

# **NON-PROPRIETARY CALCULATIONS**

**Book 2 of 8**

**Attachments to PG&E Letter DIL-01-004  
Dated December 21, 2001**

PGE-009-CALC-003

Calculation No.



ENERCON SERVICES, INC.

ENGINEERING CALCULATION  
COVER SHEET

Calc. No. PGE-009-CALC-003

Rev. 2

Sheet 1 of 89

Title: ISFSI Cask Storage Pad Seismic Analysis

Client: PG&E

Job No. PGE-009

Purpose Of Calculation:

The purpose of this calculation is to compute the size and thickness of the ISFSI Cask Storage Pads and to compute the moments within the storage pad for the controlling seismic load combinations specified for the site. Analyses are in compliance with the seismic load combinations, as set forth, in References 2, 3, 8 and 9 for load combinations, which involve Hosgri and Long-Term Seismic Program earthquakes. The ISFSI Facility will contain (7) pads, which will support (20) HI-Storm Storage Casks per pad. The storage casks are arranged in a 5 x 4 array and are located on 17'-0" centers. The results of the analyses indicate that a pad, 105'-0" (N-S direction) x 68'-0" (E-W direction) x 7'-6" thick (nominal), is acceptable for the storage casks and the seismic loads.

This Calculation considers load combinations for the sequencing of cask placements, but does not consider load conditions other than seismic (e.g., curing temperatures and shrinkage). The results from this Calculation will be used in Calculation No. PGE-009-CALC-007 to evaluate the concrete per the design codes and to determine the size of steel reinforcement.

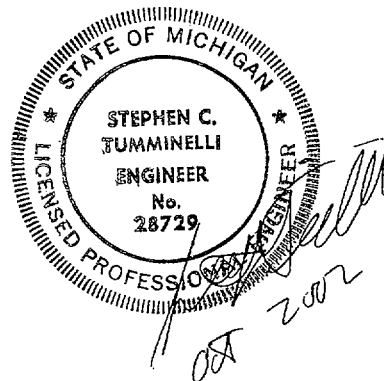
**NOTE:** This Calculation is furnished as part of PG&E Contract No. 4600010841, Change Order No. 001

Scope Of Revision:

Revised references 4 and 7 to latest revision.

Revision Impact On Results:

No impact.



☒ Safety Related

☐ Non-Safety Related

☐ Preliminary Calculation

☒ Final

Approvals  
(Print Name and Sign)

Originator S.C. TUMMINELLI

Date December 14, 2001

Reviewer

Verification Engineer K.L. WHITMORE

Date December 14, 2001

Approver R.F. EVERS

Date December 14, 2001



# **ENGINEERING CALCULATION REVISION STATUS SHEET**

**ENERCON SERVICES, INC.**

**CALCULATION NO.          PGE-009-CALC-003**

## **ENGINEERING CALCULATION REVISION SUMMARY**

<u>REVISION NO.</u>	<u>DATE</u>	<u>DESCRIPTION</u>
0	5/25/01	Initial Issue
1	11/30/01	General Revision
2	12/14/01	Revised references 4 and 7 to latest revision

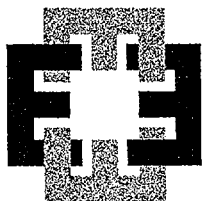
## **CALCULATION SHEET REVISION STATUS**

<u>SHEET NO.</u>	<u>REVISION NO.</u>	<u>SHEET NO.</u>	<u>REVISION NO.</u>
All	1	8	2

## **APPENDIX AND ATTACHMENT REVISION STATUS**

<u>APPENDIX NUMBER</u>	<u>ISSUE DATE</u>	<u>REV. DATE</u>	<u>REISSUE DATE</u>	<u>APPENDIX NUMBER</u>	<u>ISSUE DATE</u>	<u>REV. DATE</u>	<u>REISSUE DATE</u>
AL-1	5/25/01	11/30/01		MD-3	5/25/01	11/30/01	
DN-1	5/25/01		11/30/01	MD-4	11/30/01		
DN-2	5/25/01		11/30/01	RL-1	5/25/01		11/30/01
DN-3	5/25/01		11/30/01	RL-2	5/25/01		11/30/01
DN-4	5/25/01		11/30/01	RL-3	11/30/01		
DN-5	11/30/01			RL-4	11/30/01		
DN-6	11/30/01			RL-5	11/30/01		
DN-7	11/30/01			RL-6	11/30/01		
DP-1	5/25/01		11/30/01	SN-1	5/25/01	11/30/01	
EN-1	11/30/01			SN-2	5/25/01		11/30/01
FC-1	11/30/01			SN-3	5/25/01	11/30/01	
FC-2	11/30/01			SN-4	5/25/01		11/30/01
LT-1	11/30/01			SN-5	5/25/01		11/30/01
MD-1	5/25/01		11/30/01	SN-6	5/25/01	11/30/01	
MD-2	5/25/01	11/30/01					





ENERCON SERVICES, INC.

JOB. NO.	PGE-009	SHEET	3	OF	89
PROJECT	DCPP ISFSI	DATE	December 14, 2001		
SUBJECT	ISFSI Cask Storage Pad Seismic Analysis				
CLIENT	PG&E-DCPP	ORIGINATOR	S. C. Tumminelli		
REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
CALCULATION NO.	PGE-009-CALC-003	REVISION	2		

Method of Review:

The calculation has been independently reviewed in accordance with the requirements of ENERCON Corporate Standard Procedure 3.01. The independent verification of the calculation was performed by a detailed review and check of the entire calculation. This included verification of inputs, methodology, results and conclusions as well as a check of the mathematical accuracy of the computations.

Results:

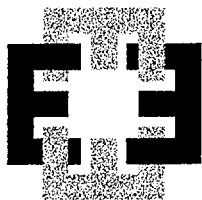
The calculation has been independently verified to be mathematically correct and to be performed in accordance with license and design basis requirements and applicable codes. Inputs are appropriate and are obtained from verified source documents. The calculation is sufficiently documented and detailed to permit independent verification. No assumptions are made other than conservative simplifying assumptions which are identified and do not require confirmation. The methodology used is appropriate and consistent with the purpose of the calculation.

With the exception of the use of non-linear contact elements between the bottom of the concrete support pad and the surface of the rock, the analysis documented in this calculation is a straightforward, first order linear static analysis. The analysis is performed using ANSYS, a computer analysis code that is in widespread use throughout the nuclear industry and that is known to produce accurate results when utilized appropriately.

The use of the non-linear contact elements has been separately verified in computer verification and validation report PGE-009-VVR-003. These elements are designed to transfer compression loads from the concrete pad to the rock but to not transfer any tension loads across the surface. This allows the pad to lift free from the rock in the model if the loads and geometry indicate that liftoff should occur. As documented in PGE-009-VVR-003, these elements have been shown to produce results that are consistent with theoretical values and hand calculations. Thus, the use of these elements in the analysis produces appropriate results.

As indicated in Appendix MD-3, the boundary conditions used in the model are appropriate and do not appreciably affect the results of the analysis. The three directional components of the earthquake load are applied in a conservative and realistic manner that adequately captures the expected behavior during an actual earthquake.

Thus, the analysis has been independently verified to be technically correct and to be consistent with license and design basis requirements. The results and conclusions accurately reflect the findings of the calculation. Thus, the concrete pad has been shown to be of an adequate size to support 20 fully loaded spent fuel storage casks during a seismic event at Diablo Canyon Power Plant.



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PROJECT	DCPP ISFSI	DATE	November 30, 2001		
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CLIENT	PG&E-DCPP	ORIGINATOR	S. C. Tumminelli		
REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
CALCULATION NO.	PGE-009-CALC-003	REVISION	1		

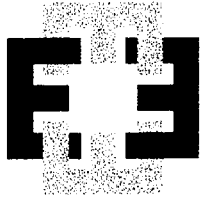
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  - Concrete Pad
  - Rock
  - Casks
  - Material Numbers
  - Contact Elements
  - Constraint Equations
  - Boundary Conditions
  - Gravity and Seismic Loads
- Analysis Results
  - Pad Response - Displacements and Stresses
  - Pad Response - Internal Forces
  - Rock Bearing Pressures
- Pad Response at Reduced Concrete Density
- Pad Response for Cask Placement Sequence
- Pad Response for Cask Extraction
- Effects of Poisson's Ratio of the Rock
- Summary and Conclusions

### Appendices:

MD-1	Cask Centerline Nodes	5 pages
MD-2	Cask/Embedment Structure Frequency	7 pages
MD-3	Boundary Condition Study	12 pages
MD-4	Pad Strips for Internal Force Calculations	51 pages
AL-1 Calculation and Application of Loads		25 pages
RL-1	Reaction Loads	109 pages
RL-3	Reaction Loads – 90% Pad Density	31 pages
RL-4	Reaction Loads – Cask Placement Sequence	151 pages
RL-5	Reaction Loads – Cask Extraction	17 pages
RL-6	Reaction Loads – Soft Rock with $\text{Nu} = 0.23$	12 pages
DN-1	Maximum Pad Displacements	63 pages
DN-2	Maximum Cask Displacements	54 pages



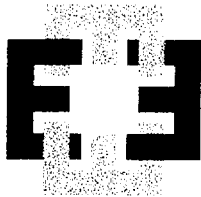
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JOB. NO.	PGE-009	DATE	November 30, 2001		
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SUBJECT	ISFSI Cask Storage Pad Seismic Analysis				
CLIENT	PG&E-DCPP	ORIGINATOR	S. C. Tumminelli		
REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
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DN-5	Max Pad and Cask Displacements – 90% Pad Density	33 pages
DN-6	Max Displacements and Stresses – Cask Extraction	43 pages
DN-7	Max Pad and Cask Displacements – Soft Rock with $Nu = 0.23$	19 pages
DP-1	Pad Vertical Displacement Plots – Soft Rock Model	11 pages
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SN-6	Max and Min Pad Stresses – Soft Rock with $Nu = 0.23$	18 pages
FC-1	Pad Internal Forces – Soft Rock Model	338 pages
FC-2	Pad Internal Forces – Soft Rock with $Nu = 0.23$	205 pages
EN-1	Envelope Data – Cask Placement Sequence	47 pages
LT-1	Analyses for Adjusted LTSP Loads	62 pages

The following appendices provide the data that supports the boundary condition study presented in Appendix MD-3.

RL-2	BC Study - Reaction Loads	85 pages
DN-3	BC Study - Maximum Pad Displacements	45 pages
DN-4	BC Study - Maximum Cask Displacements	36 pages
SN-4	BC Study - Maximum and Minimum Pad X and Z Stresses	92 pages
SN-5	BC Study - Maximum Rock Vertical Stresses	58 pages



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CLIENT	PG&E-DCPP	ORIGINATOR	S. C. Tumminelli		
REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
CALCULATION NO.	PGE-009-CALC-003	REVISION	1		

### ISFSI Pad Seismic Analysis

The primary purpose of this calculation is to determine the storage pad size and thickness required to resist the loads resulting from seismic accelerations applied to the pad and to the used fuel storage casks anchored to the pad. The limiting parameter considered in this assessment is that the pad displacement under the pad dead weight and seismic loads be held to an acceptable value. The analyses presented herein demonstrate that the pad displacements are within acceptable limits. Further this calculation demonstrates that the pad stresses are low and the rock bearing stresses are within acceptable limits for the pad configuration analyzed. Finally, this calculation provides pad internal forces and moments to be used in a subsequent calculation to demonstrate that the design is compliant with the ACI Code and to size the pad reinforcement for the seismic loads.

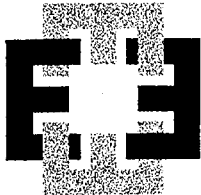
This initial portion of this calculation is performed for the fully loaded configuration, i.e., the pad is designed to accommodate 20 storage casks, and the analyses are performed for the condition of 20 fully loaded casks in place on the pad. Each cask will be physically anchored to the pad with an embedment support structure, evaluated and designed in Calculation 001 (Reference 6). The pad analyses are performed for seismic loads selected to maximize the pad displacements. These analyses are performed for a range of rock properties that have been determined to exist at the site. Additional calculations are then performed that evaluate the pad for the most demanding of the seismic loads and rock properties for the following conditions:

- Pad mass reduced to 90% of its expected value. Necessary to demonstrate ACI Code compliance and to bound the possible as built configurations.
- Cask Placement Sequence. These analyses evaluate the pad for configurations that will exist during the cask placement sequence.
- Cask Extraction. These analyses evaluate the pad for the situation where three casks must be removed from a fully loaded pad.
- Effects of Poisson's Ratio of the Rock. These analyses are designed to provide bounding data for the calculation of pad internal forces and moments.

The pad internal forces and moments will be used in subsequent calculations to demonstrate ACI Code compliance and to determine the required size of reinforcement. These subsequent calculations will also address stresses due to temperature and shrinkage that are not addressed in this calculation.

The analyses performed in this calculation are in compliance with the seismic load combinations involving the Hosgri and Long Term Seismic Program seismic events set forth in PG&E Specification 10012-N-NPG, Holtec report HI-2002511, USNRC NUREG 1536 and ACI 349-97 (References 2, 3, 8, and 9 respectively).

The ISFSI facility will contain 7 pads, each of which will support 20 HI-Storm storage casks. The casks will be arranged in a 5 x 4 array, 17 feet center to center of casks, located in the center of each pad. The



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REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
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results of these analyses indicate that the pad, 105 feet N-S by 68 feet E-W and nominally 7.5 feet thick, is acceptable for the storage casks and the seismic loads, see Figure 1.

Each cask will be attached to an embedment support structure, which will be embedded within the pads (see Reference 6). These embedment structures will transfer the applied loads from the casks to the pads. Compression from the casks to the pad will be transferred directly through a bearing plate and a prepared concrete surface within the embedment structure. Tension will be transferred through rods extending from the concrete surface to anchor plates deep within the pad. The casks are approximately 134 inches in diameter and have a support flange with an outer diameter of 146.5 inches. The diameter of the hold down stud circle is 139.5 inches (Reference 7).

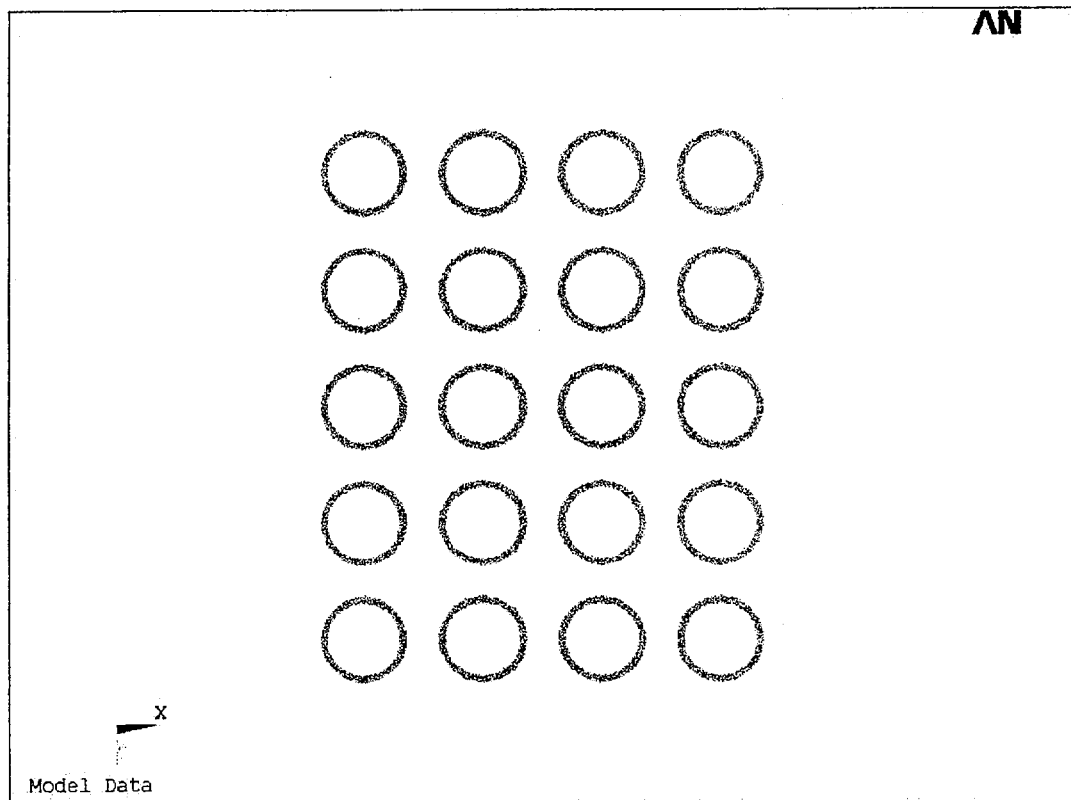
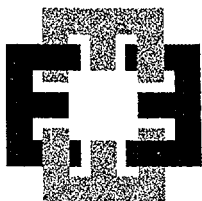


Figure 1 - Plan of One Pad with Casks

Holtec, the cask designer, has supplied the cask loads for the Hosgri and the LTSP earthquakes (Reference 4, page 9). See Table 1 herein. These, together with the seismic ZPAs from PG&E (Reference 2), are the input loads for this calculation. The pads are to be constructed from 5000 psi concrete with 60,000 psi reinforcing steel, and they are to be placed directly on the cut rock. The pads will not be physically attached to the rock.



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The analysis described below is a non-linear static analysis wherein the concrete pad is allowed to lift off the rock support if the loads and geometry dictate that liftoff should occur. All material properties are linear and small deflection theory is used. Compression only gap elements are used at the interface between the pad and the rock. This is the only non-linear modeling feature in the analyses, otherwise the analysis is first order linear. The analysis software is ANSYS, Release 5.7 (Reference 1).

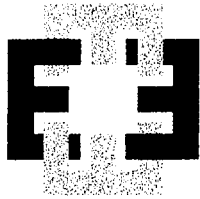
### References

- 1 ANSYS, Release 5.7, ANSYS, Inc., Southpointe, 275 Technology Drive, Canonsburg, PA 15317.
- 2 PG&E Specification, 10012-N-NPG, Rev 2.
- 3 HOLTEC Report HI-2002511, Rev.2, Design Criteria Document for the ISFSI Pad for Anchored HI-Storm 100 Deployment at the Diablo Canyon Power Plant, dated July 12, 2001.
- 4 HOLTEC Report HI-2012618, Rev. 5, Analysis of Anchored HI-Storm Casks at the Diablo Canyon ISFSI, dated December 11, 2001.
- 5 Not Used
- 6 ENERCON Calculation PGE-009-CALC-001, Embedment Support Structure, latest revision.
- 7 Holtec Drawing 3570, Rev 2, Cask Anchor Stud and Sector Lug Arrangement, Dec.12, 2001.
- 8 USNRC, NUREG 1536, Standard Review Plan for Dry Cask Storage Systems
- 9 ACI 349-97, Code Requirements for Nuclear Safety Related Concrete Structures
- 10 USNRC Draft Regulatory Guide DG-1098, Safety-Related Concrete Structures for Nuclear Power Plants (Other Than Reactor Vessels and Containments), dated August 2000.
- 11 PG&E Calculation 52.27.100.711, Development of Young's Modulus and Poisson's Ratios for the DCPD ISFSI Based on Field Data (Ref. GEO.DCPE.01.01), Rev 0, November 9, 2001.
- 12 PG&E Calculation 52.27.100.725, Development of Young's Modulus and Poisson's Ratios for the DCPD ISFSI Based on Laboratory Data (GEO Sciences # GEO.DCPE.01.15), Rev 1, November 27, 2001.

### Pad ANSYS Static Model Construction Description

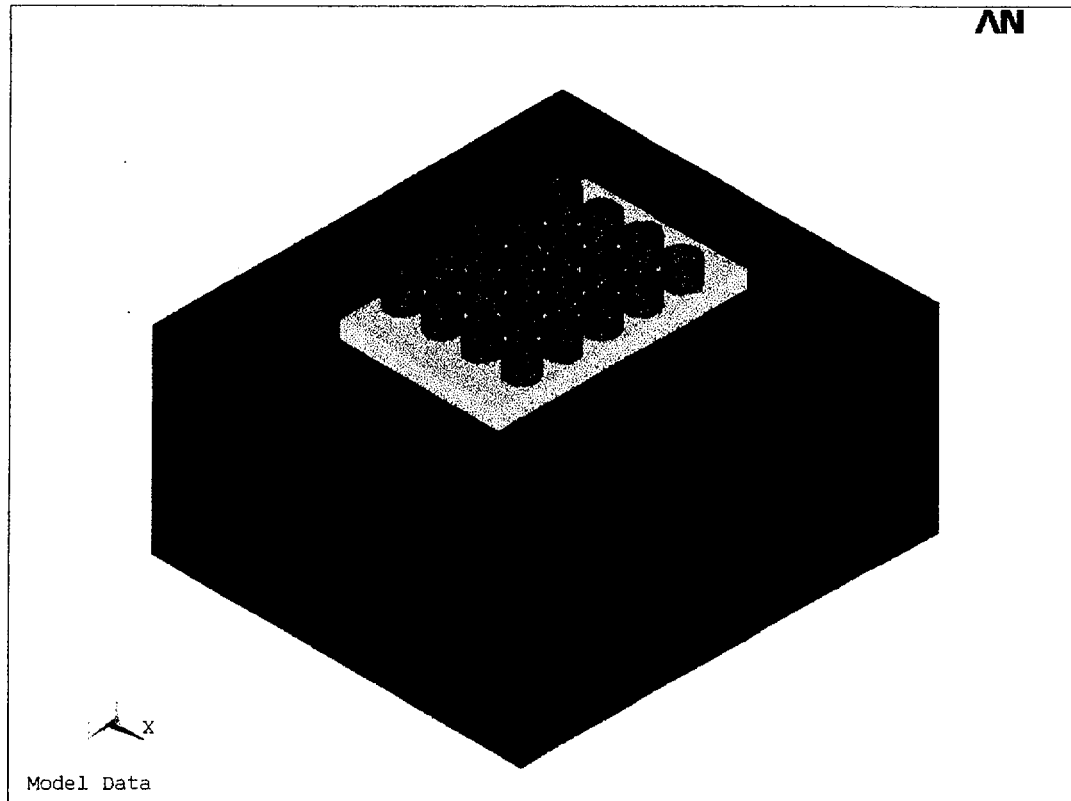
The static analysis model is a solid finite element model. This model is non-linear due to the contact surface between the rock and the concrete pad. Except for the treatment of the interface surface between the pad and the rock, the model is constructed entirely of three dimensional solid elements. At the interface surface, contact elements transmit compression loads only, no tensile loads are transmitted through this interface. Also, at the interface, shear loads are transmitted from the pad into the rock through constraint equations. This shear interface simulates a contact surface that extends over the entire area of the pad. Since the model is constructed using solid elements, there are three translation degrees of freedom at each node. The rotations at the nodes are not included in the solution. The models are constructed in a Cartesian coordinate system with X pointing West, Y pointing vertically up and Z pointing North.

The geometry of the pad, casks and rock elements is shown in Figure 2, below.



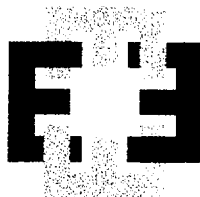
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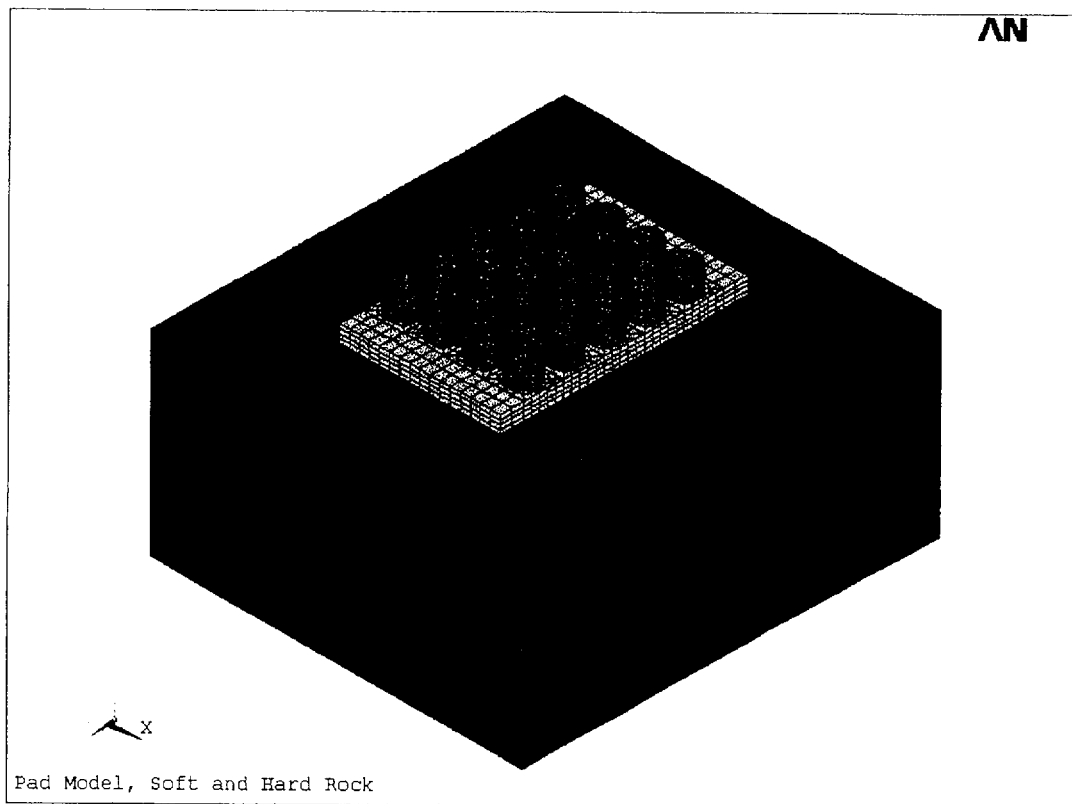
**Figure 2 - Isometric of casks, pad and rock**

The completed model with the finite element mesh is shown in Figure 3 below. The "extra strip" of elements immediately around the pad is an analysis surface for the contact (compression only) elements. The various parts of the model are presented and described below.



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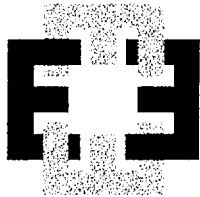
**Figure 3 – Full Model With Finite Element Mesh**

### **Concrete Pad**

The concrete pad is modeled with Element Type #1. Element Type #1 is the ANSYS SOLID45 8-noded structural solid element. No special features of this element were invoked. Thus, the element uses its full integration scheme, and its extra displacement shapes are included. Hence, the use of four elements through the thickness results in a very accurate model for the pad. In plan, the mesh is designed to accommodate the configuration of the casks. The concrete is designated Material Type 1 and is assumed to be homogenous with a Young's modulus of  $4.0 \times 10^6$  psi ( $57000 \times \text{SQRT}(5000)$ ). (The analysis results confirm that this is a reasonable assumption, since no cracking due to the application of the seismic loads is expected to occur.) A Poisson's ratio of 0.15 is used for this material. This material has a density of  $2.2465 \times 10^{-4} \text{ lb}_m/\text{in}^3$  or  $150 \text{ lb}_f/\text{ft}^3$ . This is the only element type in the model to have a density assigned to it. This will be further discussed below.

The concrete pad's overall dimensions are 105 feet in the Z-direction, 68 feet in the X-direction, and 7.5 feet thick. The cask center to center spacing is 17 feet in both directions. The pad mesh is designed to mate with the bases of the casks. Those dimensions are given in the Cask section below. The following Figures 4, 5 and 6 show the pad surface and a close up of the mesh at one cask location. The completed model with the material numbers identified for the various materials is shown in Figures 11 and 12.





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REVIEWER	<u>K. L. Whitmore</u>	APPROVED	<u>R. F. Evers</u>		
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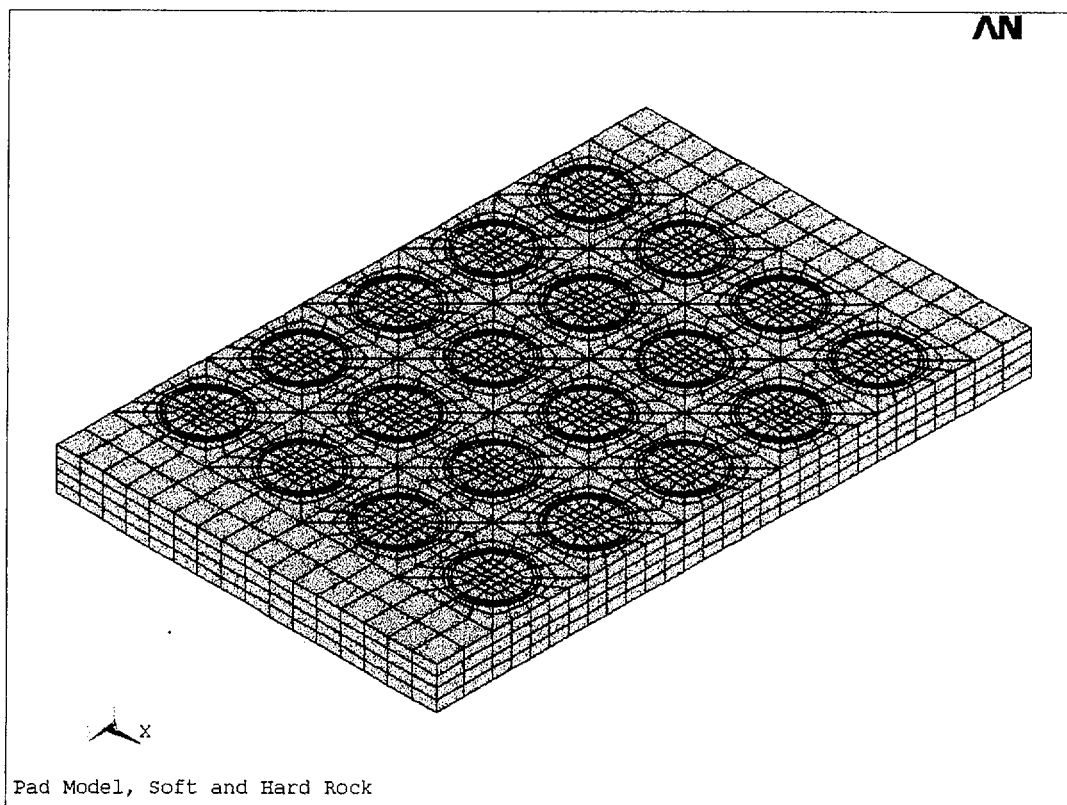
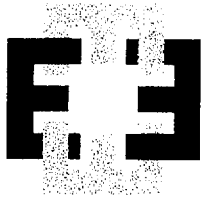


Figure 4 – Isometric view of the Concrete Pad



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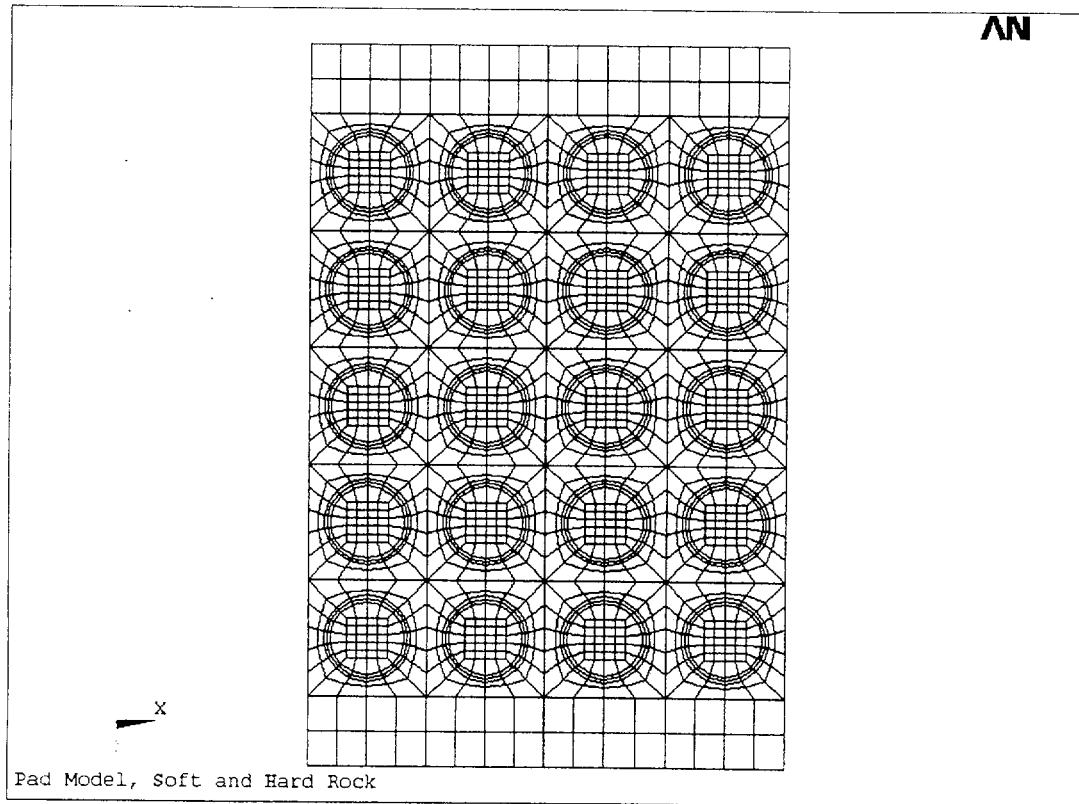


Figure 5 – Top view of the Concrete Pad

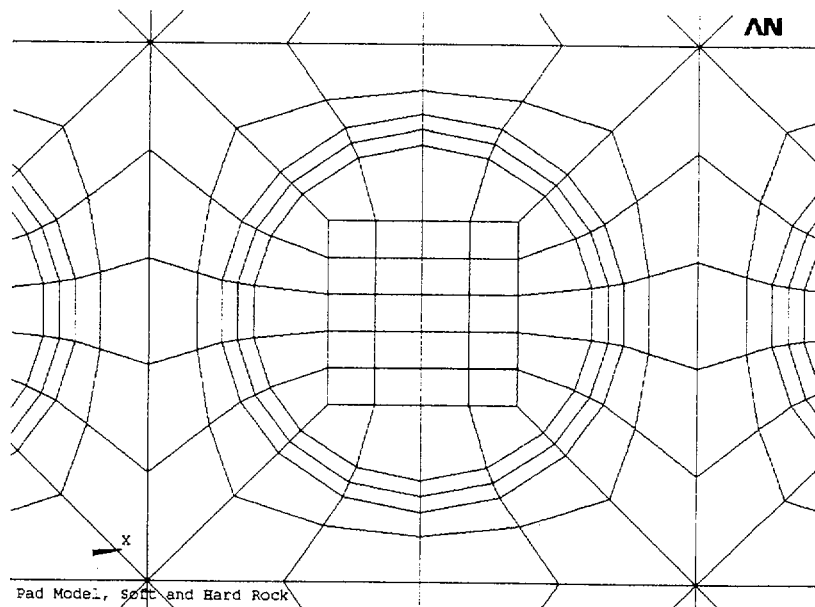
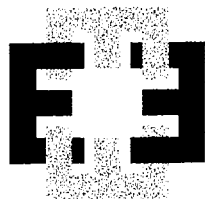


Figure 6 – Close up of the Concrete Pad at one cask location



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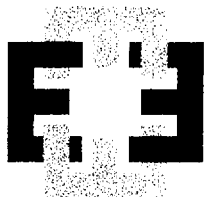
## Rock

The rock is modeled with Element Type #2. Element Type #2 is also the ANSYS SOLID45 8-noded structural solid element. As with the use of this element for the pad, no special features of this element were invoked for the rock. The rock is designated Material Type 2 and is assumed to be homogeneous.

The rock data has evolved over the course of the analysis due to the fact that rock testing and data reduction were in process while the initial analysis and design were also in process. There are two types of rock beneath the footprint of the seven pads, altered sandstone and dolomite. The altered sandstone is referred to herein as "soft rock" and the dolomite is referred to as "hard rock". The final rock properties are all documented in two PG&E calculations, References 11 and 12. These calculations document the results of testing performed on the rock using field data (Ref. 11) and lab data (Ref. 12). Three full sets of analyses were performed and are documented here. The first two are for the values concluded to be for the range of design values, the third was for an assessment for very hard rock, since one data point indicated that this was a possibility at one time. However, the final data reduction did not conclude that there was enough of this very hard rock to perform design basis analyses. A summary of the final soil properties for design is provided in Reference 12. The Poisson's ratios used in the analyses are closer to the higher values from the field data than the lab data. The effects of the lower Poisson's ratios from the lab data are subsequently discussed and evaluated in this calculation.

### **Full Set of Rock Properties Specified and Properties Used for Analysis**

Rock	Young's modulus	Poisson's ratio
Altered Sandstone		
Soft – field data	$0.2 \times 10^6$	0.31
Soft – lab data	$0.21 \times 10^6$	0.23
Used in Analysis	$0.2 \times 10^6$	0.35
Dolomite		
Hard – field data	$2.0 \times 10^6$	0.37
Hard – lab data	1.3 to $1.5 \times 10^6$	0.22
Used in Analysis	$2.0 \times 10^6$	0.35
Dolomite		
Very Hard - lab data	$4.9 \times 10^6$	0.23
Used in Analysis	$4.9 \times 10^6$	0.24



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The rock portion of the model is wide and thick to insure that the rock extends a sufficient distance from the pad so that the boundary conditions of the rock do not affect the stiffness of the rock beneath the pad. It is 158 feet in the X direction, 175 feet in the Z, and is 85 feet thick, see Figure 7 below. The pad is located in the center of the rock surface. The boundary conditions for the rock model are that all three degrees of freedom are fixed on the sides and on the bottom of the rock. These are applied as loads in the ANSYS system and will be discussed again below. The completed model with the material numbers identified for the various materials is shown in Figures 11 and 12.

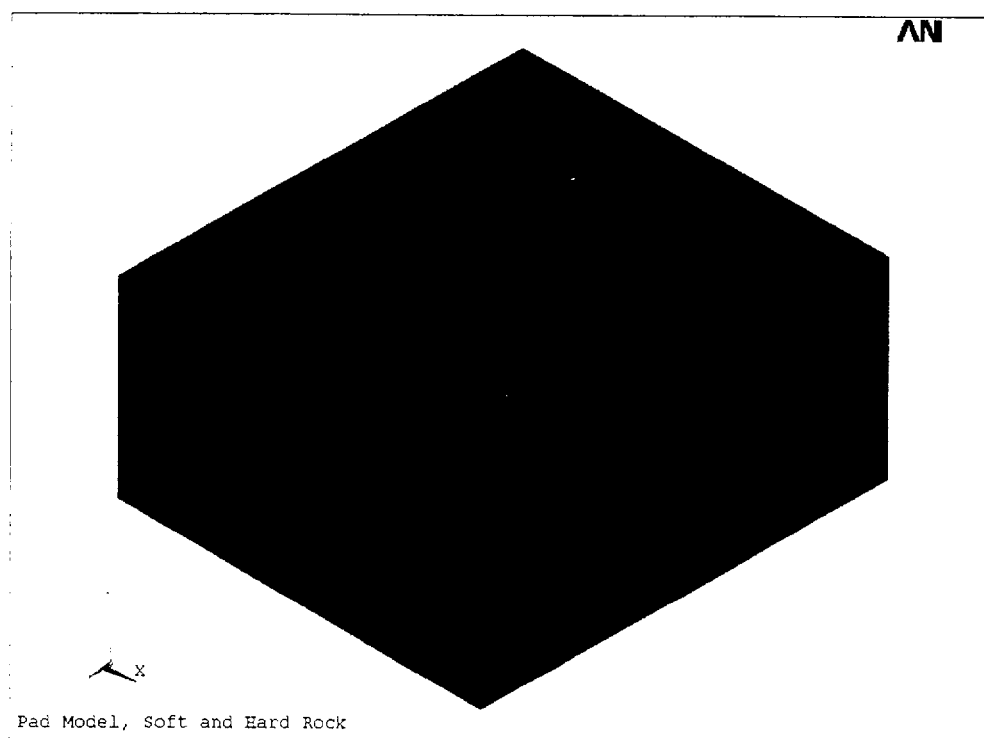
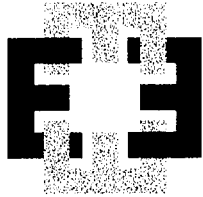


Figure 7 – Isometric view of the Rock

### Casks

The casks are modeled with Element Type #4. Element Type #4 is the ANSYS SOLID45 8-noded structural solid element. Again, as with the use of this element for the pad, no special features of this element were invoked. The casks are modeled up to a plane 118.5 inches above the pad (Reference 4, Table 1). This is the location of the Center of Gravity of the casks and is, therefore, where the loads are applied. This is further discussed in detail below.

The casks are attached to the concrete pad to transmit load directly into the pad without complex interfaces. The only function of the casks in the model is to deliver the loads and moments to the pad at the appropriate locations and with the appropriate distribution, as least with respect to delivering the load over the appropriate surface area. The mean diameter of the cask wall in the model is 139 inches,



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which is the diameter of the hold down stud circle (139.5 inches). The cask wall thickness in the model is 12 inches.

The casks have a fundamental frequency of 16 Hz when analyzed with the embedment structure. Therefore, given the geometry of the modeled casks and a total mass of 360 kips (Reference 4, Table 1 (270+90)) located at 118.5 inches from the pad surface, a Young's modulus of 409000 psi was computed to provide casks with fundamental frequencies of 16 Hz. See Appendix MD-2 for the details. A Poisson's Ratio of 0.30 is used for this element type, which is designated Material Type #4.

Twenty casks are positioned on the pad as shown in the following Figure 8. The subsequent Figures 9 and 10 show a view looking down on a cask, alone, and then with the pad beneath it. The completed model with the material numbers identified for the various materials is shown in Figures 11 and 12.

