- Type 4 - Liquid discharges and spills
 - A7 - External spill/liquid discharge
 - A8 - Internal spill/liquid discharge

A second review of the safety analyses and the original list of accidents considered specific accident considered in DOE-approved safety analyses could be represented one of the eight "generic" accidents (i.e., a fire could result in material release or result in criticality or liquid release). The use of this approach with documented avoids the need for unique identification of all initiating precursor events or the

A.2.1.1 Externally Initiated Accidents. The accident analysis section of this EIS considered

accident scenarios from external events or adjacent facilities and their potential nuclear fuel activities and facilities. Three significant sources of externally initiated mechanisms were identified as potentially applicable to these facilities and activities: adjacent fires, and adjacent explosions. As discussed above, an aircraft crash scene reasonably foreseeable event within the probability scope of this EIS. For the most explosion in a facility adjacent to the spent nuclear fuel facilities described in have a significant impact on spent nuclear fuel facilities. However, the screening that a fire and explosion in the Resin Regeneration Facility, located immediately adjacent to a Receiving Basin for Offsite Fuel, could result in the airborne release to the shield included for completeness.

A.2.1.2 Nearby Industrial or Military Facility Accidents. Within a 40-kilometer

(25-mile) radius of the SRS, there are approximately 120 industrial facilities with employees (DOE 1990). Four of these facilities are within a 16-kilometer (10-mile) radius. Other than those on the SRS, the only major storage facilities within a 40-kilometer radius are facilities at Chem-Nuclear Systems, Inc., Vogtle Electric Generating Station, and a gas storage tanks near Beech Island. The facilities within a 16-kilometer radius are still at least 10 kilometers (6 miles) from the nearest spent nuclear fuel facility. negligible risk to spent nuclear fuel activities.

A.2.1.3 Common Cause Accident. DOE considered accident scenarios based on a common

cause accident during the screening process. A severe seismic event was the only common initiator identified with the potential to simultaneously impact multiple spent nuclear

facilities at the SRS. A design basis earthquake, which has an estimated annual frequency of 2.0×10^{-4} per year (or one occurrence every 5,000 years), could cause multiple facilities within a single facility area, resulting in the simultaneous release of and/or toxic materials from these facilities to the environment. It is also considered probably less likely, than an earthquake of the same magnitude could damage facilities in one facility area (e.g., F- and H-Areas; K-, L-, and P-Reactor Disassembly Basins), simultaneous releases to the environment.

A semi-quantitative evaluation of the cumulative impacts resulting from multiple releases from a single facility area caused by a severe seismic event was performed as part of the accident scenario analysis described in Section A.2.1. A review of the safety analysis reports for the H-Canyon Receiving Basin for Offsite Fuels was performed to determine the consequences and risks individually by each facility following a design basis earthquake. The risks presented in the accident scenario analysis report were then summed to approximate the risk that would be expected if releases occurred simultaneously from a single seismic initiator. The sum of these risks was compared to the risks of the other accident scenarios presented within the EIS and were found to be less than those accidents. A similar evaluation was performed for the spent nuclear fuel reprocessing facility, F-Area, and the same conclusion was reached. For the reactor disassembly basins, based on a severe earthquake calculated for the K-Reactor Disassembly basin by three components, as the outermost bounding estimate for the three reactor disassembly basins (K-, L-, and P-Reactor Disassembly Basins). This is considered an unrealistic estimate of the cumulative impacts based on extremely conservative assumptions that were made in performing the K-Reactor Disassembly Basin analysis (Meehan 1994). However, even if the risk is increased by a factor of three, the risk is still considered to be bounded by other accidents already presented within the EIS. Therefore, with the accident methodology described in Section A.2.1, no further analysis of this risk was required. The SRS does maintain emergency plans that would provide protective measures to mitigate consequences that could occur during a common cause accident scenario.

A.2.1.4 Accidents Resulting from Terrorism. DOE considered accident scenarios based

on a terrorist attack or an act of sabotage during the screening process and conclusions resulting from such initiators would be bounded by or similar to the accident scenarios considered.

A.2.2 Reference Accident Descriptions

DOE established a reference accident for each of the eight generic or typical accidents outlined in the following paragraphs as the basis for selection of each reference accident by the DOE or submitted to DOE for approval as part of the safety basis analysis for the operation of a facility, and if the facility is to be utilized as, or is similar in design to, facilities included in the five alternatives and their subordinate cases. For example, it was assumed that the Receiving Basin for Offsite Fuel was representative of any spent nuclear fuel storage pool. If an accident could occur in any pool, the analysis selected a reference accident from the Receiving Basin for Offsite Fuel Safety Analysis Report as the reference accident. Table A-2. The following paragraphs provide the basis for each selection.

- A1. Fuel Assembly Breach - Physical damage to an assembly could occur from objects falling onto the assembly, or cutting into the fuel part of an assembly. The Receiving Basin for Offsite Fuel Safety Analysis Report (WSRC 1993a) Addendum 1 contains a current analysis of a "fuel cutting accident." The inert, non-uranium-coated cladding of some spent nuclear fuel elements are cut off (cropped) in the repackaging of the bundling of the elements. The spent nuclear fuel could be inadvertently released, resulting in the release of airborne or high water activity to the work area. Because of the low activity of SRS fuel, only a very small fraction of the gases generated in an assembly would be released to the basin water in an accident. Consistent with the safety analysis, the fuel was cooled for 90 days is used in the source term for this accident. With foreign reactor spent nuclear fuel elements, the release of fission product gases would be similar to the Mark-22 fuel assemblies previously considered. The physics of the release from research reactor fuel is similar to SRS fuel because the fuel is constant in composition. Spent nuclear fuels that could release more fission gases than a Mark-22 assembly would require an Unreviewed Safety Question analysis before the SRS would accept them in the Receiving Basin for Offsite Fuel. Air monitors in this basin would detect personnel in the event of an airborne release. The fuel cutting operation would cut a fuel element at a time. This is representative for all cutting and dropping

