

**STONE & WEBSTER ENGINEERING CORPORATION**  
**CALCULATION TITLE PAGE**

CLIENT & PROJECT: Private Fuel Storage, LLC – Private Fuel Storage Facility				PAGE 1 OF 28 +Attach. 1(8 pgs)+Attach. 2 (9 pgs)+Attach. 3 (10 pgs) + Attach. 4 (2 pgs) + Attach. 5 (9 pgs) + Attach. 6 (5 pgs)	
CALCULATION TITLE (Indicative of Objective):  <b>PFSF Flood Analysis with Larger Drainage Basin</b>				<b>QA CATEGORY</b> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> - I Nuclear Safety Related <input type="checkbox"/> - II <input type="checkbox"/> - III <input type="checkbox"/> - Non-Safety Related <input type="checkbox"/> - <input type="checkbox"/> - Fossil/Industrial Plant	
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<b>0599602</b>		<b>G(B)-12</b>		<b>345T</b>	
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V. N. Zeng 02/08/1999 <i>V. N. Zeng</i>	George H.C. Liang <i>George H.C. Liang</i>	George H.C. Liang <i>George H.C. Liang</i>	0	N/A	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO
V. N. Zeng 03/22/1999 <i>V. N. Zeng</i>	George H.C. Liang 03/22/1999 <i>George H.C. Liang</i>	George H.C. Liang 03/22/1999 <i>George H.C. Liang</i>	1	N/A	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO
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**RECORD OF CHANGES**

<b>Rev No.</b>	<b>Description of Changes</b>	<b>Pages Revised</b>	<b>Pages Added</b>	<b>Pages Replaced</b>
0	Original Issue	N/A	N/A	N/A
1	Add editorial items & correct errors	As highlighted on the pages		
	Add Record of Changes	2		
	Edit Table of Contents entries	3		
	Add References 10, 11, & 12.	4		
	Edit text	5		
	Edit text	6		
	Delete bullet and word from text	7		
	Add north arrow	8		
	Edit row 7 in Table 3	12		
	Edit text	15		
	Change Table 5 to include explanation of variables	16		
	Add to Table 6- Water level for additional case	17		
	Figure 4, add additional information and north arrow	18		
	Add north arrow	19		
	Add Section 8 "Discussion"	23 & 24		
	Add Fig. 12 & Fig.13	25 & 28		
	Add Table 7 and text	26 & 27		

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<b>Attachment 3</b>	<b>10 pages</b>
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## 1, Objectives

The objective of the calculation is to determine water surface elevation in the floodway crossing the PFSF access road to the east of PFSF site. The 100-year and the PMF flood events are evaluated based on the existing natural ground topography.

## 2, References

1. Calculation 05996.01-G(B)-02, "The PMF and the 100-yr Flood Flow at the Access Road Crossing and the PFSF Site"
2. U.S. Department of Commerce, National Oceanic And Atmospheric Administration, 1977, "Probable Maximum Precipitation Estimates, Colorado River and Great Basin Drainage" Hydrometeorological Report No. 49.
3. "Runoff Estimates for small Rural Watersheds and Development of a Sound Design Method" 1977, Federal Highway Administration. Report No. FHWA-RD-77-159.
4. "Nationwide Summary of U.S. Geological Survey Regional Regression Equations for Estimating Magnitude and Frequency of Flood for Ungaged Sites" 1993. U.S. Geological Survey, Water-Resources Investigation Report 94-4002.
5. U.S.Army Corps of Engineers, Hydrologic Center, "HEC-RAS, River Analysis System", 1997.
6. Calculation 05996.01-G(B)-10, Rev 0, "HEC-RAS Micro Computer Version 1.2 Software Test", May 20, 1997.
7. U.S.Army Corps of Engineers, Office of the Chief Engineers, "HEC-1, Flood Hydrograph Package", 1981.
8. Calculation 05996.01-G(B)-08, Rev 1, "HEC-1 Flood Hydrograph Package, Micro Computer Version 4.0 Software Test, QS 2-7", May 20, 1997.
9. "Engineering Hydrology" by Victor M. Ponce
10. "Guide for the Use of Technical Release No. 55 - Urban Hydrology", USDA Soil Conservation Services, Dec, 1977.
11. Private Fuel Storage L.L.C., "Safety Analysis Report, Private Fuel Storage Facility, Docket No. 72-22". Skull Valley Indian Reservation, Tooele County, Utah.
12. "Hydrologic Analysis and Design", by Richard H McCuen. Prentice Hall.

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### 3, Methodology

The estimation of the flood level involves two steps:

- (1) Perform hydrological analysis to determine flood flow discharge (Runoff).
- (2) Perform hydraulic analysis to calculate water surface elevation.

#### 3.1, PMF

The PMF is defined as the most severe flood that is considered reasonably possible at a site as a result of hydrologic and meteorologic meteorological conditions. Two possible types of PMF are possible in the Skull Valley Region where PFSF is located: (1) General Storm PMF which resulted from the convergence precipitation and the orographic precipitation (see note below). (2) Local PMF - While the general storm PMF is a major concern, the summer thunder storm having the greatest potential rainfall intensity and short durations may produce a larger PMF. This PMF is termed as local PMF in Reference 2 and in this calculation.

Note:

- Convergence precipitation - Precipitation caused by convective lifting , and therefore cooling of the moist air, assuming not affected by terrain.
- Orographic precipitation - Precipitation caused by lifting of moist horizontal air current over the mountain range or other natural barrier.

The general storm PMF and the local storm PMF are evaluated separately. The larger of the two is used to compute the flood level.

The first step to determine PMF is to define Probable Maximum Precipitation (PMP) from the precipitation information and procedure provided by Reference 2. The PMP is then input to the HEC-1 program (Reference 7) to calculate the runoff hydrograph.

Precipitation losses - In calculating runoff flow using HEC-1 program, the infiltration loss and other precipitation losses must be defined. The Soil Conservation Service (SCS) has developed a Curve Number Procedure for estimating runoff based on field studies of the measured runoff from numerous soil cover combinations. This method was adopted by the HEC-1 program as one of the options to account for the precipitation losses. In this analysis, the Skull Valley soil is assumed to be in the Curve Number 70 hydrologic soil group.

Unit hydrograph - The conversion of the precipitation excess (precipitation - infiltration and other losses) to runoff is accomplished by executing the HEC-1 program using SCS dimensionless unit hydrograph as basis. The "lag time" parameter, which is approximated by 0.6 times T<sub>c</sub> (concentration time), is input required to convert the dimensionless unit hydrograph to the basin unit hydrograph. The concentration time is estimated using Hathaway Equation (Ref. 9) in Table 1, This equation includes a roughness coefficient to account for different soils.

T<sub>c</sub> = 18.31 hours

Lag time = 0.6 x 18.31 = 11 hr (HEC-1 data)

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The second method using Kirpich Equation, which does not consider the soil type, is also calculated in the table for reference.