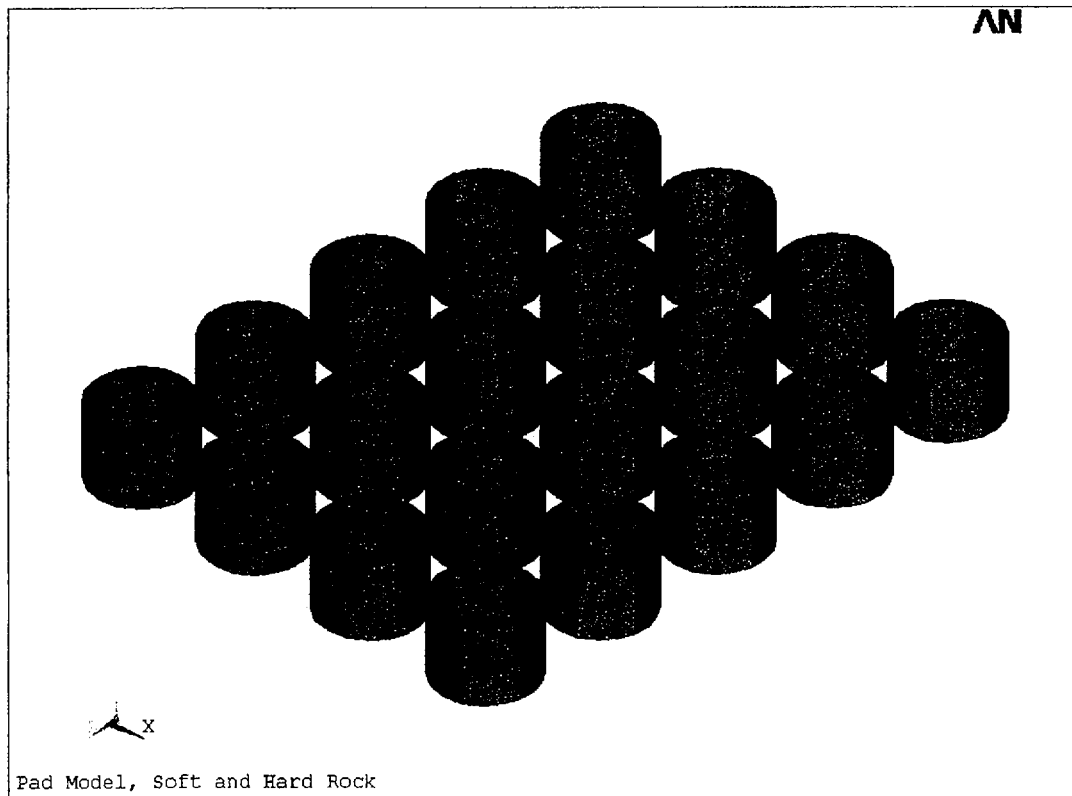
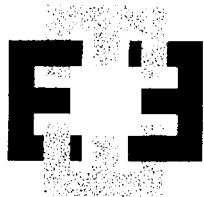


Figure 8 – Isometric view of the Casks (modeled to CG of actual cask)



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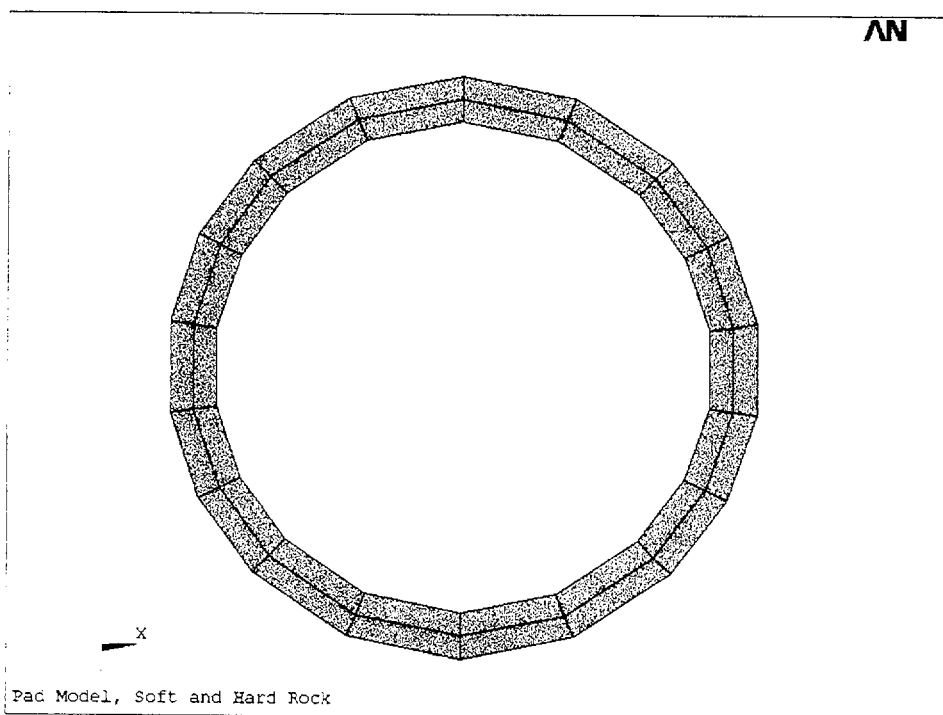


Figure 9 – Top view of one Cask model showing two elements through the thickness

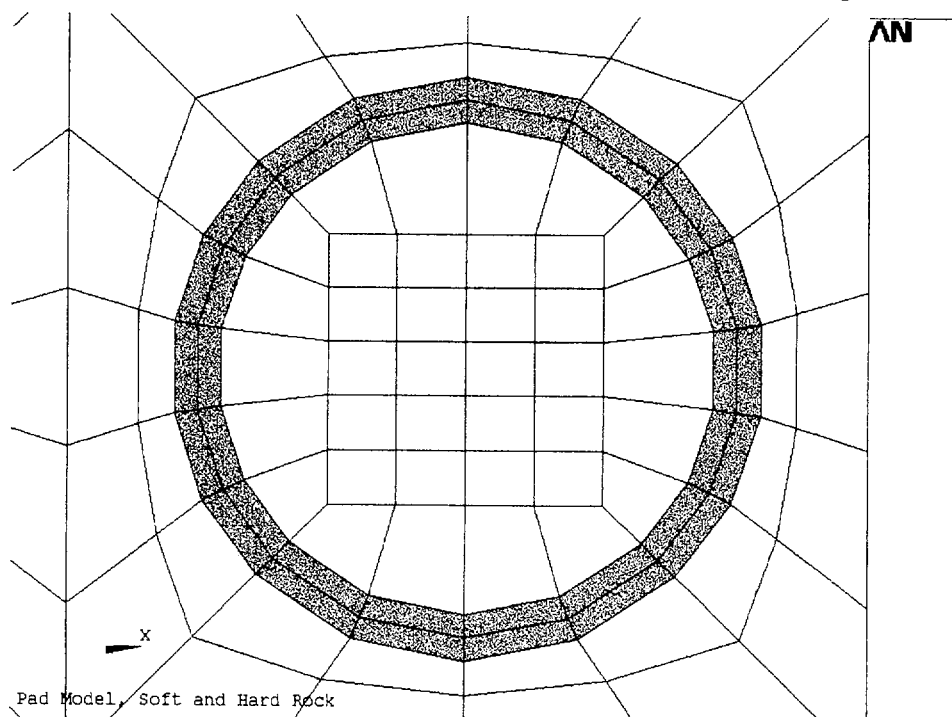
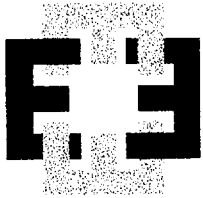


Figure 10 – Top view of one Cask with the concrete pad beneath it

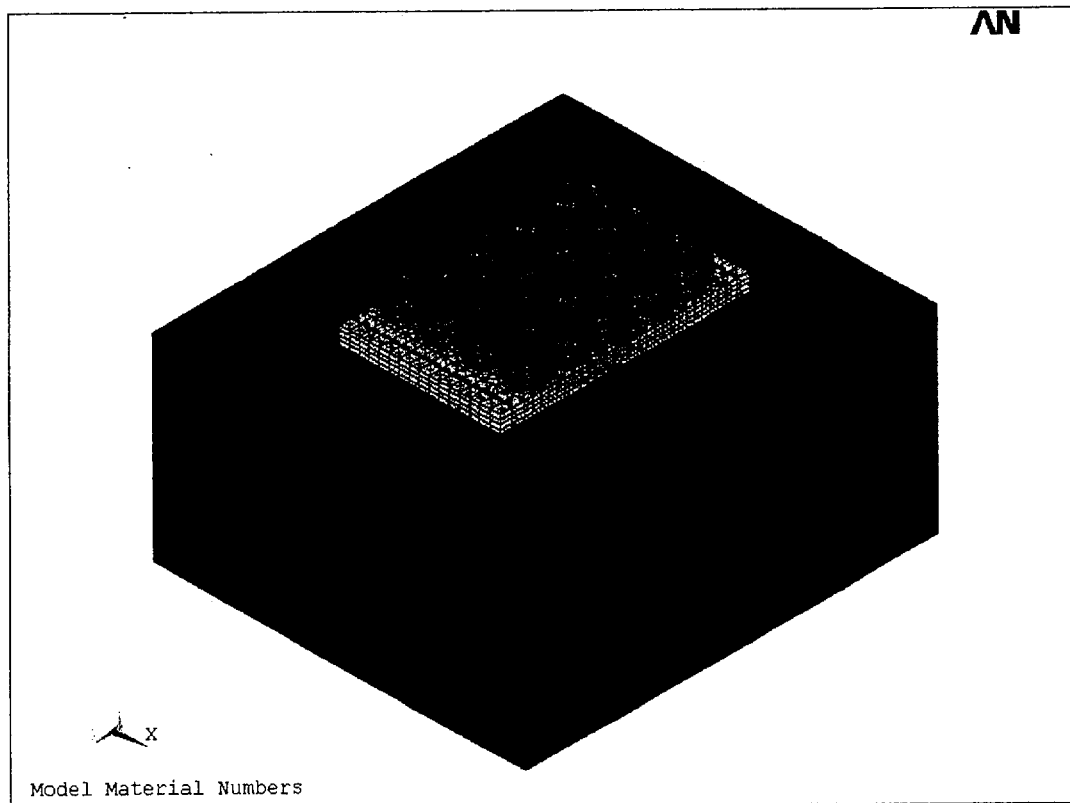


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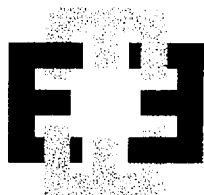
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### Material Numbers

The Figures 11 and 12 below show the completed model with the element material numbers.



**Figure 11 - Full Model with Material Numbers**



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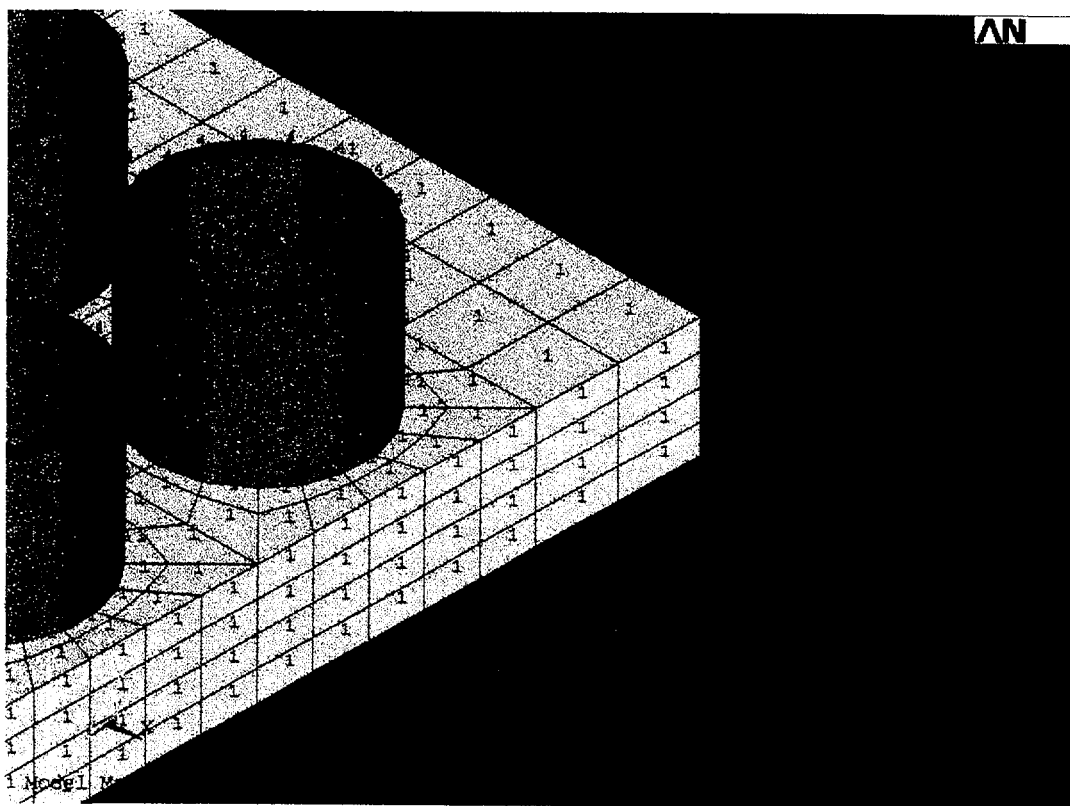


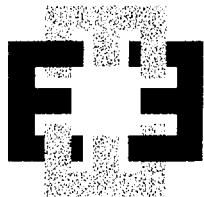
Figure 12 - Close-up of Model with Material Numbers

### Contact Elements

The contact elements are generated by the ANSYS "Contact Wizard" using 3-D surface to surface contact elements. The ANSYS software requires that the contact elements be specified between two surfaces, a "target" surface and a "contact" surface, which are defined as two different element types. The rock surface is designated the "contact" surface, Element Type #5, CONTA174, and the concrete surface is designated the "target" surface, Element Type #6, TARGE170. These elements transmit compression loads from one surface to the other. No tensile forces are transmitted through this interface. These elements are, therefore, non-linear elements.

These elements are actually surfaces that overlay the structural elements and they can be thought of as permitting the interfacing characteristics desired, i.e., permitting compressive forces between the surfaces when penetration is attempted and permitting separation between the surfaces with no forces present when gaps are present. The alignment of the meshes of the two surfaces such that the nodes are coincident is not necessary and not recommended. ANSYS handles all the necessary geometric details to create the compression only elements. The default parameters are used which have been shown to provide the best compromise between accuracy and solution convergence times. The element stiffnesses





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and convergence parameters are actually computed from the geometry and material properties of the adjoining elements. The "target" surface is recommended to be the surface with the harder material as well as the one with the finer mesh of elements, which is the pad in this model. The softer material as well as the one with the coarse mesh of elements is the "contact" surface, which is the rock in this model. The "target" surface is shown below, Figure 13, followed by a plot of the "contact" surface, Figure 14. This contact surface is also shown as the "extra strip" surrounding the pad in Figure 3, above.

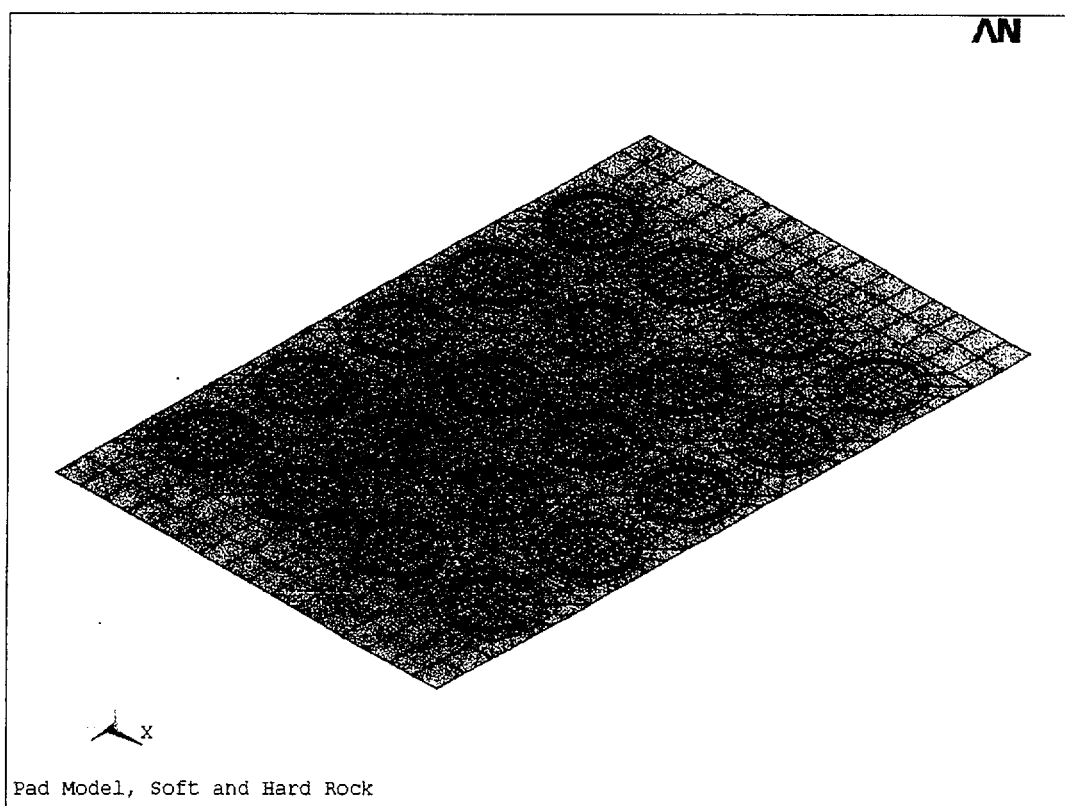
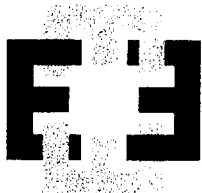


Figure 13 – Target surface located at the bottom of the Pad



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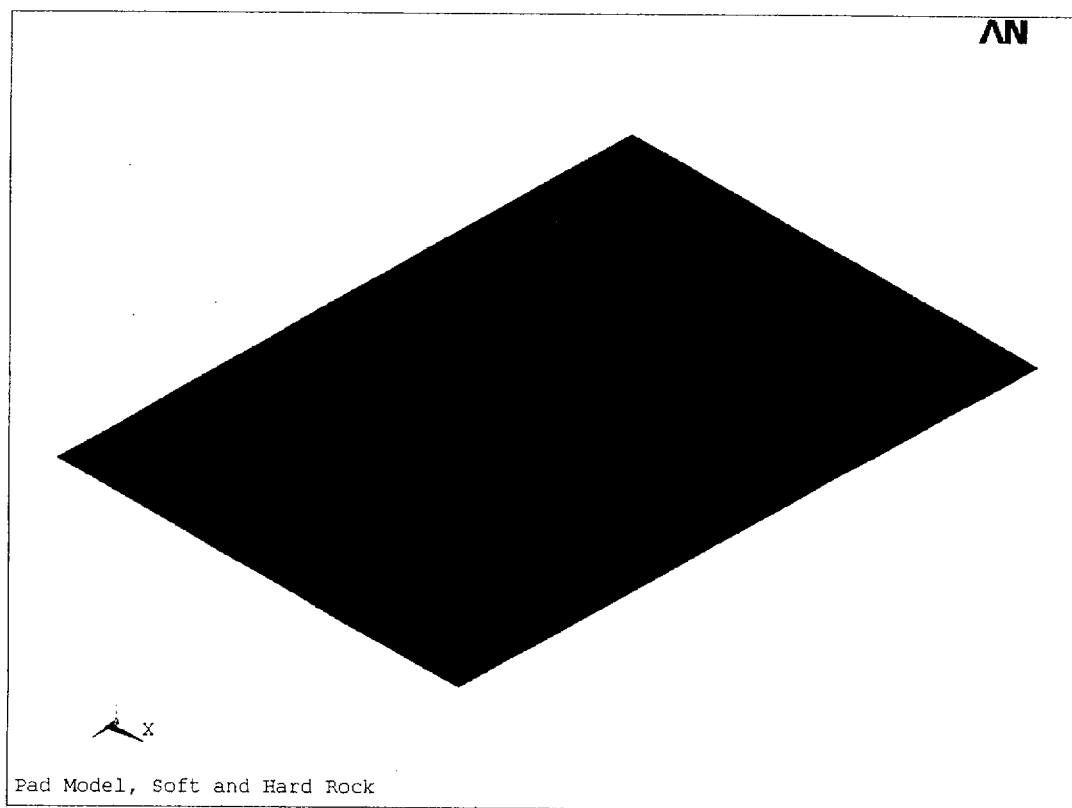
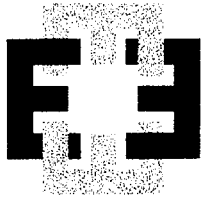


Figure 14 – Contact surface located on the surface of the Rock

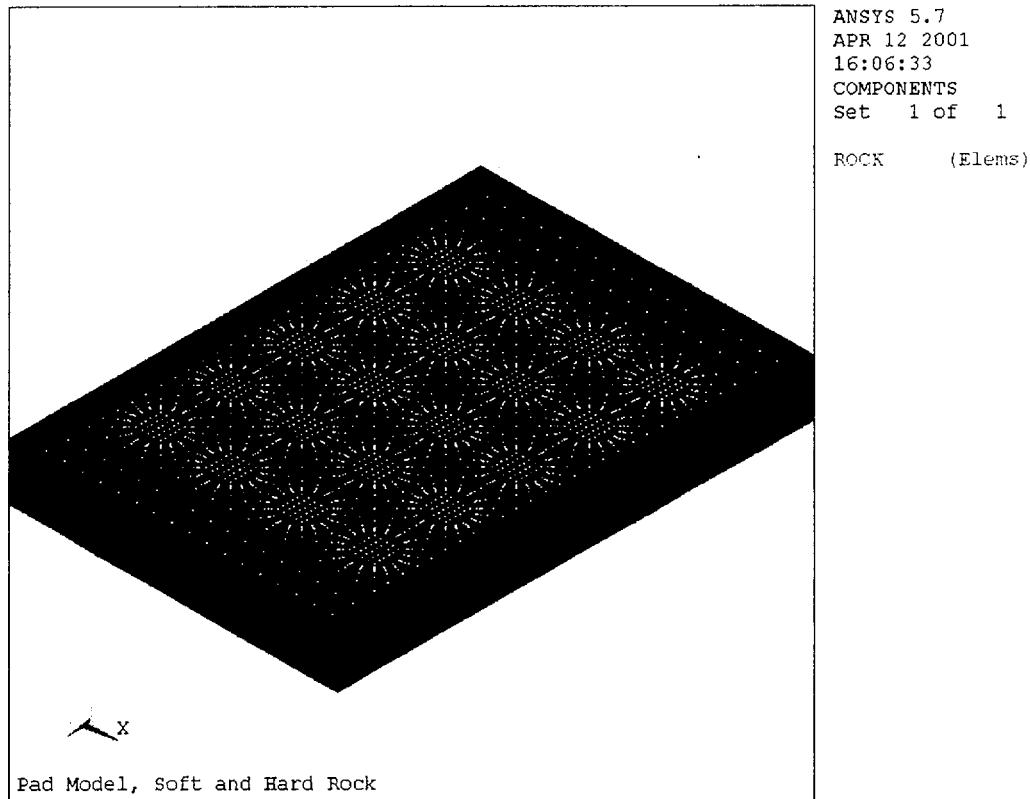
### Constraint Equations

The pad is also tied to the rock in the X and Z directions at the pad rock interface using constraint equations. In this case, the ANSYS constraint equation generator is used. This generator allows a selected set of nodes to be tied to another selected set of nodes through rigid body constraint equations. The first set of nodes is the set at the bottom of the pad, which is called "BASE" in the following Figure 15. The second set is the set associated with elements in the rock mass, called "ROCK" in the same figure. ANSYS automatically writes the constraint equations based upon the locations of the nodes associated with the elements, to those of the nodes at the bottom of the pad. These equations effectively constrain the pad to the rock surface in local areas continuously across the surface of the pad. Hence, a "rigid body" type of constraint across the entire surface is not formed. Since this portion of the model is first order linear, pad lift off does not affect shear transfer between the pad and the rock in the analysis.



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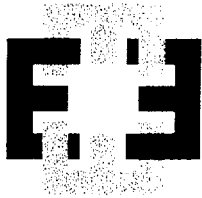
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**Figure 15 – Constraint Equations**  
**Showing the nodes at the bottom of the Pad superimposed**  
**on the related elements of the Rock**

### **Boundary Conditions**

The only boundary conditions in the model are on the rock mass. The nodes of the rock elements are constrained in the all three translation directions at the bottom and on the four sides of the rock for all load steps. Rotation degrees of freedom do not have to be constrained because rotation degrees of freedom are not in the solution set of displacements for this model. The bottom and sides of the rock mass are far enough away from the pad that any variations of boundary constraints on the boundary surfaces will not significantly affect the stiffness of the rock beneath the pad. And will not, therefore, affect the response of the pad to the applied loads. Details of a boundary condition study are presented in Appendix MD-3 and its associated Appendices that provide the justification for the boundary conditions chosen. Figure 16 shows the boundary conditions applied to the nodes on the sides and bottom of the rock mass. The following Figures 17 and 18 provide more detail.



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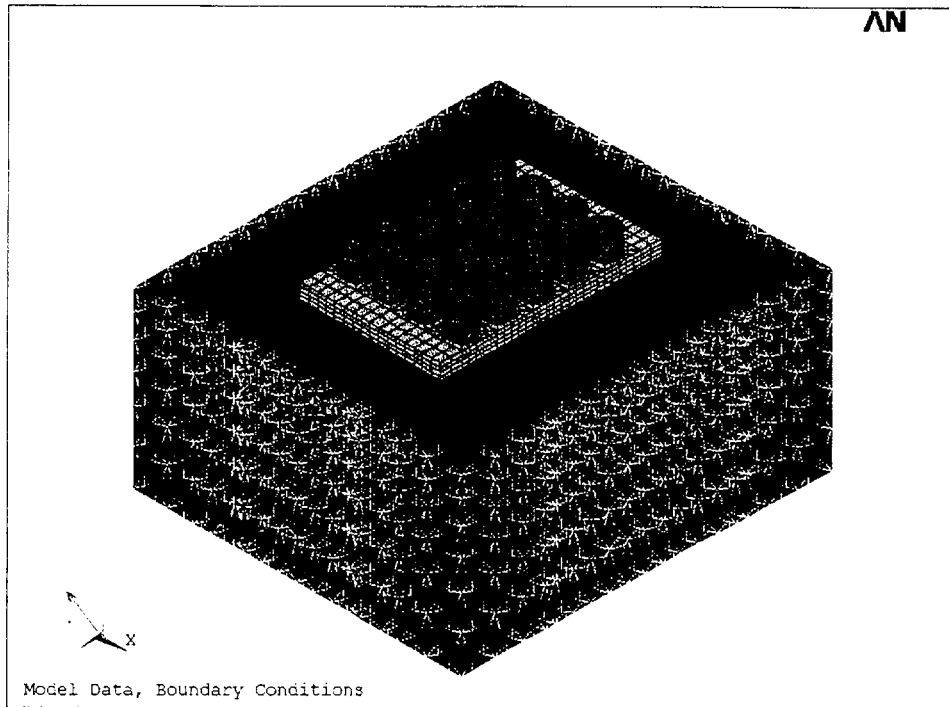


Figure 16 - Isometric of Boundary Conditions on the Rock Mass

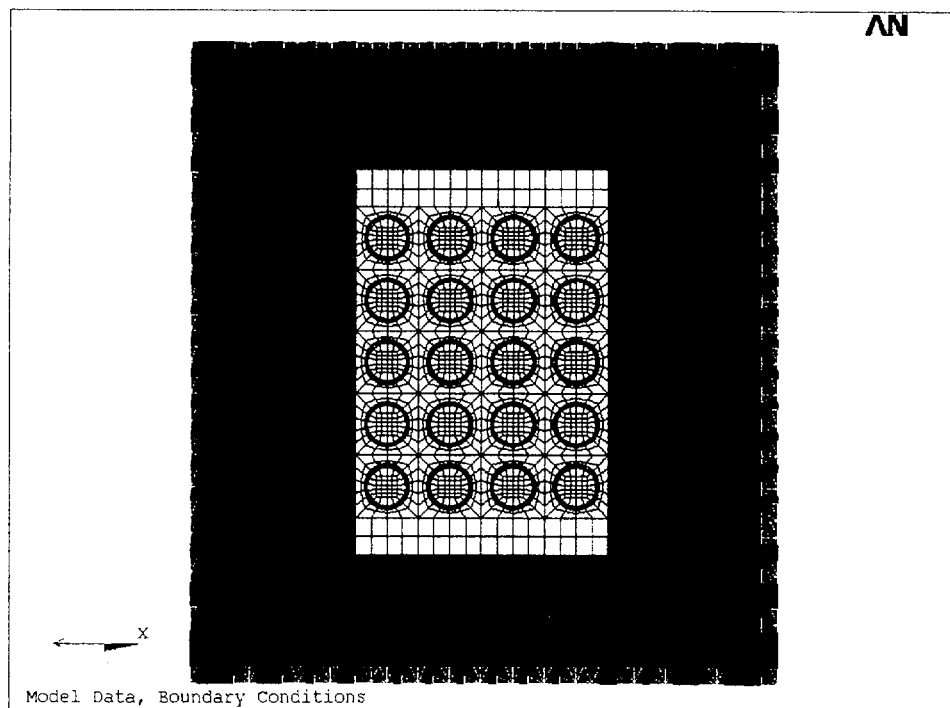
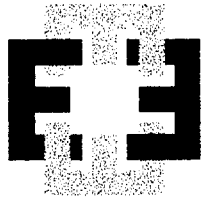


Figure 17 - Boundary Conditions on the Rock Mass Looking Down



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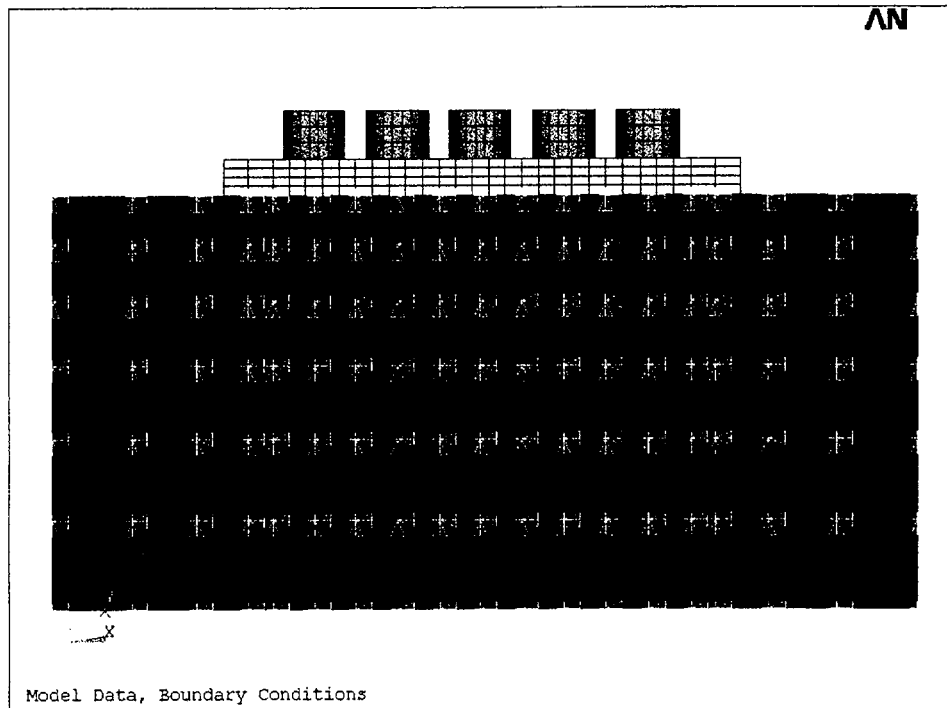
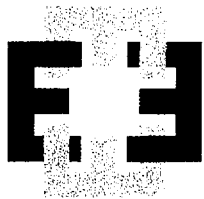


Figure 18 - Boundary Conditions on the Rock Mass Looking from the Side

### Gravity and Seismic Loads

The “soft”, “hard” and “very hard” rock models are loaded using the same load steps. Holtec supplied four sets of loads (Reference 4). The load table that Holtec provided is replicated in Table 1, column numbers are added. These loads were examined and two sets were selected for rigorous analysis. These sets were judged to be the controlling sets of loads and are the results from cask analyses for the Hosgri Earthquake (HE Column 1), and Long Term Seismic Program (LTSP Column 2). This judgement is based on an examination of those load components that are expected to produce the highest potential to uplift the pad. Therefore, the combination of net shear with minimum interface compression was used for comparison. The HE (1) values are 515.0 and 127.6 kips, and the LTSP (2) values are 440.0 and 105.8 kips. The judgement could not be made that either of these would control, so both were selected for analysis. Subsequent to these analyses, the LTSP (2) net shear was increased by 5% from the 440 kips to 462 kips. This increase does not alter any of the conclusions presented here. Supporting analyses for the adjusted LTSP loads are provided in Appendix LT-1.

The HE (3) values are 428.0 and 130.6 kips. The judgement here is that the HE (1) combination will control over the HE (3), noting that the slight increase of 130.6 Vs 127.6 does not offset the lessor shear value of 428.0 Vs. 515.0 kips. The same argument applies to the LTSP (2) Vs. LTSP (4) though two cases of LTSP (4) were run to validate the judgement. The highest cask down load is HE (3), this case



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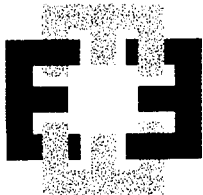
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was run to examine the potential for high moments local to a cask, particularly for the soft rock model. Finally, some cases were examined that maximized the vertical component rather than the shear, simply to insure that nothing was overlooked.

More detail regarding the explicit load vectors and directions is provided below, however the general arrangement of the load cases is as follows:

- Gravity is load case 1
- HE (1) with shear maximized is examined in load cases 2 to 6
- HE (1) with vertical up component maximized is examined in load cases 7 and 8
- HE (3) with vertical down component maximized is examined in load cases 9 and 10
- LTSP (2) with shear maximized is examined in load cases 11 to 15
- LTSP (2) with vertical up component maximized is examined in load cases 16 and 17
- LTSP (4) with vertical up component maximized is examined in load cases 18 and 19

The loads are applied at the tops of the modeled casks, 118.5 inches from the pad, which is at the center of gravity of the actual casks. This method of load application produces the same moments and shears at the bases of the casks as shown in the Holtec report (see note \* in the Table). During implementation of the load application, the total set of loads, horizontal and vertical, from all 20 casks is computed and is equally divided among all the nodes in the model at the tops of the modeled casks. These are shown in the following Figure 19. The subsequent Figure 20 shows these nodes for one cask.



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Table 1 – Seismic Loads from Holtec

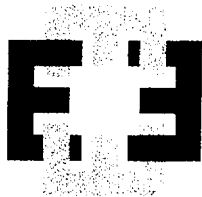
SEISMIC EVENT AT ISFSI****	HE (1)	LTSP (2)	HE** (3)	LTSP** (4)
Maximum/Minimum Interface Compression Force (kips)***	674.2/127.6	684.1/105.8	773.3/130.6	632.0/55.6
Maximum Interface Shear Force Along X-Axis (kips) *	509.4	432.0	379.9	325.8
Maximum Interface Shear Force Along Y-Axis (kips)*	460.5	355.5	426.1	364.6
Maximum Net Interface Shear Force (kips)	515.0	440.0	428.0	390.0
Maximum Interface Moment About X-Axis At Interface (kip-In)	54,564	42,139.2	50,498	43,209
Maximum Interface Moment About Y-Axis At Interface (kip-In)	60,369	51,197.2	45,017	38,603
Maximum Net Interface Moment (kip-In)	61,000	52,000	50,500	46,000
Effective COF at Cask/Embedment Interface	0.180	0.154	0.150	0.132
Maximum Tensile Load in Embedment Anchor Rods (kips)	62.13	48.85	49.73	42.34

\* Base Maximum Shear forces are computed by dividing the appropriate maximum moment by the height to the centroid (118.5 inch). Y-Shear goes with MX, X-Shear goes with MY.

\*\* These simulations have the vertical excitation reversed in direction over the total event time.

\*\*\* Includes dead load = 360,000 lb.

\*\*\*\* The moments and forces reported above act at the lower surface of the embedment plate. The X, Y, Z axes are located at a point on the cask longitudinal centerline (extended to the bottom surface of the embedment plate). The X, Y directions correspond to the East-West and North-South directions, respectively, and the Z-axis is vertically upward.



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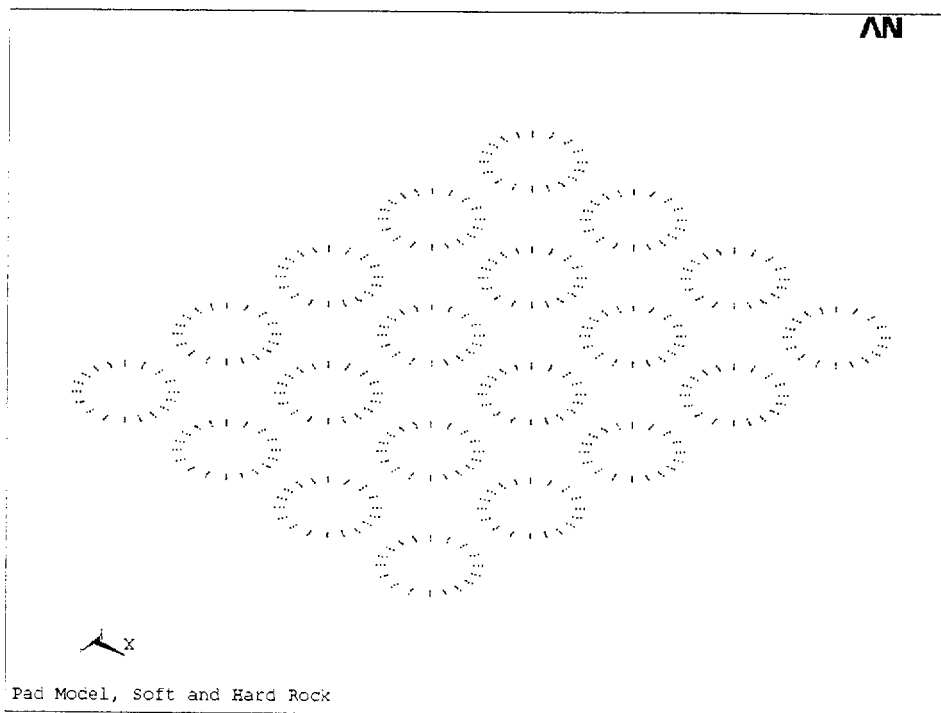


Figure 19 – Nodes at the tops of all casks where the loads are applied

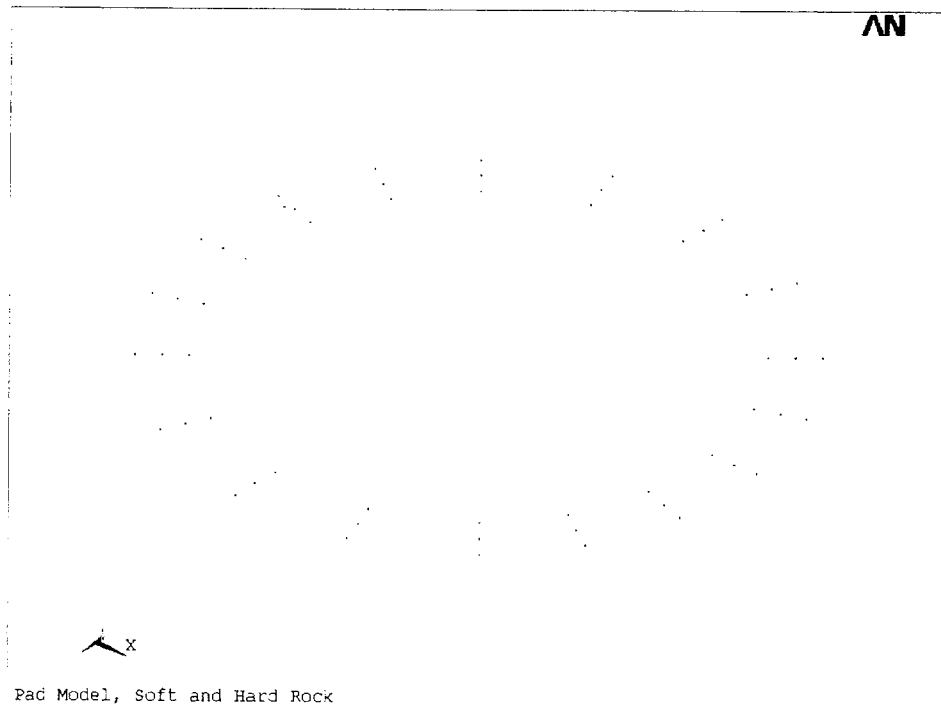
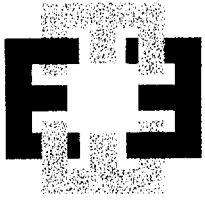


Figure 20 – Close up of the nodes at one cask





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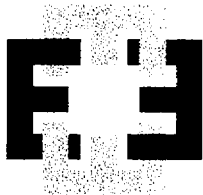
The HE loads are applied with the HE ZPAs applied to the pad, and the LTSP loads are applied with the LTSP ZPAs. See Reference 2, Appendix A for the ZPAs. These are applied as accelerations to the pad mass. This is the reason that the pad is the only portion of the model with mass. The seismic acceleration of the mass of the casks is accounted for in the cask loads supplied by Holtec.

The method of seismic load component combination was followed, as prescribed by PG&E (Reference 2). Holtec computed the net shear, vector sum of components, for each time step in their analyses and reported the maximum values. These are taken to equal 100% of the one and 40% of the other horizontal load component. This load vector was then "aimed" in various directions in an effort to produce the greatest pad uplift and moment in a seismic event that the geometry, mass distribution and loads would permit. The vertical load was taken as 40% of the seismic up load computed from the Holtec data. Since the pad with the casks is a doubly symmetric structure, the loads had to be "aimed" in only one quadrant to provide a complete set of responses. The quadrant chosen is the northwest quadrant. Therefore, the vector is aimed in the following directions: North, North 32.93 degrees West (actually aimed at the opposite corner of the pad), North 45 degrees West, North 57.07 degrees West (symmetric with the 45 degree line), and West. The vector sum of the 100% and 40% ZPAs was also computed, and "aimed" in the same direction as the cask load, along with 40% of the vertical ZPA in the up direction. These cases were analyzed for the HE (1) and LTSP (2) loads.

In addition, the 40-100-40 load components were analyzed for the HE(1) and LTSP(2) in the North and West directions only, along with HE(3) maximum downward load and LTSP(4) maximum upward load applied in the North and West directions. The pad ZPAs were phased and aimed with the cask loads for these cases also.

The applied loads for both the soft rock, hard rock, and very hard rock models are as follows (the details of the load calculations and the ANSYS input files are provided in Appendix AL-1):

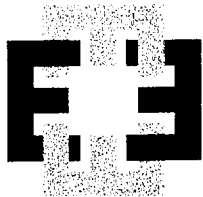
- 1 Gravity, pad plus 20 casks. This is 360 kips per cask down plus 1G applied for the pad weight.
- 2 Gravity plus the Hosgri Earthquake loads from the Holtec Report Column 1, HE(1), plus the Hosgri ZPAs applied to the pad. The cask loads are 515 kips horizontal and 267.04 kips down. The horizontal pad acceleration is 0.808G and the vertical acceleration is 0.2G up. The net vertical acceleration applied to the model is, therefore  $1.0G - 0.2G = 0.8G$  down. These are the 100-40-40 seismic components. All horizontal loads are applied in the North direction.
- 3 Gravity plus HE(1) plus Hosgri ZPAs. Same loads as Load Step 2. All horizontal loads applied at North 32.93° West.
- 4 Gravity plus HE(1) plus Hosgri ZPAs. Same loads as Load Step 2. All horizontal loads applied at North 45° West.



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- 5 Gravity plus HE(1) plus Hosgri ZPAs. Same loads as Load Step 2. All horizontal loads applied at North 57.07° West.
- 6 Gravity plus HE(1) plus Hosgri ZPAs. Same loads as Load Step 2. All horizontal loads are applied in the West direction.
- 7 Gravity plus HE(1) plus Hosgri ZPAs. The cask loads are 206 kips horizontal and 127.6 kips down. The horizontal pad acceleration is 0.424G horizontal and 0.500G up. The net vertical acceleration applied to the model is, therefore  $1.0G - 0.5G = 0.5G$  down. These are the 40-100-40 seismic components. All horizontal loads are applied in the North direction.
- 8 Gravity plus HE(1) plus Hosgri ZPAs. Same loads as Load Step 7. All horizontal loads are applied in the West direction.
- 9 Gravity plus the Hosgri Earthquake loads from the Holtec Report Column 3, HE(3), plus the Hosgri ZPAs applied to the pad. The cask loads are 171.2 kips horizontal and 773.3 kips down. The horizontal pad acceleration is 0.424G horizontal and 0.500G down. The net vertical acceleration applied to the model is, therefore  $1.0G + 0.5G = 1.5G$  down. These are the 40-100-40 seismic components for the maximum down loads for all load cases. All horizontal loads are applied in the North direction.
- 10 Gravity plus HE(3) plus Hosgri ZPAs. Same loads as Load Step 9. All horizontal loads are applied in the West direction.
- 11 Gravity plus the Long Term Seismic Program loads from the Holtec Report Column 2, LTSP(2), plus the LTSP ZPAs applied to the pad. The cask loads are 440 kips horizontal and 258.32 kips down. The horizontal pad acceleration is 0.894G horizontal and 0.280G up. The net vertical acceleration applied to the model is, therefore  $1.00G - 0.28G = 0.72G$  down. These are the 100-40-40 seismic components. All horizontal loads are applied in the North direction.
- 12 Gravity plus LTSP(2) plus LTSP ZPAs. Same loads as Load Step 11. All horizontal loads applied at North 32.93° West.
- 13 Gravity plus LTSP(2) plus LTSP ZPAs. Same loads as Load Step 11. All horizontal loads applied at North 45° West.
- 14 Gravity plus LTSP(2) plus LTSP ZPAs. Same loads as Load Step 11. All horizontal loads applied at North 57.07° West.
- 15 Gravity plus LTSP(2) plus LTSP ZPAs. Same loads as Load Step 11. All horizontal loads are applied in the West direction.



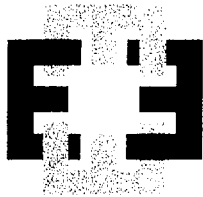
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- 16 Gravity plus LTSP(2) plus LTSP ZPAs. The cask loads are 176 kips horizontal and 105.8 kips down. The horizontal pad acceleration is 0.470G horizontal and 0.700G up. The net vertical acceleration applied to the model is, therefore  $1.0G - 0.7G = 0.3G$  down. These are the 40-100-40 seismic components. All horizontal loads are applied in the North direction.
- 17 Gravity plus LTSP(2) plus LTSP ZPAs. Same loads as Load Step 16. All horizontal loads are applied in the West direction.
- 18 Gravity plus the Long Term Seismic Program loads from the Holtec Report Column 4, LTSP(4), plus the LTSP ZPAs applied to the pad. The cask loads are 156 kips horizontal and 55.6 kips down. The horizontal pad acceleration is 0.470G horizontal and 0.700G up. The net vertical acceleration applied to the model is, therefore  $1.0G - 0.7G = 0.3G$  down. These are the 40-100-40 seismic components. All horizontal loads are applied in the North direction.
- 19 Gravity plus LTSP(4) plus LTSP ZPAs. Same loads as Load Step 18. All horizontal loads are applied in the West direction.

In each load step, these loads are applied to the model all at once, i.e., the gravity plus the seismic horizontal and vertical loads are applied concurrently. The ANSYS program was then instructed to iterate until the solution converged.

These sets of loads are conservative since the reduction in response due to phasing of the acceleration components of the pad to the response of the casks is not considered. Only the phasing of the directional acceleration components of the pad response, and cask response, is considered through the application of the 100-40-40 rule.