- cracking the cladding would release less than cutting into the fuel itself.
- A2. Material Release (Processing) - The primary activities associated with spent nuclear fuel include dissolving the fuel in acid in the F- or H-Area the radioactive and fissile isotopes, and forming those isotopes into a sol metal or powder. Because of the large volumes of liquid radioactive soluti during the dissolution process, uncontrolled reactions in the Canyons are t means of losing control of the material and inadvertently releasing potenti quantities of material to the environment. The most common uncontrolled re those considered in this scenario, include eructations, foaming, boilover, dissolving spent fuel. These types of uncontrolled reactions are typically chemical addition errors, procedural errors, or equipment failure. Although reactions can also include deflagrations and explosions (caused by excess h generation due to radiolytic decay and the presence of an ignition source), events are much less common, and because of their lower frequency, typicall lower risk to workers and members of the public. In developing this scenar assumed that the uncontrolled reaction causes a large release of material w building to the Canyon sumps which results in a greater than normal release material through the ventilation system and Canyon exhaust stack. In addit assumed that the uncontrolled reaction occurred in the F-Canyon facility si resulting from an inadvertent release of plutonium isotopes are expected to inadvertent releases of uranium isotopes from uncontrolled reactions in the facility.
 - A3. Material Release (Dry Vault) - Accident types A1 and A2 cover material from fuel handling and processing. In addition, DOE considered a reference vault-type storage. The Plutonium Storage Facility (PSF) Safety Analysis R 1989) analyzed three medium energetic events (shipping container failure, c impact-type events) and an earthquake. As discussed above, medium energeti accidents that result in release of material from the primary container and energy to penetrate the secondary confinement barriers for a short period o report contains a total frequency of these four initiating events and provi value. Because the SRS has no long-term spent nuclear fuel dry storage fac evaluation assumes that the Plutonium Storage Facility vault is representat facilities, as are the activities and precursor events. A material release energetic event in the Plutonium Storage Facility was selected as the refer nonprocessing material releases.
 - A4. Material Release (Adjacent Facility) - For completeness, DOE considere accident from a facility immediately adjacent to the Receiving Basin for Of (WSRC 1993a). This scenario includes a fire and explosion at the Resin Reg Facility in waste tank EP 38 during which the coolant of a received cask, w to the waste tank, results in a flammable or explosive concentration of vap Rupture of the tank by an explosion could release airborne activity to the accident occurred during one of the projected 150 times per year when regen portable columns takes place. While a fire and explosion have not occurred EP 38, one fire and pressure surge did occur when a shipping cask was being spent nuclear fuel remained intact and radionuclides were not released. Th been attributed to the ignition of a mixture of hydrogen, oxygen, and air e cask and created by reaction of hot aluminum fuel with water left in the ca
 - A5. Criticality in Water - This scenario assumes that a wet pool storage f most likely to have a criticality in water. The Receiving Basin for Offsit capability for underwater receipt, handling, and storage of spent nuclear f radiation shielding is provided by the water covering the spent nuclear fue analysis report determined frequency and results from many initiating event to criticality. The following activities could ultimately lead to a critic Bundling, Cask Loading, Fuel Identification and Manifest Problems, Fuel Mov Dropped Fuel, Fuel Near Basin, Cask Immersion, and Cranes and Hoist. These representative for any wet storage pool.
 - A6. Criticality During Processing - As noted in the discussion for acciden FB-Line events are representative for SRS processing facilities. The analy total of the frequencies for criticality initiators for all processing stag therefore, be conservative because not all processing stages would necessar a new facility and not all stages would necessarily occur simultaneously.
 - A7. Spill/Liquid Discharge (External) - The reference accident selected fo event is the direct discharge of water (i.e., 3.4 million gallons) from the disassembly basin to the Savannah River and the exposure of fuel and target

air. Analyses performed by the DOE while developing the EIS for the Interior of Nuclear Materials at the SRS demonstrate that this scenario could be initiated by an earthquake and would result in bounding airborne exposures (from exposed fuel exposures (contaminated drinking water) to the general public. The selected direct-discharge event is conservative for existing or possible new facilities in the F- or H-Areas because no free-flowing surface streams would be near a discharge. The use of the source term from the reactor disassembly basin is considered conservative for the spent nuclear fuel storage pools since its inventory consists of the fuel types with the largest source terms available for release (i.e., MOX). Although the disassembly basin has water circulating systems to control radionuclide chemistry, clarity, and temperature, these processes are less efficient than the Receiving Basin for Offsite Fuel, resulting in higher concentrations of tritium and other contaminants available for release.

- A8. Spill/Liquid Discharge (Internal) - DOE considered a second reference event for contaminated liquids spills or discharges to ensure the appropriate onsite discharge discussed for accident type A7 would be external to the building and that no measurable worker impact component because the reference accident occurred at the facility. The Receiving Basin for Offsite Fuel hose rack spill was selected as the reference accident because it is representative of small, unplanned, but relatively frequent storage facility and could impact the worker. Minor releases of contaminants occur at the hose rack platform during the handling of portable deionizers in these areas.

A.2.3 Source Term and Frequency Determinations

Table A-2 lists source term references from existing documents approved by DOE from Westinghouse Savannah River Company to DOE for approval for each selected reference. The same references nominally prescribed the frequency of accidents or initiating events. Where directly available, the frequency was derived from information already contained in the safety analysis report or EIS (e.g., if only a risk estimate and a dose were listed, the frequency was derived by dividing the risk by the dose). These frequencies fall into ranges associated with events (more frequent than 1×10^{-3} per year), design-basis accidents (1×10^{-3} per year), or beyond-design-basis accidents (less than 1×10^{-6} per year to 10^{-7} per year).

