

Appendix 4 Structural Integrity of Spent Fuel Pool Structures Subject to Tornadoes and High Winds

Tornado or high winds damage from missiles can affect the structural integrity of the spent fuel pool or the availability of nearby support systems, such as power supplies, cooling pumps, heat exchangers and water makeup sources, and may also affect recovery actions. A set of site specific evaluations for tornadoes and high winds was documented in NUREG/CR-5042 [Ref. 1]. It is noted that the study was performed to assess core damage frequencies at operating plants. The methodology for the assessment of tornado risk developed in NUREG/CR-2944 [Ref. 2] was used for this evaluation.

The National Climatic Data Center (NCDC) in Asheville, N.C., keeps weather records for the U.S. for the period 1950 to 1995 [Ref. 3]. Tornado data are reported as the annual average number of (all) tornadoes per 10,000 square miles per state and the annual average number of strong-violent (F2 to F5) tornadoes per square mile per state, as shown in Figures A4-1 and A4-2.

A comparison of the site-specific evaluations (from NUREG/CR-5042) and general regional values from the NCDC database are compared in Table A4-1. The NCDC data was reviewed and a range of frequencies per square mile per year was developed based on the site location and neighboring state (regional) data. In general, NUREG/CR-5042 tornado frequencies for all tornadoes the NCDC tornado frequencies for all reported tornadoes showed good agreement between the two sets of data.

The Storm Prediction Center (SPC) raw data for the period 1950 to 1995 was used to develop a database for this assessment. About 121 F5, and 924 F4, tornadoes have been recorded between 1950 and 1995 (an additional 4 in the 1996 to 1998 period). It was estimated that about 30% of all reported tornadoes were in the F2 to F3 range and about 2.5% were in the F4 to F5 range.

The Department of Energy report DOE-STD-1020-94, [Ref. 4], provides some insights into wind generated missiles:

- (1) For sites where tornadoes are not considered a viable threat, to account for objects or debris a 2x4 inch timber plank weighing 15 lbs is considered as a missile for straight winds and hurricanes. With a recommended impact speed of 50 mph at a maximum height of 30 ft above ground, this missile would break annealed glass, perforate sheet metal siding and wood siding up to to 3/4-in thick. For weak tornadoes, the timber missile horizontal speed is 100 mph effective to a height of 100 ft above ground and a vertical speed of 70 mph. A second missile is considered: a 3-in diameter steel pipe weighing 75 lbs with an impact velocity of 50 mph, effective to a height of 75 ft above ground and a vertical velocity of 35 mph. For the straight wind missile, an 8-in concrete masonry unit (CMU) wall, single wythe (single layer) brick wall with stud wall, or a 4-inch concrete (reinforced) is considered adequate to prevent penetration. For the tornado missile, an 8-to-12-in CMU wall, single wythe brick wall with stud wall and metal ties, or a 4- to 8-inch concrete (reinforced) slab is considered adequate to prevent penetration (depending on the missile). (Refer to DOE-STD-1020-94 for additional details.)

- (2) For sites where tornadoes are considered a viable threat, to account for objects or debris the same 2x4 inch timber is considered but for heights above ground to 50 ft. The tornado missiles are (1) the 15 lbs, 2x4 inch timber with a horizontal speed of 150 mph effective up to 200 ft above ground, and a vertical speed of 100 mph; (2) the 3-inch diameter, 75 lbs steel pipe with a horizontal speed of 75 mph and a vertical speed of 50 mph effective up to 100 ft above ground; and (3) a 3,000 lbs automobile with ground speed up to 25 mph. For the straight wind missile, an 8-in CMU wall, single wythe brick wall with stud wall, or a 4-inch concrete (reinforced) is considered adequate to prevent penetration. For the tornado missile, an 8 in CMU reinforced wall, or a 4- to 10-inch concrete (reinforced) slab is considered adequate to prevent penetration (depending on the missile). (Refer to DOE-STD-1020-94 for additional details.)

The winds associated with hurricanes and other storms are generally less intense and lower in magnitude than those associated with tornadoes. Generally, high winds from wind storms and hurricanes are considered to be the controlling wind level at a higher frequency but at a lower magnitude.

Recommended Values for Risk-informed Assessment of Spent Fuel Pool

The tornado strike probabilities for each F-scale interval was determined from the SPC raw data on a state-averaged basis. For each F-scale, the point strike probability was obtained from the following equation:

$$P_{fs} = \left(\frac{\sum N < a >_T}{A_{ob}} \right) \times \frac{1}{Y_{int}} \quad \text{Equation A4-1}$$

where:

| | |
|-----------|--|
| P_{fs} | = strike probability for F-scale (fs) |
| $<a>_T$ | = tornado area, mi ² |
| A_{ob} | = area of observation, mi ² (state land area) |
| Y_{int} | = interval over which observations were made, years |
| $\sum N$ | = sum of reported tornados in the area of observation |

The tornado area, $<a>_T$, was evaluated at the mid-point of the path-length and path-width intervals shown in Table A4-2a, based on the SPC path classifications. For example, an F2 tornado with a path-length scale of 2 has an average path length of 6.55 miles and with a path-width scale of 3 has an average width of 0.2 miles.