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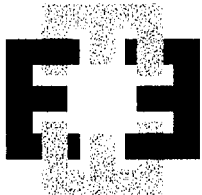
## Analysis Results

### Pad Response – Displacements and Stresses

The analyses were performed on the three models, one for soft, one for hard and one for very hard rock. These analyses produced three separate databases of results.

Prior to evaluation, all load steps were checked for equilibrium. The forces applied on all the casks, and the forces between the pad and the rock, and the rock boundary were computed manually. The ANSYS results databases were then scanned for these same values and the results were compared to each other. In all cases, they agree, see Appendix RL-1.

The analysis results were then scanned using the ANSYS Post Processor. First the data were scanned and sorted for the maximum displacement anywhere on the pad,  $\delta_{Max}$ , see Appendix DN-1 for the details. Then the results were scanned and sorted for the maximum displacements at the centerlines of all 14 casks on the perimeter of the 4 x 5 cask array,  $\delta_{Cask}$ , see Appendix DN-2 for the details. Vertical displacement plots of the pad, for the soft rock model, are provided for all 19 load steps in Appendix DP-1. Finally, the results were scanned and sorted for the max/min stresses in the two, X and Z directions, and for the maximum principal stress,  $\sigma_1_{Max}$  (largest tensile stress), and the minimum principal stress,  $\sigma_3_{Min}$  (largest compressive stress). See Appendix SN-1 for details. The results for the soft rock, hard rock and very hard rock cases are presented in Tables 2, 3, 4 and 5 below. The displacements are in inches, and the stresses in psi.



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Table 2 – MAXIMUM PAD and CASK DISPLACEMENTS

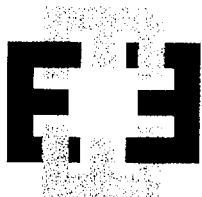
LS	EQ	Direction	Maximum Pad $\delta_{Max}$			Maximum Cask $\delta_{Cask}$		
			Soft	Hard	V Hard	Soft	Hard	V Hard
1		Gravity	-0.011	-0.001	-0.0005	-0.026**	-0.003 <sup>+</sup>	-0.0015 <sup>++</sup>
2	HE(1)	N	0.058	0.027	0.020	0.0005	0.005	0.004
3	HE(1)	N32.93W	0.099	0.045	0.035	0.022	0.015	0.013
4	HE(1)	N45W	0.101	0.046	0.036	0.027	0.018	0.015
5	HE(1)	N57.07W	0.094	0.043	0.033	0.028	0.019	0.016
6	HE(1)	W	0.047	0.032	0.027	0.013	0.014	0.013
7	HE(1)*	N	0.010	0.005	0.003	-0.007	-0.0003	0.00002
8	HE(1)*	W	0.009	0.007	0.006	-0.004	0.002	0.002
9	HE(3)*	N	-0.014	-0.001	-0.0006	-0.045	-0.005	-0.003
10	HE(3)*	W	-0.014	-0.001	-0.0007	-0.044	-0.005	-0.002
11	L(2)	N	0.049	0.022	0.017	-0.002	0.004	0.003
12	L(2)	N32.93W	0.082	0.037	0.028	0.015	0.011	0.009
13	L(2)	N45W	0.083	0.038	0.029	0.019	0.013	0.011
14	L(2)	N57.07W	0.077	0.035	0.026	0.019	0.014	0.011
15	L(2)	W	0.039	0.024	0.021	0.008	0.010	0.009
16	L(2)*	N	0.022	0.010	0.008	-0.0005	0.002	0.001
17	L(2)*	W	0.018	0.010	0.009	0.004	0.004	0.004
18	L(4)*	N	0.025	0.011	0.009	0.003	0.003	0.002
19	L(4)*	W	0.023	0.014	0.012	0.010	0.007	0.007

\* Load components are combined using the 40-100-40 rule. All others combined using 100-40-40 rule.

\*\* Values range from -0.026 to -0.034 (Perimeter casks only)

+ Values range from -0.003 to -0.004 (Perimeter casks only)

++ Values range from -0.0015 to -0.0018 (Perimeter casks only)



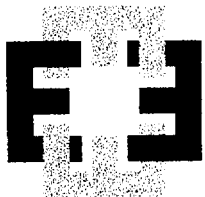
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Table 3 – PAD STRESS RESPONSES – SOFT ROCK

LS	EQ	Direction	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min	$\sigma_1$ Max	$\sigma_3$ Min
1		Gravity	33	-63	23	-55	35	-117
2	HE(1)	N	46	-107	270	-404	341	-642
3	HE(1)	N32.93W	144	-271	235	-410	359	-801
4	HE(1)	N45W	192	-322	209	-379	355	-806
5	HE(1)	N57.07W	234	-359	176	-329	347	-778
6	HE(1)	W	261	-405	62	-135	314	-595
7	HE(1)*	N	20	-44	129	-179	164	-287
8	HE(1)*	W	121	-180	28	-61	148	-265
9	HE(3)*	N	62	-117	83	-206	115	-349
10	HE(3)*	W	83	-248	60	-108	102	-349
11	L(2)	N	44	-94	261	-381	329	-600
12	L(2)	N32.93W	137	-255	227	-383	347	-748
13	L(2)	N45W	183	-302	201	-354	344	-752
14	L(2)	N57.07W	223	-338	167	-307	336	-725
15	L(2)	W	254	-379	57	-123	303	-556
16	L(2)*	N	20	-39	120	-172	151	-269
17	L(2)*	W	117	-170	24	-53	140	-250
18	L(4)*	N	19	-34	112	-162	142	-252
19	L(4)*	W	108	-159	22	-49	130	-241

\* Load components are combined using the 40-100-40 rule. All others combined using 100-40-40 rule.



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Table 4 – PAD STRESS RESPONSES – HARD ROCK

LS	EQ	Direction	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min	$\sigma_1$ Max	$\sigma_3$ Min
1		Gravity	16	-20	9	-19	17	-54
2	HE(1)	N	51	-79	75	-196	164	-230
3	HE(1)	N32.93W	70	-132	71	-168	156	-227
4	HE(1)	N45W	81	-177	63	-137	155	-231
5	HE(1)	N57.07W	89	-210	60	-103	158	-239
6	HE(1)	W	94	-244	52	-77	161	-267
7	HE(1)*	N	20	-29	31	-56	64	-94
8	HE(1)*	W	39	-86	19	-31	63	-105
9	HE(3)*	N	40	-44	37	-78	41	-163
10	HE(3)*	W	62	-71	27	-43	65	-182
11	L(2)	N	43	-69	63	-166	138	-199
12	L(2)	N32.93W	62	-111	60	-147	129	-198
13	L(2)	N45W	71	-151	54	-122	129	-202
14	L(2)	N57.07W	78	-181	51	-93	131	-208
15	L(2)	W	82	-210	41	-68	135	-231
16	L(2)*	N	17	-28	25	-70	55	-82
17	L(2)*	W	33	-87	16	-28	54	-95
18	L(4)*	N	15	-25	23	-66	52	-75
19	L(4)*	W	28	-81	16	-23	51	-87

\* Load components are combined using the 40-100-40 rule. All others combined using 100-40-40 rule.



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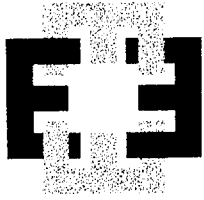
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Table 5 – PAD STRESS RESPONSES – VERY HARD ROCK

LS	EQ	Direction	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min	$\sigma_1$ Max	$\sigma_3$ Min
1		Gravity	17	-17	11	-16	17	-54
2	HE(1)	N	53	-74	80	-184	164	-229
3	HE(1)	N32.93W	70	-124	70	-157	156	-227
4	HE(1)	N45W	81	-167	60	-128	155	-230
5	HE(1)	N57.07W	89	-197	55	-94	158	-238
6	HE(1)	W	93	-230	57	-70	161	-254
7	HE(1)*	N	21	-27	32	-52	64	-94
8	HE(1)*	W	39	-82	21	-29	63	-99
9	HE(3)*	N	41	-38	40	-70	42	-163
10	HE(3)*	W	63	-65	29	-36	66	-182
11	L(2)	N	45	-64	67	-156	138	-199
12	L(2)	N32.93W	61	-104	59	-135	129	-198
13	L(2)	N45W	71	-142	51	-110	129	-201
14	L(2)	N57.07W	78	-170	48	-82	131	-207
15	L(2)	W	82	-197	47	-62	135	-219
16	L(2)*	N	18	-26	26	-66	55	-80
17	L(2)*	W	33	-81	18	-25	54	-90
18	L(4)*	N	16	-23	24	-62	52	-71
19	L(4)*	W	28	-76	19	-21	51	-82

\* Load components are combined using the 40-100-40 rule. All others combined using 100-40-40 rule.





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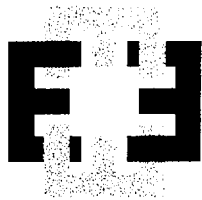
JOB. NO.	<u>PGE-009</u>	SHEET	<u>35</u>	OF	<u>89</u>
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REVIEWER	<u>K. L. Whitmore</u>	APPROVED	<u>R. F. Evers</u>		
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These results clearly show that the dominating load steps are those that result from the analyses for the soft rock model. The maximum pad displacement for any of these load steps is 0.101 inches up (LS 4) and the maximum cask vertical displacement is 0.028 inches up (LS 5). Both of these values are small and are clearly acceptable. The maximum values of stress in the X direction are 261 psi (LS 6) and -405 psi (also LS 6). In the Z direction they are 270 psi (LS 2) and -410 psi (LS 3). The maximum principal stress is 359 psi (LS 3) and the minimum value is -806 psi (LS 4).

A reasonable value for tensile stress that causes concrete to crack is  $7.5 \text{ SQRT}(f'_c) = 530 \text{ psi}$ , (Reference 9, Eq. 9-9). Therefore, as discussed above, since the largest tensile stress is 359 psi, concrete cracking due to the application of seismic loads is not expected to occur. Further, the maximum compressive stress of 806 psi is clearly acceptable since  $f'_c$  is 5000 psi.

A broader view of this data shows that the load cases where the components are combined using the 100-40-40 rule control the bending stress design of the pad and that the Hosgri (1) produces slightly more demanding pad stresses than the Long Term Seismic Program (2). Thus, these analyses also serve as a set of screening calculations, whereby, except for the applied pressures to the cut rock, see Table 12, further consideration for pad design need only be given to the Hosgri (1) seismic event analyzed using the soft rock model. A full set of displacement plots of the pad for all Load Steps for the soft rock model is provided on Appendix DP-1. A full set of plots, displacements and stresses, for Load Step 6 for the soft rock model is provided below, Figures 21 to 26.

An examination of these plots indicates that at least some of the maximum values are a result of the modeling. The high X direction stresses at the edge of the pad (405 psi), Figure 24, are a result of the fact that the rock constraint provided through the constraint equations ends abruptly. And, the Z direction stresses, Figure 25, at the same location, are a result of Poisson effects.



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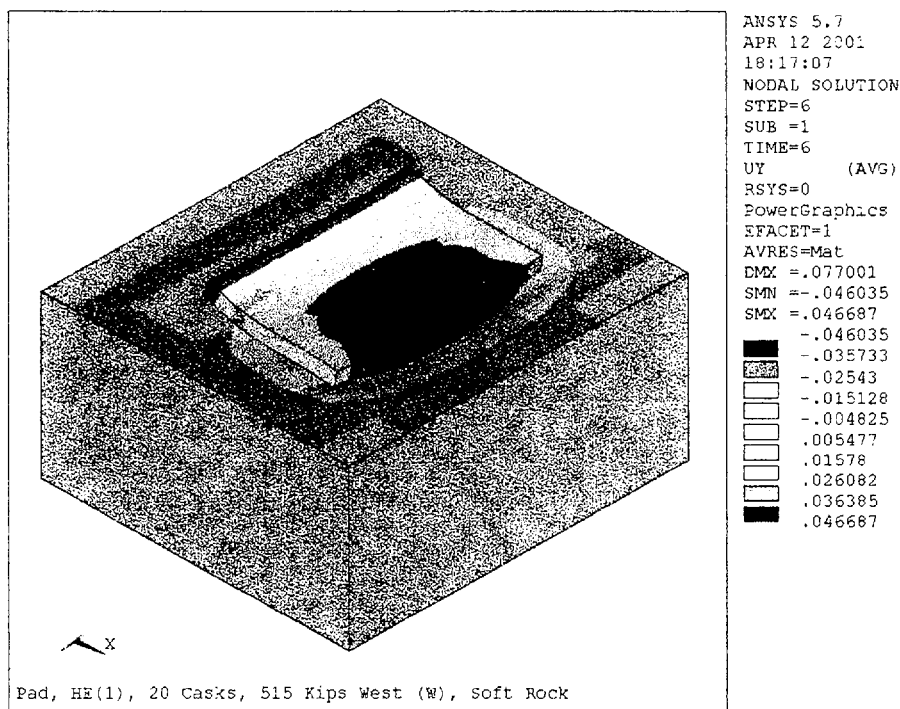


Figure 21 – Pad and rock vertical displacements for Load Step 6 – Loads are applied to the West

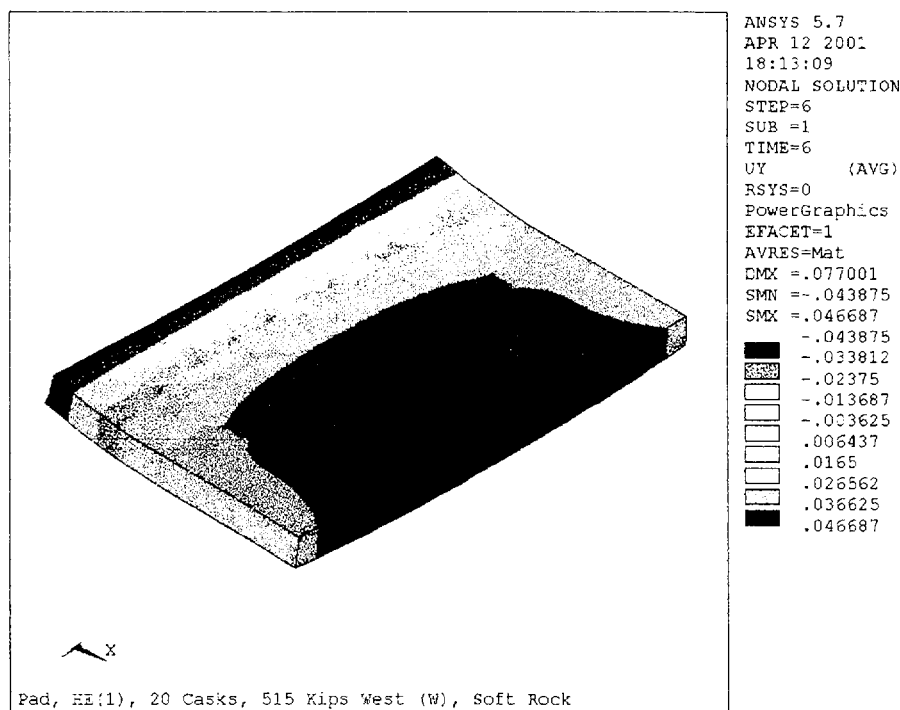
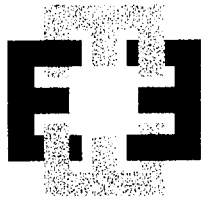


Figure 22 – Pad vertical displacements for Load Step 6 – Loads are applied to the West



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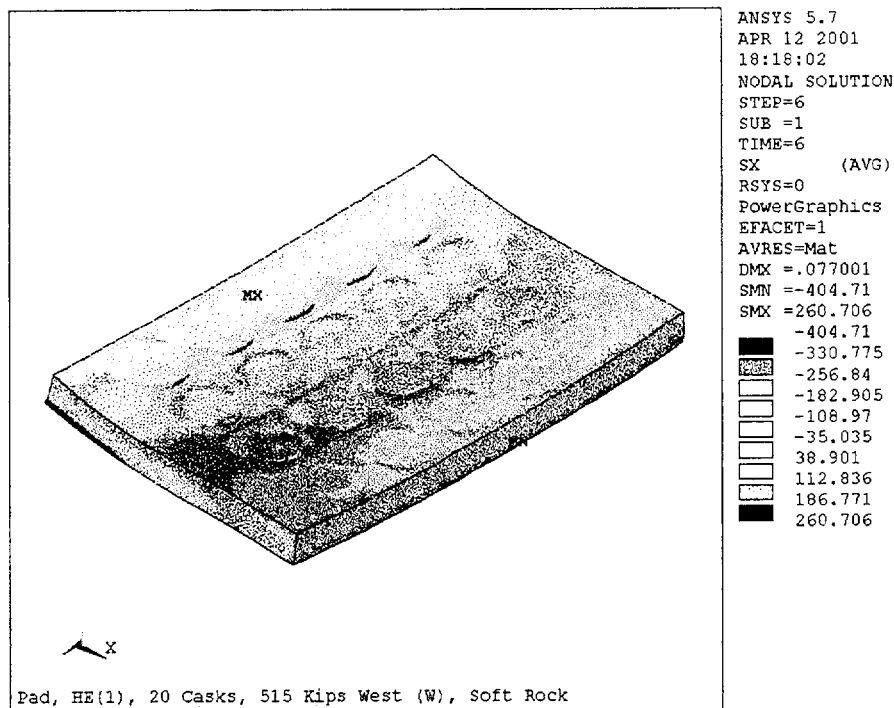


Figure 23 – X direction stresses looking from the top for Load Step 6

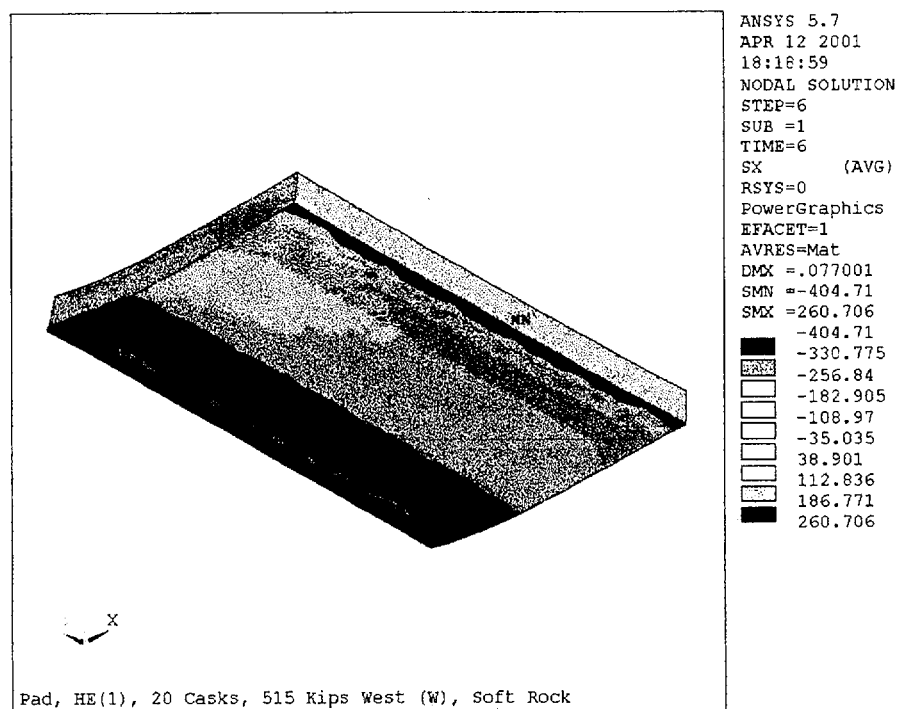
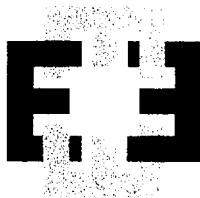


Figure 24 – X direction stresses looking from the bottom for Load Step 6



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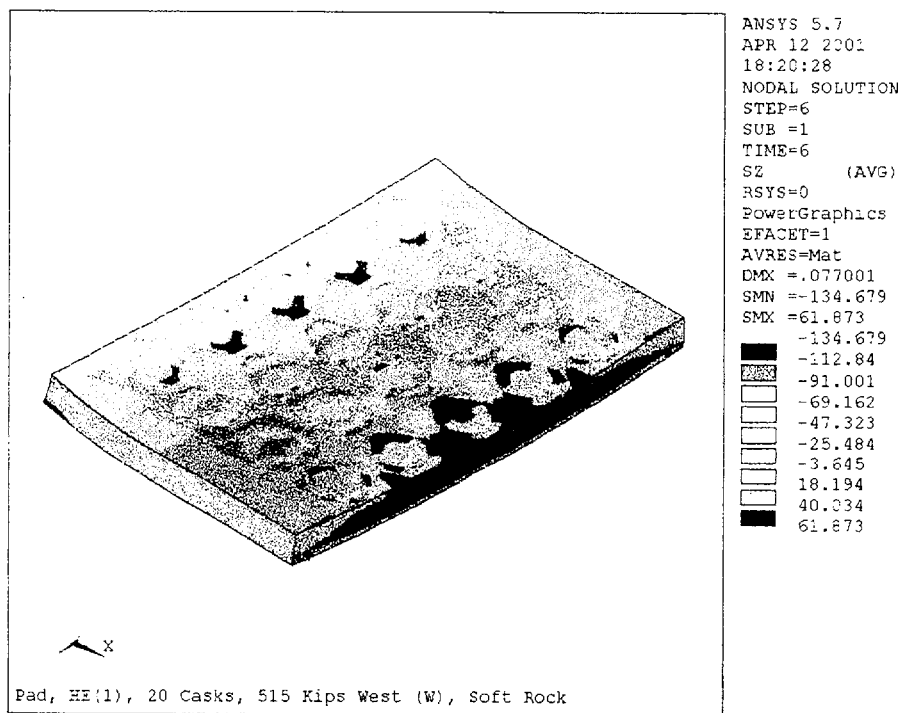


Figure 25 – Z direction stresses looking from the top for Load Step 6

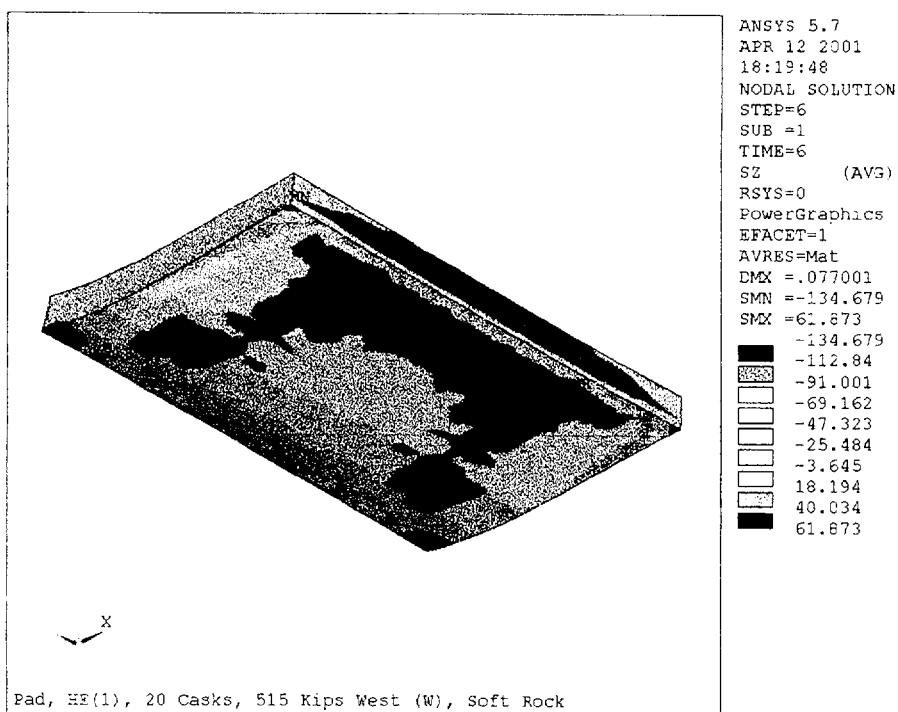
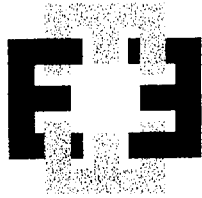


Figure 26 – Z direction stresses looking from the bottom for Load Step 6



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### Pad Response – Internal Forces

In order to evaluate the concrete sections and design the reinforcement, the pad internal forces and moments are required. These, of course, are the stress resultants, on a user specified section and the moments are computed about a user specified point. Since the model of the pad is constructed from "brick" elements, these quantities are not readily available from the ANSYS database. These values can, however, be computed from the nodal force data. In these analyses, the data for the pad are processed for a series of "strips" whereby the pad is sectioned into strips, and then each strip is further sectioned to reveal cross sections, or selected surfaces, of the pad. The center of the cross section is specified for moment calculation and the internal forces are computed for the selected surface.

An examination of the displacements and stresses indicates that the displaced shape and resultant stresses are generally consistent with a single curvature response of the pad, i.e., the pad lifts off the rock gradually and then conforms to the surface of the rock. See Figures 21 to 26, and Appendix DP-1. It does not exhibit the type of reverse curvature and resultant abrupt changes from positive moment to negative moment as would be observed for a beam with a series of concentrated applied moments. The reason for this is that the weight of the pad and the resultant inertia loads are comparable to those of the casks. The relevant parameters for the Hosgri load cases 2 to 6 are as follows:

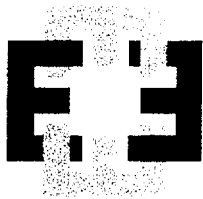
Total Cask Weight  $20 \times 360$  = 7200 kips  
Pad Weight  $0.15 \times 68 \times 105 \times 7.5$  = 8033 kips

Net Horizontal Cask Shear  $20 \times 515$  = 10300 kips  
Net Horizontal Pad Shear  $0.808 \times 8033$  = 6490 kips

Net Vertical Cask Down  $20 \times 267.04$  = 5341 kips  
Net Vertical Pad Down  $0.8 \times 8033$  = 6426 kips

Therefore, the mass of the pad and its inertia loads are as important to the overall response of the pad as the applied loads from the casks. In addition, the casks apply their loads over a diameter of approximately 12 feet while the pad in the analysis is just 7.5 feet thick. Hence, though the applied stresses tend to concentrate at the sides of the casks toward and away from the direction of the "aimed" seismic load, they do apply loads over their curved areas, and the resultant stresses do tend to "radiate" from the cask locations. Thus, the selection of pad locations midway between the casks, as opposed to the edges of the casks, will result in applied forces and moments of sufficient accuracy to appropriately size the reinforcement.

A strip is shown in Figure 27. The elements on the side(s) of a particular strip are isolated from the remainder of the pad. Further, the elements on one side of the selected surface are eliminated. Then a node (or point, defined by its coordinates) is specified. In the current analyses, the center of each selected surface is specified. The ANSYS program is then instructed to compute the stress resultants and print them to a file. The program actually uses the nodal forces rather than integrating stresses. The



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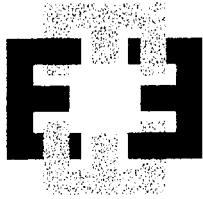
forces/moments computed are those that the elements are applying to the selected nodes. The negative of these values are the forces that must be applied to the section, i.e. selected nodes, to maintain equilibrium, such as would be seen in a free body diagram. The forces are computed in the Global Coordinate System. Figure 28 shows the two types of strips used to section and the pad, and the coordinate system.

The signs of the computed internal forces must be carefully observed. ANSYS computes the forces in the Global Coordinate System (this is the default). Hence for Z Strips positive  $M_x$  means that tensile stresses exist on the bottom of the pad, and positive  $F_z$  means that net compression exists on the cross section. For X Strips, positive  $M_z$  means that compressive stresses exist on the bottom of the pad, and positive  $F_x$  means that net compression exists on the cross section. These conventions hold true for all sections on the strips except the last section. The last sections for each strip have the contributing elements that are on the opposite sides of the cross sections from the other cross sections. Thus the signs of the computed internal forces relative to the stresses are reversed. For the last sections on the Z Strips, positive  $M_x$  means that compressive stresses exist on the bottom of the pad, and positive  $F_z$  means that net tension exists on the cross section. For the last sections on the X Strips positive  $M_z$  means that tensile stresses exist on the bottom of the pad, and positive  $F_x$  means that net tension exists on the cross section. The table below summarizes the sign convention:

#### Sign Convention for Internal Forces

<b>Z Strips</b>	+ $M_x$ → tensile stresses on bottom of pad + $F_z$ → net compression on cross section
<b>Z Strips - Last Section, Line 1</b>	+ $M_x$ → compressive stresses on bottom of pad + $F_z$ → net tension on cross section
<b>X Strips</b>	+ $M_z$ → compressive stresses on bottom of pad + $F_x$ → net compression on cross section
<b>X Strips – Last Section, Line A</b>	+ $M_z$ → tensile stresses on bottom of pad + $F_x$ → net tension on cross section

Sections throughout the pad are isolated and the internal forces acting upon them are computed. The pad is thus divided into four North-South strips, A-B through D-E, and seven East-West strips, 1-3, 3-4 through 7-8 and 8-10. Figure 29 shows the grid line layout of the strips, and Figure 30 shows the locations and designation used for two sections. Each North-South strip is then sequentially reduced a line at a time, from Line 10 to 1. Similarly, each East-West strip is sequentially reduced a line at a time, from Line E to A. Thus, there are ten sections for each of the four Z Strips isolated, and five sections for each of the seven X Strips isolated, for a total of 75 cross sections for the calculation of internal pad forces. All strips are seventeen feet wide except strips 1-3 and 8-10, which are ten feet wide.



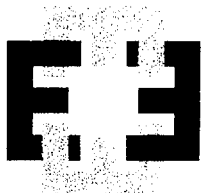
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REVIEWER	<u>K. L. Whitmore</u>	APPROVED	<u>R. F. Evers</u>		
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The last sections for the Z Strips are the Line 1 sections, and the last sections for the X strips are the Line A sections.

Figures 31 and 32 show a sample of the various sections used, generated by the ANSYS program. All are provided in Appendix MD-4.

The data from the file are then compiled and provided in Tables 6 to 10. See Appendix FC-1 for the ANSYS input and output files. Since the Hosgri HE (1) event using the soft rock analysis is the most demanding for the pad design, only the Hosgri results for the soft rock analyses were processed. The stress results show that these will provide the controlling forces and moments for the design of the pad. The forces for pad design are provided in Table 11.



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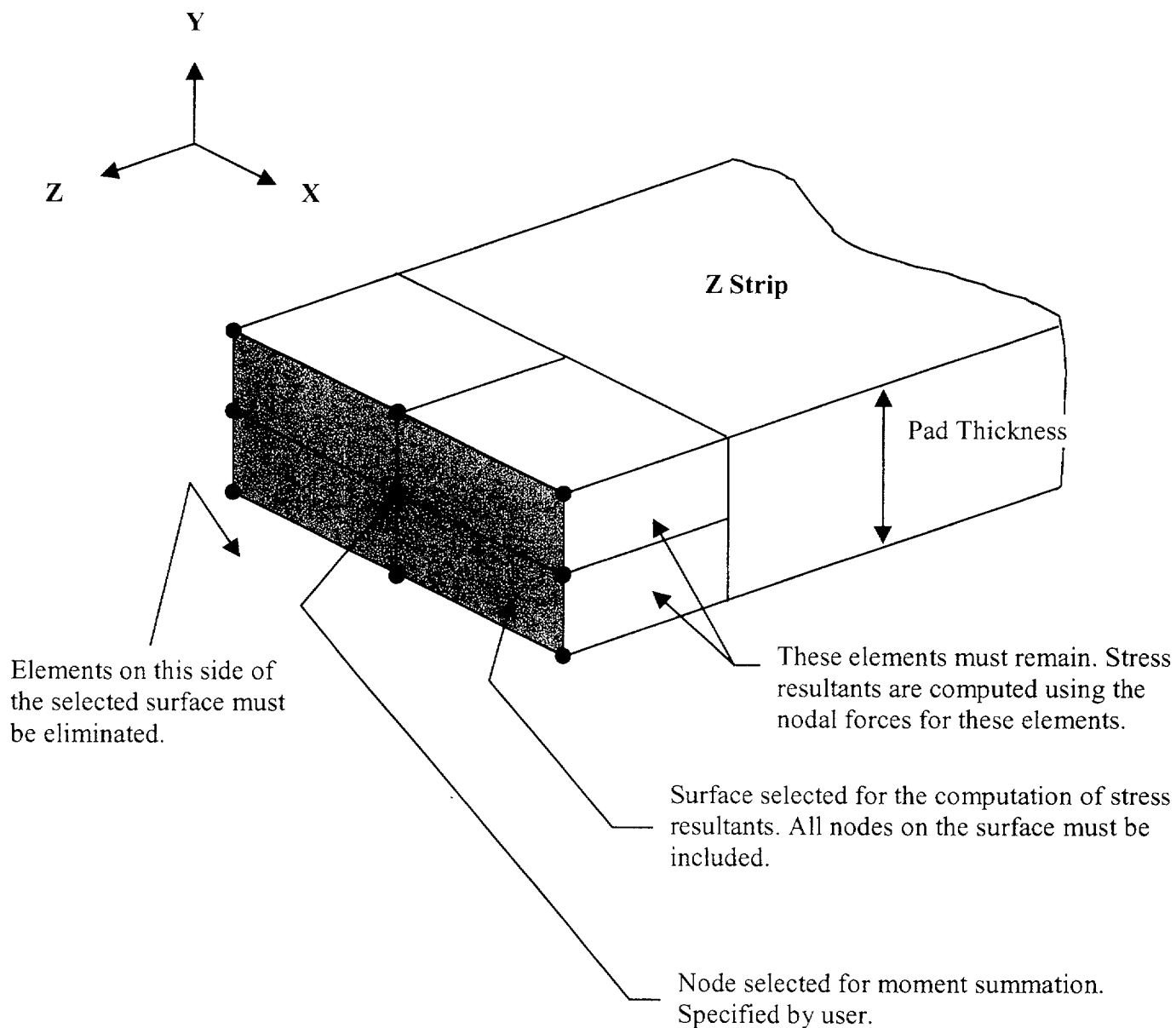
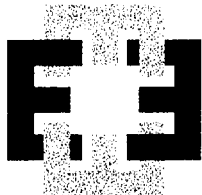


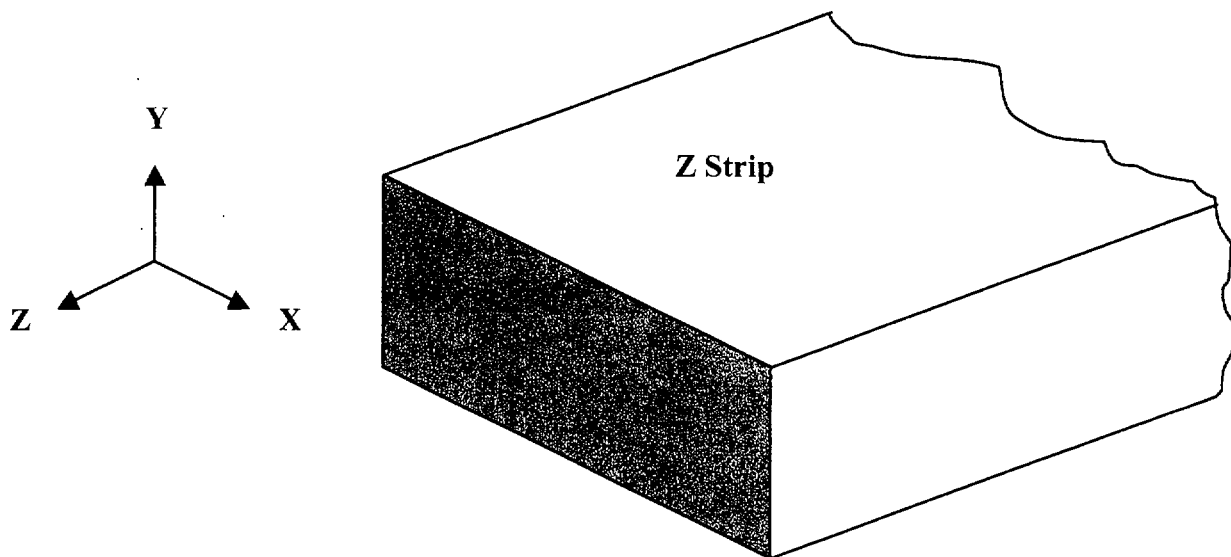
Figure 27 – Strip/Selected Surface



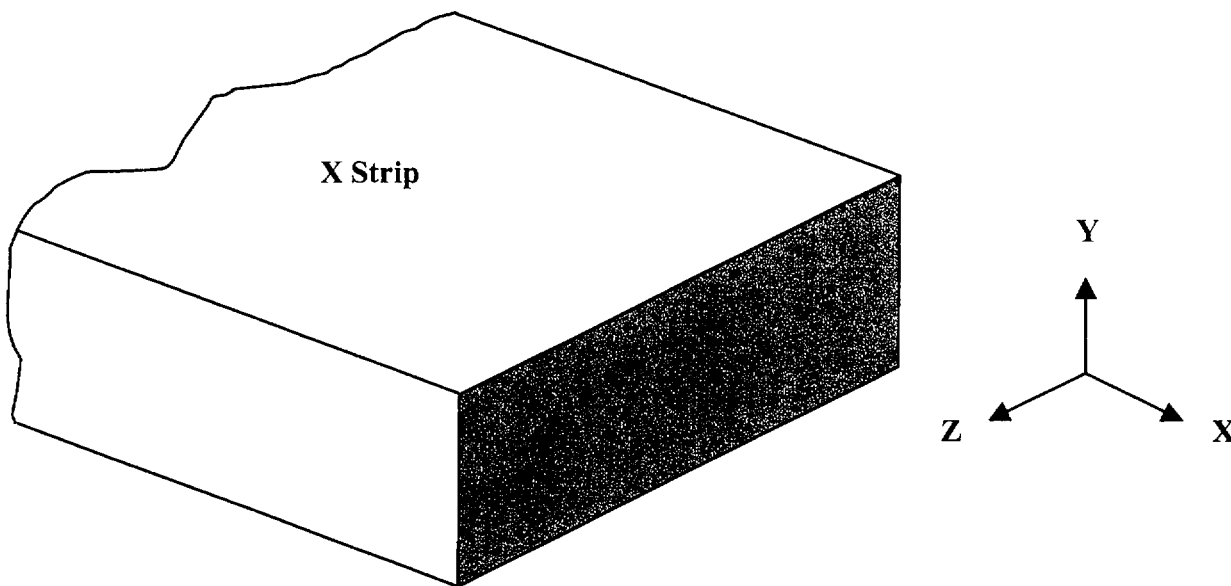


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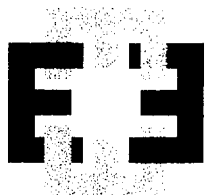
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Coordinate system and section for Z strips.