This document does not analyze beyond-design-basis accidents or accidents with frequencies less than 1.0×10^{-6} explicitly because the accident analysis source material (DOE accident analysis reports) considers these accidents to be incredible events. Beyond-design-basis accidents such as an airplane crash-induced criticality, have no different consequences (i.e., they are more severe) than the criticality estimated to occur with a frequency of 3.1×10^{-3} per year. Because aggregate frequencies in some cases, the contribution to overall risk from 1.0×10^{-6} per year events is negligible, and the higher frequency initiators dominate the point estimate of risk, precursor event frequencies from the safety analysis reports are at 10^{-7} per year or greater. Reports in fact consider events beyond the 10^{-6} frequencies.

Frequencies for reference accidents were determined as follows:

- A1. Fuel Assembly Breach - The frequency for this reference accident was obtained from DPSTSA-200-10-3, Receiving Basin for Offsite Fuel (RBOF), Addendum 1, Table 5-9, which lists the frequency as 1.6×10^{-1} per year (WSRC 1993a).
- A2. Material Release (Processing) - The frequency for this reference accident was obtained from DPSTSA-200-10-4, Safety Analysis - 200 Area, Savannah River Plant F-Canyon Operations, Addendum 2, "Accident Analysis," Revision 1, Table A.5, which lists the frequency for an uncontrolled chemical reaction (the bounding accident) as 2.6×10^{-1} per year (Meehan 1995).
- A3. Material Release (Dry Vault) - The frequency for this reference accident was obtained from DPSTSA-200-10-19, Final Safety Analysis Report - 200 Area, Savannah River Plant Separations Area Operations, Building 221F, B-Line, Plutonium Storage Facility, Table 5-9, which lists the frequency as 1.4×10^{-3} per year (Du Pont 1989).
- A4. Material Release (Adjacent Facility) - The frequency for this reference accident was obtained from DPSTSA-200-10-3, Receiving Basin for Offsite Fuel (RBOF), Addendum 1, Tables 1-5, which lists the frequency as 2.4×10^{-3} per year (WSRC 1993a).
- A5. Criticality in Water - The frequency for this reference accident was obtained from DPSTSA-200-10-3, Receiving Basin for Offsite Fuel (RBOF), Addendum 1, Table 5-9, which lists the frequency as 3.1×10^{-3} per year (WSRC 1993a).
- A6. Criticality During Processing - The frequency for this reference accident was obtained from WSRC-RP-93-1102, FB-Line Basis for Interim Operation, November 1993.

- Figure 3, which lists a frequency of 1.4×10^{-4} per year (WSRC 1993d).
- A7. Spill/Liquid Discharge (External) - The frequency for this reference is derived from analyses provided in DOE/EIS-0147, Continued Operation of K-, P-Reactors, December 1990 (DOE 1990), as well as other safety analyses developed for additional SRS facilities. The initiating event is a design basis earthquake with horizontal ground accelerations equal to 0.2 times the force of gravity (i.e., occurs with an estimated frequency of 2.0×10^{-4} per year, and results in 1.4 million gallons of basin water (3.4 million gallons) to the Savannah River.
 - A8. Spill/Liquid Discharge (Internal) - The frequency for this reference is obtained from DPSTSA-200-10-3, Receiving Basin for Offsite Fuel (RBOF), Add Tables 1 - 3, which lists the frequency as 1.1×10^{-1} per year for a repressurization system (WSRC 1993a).

A.2.4 Applicability of Accidents to Facilities

This evaluation reviewed Section 1 of the reference document Technical Data Summary Supporting the Spent Nuclear Fuel Environmental Impact Statement (WSRC 1994b) to develop a matrix of the selected radiological accidents to the facilities (modules) being considered for alternatives and cases. For proposed new facilities, the analysis used best engine extrapolation from appropriate accident scenarios based on the descriptions provided in the document. Table A-3 lists the connection of facilities to accident scenarios. For Examination and Characterization Facility (module B) identifies a potential accident defined in Table A-2, that should be considered when this facility is utilized to support the facility. Applicable accidents and facilities.

Facility	Module
Spent Fuel Receiving, Cask Handling and Fuel Unloading	A
Examination and Characterization	B
Naval Reactor Spent Fuel Examination and Characterization	C
Spent Fuel Repackaging	D
Canister Loading	E
Interim Dry Storage	F
Interim Spent Fuel Storage Pool	G
F-Canyon/F-Area Separations	H, I
H-Canyon/H-Area Separations	J, K, L
Reactor Disassembly Basins	M
Receiving Basin for Offsite Fuels	N

a. As defined in WSRC (1994b).

A.2.5 Facilities and Reference Accidents Associated with each Alternative Case

Table A-4 links alternatives, specific cases, supporting facilities (modules), accident scenarios. This table identifies the facilities that could be required to support a specific case. The combined associated accident scenarios for each facility provide a spectrum associated with the specific cases for each alternative.

A.2.6 Impacts from Radioactive Release Accidents

This section provides a quantitative discussion of potential consequences to the public identified in Section A.1.4.1. It also provides a qualitative discussion on potential consequences for workers at less than 100 meters (328 feet) for each of the potential accident scenarios.

Table A-4. Spent nuclear fuel facilities and accident spectrum by alternatives.

Alternative	Module
1. NO ACTION	
Option 1 - Wet Storage	M, N
2. DECENTRALIZATION	
Option 2a - Dry Storage	B, D, E, F, G, M, N
Option 2b - Wet Storage	B, D, E, G, M, N
Option 2c - Processing	G, H, I, J, K, L, M, N

3. PLANNING BASIS

Option 3a - Dry Storage

B, D, E, F, G, M, N

Option 3b - Wet Storage

B, D, E, G, M, N

Option 3c - Processing

G, H, I, J, K, L, M, N

4. REGIONALIZATION

Option 4a - Dry Storage

A, B, D, E, F, G, M, N

Option 4b - Wet Storage

A, B, D, E, G, M, N

Option 4c - Processing

A, G, H, I, J, K, L, M, N

Option 4d - Dry Storage

A, B, C, D, E, F, G, M, N

Option 4e - Wet Storage

A, B, C, D, E, G, M, N

Option 4f - Processing

A, C, G, H, I, J, K, L, M, N

Option 4g - Ship Out

M, N

5. CENTRALIZATION

Option 5a - Dry Storage

A, B, C, D, E, F, G, H, M, N

Option 5b - Wet Storage

A, B, C, D, E, G, M, N

Option 5c - Processing

A, C, G, H, I, J, K, L, M, N

Option 5d - Ship Out

M, N

a. Source: WSRC (1994b).