The tornado area, $<a>_T$, was then modified using the method described in NUREG/CR-2944 (based on Tables 6b and 7b) to correct the area calculation by observations of the variations in a tornado's intensity along its path length and path width, see Figure A4-3. Table A4-2b provides the path-length correction data. Table A4-2c gives the path-width correction data. The corrected effective area has a calculated $<a>_T$ of about 0.28 mi². The combined variation in intensity along the length and across the width of the tornado path is shown in Table A4-2d (Table 15b from NUREG/CR-2944). For example, an F2 tornado with a path-length scale of 2 and a path-width scale of 3 has a calculated $<a>_T$ of about 0.28 mi². The total area is reapportioned using Table A4-2d to assign 0.11 mi² to the F0 classification, 0.13 mi² to the F1 classification, and 0.04 mi² to the F2 classification.

The risk regionalization scheme used in NUREG/CR-2944, as shown in Figure A4-4, was used to determine the exceedance probability for each region identified. A continental U.S. average was also determined. Figure A4-4 gives the approximate location of commercial LWRs and independent spent fuel storage facilities.

The SPC raw data for each state was used to determine the F-scale, path-length and path-width characteristics of the reported tornadoes. The effective tornado strike area was corrected using the data from NUREG/CR-2944. Equation A4-1 was used for each state and the summation and averaging of the states within each region (A, B, C and D, as well as a continental USA average) performed. The results for the exceedance probability per year for each F-scale are given in Table A4-3, and graphically presented in Figure A4-5. The SPC data analysis is summarized in Table A4-4.

Significant Pool Damage

Only F4 to F5 tornado would be needed to consider the possibility of damage to the spent fuel pool by a tornado missile. The likelihood of the exceedance of this size tornado is estimated to be 5.6×10^{-7} per year (for Region A), or lower. In addition, the spent fuel pool is a multiple-foot thick concrete structure. Based on the DOE-STD-1020-94 information, it is very unlikely that a tornado missile would penetrate the spent fuel pool.

Support System Availability

An F2 or larger tornado would be needed to consider damage to a support system, such as power supplies, cooling pumps, heat exchangers and water makeup sources. The likelihood of the exceedance of this size tornado is estimated to be 1.5×10^{-5} per year (for Region A), or lower.

References:

- (1) NUREG/CR-5042, "Evaluation of External Hazards to Nuclear Power Plants in the United States," Lawrence Livermore National Laboratory, December 1987.
- (2) NUREG/CR-2944, "Tornado Damage Risk Assessment," Brookhaven National Laboratory, September 1982.
- (3) National Climatic Data Center, <http://www.ncdc.noaa.gov>
- (4) DOE-STD-1020-94, "Natural Phenomena Hazards Design and Evaluation Criteria for Department of Energy Facilities," January 1996, Department of Energy.