Coordinate system and section for X strips  
Figure 28 - Strips and Coordinate System



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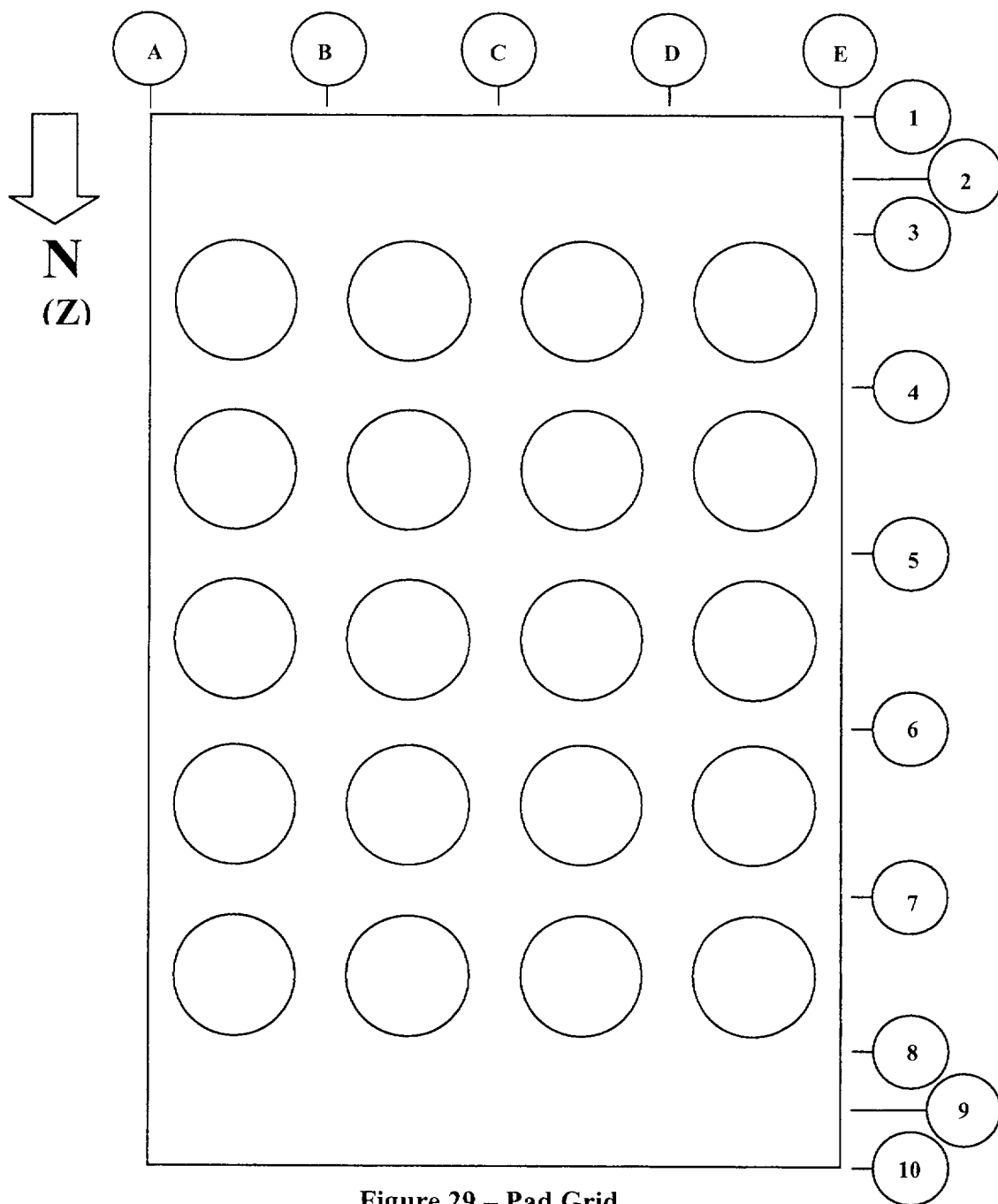
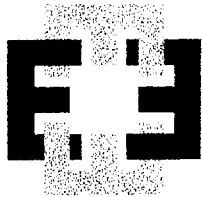


Figure 29 – Pad Grid



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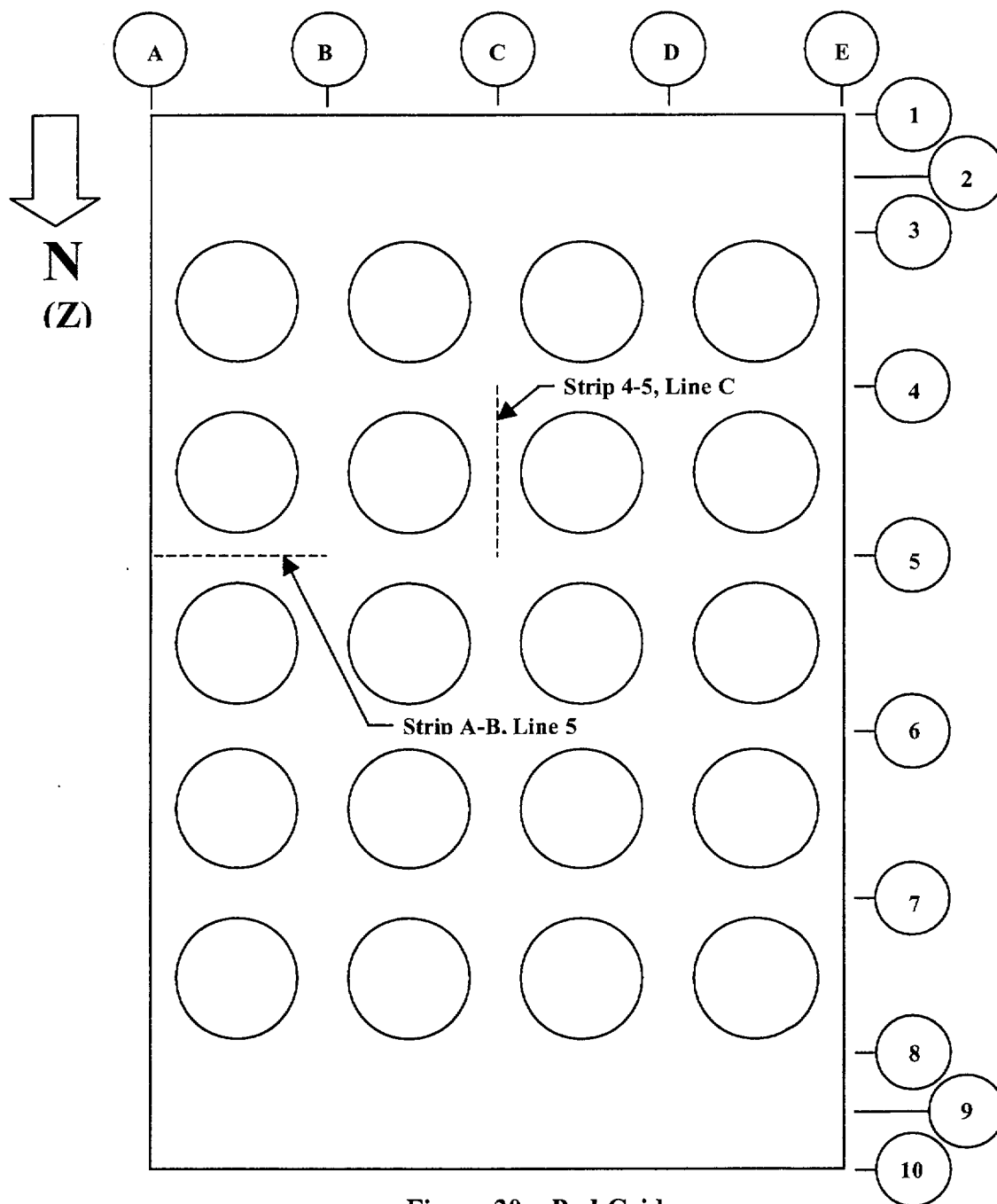
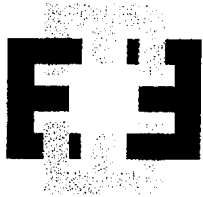


Figure 30 - Pad Grid



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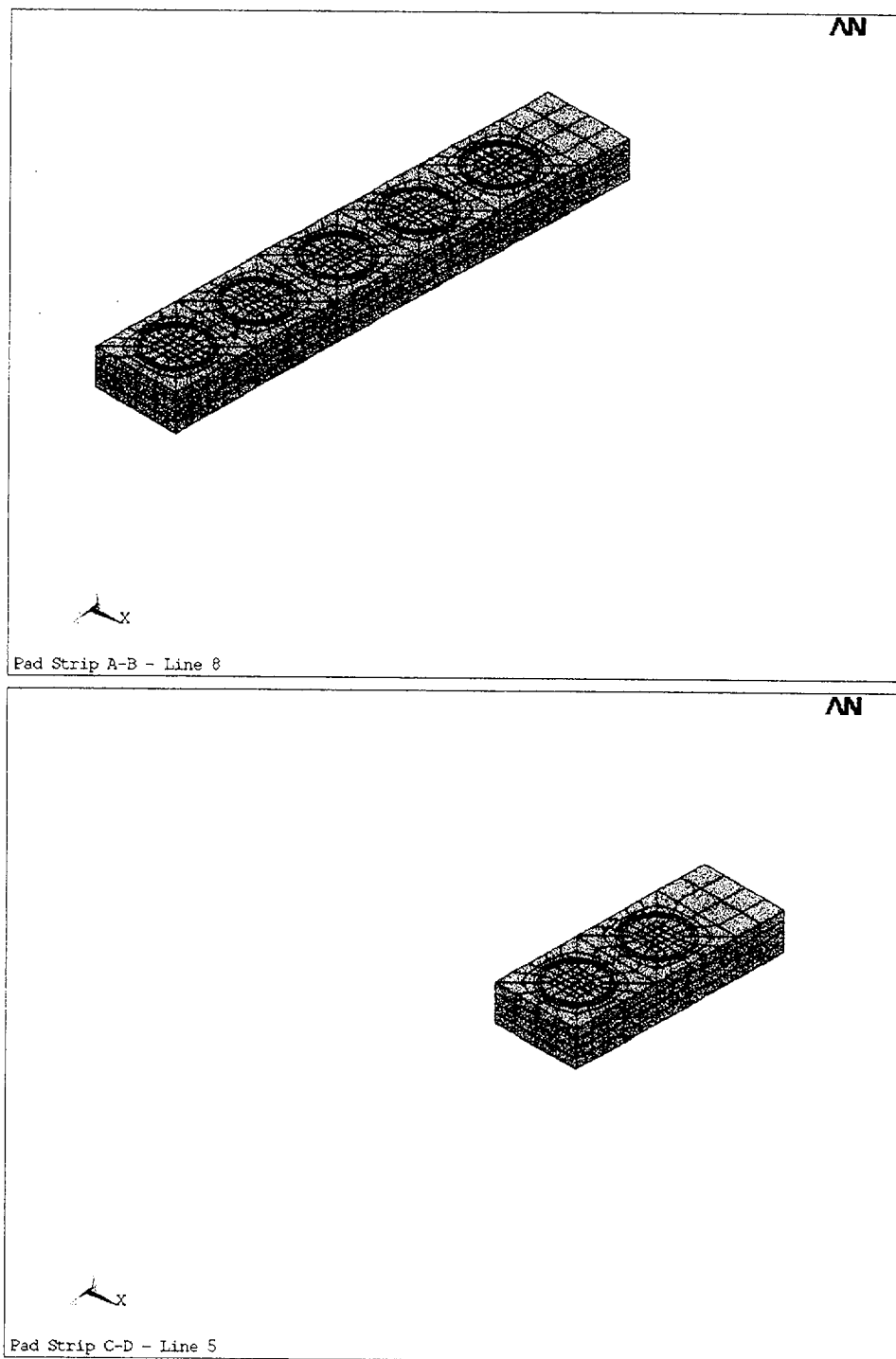
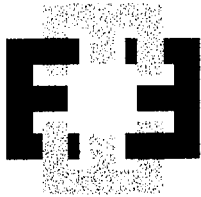


Figure 31 – North/South (Z) Strips



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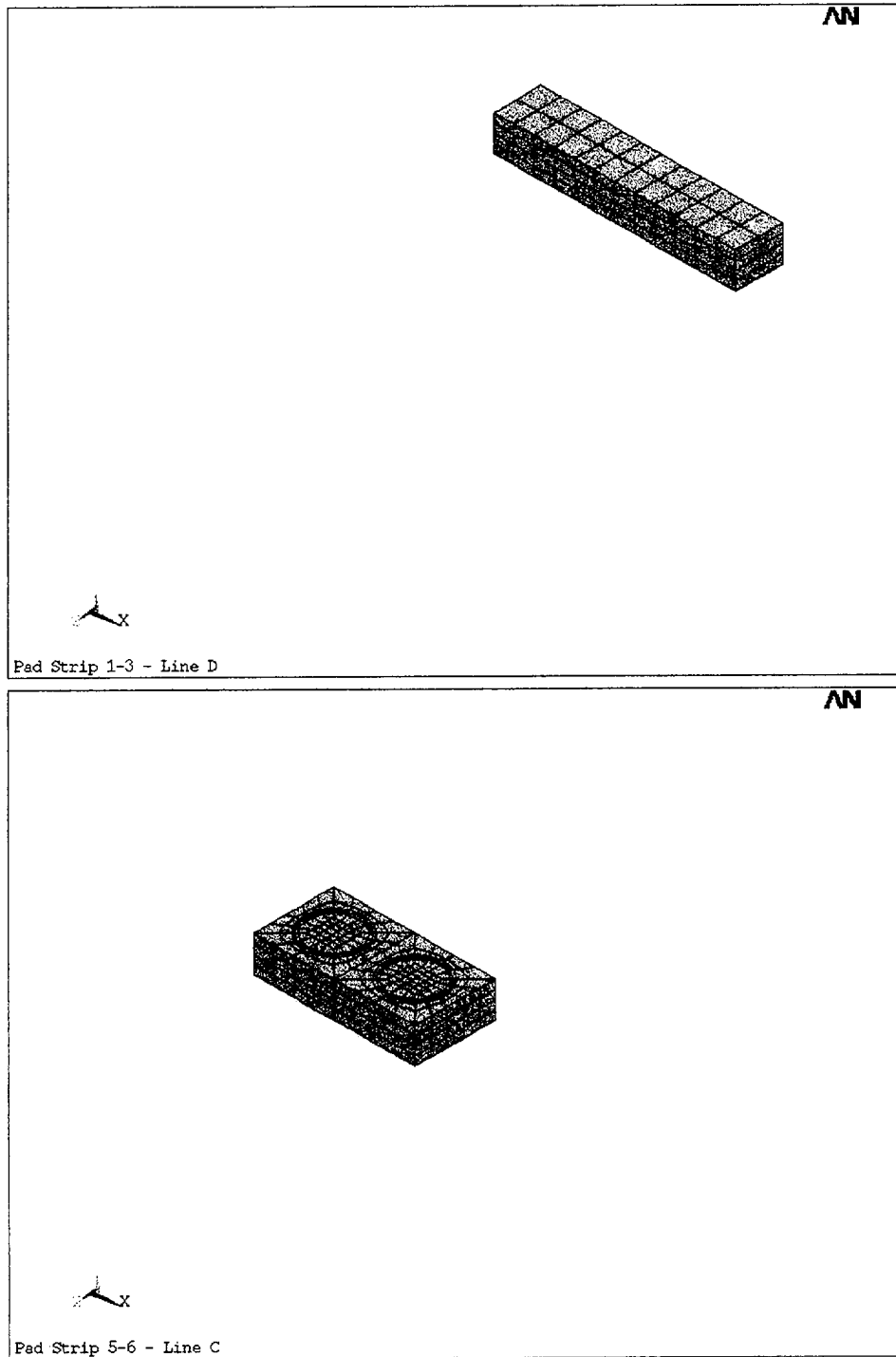
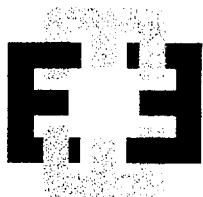


Figure 32 – East/West (X) Strips

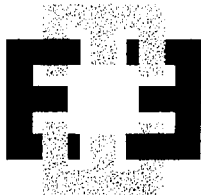


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Table 6 (1/3) - HE (1) NORTH - Z STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		A-B	B-C	C-D	D-E
10	Fy Fz Mx	-479342 984456 -0.443E8	-430237 921036 -0.414E8	Sym. With B-C	Sym. With A-B
9	Fy Fz Mx	-532371 941641 -0.197E8	-469565 785822 -0.150E8	Sym. With B-C	Sym. With A-B
8	Fy Fz Mx	-527383 971263 4488084	-436497 778974 8354419	Sym. With B-C	Sym. With A-B
7	Fy Fz Mx	-549967 776479 -900395	-440869 632337 1854746	Sym. With B-C	Sym. With A-B
6	Fy Fz Mx	-568401 488622 576226	-453052 447516 3581983	Sym. With B-C	Sym. With A-B
5	Fy Fz Mx	-625312 202111 8951040	-490995 238016 0.127E8	Sym. With B-C	Sym. With A-B
4	Fy Fz Mx	-731078 -97229 0.333E8	-634149 8119 0.345E8	Sym. With B-C	Sym. With A-B
3	Fy Fz Mx	-176465 -460244 0.165E8	-129535 -343547 0.153E8	Sym. With B-C	Sym. With A-B
2	Fy Fz Mx	-88102 -528563 0.242E8	-64899 -473992 0.233E8	Sym. With B-C	Sym. With A-B
1	Fy Fz Mx	11602 605828 -0.272E8	-11601 551257 -0.249E8	Sym. With B-C	Sym. With A-B

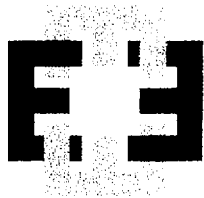


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Table 6 (2/3) - HE (1) NORTH - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		1-3	3-4	4-5	5-6
E	Fx	69141	59429	119874	130021
	Fy	-55218	-104528	-176353	-185489
	Mz	1778811	1889824	5555787	5975053
D	Fx	270128	211324	182824	194517
	Fy	-31071	-81250	-37720	-41194
	Mz	3922969	-8350719	-7976190	-7447854
C	Fx	311040	280349	208770	215522
	Fy	-4693	-55875	-15420	-18372
	Mz	-5851179	-0.107E8	-8936599	-8006198
B	Fx	243769	185685	182342	191851
	Fy	22875	-28073	12084	11885
	Mz	-4296744	-7574883	-7876086	-7733355
A	Fx	-69141	-59429	-119874	-130021
	Fy	-55218	-104528	-176353	-185490
	Mz	1778811	-1889825	-5555787	-5975054



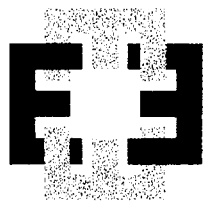
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Table 6 (3/3) - HE (1) NORTH - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip		
		6-7	7-8	8-10
E	Fx	123553	115783	29304
	Fy	-177456	-187168	-85803
	Mz	5562018	5165282	3192955
D	Fx	194123	85375	-157783
	Fy	-42445	-49296	-28401
	Mz	-7318432	-7170075	-1449223
C	Fx	208684	46752	-175859
	Fy	-22028	-32661	-28973
	Mz	-7748704	-7143824	-1135164
B	Fx	191504	119437	-138212
	Fy	5855	-4868	-21959
	Mz	-7564913	-7416332	-1359089
A	Fx	-123553	-115783	-29304
	Fy	-177456	-187168	-85803
	Mz	5562019	-5165281	-3192957



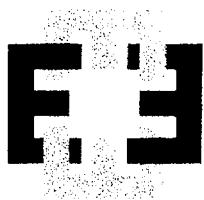


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Table 7 (1/3) - HE (1) N 32.93 W - Z STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		A-B	B-C	C-D	D-E
10	Fy	-389254	-388772	-383148	-442900
	Fz	801209	783126	798373	873057
	Mx	-0.345E8	-0.353E8	-0.359E8	-0.408E8
9	Fy	-433936	-413802	-412225	-486561
	Fz	836009	677379	678284	769405
	Mx	-0.141E8	-0.122E8	-0.127E8	-0.187E8
8	Fy	-410580	-380100	-379675	-507225
	Fz	932447	680829	662665	723971
	Mx	5679663	7885156	7661142	3114136
7	Fy	-460869	-381138	-372961	-488408
	Fz	934240	623931	494679	420015
	Mx	1656574	2821450	2541931	-914486
6	Fy	-498597	-394766	-382051	-493842
	Fz	782025	507279	302985	91509
	Mx	5782106	4869688	3437506	-855625
5	Fy	-545048	-430138	-403350	-517184
	Fz	555056	333949	123732	-170261
	Mx	0.183E8	0.136E8	9497611	3131378
4	Fy	-456383	-513914	-454508	-549745
	Fz	224496	96580	-52112	-387865
	Mx	0.336E8	0.308E8	0.241E8	0.149E8
3	Fy	-151186	-106893	-127649	-226272
	Fz	-300717	-265320	-294964	-491737
	Mx	0.122E8	0.128E8	0.122E8	0.103E8
2	Fy	-71335	-55886	-63676	-115104
	Fz	-417731	-388470	-405838	-487285
	Mx	0.202E8	0.195E8	0.198E8	0.195E8
1	Fy	-5165	-20614	-12824	38604
	Fz	482565	453304	470671	552119
	Mx	-0.221E8	-0.206E8	-0.213E8	-0.241E8

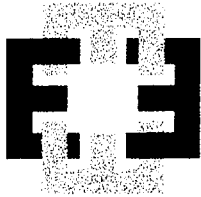


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Table 7 (2/3) - HE (1) N 32.93 W – X STRIPS – INTERNAL FORCES

Line	Force/Moment	Strip			
		1-3	3-4	4-5	5-6
E	Fx	283498	452129	529907	538508
	Fy	-79106	-380041	-448504	-443223
	Mz	0.111E8	0.203E8	0.239E8	0.242E8
D	Fx	386061	347454	305481	317380
	Fy	-97049	-378377	-328155	-312784
	Mz	-1256206	-2437693	-1664003	-1234268
C	Fx	321049	334474	255649	250783
	Fy	-66042	-378145	-310132	-284839
	Mz	-9826424	-0.164E8	-0.117E8	-9174402
B	Fx	153172	174951	134715	119990
	Fy	-6305	-277562	-323232	-270045
	Mz	-0.126E8	-0.247E8	-0.226E8	-0.181E8
A	Fx	105479	210988	238003	252640
	Fy	-56731	-11001	-23791	-456
	Mz	5947292	9325835	0.109E8	0.115E8

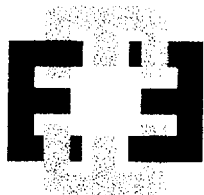


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Table 7 (3/3) - HE (1) N 32.93 W - X Strips - Internal Forces

Line	Force/Moment	Strip		
		6-7	7-8	8-10
E	Fx	518752	478957	283952
	Fy	-432162	-426549	-184953
	Mz	0.232E8	0.213E8	0.149E8
D	Fx	307254	221313	10178
	Fy	-305279	-301199	-119097
	Mz	-1270735	-1470806	2597690
C	Fx	236869	89813	-141236
	Fy	-275898	-273999	-115063
	Mz	-8288187	-7253060	150097
B	Fx	115016	40040	-246062
	Fy	-256132	-252228	-116171
	Mz	-0.162E8	-0.143E8	-3002323
A	Fx	248129	234107	219737
	Fy	11657	11915	24900
	Mz	0.110E8	0.103E8	8945723

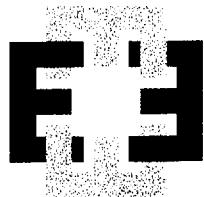


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Table 8 (1/3) - HE (1) N 45 W – Z STRIPS – INTERNAL FORCES

Line	Force/Moment	Strip			
		A-B	B-C	C-D	D-E
10	Fy	-325352	-357842	-347015	-396089
	Fz	664004	674343	693901	761311
	Mx	-0.276E8	-0.305E8	-0.313E8	-0.363E8
9	Fy	-362194	-371083	-365986	-438809
	Fz	727818	589027	589800	643616
	Mx	-0.104E8	-0.101E8	-0.107E8	-0.170E8
8	Fy	-343322	-336051	-333261	-462441
	Fz	840754	595729	571757	573564
	Mx	6379130	7532480	7168576	2584175
7	Fy	-399885	-332033	-318752	-426063
	Fz	922218	580897	414353	258937
	Mx	3262280	3685275	3172163	-393060
6	Fy	-438641	-342728	-325679	-426967
	Fz	831122	497441	236265	-54653
	Mx	7631121	5575850	3587737	-881510
5	Fy	-465772	-369446	-339732	-440479
	Fz	638180	350564	84504	-282309
	Mx	0.184E8	0.126E8	7999275	1976080
4	Fy	-373012	-413726	-348295	-441523
	Fz	307826	124277	-44466	-436877
	Mx	0.280E8	0.255E8	0.180E8	9904902
3	Fy	-137725	-92139	-120453	-214610
	Fz	-224139	-211155	-241789	-453792
	Mx	-186997	0.111E8	0.100E8	5127026
2	Fy	-61874	-48875	-59466	-135786
	Fz	-351226	-325452	-340128	-417498
	Mx	0.176E8	0.167E8	0.167E8	0.141E8
1	Fy	-14626	-27625	-17034	59286
	Fz	405828	380054	394730	472100
	Mx	-0.190E8	-0.174E8	-0.180E8	-0.200E8

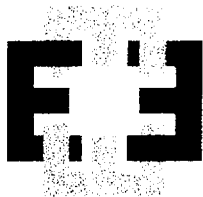


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Table 8 (2/3) - HE (1) N 45 W - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		1-3	3-4	4-5	5-6
E	Fx	372673	579982	652001	662871
	Fy	-126085	-470689	-520256	-518256
	Mz	0.155E8	0.261E8	0.293E8	0.297E8
D	Fx	426121	402216	351134	360782
	Fy	-138189	-454611	-411375	-397072
	Mz	-1335521	-2050754	-345760	325408
C	Fx	325233	362866	283100	272998
	Fy	-99116	-468289	-402202	-378309
	Mz	-0.122E8	-0.199E8	-0.145E8	-0.114E8
B	Fx	125910	190056	149033	117907
	Fy	-19847	-344044	-448914	-424565
	Mz	-0.162E8	-0.324E8	-0.319E8	-0.273E8
A	Fx	157191	282957	318364	340419
	Fy	-59518	5109	-14886	97
	Mz	8290350	0.124E8	0.143E8	0.153E8

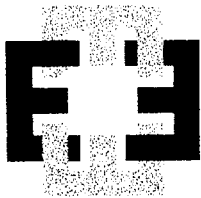


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Table 8 (3/3) - HE (1) N 45 W – X Strips – Internal Forces

Line	Force/Moment	Strip		
		6-7	7-8	8-10
E	Fx	640137	589823	366057
	Fy	-507141	-493633	-215619
	Mz	0.286E8	0.262E8	0.185E8
D	Fx	346794	275615	86547
	Fy	-387703	-379997	-147402
	Mz	397700	263964	3755967
C	Fx	257122	126085	-99190
	Fy	-362466	-353165	-146313
	Mz	-9854861	-8168614	228578
B	Fx	108262	33846	-248825
	Fy	-382498	-350581	-157283
	Mz	-0.240E8	-0.199E8	-4749089
A	Fx	338346	325587	282880
	Fy	13916	20970	33425
	Mz	0.150E8	0.142E8	0.125E8



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Table 9 (1/3) - HE (1) N 57.07 W - Z STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		A-B	B-C	C-D	D-E
10	Fy	-247620	-318496	-303039	-340405
	Fz	500694	540665	564231	620784
	Mx	-0.197E8	-0.246E8	-0.255E8	-0.303E8
9	Fy	-275731	-315240	-308980	-375239
	Fz	592301	480352	480970	493941
	Mx	-6523518	-7340447	-8158849	-0.143E8
8	Fy	-263576	-278920	-275781	-399808
	Fz	715855	490374	461400	402743
	Mx	6524561	7092327	6608839	2220029
7	Fy	-315591	-268302	-251966	-345651
	Fz	874679	521455	326173	96470
	Mx	5162040	4810041	3973422	372199
6	Fy	-346785	-275775	-256457	-342788
	Fz	846870	473106	171235	-184069
	Mx	8720461	6222828	3842488	-685040
5	Fy	-354246	-295110	-265631	-349588
	Fz	690846	354621	53375	-362607
	Mx	0.155E8	0.111E8	6744046	1317446
4	Fy	-293556	-302758	-257699	-336965
	Fz	378042	158280	-25643	-446219
	Mx	0.215E8	0.194E8	0.127E8	6974362
3	Fy	-118617	-73319	-119870	-160367
	Fz	-137704	-143957	-170375	-372712
	Mx	8640674	9219277	6553221	1536800
2	Fy	-49072	-39726	-56627	-126340
	Fz	-271218	-245947	-250692	-306845
	Mx	0.146E8	0.133E8	0.125E8	8396794
1	Fy	-27428	-36774	-19873	49840
	Fz	313198	287926	292671	348825
	Mx	-0.153E8	-0.134E8	-0.136E8	-0.137E8



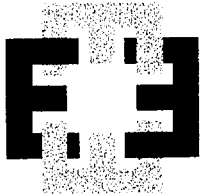
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Table 9 (2/3) - HE (1) N 57.07 W - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		1-3	3-4	4-5	5-6
E	Fx	450218	679590	749805	763680
	Fy	-177633	-528402	-577059	-579257
	Mz	0.197E8	0.304E8	0.336E8	0.342E8
D	Fx	444534	443412	388621	396899
	Fy	-182106	-491581	-475709	-465942
	Mz	-136072	-879857	702827	1401693
C	Fx	314728	380706	306788	291856
	Fy	-142078	-526190	-476190	-459813
	Mz	-0.140E8	-0.227E8	-0.172E8	-0.141E8
B	Fx	94084	200348	170344	139190
	Fy	-38765	-399797	-482381	-539145
	Mz	-0.195E8	-0.390E8	-0.401E8	-0.359E8
A	Fx	203417	342100	379049	403341
	Fy	-61455	16577	-3860	4614
	Mz	0.104E8	0.150E8	0.169E8	0.180E8



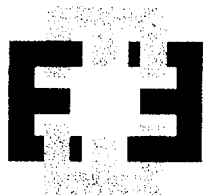


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Table 9 (3/3) - HE (1) N 57.07 W - X Strips - Internal Forces

Line	Force/Moment	Strip		
		6-7	7-8	8-10
E	Fx	739447	680607	432652
	Fy	-568509	-546884	-232478
	Mz	0.330E8	0.302E8	0.213E8
D	Fx	380446	327981	165085
	Fy	-456362	-445652	-171680
	Mz	1600167	1638774	4643853
C	Fx	275914	170069	-42161
	Fy	-441812	-424563	-176363
	Mz	-0.121E8	-9714659	-51248
B	Fx	118953	41416	-225013
	Fy	-531133	-471289	-201104
	Mz	-0.320E8	-0.269E8	-7807333
A	Fx	403758	393858	315633
	Fy	15376	27793	955
	Mz	0.178E8	0.172E8	0.146E8

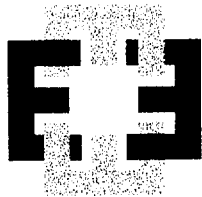


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REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers			
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Table 10 (1/3) - HE (1) WEST - Z STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		A-B	B-C	C-D	D-E
10	Fy Fz Mx	-89382 38589 983130	-127868 91044 -3706622	-152281 129661 -6061128	-143481 140044 -9185582
9	Fy Fz Mx	-65182 174217 4598607	-119504 123475 1073714	-116961 122259 395996	-150936 19445 -4240410
8	Fy Fz Mx	-36098 298134 7173904	-106948 144979 5903260	-88183 106397 4849006	-171805 -102709 1543524
7	Fy Fz Mx	-15956 648248 9604255	-31402 318485 9232858	-23333 88655 6862494	-60070 -291139 3417829
6	Fy Fz Mx	-28443 796550 9092937	-26025 383567 8121906	-23057 41805 5033766	-52228 -401664 764098
5	Fy Fz Mx	-46973 776337 8985788	-28304 373753 8376861	-27930 45884 5228107	-54469 -389753 1073675
4	Fy Fz Mx	-55924 586490 9173212	-17482 289296 9953764	-15753 101657 7341382	-34866 -253450 4496735
3	Fy Fz Mx	-11424 174172 6188009	42596 123453 5921344	40225 122275 5107146	74413 19398 2521466
2	Fy Fz Mx	12764 38618 4038801	51143 90943 1664371	75743 129645 780213	66980 139995 -2869666
1	Fy Fz Mx	-89264 -38618 -977960	-127643 -90943 3699209	-152243 -129645 6059382	-143480 -139995 9183442



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Table 10 (2/3) - HE (1) WEST - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip			
		1-3	3-4	4-5	5-6
E	Fx	525273	793710	864466	886415
	Fy	-239121	-603514	-644896	-653720
	Mz	0.245E8	0.353E8	0.386E8	0.396E8
D	Fx	359377	439877	428621	442417
	Fy	-207832	-537258	-547955	-550606
	Mz	4887233	2676159	2511197	2533592
C	Fx	155772	313732	319608	322227
	Fy	-229902	-533490	-544956	-547001
	Mz	-5421793	-0.174E8	-0.182E8	-0.184E8
B	Fx	-49505	154160	176810	171332
	Fy	-146374	-511333	-540098	-546142
	Mz	-0.218E8	-0.449E8	-0.476E8	-0.481E8
A	Fx	304554	439648	461317	471814
	Fy	-51285	28776	15306	14470
	Mz	0.148E8	0.193E8	0.203E8	0.208E8

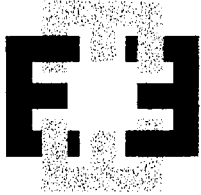


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Table 10 (3/3) - HE (1) WEST - X STRIPS - INTERNAL FORCES

Line	Force/Moment	Strip		
		6-7	7-8	8-10
E	Fx Fy Mz	Sym. with 4-5	Sym. with 3-4	Sym. with 1-3
D	Fx Fy Mz	Sym. with 4-5	Sym. with 3-4	Sym. with 1-3
C	Fx Fy Mz	Sym. with 4-5	Sym. with 3-4	Sym. with 1-3
B	Fx Fy Mz	Sym. with 4-5	Sym. with 3-4	Sym. with 1-3
A	Fx Fy Mz	Sym. With 4-5	Sym. with 3-4	Sym. with 1-3

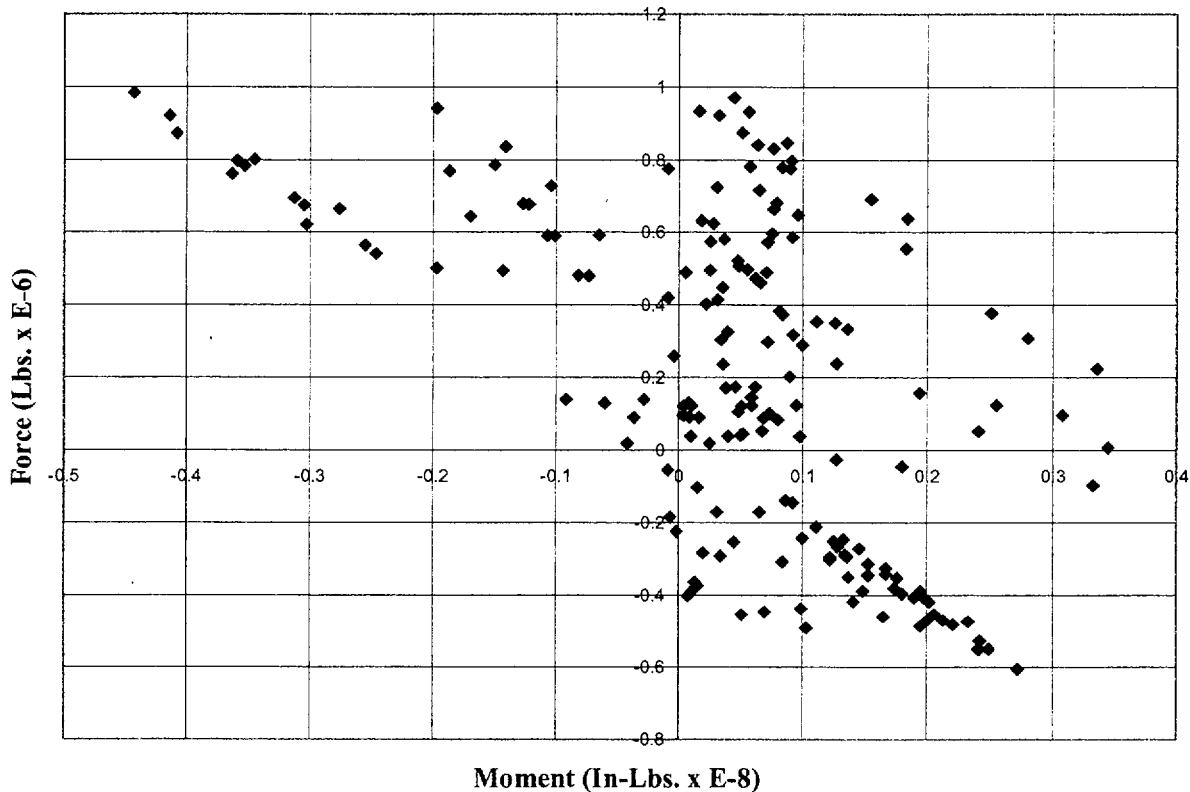


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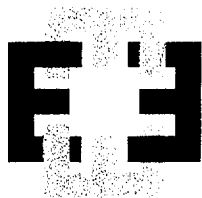
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REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers			
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All the moment and axial force data in Tables 6 through 10 are plotted in Figures 33 and 34 below. The input data was adjusted for the 10 foot strips (factored by 1.7) and for the last section (signs were reversed). Table 11 presents design data from each quadrant, i.e., all the combinations of controlling signed values of moment and axial force, along with the maximum shear values, scanned manually.

**Z Strips Force/Moment Plot**



**Figure 33 – Z Strips Internal Forces**



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### X Strips Force/Moment Plot

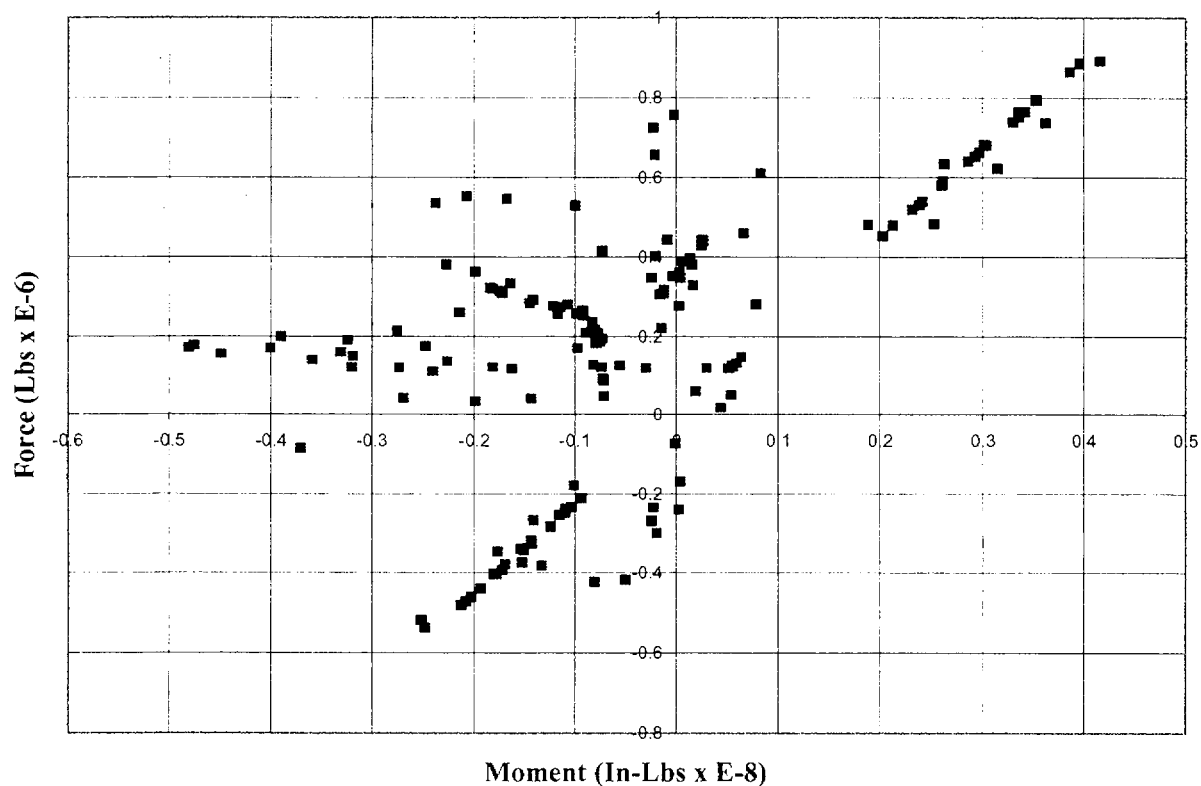
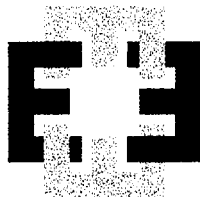


Figure 34 – X Strips Internal Forces



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Table 11 (1/2) - Z Strips – Internal Forces for Design

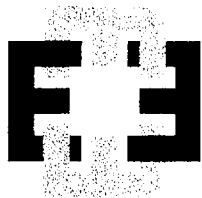
Quadrant	Mx	Fz	Location/Table Ref.
+Mx Ten. on Bot.	0.0449E8	0.971E6	A-B/8 Table 6
+Fz Comp. on Sect.	0.184E8	0.638E6	A-B/5 Table 8
	0.336E8	0.224E6	A-B/4 Table 7
	0.345E8	0.00812E6	B-C/4 Table 6
-Mx Comp. On Bot.	-0.443E8	0.984E6	A-B/10 Table 6
+Fz Comp. on Sect.			
-Mx Comp. On Bot.	-0.00187E8	-0.224E6	A-B/3 Table 8
-Fz Ten. on Sect.			
+Mx Ten. on Bot.	0.333E8	-0.097E6	B-C/4 Table 6
-Fz Ten. on Sect.	0.272E8	-0.606E6	A-B/1 Table 6
Shear Force	Fy	-731078	A-B/4 Table 6

Table 11 (2/2) - X Strips – Internal Forces for Design

Quadrant	Mz	Fx	Location/Table Ref.
+Mz Comp. on Bot.	0.4165E8	0.8925E6	1-3/E Table 10*
+Fx Comp. on Sect.			
-Mz Ten. on Bot.	-0.00231E8	0.7565E6	1-3/D Table 9*
+Fx Comp. on Sect.	-0.238E8	0.5355E6	1-3/C Table 9*
	-0.476E8	0.177E6	4-5/B Table 10
	-0.481E8	0.171E6	5-6/B Table 10
-Mz Ten. on Bot.	-0.370E8	-0.08415E6	1-3/B Table 10*
-Fx Ten. on Sect.	-0.2516E8	-0.5185E6	1-3/A Table 10*
	-0.2482E8	-0.5372E6	8-10/A Table 9*
+Mz Comp. on Bot.	0.00255E8	-0.2397E6	8-10/C Table 7*
-Fx Ten. on Sect.			
Shear Force	Fy	-653720	5-6/E Table 10

\* Factor of 1.7 applied.

Adjustments to these values will be made using factors developed later in this calculation.



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REVIEWER	K. L. Whitmore	APPROVED	R. F. Evers		
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### Rock Bearing Pressures

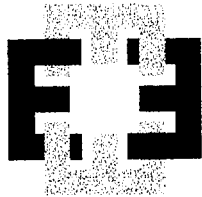
The database was scanned using the ANSYS post processor for the maximum compressive stress in the rock beneath the pad. The results are provided in Table 12 below. See Appendix SN-2 for the details.

**Table 12 - ROCK RESPONSE – PRESSURE (STRESS) RESULTS**

LS	EQ	Direction	SOFT	HARD	V HARD
			$\sigma_{Y \text{ Max}}$	$\sigma_{Y \text{ Max}}$	$\sigma_{Y \text{ Max}}$
1		Gravity	-15.72	-16.32	-16.36
2	HE(1)	N	-18.25	-20.38	-23.86
3	HE(1)	N32.93W	-21.72	-25.06	-27.61
4	HE(1)	N45W	-24.20	-27.92	-31.13
5	HE(1)	N57.07W	-26.36	-30.61	-34.42
6	HE(1)	W	-29.31	-34.28	-38.92
7	HE(1)*	N	-8.77	-9.60	-11.05
8	HE(1)*	W	-13.39	-15.39	-17.35
9	HE(3)*	N	-28.94	-30.10	-30.18
10	HE(3)*	W	-32.05	-34.13	-36.24
11	L(2)	N	-16.65	-17.93	-21.00
12	L(2)	N32.93W	-19.61	-22.38	-24.61
13	L(2)	N45W	-21.78	-24.93	-27.77
14	L(2)	N57.07W	-23.71	-27.35	-30.75
15	L(2)	W	-26.32	-30.55	-34.68
16	L(2)*	N	-7.17	-7.16	-8.50
17	L(2)*	W	-10.95	-12.64	-14.37
18	L(4)*	N	-6.63	-6.11	-7.27
19	L(4)*	W	-9.44	-10.93	-12.47

\* Load components are combined using the 40-100-40 rule. All others combined using 100-40-40 rule.





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CLIENT	PG&E-DCPP	ORIGINATOR	S. C. Tumminelli		
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The applied gravity bearing pressure is 16.36 psi =  $16.36 \times 144 / 1000 = 2.36$  ksf. The allowable bearing pressure is 40 ksf, (Section 6.4.3.5, Reference 2). Therefore, this is acceptable with ample margin.

The maximum applied gravity plus seismic pressures all occur in the very hard rock analyses. These pressures are (see Table 12):

38.92 psi for LS 6, HE(1) West, combined via the 100-40-40 rule  
36.24 psi for LS 10 HE(3) West, combined via the 40-100-40 rule  
34.68 psi for LS 15 LTSP(2) West, combined via the 100-40-40 rule

The application of the Holtec force components and the pad accelerations for LS 10 were designed to maximize the applied bearing pressure. However, the components and accelerations for LS 6 and 15 were designed to maximize uplift. The results from these two analyses are adjusted to reflect the maximum down components. Use a 17-foot square associated with a single cask.

For the Hosgri load cases, use the maximum down component from HE(3) rather than HE(1) to be conservative (See Table 1 and the descriptions of the load steps). Therefore:

Max. Dn for HE is  $360 + 0.40 \times (773.3 - 360) = 525.32$  kips and  
 $\Delta$  Dn =  $525.32 - 267.04$  kips = 258.28 kips

Max  $\Delta$  Dn acceleration is  $2 \times 0.20 = 0.40G$   
Thus,  $\Delta$  pad load is  $0.40 \times (17 \times 17 \times 7.5 \times 0.15) = 130.05$  kips.

Thus, Net  $\Delta$  Dn =  $258.28 + 130.05 = 388.33$  kips.

And the increase in bearing pressure is  $\frac{388.33}{17 \times 17} = 1.344$  ksf

Adding this to the LS 6 result of 38.92 psi is:

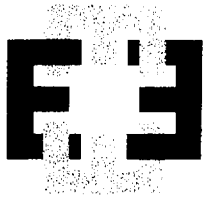
Net Pressure =  $38.92 \times 144 / 1000 + 1.344 = 6.95$  ksf.

The LTSP value is computed similarly:

Max. Dn for LTSP is  $360 + 0.40 \times (684.1 - 360) = 489.64$  kips and  
 $\Delta$  Dn =  $489.64 - 258.32$  kips = 231.32 kips

Max  $\Delta$  Dn acceleration is  $2 \times 0.28 = 0.56G$   
Thus,  $\Delta$  pad load is  $0.56 \times (17 \times 17 \times 7.5 \times 0.15) = 182.07$  kips.

Thus, Net  $\Delta$  Dn =  $231.32 + 182.07 = 413.39$  kips.



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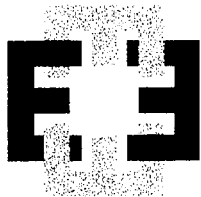
And the increase in bearing pressure is  $\frac{413.39}{17*17} = 1.430$  ksf

Adding this to the LS 15 result of 34.68 psi is:

Net Pressure =  $34.68*144/1000 + 1.430 = 6.42$  ksf.

Therefore, the maximum applied gravity plus seismic bearing pressure is 6.95 ksf. The allowable bearing pressure is 52 ksf, (Section 6.4.3.5, Reference 2). This is also acceptable with ample margin.

The vertical stresses are plotted below in Figures 35 to 38 for Load Steps 6 and 10. These plots show that the computed maximum pressures are very local within the rock mass.