**Table 1**

**PFSF, Estimate Concentration Time From South Rim of Basin to Access Road**

Kirpich Formula:  $T_c = (0.0078 \times L^{0.77}) / S^{0.385}$

Hathaway Formula:  $T_c = 0.0606 \times (L \times n)^{0.467} / S^{0.234}$ , n is the roughness for various types of surface

From Elev 1 ft	To Elev 2 ft	L mile	L ft	L Km	S	n	Kirpich Tc hour	Hathaway Tc hour	
6400	5400	3.5	18480	5.6	0.054113	0.5	0.77	1.95	Trees
5400	5200	1.0	5280	1.6	0.037879	0.2	0.34	0.77	
5200	5000	2.5	13200	4.0	0.015152	0.5	0.97	2.24	Pasture
5000	4800	4.9	25872	7.9	0.007730	0.5	2.11	3.59	Pasture
4800	4600	8.4	44352	13.5	0.004509	0.5	3.94	5.24	Pasture
4600	4465	6.0	31680	9.7	0.004261	0.5	3.11	4.53	Pasture
<b>Total</b>		<b>26.3</b>					<b>11.24</b>	<b>18.31</b>	

### 3.2, 100-year Flow

The 100-year flow is estimated using regression equations provided in References 3 and 4.

### 3.3, Hydraulic Analysis

Flood level profile for the PMF and the 100-year flow are computed using the HEC-RAS program (Reference 5).

### 3.4, Computer Programs

The two computer programs, HEC-1 for the hydrological analysis and HEC-RAS for the hydraulic calculation, have been tested and qualified by Stone & Webster (References 5, 6, 7, and 8).

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#### 4, Hydrological Analysis

##### 4.1, Drainage Area

As shown in Figure 1, watershed areas that contribute runoff to the floodway which flows south to north through the access road, is primarily from the following sources:

- West slope of the Stansbury Mountains, south of Indian Hickman Canyon.
- West slope of the Onaqui Mountains.
- North slope of the Lookout Mountain.
- South tip of the Lower Cedar Mountain Range below White Rock Spring.
- Lowlands in the valley sounded by the above 4.

The total drainage area is about **270 square miles**. The distance from PFSF site to the farthest boundary point near Lookout Mountain is about **26 miles**.

Precipitation runoff from the Cedar Mountain slope and the associated discharge fan would not converged to the above mentioned floodway.

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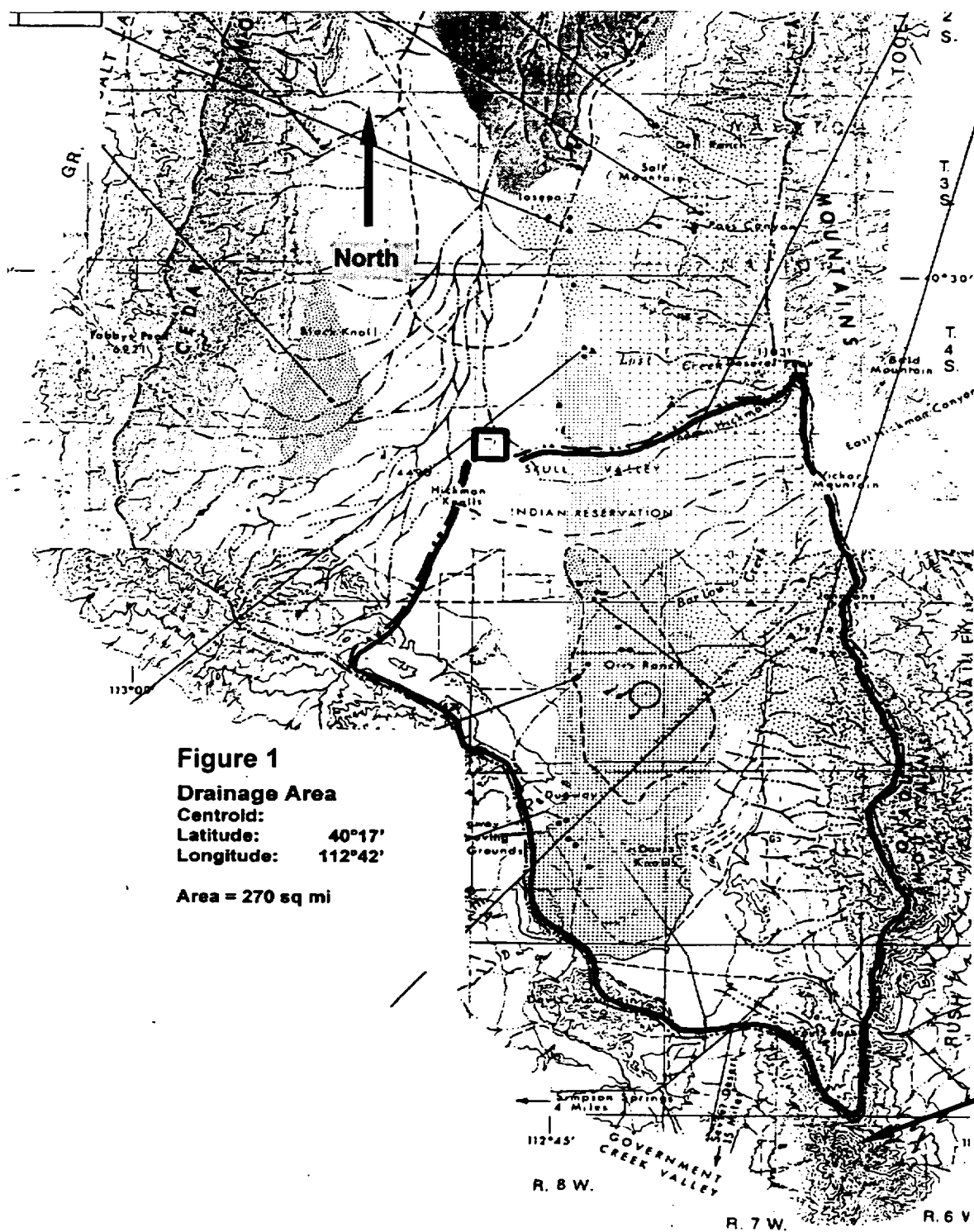


Figure 1

Drainage Area

Centroid:

Latitude: 40°17'

Longitude: 112°42'

Area = 270 sq mi

Base from Army Map Service 1:250,000  
series: Tooele (1962)

CONTOUR INTERVAL 200 FEET  
WITH SUPPLEMENTARY CONTOURS AT 100 FOOT  
DATUM IS MEAN SEA LEVEL



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#### 4.2, General Storm PMP

Table 1 computes general storm PMP for the 6, 12, 18, 24, 48, and 72 hours in item C. The result is plotted in Figure 2. The values of the 3-hour interval precipitation are read from Figure 2 and listed in Table 2.

Table 2 also calculates the 3-hour incremental PMP. Time distribution of the 18 hour incremental is composed in the 3-1-2-4 sequence in the last column for HEC-1 input.