Table A4-1 Tornado and High Wind Data Summary

| Site | NUREG/CR-5042 Data | | | | NCDC data | |
|-----------------|---|-------------------------------------|---------------------------------------|-------------------------------------|---|---|
| | Tornado frequency (per mi ² -per year) | Tornado strike frequency (per year) | High wind damage frequency (per year) | Tornado damage frequency (per year) | Frequency 1950-1995 average for F0-F5 (per mi ² -year) | Frequency 1950-1995 average for F2-F5 (per mi ² -year) |
| Indian Pt. 2 | 1.00x10 ⁻⁴ | 1.00x10 ⁻⁴ | 2.50x10 ⁻⁵ | <1.0x10 ⁻⁷ | 1.2-2.2x10 ⁻⁴ | 0.2-0.7x10 ⁻⁴ |
| Indian Pt. 3 | 1.00x10 ⁻⁴ | 1.00x10 ⁻⁴ | 1.80x10 ⁻⁵ | <1.0x10 ⁻⁷ | 1.2-2.2x10 ⁻⁴ | 0.2-0.7x10 ⁻⁴ |
| Limerick 1-2 | 1.13x10 ⁻⁴ | 2.30x10 ⁻⁴ (<F1) | 9.00x10 ⁻⁹ | <1.0x10 ⁻⁸ | 2.2-3.4x10 ⁻⁴ | 0.7-1.3x10 ⁻⁴ |
| Millstone 3 | 1.87x10 ⁻⁴ | 1.87x10 ⁻⁴ | Low | <1.0x10 ⁻⁷ | 2.8-3.4x10 ⁻⁴ | 0.2-1.1x10 ⁻⁴ |
| Oconee 3 | 2.50x10 ⁻⁴ | 3.50x10 ⁻³ 1 mi rad. | Low | <1.0x10 ⁻⁹ | 2.8-3.4x10 ⁻⁴ | 0.7-0.9x10 ⁻⁴ |
| Seabrook 1-2 | 1.26x10 ⁻³ | 7.75x10 ⁻⁵ | <3.89x10 ⁻⁸ | 2.06x10 ⁻⁹ LOSP & RWST | 1.8-3.8x10 ⁻⁴ | 0.4-1.1x10 ⁻⁴ |
| Zion ½ | 1.00x10 ⁻³ | 1.00x10 ⁻³ | N.A. | <1.0x10 ⁻⁸ | 3.4-5.4x10 ⁻⁴ | 1.2-2.0x10 ⁻⁴ |
| GSI A-45 PRAs | Regional Local | | w/o recovery of offsite power | | | |
| ANO 1 | 5.18x10 ⁻⁴ 4.37x10 ⁻⁴ | 1.53x10 ⁻³ | 5.69x10 ⁻⁶ | 2.53x10 ⁻⁴ | 3.7-7.5x10 ⁻⁴ | 1.7-2.4x10 ⁻⁴ |
| Point Beach 1-2 | 6.98x10 ⁻⁴ 4.11x10 ⁻⁴ | 5.38x10 ⁻⁴ | 1.00x10 ⁻⁵ | 5.00x10 ⁻⁵ | 3.4-4.7x10 ⁻⁴ | 1.2-1.5x10 ⁻⁴ |
| Quad Cities 1-2 | 5.18x10 ⁻⁴ 5.44x10 ⁻⁴ | 1.04x10 ⁻³ | <<1.0x10 ⁻⁸ | 5.08x10 ⁻⁷ | 3.4-5.4x10 ⁻⁴ | 1.2-2.0x10 ⁻⁴ |
| St. Lucie 1 | 6.98x10 ⁻⁴ 1.20x10 ⁻³ | 1.70x10 ⁻⁴ | <<1.0x10 ⁻⁸ | 1.61x10 ⁻⁸ | 8.4x10 ⁻⁴ | 1.2x10 ⁻⁴ |
| Turkey Pt. 3 | 3.37x10 ⁻⁴ 5.83x10 ⁻³ | 1.70x10 ⁻⁴ | 3.30x10 ⁻⁵ | 2.54x10 ⁻⁶ | 8.4x10 ⁻⁴ | 1.2x10 ⁻⁴ |

Table A4-2a Tornado Characteristics

| F-scale | Damage and wind speed | Path-length scale | | Path-width scale | |
|---------|----------------------------------|-------------------|-------------|------------------|-------------|
| | | Scale | Length (mi) | Scale | Width (yds) |
| 0 | Light Damage (40-72 mph) | 0 | < 1.0 | 0 | < 18 |
| 1 | Moderate Damage (73-112 mph) | 1 | 1.0 - 3.1 | 1 | 18 - 55 |
| 2 | Significant Damage (113-157 mph) | 2 | 3.2 - 9.9 | 2 | 56 - 175 |
| 3 | Severe Damage (158-206 mph) | 3 | 10.0 - 31.9 | 3 | 176 - 527 |
| 4 | Devastating Damage (207-260 mph) | 4 | 32 - 99.9 | 4 | 528 - 1759 |
| 5 | Incredible Damage (261-318 mph) | 5 | 100 > | 5 | 1760 > |

Table A4-2b Variation of Intensity Along Length
Based on Fraction of Length Per Tornado^(*)

| Local tornado state | Recorded tornado state | | | | | |
|------------------------|------------------------|-------|-------|-------|-------|-------|
| | F0 | F1 | F2 | F3 | F4 | F5 |
| PL-F0 | 1 | 0.383 | 0.180 | 0.077 | 0.130 | 0.118 |
| PL-F1 | | 0.617 | 0.279 | 0.245 | 0.131 | 0.125 |
| PL-F2 | | | 0.541 | 0.310 | 0.248 | 0.162 |
| PL-F3 | | | | 0.368 | 0.234 | 0.236 |
| PL-F4 | | | | | 0.257 | 0.187 |
| PL-F5 | | | | | | 0.172 |

(*) - Table 6b from NUREG/CR-2944

Table A4-2c Variation of Intensity Along Width Based on Fraction of Width Per Tornado^(*)

| Local tornado state | Recorded tornado state | | | | | |
|------------------------|------------------------|-------|-------|-------|-------|-------|
| | F0 | F1 | F2 | F3 | F4 | F5 |
| PW-F0 | 1 | 0.418 | 0.154 | 0.153 | 0.152 | 0.152 |
| PW-F1 | | 0.582 | 0.570 | 0.310 | 0.264 | 0.262 |
| PW-F2 | | | 0.276 | 0.363 | 0.216 | 0.143 |
| PW-F3 | | | | 0.174 | 0.246 | 0.168 |
| PW-F4 | | | | | 0.122 | 0.183 |
| PW-F5 | | | | | | 0.092 |