A.2.6.1 Radioactive Release Accidents and Consequences for Spent Nuclear Fuel

Alternatives. Table A-5 summarizes the information in Tables A-2 through A-4 and p individual consequences (doses) based on accident type for each case. The table li the four receptor groups as follows: Maximum Offsite Individual Dose, the Populati 80 kilometers (50 miles) Dose, the Worker Dose, and the Colocated Worker Dose. Table A-5. Radioactive release accidents and consequences for spent nuclear fuel alternatives.

Description	Accident	Accident frequency (per year)
Option 1 Wet Storage	1. NO ACTION	
	A1 Fuel Assembly Breach	1.6x10 ⁻¹
	A4 Material Release (adjacent facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
	2. DECENTRALIZATION	
	A1 Fuel Assembly Breach	1.6x10 ⁻¹
Option 2a Dry Storage	A3 Material Release (dry vault)	1.4x10 ⁻³
	A4 Material Release (adjacent facility)	2.4x10 ⁻³
	A5 Criticality in Water	3.1x10 ⁻³
	A7 Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8 Spill/Liquid	1.1x10 ⁻¹

Option 2b Wet Storage		Discharge (internal)	
	A1	Fuel Assembly Breach	1.6x10 ⁻¹
	A4	Material Release (adjacent facility)	2.4x10 ⁻³
	A5	Criticality in Water	3.1x10 ⁻³
	A7	Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
Option 2c Processing	A8	Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
	A1	Fuel Assembly Breach	1.6x10 ⁻¹
	A2	Material Release (processing)	2.6x10 ⁻¹
	A3	Material Release (dry vault)	1.4x10 ⁻³
	A4	Material Release (adjacent facility)	2.4x10 ⁻³
	A5	Criticality in Water	3.1x10 ⁻³
	A6	Criticality in Processing	1.4x10 ⁻⁴
		Accident	Accident frequency (per year)
	2.	DECENTRALIZATION	
	A7	Spill/Liquid Discharge (external)	2.0x10 ⁻⁴
	A8	Spill/Liquid Discharge (internal)	1.1x10 ⁻¹
	3.	PLANNING BASIS	
Option 3a Dry Storage		Same as Option 2a for Decentralization	
Option 3b Wet Storage		Same as Option 2b for Decentralization	
Option 3c Processing		Same as Option 2c for Decentralization	
Option 4a and 4d Dry Storage Option 4b and 4e Wet Storage Option 4c and 4f Processing Option 4g	4.	REGIONALIZATION	
		Same as Option 2a for Decentralization	
		Same as Option 2b for Decentralization	
		Same as Option 2c for Decentralization	
		Same as Alternative 1, No Action	

Ship Out

5. CENTRALIZATION

Option 5a Same as Option 2a for Decentralization

Dry Storage

Option 5b Same as Option 2b for Decentralization

Wet Storage

Option 5c Same as Option 2c for Decentralization

Processing

Option 5d Same as Alternative 1, No Action

Ship Out

- a. The safety analysis reports from which information was extracted for these accidents were written before the issuance of DOE Orders 5480.23 (DOE 1992); previous orders did not require the inclusion of worker doses.

A.2.6.2 Impacts to Workers at Less than 100 Meters from Radiological

Releases. This section provides a qualitative discussion addressing the impacts due to potential radiological accident scenarios to workers at less than 100 meters (328 feet) involved in SRS spent nuclear fuel management. While worker fatalities may result from release initiators (i.e., plane crashes, seismic event, crane failure, etc.) and not as a direct consequence of a radiation release, this discussion considers only the radiological impacts of an accident, should it occur.

- A1. Fuel Assembly Breach - No fatalities to workers would be expected from radiological consequences because the release of the source term would be under water. Attenuation by the water would occur for most products, but the release of noble gases would cause a direct radiation exposure to workers in the area. However, because of the high metallic content of SRS spent nuclear fuel, only a very small fraction of the gases generated in an assembly would be released to the basin water. Air monitors in the area would warn personnel in the event of an airborne release. Timely evacuation would prevent substantial radiation exposures.
- A2. Material Release (Processing) - No fatalities to workers would be likely from radiological consequences (Meehan 1995). This scenario assumes that the material released from the process vessels would remain within the Canyon structure and be processed through the Canyon's ventilation and filtration system. Because of shielding effect from the thick concrete walls separating the vessels and areas occupied by workers, the exposures to workers are not expected to be significantly larger than those that would be received during routine operations.
- A3. Material Release (Dry Vault) - No fatalities to workers would be likely from radiological consequences. Medium energetic events resulting in the release of radioactive material from the Plutonium Storage Facility vault can result in the dispersal of radioactive materials. For these events, the radioactive material present would bypass the containment and disperse, but would result in a dose well below the lethal level. This assumes that a material release would be distributed into the volume of the smallest room for each unit of operation. It is further assumed that the operator is able to exit the room in 30 seconds (Du Pont 1989). This scenario presumes that the fractions of the plutonium volatilized and transported are the same as those applied to the dispersal of the nonvolatile fission products of a criticality. Based on these assumptions, radiological exposure to the worker could occur.
- A4. Material Release (Adjacent Facility) - No fatalities to workers would be likely from radiological consequences. The rupture of a waste tank by an explosion could release airborne activity to the shielded cell if the accident occurred during one of the projected 150

times per year when regeneration of the portable columns took place (WSRC 1993a). Although some radiological exposure to the worker could occur, the risk to the worker from the initiating fire and explosion would predominate. Air monitors in the area would warn personnel in the event of an airborne release. Timely evacuation would prevent substantial radiation exposures.