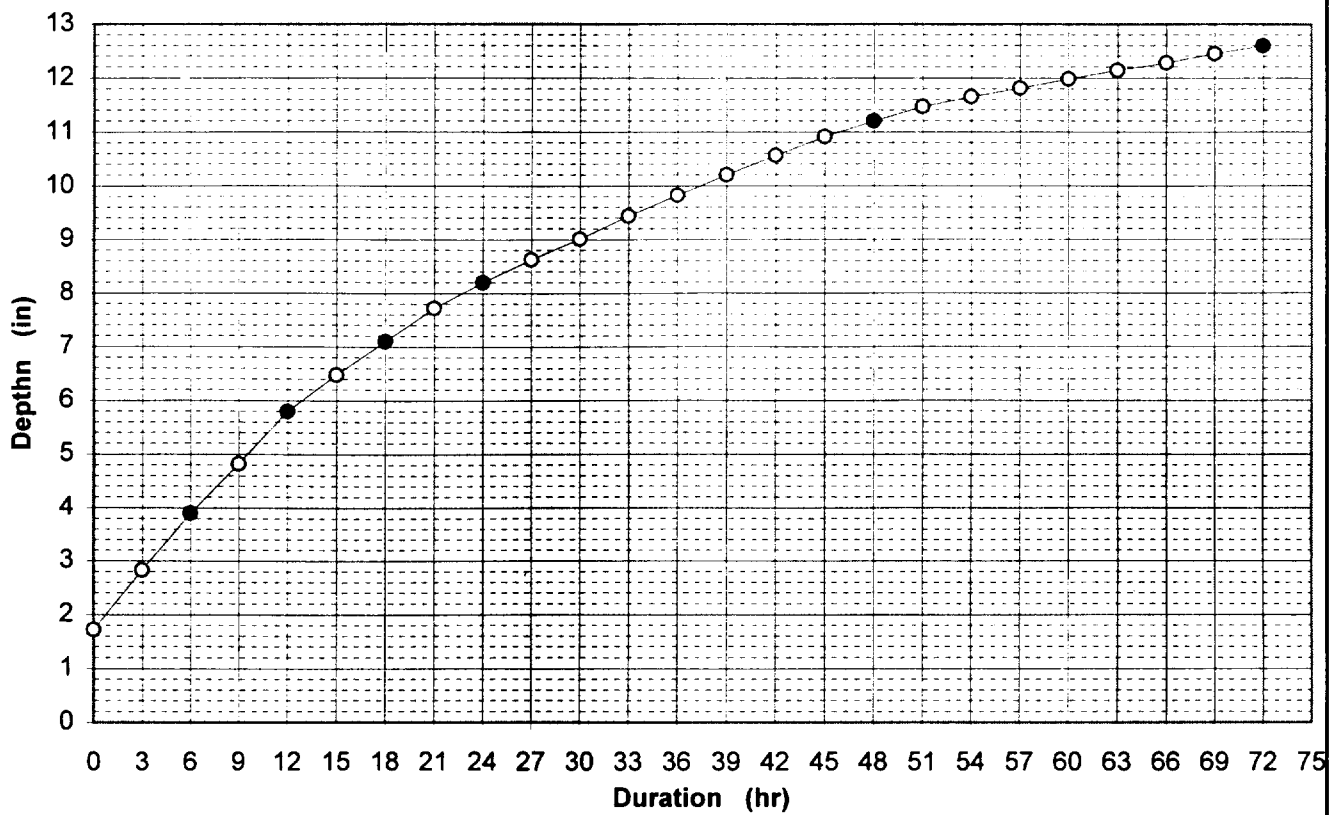
**Table 1, General Storm PMP Computation (Refer all figures and tables to Ref. 2)**

General Storm PMP Computation										
Based on NOAA Report No. 49 "Probable Maximum Precipitation Estimates, Basin Drainages, Colorado River and Great Basin Drainages"										
Drainage: Access Road Crossing			Latitude: 40°17'			Month: August				
Area (mi <sup>2</sup> ): 270 mi <sup>2</sup>			Longitude: 112°42'							
A. Convergence PMP										
1. Drainage average value			Fig 2.5 - 2.16		10.7 in					
2. Reduction for barrier elev			Fig 2.18		55 %					
3. Barrier-elev reduced PMP			1 x 2		5.9 in					
			Duration (hrs)							
			6	12	18	24	48	72		
4. Duration variation			Fig 2.25 - 2.27, & Table 2.7		67	85	94	100	116	123 %
5. Convergence PMP for indicated duration			3 x 4		3.9	5.0	5.5	5.9	6.8	7.2 in
6. Incremental 10 mi2 PMP			Successive - of 5		3.9	1.1	0.5	0.4	0.9	0.4 in
7. Area reduction			Fig 2.28 & 2.29		72	89	94	98	100	100 %
8. Areally reduced PMP			6 x 7		2.8	0.9	0.5	0.3	0.9	0.4 in
9. Drainage average PMP			Accu 8		2.8	3.8	4.3	4.6	5.6	6.0 in
B. Orographic PMP										
1. Drainage average orographic index			Fig 3.11a - d		4 in					
2. Areal reduction			Fig 3.20		88.5 %					
3. Adjustment for month			Fig 3.12 - 3.17		100 %					
4. Areally & seasonally adjusted PMP			1 x 2 x 3		3.5 in					
			Duration (hrs)							
			6	12	18	24	48	72		
5. Durational variation			Table 3.9		30	57	80	100	159	187 %
6. Orographic PMP for given duration			4 x 5		1.1	2.0	2.8	3.5	5.6	6.6 in
C. Total PMP										
1. A9+B6			3.9 5.8 7.1 8.2 11.2 12.6 in							

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**Figure 2, General PMP (3 hr interval)**

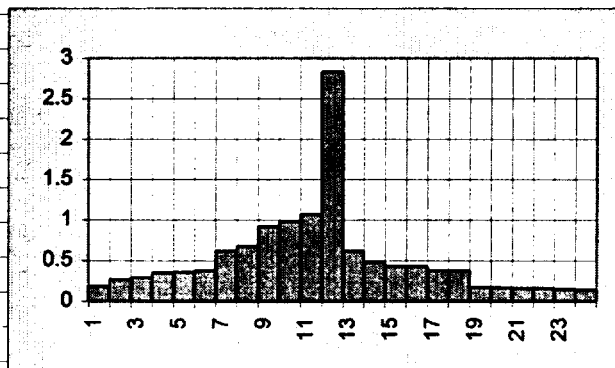


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**Table 2, Synthetic Rainfall Hyetograph (General Storm PMF)**

	Hour	3-Hour PMP (in)	PMP Increment		Input to HEC-1 Hyetograph
<b>1</b>	0	1.72			
	3	2.83	2.83	<b>3</b>	0.18
	6	3.9	1.07		0.27
	9	4.82	0.92		0.29
	12	5.8	0.98		0.35
	15	6.48	0.68		0.36
	18	7.1	0.62		0.38
<b>2</b>	21	7.72	0.62	<b>1</b>	0.62
	24	8.2	0.48		0.68
	27	8.63	0.43		0.92
	30	9.01	0.38		0.98
	33	9.44	0.43		1.07
	36	9.82	0.38		2.83
<b>3</b>	39	10.2	0.38	<b>2</b>	0.62
	42	10.56	0.36		0.48
	45	10.91	0.35		0.43
	48	11.2	0.29		0.43
	51	11.47	0.27		0.38
	54	11.65	0.18		0.38
<b>4</b>	57	11.81	0.16	<b>4</b>	0.17
	60	11.98	0.17		0.17
	63	12.14	0.16		0.16
	66	12.28	0.14		0.16
	69	12.45	0.17		0.15
	72	12.6	0.15		0.14



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### 4.3, Local Storm PMP

Table 3 computes local storm PMP at ¼, ½, ¾ and 1, 2, 3, 4, 5 and 6 hours, The resulting precipitation is shown in item 7 of the table and is plotted in Figure 3.