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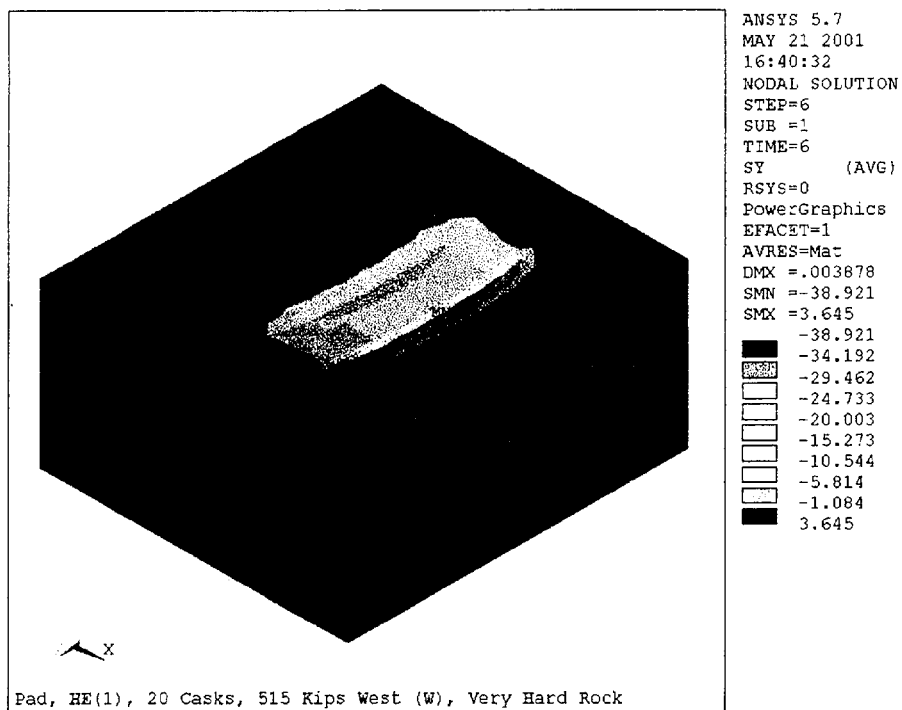


Figure 35 – Rock Y direction stresses for Load Step 6

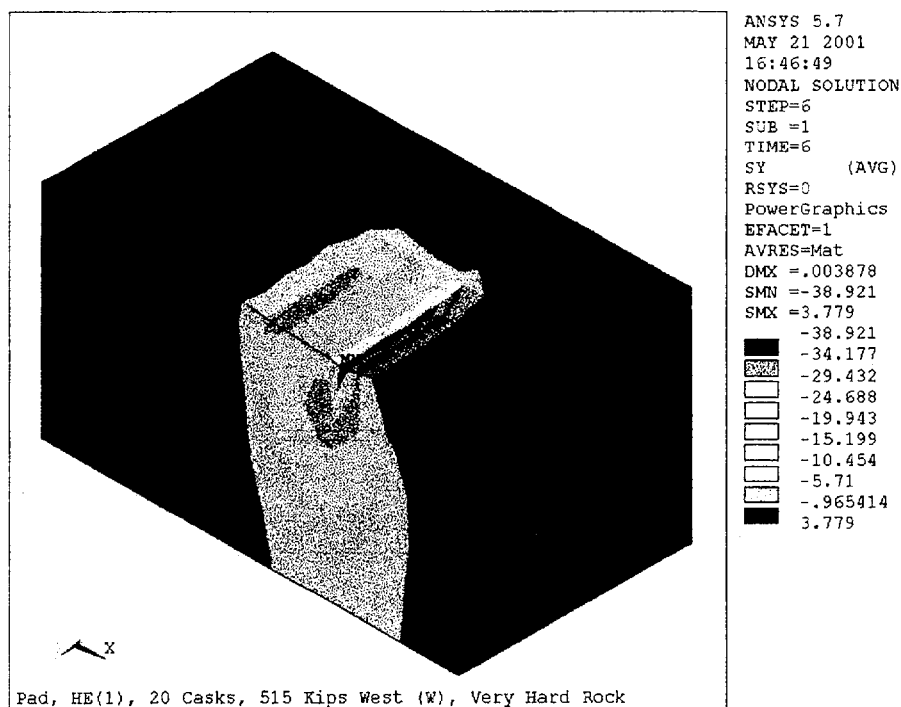
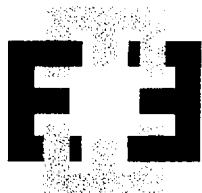


Figure 36 – Rock Y direction stresses, cutaway, for Load Step 6



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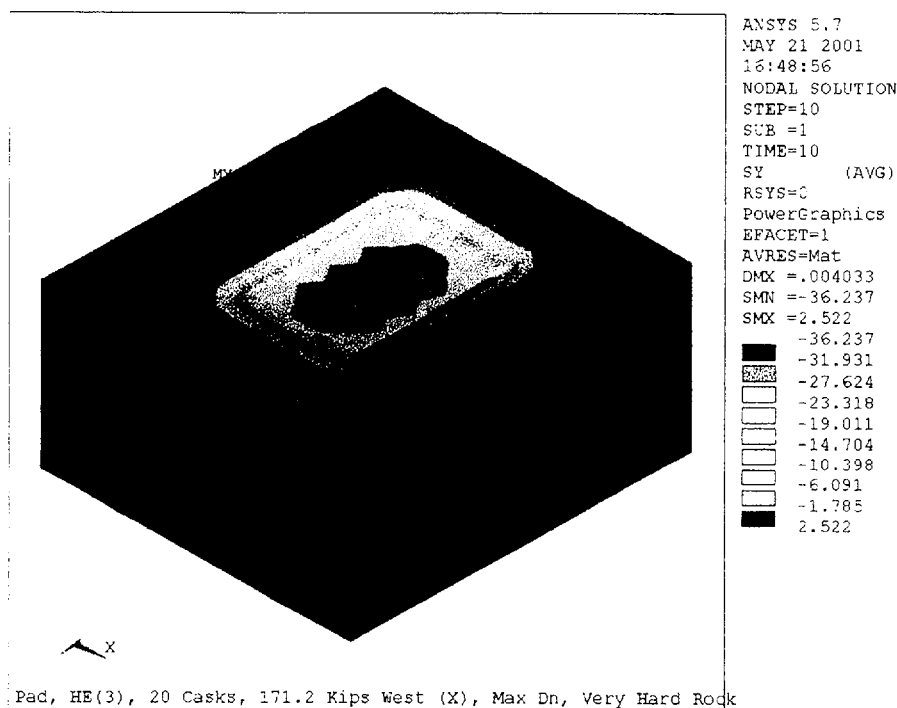


Figure 37 – Rock Y direction stresses for Load Step 10 – Max Down

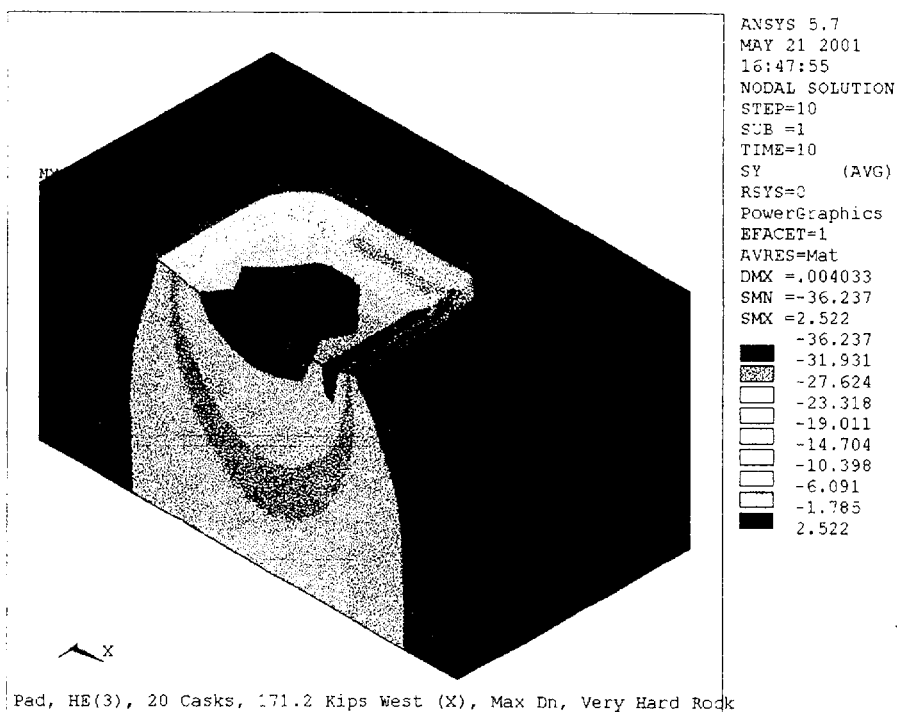
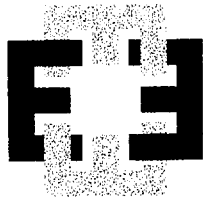


Figure 38 – Rock Y direction stresses, cutaway, Load Step 10 – Max Down



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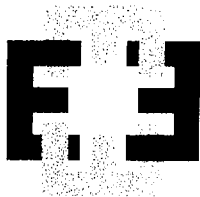
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### **Pad Response at Reduced Concrete Density**

The various design codes and documents require that when dead weight assists in providing resistance to the applied loads, that the structure be assessed assuming that the dead weight is reduced to 90% of its design value (See Reference 9, Section 9.2.3. Reference 8, Table 3-1 requires a reduction to 95%, see definition of D.). In the case of the pad, of course, the dead weight of the pad provides the resistance to lift off during a seismic event. The pad, however, also participates on the demand side of this evaluation. Since the center of gravity of the pad is above the rock, the acceleration of the pad itself will result in an applied moment tending to lift the pad off the rock. However, the pad can have only one density. Therefore, the analysis was rerun for the soft rock model, using a concrete weight density of 135 pcf, which is equal to 90% of 150 pcf. The applied load on the pad along with its resisting effects were both reduced.

Since the relative proportions of response could not be ascertained a priori, both the Hosgri and LTSP loads were applied. These are Load Steps 2 through 6 and 11 through 15, see Tables 2 and 3.

The reaction evaluation is presented in Appendix RL-3, the pad and cask displacements are presented in Appendix DN-5, and the pad X and Z stresses are presented in Appendix SN-3. The results are presented in Table 13 along with the bounding results from the soft rock analyses using normal weight concrete.



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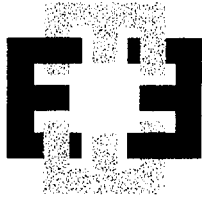
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**Table 13 – MAXIMUM PAD RESPONSES - REDUCED CONCRETE DENSITY  
SOFT ROCK**

LS	EQ	Direction	$\delta_{Max}$	$\delta_{Cask}$	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min
Envelope of 19 Basic Load Cases, normal density see Tables 2 and 3			0.101	0.028	261	-405	270	-410
2	HE(1)	N	0.067	0.00529	46	-106	254	-392
3	HE(1)	N32.93W	0.110	0.0295	141	-262	220	-398
4	HE(1)	N45W	0.112	0.0351	185	-311	196	-368
5	HE(1)	N57.07W	0.105	0.0359	225	-348	166	-320
6	HE(1)	W	0.052	0.0178	247	-393	60	-131
11	L(2)	N	0.054	0.00104	42	-94	245	-366
12	L(2)	N32.93W	0.089	0.0199	131	-244	212	-370
13	L(2)	N45W	0.091	0.0238	176	-290	188	-341
14	L(2)	N57.07W	0.084	0.0243	213	-324	158	-296
15	L(2)	W	0.042	0.0111	240	-365	55	-119

\* Load components are combined using the 40-100-40 rule.

Comparing these results to the normal weight concrete results, the displacements are increased by 10 to 11 percent owing to the reduction in weight holding the pad and casks down. These displacements are, however, still small and acceptable. The stresses are all either the same or slightly lower than those shown in Table 3, since the net horizontal force is reduced. These results clearly show that additional evaluations of this analysis are not warranted and that the postulation of a reduced concrete density to 90 percent of its design value does not present a challenge to the design.



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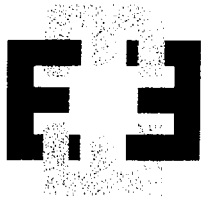
### Pad Response for Cask Placement Sequence

The pad has been analyzed for a cask placement sequence that begins with placing the first cask at the southern most row. Figure 39 shows the placement sequence beginning with cask number 1 and ending with cask number 20. The pad was analyzed for the various cask configurations that will occur through the sequence of placing the casks on the pad. All configurations were analyzed from the placement of cask number 1 to the placement of cask number 14. The remaining configurations, 15 through 19, were not specifically analyzed, since the results clearly show that the pad response approaches that of the fully loaded pad, all 20 casks, asymptotically.

Each configuration was analyzed for the Hosgri HE(1) earthquake aimed at 45 degrees around the compass, since many of the cask placement configurations are not symmetrical. Where symmetrical configurations were encountered, the analysis took advantage of them. Therefore, the analyses are for HE(1) aimed at North, North 45 West, West, South 45 West, South, South 45 East, East, and North 45 East. The pad accelerations were also aimed in the same directions as the loads. The soft rock model was used for analysis since that has been shown to result in the highest displacements and stresses.

The calculations were performed in sets. Thus cask placement sequence 1 through 1 to 6 were analyzed together (42 load steps), 1 to 7 through 1 to 10 (26 load steps), and then 1 to 11 through 1 to 14 (26 load steps). In all, therefore, 94 load steps were analyzed. In order to minimize the volume of paperwork, these three sets were then enveloped to produce a conservative set of response results. The individual load cases were enveloped for maximum responses, which provide the displacements and the maximum positive (tensile) stresses, and they were enveloped for minimum responses, which provide the maximum negative (compressive) stresses. The displacement envelopes are exact, the stress envelopes are either exact or conservative, since ANSYS envelopes the element stresses and then provides nodal average stresses from these.

As an example, take two elements with a node between them. Say for the first load case, the element stresses are 100 and 200, with the nodal average of 150. See Table below. Now, say for the second load case, the element stresses are 150 and 150, with a nodal average of 150. The true envelope of these cases would be a nodal average of 150. However, since ANSYS envelops the element stresses, it will provide an enveloped nodal average of 175.



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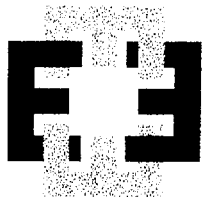
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Load Case	Stress in Element Number 1	Stress in Element Number 2	Nodal Stress
1	100	200	150
2	150	150	150
Envelope using nodal envelope			150
Envelope using element envelope	150	200	175

Obviously, this is a vastly simplified representation of the process ANSYS actually uses since the elements are numerically integrated and the nodal averaging algorithms are much more complex than a simple average, yet the concept presented is accurate. Of course, if the maximum and minimum values are controlled by adjacent elements from the same load case, then the envelope algorithm will provide the exact result.

The reaction calculation is provided in Appendix RL-4, and the enveloping data files are provided in Appendix EN-1. The results are provided in Table 14 below.





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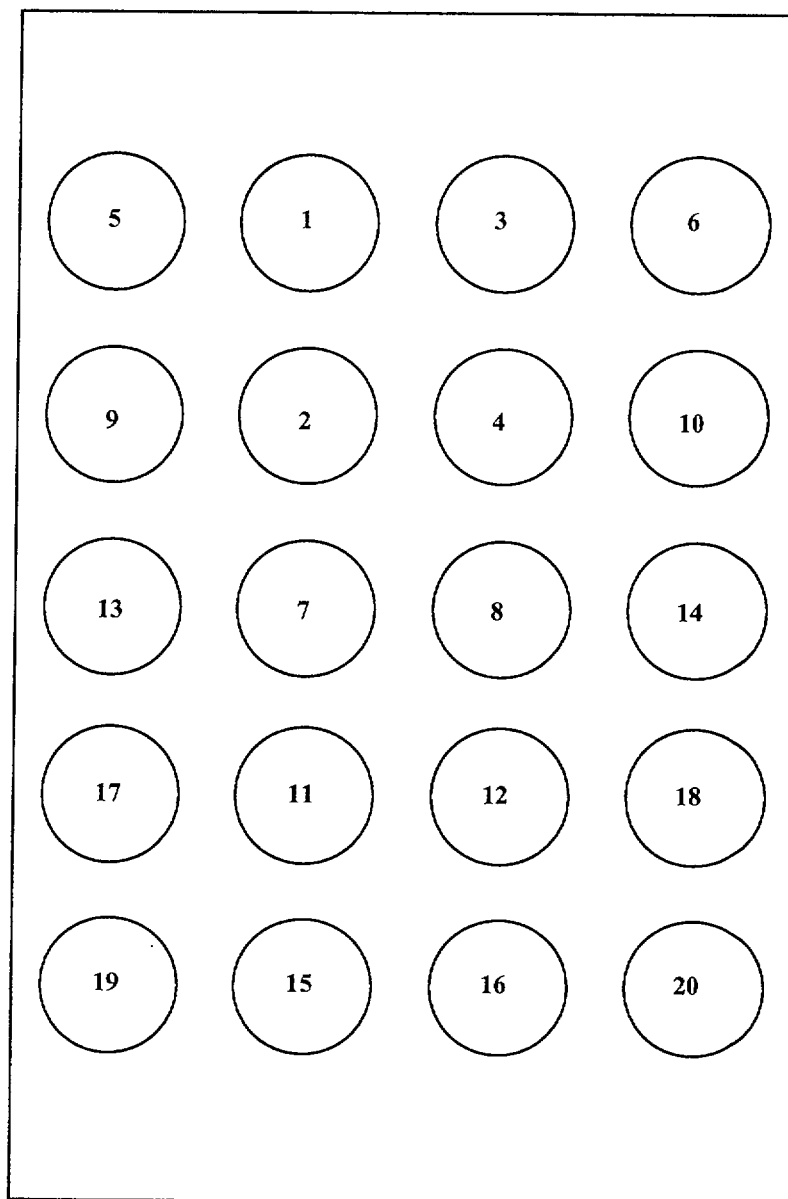
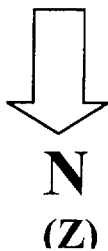
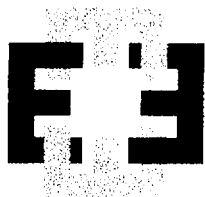


Figure 39 – Cask Placement Sequence



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**Table 14 - CASK PLACEMENT SEQUENCCE  
ENVELOPE OF PAD RESPONSES – SOFT ROCK**

Loads/Rock Characteristics	$\delta_{Max}$	$\delta_{Cask}$	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min
Envelope of 19 Basic Load Cases, see Tables 2 and 3	0.101	0.028	261	-405	270	-410
42 Hosgri Load Cases/Soft Rock/Casks 1 to 1 to 6*	0.035	-0.003	199	-280	163	-243
26 Hosgri Load Cases/Soft Rock/Casks 1 to 7, to 1 to 10**	0.061	0.008	230	-332	199	-295
26 Hosgri Load Cases/Soft Rock/Casks 1 to 11, to 1 to 14***	0.080	0.017	247	-364	237	-337

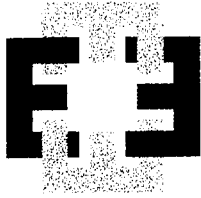
All load components are combined using the 100-40-40 rule.

\* Includes casks placed in sequence 1, 1 and 2, 1 to 3, 1 to 4, 1 to 5 and 1 to 6.

\*\* Includes casks placed in sequence 1 to 7, 1 to 8, 1 to 9 and 1 to 10.

\*\*\* Includes casks placed in sequence 1 to 11, 1 to 12, 1 to 13 and 1 to 14.

The results provided in the Table show that the displacements and stresses for the cases analyzed for the placement sequence configurations described above, are all bounded by the fully loaded analyses (all 20 casks on the pad) previously presented. Thus the results for the fully loaded analyses will be used for concrete section evaluation and reinforcement design, and further consideration of the cask placement sequence results is not warranted.



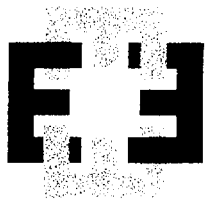
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### Pad Response for Cask Extraction

The pad has been analyzed for a cask extraction event. In this analyses one of the two casks in the middle of the pad is to be removed (extracted), i.e., either cask 7 or 8, either from the North or the South. Due to the symmetry of the pad and the casks, it does not matter whether the cask to be removed is 7 or 8, nor does it matter if either of these is removed from the North or South. In this analysis the cask to be removed is number 7 and it is assumed that it will be removed from the South, hence the analysis was performed with casks 1, 2 and 7 removed, see Figure 40. As with the analyses for the cask placement, this configuration was analyzed for the 8 Hosgri load cases aimed at 45 degrees around the compass, again using the soft rock model.

The reaction results are presented in Appendix RL-5 and the displacement and stress results are shown in Appendix DN-6. The results are tabulated in Table 16 below along with the results for the envelope of the 19 load cases from Tables 2 and 3. And, as with the sequencing calculations, these results show that the cask extraction pad response is bounded by the fully loaded pad response. Therefore, the fully loaded pad response will be used for the design of the pad, and further consideration of the cask extraction pad response is not warranted.



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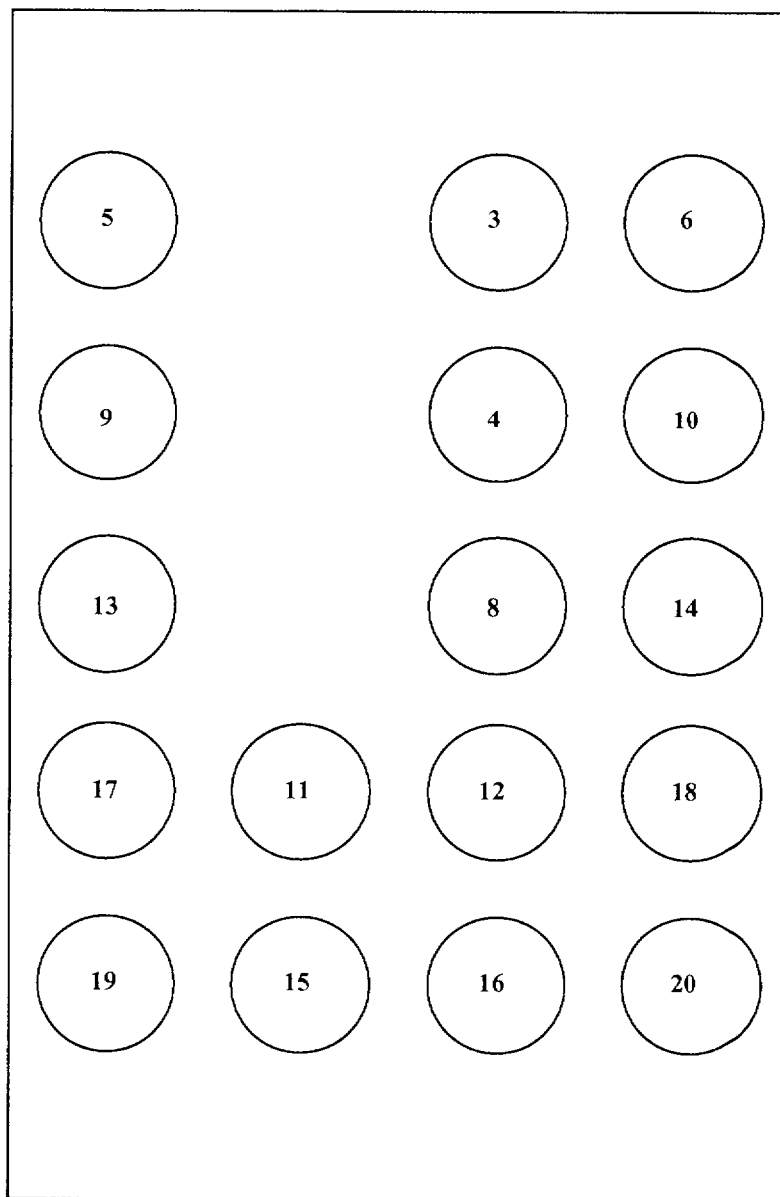
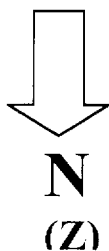
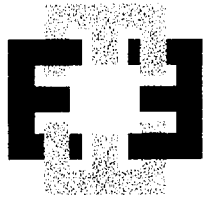


Figure 40 – Cask Extraction



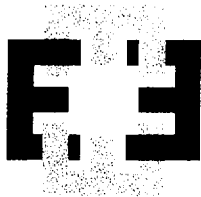
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Table 15 - PAD RESPONSES CASK EXTRACTION  
SOFT ROCK

Direction of Seismic Accel.	$\delta_{Max}$	$\delta_{Cask}$	$\sigma_X$ Max	$\sigma_X$ Min	$\sigma_Z$ Max	$\sigma_Z$ Min
Envelope of 19 Basic Load Cases, see Tables 2 and 3	0.101	0.028	261	-405	270	-410
N Load Step 1	0.040	-0.005	48	-100	257	-373
N 45 W Load Step 2	0.056	0.006	174	-301	201	-344
W Load Step 3	0.039	0.008	246	-366	64	-130
S 45 W Load Step 4	0.086	0.020	169	-277	184	-354
S Load Step 5	0.050	-0.002	48	-108	252	-376
S 45 E Load Step 6	0.088	0.021	168	-277	190	-336
E Load Step 7	0.041	0.010	245	-370	71	-122
N 45 E Load Step 8	0.073	0.014	182	-310	205	-340

All load components are combined using the 100-40-40 rule.



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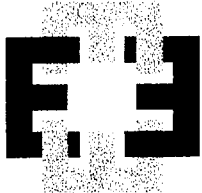
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### Effects of Poisson's Ratio of the Rock

As presented earlier, the lab data for the rock at the site suggests that the Poisson's ratio for the altered sandstone, the "soft rock", may be as low as 0.23, rather than the 0.35 used in the soft rock analyses. Further, the lab data suggests that the Poisson's ratio for the dolomite, the "hard rock", may be as low as 0.22, rather than the 0.35 used in the analyses, and that the Young's modulus may be  $1.3$  to  $1.5 \times 10^6$  psi rather than the  $2.0 \times 10^6$  psi used in the analyses.

The dolomite will be addressed first. The pad was analyzed for "hard rock" using a Young's modulus of  $2.0 \times 10^6$  psi with a Poisson's ratio of 0.35, and for "very hard rock" using a Young's modulus of  $4.9 \times 10^6$  psi with a Poisson's ratio of 0.24. These analyses show that the pad displacements for both are much less than those for the soft rock cases (see Table 2). Further, the stresses for these two cases are quite similar to one another and much less demanding on the pad than stresses from the soft rock analyses (see Tables 3, 4 and 5). Thus for the relatively hard rock cases, the analyses show that the pad responses are both lower than the soft rock responses, and relatively insensitive to the value of Poisson's ratio. Also, the reduction of the Young's modulus for the hard rock is bounded by the soft rock analyses for the Poisson's ratio of 0.35. Further, the reduction of Poisson's ratio for the soft rock is addressed below. Therefore, the reduction of the Young's modulus and Poisson's ratio for the hard rock do not require further analysis.

Concentrating on the effects of the reduction in Poisson's ratio for the soft rock, the pad was reanalyzed for the HE(1) load cases, North, N 45 W and W and the LTSP L(2) load cases North, N 45 W and W for the soft rock with Poisson's ratio of 0.23. The reactions are evaluated in Appendix RL-6. The pad and cask displacements are provided in Appendix DN-7, and the maximum and minimum stresses are provided in Appendix SN-6. The results are compared to the pad results for soft rock with Poisson's ratio of 0.35. The comparisons are tabulated below for the displacements and stresses.



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**Table 16 - SOFT ROCK – COMPARITIVE DISPLACEMENT ANALYSIS**

LS*	EQ	Dir.	$\delta_{Max}$ $v = 0.35$	$\delta_{Max}$ $v = 0.23$	Ratio** 0.23/0.35	$\delta_{Cask}$ $v = 0.35$	$\delta_{Cask}$ $v = 0.23$	Ratio** 0.23/0.35
2/1	HE(1)	N	0.0584	0.0576	0.986	.000451	-.000578	See ***
4/2	HE(1)	N45W	0.1006	0.1023	1.017	0.0271	0.0272	1.004
6/3	HE(1)	W	0.0467	0.0470	1.006	0.0133	0.0127	0.955
11/4	L(2)	N	0.0488	0.0484	0.992	-0.00237	-0.00308	See ***
13/5	L(2)	N45W	0.0832	0.0848	1.019	0.0186	0.0187	1.005
15/6	L(2)	W	0.0387	0.0391	1.010	0.00824	0.00767	See ***

\* LS X/Y where X is the load step from the  $v = 0.35$  analyses and Y is the load step from the  $v = 0.23$  analyses.

\*\* Ratio of the value from the  $v = 0.23$  divided by the value from the  $v = 0.35$  analyses.

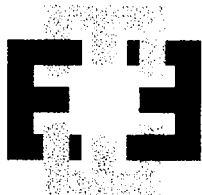
\*\*\* Values are too small for the Ratio to have meaning.

**Table 17 - SOFT ROCK – PAD COMPARITIVE STRESS (SIG X) ANALYSIS**

LS*	EQ	Dir.	$\sigma_X$ Max $v = 0.35$	$\sigma_X$ Max $v = 0.23$	Ratio** 0.23/0.35	$\sigma_X$ Min $v = 0.35$	$\sigma_X$ Min $v = 0.23$	Ratio** 0.23/0.35
2/1	HE(1)	N	45.59	44.63	0.979	-106.68	-139.90	1.311
4/2	HE(1)	N45W	192.06	189.04	0.984	-321.51	-394.56	1.227
6/3	HE(1)	W	260.71	272.47	1.045	-404.71	-460.11	1.137
11/4	L(2)	N	43.57	35.95	0.825	-93.91	-128.78	1.371
13/5	L(2)	N45W	183.34	180.17	0.983	-302.29	-369.68	1.223
15/6	L(2)	W	253.65	263.02	1.037	-378.76	-429.04	1.133

\* LS X/Y where X is the load step from the  $v = 0.35$  analyses and Y is the load step from the  $v = 0.23$  analyses.

\*\* Ratio of the value from the  $v = 0.23$  divided by the value from the  $v = 0.35$  analyses.



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Table 18 - SOFT ROCK – PAD COMPARITIVE STRESS (SIG Z) ANALYSIS

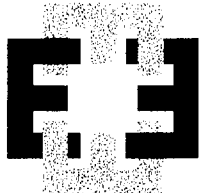
LS*	EQ	Direction	$\sigma_Z$ Max $\nu = 0.35$	$\sigma_Z$ Max $\nu = 0.23$	Ratio** 0.23/0.35	$\sigma_Z$ Min $\nu = 0.35$	$\sigma_Z$ Min $\nu = 0.23$	Ratio** 0.23/0.35
2/1	HE(1)	N	269.97	280.07	1.037	-404.12	-449.39	1.112
4/2	HE(1)	N45W	208.72	222.39	1.065	-378.79	-433.00	1.143
6/3	HE(1)	W	61.87	56.02	0.905	-134.68	-177.74	1.320
11/4	L(2)	N	260.53	269.72	1.035	-380.65	-422.34	1.110
13/5	L(2)	N45W	200.56	213.55	1.065	-353.70	-403.75	1.142
15/6	L(2)	W	56.50	51.16	0.905	-122.82	-162.76	1.325

\* LS X/Y where X is the load step from the  $\nu = 0.35$  analyses and Y is the load step from the  $\nu = 0.23$  analyses.

\*\* Ratio of the value from the  $\nu = 0.23$  divided by the value from the  $\nu = 0.35$  analyses.

The displacements are very well behaved (Table 16) with the maximum pad displacements all within 2% of each other. The stresses, however, show variances of almost 40% in some cases. In order to further assess this sensitivity, the pad internal forces were computed and compared to one another. See Appendix FC-2 for the details of the internal force calculation. Ratios for moment and axial force are computed only for moments greater than 0.1E8. Ratios for all shear forces are computed. The comparisons are made for the North and West analyses, only, since these have resulted in the largest pad responses, see Tables 17 and 18.





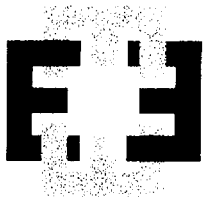
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Table 19 HE (1) NORTH – Z STRIPS INTERNAL FORCES – COMPARATIVE ANALYSIS

Line	Force/Moment	Strip		
		A-B (0.35)	A-B (0.23)	0.23/0.35*
10	Fy	-479342	-486236	1.014
	Fz	984456	1056226	1.073
	Mx	-0.443E8	-0.477E8	1.077
9	Fy	-532371	-579752	1.089
	Fz	941641	986962	1.048
	Mx	-0.197E8	-0.217E8	1.102
8	Fy	-527383	-542959	1.030
	Fz	971263	1008112	
	Mx	4488084	3083858	
7	Fy	-549967	-559467	1.017
	Fz	776479	835299	
	Mx	-900395	-1285165	
6	Fy	-568401	-570592	1.004
	Fz	488622	560207	
	Mx	576226	578436	
5	Fy	-625312	-618684	0.989
	Fz	202111	272231	
	Mx	8951040	8473042	
4	Fy	-731078	-731523	1.001
	Fz	-97229	-73224	0.753
	Mx	0.333E8	0.324E8	0.973
3	Fy	-176465	-176349	0.999
	Fz	-460244	-453476	0.985
	Mx	0.165E8	0.162E8	0.982
2	Fy	-88102	-87845	0.997
	Fz	-528563	-534106	1.010
	Mx	0.242E8	0.245E8	1.012
1	Fy	11602	11345	0.978
	Fz	605828	611371	1.009
	Mx	-0.272E8	-0.274E8	1.007

\* Only ratios of moments greater than 0.1E8 are computed.



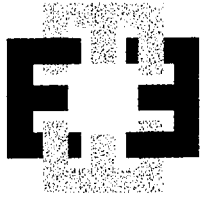
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Table 20 (1/2) HE (1) WEST – X STRIPS INTERNAL FORCES – COMPARATIVE ANALYSIS

Line	Force/Moment	Strip		
		3-4 (0.35)	3-4 (0.23)	0.23/0.35*
E	Fx	793710	888726	1.120
	Fy	-603514	-613179	1.016
	Mz	0.353E8	0.395E8	1.119
D	Fx	439877	489562	1.013
	Fy	-537258	-543989	
	Mz	2676159	3583756	
C	Fx	313732	358032	1.141
	Fy	-533490	-530277	0.994
	Mz	-0.174E8	-0.167E8	0.960
B	Fx	154160	155203	1.007
	Fy	-511333	-511651	1.001
	Mz	-0.449E8	-0.449E8	1.000
A	Fx	439648	449329	1.022
	Fy	28776	28907	1.005
	Mz	0.193E8	0.197E8	1.021

\* Only ratios of moments greater than 0.1E8 are computed.



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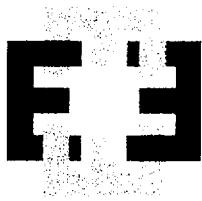
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Table 2- (2/2) HE (1) WEST – X STRIPS INTERNAL FORCES – COMPARATIVE ANALYSIS

Line	Force/Moment	Strip		
		5-6 (0.35)	5-6 (0.23)	0.23/0.35*
E	Fx	886415	989014	1.116
	Fy	-653720	-661832	1.012
	Mz	0.396E8	0.442E8	1.116
D	Fx	442417	497106	1.010
	Fy	-550606	-555914	
	Mz	2533592	3455052	
C	Fx	322227	378021	1.173
	Fy	-547001	-541934	0.991
	Mz	-0.184E8	-0.177E8	0.962
B	Fx	171332	181250	1.058
	Fy	-546142	-544841	0.998
	Mz	-0.481E8	-0.477E8	0.992
A	Fx	471814	474332	1.005
	Fy	14470	14191	0.981
	Mz	0.208E8	0.210E8	1.010

\* Only ratios of moments greater than 0.1E8 are computed.

The tables provide ratios, as before. An examination of this data shows that the internal forces are somewhat better behaved than the stresses, but they still appear to be very sensitive to the value of Poisson's ratio. These ratios are plotted in Figures 41 and 42 below.



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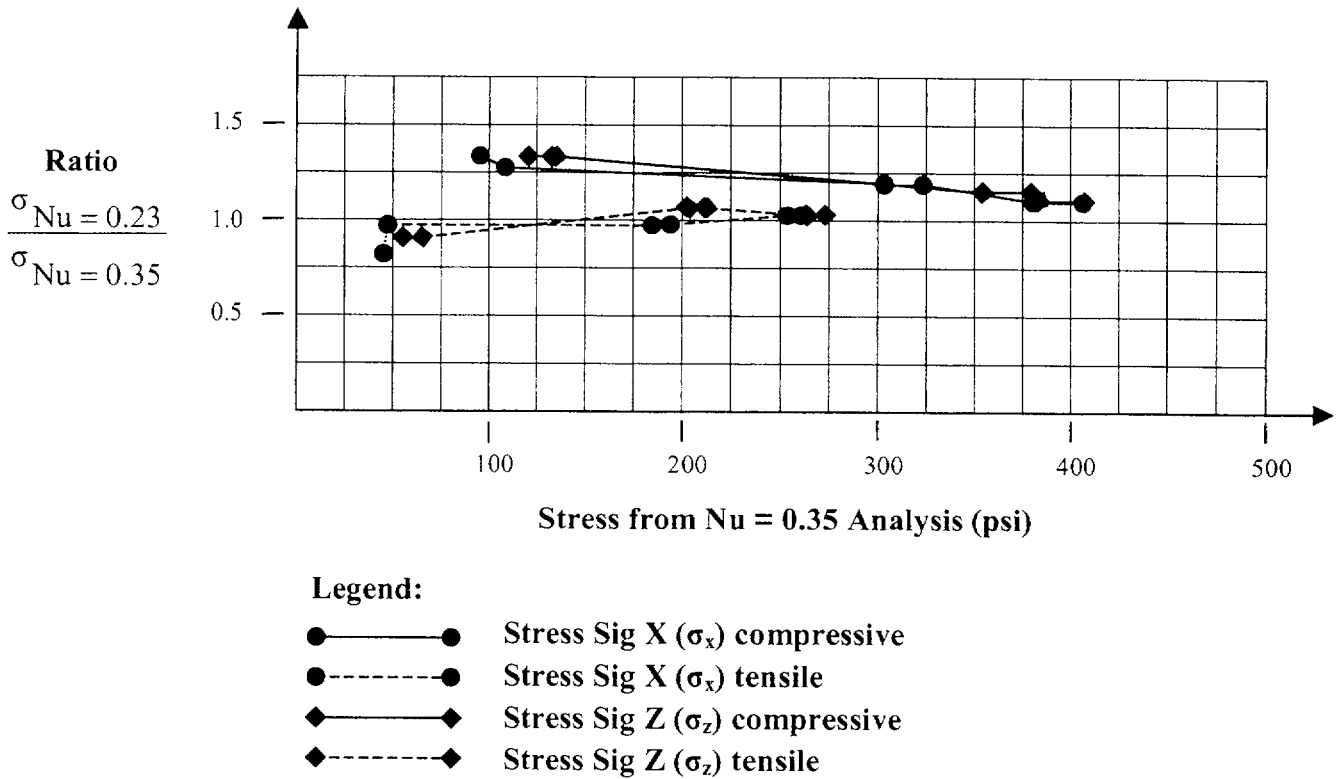
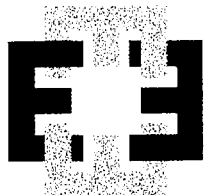


Figure 41 – Plot of Stress Sensitivity to Nu



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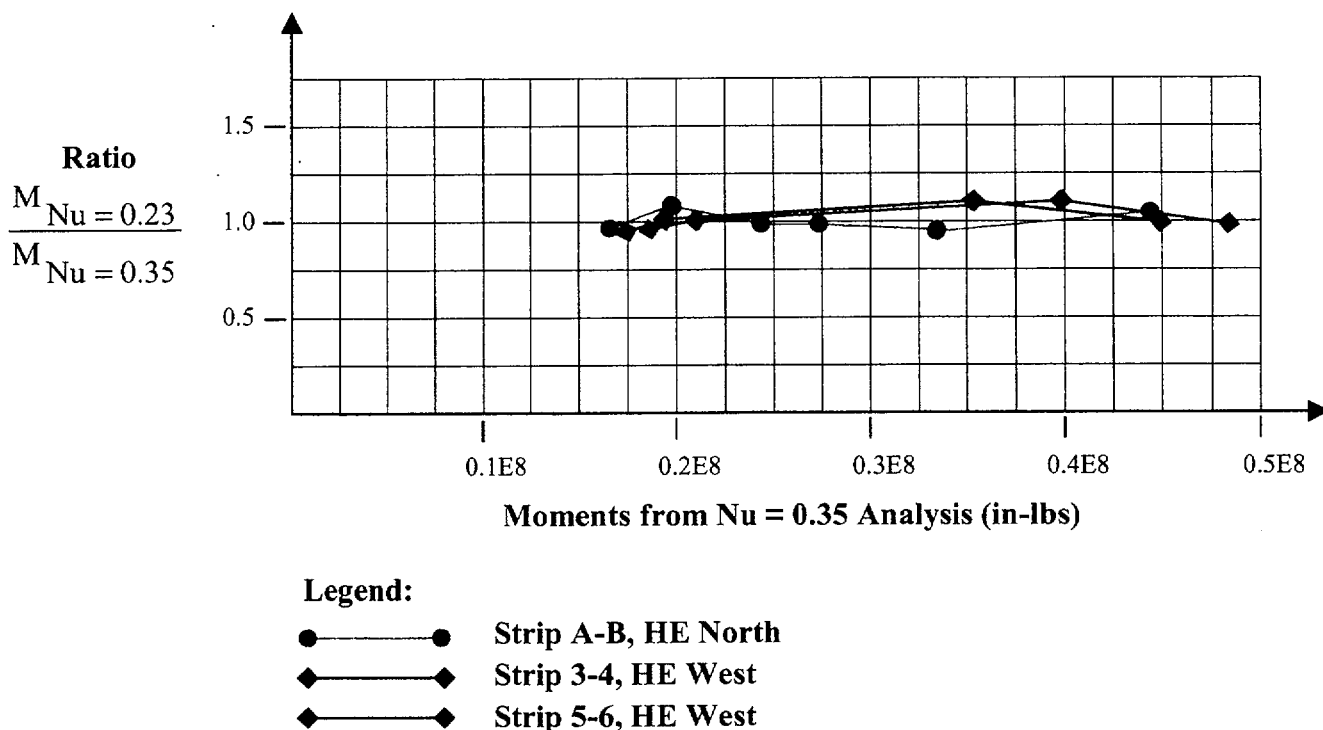
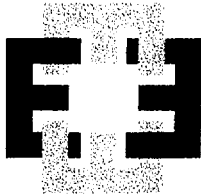


Figure 42 – Plot of Internal Moment Sensitivity to Nu

These plots demonstrate that, generally, as the values of the response parameter become larger, the sensitivity of the value to Poisson's becomes smaller. Referring back to the stress Tables 17 and 18, a close examination of this data shows that the most sensitive stresses are those that are the result of maintaining compatibility between the pad and the rock alone, and not a response that is required to maintain equilibrium to the applied loads. (Such stresses would be referred to as "Secondary Stresses" in ASME analyses.) The most sensitive stresses are the X stresses due to the applied load in the North (Z direction) and the Z stresses due to the applied load in the West (X direction). The sensitivity becomes less for the NW load cases and then less again for those stresses that are required to maintain equilibrium to the applied loads, i.e., X stresses due to W (X) loads, and Z stresses due to N (Z) loads. The ratios for this last class of stress range from a low of 1.110 to a high of 1.137.

The internal force comparisons are only for the internal forces that are required for equilibrium, Z strips for the North (Z) HE(1) and X strips for the West (X) HE(1), and the ratios are only computed for moments that are greater than 0.1E8, i.e., only moments of some significance are examined. These



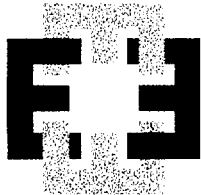
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values are better behaved than the stresses, i.e., all closer to one. The internal forces must sum to provide equilibrium together with the applied loads, which is a condition not imposed on maximum stresses.

The plots and the tables show that the controlling moments are very well behaved, where the ratio for the controlling Mx moment due to the North HE(1) is 1.077 (see Table 19, Strip A-B/Line 10), and the ratios for the controlling Mz moment due to the West HE(1) is 0.992 (see Table 20 (1/2), Strip 5-6/Line B). In most instances, the ratios of the axial forces vary as the moments; see Table 19 A-B/Lines 10,3,2 and 1, and Table 20 (1/2) 3-4, lines E, B and A. In some instances, the axial forces do not exhibit this behavior as in A-B/Line 9 and 3-4/Line C, but the force ratios are all within the range of moment ratios. The shear ratios are very well behaved, most being within 5% of one another, regardless of the variances in moments and axial forces. The ratio for the controlling axial force is 1.001, see A-B, Line 4.

In order to provide conservative values for design, and to provide for variability in Young's modulus and Poisson's ratio presented in the supporting calculations, References 11 and 12, a factor of 1.15 will be applied to all the internal forces presented in Table 11. These factored forces will be used for the pad design.



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### Summary and Conclusions

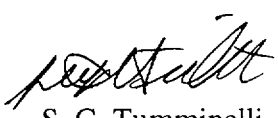
This calculation has presented the results of seismic analyses for the ISFSI storage pad to be installed at the ISFSI site at the Diablo Canyon Power Plant. The pad has been analyzed for a variety of loads taken from the Holtec cask analysis, together with several sets of rock properties identified for the site. These analyses comprise a screening set of analyses that identify that the "soft rock" conditions are the most demanding for the pad. The pad has been shown to respond to the various seismic loads with the specified sets of rock properties with low and acceptable displacements and low stresses. The internal forces computed will be used to size the reinforcing steel and formally evaluate the pad per the applicable Codes and Specifications.

Subsequent to these screening calculations, the pad response was assessed for its seismic response under the following:

- A postulated reduction in density to 90% of its original value.
- Cask placement sequence
- Cask extraction configuration
- Effects of variations in the specified rock parameters

The pad response including the first three effects were all shown to be bounded by the pad response from the soft rock analysis that was part of the screening calculations. The effects of variation of rock parameters resulted in a factor to be applied to the internal forces for the formal Code assessment to be performed in subsequent calculations. The pad displacements for all analyzed conditions and configurations are shown to be small and acceptable. Therefore, the ISFSI storage pad analyzed in this calculation is suitable for use at the Diablo Canyon Power Plant ISFSI site.

Table 11 provides the calculated internal forces and moments resulting from the screening sets of analyses. These values are to be factored up by 1.15 and the resulting forces and moments are to be used to demonstrate compliance with the design Codes and Specifications, and to design the reinforcing steel.

  
Originator: S. C. Tumminelli  
Date: May 25, 2001  
Revised: November 30, 2001

## **Appendix AL-1**

### **Calculation and Application of Loads**

This Appendix presents the calculations for the applied loads, both the specified cask and accelerated pad, for all 19 load cases analyzed for the soft rock, hard rock and very hard rock models.

The description of the loads and their load steps is provided in the body of the calculation. The loads are from Holtec, Reference 4, and the ZPAs are from PG&E, Reference 2.

Following the calculations of the loads, the input files for the soft, hard and very hard rock models are provided. The only difference in the input files is in the title, "Soft" Vs "Hard" Vs "Very Hard".