- A5. Criticality in Water - No fatalities to workers would be likely from radiological consequences. The use of casks and the underwater handling of spent nuclear fuel greatly reduce the possibility of over-exposure of workers to radiation. The approximately 3 meters (10 feet) of water that covers all fuel provides an attenuation factor of 105 for intense gamma radiation and provides protection from direct radiation, even in the event of a criticality. However, a small chance of direct radiation exposure could result due to a floating fuel element or a fuel element inadvertently being raised too high. Strategically located radiation monitors reduce even this probability by alerting workers and sounding an evacuation alarm.
- A6. Criticality During Processing - The radiation field generated by a criticality incident could lead to fatalities among workers at the FB-Line facility. As discussed in Section A.2.2, FB-Line inadvertent criticality events are bounding for F- and H-Area spent fuel management processing facilities. This is assumed because workers involved in the FB-Line activities are in close proximity to plutonium metal. Of the 74 personnel that could be present during normal operations, 56 are expected to be within areas which the safety analysis report (WSRC 1993d) identifies as potential criticality accident locations. The shielding due to the concrete floors and walls, the distance between personnel, and the specific nature of the event reduce personnel dose so that only nearby personnel on the floor where the accident occurred would potentially receive a fatal dose. In the event of a criticality accident, DOE estimates that up to 4 deaths could occur, and as many as 50 other workers could receive non-fatal levels of direct radiation.
- A7. Spill/Liquid Discharge (External) - No fatalities to workers would be likely from radiological consequences because drainage of the water from the pool or basin would be expected to take several days, or under the most extreme circumstances, several hours, which provides sufficient time for workers to evacuate the area.
- A8. Spill/Liquid Discharge (Internal) - No fatalities to workers would be likely from radiological consequences. Minor releases of contaminated water have occurred at the Receiving Basin for Offsite Fuel hose rack platform during the handling of portable deionizers from the reactor areas. One such release was the result of an operator attempting to correct a small leak on a pressurized portable deionizer. The operator was subsequently sprayed with contaminated water, resulting in a radioactive exposure. A spill at the hose rack is not expected to release more than 378.5-liters (100 gallons) of contaminated water.

A.2.7 Point Estimates of Risk

Table A-6 lists the point estimate of risk for each reference accident considered for two receptors. The point estimate of risk is the product of frequency (in occurrences per year) and the number of potential latent fatal cancers. The number of potential latent fatal cancers is the product of dose (in rem for the individual or person-rem for the population) and the ICRP 60 risk factors (4.0×10^{-4} latent fatal cancer per rem for the worker or 5.0×10^{-4} latent fatal cancer per rem for the general public). These point

estimates were used to determine the relative risk for each case and to determine the accident that becomes dominant if DOE retires specific facilities during the total period under consideration. For example, all alternatives begin with the immediate storage of spent nuclear fuel in wet pools; however, for the alternative considering interim dry storage, the accident dominating risk will change as the configuration of facilities utilized changes and as spent nuclear fuel or special nuclear material is placed in and remains in interim storage rather than being handled.

A.2.8 Fuel Transition Staging Risk

Table A-7 facilitates the examination of the dominant reference accident during the fuel handling, processing, and storage stages. The use of stages enabled a realistic comparison of risk over the evaluated period. For example, when all fuel has been unloaded, characterized, canned, and put into an interim storage position, consideration of fuel handling events is no longer meaningful.

A.2.9 Adjustment Factors for Comparison Between Alternatives

The accident scenarios described in this document (i.e., Appendix C) differ only slightly between the various alternatives. The scenarios do not account for variations in spent nuclear fuel shipments (including onsite operational transfers) and spent nuclear fuel storage inventories across the alternatives. To provide a realistic comparison across alternatives, DOE developed factors to adjust

Table A-6. Point Estimates of Risk for Reference Accident Scenarios.

Accident Scenario	Descriptions	Frequency (per year)	Potential Fatal Cancers	Population Exposed to 80 kilometers	Point Est Maximally Exposed Individual
A1	Fuel Assembly Breach	1.6×10^{-1}	1.0×10^{-6}	8.5×10^{-3}	1.6×10^{-7}
A2	Material Release (processing)	2.6×10^{-1}	3.4×10^{-8}	2.6×10^{-4}	8.8×10^{-9}
A3	Material Release (dry vault)	1.4×10^{-3}	1.1×10^{-9}	3.5×10^{-6}	1.5×10^{-12}
A4	Material Release (adjacent facility)	2.4×10^{-3}	3.0×10^{-6}	2.5×10^{-2}	7.2×10^{-9}
A5	Criticality in Water	3.1×10^{-3}	1.5×10^{-6}	4.4×10^{-3}	4.7×10^{-9}
A6	Criticality in Processing	1.4×10^{-4}	3.5×10^{-6}	4.3×10^{-3}	4.9×10^{-10}
A7	Spill/Liquid Discharge (external)	2.0×10^{-4}	2.7×10^{-6}	9.0×10^{-3}	5.4×10^{-10}
A8	Spill/Liquid Discharge (internal)	1.1×10^{-1}	1.2×10^{-13}	1.0×10^{-9}	1.3×10^{-14}

- ICRP 60 risk factor (5.0×10^{-4}) latent fatal cancer per rem was used to determine potential latent fatal cancers.
- Units for point estimates of risk are given in potential fatal cancers per year.

Table A-7. Dominant risks based on fuel transition stages.

Fuel/Material Stage	Maximally Exposed Individual Risk	Populat
Wet storage	1.6x10 ⁻⁷ potential fatal cancer/yr based on accident scenario A1.	80 Kilo 1.4x10 ⁻ cancer/ acciden
Dry storage	1.5x10 ⁻¹² potential fatal cancers/yr based on accident scenario A3.	4.9x10 ⁻ cancers acciden
Processing (fuel "in-process" by DOE definition)	1.6x10 ⁻⁷ potential fatal cancer/yr based on accident scenario A1.	1.4x10 ⁻ cancer/ acciden

frequencies or consequences, depending on the specific circumstances of each alternative. This section describes the methodology and justification used to develop adjustment (scaling) factors for a relative comparison of adjusted point estimates of risk for each alternative on a case-by-case basis.