From Figure 3, the 15-min pmp PMP is interpolated and the corresponding incremental are calculated in Table 4. The incremental precipitation is rearranged in 5-3-1-2-4-6 sequence to form time distribution precipitation for HEC-1 input.

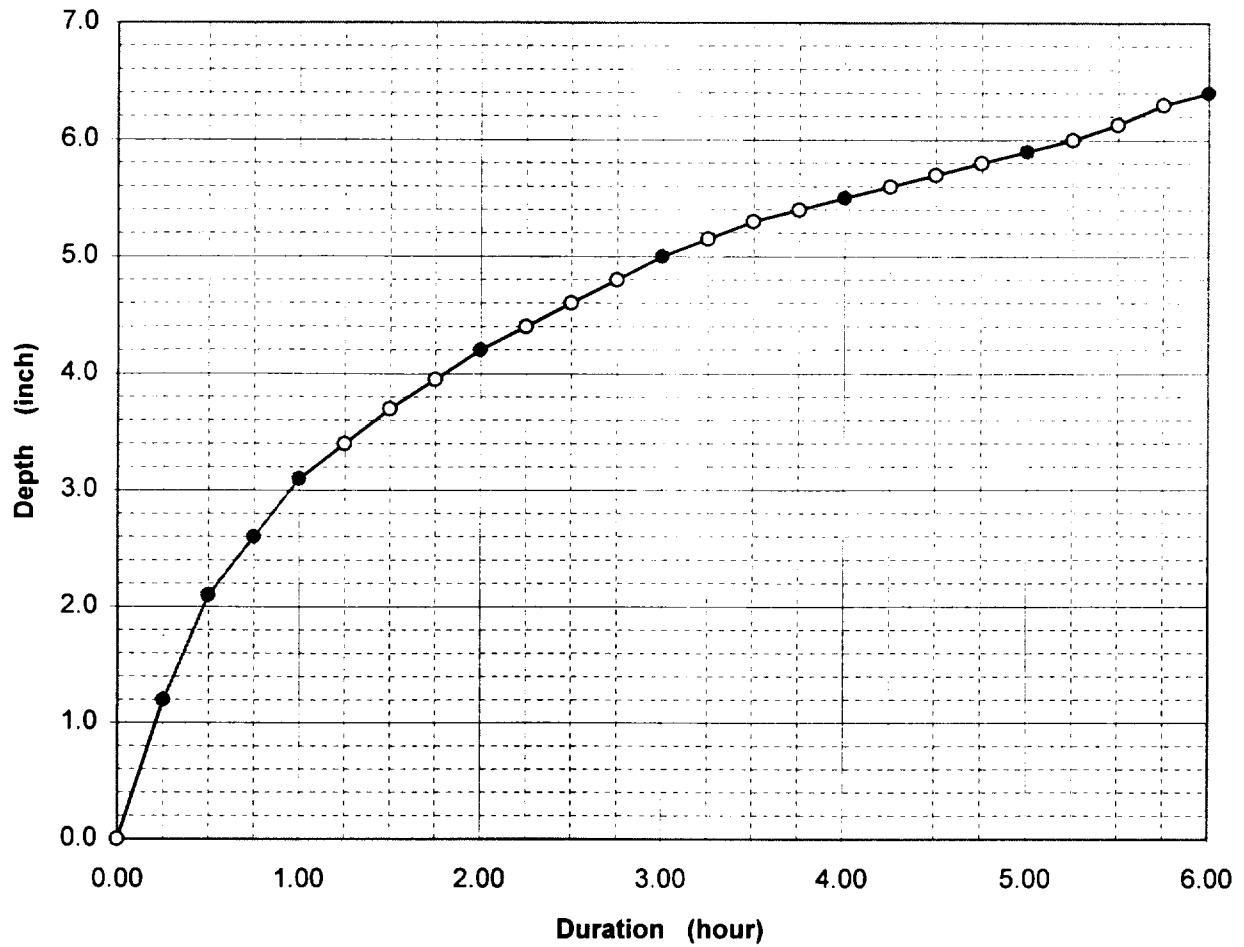
**Table 3, Local Storm PMP Computation (Refer all figures and tables to Ref. 2)**

Local Storm PMP Computation												
PFSF (Private Fuel Storage Facility) Project												
Based on NOAA Report No. 49 "Probable Maximum Precipitation Estimates, Colorado River and Great Basin Drainages"												
Drainage: Access Road		Latitude:		40°17'								
Area (mi <sup>2</sup> ): 270 mi <sup>2</sup>		Longitude:		112°42'		Minimum Elev 4465 ft						
1. Average 1-hr 1 mi <sup>2</sup> PMP for drainageFig 4.5, Page 115		10.1		in								
2a. Reduction for elev		50		%								
No adjustment up to 5000'												
5% decrease/1000' above 5000'		100		%								
2b. 1 x 2a		10.1		in								
3. Average 6/1 hour ratio for drainageFig 4.7 - Page 11		1.4										
				Duration (hrs)								
		0.25		0.50	0.75	1.00	2.00	3.00	4.00	5.00	6.00	
4. Durational variation for 6/1-hr ratio Table 4.4, Page 1		63		83	93	100	118	126	132	137	140	%
5. 1-mi2 PMP for indicated durations 2b x 4		6.4		8.4	9.4	10.1	11.9	12.7	13.3	13.8	14.1	in
6. Areal reduction Fig 4.9, Page 123		19.0		24.5	27.5	31.0	35.0	39.0	41	43	45	%
7. Area reduced PMP 5 x 6		1.2		2.1	2.6	3.1	4.2	5.0	5.5	5.9	6.4	in
8. Incremental PMP Success (-) in 7												
		15 min increments										
		1.2		0.8	0.5	0.5						
9. Time sequences of incremental PMP												
Hourly increments						0.5	0.8	3.1	1	0.5	0.4	
Four largest 15-min.		1.2		0.8	0.5	0.5						

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Figure 3, Local PMP (15-min interval)



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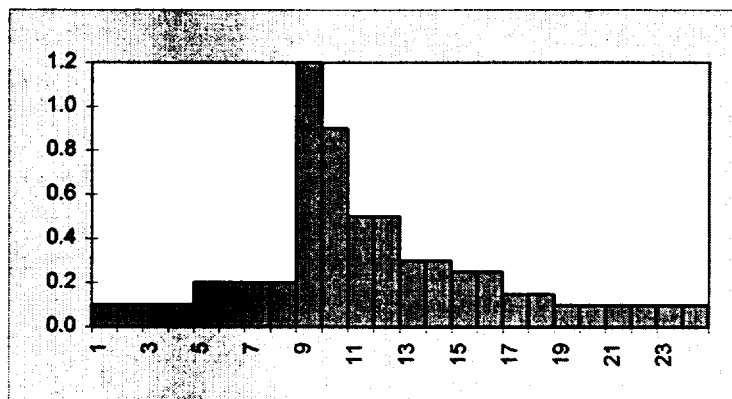
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**Table 4, Synthetic Rainfall Hyetograph (Local Storm PMF)**