### **Appendix Contents**

Manual load calculations	sheet 2
ANSYS input file for loads for soft rock model	sheet 8
ANSYS input file for loads for hard rock model	sheet 14
ANSYS input file for loads for very hard rock model	sheet 20





**Below are the calculations for the pad accelerations and the cask loads for each load step:**

Hosgri ZPAs, X, Y and Z are 0.75, 0.50, and 0.75 G.

Combine by 100-40-40 rule:

$$\begin{array}{lll} \text{Horizontal} & = \text{Vector sum } (0.75, 0.4*0.75) & = 0.808\text{G Horizontal} \\ \text{Vertical} & = 0.4*0.50 & = 0.200\text{G Up} \\ \text{Vertical w/gravity} & = 1.00 - 0.20 & = 0.800\text{G Down} \end{array}$$

Combine by 40-100-40 rule:

$$\begin{array}{lll} \text{Horizontal} & = \text{Vector sum } 0.4*(0.75, 0.75) & = 0.424\text{G Horizontal} \\ \text{Vertical} & = 0.50 & = 0.500\text{G Up} \\ \text{Vertical w/gravity} & = 1.00 - 0.50 & = 0.500\text{G Down} \end{array}$$

LTSP ZPAs, X, Y and Z are 0.83, 0.70, and 0.83 G.

Combine by 100-40-40 rule:

$$\begin{array}{lll} \text{Horizontal} & = \text{Vector sum } (0.83, 0.4*0.83) & = 0.894\text{G Horizontal} \\ \text{Vertical} & = 0.4*0.70 & = 0.280\text{G Up} \\ \text{Vertical w/gravity} & = 1.00 - 0.28 & = 0.720\text{G Down} \end{array}$$

Combine by 40-100-40 rule:

$$\begin{array}{lll} \text{Horizontal} & = \text{Vector sum } 0.4*(0.83, 0.83) & = 0.470\text{G Horizontal} \\ \text{Vertical} & = 0.70 & = 0.700\text{G Up} \\ \text{Vertical w/gravity} & = 1.00 - 0.70 & = 0.300\text{G Down} \end{array}$$

Application of Holtec Loads:

Cask weight is always 360 Kip

Hosgri Earthquake, HE, Column 1

$$\begin{array}{ll} \text{Max/Min Vert.} & = 674.2/127.6 \text{ Kip includes gravity} \\ \text{Max Shear} & = 515 \text{ Kip} \end{array}$$

Combine by 100-40-40 rule:

Shear will be = 515 Kip in the specified direction

Adjust vertical load:

$$\text{Maximum Seismic Vertical up} = 360 - 127.6 = 232.4 \text{ Kip Up}$$



$$40\% * \text{Max. Seismic Vertical} = 0.40 * 232.4 = 92.96 \text{ Kip Up}$$

$$\text{Thus, net gravity} + 40\% \text{ Vertical Up} = 360 - 92.96 = 267.04 \text{ Kip Down}$$

Load Step 2 - Apply in the North (Z) direction:

$$F_x = 0$$

$$F_z = 515000$$

$$F_y = -267040$$

$$A_x = 0$$

$$A_y = +0.800G$$

$$A_z = -0.808G$$

Note the order, X, Z and Y for forces and  
x, y, and z for accelerations.

In ANSYS the supports are accelerated into the  
structure. Therefore a +y (up) acceleration is in the  
direction of gravity.

Load Step 3 - Apply in the North 32.93 degrees West direction (see notes LS 2):

$$F_x = 515000 * \sin(32.93) = 279961$$

$$F_z = 515000 * \cos(32.93) = 432258$$

$$F_y = -267040$$

$$A_x = -0.808 * \sin(32.93) = -0.439G$$

$$A_y = 0.800G$$

$$A_z = -0.808 * \cos(32.93) = -0.678G$$

Load Step 4 - Apply in the North 45 degrees West direction (see notes LS 2):

$$F_x = 515000 * \sin(45) = 364160$$

$$F_z = 515000 * \cos(45) = 364160$$

$$F_y = -267040$$

$$A_x = -0.808 * \sin(45) = -0.571G$$

$$A_y = 0.800G$$

$$A_z = -0.808 * \cos(45) = -0.571G$$

Load Step 5 - Apply in the North 57.07 degrees West direction (see notes LS 2):

$$F_x = 515000 * \sin(57.07) = 432258$$

$$F_z = 515000 * \cos(57.07) = 279961$$

$$F_y = -267040$$

$$A_x = -0.808 * \sin(57.07) = -0.678G$$

$$A_y = 0.800G$$

$$A_z = -0.808 * \cos(57.07) = -0.439G$$

Load Step 6 - Apply in the West direction (see notes LS 2):

$$F_x = 515000$$

$$F_z = 0$$

**Appendix AL-1 to Calculation PGE-009-CALC-003**

$$\begin{aligned}F_y &= -267040 \\A_x &= -0.808G \\A_y &= 0.800G \\A_z &= 0\end{aligned}$$

Combine by 40-100-40 rule:

$$\begin{aligned}\text{Shear will be} &= 0.40 \times 515 = 206 \text{ Kip in the specified direction} \\ \text{Maximum Seismic Vertical Down} &= 127.6 \text{ Kip Down}\end{aligned}$$

Load Step 7 - Apply in the North direction (see notes LS 2):

$$\begin{aligned}F_x &= 0 \\F_z &= 206000 \\F_y &= -127600 \\A_x &= 0 \\A_y &= 0.500G \\A_z &= -0.424G\end{aligned}$$

Load Step 8 - Apply in the West direction (see notes LS 2):

$$\begin{aligned}F_x &= 206000 \\F_z &= 0 \\F_y &= -127600 \\A_x &= -0.424G \\A_y &= 0.500G \\A_z &= 0\end{aligned}$$

Hosgri Earthquake, HE, Column 3. This load case has the maximum down load.

$$\begin{aligned}\text{Max/Min Vert.} &= 773.3/130.6 \text{ Kip includes gravity} \\ \text{Max Shear} &= 428 \text{ Kip}\end{aligned}$$

Combine by 40-100-40 rule:

$$\begin{aligned}\text{Shear will be} &= 0.40 \times 428 = 171.2 \text{ Kip in the specified direction} \\ \text{Maximum Seismic Vertical Down} &= 773.3 \text{ Kip Down}\end{aligned}$$

$$\text{Apply maximum vertical down acceleration} = 1.0 + 0.5 = 1.5G$$

Load Step 9 - Apply in the North direction (see notes LS 2):



## Appendix AL-1 to Calculation PGE-009-CALC-003

$$\begin{aligned}
 F_x &= 0 \\
 F_z &= 171200 \\
 F_y &= -773300 \\
 A_x &= 0 \\
 A_y &= 1.500G \\
 A_z &= -0.424G
 \end{aligned}$$

Load Step 10 - Apply in the West direction (see notes LS 2):

$$\begin{aligned}
 F_x &= 171200 \\
 F_z &= 0 \\
 F_y &= -773300 \\
 A_x &= -0.424G \\
 A_y &= 1.500G \\
 A_z &= 0
 \end{aligned}$$

Long Term Seismic Program Earthquake, LTSP, Column 2

$$\begin{aligned}
 \text{Max/Min Vert.} &= 684.1/105.8 \text{ Kip includes gravity} \\
 \text{Max Shear} &= 440 \text{ Kip}
 \end{aligned}$$

Combine by 100-40-40 rule:

$$\begin{aligned}
 \text{Shear will be} &= 440 \text{ Kip in the specified direction} \\
 \text{Adjust vertical load:} & \\
 \text{Maximum Seismic Vertical up} &= 360 - 105.8 = 254.2 \text{ Kip Up} \\
 40\% * \text{Max. Seismic Vertical} &= 0.40 * 254.2 = 101.68 \text{ Kip Up} \\
 \text{Thus, net gravity + 40\% Vertical Up} &= 360 - 101.68 = 258.32 \text{ Kip Down}
 \end{aligned}$$

Load Step 11 - Apply in the North (Z) direction (see notes LS 2):

$$\begin{aligned}
 F_x &= 0 \\
 F_z &= 440000 \\
 F_y &= -258320 \\
 A_x &= 0 \\
 A_y &= +0.720G \\
 A_z &= -0.894G
 \end{aligned}$$

Load Step 12 - Apply in the North 32.93 degrees West direction (see notes LS 2):

$$\begin{aligned}
 F_x &= 440000 * \sin(32.93) &= 239190 \\
 F_z &= 440000 * \cos(32.93) &= 369308 \\
 F_y & &= -258320 \\
 A_x &= -0.894 * \sin(32.93) &= -0.486G
 \end{aligned}$$



$$\begin{aligned}A_y &= 0.720G \\A_z &= -0.894 \cdot \cos(32.93) = -0.750G\end{aligned}$$

Load Step 13 - Apply in the North 45 degrees West direction (see notes LS 2):

$$\begin{aligned}F_x &= 440000 \cdot \sin(45) = 311127 \\F_z &= 440000 \cdot \cos(45) = 311127 \\F_y &= -258320 \\A_x &= -0.894 \cdot \sin(45) = -0.632G \\A_y &= 0.720G \\A_z &= -0.894 \cdot \cos(45) = -0.632G\end{aligned}$$

Load Step 14 - Apply in the North 57.07 degrees West direction (see notes LS 2):

$$\begin{aligned}F_x &= 440000 \cdot \sin(57.07) = 369308 \\F_z &= 440000 \cdot \cos(57.07) = 239190 \\F_y &= -258320 \\A_x &= -0.894 \cdot \sin(57.07) = -0.750G \\A_y &= 0.720G \\A_z &= -0.894 \cdot \cos(57.07) = -0.486G\end{aligned}$$

Load Step 15 - Apply in the West direction (see notes LS 2):

$$\begin{aligned}F_x &= 440000 \\F_z &= 0 \\F_y &= -258320 \\A_x &= -0.894G \\A_y &= 0.720G \\A_z &= 0\end{aligned}$$

Combine by 40-100-40 rule:

$$\begin{aligned}\text{Shear will be} &= 0.40 \cdot 440 = 176 \text{ Kip in the specified direction} \\ \text{Maximum Seismic Vertical Down} &= 105.8 \text{ Kip Down}\end{aligned}$$

Load Step 16 - Apply in the North direction (see notes LS 2):

$$\begin{aligned}F_x &= 0 \\F_z &= 176000 \\F_y &= -105800 \\A_x &= 0 \\A_y &= 0.300G \\A_z &= -0.470G\end{aligned}$$



Load Step 17 - Apply in the West direction (see notes LS 2):

$$\begin{aligned}F_x &= 176000 \\F_z &= 0 \\F_y &= -105800 \\A_x &= -0.470G \\A_y &= 0.300G \\A_z &= 0\end{aligned}$$

Long Term Seismic Program Earthquake, LTSP, Column 4

$$\begin{aligned}\text{Max/Min Vert.} &= 632/55.6 \text{ Kip includes gravity} \\ \text{Max Shear} &= 390 \text{ Kip}\end{aligned}$$

Combine by 40-100-40 rule:

$$\begin{aligned}\text{Shear will be} &= 0.40 \times 390 = 156 \text{ Kip in the specified direction} \\ \text{Maximum Seismic Vertical Down} &= 55.6 \text{ Kip Down}\end{aligned}$$

Load Step 18 - Apply in the North direction (see notes LS 2):

$$\begin{aligned}F_x &= 0 \\F_z &= 156000 \\F_y &= -55600 \\A_x &= 0 \\A_y &= 0.300G \\A_z &= -0.470G\end{aligned}$$

Load Step 19 - Apply in the West direction (see notes LS 2):

$$\begin{aligned}F_x &= 156000 \\F_z &= 0 \\F_y &= -55600 \\A_x &= -0.470G \\A_y &= 0.300G \\A_z &= 0\end{aligned}$$



Following is the ANSYS input file that generates load steps for the soft rock analyses:

```
nall
eall
!
!           "cask" is all 20 casks
!
!           Load Step #1
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, Gravity, 20 Casks, Soft Rock
acel,,386.4
cmsel,s,cask
f,all,fy,-360000*20/1080
nall
eall
lswrite,1
!
!           Load Step #2
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips North (Z), Soft Rock
acel,,0.8*386.4,-0.808*386.4
cmsel,s,cask
f,all,fz,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,2
!
!           Load Step #3
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Soft Rock
acel,-0.439*386.4,0.8*386.4,-0.678*386.4
cmsel,s,cask
f,all,fx,279961*20/1080
f,all,fz,432258*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,3
!
!           Load Step #4
!
lsclear,all
cmsel,s,boundary
```



Appendix AL-1 to Calculation PGE-009-CALC-003

```
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Soft Rock
acel,-0.571*386.4,0.800*386.4,-0.571*386.4
cmsel,s,cask
f,all,fx,364160*20/1080
f,all,fz,364160*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,4
!
!           Load Step #5
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Soft Rock
acel,-0.678*386.4,0.800*386.4,-0.439*386.4
cmsel,s,cask
f,all,fx,432258*20/1080
f,all,fz,279961*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,5
!
!           Load Step #6
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips West (W), Soft Rock
acel,-0.808*386.4,0.800*386.4
cmsel,s,cask
f,all,fx,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,6
!
!           Load Step #7
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Soft Rock
acel,,0.50*386.4,-0.424*386.4
cmsel,s,cask
f,all,fz,206000*20/1080
f,all,fy,-127600*20/1080
nall
eall
lswrite,7
```





Appendix AL-1 to Calculation PGE-009-CALC-003

```
!  
!           Load Step #8  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Soft Rock  
acel,-0.424*386.4,0.500*386.4  
cmsel,s,cask  
f,all,fx,206000*20/1080  
f,all,fy,-127600*20/1080  
nall  
eall  
lswrite,8  
!  
!           Load Step #9  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Soft Rock  
acel,,1.500*386.4,-0.424*386.4  
cmsel,s,cask  
f,all,fz,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,9  
!  
!           Load Step #10  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Soft Rock  
acel,-0.424*386.4,1.50*386.4  
cmsel,s,cask  
f,all,fx,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,10  
!  
!           Load Step #11  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Soft Rock  
acel,,0.72*386.4,-0.894*386.4  
cmsel,s,cask  
f,all,fz,440000*20/1080  
f,all,fy,-258320*20/1080
```

```

na11
eall
lswrite,11
!
!
Load Step #12
!
!
!
lsclear,all
cmse1,s,boundary
d,all,all
/c1tle,pad,LTSP(2),20 Casks,440 Kips N 32.93 W (Z,X),Soft Rock
acel,-0.486*386.4,0.72*386.4,-0.750*386.4
cmse1,s,cask
f,all,fx,239190*20/1080
f,all,fz,369308*20/1080
f,all,fy,-258320*20/1080
na11
eall
lswrite,12
!
!
!
Load Step #13
!
!
!
lsclear,all
cmse1,s,boundary
d,all,all
/c1tle,pad,LTSP(2),20 Casks,440 Kips N 45 W (Z,X),Soft Rock
acel,-0.632*386.4,0.720*386.4,-0.632*386.4
cmse1,s,cask
f,all,fx,311127*20/1080
f,all,fz,311127*20/1080
f,all,fy,-258320*20/1080
na11
eall
lswrite,13
!
!
!
Load Step #14
!
!
!
lsclear,all
cmse1,s,boundary
d,all,all
/c1tle,pad,LTSP(2),20 Casks,440 Kips N 57.03 W (Z,X),Soft Rock
acel,-0.750*386.4,0.72*386.4,-0.486*386.4
cmse1,s,cask
f,all,fx,369308*20/1080
f,all,fz,239190*20/1080
f,all,fy,-258320*20/1080
na11
eall
lswrite,14
!
!
!
Load Step #15
!
!
!
lsclear,all
cmse1,s,boundary

```

**Appendix AL-1 to Calculation PGE-009-CALC-003**

```
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips West (X), Soft Rock
acel,-0.894*386.4,0.720*386.4
cmsel,s,cask
f,all,fx,440000*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,15
!
!           Load Step #16
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Soft Rock
acel,,0.300*386.4,-0.470*386.4
cmsel,s,cask
f,all,fz,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,16
!
!           Load Step #17
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Soft Rock
acel,-0.470*386.4,0.300*386.4
cmsel,s,cask
f,all,fx,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,17
!
!           Load Step #18
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Soft Rock
acel,,0.300*386.4,-0.470*386.4
cmsel,s,cask
f,all,fz,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,18
!
!           Load Step #19
!
```

**ENERCON  
SERVICES, INC.****Appendix AL-1 to Calculation PGE-009-CALC-003**

```
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock
acel,-0.470*386.4,0.300*386.4
cmsel,s,cask
f,all,fx,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,19
!
```



Following is the ANSYS input file that generates load steps for the hard rock analyses:

```
nall
eall
!
!           "cask" is all 20 casks
!
!           Load Step #1
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, Gravity, 20 Casks, Hard Rock
acel,,386.4
cmselect,s,cask
f,all,fy,-360000*20/1080
nall
eall
lswrite,1
!
!           Load Step #2
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips North (Z), Hard Rock
acel,,0.8*386.4,-0.808*386.4
cmselect,s,cask
f,all,fz,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,2
!
!           Load Step #3
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Hard Rock
acel,-0.439*386.4,0.8*386.4,-0.678*386.4
cmselect,s,cask
f,all,fx,279961*20/1080
f,all,fz,432258*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,3
!
!           Load Step #4
!
lsclear,all
cmselect,s,boundary
```



**ENERCON  
SERVICES, INC.**

**Appendix AL-1 to Calculation PGE-009-CALC-003**

```
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Hard Rock
acel,-0.571*386.4,0.800*386.4,-0.571*386.4
cmsel,s,cask
f,all,fx,364160*20/1080
f,all,fz,364160*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,4
!
!           Load Step #5
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Hard Rock
acel,-0.678*386.4,0.800*386.4,-0.439*386.4
cmsel,s,cask
f,all,fx,432258*20/1080
f,all,fz,279961*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,5
!
!           Load Step #6
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips West (W), Hard Rock
acel,-0.808*386.4,0.800*386.4
cmsel,s,cask
f,all,fx,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,6
!
!           Load Step #7
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Hard Rock
acel,,0.50*386.4,-0.424*386.4
cmsel,s,cask
f,all,fz,206000*20/1080
f,all,fy,-127600*20/1080
nall
eall
lswrite,7
```



Appendix AL-1 to Calculation PGE-009-CALC-003

```
!  
!           Load Step #8  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Hard Rock  
acel,-0.424*386.4,0.500*386.4  
cmsel,s,cask  
f,all,fx,206000*20/1080  
f,all,fy,-127600*20/1080  
nall  
eall  
lswrite,8  
!  
!           Load Step #9  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Hard Rock  
acel,,1.500*386.4,-0.424*386.4  
cmsel,s,cask  
f,all,fz,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,9  
!  
!           Load Step #10  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Hard Rock  
acel,-0.424*386.4,1.50*386.4  
cmsel,s,cask  
f,all,fx,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,10  
!  
!           Load Step #11  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Hard Rock  
acel,,0.72*386.4,-0.894*386.4  
cmsel,s,cask  
f,all,fz,440000*20/1080  
f,all,fy,-258320*20/1080
```



**ENERCON  
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**Appendix AL-1 to Calculation PGE-009-CALC-003**

```

nall
eall
lswrite,11
!
!           Load Step #12
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Hard Rock
acel,-0.486*386.4,0.72*386.4,-0.750*386.4
cmsel,s,cask
f,all,fx,239190*20/1080
f,all,fz,369308*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,12
!
!           Load Step #13
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Hard Rock
acel,-0.632*386.4,0.720*386.4,-0.632*386.4
cmsel,s,cask
f,all,fx,311127*20/1080
f,all,fz,311127*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,13
!
!           Load Step #14
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Hard Rock
acel,-0.750*386.4,0.72*386.4,-0.486*386.4
cmsel,s,cask
f,all,fx,369308*20/1080
f,all,fz,239190*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,14
!
!           Load Step #15
!
lsclear,all
cmsel,s,boundary

```





Appendix AL-1 to Calculation PGE-009-CALC-003

```
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips West (X), Hard Rock
acel,-0.894*386.4,0.720*386.4
cmselect,s,cask
f,all,fx,440000*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,15
!
!           Load Step #16
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Hard Rock
acel,,0.300*386.4,-0.470*386.4
cmselect,s,cask
f,all,fz,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,16
!
!           Load Step #17
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Hard Rock
acel,-0.470*386.4,0.300*386.4
cmselect,s,cask
f,all,fx,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,17
!
!           Load Step #18
!
lsclear,all
cmselect,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Hard Rock
acel,,0.300*386.4,-0.470*386.4
cmselect,s,cask
f,all,fz,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,18
!
!           Load Step #19
!
```

**ENERCON  
SERVICES, INC.****Appendix AL-1 to Calculation PGE-009-CALC-003**

```
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Hard Rock
acel,-0.470*386.4,0.300*386.4
cmsel,s,cask
f,all,fx,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,19
!
!
```

Following is the ANSYS input file that generates load steps for the very hard rock analyses:

```
nall
eall
!
!           "cask" is all 20 casks
!
!           Load Step #1
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, Gravity, 20 Casks, Very Hard Rock
acel,,386.4
cmsel,s,cask
f,all,fy,-360000*20/1080
nall
eall
lswrite,1
!
!           Load Step #2
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips North (Z), Very Hard Rock
acel,,0.8*386.4,-0.808*386.4
cmsel,s,cask
f,all,fz,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,2
!
!           Load Step #3
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Very Hard Rock
acel,-0.439*386.4,0.8*386.4,-0.678*386.4
cmsel,s,cask
f,all,fx,279961*20/1080
f,all,fz,432258*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,3
!
!           Load Step #4
!
lsclear,all
cmsel,s,boundary
```



**ENERCON  
SERVICES, INC.**

**Appendix AL-1 to Calculation PGE-009-CALC-003**

```

d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Very Hard Rock
acel,-0.571*386.4,0.800*386.4,-0.571*386.4
cmsel,s,cask
f,all,fx,364160*20/1080
f,all,fz,364160*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,4
!
!           Load Step #5
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Very Hard Rock
acel,-0.678*386.4,0.800*386.4,-0.439*386.4
cmsel,s,cask
f,all,fx,432258*20/1080
f,all,fz,279961*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,5
!
!           Load Step #6
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 515 Kips West (W), Very Hard Rock
acel,-0.808*386.4,0.800*386.4
cmsel,s,cask
f,all,fx,515000*20/1080
f,all,fy,-267040*20/1080
nall
eall
lswrite,6
!
!           Load Step #7
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Very Hard Rock
acel,,0.50*386.4,-0.424*386.4
cmsel,s,cask
f,all,fz,206000*20/1080
f,all,fy,-127600*20/1080
nall
eall
lswrite,7

```



Appendix AL-1 to Calculation PGE-009-CALC-003

```
!  
!           Load Step #8  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Very Hard Rock  
acel,-0.424*386.4,0.500*386.4  
cmsel,s,cask  
f,all,fx,206000*20/1080  
f,all,fy,-127600*20/1080  
nall  
eall  
lswrite,8  
!  
!           Load Step #9  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Very Hard Rock  
acel,,1.500*386.4,-0.424*386.4  
cmsel,s,cask  
f,all,fz,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,9  
!  
!           Load Step #10  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Very Hard Rock  
acel,-0.424*386.4,1.50*386.4  
cmsel,s,cask  
f,all,fx,171200*20/1080  
f,all,fy,-773300*20/1080  
nall  
eall  
lswrite,10  
!  
!           Load Step #11  
!  
lsclear,all  
cmsel,s,boundary  
d,all,all  
/title,Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Very Hard Rock  
acel,,0.72*386.4,-0.894*386.4  
cmsel,s,cask  
f,all,fz,440000*20/1080  
f,all,fy,-258320*20/1080
```



**ENERCON  
SERVICES, INC.**

**Appendix AL-1 to Calculation PGE-009-CALC-003**

```

nall
eall
lswrite,11
!
!           Load Step #12
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Very Hard Rock
acel,-0.486*386.4,0.72*386.4,-0.750*386.4
cmsel,s,cask
f,all,fx,239190*20/1080
f,all,fz,369308*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,12
!
!           Load Step #13
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Very Hard Rock
acel,-0.632*386.4,0.720*386.4,-0.632*386.4
cmsel,s,cask
f,all,fx,311127*20/1080
f,all,fz,311127*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,13
!
!           Load Step #14
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Very Hard Rock
acel,-0.750*386.4,0.72*386.4,-0.486*386.4
cmsel,s,cask
f,all,fx,369308*20/1080
f,all,fz,239190*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,14
!
!           Load Step #15
!
lsclear,all
cmsel,s,boundary

```


```
d,all,all
/title,Pad, LTSP(2), 20 Casks, 440 Kips West (X), Very Hard Rock
acel,-0.894*386.4,0.720*386.4
cmsel,s,cask
f,all,fx,440000*20/1080
f,all,fy,-258320*20/1080
nall
eall
lswrite,15
!
!           Load Step #16
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Very Hard Rock
acel,,0.300*386.4,-0.470*386.4
cmsel,s,cask
f,all,fz,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,16
!
!           Load Step #17
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Very Hard Rock
acel,-0.470*386.4,0.300*386.4
cmsel,s,cask
f,all,fx,176000*20/1080
f,all,fy,-105800*20/1080
nall
eall
lswrite,17
!
!           Load Step #18
!
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Very Hard Rock
acel,,0.300*386.4,-0.470*386.4
cmsel,s,cask
f,all,fz,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,18
!
!           Load Step #19
!
```

**ENERCON  
SERVICES, INC.****Appendix AL-1 to Calculation PGE-009-CALC-003**

```
lsclear,all
cmsel,s,boundary
d,all,all
/title,Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock
acel,-0.470*386.4,0.300*386.4
cmsel,s,cask
f,all,fx,156000*20/1080
f,all,fy,-55600*20/1080
nall
eall
lswrite,19
!
!
```



**ENERCON  
SERVICES, INC.****Appendix DN-1 to Calculation PGE-009-CALC-003**

Originator:  S. C. Tumminelli  
Date: May 25, 2001  
Reissued: November 30, 2001

**Appendix DN-1****Maximum Pad Displacements**

This Appendix presents the maximum displacements of the pad for all 19 load cases analyzed for the soft rock, hard rock and the very hard rock models. The input file is presented followed by the two output files for the soft and hard rock models. The input file scans the two databases in one execution. This is followed by the input and output files for the very hard rock model.

**Appendix Contents**

ANSYS input file for pad displacements for soft and hard rock models	sheet 2
ANSYS output file for the soft rock model	sheet 13
ANSYS output file for the hard rock model	sheet 28
ANSYS input file for pad displacements for the very hard rock model	sheet 43
ANSYS output file for the very hard rock model	sheet 49



Below is the ANSYS input file that scans the database for the maximum pad displacements. Element type 1 is the pad. This file processes that data for both the soft rock and hard rock analyses. Two output files are created.

```
/COM
/OUTPUT,padsoftdisp.out
/com
/COM      DISPLACEMENT DATA SORTED AND PRINTED BY LOAD STEP
/COM
/COM
/COM
/COM      THIS ROUTINE SORTS AND PRINTS DISPLACEMENT DATA BY LOAD STEP
/COM      FOR BOTH THE SOFT AND HARD ROCK MODELS
/COM
/COM
/FILE,DCSLABS2
RESUME
/header,on,off,off,off,on,off
/POST1
/COM
/COM
EALL
NALL
/COM
/COM =====
/COM ===== SET 1 =====
/COM
SET,1
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 2 =====
/COM
SET,2
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
```



Appendix DN-1 to Calculation PGE-009-CALC-003

```
/COM ===== SET 3 =====
/COM
SET, 3
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 4 =====
/COM
SET, 4
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 5 =====
/COM
SET, 5
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 6 =====
/COM
SET, 6
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
```



Appendix DN-1 to Calculation PGE-009-CALC-003

```
NUSORT
/COM
/COM =====
/COM ===== SET 7 =====
/COM
SET, 7
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 8 =====
/COM
SET, 8
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 9 =====
/COM
SET, 9
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 10 =====
/COM
SET, 10
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
```



```
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 11 =====
/COM
SET,11
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 12 =====
/COM
SET,12
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 13 =====
/COM
SET,13
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 14 =====
/COM
SET,14
ESEL,TYPE,1
NELEM
```



Appendix DN-1 to Calculation PGE-009-CALC-003

```
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 15 =====
/COM
SET,15
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 16 =====
/COM
SET,16
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 17 =====
/COM
SET,17
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 18 =====
/COM
```



**ENERCON  
SERVICES, INC.**

**Appendix DN-1 to Calculation PGE-009-CALC-003**

```

SET,18
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 19 =====
/COM
SET,19
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM
/COM
FINISH
/OUTPUT,padharddisp.out
/FILE,DCSLABH2
RESUME
/header,on,off,off,off,on,off
/POST1
/COM
/COM
EALL
NALL
/COM
/COM =====
/COM ===== SET 1 =====
/COM
SET,1
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM

```



```
/COM =====
/COM ===== SET 2 =====
/COM
SET, 2
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 3 =====
/COM
SET, 3
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 4 =====
/COM
SET, 4
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 5 =====
/COM
SET, 5
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
```





ENERCON  
SERVICES, INC.

# Appendix DN-1 to Calculation PGE-009-CALC-003

```

PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 6 =====
/COM
SET,6
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 7 =====
/COM
SET,7
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 8 =====
/COM
SET,8
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 9 =====
/COM
SET,9
ESEL,TYPE,1
NELEM
/COM
/COM =====

```



Appendix DN-1 to Calculation PGE-009-CALC-003

```
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 10 =====
/COM
SET,10
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 11 =====
/COM
SET,11
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 12 =====
/COM
SET,12
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 13 =====
/COM
SET,13
ESEL,TYPE,1
```



ENERCON  
SERVICES, INC.

# Appendix DN-1 to Calculation PGE-009-CALC-003

```

NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 14 =====
/COM
SET,14
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 15 =====
/COM
SET,15
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 16 =====
/COM
SET,16
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 17 =====

```



Appendix DN-1 to Calculation PGE-009-CALC-003

```
/COM
SET, 17
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 18 =====
/COM
SET, 18
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET' 19 =====
/COM
SET, 19
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM
FINI
/OUTPUT
/EXIT
```



Below is the ANSYS output file for the maximum pad displacements for the soft rock analyses:

DISPLACEMENT DATA SORTED AND PRINTED BY LOAD STEP

THIS ROUTINE SORTS AND PRINTS DISPLACEMENT DATA BY LOAD STEP  
FOR BOTH THE SOFT AND HARD ROCK MODELS

CURRENT JOBNAME REDEFINED AS DCSLABS2

RESUME ANSYS DATA FROM FILE NAME=DCSLABS2.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock

ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

15348 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

17051 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabs2

CURRENT JOBNAME = DCSLABS2

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 5.7 \*\*\*\*\*

ANSYS/Structural U

00150104 VERSION=INTEL NT 16:49:39 MAY 17, 2001 CP= 2.454

Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*



Appendix DN-1 to Calculation PGE-009-CALC-003

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY  
ENTER FINISH TO LEAVE POST1

\*\*\* NOTE \*\*\* CP= 2.454 TIME= 16:49:39  
Reading results into the database (SET command) will update the current displacement and force boundary conditions in the database with the values from the results file for that load set. Note that any subsequent solutions will use these values unless action is taken to either SAVE the current values or not overwrite them (/EXIT,NOSAVE).

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

=====

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 4  
TIME/FREQUENCY= 1.0000

TITLE= Pad, Gravity, 20 Casks, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	-0.66050E-03	-0.10190E-01	-0.63869E-03	0.10231E-01
7439	0.66049E-03	-0.10190E-01	-0.63869E-03	0.10231E-01

NODE SORT REMOVED



Appendix DN-1 to Calculation PGE-009-CALC-003

=====

===== SET 2 =====

=====

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17

TIME/FREQUENCY= 2.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM

9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.28909E-02	0.58371E-01	0.24098E-01	0.63216E-01
7439	-0.28909E-02	0.58371E-01	0.24098E-01	0.63216E-01

NODE SORT REMOVED

=====

===== SET 3 =====

=====

USE LOAD STEP 3 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 3 SUBSTEP= 1 CUMULATIVE ITERATION= 26

TIME/FREQUENCY= 3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.



Appendix DN-1 to Calculation PGE-009-CALC-003

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.13572E-01	0.98570E-01	0.21747E-01	0.10185
15453	0.19969E-01	0.97876E-01	0.31920E-01	0.10487

NODE SORT REMOVED

=====

=====	SET 4	=====
-------	-------	-------

=====

USE LOAD STEP 4 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 4 SUBSTEP= 1 CUMULATIVE ITERATION= 30  
TIME/FREQUENCY= 4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.16478E-01	0.10059	0.19540E-01	0.10379
15453	0.24681E-01	0.99877E-01	0.28320E-01	0.10671





Appendix DN-1 to Calculation PGE-009-CALC-003

NODE SORT REMOVED

=====

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 34  
TIME/FREQUENCY= 5.0000  
TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.18842E-01	0.93894E-01	0.16674E-01	0.97207E-01
15453	0.28349E-01	0.93182E-01	0.23602E-01	0.10022

NODE SORT REMOVED

=====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 42  
TIME/FREQUENCY= 6.0000  
TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.



Appendix DN-1 to Calculation PGE-009-CALC-003

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.22263E-01	0.46687E-01	0.51699E-02	0.51981E-01
15363	0.22266E-01	0.46572E-01	-0.51728E-02	0.51880E-01

NODE SORT REMOVED

=====

=====	SET 7	=====
-------	-------	-------

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 54  
TIME/FREQUENCY= 7.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.12943E-02	0.10033E-01	0.11569E-01	0.15368E-01



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# Appendix DN-1 to Calculation PGE-009-CALC-003

7439 -0.12943E-02 0.10033E-01 0.11569E-01 0.15368E-01

NODE SORT REMOVED

=====

===== SET 8 =====

USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 63  
TIME/FREQUENCY= 8.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.10564E-01	0.90342E-02	0.22392E-02	0.14079E-01
15363	0.10564E-01	0.90317E-02	0.22393E-02	0.14078E-01

NODE SORT REMOVED

=====

===== SET 9 =====

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 69  
TIME/FREQUENCY= 9.0000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1



Appendix DN-1 to Calculation PGE-009-CALC-003

```
9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT      ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====
=====          MAXIMUM VALUES OF Uy          =====

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0  KABS= 0  NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE

      NODE      UX      UY      UZ      USUM
15453  0.12601E-02-0.13758E-01 0.14189E-01 0.19804E-01
7449  -0.12599E-02-0.13758E-01 0.14189E-01 0.19804E-01

NODE SORT REMOVED

=====
=====          SET 10          =====

USE LOAD STEP      10  SUBSTEP      0  FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP=      10  SUBSTEP=      1  CUMULATIVE ITERATION=      73
TIME/FREQUENCY= 10.000
TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Soft Rock

ESEL FOR LABEL= TYPE FROM      1 TO      1 BY      1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT      ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====
=====          MAXIMUM VALUES OF Uy          =====

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0  KABS= 0  NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE
```



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# Appendix DN-1 to Calculation PGE-009-CALC-003

NODE	UX	UY	UZ	USUM
15363	0.94049E-02	-0.13706E-01	-0.10578E-02	0.16656E-01
15443	0.94049E-02	-0.13706E-01	-0.10577E-02	0.16656E-01

NODE SORT REMOVED

=====

===== SET 11 =====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 85

TIME/FREQUENCY= 11.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM

9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.27762E-02	0.48794E-01	0.23252E-01	0.54122E-01
7439	-0.27762E-02	0.48794E-01	0.23252E-01	0.54122E-01

NODE SORT REMOVED

=====

===== SET 12 =====

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 94

TIME/FREQUENCY= 12.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Soft Rock



Appendix DN-1 to Calculation PGE-009-CALC-003

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.13264E-01	0.81825E-01	0.21000E-01	0.85512E-01
15453	0.19028E-01	0.81150E-01	0.30368E-01	0.88711E-01

NODE SORT REMOVED

=====

=====	SET 13	=====
-------	--------	-------

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 98  
TIME/FREQUENCY= 13.000  
TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.



Appendix DN-1 to Calculation PGE-009-CALC-003

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.16115E-01	0.83204E-01	0.18824E-01	0.86816E-01
15453	0.23498E-01	0.82509E-01	0.26929E-01	0.89917E-01

NODE SORT REMOVED

=====

===== SET 14 =====

=====

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 102  
TIME/FREQUENCY= 14.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.18441E-01	0.77183E-01	0.15965E-01	0.80946E-01
15453	0.26968E-01	0.76491E-01	0.22417E-01	0.84147E-01

NODE SORT REMOVED

=====

===== SET 15 =====

=====

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 110  
TIME/FREQUENCY= 15.000



Appendix DN-1 to Calculation PGE-009-CALC-003

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.21562E-01	0.38709E-01	0.47068E-02	0.44559E-01
15363	0.21563E-01	0.38699E-01	-0.47073E-02	0.44550E-01

NODE SORT REMOVED

=====

===== SET 16 =====

=====

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 123  
TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2





Appendix DN-1 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.12772E-02	0.22290E-01	0.10659E-01	0.24741E-01
7439	-0.12774E-02	0.22282E-01	0.10659E-01	0.24734E-01

NODE SORT REMOVED

=====

===== SET 17 =====

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 1 CUMULATIVE ITERATION= 136  
TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.99218E-02	0.17631E-01	0.20669E-02	0.20336E-01
15363	0.99230E-02	0.17593E-01	0.20680E-02	0.20304E-01

NODE SORT REMOVED

=====

===== SET 18 =====

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0



Appendix DN-1 to Calculation PGE-009-CALC-003

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 1 CUMULATIVE ITERATION= 151  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.12293E-02	0.25461E-01	0.99999E-02	0.27382E-01
7439	-0.12295E-02	0.25455E-01	0.10000E-01	0.27377E-01

NODE SORT REMOVED

=====

===== SET 19 =====

=====

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 1 CUMULATIVE ITERATION= 168  
TIME/FREQUENCY= 19.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====



Appendix DN-1 to Calculation PGE-009-CALC-003

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.92041E-02	0.22962E-01	0.20536E-02	0.24823E-01
15363	0.92041E-02	0.22960E-01	0.20537E-02	0.24822E-01

NODE SORT REMOVED

=====

EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 49.241

\*\*\* NOTE \*\*\* CP= 49.241 TIME= 16:50:46  
A total of 1 warnings and errors written to dcslabs2.err.

/OUTPUT FILE= padharddisp.out



Below is the ANSYS output file for the maximum pad displacements for the hard rock analyses:

CURRENT JOBNAME REDEFINED AS DCSLABH2

RESUME ANSYS DATA FROM FILE NAME=DCSLABH2.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Hard Rock  
ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

15348 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

17051 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabs2

CURRENT JOBNAME = DCSLABH2

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY

ENTER FINISH TO LEAVE POST1

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

=====

SET 1

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0



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# Appendix DN-1 to Calculation PGE-009-CALC-003

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 2  
TIME/FREQUENCY= 1.0000  
TITLE= Pad, Gravity, 20 Casks, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.79339E-04	-0.94462E-03	0.12113E-03	0.95566E-03
7439	-0.79339E-04	-0.94462E-03	0.12113E-03	0.95566E-03

NODE SORT REMOVED

=====

=====	SET 2	=====
-------	-------	-------

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17  
TIME/FREQUENCY= 2.0000  
TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------



Appendix DN-1 to Calculation PGE-009-CALC-003

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.50071E-03	0.26620E-01	0.18167E-02	0.26687E-01
7439	-0.50071E-03	0.26620E-01	0.18167E-02	0.26687E-01

NODE SORT REMOVED

=====

===== SET 3 =====

=====

USE LOAD STEP 3 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 3 SUBSTEP= 1 CUMULATIVE ITERATION= 30

TIME/FREQUENCY= 3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM

9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y. ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.99650E-03	0.45234E-01	0.17185E-02	0.45278E-01
15453	0.30152E-02	0.45148E-01	0.45525E-02	0.45477E-01

NODE SORT REMOVED

=====

===== SET 4 =====

=====



USE LOAD STEP 4 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 4 SUBSTEP= 1 CUMULATIVE ITERATION= 36  
TIME/FREQUENCY= 4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.11166E-02	0.46181E-01	0.16295E-02	0.46223E-01
15453	0.37418E-02	0.46093E-01	0.39783E-02	0.46416E-01

NODE SORT REMOVED

=====

===== SET 5 =====

=====

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 42  
TIME/FREQUENCY= 5.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====



Appendix DN-1 to Calculation PGE-009-CALC-003

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.12264E-02	0.42812E-01	0.15071E-02	0.42856E-01
15453	0.42545E-02	0.42724E-01	0.32051E-02	0.43055E-01

NODE SORT REMOVED

===== SET 6 =====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 54  
TIME/FREQUENCY= 6.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.17919E-01	0.31514E-01	-0.65700E-04	0.36253E-01
13266	0.17919E-01	0.31514E-01	0.67712E-04	0.36252E-01

NODE SORT REMOVED

===== SET 7 =====





Appendix DN-1 to Calculation PGE-009-CALC-003

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 74  
TIME/FREQUENCY= 7.0000  
TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.25481E-03	0.47173E-02	0.94887E-03	0.48185E-02
7439	-0.25484E-03	0.47147E-02	0.94891E-03	0.48160E-02

NODE SORT REMOVED

=====

===== SET 8 =====

=====

USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 90  
TIME/FREQUENCY= 8.0000  
TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.



=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.60604E-02	0.65000E-02	-0.13646E-04	0.88870E-02
13266	0.60604E-02	0.64998E-02	0.13978E-04	0.88868E-02

NODE SORT REMOVED

=====

===== SET 9 =====

=====

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 95  
TIME/FREQUENCY= 9.0000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15453	0.54805E-03	-0.11026E-02	0.17593E-02	0.21474E-02
7449	-0.54805E-03	-0.11027E-02	0.17593E-02	0.21474E-02

NODE SORT REMOVED



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# Appendix DN-1 to Calculation PGE-009-CALC-003

=====

===== SET 10 =====

=====

USE LOAD STEP 10 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 10 SUBSTEP= 1 CUMULATIVE ITERATION= 99  
TIME/FREQUENCY= 10.000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15363	0.95802E-03	-0.11714E-02	0.48684E-03	0.15896E-02
15443	0.95802E-03	-0.11714E-02	0.48684E-03	0.15896E-02

NODE SORT REMOVED

=====

===== SET 11 =====

=====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 117  
TIME/FREQUENCY= 11.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.



Appendix DN-1 to Calculation PGE-009-CALC-003

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.48347E-03	0.22444E-01	0.17728E-02	0.22519E-01
7439	-0.48347E-03	0.22444E-01	0.17728E-02	0.22519E-01

NODE SORT REMOVED

=====

=====	SET 12	=====
-------	--------	-------

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 130  
TIME/FREQUENCY= 12.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.10159E-02	0.37043E-01	0.16769E-02	0.37095E-01
15453	0.27632E-02	0.36957E-01	0.42179E-02	0.37299E-01



Appendix DN-1 to Calculation PGE-009-CALC-003

NODE SORT REMOVED

=====

===== SET 13 =====

=====

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 135  
TIME/FREQUENCY= 13.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.11463E-02	0.37647E-01	0.15787E-02	0.37698E-01
15453	0.34092E-02	0.37559E-01	0.37021E-02	0.37895E-01

NODE SORT REMOVED

=====

===== SET 14 =====

=====

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 141  
TIME/FREQUENCY= 14.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.



Appendix DN-1 to Calculation PGE-009-CALC-003

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.12607E-02	0.34671E-01	0.14434E-02	0.34724E-01
15453	0.38624E-02	0.34582E-01	0.30058E-02	0.34927E-01

NODE SORT REMOVED

=====

=====	SET 15	=====
-------	--------	-------

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 153  
TIME/FREQUENCY= 15.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.15349E-01	0.23823E-01	0.41179E-04	0.28339E-01



Appendix DN-1 to Calculation PGE-009-CALC-003

13266 0.15349E-01 0.23822E-01 0.42947E-04 0.28339E-01

NODE SORT REMOVED

=====

===== SET 16 =====

=====

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 177  
TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.21940E-03	0.10184E-01	0.81156E-03	0.10218E-01
7439	-0.21941E-03	0.10183E-01	0.81157E-03	0.10218E-01

NODE SORT REMOVED

=====

===== SET 17 =====

=====

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 1 CUMULATIVE ITERATION= 202  
TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1



Appendix DN-1 to Calculation PGE-009-CALC-003

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.66985E-02	0.10288E-01	-0.13515E-04	0.12277E-01
13266	0.66985E-02	0.10288E-01	0.14050E-04	0.12276E-01

NODE SORT REMOVED

=====

=====	SET 18	=====
-------	--------	-------

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 1 CUMULATIVE ITERATION= 227  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE





Appendix DN-1 to Calculation PGE-009-CALC-003

NODE	UX	UY	UZ	USUM
15443	0.20127E-03	0.11268E-01	0.75320E-03	0.11295E-01
7439	-0.20131E-03	0.11261E-01	0.75325E-03	0.11288E-01

NODE SORT REMOVED

=====

===== SET 19 =====

=====

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 1 CUMULATIVE ITERATION= 252  
TIME/FREQUENCY= 19.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.72037E-02	0.14238E-01	-0.23322E-04	0.15956E-01
13266	0.72037E-02	0.14237E-01	0.24307E-04	0.15956E-01

NODE SORT REMOVED

=====

EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 97.380

\*\*\* NOTE \*\*\* CP= 97.380 TIME= 16:51:51



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**Sheet 42 of 63**

**Appendix DN-1 to Calculation PGE-009-CALC-003**

A total of 1 warnings and errors written to dcslabs2.err.