(*) - Table 7b from NUREG/CR-2944

Table A4-2d Combined Variation in Intensity Along Length
and Across Width of Tornado Path^(*)

| Local tornado state | True maximum tornado state | | | | | |
|------------------------|----------------------------|-------|-------|-------|-------|-------|
| | F0 | F1 | F2 | F3 | F4 | F5 |
| CV-F0 | 1.0 | 0.641 | 0.380 | 0.283 | 0.298 | 0.286 |
| CV-F1 | | 0.359 | 0.471 | 0.433 | 0.358 | 0.333 |
| CV-F2 | | | 0.149 | 0.220 | 0.209 | 0.195 |
| CV-F3 | | | | 0.064 | 0.104 | 0.116 |
| CV-F4 | | | | | 0.031 | 0.054 |
| CV-F5 | | | | | | 0.016 |

(*) - Table 15b from NUREG/CR-2944

Table A4-3 Exceedance Probability for Each F-scale

| NUREG/CR-2944 Region | Exceedance probability (per year) | | | | | |
|-------------------------|-----------------------------------|---------|---------|---------|---------|---------|
| | F0 | F1 | F2 | F3 | F4 | F5 |
| A | 7.4E-05 | 4.4E-05 | 1.5E-05 | 3.5E-06 | 5.6E-07 | 3.1E-08 |
| B | 5.6E-05 | 3.3E-05 | 1.1E-05 | 2.5E-06 | 3.7E-07 | 2.1E-08 |
| C | 2.9E-05 | 1.5E-05 | 4.1E-06 | 8.9E-07 | 1.3E-07 | 4.7E-09 |
| D | 3.6E-06 | 1.6E-06 | 3.9E-07 | 8.7E-08 | 1.6E-08 | --- |
| USA | 3.5E-05 | 2.0E-05 | 6.1E-06 | 1.4E-06 | 2.2E-07 | 1.0E-08 |