A.2.9.1 Classification of SRS Accident Scenarios for Applicability to

Adjustment Factors. This evaluation screened the SRS accident scenarios to determine which adjustment factor categories were applicable. Table A-8 lists the classification of the different SRS accident scenarios. These adjustment categories are as follows:

- Frequency sensitive due to spent nuclear fuel handling
- Frequency sensitive due to spent nuclear fuel inventories
- Consequence sensitive due to spent nuclear fuel inventories

Table A-8. Adjustment factor classification of SRS accidents.

Accident Scenarios	Accident Description	Frequency Sensitive (Handling)	Fr Se (I
A1	Fuel Assembly Breach	X	
A2	Material Release (Processing)		X
A3	Material Release (Dry Vault)		
A4	Material Release (Adjacent Facility)	X	
A5	Criticality in Water	X	
A6	Criticality during Processing		X
A7	Spill/Liquid Discharge (External)		
A8	Spill/Liquid Discharge (Internal)		

The following paragraphs provide the basis for each category selection:

- A1. Fuel Assembly Breach - The major initiator for this accident is the mishandling of a fuel assembly. For this reason, the accident frequency for this accident is adjusted to account for the annual number of fuel handling events. The amount of material involved in this accident is limited by the amount of damage that would occur due to the mishandling of a fuel assembly. Therefore, the bounding consequences of this accident are constant and independent of the amount of material available.
- A2. Material Release (Processing) - The probability that a release could occur during processing depends on the amount of material that would be processed. Therefore, the accident frequency for this accident is adjusted based on the spent nuclear fuel inventory. Because a maximum amount of material can be processed at any one time, the bounding consequences of this accident are independent of the amount of material on the site.
- A3. Material Release (Dry Vault) - The major contributor to the

probability of occurrence for this release was external initiators that did not involve material handling. This supports using the same frequency for each alternative. The consequences of this accident are proportional to the amount of material available for release. Therefore, the bounding consequences for this accident are based on the amount of material to be stored.

- A4. Material Release (Adjacent Facility) - The initiator for this accident involves the discharge of coolant from a cask into a waste tank. The frequency of occurrence for this accident depends on the number of casks received; therefore, the frequency is adjusted to account for the annual number of fuel shipments.
- A5. Criticality in Water - The probability of occurrence of this accident was determined by considering the probability of occurrence of several initiating events. Many of these initiating events involved a criticality due to the mishandling of fuel. Therefore, the frequency for this accident is adjusted to account for the annual number of fuel handling events. The magnitude of the criticality accident is not a function of the amount of material available because the criticality is a highly unlikely, localized event. The consequences for this accident are not adjusted to account for the amount of material available.
- A6. Criticality During Processing - The probability that a criticality could occur during processing depends on the amount of material that will be processed. Therefore, the frequency for this accident is adjusted based on the spent nuclear fuel inventory. The magnitude of the criticality accident is not a function of the amount of material available because the criticality is a highly unlikely, localized event. The consequences for this accident are not adjusted to account for the amount of material available.
- A7. Spill/Liquid Discharge (External) - The major contributor to the probability of occurrence for this release was external initiators that did not involve material handling. This supports using the same frequency for each alternative. The consequences depend on the amount of fuel in the basin because an increase in the amount of fuel will increase the source term in the basin water. Therefore, the bounding consequences are adjusted for the amount of fuel to be stored.
- A8. Spill/Liquid Discharge (Internal) - The major contributor to the probability of occurrence for this release was external initiators that did not involve material handling. This supports using the same frequency for each alternative. The consequences depend on the amount of fuel in the basin because an increase in the amount of fuel will increase the source term in the basin water. For this reason the bounding consequences are adjusted for the amount of fuel to be stored.

A.2.9.2 Methodology for Determination of Onsite Shipping Frequencies.

This section discusses the methodology for determining the onsite shipping frequencies of spent nuclear fuel on a case-by-case basis for each alternative. The annual frequency of handling accidents will vary in direct proportion to the annual number of handling events. However, the consequences of the accident will not vary as a result of spent nuclear fuel handling activities because the amount of material involved in each handling event does not vary. This evaluation assumes that onsite shipments of spent nuclear fuel are near-term shipments, averaged over 5 years. Table A-9 provides a breakdown of current spent nuclear fuel inventories at SRS facilities. Table A-9. Spent nuclear fuel inventories.

Number of	Number of	Number of	Number
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Facility	Aluminum Assembliesb	Aluminum Slugs (Bucketsc)	Nonaluminum- Clad Assemblies	Aluminu Clad Assembl Shipmen 20
Receiving Basin for Offsite Fuel (RBOF)	234	107 (2)	261	
K-Reactor Basin	1,783	349 (7)	0	149
L-Reactor Basin	861	13,840 (256)	0	72
P-Reactor Basin	577	61 (2)	0	48
Totals	3,455	14,477 (268)	261	289

a

. Basis for inventory numbers: (WSRC 1994c).

b

. Assemblies include targets and fuel assemblies. Assembly shipments are based on 12 assemblies per shipment.

c

. Number of buckets calculated using 54 slugs per bucket. Bucket shipments are based on 3 buckets per shipment.

A.2.9.2.1 Alternative 1 - No Action - The SRS would send the

following number of shipments of aluminum-clad fuel sent to the Receiving Basin for Offsite Fuel from:

- K-Reactor Basin - 152;
- L-Reactor Basin - 158;
- P-Reactor Basin - 49;
- Total - 359 shipments.

All nonaluminum-clad fuel would be sent from the Receiving Basin for Offsite Fuel to a reactor basin (a total of 22 shipments).