Computation of 15-min PMP and Incremental

HEC-1  
Input  
5-3-1-2-4-6

Duration	No	Depth	No	Incremental		
0.00		0.0				
0.25	1	1.2	1	1.2	5	0.1
0.50		2.1		0.9		0.1
0.75		2.6		0.5		0.1
1.00		3.1		0.5		0.1
1.25	2	3.4	2	0.3	3	0.2
1.50		3.7		0.3		0.2
1.75		4.0		0.3		0.2
2.00		4.2		0.3		0.2
2.25	3	4.4	3	0.2	1	1.2
2.50		4.6		0.2		0.9
2.75		4.8		0.2		0.5
3.00		5.0		0.2		0.5
3.25	4	5.2	4	0.2	2	0.3
3.50		5.3		0.1		0.3
3.75		5.4		0.1		0.3
4.00		5.5		0.1		0.3
4.25	5	5.6	5	0.1	4	0.2
4.50		5.7		0.1		0.1
4.75		5.8		0.1		0.1
5.00		5.9		0.1		0.1
5.25	6	6.0	6	0.1	6	0.1
5.50		6.1		0.1		0.1
5.75		6.3		0.2		0.1
6.00		6.4		0.1		0.1



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### 5, Result of PMF and 100-year Runoff Flow

#### PMF

Precipitation data developed in the the last column of Table 2 and 4, is input to HEC-1 program to compute hydrograph at the Access Road, the outlet of the drainage basin. The result of HEC-1 runs made for the general storm PMF and the local storm PMF are included in Attachments 1 and 2. The peaks of hydrographs are:

General Storm PMF:	Q = 52983 cfs
Local Storm PMF:	Q = 40237 cfs

Since the general storm PMF is greater, the final PMF for the hydraulic computation is determined to be:

$$Q_{PMF} = 53,000 \text{ cfs}$$

#### 100-year flow

The 100-year flow for the 270 mi<sup>2</sup> drainage basin is estimated from the FHWA method (Ref. 3) and the USGS Method (Ref. 4)

**FHWA Method** - Based on hydrological analysis of many watersheds, the Federal Highway Administration has developed a method to estimate peak runoff for the ungaged watersheds. The step-by-step procedure of this method is described in Ref. 3. Detail calculation using this method is included in Table 5. The result is

$$Q_{100} = 2430 \text{ cfs}$$

**USGS Method** - The USGS has also developed flood-regionalization procedures to predict the magnitude of peak runoff (Ref.4). The 50 states in the country are divided into several hydrophysiographic zones. Within each zone, regression equations are developed to compute peak runoff for various return periods of flood. In the Skull Valley of Utah where PFSF is located, The regression equation for 100-year flood is

$$Q_{100} = 68.1 \times A^{0.63}, \text{ where } A \text{ is the drainage area in square miles.}$$

$$Q_{100} = (68.1)(270^{0.63}) = 2317 \text{ cfs}$$

Since the flow calculated by FHWA method is greater, the 100-year flood flow is determined to be 2430 cfs

FHWA Method:  $Q_{100} = 2,430 \text{ cfs}$  (Table 5)

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USGS Method  ~~$Q_{100} = 68.1 \times A^{0.42} = (68.1)(270^{0.42}) = 2317 \text{ cfs}$~~

Use  $Q_{100} = 2430 \text{ cfs}$  for hydraulic analysis.

Table 5, Calculating 100-year flow using FHWA method (Based on Ref 3)

**PFSF Utah**

**100-year Flow**

**FHWA Method**

1 Area= 270 sq mi  
Latitude= 40°17'  
Longitude= 112°42'

2 Probable Maximum Runoff Peak  $Q_p(\text{max})$ , See note 1 below.

log(Area)= 2.43  
Exp= 5.70

$Q_p(\text{max}) = 503666 \text{ cfs}$

$$Q_p(\text{max}) = 10^{(3.92 + 0.812(\log A) - 0.0325(\log A)(\log A))}$$

3 Hydrophysiographic Parameters

3a	R=	12	Iso-erodent factor
3b	DH=	1935 ft	Elevation different
3c	S=	0	Reservoir or lake area
3d	Zone	17	Hydrophysiographic zone
3e	L=	25 miles	Principal channel length
3f	P60=	0.92 inch	10-year, 60-minute rainfall
3g	LL=	258 miles	Total channel length including secondary streams
3h	P10=	3.01 inch	10-year, 10-minute rainfall intensity

4 10-year Runoff  $Q_{10}$

$Q_{10} = 1201 \text{ cfs}$  10-year runoff peak, 7 parameter equation (Note 2)

5 Skip

6  $Q_{100} = 2428.9$  say 2430 100-year peak runoff (Note 3)

Note 1: This is the PMF for watersheds in the U.S. and Puerto Rico.

The procedure uses this as a basis to make adjustment for different hydrophysiographic zones of rainfall and soil condition in the country

Note 2:  $Q_{10} = 157.4954 A^{0.5615} R^{1.2801} DH^{-0.6249} L^{-0.0429} LL^{0.4032} P_{10}^{-1.5484} P_{60}^{-0.5034}$

Note 3:  $Q_{100} = 1.6438 Q_{10}^{1.02918}$



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## 6, Water Surface Profile

Cross sections in the HEC-RAS model is plotted in Figure 4. The flow discharges used in the computation are:

$$Q_{100} = 2,430 \text{ cfs}$$

$$Q_{PMF} = 53,000 \text{ cfs}$$

The result of the water surface can be found in Table 6 and the detail hydraulic report is included in Attachment 3.

Figure 5 plots the limit of the floodway.

Figure 6 plot the profile of the water surface.

Figures 7 to 11 shows water levels in each cross-section of Figure4.