Table A4-4 SPC Data Analysis Summary by State

| State | NUREG/CR -2944 Region | | | | Years | Tornado F-scale | | | | | | Total | Point strike probability (per year) | | | | | | Land Area (mi ²) |
|-------|--------------------------|---|---|---|-------|-----------------|-----|-----|-----|----|----|-------|-------------------------------------|---------|---------|---------|---------|---------|---------------------------------|
| | A | B | C | D | | F0 | F1 | F2 | F3 | F4 | F5 | | F0 | F1 | F2 | F3 | F4 | F5 | |
| AL | X | X | | | 46 | 165 | 364 | 323 | 129 | 36 | 14 | 1031 | 2.9e-05 | 3.2e-05 | 1.3e-05 | 3.7e-06 | 6.9e-07 | 4.3e-08 | 50750 |
| AZ | | | | X | 44 | 90 | 57 | 11 | 2 | 0 | 0 | 160 | 6.7e-07 | 2.9e-07 | 3.6e-08 | 1.8e-09 | 0 | 0 | 113642 |
| AR | X | | | | 46 | 198 | 298 | 331 | 149 | 31 | 0 | 1007 | 3.2e-05 | 3.5e-05 | 1.3e-05 | 2.4e-06 | 1.9e-07 | 0 | 52075 |
| CA | | | | X | 45 | 142 | 58 | 21 | 2 | 0 | 0 | 223 | 5.1e-07 | 2.7e-07 | 6.0e-08 | 2.7e-09 | 0 | 0 | 155973 |
| CO | | | X | X | 46 | 616 | 441 | 99 | 15 | 1 | 0 | 1172 | 4.4e-06 | 2.0e-06 | 4.2e-07 | 3.9e-08 | 3.3e-11 | 0 | 103730 |
| CT | | | X | | 46 | 9 | 29 | 20 | 5 | 2 | 0 | 65 | 1.1e-05 | 1.1e-05 | 3.6e-06 | 8.5e-07 | 2.2e-07 | 0 | 4845 |
| DE | | | X | | 42 | 20 | 23 | 11 | 1 | 0 | 0 | 55 | 2.6e-05 | 1.5e-05 | 1.5e-06 | 6.4e-09 | 0 | 0 | 1955 |
| DC* | | | | | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1.3e-04 | 0 | 0 | 0 | 0 | 0 | 61 |
| FL | | X | X | | 46 | 1156 | 665 | 293 | 30 | 4 | 0 | 2148 | 1.5e-05 | 8.6e-06 | 2.2e-06 | 2.8e-07 | 2.0e-08 | 0 | 53997 |
| GA | | X | | | 46 | 147 | 537 | 266 | 65 | 17 | 0 | 1032 | 2.9e-05 | 3.0e-05 | 1.2e-05 | 3.4e-06 | 4.3e-07 | 0 | 57919 |
| ID | | | | X | 42 | 63 | 53 | 8 | 0 | 0 | 0 | 124 | 4.7e-07 | 1.9e-07 | 1.4e-08 | 0 | 0 | 0 | 82751 |
| IN | X | | | | 46 | 246 | 336 | 263 | 108 | 77 | 8 | 1038 | 3.3e-05 | 3.5e-05 | 1.5e-05 | 5.2e-06 | 1.2e-06 | 6.7e-08 | 35870 |
| IA | X | | | | 46 | 478 | 506 | 421 | 119 | 74 | 9 | 1607 | 3.7e-05 | 3.7e-05 | 1.4e-05 | 3.1e-06 | 6.1e-07 | 2.5e-08 | 55875 |
| IL | X | | | | 46 | 431 | 440 | 316 | 113 | 39 | 3 | 1342 | 3.0e-05 | 2.7e-05 | 9.8e-06 | 2.5e-06 | 3.3e-07 | 2.1e-08 | 55875 |
| KS | X | X | | | 46 | 1111 | 610 | 404 | 168 | 54 | 16 | 2363 | 3.5e-05 | 3.0e-05 | 1.1e-05 | 3.0e-06 | 5.8e-07 | 1.1e-07 | 81823 |
| KY | X | | | | 46 | 79 | 168 | 133 | 65 | 35 | 3 | 483 | 1.6e-05 | 1.7e-05 | 6.9e-06 | 1.8e-06 | 3.1e-07 | 1.4e-08 | 39732 |
| LA | | X | | | 46 | 225 | 620 | 268 | 123 | 16 | 2 | 1254 | 2.4e-05 | 2.2e-05 | 6.9e-06 | 1.4e-06 | 1.2e-07 | 1.9e-08 | 43566 |
| ME | | | | X | 42 | 21 | 44 | 17 | 0 | 0 | 0 | 82 | 1.8e-06 | 1.1e-06 | 1.7e-07 | 0 | 0 | 0 | 30865 |
| MD | | | X | | 46 | 49 | 92 | 26 | 5 | 0 | 0 | 172 | 1.5e-05 | 9.2e-06 | 9.4e-07 | 8.2e-09 | 0 | 0 | 9775 |
| MA | | | X | | 45 | 24 | 72 | 31 | 8 | 3 | 0 | 138 | 1.2e-05 | 1.1e-05 | 4.3e-06 | 1.6e-06 | 3.7e-07 | 0.0e+00 | 7838 |
| MI | | X | X | | 45 | 195 | 308 | 210 | 57 | 30 | 7 | 807 | 1.4e-05 | 1.4e-05 | 5.2e-06 | 1.4e-06 | 2.8e-07 | 1.4e-08 | 56809 |
| MN | | X | X | | 46 | 372 | 336 | 158 | 53 | 28 | 6 | 953 | 1.4e-05 | 1.2e-05 | 3.5e-06 | 7.2e-07 | 1.3e-07 | 6.6e-09 | 79617 |
| MS | X | X | | | 46 | 226 | 468 | 369 | 136 | 59 | 10 | 1268 | 4.4e-05 | 4.4e-05 | 1.7e-05 | 5.0e-06 | 1.0e-06 | 1.3e-08 | 46914 |
| MO | X | | | | 46 | 298 | 577 | 334 | 109 | 48 | 1 | 1367 | 1.8e-05 | 1.6e-05 | 5.3e-06 | 1.3e-06 | 2.3e-07 | 2.6e-11 | 68898 |
| MT | | | | X | 44 | 174 | 42 | 33 | 4 | 0 | 0 | 253 | 1.0e-06 | 7.0e-07 | 2.3e-07 | 2.2e-08 | 0 | 0 | 145556 |
| NE | | X | X | | 46 | 827 | 585 | 255 | 105 | 42 | 4 | 1818 | 2.9e-05 | 2.9e-05 | 1.2e-05 | 3.5e-06 | 3.5e-07 | 1.6e-08 | 76878 |
| NV | | | | X | 34 | 41 | 8 | 0 | 0 | 0 | 0 | 49 | 2.9e-07 | 4.0e-08 | 0 | 0 | 0 | 0 | 109806 |
| NH | | | | X | 45 | 24 | 34 | 15 | 2 | 0 | 0 | 75 | 4.7e-06 | 2.4e-06 | 4.7e-07 | 1.1e-08 | 0 | 0 | 8969 |