The number of shipments would be 380. Because fuel handling would occur at both origin and destination, this number would double (i.e., 760 total shipments). Therefore, over 5 years, this alternative would have an average shipping rate of 152 shipments per year.

A.2.9.2.2 Alternative 2 - Decentralization

- Option 2a - Dry Storage - For this option, initial shipments would be the same as those for Alternative 1 (760 shipments at a rate of 152 per year). Subsequent shipments from all storage locations to the new dry storage facilities would total 402 shipments. Because fuel handling would occur at both origin and destination, this number would double (i.e., 804 total shipments). Because all fuel would be moved to dry storage within a 5-year period, this total would have an average rate of 161 shipments per year. Adding all shipments would produce a total of 1,564 shipments at a rate of 313 per year.
- Option 2b - Wet Storage - For this option, initial shipments would be the same as those for Alternative 1 (760 shipments at a rate of 152 per year). Subsequent shipments from all storage locations to the new wet storage facilities would total 402 shipments for existing SRS fuel. Because the receipt of offsite fuel would continue prior to the relocation of fuel to the new wet storage facilities, an additional 50 shipments would occur [assuming receipt of five shipments per year of offsite fuel (per Volume 1, Appendix I "Offsite Transportation of

Spent Nuclear Fuel"] until 2005. The resulting fuel movement would total 452 shipments. Because fuel handling would occur at both origin and destination, this number would double (i.e., 904 total shipments). Therefore, over 5 years this option would have an average shipping rate of 181 shipments per year. Adding all shipments under this option would produce a total of 1,664 shipments at a rate of 333 per year.

- Option 2c - Processing - In this option, all aluminum-clad fuel would move from its present location to the process facilities. All nonaluminum-clad fuel would remain in its present storage locations. The result would be in a total of 380 shipments. As in the previous options, this number would double for a total of 760 shipments. Therefore, over 5 years this option would have an average shipping rate of 152 shipments per year.

A.2.9.2.3 Alternative 3 - Planning Basis

- Option 3a - Dry Storage - The movement of materials for this option would be identical to that for Option 2a, resulting in a total of 1,564 shipments at a rate of 313 per year.
- Option 3b - Wet Storage - The movement of materials for this option would be identical to that for Option 2b, with the exception of a delay in the receipt of foreign fuel until the new facilities are in operation. This would result in a total of 1,564 shipments at a rate of 313 per year.
- Option 3c - Processing - The movement of materials for this option would be identical to that for Option 2c, resulting in a total of 760 shipments at a rate of 152 shipments per year.

A.2.9.2.4 Alternative 4 - Regionalization

- Option 4a - Dry Storage - For this option, initial shipments would be the same as Alternative 1 (760 shipments at a rate of 152 per year). Subsequent shipments of the aluminum-clad fuel to the new dry storage facilities would total 380 shipments. (Note: Nonaluminum-clad fuel would be sent offsite from the reactor basins and would not contribute to any further onsite movements.). Because fuel handling would occur at both origin and destination, this number would double (i.e., 760 total shipments). Because all fuel would move to dry storage within about 5 years, this total would have an average shipping rate of 152 shipments per year. Adding all shipments would produce a total of 1,520 shipments at a rate of 304 per year.
- Option 4b - Wet Storage - The movement of materials for this option would be identical to that for Option 3b, with the exception of movement of the nonaluminum-clad fuel to the new wet storage facility. This fuel would move off the Site from the reactor basins and would not contribute to any further onsite movements. This would result in a total of 1,520 shipments at a rate of 304 per year.
- Option 4c - Processing - The movement of materials for this option would be identical to that for Options 2c and 3c, resulting in a total of 760 shipments at a rate of 152 per year.
- Option 4d - Dry Storage - The movement of materials for this option would be identical to those for Options 2a and 3a, resulting in a total of 1,564 shipments at a rate of 313 per year.

- Option 4e - Wet Storage - The movement of materials for this option would be identical to that for Option 3b, resulting in a total of 1,564 shipments at a rate of 313 per year.
- Option 4f - Processing - The movement of materials for this option would be identical to those for Options 2c, 3c, and 4c, resulting in a total of 760 shipments at a rate of 152 per year.
- Option 4g - Ship Out - This option would require the shipping of all spent nuclear fuel at the SRS to a selected regional location. The movement of materials for this option would include the entire spent nuclear fuel inventory at the SRS, resulting in a total of 402 shipments at a rate of 81 per year.

A.2.9.2.5 Alternative 5 - Centralization

- Option 5a - Dry Storage - The movement of materials for this option would be identical to those for Options 2a and 3a, resulting in a total of 1,564 shipments at a rate of 313 per year.
- Option 5b - Wet Storage - The movement of materials for this option would be identical to that for Option 3b, resulting in a total of 1,564 shipments at a rate of 313 per year.
- Option 5c - Processing - The movement of materials for this option would be identical to those for Options 2c, 3c, and 4c, resulting in a total of 760 shipments at a rate of 152 shipments per year.
- Option 5d - Ship Out - This option would require the shipping of all spent nuclear fuel at the SRS to a selected central location. The movement of materials for this option would include the entire spent nuclear fuel inventory at the SRS, resulting in a total of 402 shipments at a rate of 81 per year.

A.2.9.3 Methodology for Determination of Offsite Shipping Frequencies.

This evaluation determined the total number of offsite shipments using the data contained in Volume 1, Appendix I, "Offsite Transportation of Spent Nuclear Fuel." The total number of Naval Fuel shipments was determined from Table 3 of "Methodology for Adjusting SNF Facility Accident Probabilities and Consequences For Different EIS Alternatives" (dated March 18, 1994).

Naval, foreign, and university shipments would occur throughout the interim management period and could be averaged over the 40-year period covered by this EIS. All other shipments would be averaged over 5 years.