Below is the ANSYS input file that scans the database for the maximum pad displacements. Element type 1 is the pad. This file processes that data for the very hard rock analysis.

```

/COM
/OUTPUT,padvharddisp.out
/com
/COM      DISPLACEMENT DATA SORTED AND PRINTED BY LOAD STEP
/COM
/COM
/COM
/COM      THIS ROUTINE SORTS AND PRINTS DISPLACEMENT DATA BY LOAD STEP
/COM      FOR VERY HARD ROCK MODELS
/COM
/COM
/FILE,DCSLABH6
RESUME
/header,on,off,off,off,on,off
/POST1
/COM
/COM
EALL
NALL
/COM
/COM =====
/COM ===== SET 1 =====
/COM
SET,1
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 2 =====
/COM
SET,2
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 3 =====

```



```
/COM
SET, 3
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 4 =====
/COM
SET, 4
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 5 =====
/COM
SET, 5
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 6 =====
/COM
SET, 6
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
```



```
/COM
/COM =====
/COM ===== SET 7 =====
/COM
SET, 7
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 8 =====
/COM
SET, 8
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 9 =====
/COM
SET, 9
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 10 =====
/COM
SET, 10
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
```



```
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 11 =====
/COM
SET,11
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 12 =====
/COM
SET,12
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 13 =====
/COM
SET,13
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 14 =====
/COM
SET,14
ESEL,TYPE,1
NELEM
/COM
```



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Appendix DN-1 to Calculation PGE-009-CALC-003

```

/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 15 =====
/COM
SET,15
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 16 =====
/COM
SET,16
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 17 =====
/COM
SET,17
ESEL,TYPE,1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT,U,Y,0,0,2,SEL
PRNSOL,U
NUSORT
/COM
/COM =====
/COM ===== SET 18 =====
/COM
SET,18

```



```
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM ===== SET 19 =====
/COM
SET, 19
ESEL, TYPE, 1
NELEM
/COM
/COM =====
/COM ===== MAXIMUM VALUES OF Uy =====
/COM
NSORT, U, Y, 0, 0, 2, SEL
PRNSOL, U
NUSORT
/COM
/COM =====
/COM
/COM
FINISH
/OUTPUT
/EXIT
```





Below is the ANSYS output file for the maximum pad displacements for the very hard rock analyses:

DISPLACEMENT DATA SORTED AND PRINTED BY LOAD STEP

THIS ROUTINE SORTS AND PRINTS DISPLACEMENT DATA BY LOAD STEP  
FOR VERY HARD ROCK MODELS

CURRENT JOBNAME REDEFINED AS DCSLABH6

RESUME ANSYS DATA FROM FILE NAME=DCSLABH6.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock

ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

1728 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

731 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabh6

CURRENT JOBNAME = DCSLABH6

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

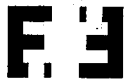
DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 5.7 \*\*\*\*\*

ANSYS/Structural U

00150104 VERSION=INTEL NT 10:27:53 MAY 21, 2001 CP= 4.146

Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock



Appendix DN-1 to Calculation PGE-009-CALC-003

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY  
ENTER FINISH TO LEAVE POST1

\*\*\* NOTE \*\*\* CP= 4.146 TIME= 10:27:53  
Reading results into the database (SET command) will update the current displacement and force boundary conditions in the database with the values from the results file for that load set. Note that any subsequent solutions will use these values unless action is taken to either SAVE the current values or not overwrite them (/EXIT,NOSAVE).

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

=====

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 2  
TIME/FREQUENCY= 1.0000  
TITLE= Pad, Gravity, 20 Casks, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.11611E-03	-0.50355E-03	0.15408E-03	0.53925E-03
7439	-0.11611E-03	-0.50355E-03	0.15408E-03	0.53925E-03

NODE SORT REMOVED



Appendix DN-1 to Calculation PGE-009-CALC-003

=====

SET 2

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17  
TIME/FREQUENCY= 2.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

MAXIMUM VALUES OF Uy

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.18716E-03	0.19824E-01	0.75537E-03	0.19840E-01
7439	-0.18716E-03	0.19824E-01	0.75537E-03	0.19840E-01

NODE SORT REMOVED

=====

SET 3

USE LOAD STEP 3 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 3 SUBSTEP= 1 CUMULATIVE ITERATION= 32  
TIME/FREQUENCY= 3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.



Appendix DN-1 to Calculation PGE-009-CALC-003

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0    KABS= 0    NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.39024E-03	0.34871E-01	0.68632E-03	0.34880E-01
15453	0.18734E-02	0.34831E-01	0.25981E-02	0.34978E-01

NODE SORT REMOVED

=====

=====	SET 4	=====
-------	-------	-------

USE LOAD STEP      4    SUBSTEP      0    FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP=      4    SUBSTEP=      1    CUMULATIVE ITERATION=      39  
TIME/FREQUENCY= 4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM      1 TO      1 BY      1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT      ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0    KABS= 0    NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.44144E-03	0.35672E-01	0.64613E-03	0.35680E-01
15453	0.23948E-02	0.35631E-01	0.21788E-02	0.35778E-01



NODE SORT REMOVED

=====

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 46

TIME/FREQUENCY= 5.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM

9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.49041E-03	0.33141E-01	0.59545E-03	0.33150E-01
15453	0.27571E-02	0.33100E-01	0.16193E-02	0.33254E-01

NODE SORT REMOVED

=====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 58

TIME/FREQUENCY= 6.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.



Appendix DN-1 to Calculation PGE-009-CALC-003

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

	MAXIMUM VALUES OF Uy	
--	----------------------	--

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.13253E-01	0.27089E-01	-0.10759E-03	0.30158E-01
13266	0.13253E-01	0.27089E-01	0.10849E-03	0.30157E-01

NODE SORT REMOVED

=====

	SET 7	
--	-------	--

=====

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 80  
TIME/FREQUENCY= 7.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

	MAXIMUM VALUES OF Uy	
--	----------------------	--

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
------	----	----	----	------



15443 0.10318E-03 0.31833E-02 0.40690E-03 0.32109E-02  
7439 -0.10320E-03 0.31806E-02 0.40691E-03 0.32082E-02

NODE SORT REMOVED

=====

===== SET 8 =====

USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 99  
TIME/FREQUENCY= 8.0000  
TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.41494E-02	0.55875E-02	-0.29945E-04	0.69598E-02
13266	0.41494E-02	0.55875E-02	0.29960E-04	0.69598E-02

NODE SORT REMOVED

=====

===== SET 9 =====

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 103  
TIME/FREQUENCY= 9.0000  
TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1



Appendix DN-1 to Calculation PGE-009-CALC-003

```
9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT      ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====
=====          MAXIMUM VALUES OF Uy          =====

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0  KABS= 0  NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE

      NODE      UX      UY      UZ      USUM
      7449 -0.35038E-03-0.64491E-03 0.93325E-03 0.11873E-02
      15453 0.35038E-03-0.64492E-03 0.93325E-03 0.11873E-02

NODE SORT REMOVED

=====
=====          SET 10          =====

USE LOAD STEP      10  SUBSTEP      0  FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP=      10  SUBSTEP=      1  CUMULATIVE ITERATION=      106
TIME/FREQUENCY= 10.000
TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Very Hard Rock

ESEL FOR LABEL= TYPE FROM      1 TO      1 BY      1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT      ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====
=====          MAXIMUM VALUES OF Uy          =====

SORT ON ITEM=U      COMPONENT=Y      ORDER= 0  KABS= 0  NMAX=      2

SORT COMPLETED FOR      2 VALUES.

PRINT U      NODAL SOLUTION PER NODE
```





NODE	UX	UY	UZ	USUM
15453	0.75154E-03	-0.67112E-03	0.51199E-03	0.11302E-02
15373	0.75131E-03	-0.67317E-03	0.51179E-03	0.11312E-02

NODE SORT REMOVED

=====

===== SET 11 =====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 122  
TIME/FREQUENCY= 11.000  
TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.18080E-03	0.16632E-01	0.73672E-03	0.16650E-01
7439	-0.18080E-03	0.16632E-01	0.73672E-03	0.16650E-01

NODE SORT REMOVED

=====

===== SET 12 =====

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 136  
TIME/FREQUENCY= 12.000  
TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Very Hard Rock



ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

	MAXIMUM VALUES OF Uy	
--	----------------------	--

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.40006E-03	0.28221E-01	0.66923E-03	0.28231E-01
15453	0.16565E-02	0.28180E-01	0.23568E-02	0.28327E-01

NODE SORT REMOVED

=====

	SET 13	
--	--------	--

=====

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 142  
TIME/FREQUENCY= 13.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

	MAXIMUM VALUES OF Uy	
--	----------------------	--

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.



PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.45615E-03	0.28732E-01	0.62523E-03	0.28742E-01
15453	0.21069E-02	0.28691E-01	0.19908E-02	0.28837E-01

NODE SORT REMOVED

=====

===== SET 14 =====

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 149  
TIME/FREQUENCY= 14.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.50798E-03	0.26450E-01	0.56891E-03	0.26461E-01
15453	0.24136E-02	0.26409E-01	0.15048E-02	0.26561E-01

NODE SORT REMOVED

=====

===== SET 15 =====

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 161



Appendix DN-1 to Calculation PGE-009-CALC-003

TIME/FREQUENCY= 15.000  
TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.11119E-01	0.20649E-01	-0.80301E-04	0.23453E-01
13266	0.11119E-01	0.20649E-01	0.81810E-04	0.23452E-01

NODE SORT REMOVED

=====

=====	SET 16	=====
-------	--------	-------

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 186

TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

=====	MAXIMUM VALUES OF Uy	=====
-------	----------------------	-------

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2



Appendix DN-1 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.80410E-04	0.75494E-02	0.33461E-03	0.75572E-02
7439	-0.80410E-04	0.75494E-02	0.33461E-03	0.75572E-02

NODE SORT REMOVED

=====

===== SET 17 =====

=====

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 3 CUMULATIVE ITERATION= 257

TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM

9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.48046E-02	0.88795E-02	-0.30918E-04	0.10096E-01
13266	0.48046E-02	0.88794E-02	0.31071E-04	0.10096E-01

NODE SORT REMOVED

=====

===== SET 18 =====

=====

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0



Appendix DN-1 to Calculation PGE-009-CALC-003

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 3 CUMULATIVE ITERATION= 338  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
15443	0.70791E-04	0.85939E-02	0.30561E-03	0.85996E-02
7439	-0.70794E-04	0.85932E-02	0.30561E-03	0.85989E-02

NODE SORT REMOVED

=====

===== SET 19 =====

=====

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 3 CUMULATIVE ITERATION= 412  
TIME/FREQUENCY= 19.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock

ESEL FOR LABEL= TYPE FROM 1 TO 1 BY 1

9056 ELEMENTS (OF 15348 DEFINED) SELECTED BY ESEL COMMAND.

SELECT ALL NODES HAVING ANY ELEMENT IN ELEMENT SET.

11550 NODES (OF 17051 DEFINED) SELECTED FROM  
9056 SELECTED ELEMENTS BY NELE COMMAND.

=====

===== MAXIMUM VALUES OF Uy =====

=====



SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 2

SORT COMPLETED FOR 2 VALUES.

PRINT U NODAL SOLUTION PER NODE

NODE	UX	UY	UZ	USUM
13267	0.53249E-02	0.12126E-01	-0.38744E-04	0.13244E-01
13266	0.53249E-02	0.12126E-01	0.38799E-04	0.13244E-01

NODE SORT REMOVED


=====

EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 50.813

\*\*\* NOTE \*\*\* CP= 50.813 TIME= 10:29:04  
A total of 1 warnings and errors written to dcslabh6.err.

**ENERCON  
SERVICES, INC.****Appendix DN-2 to Calculation PGE-009-CALC-003**

Originator:   
Date: May 25, 2001  
Reissued: November 30, 2001

**Appendix DN-2****Maximum Cask Displacements**

This Appendix presents the maximum cask displacements for all 19 load cases analyzed for the soft rock, hard rock and very hard models. The first input file creates two output files, one for the soft and one for the hard rock models. This is followed by the input and output files for the very hard rock analyses.

**Appendix Contents**

ANSYS input file for cask displacements for soft and hard rock models	sheet 2
ANSYS output file for the soft rock model	sheet 8
ANSYS output file for the hard rock model	sheet 23
ANSYS input file for cask displacements for the very hard rock model	sheet 37
ANSYS output file for the very hard rock model	sheet 40





Below is the ANSYS input file that scans the database for the maximum cask displacements for the soft and hard rock models. Two output files are created in one execution.

```
/output, padsoftcaskd.out
/com
/file,dcslabs2
resume
/header,on,off,off,off,on,off
/post1
eall
nall
/com,
/com, This routine selects the nodes at the centerlines of the perimeter casks
/com, and prints out the displacements for these nodes for all 19 load steps.
/com,
/COM =====
/COM =====
/COM
/COM ===== SELECT NODES AT THE CL OF THE CASKS =====
/COM
nselect,node,159
nselect,node,3022
nselect,node,3735
nselect,node,4467
nselect,node,5178
nselect,node,5890
nselect,node,6602
nselect,node,8183
nselect,node,11046
nselect,node,11759
nselect,node,12491
nselect,node,13202
nselect,node,13914
nselect,node,14626
/COM =====
/COM =====
/COM ===== SET 1 =====
set,1
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 2 =====
set,2
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 3 =====
set,3
nsort,u,y
prdi
/COM =====
```

**ENERCON  
SERVICES, INC.****Appendix DN-2 to Calculation PGE-009-CALC-003**

```
/COM =====
/COM ===== SET 4 =====
set,4
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 5 =====
set,5
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 6 =====
set,6
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 7 =====
set,7
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 8 =====
set,8
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 9 =====
set,9
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 10 =====
set,10
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 11 =====
set,11
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 12 =====
set,12
nsort,u,y
prdi
```



Appendix DN-2 to Calculation PGE-009-CALC-003

```
/COM =====
/COM =====
/COM ===== SET 13 =====
set,13
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 14 =====
set,14
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 15 =====
set,15
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 16 =====
set,16
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 17 =====
set,17
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 18 =====
set,18
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 19 =====
set,19
nsort,u,y
prdi
/COM =====
/COM =====
fini
/output,padhardcaskd,out
/file,dcslabh2
resume
/header,on,off,off,off,on,off
/post1
eall
nall
/COM =====
```



**ENERCON  
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**Appendix DN-2 to Calculation PGE-009-CALC-003**

```

/COM =====
/COM
/COM ===== SELECT NODES AT THE CL OF THE CASKS =====
/COM
nset,node,159
nset,node,3022
nset,node,3735
nset,node,4467
nset,node,5178
nset,node,5890
nset,node,6602
nset,node,8183
nset,node,11046
nset,node,11759
nset,node,12491
nset,node,13202
nset,node,13914
nset,node,14626
/COM =====
/COM =====
/COM ===== SET 1 =====
set,1
nset,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 2 =====
set,2
nset,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 3 =====
set,3
nset,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 4 =====
set,4
nset,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 5 =====
set,5
nset,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 6 =====
set,6
nset,u,y

```



```
prdi
/COM =====
/COM =====
/COM ===== SET 7 =====
set,7
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 8 =====
set,8
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 9 =====
set,9
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 10 =====
set,10
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 11 =====
set,11
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 12 =====
set,12
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 13 =====
set,13
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 14 =====
set,14
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 15 =====
set,15
```



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Appendix DN-2 to Calculation PGE-009-CALC-003

```

nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 16 =====
set,16
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 17 =====
set,17
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 18 =====
set,18
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 19 =====
set,19
nsort,u,y
prdi
/COM =====
/COM =====
fini
/output
/exit

```



**Below is the ANSYS output file for the maximum cask displacements for the soft rock analyses:**

CURRENT JOBNAME REDEFINED AS dcslabs2

RESUME ANSYS DATA FROM FILE NAME=dcslabs2.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock  
ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

15348 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

17051 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabs2

CURRENT JOBNAME = dcslabs2

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 5.7 \*\*\*\*\*

ANSYS/Structural U

00150104 VERSION=INTEL NT 17:10:19 MAY 17, 2001 CP= 2.464

Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY

ENTER FINISH TO LEAVE POST1

\*\*\* NOTE \*\*\*

CP= 2.474 TIME= 17:10:19

Reading results into the database (SET command) will update the current displacement and force boundary conditions in the database with the values from the results file for that load set. Note that any subsequent solutions will use these values unless action is taken to



Appendix DN-2 to Calculation PGE-009-CALC-003

either SAVE the current values or not overwrite them (/EXIT,NOSAVE).

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

This routine selects the nodes at the centerlines of the perimeter casks  
and prints out the displacements for these nodes for all 19 load steps.

=====

===== SELECT NODES AT THE CL OF THE CASKS =====

NSEL FOR LABEL= NODE FROM 159 TO 159 BY 1  
1 NODES (OF 17051 DEFINED) SELECTED BY NSEL COMMAND.  
NASE FOR LABEL= NODE FROM 3022 TO 3022 BY 1  
2 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 3735 TO 3735 BY 1  
3 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 4467 TO 4467 BY 1  
4 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 5178 TO 5178 BY 1  
5 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 5890 TO 5890 BY 1  
6 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 6602 TO 6602 BY 1  
7 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 8183 TO 8183 BY 1  
8 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 11046 TO 11046 BY 1  
9 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 11759 TO 11759 BY 1





Appendix DN-2 to Calculation PGE-009-CALC-003

10 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 12491 TO 12491 BY 1

11 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 13202 TO 13202 BY 1

12 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 13914 TO 13914 BY 1

13 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 14626 TO 14626 BY 1

14 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

=====

=====

===== SET 1 =====

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 4  
TIME/FREQUENCY= 1.0000

TITLE= Pad, Gravity, 20 Casks, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
11759	0.23976E-02	-0.25934E-01	-0.29898E-02
14626	0.23976E-02	-0.25934E-01	0.29899E-02
6602	-0.23976E-02	-0.25934E-01	0.29899E-02
3735	-0.23976E-02	-0.25934E-01	-0.29899E-02
11046	0.84671E-03	-0.32000E-01	0.33257E-02
8183	0.84671E-03	-0.32000E-01	-0.33257E-02
3022	-0.84672E-03	-0.32000E-01	0.33257E-02
159	-0.84672E-03	-0.32000E-01	-0.33257E-02
12491	0.28853E-02	-0.32324E-01	-0.13605E-02
13914	0.28853E-02	-0.32324E-01	0.13605E-02
4467	-0.28853E-02	-0.32324E-01	-0.13605E-02
5890	-0.28853E-02	-0.32324E-01	0.13605E-02
13202	0.30497E-02	-0.34160E-01	0.38396E-04
5178	-0.30497E-02	-0.34160E-01	0.38396E-04

=====

=====

===== SET 2 =====



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# Appendix DN-2 to Calculation PGE-009-CALC-003

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17  
TIME/FREQUENCY= 2.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.17946E-02	0.45089E-03	0.54158E-01
6602	-0.17946E-02	0.45089E-03	0.54158E-01
11046	0.85672E-03	-0.31840E-02	0.55992E-01
3022	-0.85672E-03	-0.31840E-02	0.55992E-01
13914	0.19712E-02	-0.22290E-01	0.48499E-01
5890	-0.19712E-02	-0.22290E-01	0.48499E-01
11759	0.17184E-02	-0.25651E-01	0.42247E-01
3735	-0.17184E-02	-0.25651E-01	0.42247E-01
13202	0.23280E-02	-0.26958E-01	0.46081E-01
5178	-0.23280E-02	-0.26958E-01	0.46081E-01
12491	0.23114E-02	-0.26967E-01	0.44366E-01
4467	-0.23114E-02	-0.26967E-01	0.44366E-01
8183	0.52785E-03	-0.31633E-01	0.44127E-01
159	-0.52786E-03	-0.31633E-01	0.44127E-01

=====

=====

===== SET 3 =====

USE LOAD STEP 3 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 3 SUBSTEP= 1 CUMULATIVE ITERATION= 26  
TIME/FREQUENCY= 3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.32931E-01	0.22345E-01	0.49506E-01
11046	0.28977E-01	-0.22689E-02	0.47994E-01
13914	0.32714E-01	-0.78650E-02	0.43654E-01
3022	0.25852E-01	-0.12221E-01	0.45401E-01
6602	0.25115E-01	-0.17162E-01	0.41103E-01
13202	0.31900E-01	-0.17466E-01	0.39184E-01
11759	0.26874E-01	-0.18986E-01	0.33611E-01



Appendix DN-2 to Calculation PGE-009-CALC-003

```
12491 0.30241E-01-0.19177E-01 0.36121E-01
8183 0.24738E-01-0.29550E-01 0.36194E-01
3735 0.23030E-01-0.29725E-01 0.36618E-01
5890 0.26047E-01-0.30233E-01 0.39132E-01
159 0.23551E-01-0.31520E-01 0.36962E-01
4467 0.25018E-01-0.32689E-01 0.38083E-01
5178 0.26083E-01-0.33283E-01 0.38630E-01
```

```
=====
=====
===== SET 4 =====
```

USE LOAD STEP 4 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 4 SUBSTEP= 1 CUMULATIVE ITERATION= 30  
TIME/FREQUENCY= 4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS=0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.42876E-01	0.27094E-01	0.42550E-01
13914	0.43340E-01	-0.86190E-04	0.37672E-01
11046	0.37434E-01	-0.50810E-02	0.40415E-01
13202	0.42471E-01	-0.10456E-01	0.33319E-01
12491	0.40105E-01	-0.13431E-01	0.30105E-01
11759	0.35572E-01	-0.14464E-01	0.27648E-01
3022	0.33444E-01	-0.16873E-01	0.37536E-01
6602	0.32449E-01	-0.21741E-01	0.33407E-01
8183	0.32492E-01	-0.28170E-01	0.29960E-01
3735	0.30684E-01	-0.30552E-01	0.31117E-01
159	0.31042E-01	-0.31009E-01	0.30857E-01
5890	0.34396E-01	-0.32432E-01	0.32474E-01
4467	0.33434E-01	-0.34319E-01	0.32305E-01
5178	0.34744E-01	-0.35161E-01	0.32470E-01

```
=====
=====
===== SET 5 =====
```

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 34  
TIME/FREQUENCY= 5.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.



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# Appendix DN-2 to Calculation PGE-009-CALC-003

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.50621E-01	0.28189E-01	0.33449E-01
13914	0.52050E-01	0.70019E-02	0.29670E-01
13202	0.51492E-01	-0.25844E-02	0.25941E-01
12491	0.48736E-01	-0.66512E-02	0.22786E-01
11759	0.43385E-01	-0.87057E-02	0.20437E-01
11046	0.43873E-01	-0.90003E-02	0.31083E-01
3022	0.39220E-01	-0.20944E-01	0.28479E-01
6602	0.38233E-01	-0.25008E-01	0.24915E-01
8183	0.39081E-01	-0.26420E-01	0.22351E-01
159	0.37234E-01	-0.30246E-01	0.23291E-01
3735	0.36981E-01	-0.30957E-01	0.24124E-01
5890	0.41098E-01	-0.34183E-01	0.24554E-01
4467	0.40316E-01	-0.35577E-01	0.25044E-01
5178	0.41761E-01	-0.36683E-01	0.24889E-01

=====

=====

===== SET 6 =====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 42  
TIME/FREQUENCY= 6.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.56712E-01	0.13291E-01	0.46813E-02
11759	0.56703E-01	0.13224E-01	-0.46705E-02
13914	0.61313E-01	0.10306E-01	0.25948E-02
12491	0.61307E-01	0.10278E-01	-0.25853E-02
13202	0.62871E-01	0.93899E-02	0.90377E-04
11046	0.49075E-01	-0.19406E-01	0.31026E-02
8183	0.49062E-01	-0.19435E-01	-0.30942E-02
3022	0.45467E-01	-0.26991E-01	0.19283E-02
159	0.45462E-01	-0.26995E-01	-0.19250E-02
3735	0.45083E-01	-0.29784E-01	0.25944E-03
6602	0.45085E-01	-0.29785E-01	-0.25670E-03
4467	0.49000E-01	-0.36700E-01	0.58681E-03
5890	0.49001E-01	-0.36701E-01	-0.58399E-03
5178	0.50301E-01	-0.38610E-01	-0.26849E-04

=====

=====

===== SET 7 =====



Appendix DN-2 to Calculation PGE-009-CALC-003

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 54  
TIME/FREQUENCY= 7.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.11303E-02	-0.73636E-02	0.21763E-01
6602	-0.11304E-02	-0.73637E-02	0.21763E-01
11046	0.47549E-03	-0.96951E-02	0.22641E-01
3022	-0.47545E-03	-0.96952E-02	0.22641E-01
13914	0.11994E-02	-0.13223E-01	0.20563E-01
5890	-0.11994E-02	-0.13223E-01	0.20563E-01
11759	0.96255E-03	-0.13303E-01	0.18162E-01
3735	-0.96256E-03	-0.13303E-01	0.18162E-01
12491	0.12680E-02	-0.14430E-01	0.19174E-01
4467	-0.12680E-02	-0.14430E-01	0.19174E-01
13202	0.13044E-02	-0.14622E-01	0.19915E-01
5178	-0.13044E-02	-0.14622E-01	0.19915E-01
8183	0.30548E-03	-0.16420E-01	0.18955E-01
159	-0.30549E-03	-0.16420E-01	0.18955E-01

=====  
===== SET 8 =====

USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 63  
TIME/FREQUENCY= 8.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.22906E-01	-0.35240E-02	0.23635E-02
11759	0.22906E-01	-0.35254E-02	0.23634E-02
13914	0.24859E-01	-0.54216E-02	0.12675E-02
12491	0.24859E-01	-0.54221E-02	0.12674E-02
13202	0.25525E-01	-0.59826E-02	0.41558E-04
11046	0.20540E-01	-0.12707E-01	0.16385E-02



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

8183  0.20539E-01-0.12708E-01-0.16386E-02
3022  0.19414E-01-0.14626E-01  0.11071E-02
 159  0.19414E-01-0.14626E-01-0.11071E-02
6602  0.19202E-01-0.14994E-01  0.11472E-03
3735  0.19202E-01-0.14994E-01-0.11467E-03
4467  0.20821E-01-0.18398E-01  0.14698E-03
5890  0.20821E-01-0.18398E-01-0.14694E-03
5178  0.21363E-01-0.19346E-01-0.89786E-05

```

```

=====
=====
===== SET 9 =====
=====

```

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 69  
TIME/FREQUENCY= 9.0000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.43984E-02	-0.45154E-01	0.22838E-01
6602	-0.43979E-02	-0.45154E-01	0.22838E-01
11759	0.42240E-02	-0.48613E-01	0.11576E-01
3735	-0.42236E-02	-0.48613E-01	0.11576E-01
3022	-0.15868E-02	-0.55730E-01	0.24274E-01
11046	0.15871E-02	-0.55730E-01	0.24274E-01
13914	0.52200E-02	-0.58661E-01	0.20060E-01
5890	-0.52195E-02	-0.58661E-01	0.20060E-01
12491	0.52669E-02	-0.59592E-01	0.14930E-01
4467	-0.52665E-02	-0.59592E-01	0.14930E-01
159	-0.14632E-02	-0.59969E-01	0.11769E-01
8183	0.14634E-02	-0.59969E-01	0.11769E-01
13202	0.55591E-02	-0.62611E-01	0.17664E-01
5178	-0.55587E-02	-0.62611E-01	0.17664E-01

```

=====
=====
===== SET 10 =====
=====

```

USE LOAD STEP 10 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 10 SUBSTEP= 1 CUMULATIVE ITERATION= 73  
TIME/FREQUENCY= 10.000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051



Appendix DN-2 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
11759	0.22000E-01	-0.43810E-01	-0.66480E-02
14626	0.22000E-01	-0.43810E-01	0.66477E-02
3735	0.13429E-01	-0.49996E-01	-0.46247E-02
6602	0.13429E-01	-0.49996E-01	0.46245E-02
13914	0.24520E-01	-0.55399E-01	0.31966E-02
12491	0.24520E-01	-0.55399E-01	-0.31968E-02
11046	0.18807E-01	-0.57280E-01	0.65071E-02
8183	0.18807E-01	-0.57280E-01	-0.65074E-02
159	0.15765E-01	-0.58405E-01	-0.60168E-02
3022	0.15765E-01	-0.58405E-01	0.60166E-02
13202	0.25371E-01	-0.58750E-01	0.93299E-04
5890	0.14073E-01	-0.62887E-01	0.19364E-02
4467	0.14073E-01	-0.62887E-01	-0.19366E-02
5178	0.14288E-01	-0.66572E-01	0.48726E-04

=====  
===== SET 11 =====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 85  
TIME/FREQUENCY= 11.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.17323E-02	-0.23658E-02	0.50293E-01
6602	-0.17323E-02	-0.23658E-02	0.50293E-01
11046	0.80541E-03	-0.58241E-02	0.52049E-01
3022	-0.80541E-03	-0.58241E-02	0.52049E-01
13914	0.18807E-02	-0.21356E-01	0.45457E-01
5890	-0.18807E-02	-0.21356E-01	0.45457E-01
11759	0.15520E-02	-0.23307E-01	0.39923E-01
3735	-0.15520E-02	-0.23307E-01	0.39923E-01
12491	0.21362E-02	-0.24868E-01	0.41876E-01
4467	-0.21362E-02	-0.24868E-01	0.41876E-01
13202	0.21764E-02	-0.25123E-01	0.43435E-01
5178	-0.21764E-02	-0.25123E-01	0.43435E-01
8183	0.47436E-03	-0.28766E-01	0.41701E-01
159	-0.47437E-03	-0.28766E-01	0.41701E-01

=====  
=====



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# Appendix DN-2 to Calculation PGE-009-CALC-003

===== SET 12 =====

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 94  
TIME/FREQUENCY= 12.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.30100E-01	0.14871E-01	0.45855E-01
11046	0.26623E-01	-0.53918E-02	0.44546E-01
13914	0.29993E-01	-0.10246E-01	0.40573E-01
3022	0.23928E-01	-0.13070E-01	0.42312E-01
6602	0.23254E-01	-0.16598E-01	0.38441E-01
13202	0.29513E-01	-0.17505E-01	0.36744E-01
11759	0.25157E-01	-0.17595E-01	0.31741E-01
12491	0.28166E-01	-0.18329E-01	0.34051E-01
3735	0.21717E-01	-0.26893E-01	0.34570E-01
8183	0.23261E-01	-0.27009E-01	0.34198E-01
5890	0.24259E-01	-0.27970E-01	0.36797E-01
159	0.22200E-01	-0.28675E-01	0.34914E-01
4467	0.23458E-01	-0.29847E-01	0.35901E-01
5178	0.24371E-01	-0.30569E-01	0.36398E-01

=====

===== SET 13 =====

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 98  
TIME/FREQUENCY= 13.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.39168E-01	0.18624E-01	0.39440E-01
13914	0.39657E-01	-0.40683E-02	0.34968E-01
11046	0.34406E-01	-0.78550E-02	0.37514E-01
13202	0.39086E-01	-0.11980E-01	0.31185E-01
12491	0.37134E-01	-0.13796E-01	0.28312E-01





Appendix DN-2 to Calculation PGE-009-CALC-003

```
11759 0.33151E-01-0.13931E-01 0.26023E-01
3022 0.31024E-01-0.16985E-01 0.35024E-01
6602 0.30150E-01-0.20443E-01 0.31312E-01
8183 0.30488E-01-0.25881E-01 0.28287E-01
3735 0.28878E-01-0.27636E-01 0.29374E-01
159 0.29214E-01-0.28250E-01 0.29144E-01
5890 0.32060E-01-0.29835E-01 0.30552E-01
4467 0.31314E-01-0.31272E-01 0.30445E-01
5178 0.32450E-01-0.32187E-01 0.30591E-01
```

```
=====
=====
===== SET 14 =====
```

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 102  
TIME/FREQUENCY= 14.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.46150E-01	0.19220E-01	0.31143E-01
13914	0.47481E-01	0.12160E-02	0.27580E-01
13202	0.47174E-01	0.61747E-02	0.24179E-01
12491	0.44920E-01	0.85505E-02	0.21285E-01
11759	0.40276E-01	0.92223E-02	0.19114E-01
11046	0.40288E-01	0.11067E-01	0.28955E-01
3022	0.36457E-01	0.20131E-01	0.26701E-01
6602	0.35649E-01	0.23092E-01	0.23419E-01
8183	0.36584E-01	0.24456E-01	0.21072E-01
159	0.34985E-01	0.27616E-01	0.21997E-01
3735	0.34745E-01	0.28016E-01	0.22774E-01
5890	0.38323E-01	0.31305E-01	0.23124E-01
4467	0.37717E-01	0.32377E-01	0.23597E-01
5178	0.38982E-01	0.33499E-01	0.23452E-01

```
=====
=====
===== SET 15 =====
```

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 110  
TIME/FREQUENCY= 15.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051



Appendix DN-2 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.52118E-01	0.82447E-02	0.45791E-02
11759	0.52117E-01	0.82391E-02	0.45780E-02
13914	0.56185E-01	0.48365E-02	0.25176E-02
12491	0.56185E-01	0.48343E-02	0.25169E-02
13202	0.57567E-01	0.37824E-02	0.84124E-04
11046	0.45613E-01	0.18894E-01	0.29519E-02
8183	0.45612E-01	0.18896E-01	0.29514E-02
3022	0.42584E-01	0.24949E-01	0.18120E-02
159	0.42584E-01	0.24949E-01	0.18117E-02
3735	0.42254E-01	0.27103E-01	0.26235E-03
6602	0.42254E-01	0.27103E-01	0.26204E-03
4467	0.45800E-01	0.33426E-01	0.54395E-03
5890	0.45800E-01	0.33426E-01	0.54365E-03
5178	0.46983E-01	0.35177E-01	0.26233E-04

=====  
===== SET 16 =====

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 123  
TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.74511E-03	-0.52798E-03	0.22797E-01
6602	-0.74452E-03	-0.53313E-03	0.22796E-01
11046	0.35204E-03	-0.20036E-02	0.23587E-01
3022	-0.35087E-03	-0.20057E-02	0.23587E-01
13914	0.77917E-03	-0.88488E-02	0.20644E-01
5890	-0.77888E-03	-0.88498E-02	0.20643E-01
3735	-0.61210E-03	-0.95070E-02	0.18262E-01
11759	0.61219E-03	-0.95070E-02	0.18262E-01
4467	-0.87549E-03	-0.10207E-01	0.19087E-01
12491	0.87563E-03	-0.10207E-01	0.19087E-01
13202	0.89858E-03	-0.10405E-01	0.19758E-01
5178	-0.89839E-03	-0.10405E-01	0.19758E-01
159	-0.18296E-03	-0.11748E-01	0.19082E-01
8183	0.18305E-03	-0.11748E-01	0.19082E-01

=====



Appendix DN-2 to Calculation PGE-009-CALC-003

=====

SET 17

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 1 CUMULATIVE ITERATION= 136  
TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.23426E-01	0.40128E-02	0.20481E-02
11759	0.23423E-01	0.39923E-02	0.20448E-02
13914	0.25147E-01	0.24083E-02	0.11242E-02
12491	0.25145E-01	0.23999E-02	0.11214E-02
13202	0.25732E-01	0.19068E-02	0.38583E-04
11046	0.20620E-01	0.77241E-02	0.12615E-02
8183	0.20617E-01	0.77314E-02	0.12598E-02
3022	0.19311E-01	0.10294E-01	0.72565E-03
159	0.19310E-01	0.10295E-01	0.72479E-03
3735	0.19174E-01	0.11206E-01	0.21338E-03
6602	0.19175E-01	0.11206E-01	0.21256E-03
4467	0.20721E-01	0.13785E-01	0.28117E-03
5890	0.20722E-01	0.13786E-01	0.28034E-03
5178	0.21240E-01	0.14501E-01	0.12425E-04

=====

SET 18

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 1 CUMULATIVE ITERATION= 151  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.57828E-03	0.27135E-02	0.22021E-01
6602	-0.57788E-03	0.27095E-02	0.22021E-01
11046	0.28774E-03	0.16475E-02	0.22736E-01
3022	-0.28687E-03	0.16458E-02	0.22736E-01



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

13914  0.56408E-03-0.63085E-02  0.19783E-01
5890   -0.56394E-03-0.63096E-02  0.19783E-01
3735   -0.45481E-03-0.75670E-02  0.17565E-01
11759  0.45485E-03-0.75670E-02  0.17565E-01
4467   -0.67289E-03-0.78619E-02  0.18241E-01
12491  0.67296E-03-0.78619E-02  0.18241E-01
13202  0.68024E-03-0.79638E-02  0.18833E-01
5178   -0.68016E-03-0.79640E-02  0.18833E-01
159    -0.12879E-03-0.93626E-02  0.18367E-01
8183   0.12884E-03-0.93626E-02  0.18367E-01

```

```

=====
=====
===== SET 19 =====
=====

```

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 1 CUMULATIVE ITERATION= 168  
TIME/FREQUENCY= 19.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Soft Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.23333E-01	0.98912E-02	0.15722E-02
11759	0.23333E-01	0.98899E-02	0.15721E-02
13914	0.24984E-01	0.92044E-02	0.89434E-03
12491	0.24984E-01	0.92038E-02	0.89419E-03
13202	0.25553E-01	0.89742E-02	0.30929E-04
11046	0.20392E-01	0.43832E-02	0.91735E-03
8183	0.20392E-01	0.43839E-02	0.91730E-03
3022	0.18749E-01	0.80209E-02	0.44415E-03
159	0.18749E-01	0.80210E-02	0.44412E-03
6602	0.18557E-01	0.92607E-02	0.41629E-03
3735	0.18557E-01	0.92607E-02	0.41634E-03
5890	0.20032E-01	0.11186E-01	0.35996E-03
4467	0.20032E-01	0.11186E-01	0.36001E-03
5178	0.20526E-01	0.11717E-01	0.14496E-04

EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 44.594

\*\*\* NOTE \*\*\* CP= 44.594 TIME= 17:11:21



A total of 1 warnings and errors written to dcslabs2.err.

/OUTPUT FILE= padhardcaskd.out



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# Appendix DN-2 to Calculation PGE-009-CALC-003

Below is the ANSYS output file for the maximum cask displacements for the hard rock analyses:

CURRENT JOBNAME REDEFINED AS dcslabh2

RESUME ANSYS DATA FROM FILE NAME=dcslabh2.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Hard Rock

ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

9056 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

11550 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabs2

CURRENT JOBNAME = dcslabh2

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY

ENTER FINISH TO LEAVE POST1

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

=====

===== SELECT NODES AT THE CL OF THE CASKS =====

NSEL FOR LABEL= NODE FROM 159 TO 159 BY 1

1 NODES (OF 17051 DEFINED) SELECTED BY NSEL COMMAND.



Appendix DN-2 to Calculation PGE-009-CALC-003

NASE FOR LABEL= NODE FROM 3022 TO 3022 BY 1  
2 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 3735 TO 3735 BY 1  
3 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 4467 TO 4467 BY 1  
4 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 5178 TO 5178 BY 1  
5 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 5890 TO 5890 BY 1  
6 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 6602 TO 6602 BY 1  
7 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 8183 TO 8183 BY 1  
8 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 11046 TO 11046 BY 1  
9 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 11759 TO 11759 BY 1  
10 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 12491 TO 12491 BY 1  
11 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 13202 TO 13202 BY 1  
12 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 13914 TO 13914 BY 1  
13 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 14626 TO 14626 BY 1  
14 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

=====



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# Appendix DN-2 to Calculation PGE-009-CALC-003

=====

===== SET 1 =====

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 2  
TIME/FREQUENCY= 1.0000

TITLE= Pad, Gravity, 20 Casks, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
11759	0.44504E-03	-0.29552E-02	-0.52675E-03
3735	-0.44504E-03	-0.29552E-02	-0.52675E-03
14626	0.44504E-03	-0.29552E-02	0.52675E-03
6602	-0.44504E-03	-0.29552E-02	0.52675E-03
12491	0.53987E-03	-0.35662E-02	-0.22916E-03
13914	0.53987E-03	-0.35662E-02	0.22916E-03
4467	-0.53987E-03	-0.35662E-02	-0.22916E-03
5890	-0.53987E-03	-0.35662E-02	0.22916E-03
8183	0.14819E-03	-0.36065E-02	-0.59842E-03
159	-0.14819E-03	-0.36065E-02	-0.59842E-03
11046	0.14819E-03	-0.36065E-02	0.59842E-03
3022	-0.14819E-03	-0.36065E-02	0.59842E-03
13202	0.56911E-03	-0.37223E-02	0.27296E-05
5178	-0.56911E-03	-0.37223E-02	0.27296E-05

=====

===== SET 2 =====

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17  
TIME/FREQUENCY= 2.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.44006E-03	0.48840E-02	0.11349E-01
6602	-0.44006E-03	0.48840E-02	0.11349E-01
3022	-0.22353E-03	0.43763E-02	0.11865E-01
11046	0.22353E-03	0.43763E-02	0.11865E-01





Appendix DN-2 to Calculation PGE-009-CALC-003

```
13914  0.41936E-03-0.23911E-02  0.76633E-02
5890   -0.41936E-03-0.23911E-02  0.76633E-02
13202  0.39762E-03-0.28811E-02  0.68058E-02
5178   -0.39762E-03-0.28811E-02  0.68058E-02
12491  0.30625E-03-0.30795E-02  0.61932E-02
4467   -0.30625E-03-0.30795E-02  0.61932E-02
3735   -0.16636E-03-0.31492E-02  0.53467E-02
11759  0.16636E-03-0.31492E-02  0.53467E-02
8183   0.37567E-04-0.38261E-02  0.59486E-02
159    -0.37567E-04-0.38261E-02  0.59486E-02
```

```
=====
=====
===== SET 3 =====
```

USE LOAD STEP        3    SUBSTEP        0    FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP=        3    SUBSTEP=        1    CUMULATIVE ITERATION=        30  
TIME/FREQUENCY=    3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Hard Rock

SORT ON ITEM=U        COMPONENT=Y        ORDER= 0    KABS= 0    NMAX=    17051

SORT COMPLETED FOR        14 VALUES.