**Table 6**

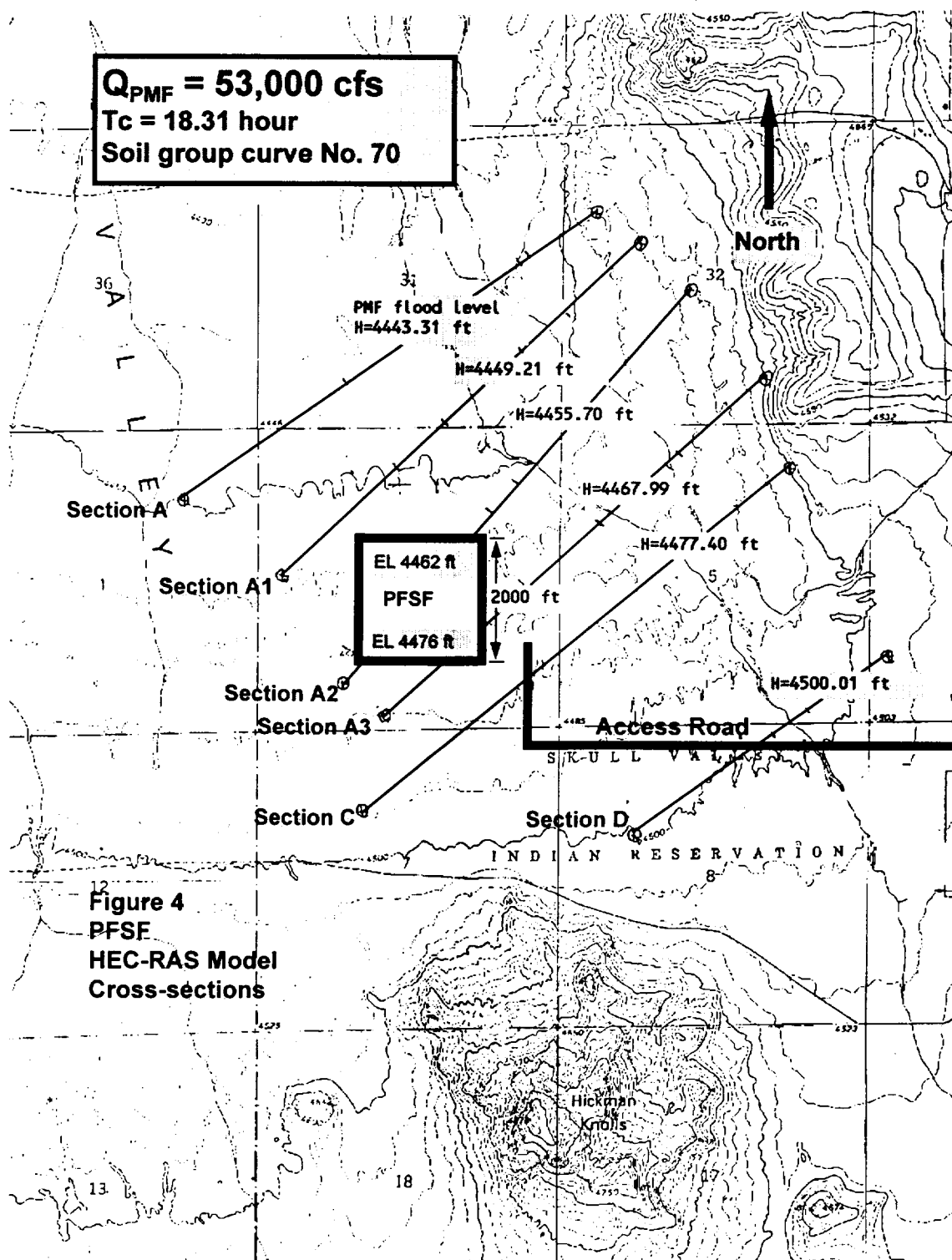
Profile Output Table - Standard Table 1  
HEC-RAS Plan: PFSF\_0 River: Skull Valey Reach: PFSF

# Rivers = 1  
# Hydraulic Reaches = 1  
# River Stations = 18  
# Plans = 1  
# Profiles = 3

Reach	River Sta	Profile	Q Total (cfs)	W.S. Elev (ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude	# Chl
PFSF	9400 D	100-year Q	2430.00	4496.52	5.00	486.13	639.02	1.01	Section D
PFSF	9400	PMF	53000.00	4500.51	7.89	7600.73	4643.96	0.80	
PFSF	9400	PMF1	85000.00	4501.27	9.01	11174.31	4854.65	0.82	
PFSF	5900 C	100-year Q	2430.00	4474.39	1.83	1333.60	1974.90	0.39	Section C
PFSF	5900	PMF	53000.00	4477.40	6.52	9332.06	3331.49	0.60	
PFSF	5900	PMF1	85000.00	4478.35	7.87	12682.43	3756.88	0.64	
PFSF	4500 A3	100-year Q	2430.00	4465.49	3.79	675.00	1570.35		Section A3
PFSF	4500	PMF	53000.00	4467.99	9.26	6975.88	3470.35	0.94	
PFSF	4500	PMF1	85000.00	4468.83	10.50	10154.45	4107.89	0.95	
PFSF	2800 A2	100-year Q	2430.00	4451.91	2.34	1038.28	1087.95	0.42	Section A2
PFSF	2800	PMF	53000.00	4455.70	5.77	9184.57	3065.85	0.59	
PFSF	2800	PMF1	85000.00	4456.72	6.80	12492.89	3383.87	0.62	
PFSF	1300 A1	100-year Q	2430.00	4446.32	2.12	1147.98	1740.88	0.46	Section A1
PFSF	1300	PMF	53000.00	4449.21	5.43	9978.53	4008.66	0.59	
PFSF	1300	PMF1	85000.00	4450.13	6.27	13923.87	4540.63	0.61	
PFSF	0 A	100-year Q	2430.00	4440.60	2.02	1241.60	2258.30	0.46	section A
PFSF	0	PMF	53000.00	4443.31	6.33	9591.24	3888.38	0.61	
PFSF	0	PMF1	85000.00	4444.23	7.45	13396.12	4436.82	0.64	