A.2.9.4 Frequency Adjustment Factors for Fuel Handling. For this

analysis, DOE assumed the baseline fuel handling rate (events per year) to be the No Action alternative. For the other alternatives, this evaluation divided the expected spent nuclear fuel handling rate by the baseline spent nuclear fuel handling rate (No Action) to obtain the adjustment factor (see Table A-10).

A.2.9.5 Frequency/Consequence Adjustment Factors Due to Inventory. The

No Action alternative for the SRS would require the storage of 206 MTHM (227 tons) of fuel. Using this amount as the baseline, this evaluation compared the amount of fuel for the other alternatives to the base number, as listed in Table A-11. These adjustment factors can be applied to either a

frequency or a consequence, depending on the classification of the accident scenario as listed in Table A-8.

A.3 Chemical Hazard Evaluation

A.3.1 Selection of Reference Chemical Hazard

A review of the same safety analyses used to generate the spectrum of radiological accident scenarios failed to identify a quantitative discussion of chemical hazards. However, each of the safety analyses provided a qualitative discussion of chemical hazards. Thus, Section 5.15.3 discusses chemical hazards associated with existing spent nuclear fuel facilities qualitatively. This qualitative evaluation was determined to be appropriate based on three criteria: sliding scale in proportion to significance, public perception of severity, and long-term effects of chemicals not known. For completeness, a separate risk assessment (WSRC 1993c) provided a quantitative discussion of chemical hazards for the Receiving Basin for Offsite Fuel facility. This assessment described a bounding chemical hazard accident involving the release of nitrogen dioxide vapor.

Table A-10. Fuel handling frequency adjustment factors.

Option Number	Estimated Annual Shipping Rate	Frequen Adjustm
Alternative 1 - No Action		
Option 1	152	Baselin
Alternative 2 - Decentralization		
Option 2a	316	2.08
Option 2b	333	2.19
Option 2c	157	1.03
Alternative 3 - Planning Basis		
Option 3a	375	2.47
Option 3b	375	2.47
Option 3c	216	1.42
Alternative 4 - Regionalization		
Option 4a	421	2.77
Option 4b	421	2.77
Option 4c	269	1.77
Option 4d	394	2.59
Option 4e	394	2.59
Option 4f	234	1.54
Option 4g	160	1.05
Alternative 5 - Centralization		
Option 5a	803	5.28
Option 5b	803	5.28
Option 5c	643	4.23
Option 5d	160	1.05

Table A-11. Inventory adjustment factors for each alternative.

Alternative	Inventory ^a (MTHM ^b)	Adjustm
No Action	206.27	Baselin
Decentralization	219.89	1.07
Planning Basis	222.76	1.08
Regionalization	213.09	1.03
- A		
Regionalization	256.62	1.24
- B		
Centralization	2,741.80	13.30

a. Source: Wichmann (1995).

b. Metric Tons Heavy Metal; to convert to tons, multiply by 1.1023.

A.3.2 Hazardous Chemical Inventories

The inventory of hazardous chemicals at each facility was determined by using the "Savannah River Site Tier Two Emergency and Hazardous Chemical Inventory Report" (WSRC 1994a) to get the facility's total chemical inventory, then listing those chemicals that also appeared on the EPA's "List of Lists" (EPA 1990). The chemical inventories listed in Tables A-12 through A-15 represent facilities used for wet storage and/or processing of spent nuclear fuel. The SRS maintains no large-scale dry storage facilities; thus, chemical inventories for dry storage facilities are not listed.

Table A-12. Hazardous chemical inventory for the Receiving Basin for Offsite Fuel.

Chemical	Maximum Daily Amount (Kg) ^a	Average Daily Amount (Kg)
Ethylene glycol	2,981	23
Methyl ethyl ketone	2	2
Nitric acid	4,731	2,365
Phosphoric acid	3,953	3,953
Sodium hydroxide (caustic soda)	5,800	2,900
Sodium nitrite	3,070	1,535

a. To convert kilograms to pounds, multiply by 2.2046.

Table A-13. Hazardous chemical inventory for the reactor basins (typical).

Chemical	Maximum Daily Amount (Kg) ^a	Average Daily Amount (Kg)
Aluminum sulfate (solution)	570	230
Ethylene glycol (thermal arc torch coolant concentrate)	2	2
Hydrogen peroxide	1	1
Nitric acid	75	75
Sodium hydroxide	454	454
Sodium hypochlorite	11	6
Zinc	0.5	0.5

a . To convert kilograms to pounds, multiply by 2.2046.

Table A-14. Hazardous chemical inventory for H-Area.

Chemical	Maximum Daily Amount (Kg) ^a	Average Daily Amount (Kg)
Dichlorodifluoromethane (Freon 12)	227	68
Dichlorodifluoromethane (Racon 12)	227	0
Ethylene glycol	4.0	2.0
Hydrofluoric acid	1	0.5
Hydrogen peroxide	0.5	0.0
Mercury	4,900	4,900
Methyl ethyl ketone	3	3
Nitric acid	10	5
Nitric oxide	1,300	1,300
Phosphorus pentoxide	1	1
Potassium permanganate (Cairox)	200	100
Sodium hydroxide	1	1
Sodium hypochlorite	41	29
Sulfuric acid	1	0.5
Trichlorofluoromethane (Freon 11)	1,150	1,000
Trichlorofluoromethane (Genetron 11)	450	0

a . To convert kilograms to pounds, multiply by 2.2048.

Table A-15. Hazardous chemical inventory for F-Area.

Chemical	Maximum Daily Amount (Kg) a	Average Daily Amount (Kg)
Dichlorodifluoromethane (Freon 12)	1	0.5
Dichlorodifluoromethane (Racon 12)	1	0
Ethylene glycol	4	2
Hydrofluoric acid	1,177	1,177
Potassium permanganate	3	1
Sodium hydroxide	0.5	-
Sodium hypochlorite	7	4
Sulfuric acid	30	-
Trichlorofluoromethane (Freon 11)	900	450

a . To convert kilograms to pounds, multiply by 2.2048.

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