Table A4-4 SPC Data Analysis Summary by State

| State | NUREG/CR -2944 Region | | | | Years | Tornado F-scale | | | | | | Total | Point strike probability (per year) | | | | | | Land Area (mi ²) |
|-------|--------------------------|---|---|---|-------|-----------------|-------|------|------|-----|-----|-------|-------------------------------------|---------|---------|---------|---------|---------|---------------------------------|
| | A | B | C | D | | F0 | F1 | F2 | F3 | F4 | F5 | | F0 | F1 | F2 | F3 | F4 | F5 | |
| NJ | | | X | | 45 | 43 | 58 | 23 | 4 | 0 | 0 | 128 | 1.7e-05 | 6.6e-06 | 7.9e-07 | 7.1e-09 | 0 | 0 | 7419 |
| NM | | | X | | 46 | 261 | 104 | 31 | 4 | 0 | 0 | 400 | 1.5e-06 | 5.2e-07 | 8.0e-08 | 1.1e-09 | 0 | 0 | 121365 |
| NY | | | | X | 44 | 101 | 106 | 35 | 21 | 5 | 0 | 268 | 7.6e-06 | 6.1e-06 | 2.3e-06 | 8.8e-07 | 2.2e-07 | 0 | 47224 |
| NC | | | X | | 46 | 153 | 321 | 143 | 44 | 26 | 0 | 687 | 1.5e-05 | 1.4e-05 | 4.9e-06 | 1.5e-06 | 2.5e-07 | 0 | 48718 |
| ND | | | X | | 46 | 490 | 211 | 91 | 28 | 7 | 3 | 830 | 4.7e-06 | 3.2e-06 | 1.1e-06 | 3.6e-07 | 9.1e-08 | 1.1e-08 | 68994 |
| OH | X | | | | 46 | 157 | 321 | 166 | 53 | 27 | 9 | 733 | 2.1e-05 | 1.8e-05 | 5.6e-06 | 1.3e-06 | 3.0e-07 | 2.8e-08 | 40953 |
| OK | X | | | | 46 | 845 | 808 | 626 | 209 | 83 | 9 | 2580 | 4.1e-05 | 3.9e-05 | 1.4e-05 | 3.6e-06 | 7.0e-07 | 5.5e-08 | 68679 |
| OR | | | | X | 45 | 31 | 15 | 3 | 0 | 0 | 0 | 49 | 2.9e-07 | 1.5e-07 | 3.1e-08 | 0 | 0 | 0 | 96003 |
| PA | | | X | | 46 | 93 | 220 | 143 | 26 | 22 | 2 | 506 | 9.4e-06 | 9.0e-06 | 3.3e-06 | 9.3e-07 | 2.0e-07 | 5.4e-09 | 44820 |
| RI | | | X | | 23 | 3 | 4 | 1 | 0 | 0 | 0 | 8 | 1.9e-05 | 1.3e-05 | 1.7e-06 | 0 | 0 | 0 | 1045 |
| SC | | X | | | 46 | 136 | 234 | 100 | 31 | 15 | 0 | 516 | 1.9e-05 | 1.9e-05 | 6.8e-06 | 1.8e-06 | 3.0e-07 | 0 | 30111 |
| SD | | X | X | | 46 | 651 | 259 | 197 | 57 | 7 | 1 | 1172 | 9.7e-06 | 8.1e-06 | 3.0e-06 | 7.7e-07 | 1.5e-07 | 1.2e-08 | 75898 |
| TN | X | | | | 46 | 107 | 241 | 139 | 76 | 29 | 4 | 596 | 2.2e-05 | 2.2e-05 | 8.3e-06 | 2.1e-06 | 2.0e-07 | 1.7e-10 | 41220 |
| TX | | X | X | | 46 | 2632 | 1837 | 1067 | 317 | 76 | 5 | 5934 | 1.6e-05 | 1.3e-05 | 4.3e-06 | 1.1e-06 | 1.8e-07 | 3.8e-09 | 261914 |
| UT | | | | X | 43 | 53 | 19 | 6 | 1 | 0 | 0 | 79 | 5.1e-07 | 3.2e-07 | 1.0e-07 | 2.8e-08 | 0 | 0 | 82168 |
| VT | | | | X | 41 | 7 | 14 | 12 | 0 | 0 | 0 | 33 | 3.3e-06 | 2.0e-06 | 3.4e-07 | 0 | 0 | 0 | 9249 |
| VA | | | X | | 45 | 84 | 132 | 68 | 28 | 6 | 0 | 318 | 8.5e-06 | 7.0e-06 | 2.0e-06 | 4.4e-07 | 7.1e-08 | 0 | 39598 |
| WA | | | | X | 41 | 24 | 17 | 12 | 3 | 0 | 0 | 56 | 4.9e-07 | 9.6e-08 | 2.3e-08 | 3.6e-09 | 0 | 0 | 66582 |
| WV | | | X | | 45 | 27 | 36 | 16 | 8 | 0 | 0 | 87 | 2.2e-06 | 2.4e-06 | 9.7e-07 | 2.5e-07 | 0 | 0 | 24087 |
| WI | | X | X | | 46 | 204 | 378 | 276 | 62 | 24 | 5 | 949 | 2.6e-05 | 2.4e-05 | 7.9e-06 | 1.4e-06 | 2.5e-07 | 3.3e-08 | 54314 |
| WY | | | | X | 46 | 247 | 145 | 43 | 8 | 1 | 0 | 444 | 2.5e-06 | 1.2e-06 | 3.1e-07 | 7.1e-08 | 1.9e-08 | 0 | 97105 |
| Sum | | | | | | 13776 | 13251 | 7834 | 2553 | 924 | 121 | 38459 | | | | | | | 3536342 |

* - DC was not included in the exceedance analysis.