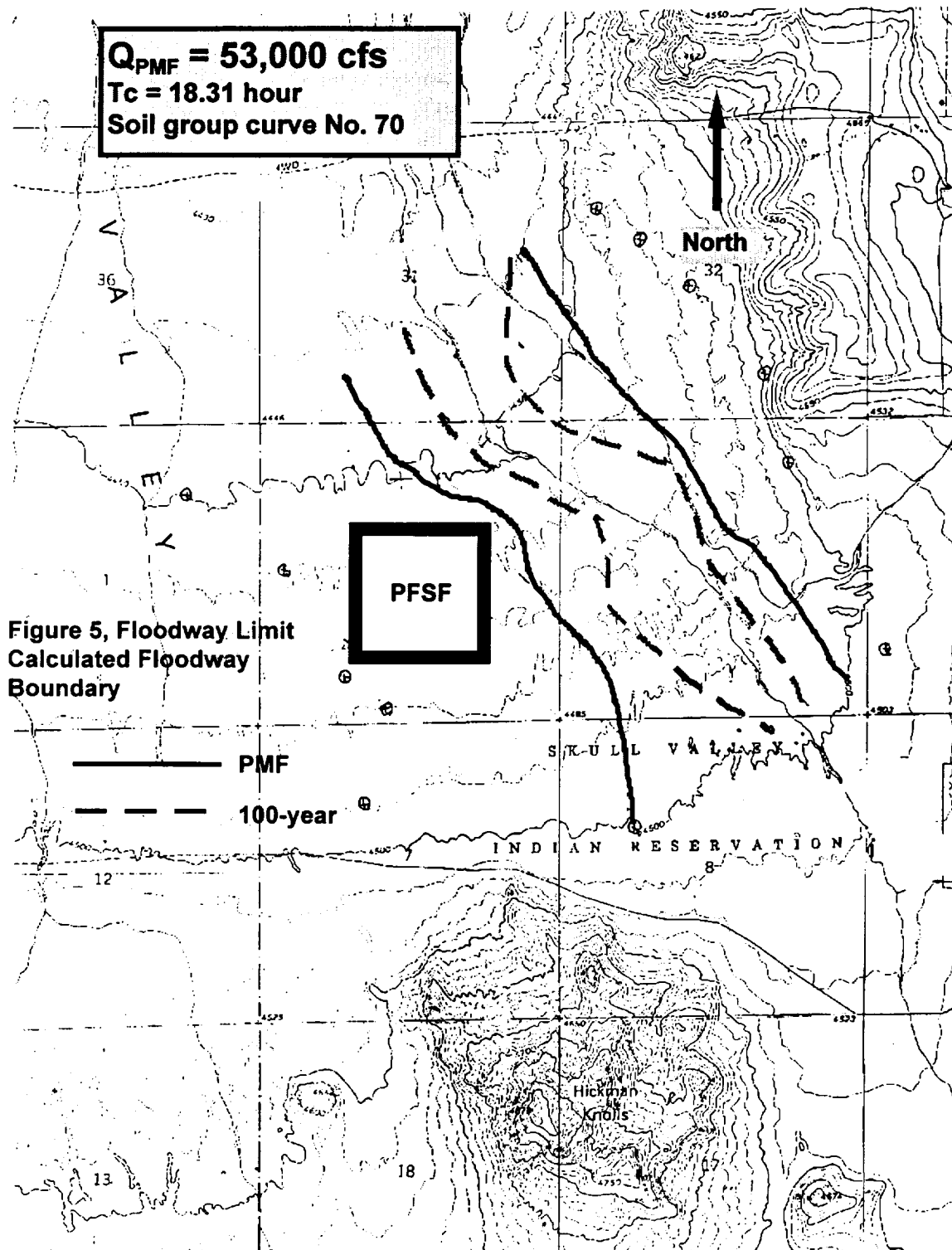
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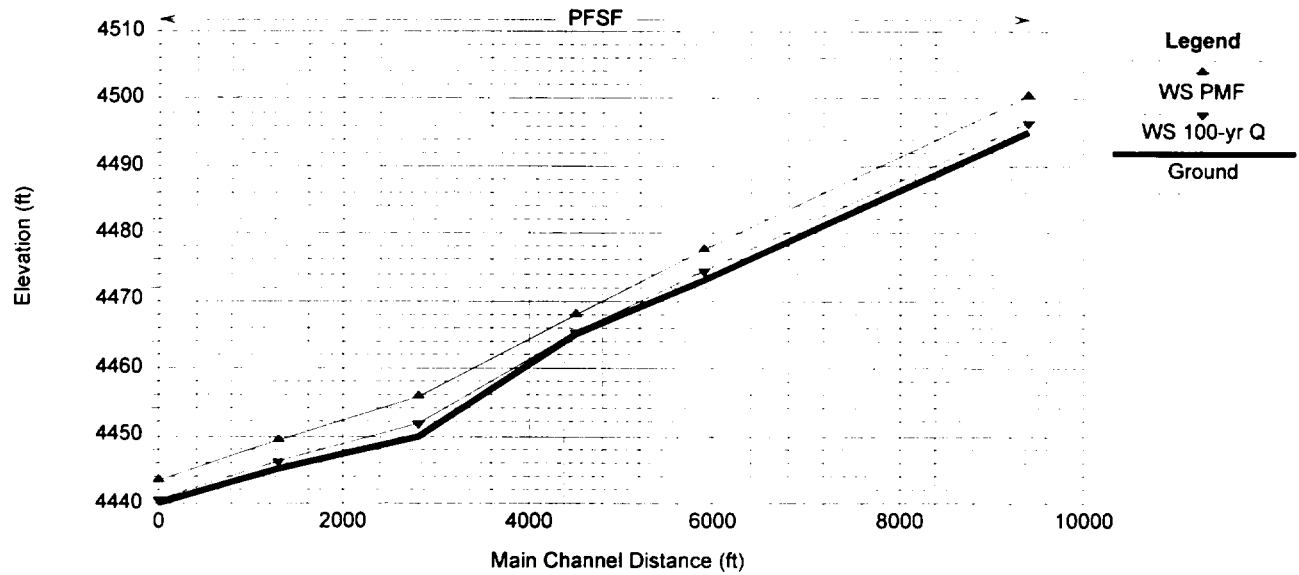
CALCULATION IDENTIFICATION NUMBER				REV. NO.1
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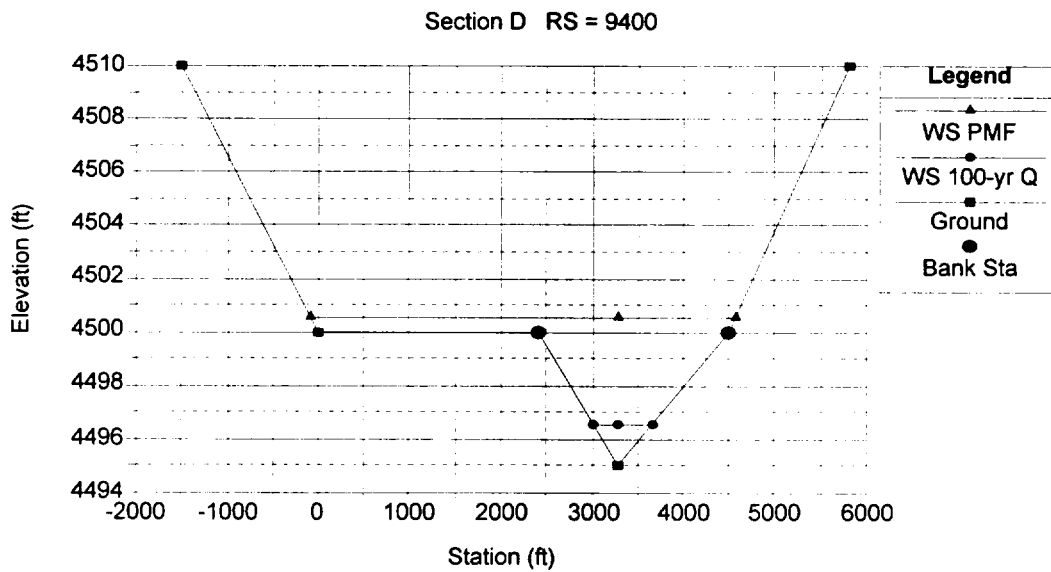
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**Figure 6, Water Surface Profile**