PRINT DOF    NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.86533E-02	0.15392E-01	0.11312E-01
11046	0.61468E-02	0.45843E-02	0.10317E-01
13914	0.76855E-02	0.30527E-02	0.82487E-02
3022	0.44425E-02	0.85221E-03	0.87102E-02
13202	0.64891E-02-0.28510E-03	0.62057E-02	
6602	0.40611E-02-0.91220E-03	0.68442E-02	
12491	0.55280E-02-0.11787E-02	0.52614E-02	
11759	0.41555E-02-0.19328E-02	0.44723E-02	
5890	0.39022E-02-0.33013E-02	0.58076E-02	
3735	0.31665E-02-0.35752E-02	0.46795E-02	
8183	0.34331E-02-0.35756E-02	0.49151E-02	
5178	0.39076E-02-0.36086E-02	0.56498E-02	
4467	0.36995E-02-0.37299E-02	0.53345E-02	
159	0.32519E-02-0.37609E-02	0.50107E-02	

```
=====
=====
===== SET 4 =====
```

USE LOAD STEP        4    SUBSTEP        0    FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP=        4    SUBSTEP=        1    CUMULATIVE ITERATION=        36  
TIME/FREQUENCY=    4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Hard Rock



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# Appendix DN-2 to Calculation PGE-009-CALC-003

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.11532E-01	0.17918E-01	0.94753E-02
13914	0.10923E-01	0.71096E-02	0.72918E-02
11046	0.79286E-02	0.33469E-02	0.83738E-02
13202	0.97055E-02	0.29816E-02	0.55847E-02
12491	0.82830E-02	0.10972E-02	0.46767E-02
11759	0.61874E-02-0.58991E-03	0.40080E-02	
3022	0.55114E-02-0.82137E-03	0.66374E-02	
6602	0.48707E-02-0.20356E-02	0.50061E-02	
8183	0.46628E-02-0.34002E-02	0.41188E-02	
5890	0.51738E-02-0.35451E-02	0.47105E-02	
3735	0.42201E-02-0.36380E-02	0.39985E-02	
159	0.43279E-02-0.36649E-02	0.42020E-02	
5178	0.52444E-02-0.38312E-02	0.47219E-02	
4467	0.49611E-02-0.39040E-02	0.45359E-02	

=====

=====

===== SET 5 =====

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 42

TIME/FREQUENCY= 5.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.13635E-01	0.18574E-01	0.69278E-02
13914	0.13595E-01	0.10908E-01	0.56655E-02
13202	0.12657E-01	0.70651E-02	0.45683E-02
12491	0.11029E-01	0.43538E-02	0.39170E-02
11046	0.90694E-02	0.16715E-02	0.59644E-02
11759	0.84107E-02	0.15312E-02	0.34458E-02
3022	0.61582E-02-0.21273E-02	0.44883E-02	
6602	0.54205E-02-0.27157E-02	0.33974E-02	
8183	0.58293E-02-0.31613E-02	0.31438E-02	
159	0.52484E-02-0.35372E-02	0.31900E-02	
3735	0.50973E-02-0.36452E-02	0.31234E-02	
5890	0.61778E-02-0.37496E-02	0.34782E-02	
5178	0.63276E-02-0.40149E-02	0.35974E-02	
4467	0.60013E-02-0.40298E-02	0.35307E-02	



Appendix DN-2 to Calculation PGE-009-CALC-003

=====  
=====  
===== SET 6 =====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 54  
TIME/FREQUENCY= 6.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.16666E-01	0.14469E-01	-0.34315E-05
13914	0.16039E-01	0.13838E-01	-0.18673E-04
12491	0.16037E-01	0.13833E-01	0.20862E-04
14626	0.14012E-01	0.12263E-01	0.40789E-05
11759	0.14010E-01	0.12250E-01	-0.19132E-05
11046	0.87344E-02	-0.15701E-02	0.36581E-03
8183	0.87310E-02	-0.15755E-02	-0.36392E-03
3022	0.66937E-02	-0.30590E-02	0.26933E-03
159	0.66930E-02	-0.30593E-02	-0.26897E-03
3735	0.63030E-02	-0.33831E-02	0.78972E-04
6602	0.63033E-02	-0.33831E-02	-0.78826E-04
4467	0.73771E-02	-0.40973E-02	0.13031E-03
5890	0.73773E-02	-0.40973E-02	-0.13013E-03
5178	0.76785E-02	-0.42722E-02	-0.67806E-05

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=====  
===== SET 7 =====

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 74  
TIME/FREQUENCY= 7.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.27107E-03	-0.29874E-03	0.35288E-02
6602	-0.27085E-03	-0.29975E-03	0.35284E-02
11046	0.11385E-03	-0.58232E-03	0.37713E-02



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

3022 -0.11363E-03-0.58305E-03 0.37711E-02
13914 0.25855E-03-0.14222E-02 0.29719E-02
5890 -0.25849E-03-0.14222E-02 0.29718E-02
13202 0.23895E-03-0.15700E-02 0.28410E-02
5178 -0.23892E-03-0.15700E-02 0.28410E-02
11759 0.11971E-03-0.16125E-02 0.22651E-02
3735 -0.11971E-03-0.16125E-02 0.22651E-02
12491 0.19358E-03-0.16402E-02 0.26244E-02
4467 -0.19357E-03-0.16402E-02 0.26244E-02
8183 0.31759E-04-0.19612E-02 0.25213E-02
159 -0.31753E-04-0.19612E-02 0.25213E-02

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===== SET 8 =====

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USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 90  
TIME/FREQUENCY= 8.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.55527E-02	0.15566E-02	0.19105E-05
13914	0.53149E-02	0.14344E-02	0.10176E-03
12491	0.53144E-02	0.14334E-02	0.10138E-03
14626	0.45390E-02	0.11493E-02	0.20775E-03
11759	0.45384E-02	0.11469E-02	0.20770E-03
11046	0.30803E-02	0.14531E-02	0.25409E-03
8183	0.30800E-02	0.14532E-02	0.25407E-03
159	0.27005E-02	0.16478E-02	0.18127E-03
3022	0.27006E-02	0.16478E-02	0.18129E-03
3735	0.25711E-02	0.17114E-02	0.21453E-04
6602	0.25711E-02	0.17114E-02	0.21468E-04
4467	0.30031E-02	0.20613E-02	0.29735E-04
5890	0.30031E-02	0.20613E-02	0.29713E-04
5178	0.31250E-02	0.21484E-02	0.22772E-05

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=====
===== SET 9 =====

```

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 95  
TIME/FREQUENCY= 9.0000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Hard Rock



Appendix DN-2 to Calculation PGE-009-CALC-003

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.85853E-03	-0.50733E-02	0.31954E-02
6602	-0.85849E-03	-0.50733E-02	0.31954E-02
3735	-0.72388E-03	-0.56299E-02	0.12086E-02
11759	0.72393E-03	-0.56299E-02	0.12086E-02
3022	-0.29435E-03	-0.61940E-02	0.35791E-02
11046	0.29436E-03	-0.61940E-02	0.35791E-02
5890	-0.10019E-02	-0.64380E-02	0.28171E-02
13914	0.10020E-02	-0.64381E-02	0.28171E-02
4467	-0.93981E-03	-0.66215E-02	0.19603E-02
12491	0.93988E-03	-0.66215E-02	0.19603E-02
5178	-0.10275E-02	-0.68044E-02	0.24590E-02
13202	0.10276E-02	-0.68044E-02	0.24590E-02
159	-0.23559E-03	-0.68595E-02	0.13290E-02
8183	0.23560E-03	-0.68595E-02	0.13290E-02

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=====  
===== SET 10 =====

USE LOAD STEP 10 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 10 SUBSTEP= 1 CUMULATIVE ITERATION= 99

TIME/FREQUENCY= 10.000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
11759	0.31324E-02	-0.49924E-02	-0.11529E-02
14626	0.31324E-02	-0.49924E-02	-0.11529E-02
3735	0.15533E-02	-0.57097E-02	-0.82886E-03
6602	0.15533E-02	-0.57097E-02	-0.82886E-03
12491	0.37034E-02	-0.60852E-02	-0.53025E-03
13914	0.37034E-02	-0.60852E-02	-0.53025E-03
13202	0.38701E-02	-0.63638E-02	-0.67922E-05
8183	0.25623E-02	-0.64697E-02	-0.11669E-02
11046	0.25623E-02	-0.64697E-02	-0.11669E-02
159	0.20330E-02	-0.65833E-02	-0.10813E-02
3022	0.20330E-02	-0.65833E-02	-0.10813E-02
4467	0.17653E-02	-0.69733E-02	-0.32533E-03
5890	0.17653E-02	-0.69733E-02	-0.32533E-03



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# Appendix DN-2 to Calculation PGE-009-CALC-003

5178 0.18208E-02-0.72913E-02 0.78036E-06

=====

=====

===== SET 11 =====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 117

TIME/FREQUENCY= 11.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.43451E-03	0.35457E-02	0.10113E-01
6602	-0.43451E-03	0.35457E-02	0.10113E-01
3022	-0.21571E-03	0.30388E-02	0.10606E-01
11046	0.21571E-03	0.30388E-02	0.10606E-01
13914	0.40268E-03	-0.22879E-02	0.70331E-02
5890	-0.40268E-03	-0.22879E-02	0.70331E-02
13202	0.37430E-03	-0.26908E-02	0.63400E-02
5178	-0.37430E-03	-0.26908E-02	0.63400E-02
12491	0.28597E-03	-0.28465E-02	0.57939E-02
4467	-0.28597E-03	-0.28465E-02	0.57939E-02
11759	0.14707E-03	-0.28640E-02	0.50202E-02
3735	-0.14707E-03	-0.28640E-02	0.50202E-02
8183	0.32083E-04	-0.34801E-02	0.55898E-02
159	-0.32083E-04	-0.34801E-02	0.55898E-02

=====

=====

===== SET 12 =====

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 130

TIME/FREQUENCY= 12.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.74655E-02	0.11385E-01	0.10000E-01
11046	0.52963E-02	0.28351E-02	0.91236E-02



Appendix DN-2 to Calculation PGE-009-CALC-003

```
13914 0.66108E-02 0.15523E-02 0.72545E-02
3022 0.39163E-02 0.16551E-03 0.77803E-02
13202 0.56828E-02-0.73379E-03 0.56403E-02
6602 0.36032E-02-0.10915E-02 0.61883E-02
12491 0.49381E-02-0.13321E-02 0.48642E-02
11759 0.37852E-02-0.18550E-02 0.41427E-02
5890 0.35537E-02-0.30563E-02 0.53754E-02
3735 0.29569E-02-0.32391E-02 0.43842E-02
8183 0.31939E-02-0.32654E-02 0.46020E-02
5178 0.35864E-02-0.33247E-02 0.52582E-02
4467 0.34173E-02-0.34145E-02 0.49787E-02
159 0.30411E-02-0.34247E-02 0.46973E-02
=====
=====
===== SET 13 =====
```

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 135  
TIME/FREQUENCY= 13.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

```
      NODE      UX      UY      UZ
14626 0.99213E-02 0.13312E-01 0.84233E-02
13914 0.93705E-02 0.45863E-02 0.64131E-02
11046 0.68159E-02 0.18082E-02 0.74145E-02
13202 0.84059E-02 0.16506E-02 0.50015E-02
12491 0.72982E-02 0.40148E-03 0.42418E-02
11759 0.55619E-02-0.77833E-03 0.36418E-02
3022 0.49029E-02-0.11347E-02 0.59663E-02
6602 0.43842E-02-0.19827E-02 0.45891E-02
8183 0.43125E-02-0.31183E-02 0.38410E-02
5890 0.47235E-02-0.32652E-02 0.43754E-02
3735 0.39298E-02-0.32962E-02 0.37435E-02
159 0.40347E-02-0.33429E-02 0.39340E-02
5178 0.48118E-02-0.35181E-02 0.43971E-02
4467 0.45763E-02-0.35668E-02 0.42313E-02
=====
=====
===== SET 14 =====
```

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 141  
TIME/FREQUENCY= 14.000



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# Appendix DN-2 to Calculation PGE-009-CALC-003

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.11709E-01	0.13734E-01	0.62366E-02
13914	0.11657E-01	0.74399E-02	0.50067E-02
13202	0.10915E-01	0.46812E-02	0.40272E-02
12491	0.96310E-02	0.28662E-02	0.34583E-02
11759	0.74689E-02	0.88278E-03	0.30256E-02
11046	0.77869E-02	0.47801E-03	0.53126E-02
3022	0.55284E-02	-0.21242E-02	0.40975E-02
6602	0.49452E-02	-0.25219E-02	0.31580E-02
8183	0.53505E-02	-0.29219E-02	0.29062E-02
159	0.48768E-02	-0.32338E-02	0.29787E-02
3735	0.47341E-02	-0.33053E-02	0.29199E-02
5890	0.56500E-02	-0.34414E-02	0.32409E-02
4467	0.55277E-02	-0.36777E-02	0.32899E-02
5178	0.58033E-02	-0.36780E-02	0.33508E-02

=====

=====

===== SET 15 =====

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 153

TIME/FREQUENCY= 15.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.14234E-01	0.98995E-02	0.94289E-06
13914	0.13716E-01	0.95040E-02	0.11255E-03
12491	0.13715E-01	0.94986E-02	-0.11085E-03
14626	0.12021E-01	0.86057E-02	0.26152E-03
11759	0.12019E-01	0.85957E-02	-0.26085E-03
11046	0.75962E-02	-0.18932E-02	0.42316E-03
8183	0.75930E-02	-0.18982E-02	-0.42272E-03
3022	0.61231E-02	-0.28288E-02	0.27196E-03
159	0.61226E-02	-0.28290E-02	-0.27185E-03
3735	0.57977E-02	-0.30846E-02	0.62826E-04
6602	0.57978E-02	-0.30846E-02	-0.62749E-04
4467	0.67544E-02	-0.37403E-02	0.11280E-03





Appendix DN-2 to Calculation PGE-009-CALC-003

5890 0.67545E-02-0.37403E-02-0.11269E-03  
5178 0.70241E-02-0.39013E-02-0.62817E-05

=====  
=====  
===== SET 16 =====

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 177  
TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.18872E-03	0.16731E-02	0.45534E-02
6602	-0.18863E-03	0.16727E-02	0.45534E-02
11046	0.94550E-04	0.14543E-02	0.47766E-02
3022	-0.94464E-04	0.14542E-02	0.47766E-02
13914	0.16789E-03	-0.94657E-03	0.31735E-02
5890	-0.16788E-03	-0.94661E-03	0.31734E-02
13202	0.15350E-03	-0.11165E-02	0.28603E-02
5178	-0.15349E-03	-0.11165E-02	0.28603E-02
12491	0.11352E-03	-0.11731E-02	0.26209E-02
4467	-0.11352E-03	-0.11731E-02	0.26209E-02
11759	0.50243E-04	-0.11732E-02	0.22852E-02
3735	-0.50242E-04	-0.11732E-02	0.22852E-02
8183	0.91003E-05	-0.14256E-02	0.25471E-02
159	-0.90989E-05	-0.14256E-02	0.25471E-02

=====  
=====  
===== SET 17 =====

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 1 CUMULATIVE ITERATION= 202  
TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.62262E-02	0.43516E-02	0.10994E-05



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

13914  0.60143E-02  0.42101E-02  0.68834E-04
12491  0.60140E-02  0.42085E-02-0.68377E-04
14626  0.53207E-02  0.39055E-02  0.15066E-03
11759  0.53203E-02  0.39028E-02-0.15052E-03
11046  0.34235E-02-0.73990E-03  0.18635E-03
 8183  0.34227E-02-0.74124E-03-0.18624E-03
 3022  0.27621E-02-0.11706E-02  0.10885E-03
  159  0.27620E-02-0.11707E-02-0.10883E-03
 6602  0.26105E-02-0.12778E-02-0.42183E-04
 3735  0.26105E-02-0.12778E-02  0.42202E-04
 5890  0.30224E-02-0.15467E-02-0.54679E-04
 4467  0.30223E-02-0.15467E-02  0.54708E-04
 5178  0.31391E-02-0.16129E-02-0.28808E-05

```

```

=====
=====
===== SET 18 =====
=====

```

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 1 CUMULATIVE ITERATION= 227  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

```

      NODE      UX      UY      UZ
14626  0.16024E-03  0.25386E-02  0.45834E-02
 6602 -0.15990E-03  0.25339E-02  0.45829E-02
11046  0.87071E-04  0.23424E-02  0.47898E-02
 3022 -0.85705E-04  0.23397E-02  0.47899E-02
13914  0.12673E-03-0.63955E-03  0.31237E-02
 5890 -0.12696E-03-0.64126E-03  0.31225E-02
 5178 -0.11447E-03-0.85343E-03  0.27327E-02
13202  0.11452E-03-0.85344E-03  0.27328E-02
 4467 -0.78738E-04-0.90759E-03  0.25022E-02
12491  0.78772E-04-0.90759E-03  0.25022E-02
 3735 -0.24962E-04-0.94112E-03  0.22010E-02
11759  0.24979E-04-0.94112E-03  0.22011E-02
  159 -0.96546E-06-0.11443E-02  0.24550E-02
 8183  0.98444E-06-0.11443E-02  0.24550E-02

```

```

=====
=====
===== SET 19 =====
=====

```

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 1 CUMULATIVE ITERATION= 252



Appendix DN-2 to Calculation PGE-009-CALC-003

TIME/FREQUENCY= 19.000  
TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Hard Rock  
SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051  
SORT COMPLETED FOR 14 VALUES.  
PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.67677E-02	0.74629E-02	-0.16855E-05
13914	0.65405E-02	0.71864E-02	-0.43871E-04
12491	0.65400E-02	0.71835E-02	0.44795E-04
14626	0.58269E-02	0.64564E-02	-0.76524E-04
11759	0.58262E-02	0.64510E-02	0.77119E-04
11046	0.38101E-02	0.23614E-05	0.72071E-04
8183	0.38090E-02	-0.12716E-05	-0.71403E-04
3022	0.27673E-02	-0.92069E-03	0.48579E-04
159	0.27669E-02	-0.92086E-03	-0.48483E-04
3735	0.25656E-02	-0.10508E-02	0.84479E-04
6602	0.25657E-02	-0.10509E-02	-0.84428E-04
4467	0.29596E-02	-0.12518E-02	0.70350E-04
5890	0.29597E-02	-0.12518E-02	-0.70282E-04
5178	0.30717E-02	-0.13014E-02	-0.27696E-05

=====

=====

EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 87.516

\*\*\* NOTE \*\*\* CP= 87.516 TIME= 17:12:22  
A total of 1 warnings and errors written to dcslabs2.err.



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# Appendix DN-2 to Calculation PGE-009-CALC-003

Below is the ANSYS input file that scans the database for the maximum cask displacements for the very hard rock model.

```
/output,padvhardcaskd.out
/com
/file,dcslabh6
resume
/header,on,off,off,off,on,off
/post1
eall
nall
/com,
/com, This routine selects the nodes at the centerlines of the perimeter casks
/com, and prints out the displacements for these nodes for all 19 load steps.
/com,
/COM =====
/COM =====
/COM
/COM ===== SELECT NODES AT THE CL OF THE CASKS =====
/COM
nsel,node,159
nsel,node,3022
nsel,node,3735
nsel,node,4467
nsel,node,5178
nsel,node,5890
nsel,node,6602
nsel,node,8183
nsel,node,11046
nsel,node,11759
nsel,node,12491
nsel,node,13202
nsel,node,13914
nsel,node,14626
/COM =====
/COM =====
/COM ===== SET 1 =====
set,1
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 2 =====
set,2
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 3 =====
set,3
nsort,u,y
prdi
/COM =====
```



```
/COM =====
/COM ===== SET 4 =====
set,4
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 5 =====
set,5
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 6 =====
set,6
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 7 =====
set,7
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 8 =====
set,8
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 9 =====
set,9
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 10 =====
set,10
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 11 =====
set,11
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 12 =====
set,12
nsort,u,y
prdi
```



```
/COM =====
/COM =====
/COM ===== SET 13 =====
set,13
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 14 =====
set,14
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 15 =====
set,15
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 16 =====
set,16
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 17 =====
set,17
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 18 =====
set,18
nsort,u,y
prdi
/COM =====
/COM =====
/COM ===== SET 19 =====
set,19
nsort,u,y
prdi
/COM =====
/COM =====
fini
/output
/exit
```



**Below is the ANSYS output file for the maximum cask displacements for the very hard rock analyses:**

CURRENT JOBNAME REDEFINED AS dcslabh6

RESUME ANSYS DATA FROM FILE NAME=dcslabh6.db

\*\*\* ANSYS GLOBAL STATUS \*\*\*

TITLE = Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock

ANALYSIS TYPE = STATIC (STEADY-STATE)

NUMBER OF ELEMENT TYPES = 6

9056 ELEMENTS CURRENTLY SELECTED. MAX ELEMENT NUMBER = 33177

11550 NODES CURRENTLY SELECTED. MAX NODE NUMBER = 17051

259 KEYPOINTS CURRENTLY SELECTED. MAX KEYPOINT NUMBER = 259

250 LINES CURRENTLY SELECTED. MAX LINE NUMBER = 396

181 AREAS CURRENTLY SELECTED. MAX AREA NUMBER = 295

70 VOLUMES CURRENTLY SELECTED. MAX VOL. NUMBER = 70

11 COMPONENTS CURRENTLY DEFINED

MAXIMUM LINEAR PROPERTY NUMBER = 5

MAXIMUM REAL CONSTANT SET NUMBER = 6

ACTIVE COORDINATE SYSTEM = 0 (CARTESIAN)

MAXIMUM CONSTRAINT EQUATION NUMBER = 4620

NUMBER OF SPECIFIED CONSTRAINTS = 2193

NUMBER OF NODAL LOADS = 2160

INITIAL JOBNAME = dcslabh6

CURRENT JOBNAME = dcslabh6

PRINT HEADER

DO NOT PRINT SUBTITLE(S)

DO NOT PRINT LOAD STEP ID

DO NOT PRINT NOTE LINE(S)

PRINT COLUMN HEADER LABELS

DO NOT PRINT REPORT TOTALS

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 5.7 \*\*\*\*\*

ANSYS/Structural U

00150104 VERSION=INTEL NT 10:30:17 MAY 21, 2001 CP= 4.376

Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock

\*\*\*\*\* ANSYS RESULTS INTERPRETATION (POST1) \*\*\*\*\*

ENTER /SHOW,DEVICE-NAME TO ENABLE GRAPHIC DISPLAY

ENTER FINISH TO LEAVE POST1

\*\*\* NOTE \*\*\*

CP= 4.376 TIME= 10:30:17

Reading results into the database (SET command) will update the current displacement and force boundary conditions in the database with the values from the results file for that load set. Note that any



Appendix DN-2 to Calculation PGE-009-CALC-003

subsequent solutions will use these values unless action is taken to either SAVE the current values or not overwrite them (/EXIT,NOSAVE).

15348 ELEMENTS (OF 15348 DEFINED) SELECTED BY EALL COMMAND.

17051 NODES (OF 17051 DEFINED) SELECTED BY NALL COMMAND.

This routine selects the nodes at the centerlines of the perimeter casks and prints out the displacements for these nodes for all 19 load steps.

=====

===== SELECT NODES AT THE CL OF THE CASKS =====

NSEL FOR LABEL= NODE FROM 159 TO 159 BY 1

1 NODES (OF 17051 DEFINED) SELECTED BY NSEL COMMAND.

NASE FOR LABEL= NODE FROM 3022 TO 3022 BY 1

2 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 3735 TO 3735 BY 1

3 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 4467 TO 4467 BY 1

4 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 5178 TO 5178 BY 1

5 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 5890 TO 5890 BY 1

6 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 6602 TO 6602 BY 1

7 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 8183 TO 8183 BY 1

8 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 11046 TO 11046 BY 1

9 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.

NASE FOR LABEL= NODE FROM 11759 TO 11759 BY 1





Appendix DN-2 to Calculation PGE-009-CALC-003

10 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 12491 TO 12491 BY 1

11 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 13202 TO 13202 BY 1

12 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 13914 TO 13914 BY 1

13 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
NASE FOR LABEL= NODE FROM 14626 TO 14626 BY 1

14 NODES (OF 17051 DEFINED) SELECTED BY NASE COMMAND.  
=====

USE LOAD STEP 1 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 1 SUBSTEP= 1 CUMULATIVE ITERATION= 2  
TIME/FREQUENCY= 1.0000  
TITLE= Pad, Gravity, 20 Casks, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
11759	0.26914E-03	-0.14995E-02	-0.32977E-03
3735	-0.26914E-03	-0.14995E-02	-0.32977E-03
14626	0.26914E-03	-0.14995E-02	0.32977E-03
6602	-0.26914E-03	-0.14995E-02	0.32977E-03
12491	0.32542E-03	-0.17711E-02	-0.14923E-03
13914	0.32542E-03	-0.17711E-02	0.14923E-03
4467	-0.32542E-03	-0.17711E-02	-0.14923E-03
5890	-0.32542E-03	-0.17711E-02	0.14923E-03
8183	0.97119E-04	-0.17835E-02	-0.37368E-03
159	-0.97119E-04	-0.17835E-02	-0.37368E-03
11046	0.97119E-04	-0.17835E-02	0.37368E-03
3022	-0.97119E-04	-0.17835E-02	0.37368E-03
13202	0.34362E-03	-0.18427E-02	0.14098E-06
5178	-0.34362E-03	-0.18427E-02	0.14098E-06

=====

SET 2



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# Appendix DN-2 to Calculation PGE-009-CALC-003

USE LOAD STEP 2 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 2 SUBSTEP= 1 CUMULATIVE ITERATION= 17  
TIME/FREQUENCY= 2.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips North (Z), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.15991E-03	0.41046E-02	0.73726E-02
6602	-0.15991E-03	0.41046E-02	0.73726E-02
3022	-0.10460E-03	0.39005E-02	0.76401E-02
11046	0.10460E-03	0.39005E-02	0.76401E-02
13914	0.20138E-03	-0.10760E-02	0.41609E-02
5890	-0.20138E-03	-0.10760E-02	0.41609E-02
13202	0.23798E-03	-0.13847E-02	0.35184E-02
5178	-0.23798E-03	-0.13847E-02	0.35184E-02
12491	0.21592E-03	-0.16367E-02	0.31418E-02
4467	-0.21592E-03	-0.16367E-02	0.31418E-02
11759	0.16481E-03	-0.17420E-02	0.26260E-02
3735	-0.16481E-03	-0.17420E-02	0.26260E-02
8183	0.57095E-04	-0.20616E-02	0.29232E-02
159	-0.57095E-04	-0.20616E-02	0.29232E-02

=====

=====

===== SET 3 =====

USE LOAD STEP 3 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 3 SUBSTEP= 1 CUMULATIVE ITERATION= 32  
TIME/FREQUENCY= 3.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 32.93 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.62141E-02	0.12714E-01	0.75992E-02
11046	0.40544E-02	0.41919E-02	0.66896E-02
13914	0.52303E-02	0.31999E-02	0.50974E-02
3022	0.26649E-02	0.12681E-02	0.53669E-02
13202	0.41532E-02	0.54330E-03	0.34520E-02
6602	0.24399E-02	-0.11152E-03	0.40328E-02



Appendix DN-2 to Calculation PGE-009-CALC-003

```
12491 0.34440E-02-0.26965E-03 0.28443E-02
11759 0.25022E-02-0.92172E-03 0.24075E-02
5890 0.20748E-02-0.16027E-02 0.30911E-02
5178 0.20206E-02-0.18209E-02 0.28997E-02
8183 0.18702E-02-0.18791E-02 0.24529E-02
3735 0.16261E-02-0.19827E-02 0.22180E-02
4467 0.19092E-02-0.20038E-02 0.26542E-02
159 0.16842E-02-0.20246E-02 0.24397E-02
```

```
=====
=====
===== SET 4 =====
```

USE LOAD STEP 4 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 4 SUBSTEP= 1 CUMULATIVE ITERATION= 39  
TIME/FREQUENCY= 4.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 45 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.84195E-02	0.14817E-01	0.62298E-02
13914	0.77063E-02	0.65603E-02	0.45662E-02
11046	0.52501E-02	0.32221E-02	0.52961E-02
13202	0.65959E-02	0.32113E-02	0.32634E-02
12491	0.54683E-02	0.15511E-02	0.27051E-02
11759	0.38926E-02	0.57587E-04	0.23724E-02
3022	0.31944E-02	0.22565E-04	0.38945E-02
6602	0.27299E-02	0.91048E-03	0.28132E-02
5890	0.27289E-02	0.17574E-02	0.25054E-02
8183	0.25526E-02	0.17583E-02	0.20877E-02
5178	0.27199E-02	0.19563E-02	0.24198E-02
159	0.22561E-02	0.19606E-02	0.20361E-02
3735	0.21898E-02	0.20096E-02	0.18576E-02
4467	0.25771E-02	0.20941E-02	0.22350E-02

```
=====
=====
===== SET 5 =====
```

USE LOAD STEP 5 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 5 SUBSTEP= 1 CUMULATIVE ITERATION= 46  
TIME/FREQUENCY= 5.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips N 57.07 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051



Appendix DN-2 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.10053E-01	0.15531E-01	0.42961E-02
13914	0.98102E-02	0.99017E-02	0.34898E-02
13202	0.89168E-02	0.67691E-02	0.28128E-02
12491	0.75931E-02	0.42643E-02	0.25079E-02
11046	0.59853E-02	0.19503E-02	0.35738E-02
11759	0.55404E-02	0.16982E-02	0.23153E-02
3022	0.34412E-02-0.96303E-03		0.24446E-02
6602	0.28992E-02-0.13666E-02		0.18646E-02
8183	0.32324E-02-0.16027E-02		0.16422E-02
159	0.27520E-02-0.18744E-02		0.15342E-02
5890	0.32470E-02-0.18927E-02		0.18662E-02
3735	0.26608E-02-0.20005E-02		0.14065E-02
5178	0.32908E-02-0.20685E-02		0.18437E-02
4467	0.31308E-02-0.21530E-02		0.17154E-02

=====  
===== SET 6 =====

USE LOAD STEP 6 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 6 SUBSTEP= 1 CUMULATIVE ITERATION= 58  
TIME/FREQUENCY= 6.0000

TITLE= Pad, HE(1), 20 Casks, 515 Kips West (W), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.12132E-01	0.13108E-01	0.15841E-04
13914	0.11661E-01	0.12406E-01	0.35794E-03
12491	0.11661E-01	0.12403E-01	0.35881E-03
14626	0.10097E-01	0.10533E-01	0.63440E-03
11759	0.10096E-01	0.10528E-01	0.63500E-03
11046	0.53510E-02-0.46913E-03		0.52366E-04
8183	0.53496E-02-0.47138E-03		0.51658E-04
3022	0.35822E-02-0.15483E-02		0.19426E-03
159	0.35820E-02-0.15484E-02		0.19420E-03
3735	0.33198E-02-0.18029E-02		0.13373E-03
6602	0.33199E-02-0.18029E-02		0.13375E-03
4467	0.38720E-02-0.21452E-02		0.30111E-04
5890	0.38720E-02-0.21452E-02		0.30142E-04
5178	0.40089E-02-0.22344E-02		0.14194E-05

=====  
=====



Appendix DN-2 to Calculation PGE-009-CALC-003

===== SET 7 =====

USE LOAD STEP 7 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 7 SUBSTEP= 1 CUMULATIVE ITERATION= 80  
TIME/FREQUENCY= 7.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips North (z), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.13159E-03	0.16427E-04	0.19894E-02
6602	-0.13123E-03	0.15313E-04	0.19889E-02
11046	0.58808E-04	-0.10488E-03	0.21111E-02
3022	-0.58496E-04	-0.10522E-03	0.21109E-02
13914	0.14272E-03	-0.65688E-03	0.15485E-02
5890	-0.14267E-03	-0.65691E-03	0.15484E-02
13202	0.14564E-03	-0.76323E-03	0.14554E-02
5178	-0.14562E-03	-0.76323E-03	0.14554E-02
12491	0.13004E-03	-0.86189E-03	0.13264E-02
4467	-0.13003E-03	-0.86189E-03	0.13264E-02
11759	0.10001E-03	-0.88228E-03	0.11071E-02
3735	-0.10000E-03	-0.88228E-03	0.11071E-02
8183	0.34488E-04	-0.10444E-02	0.12337E-02
159	-0.34484E-04	-0.10444E-02	0.12337E-02

=====

===== SET 8 =====

USE LOAD STEP 8 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 8 SUBSTEP= 1 CUMULATIVE ITERATION= 99  
TIME/FREQUENCY= 8.0000

TITLE= Pad, HE(1), 20 Casks, 206 Kips West (X), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.36986E-02	0.16457E-02	-0.27203E-05
13914	0.35333E-02	0.15116E-02	-0.28257E-04
12491	0.35333E-02	0.15115E-02	-0.28259E-04
14626	0.29664E-02	0.11351E-02	-0.50395E-04
11759	0.29664E-02	0.11351E-02	-0.50389E-04



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

11046  0.16921E-02-0.69356E-03  0.11848E-03
 8183  0.16920E-02-0.69356E-03-0.11848E-03
  159  0.14128E-02-0.83401E-03-0.13201E-03
3022   0.14128E-02-0.83401E-03  0.13201E-03
3735   0.13433E-02-0.90985E-03-0.93192E-04
6602   0.13433E-02-0.90985E-03  0.93192E-04
4467   0.15602E-02-0.10772E-02-0.30276E-04
5890   0.15602E-02-0.10772E-02  0.30276E-04
5178   0.16139E-02-0.11211E-02-0.17641E-06

```

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=====
===== SET 9 =====

```

USE LOAD STEP 9 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 9 SUBSTEP= 1 CUMULATIVE ITERATION= 103  
TIME/FREQUENCY= 9.0000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips North (Z), Max Dn, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.49231E-03	-0.25179E-02	0.17231E-02
6602	-0.49234E-03	-0.25179E-02	0.17231E-02
11759	0.45861E-03	-0.29162E-02	0.48693E-03
3735	-0.45864E-03	-0.29162E-02	0.48693E-03
11046	0.18058E-03	-0.29973E-02	0.19346E-02
3022	-0.18058E-03	-0.29973E-02	0.19346E-02
5890	-0.59076E-03	-0.31524E-02	0.15009E-02
13914	0.59073E-03	-0.31524E-02	0.15009E-02
12491	0.57295E-03	-0.33257E-02	0.94499E-03
4467	-0.57296E-03	-0.33257E-02	0.94499E-03
13202	0.61680E-03	-0.33520E-02	0.12596E-02
5178	-0.61681E-03	-0.33520E-02	0.12596E-02
8183	0.16626E-03	-0.34608E-02	0.53458E-03
159	-0.16626E-03	-0.34608E-02	0.53458E-03

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=====
===== SET 10 =====

```

USE LOAD STEP 10 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 10 SUBSTEP= 1 CUMULATIVE ITERATION= 106  
TIME/FREQUENCY= 10.000

TITLE= Pad, HE(3), 20 Casks, 171.2 Kips West (X), Max Dn, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051



Appendix DN-2 to Calculation PGE-009-CALC-003

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.17206E-02	-0.24970E-02	0.65073E-03
11759	0.17205E-02	-0.24970E-02	-0.65067E-03
3735	0.77053E-03	-0.29370E-02	-0.58515E-03
6602	0.77054E-03	-0.29370E-02	0.58516E-03
12491	0.20250E-02	-0.29708E-02	-0.30219E-03
13914	0.20250E-02	-0.29708E-02	0.30220E-03
13202	0.21095E-02	-0.30948E-02	-0.74582E-06
8183	0.13789E-02	-0.31823E-02	-0.70738E-03
11046	0.13789E-02	-0.31823E-02	0.70739E-03
159	0.10322E-02	-0.32757E-02	-0.69250E-03
3022	0.10322E-02	-0.32757E-02	0.69250E-03
4467	0.86248E-03	-0.35071E-02	-0.25369E-03
5890	0.86248E-03	-0.35071E-02	0.25369E-03
5178	0.87786E-03	-0.36558E-02	-0.13663E-05

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=====

===== SET 11 =====

USE LOAD STEP 11 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 11 SUBSTEP= 1 CUMULATIVE ITERATION= 122

TIME/FREQUENCY= 11.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips North (Z), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.16423E-03	0.30752E-02	0.64451E-02
6602	-0.16423E-03	0.30752E-02	0.64451E-02
3022	-0.10178E-03	0.28695E-02	0.66997E-02
11046	0.10178E-03	0.28695E-02	0.66997E-02
13914	0.19722E-03	-0.10322E-02	0.37719E-02
5890	-0.19722E-03	-0.10322E-02	0.37719E-02
13202	0.22466E-03	-0.12978E-02	0.32538E-02
5178	-0.22466E-03	-0.12978E-02	0.32538E-02
12491	0.20122E-03	-0.15137E-02	0.29206E-02
4467	-0.20122E-03	-0.15137E-02	0.29206E-02
11759	0.14957E-03	-0.15916E-02	0.24522E-02
3735	-0.14957E-03	-0.15916E-02	0.24522E-02
8183	0.51577E-04	-0.18828E-02	0.27338E-02
159	-0.51577E-04	-0.18828E-02	0.27338E-02

=====



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# Appendix DN-2 to Calculation PGE-009-CALC-003

=====

===== SET 12 =====

USE LOAD STEP 12 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 12 SUBSTEP= 1 CUMULATIVE ITERATION= 136  
TIME/FREQUENCY= 12.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 32.93 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.52259E-02	0.93959E-02	0.65703E-02
11046	0.33754E-02	0.27545E-02	0.57651E-02
13914	0.43580E-02	0.19011E-02	0.43337E-02
3022	0.22861E-02	0.70097E-03	0.46754E-02
13202	0.35270E-02	0.11962E-03	0.30555E-02
6602	0.21191E-02	-0.29022E-03	0.35729E-02
12491	0.30047E-02	-0.43895E-03	0.25848E-02
11759	0.22403E-02	-0.91256E-03	0.21920E-02
5890	0.18711E-02	-0.14887E-02	0.28351E-02
5178	0.18409E-02	-0.16847E-02	0.26809E-02
8183	0.17262E-02	-0.17211E-02	0.22803E-02
3735	0.15070E-02	-0.18077E-02	0.20689E-02
4467	0.17513E-02	-0.18400E-02	0.24633E-02
159	0.15655E-02	-0.18513E-02	0.22755E-02

=====

===== SET 13 =====

USE LOAD STEP 13 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 13 SUBSTEP= 1 CUMULATIVE ITERATION= 142  
TIME/FREQUENCY= 13.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 45 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.70751E-02	0.10994E-01	0.54197E-02
13914	0.64375E-02	0.44050E-02	0.38834E-02
13202	0.55569E-02	0.20663E-02	0.28228E-02
11046	0.43617E-02	0.19503E-02	0.45639E-02





Appendix DN-2 to Calculation PGE-009-CALC-003

```
12491 0.47036E-02 0.94615E-03 0.23874E-02
11759 0.34314E-02-0.13091E-03 0.20984E-02
3022 0.27716E-02-0.29126E-03 0.34159E-02
6602 0.24177E-02-0.91686E-03 0.25429E-02
8183 0.23395E-02-0.16160E-02 0.19278E-02
5890 0.24707E-02-0.16253E-02 0.23092E-02
159 0.20905E-02-0.17956E-02 0.18952E-02
5178 0.24785E-02-0.18044E-02 0.22393E-02
3735 0.20248E-02-0.18325E-02 0.17321E-02
4467 0.23614E-02-0.19204E-02 0.20736E-02
```

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=====
===== SET 14 =====
```

USE LOAD STEP 14 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 14 SUBSTEP= 1 CUMULATIVE ITERATION= 149  
TIME/FREQUENCY= 14.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips N 57.03 W (Z,X), Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.84149E-02	0.11429E-01	0.38062E-02
13914	0.81822E-02	0.68306E-02	0.29998E-02
13202	0.74775E-02	0.45853E-02	0.23752E-02
12491	0.64564E-02	0.29328E-02	0.21074E-02
11759	0.48040E-02	0.11344E-02	0.19554E-02
11046	0.49453E-02	0.94387E-03	0.31009E-02
3022	0.30237E-02-0.98776E-03	0.21940E-02	
6602	0.26185E-02-0.12766E-02	0.17210E-02	
8183	0.29298E-02-0.14840E-02	0.14920E-02	
159	0.25392E-02-0.17200E-02	0.14212E-02	
5890	0.29456E-02-0.17453E-02	0.17272E-02	
3735	0.24537E-02-0.18257E-02	0.13092E-02	
5178	0.29962E-02-0.19041E-02	0.17066E-02	
4467	0.28635E-02-0.19735E-02	0.15894E-02	

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=====
===== SET 15 =====
```

USE LOAD STEP 15 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 15 SUBSTEP= 1 CUMULATIVE ITERATION= 161  
TIME/FREQUENCY= 15.000

TITLE= Pad, LTSP(2), 20 Casks, 440 Kips West (X), Very Hard Rock



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# Appendix DN-2 to Calculation PGE-009-CALC-003

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.10129E-01	0.92667E-02	-0.10312E-04
13914	0.97491E-02	0.87823E-02	-0.20749E-03
12491	0.97481E-02	0.87782E-02	0.20903E-03
14626	0.84664E-02	0.75292E-02	-0.34840E-03
11759	0.84650E-02	0.75210E-02	0.34936E-03
11046	0.45051E-02	-0.74842E-03	0.12668E-03
8183	0.45025E-02	-0.75229E-03	-0.12604E-03
3022	0.32451E-02	-0.14361E-02	0.19827E-03
159	0.32447E-02	-0.14362E-02	-0.19820E-03
3735	0.30342E-02	-0.16545E-02	-0.13025E-03
6602	0.30343E-02	-0.16545E-02	0.13029E-03
4467	0.35208E-02	-0.19700E-02	-0.32162E-04
5890	0.35208E-02	-0.19700E-02	0.32215E-04
5178	0.36421E-02	-0.20522E-02	-0.13675E-05

=====

=====

===== SET 16 =====

USE LOAD STEP 16 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 16 SUBSTEP= 1 CUMULATIVE ITERATION= 186  
TIME/FREQUENCY= 16.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips North (Z), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.69534E-04	0.14295E-02	0.28905E-02
6602	-0.69534E-04	0.14295E-02	0.28905E-02
3022	-0.44063E-04	0.13406E-02	0.30056E-02
11046	0.44063E-04	0.13406E-02	0.30056E-02
13914	0.80817E-04	-0.42450E-03	0.16918E-02
5890	-0.80817E-04	-0.42450E-03	0.16918E-02
13202	0.92090E-04	-0.53901E-03	0.14568E-02
5178	-0.92090E-04	-0.53901E-03	0.14568E-02
12491	0.81351E-04	-0.62699E-03	0.13111E-02
4467	-0.81351E-04	-0.62699E-03	0.13111E-02
11759	0.58271E-04	-0.65890E-03	0.11099E-02
3735	-0.58271E-04	-0.65890E-03	0.11099E-02
8183	0.19885E-04	-0.77928E-03	0.12397E-02
159	-0.19885E-04	-0.77928E-03	0.12397E-02

Appendix DN-2 to Calculation PGE-009-CALC-003

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===== SET 17 =====

USE LOAD STEP 17 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 17 SUBSTEP= 3 CUMULATIVE ITERATION= 257  
TIME/FREQUENCY= 17.000

TITLE= Pad, LTSP(2), 20 Casks, 176 Kips West (X), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
13202	0.43869E-02	0.40415E-02	-0.39809E-05
13914	0.42340E-02	0.38564E-02	-0.72125E-04
12491	0.42339E-02	0.38560E-02	0.72332E-04
14626	0.37165E-02	0.33850E-02	-0.11788E-03
11759	0.37164E-02	0.33840E-02	0.11795E-03
11046	0.20204E-02	-0.27861E-03	0.58217E-04
8183	0.20200E-02	-0.27934E-03	-0.58303E-04
3022	0.14551E-02	-0.59631E-03	0.80848E-04
159	0.14551E-02	-0.59633E-03	-0.80845E-04
6602	0.13554E-02	-0.69202E-03	0.48826E-04
3735	0.13554E-02	-0.69202E-03	-0.48822E-04
5890	0.15635E-02	-0.82246E-03	0.10884E-04
4467	0.15635E-02	-0.82246E-03	-0.10878E-04
5178	0.16159E-02	-0.85650E-03	-0.65767E-06

=====

=====

===== SET 18 =====

USE LOAD STEP 18 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 18 SUBSTEP= 3 CUMULATIVE ITERATION= 338  
TIME/FREQUENCY= 18.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips North (Z), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

NODE	UX	UY	UZ
14626	0.51835E-04	0.21591E-02	0.30013E-02
6602	-0.51742E-04	0.21586E-02	0.30012E-02
11046	0.39450E-04	0.20798E-02	0.31076E-02



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# Appendix DN-2 to Calculation PGE-009-CALC-003

```

3022 -0.39306E-04 0.20796E-02 0.31076E-02
13914 0.52679E-04-0.25410E-03 0.17179E-02
5890 -0.52659E-04-0.25435E-03 0.17177E-02
5178 -0.68046E-04-0.41044E-03 0.13944E-02
13202 0.68051E-04-0.41044E-03 0.13944E-02
4467 -0.60100E-04-0.49248E-03 0.12498E-02
12491 0.60103E-04-0.49248E-03 0.12498E-02
11759 0.42236E-04-0.53723E-03 0.10696E-02
3735 -0.42235E-04-0.53723E-03 0.10696E-02
159 -0.13927E-04-0.63607E-03 0.11958E-02
8183 0.13928E-04-0.63607E-03 0.11958E-02
=====
=====
===== SET 19 =====

```

USE LOAD STEP 19 SUBSTEP 0 FOR LOAD CASE 0

SET COMMAND GOT LOAD STEP= 19 SUBSTEP= 3 CUMULATIVE ITERATION= 412  
TIME/FREQUENCY= 19.000

TITLE= Pad, LTSP(4), 20 Casks, 156 Kips West (X), Max Up, Very Hard Rock

SORT ON ITEM=U COMPONENT=Y ORDER= 0 KABS= 0 NMAX= 17051

SORT COMPLETED FOR 14 VALUES.

PRINT DOF NODAL SOLUTION PER NODE

```

      NODE      UX      UY      UZ
13202 0.49370E-02 0.65705E-02-0.63988E-05
13914 0.47659E-02 0.62738E-02-0.16591E-03
12491 0.47659E-02 0.62737E-02 0.16594E-03
14626 0.42158E-02 0.54603E-02-0.30501E-03
11759 0.42158E-02 0.54602E-02 0.30501E-03
11046 0.24034E-02 0.24169E-03-0.34343E-04
8183 0.24033E-02 0.24160E-03 0.34346E-04
3022 0.14750E-02-0.46950E-03 0.37930E-04
159 0.14749E-02-0.46950E-03-0.37930E-04
3735 0.13278E-02-0.57497E-03-0.17641E-04
6602 0.13278E-02-0.57497E-03 0.17642E-04
4467 0.15291E-02-0.67422E-03 0.23797E-05
5890 0.15291E-02-0.67422E-03-0.23788E-05
5178 0.15807E-02-0.70048E-03-0.50913E-06
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EXIT THE ANSYS POST1 DATABASE PROCESSOR

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 46.517



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Appendix DN-2 to Calculation PGE-009-CALC-003

\*\*\* NOTE \*\*\*

CP= 46.527 TIME= 10:31:17

A total of 1 warnings and errors written to dcslabh6.err.