Figure A4-1

**Annual Average Number of Tornadoes per
10,000 Square Miles by State, 1950-1995**

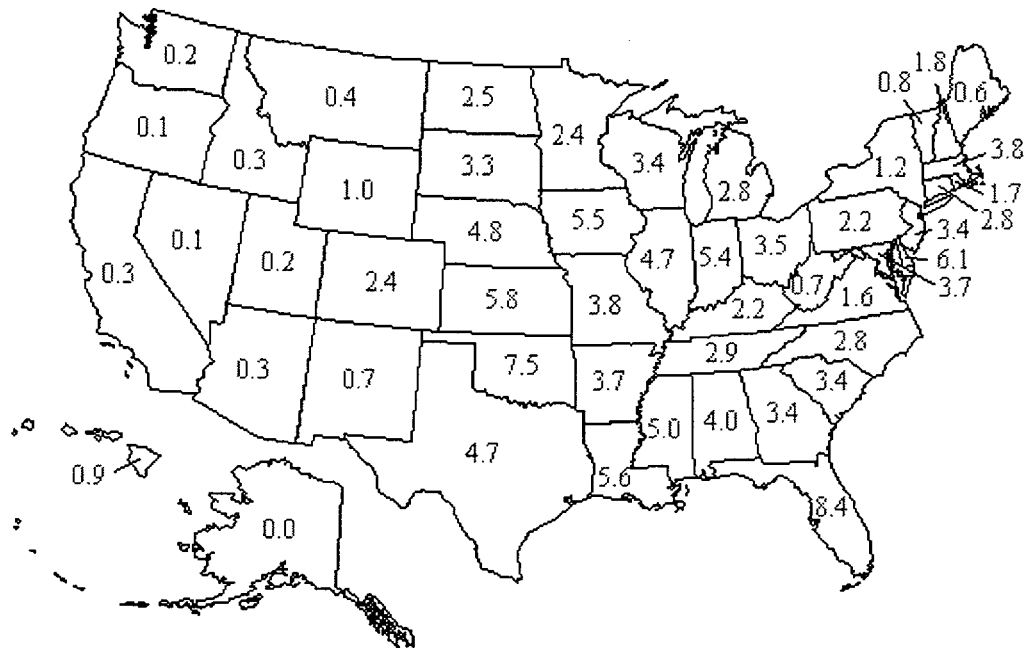


Figure A4-2

**Average Annual Number of Strong-Violent (F2-F5)
Tornadoes per 10,000 Square Miles by State**

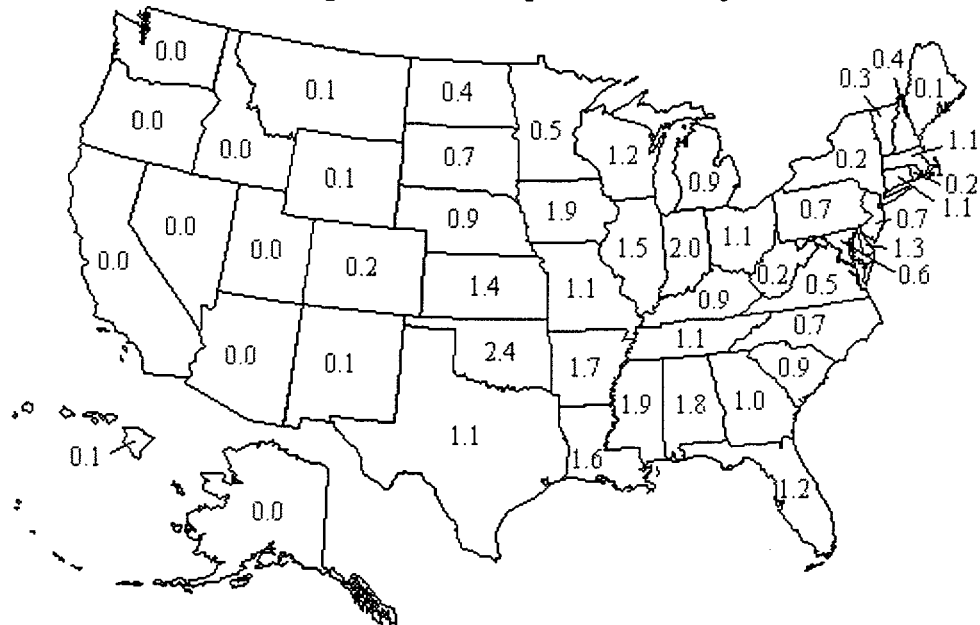


Figure A4-3 Sketch of Hypothetical F2 Tornado Illustrating Variations

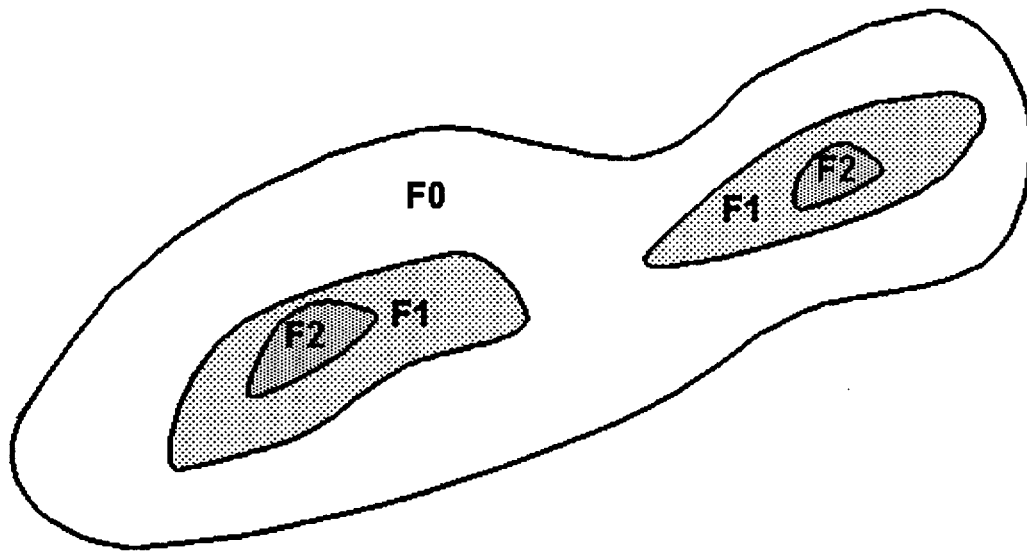


Figure A4-4 Tornado Risk Regionalization Scheme (from NUREG/CR-2944)

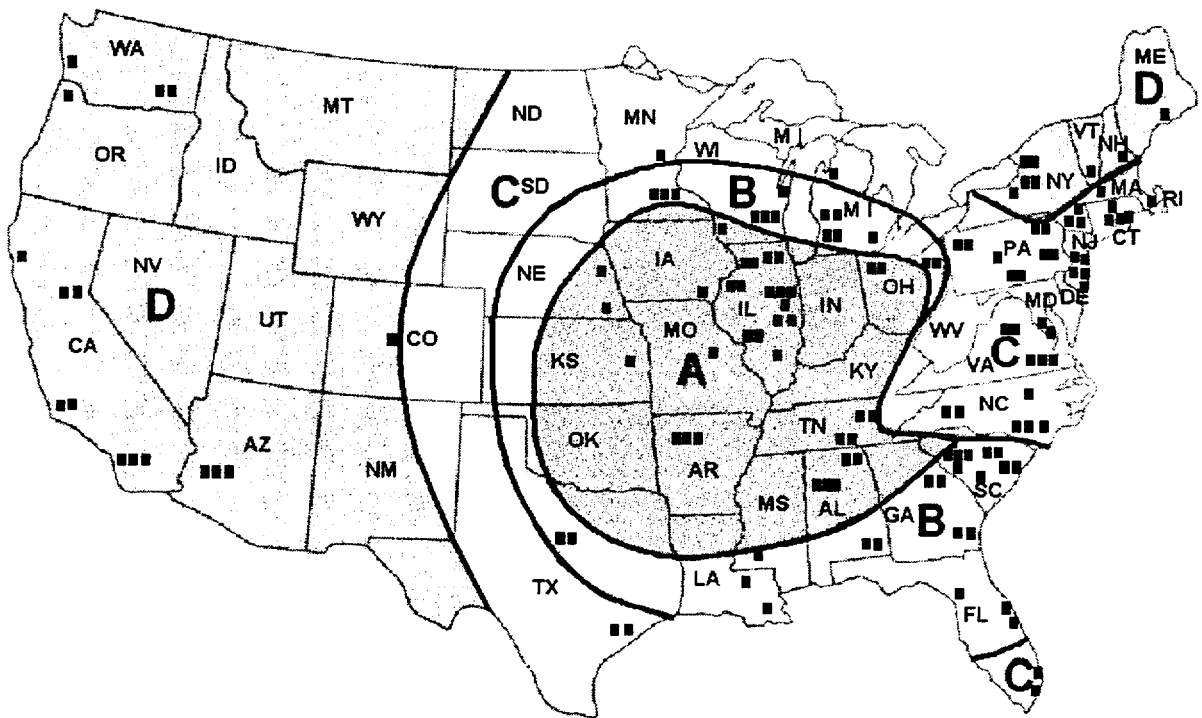


Figure A4-5 Tornado Exceedance Probability for each F-scale