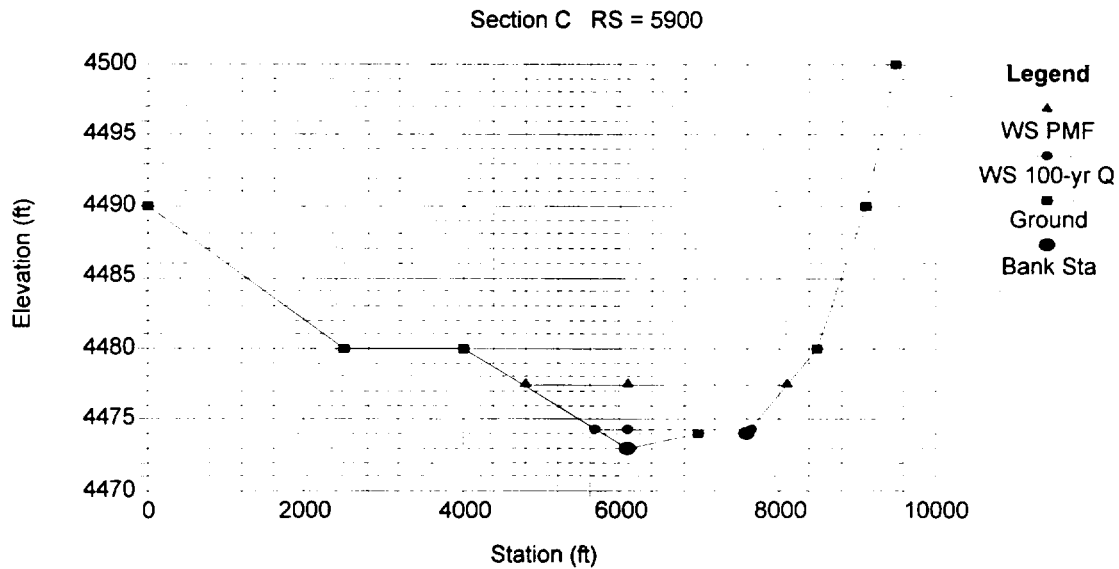
**Figure 7**



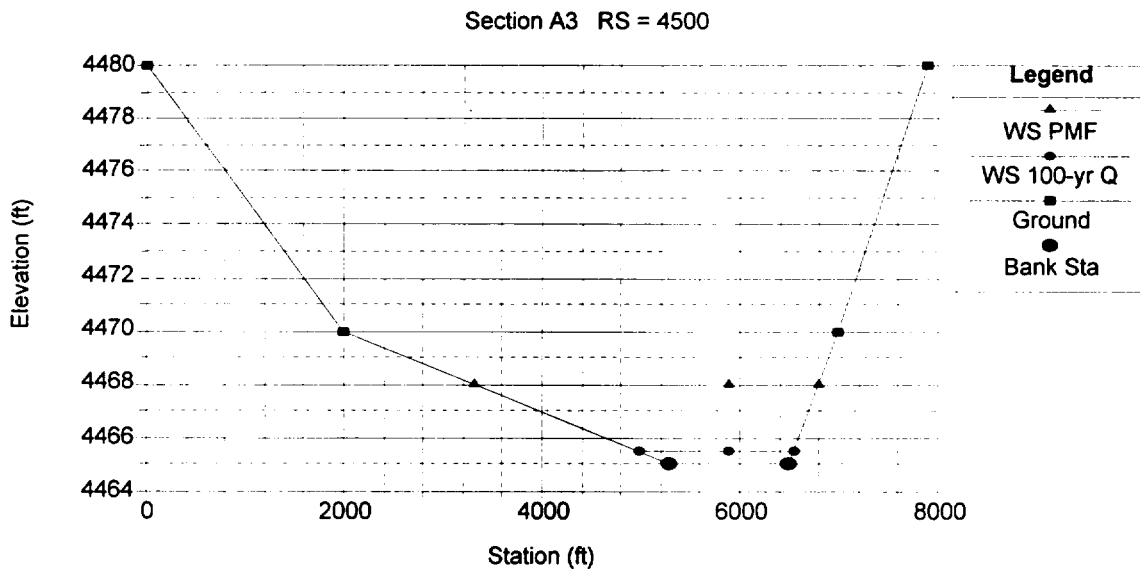
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**Figure 8**



**Figure 9**



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Figure 10

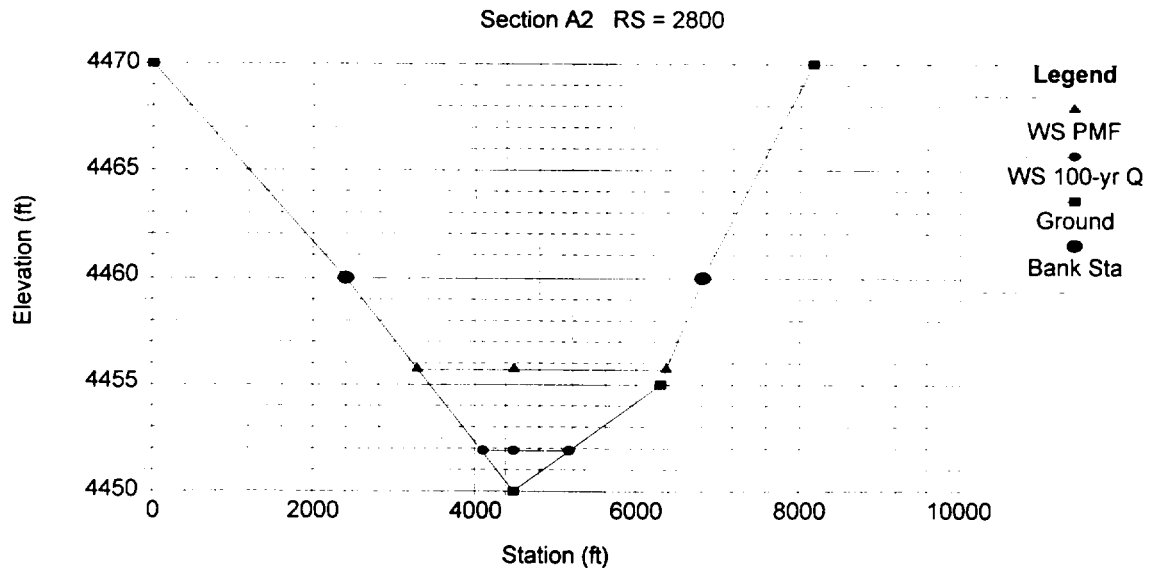
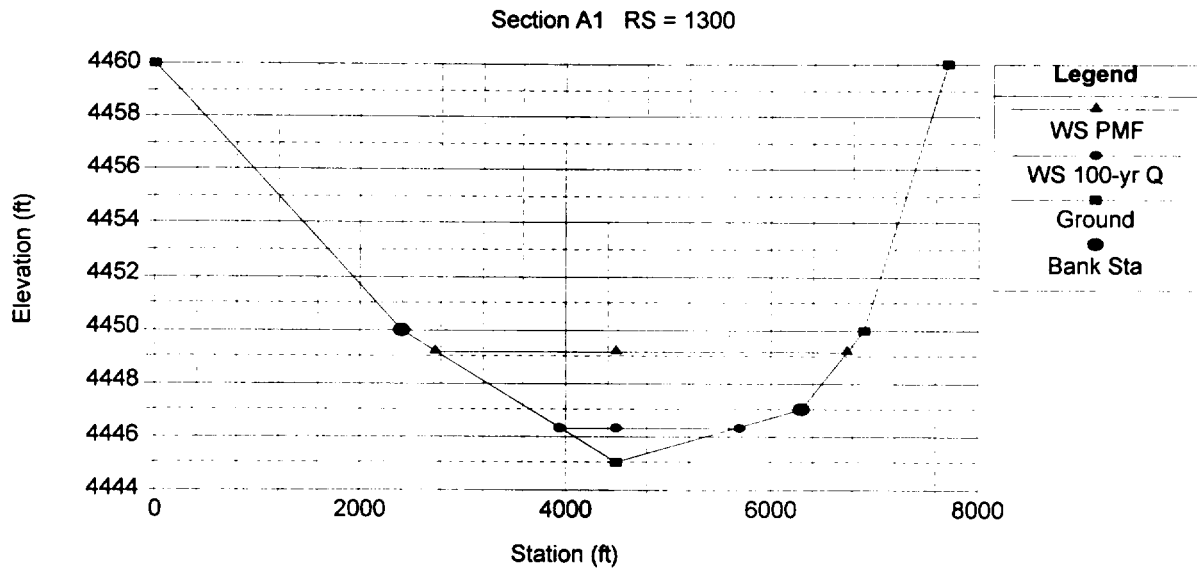


Figure 11



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## 7, Conclusion

The calculated peak runoff for the 100-year and the PMF flood events are:

$$Q_{100} = 2,430 \text{ cfs}$$
$$Q_{PMF} = 53,000 \text{ cfs}$$

Referring to Figure 4 and Table 6, the water level at Section A2, which has the closest point to the PFSF site is:

$$H_{100} = 4451.9 \text{ ft}$$
$$H_{PMF} = 4455.7 \text{ ft}$$

The access road is running obliquely to the flood way . The calculated water surface elevations are:

100-year flood	4496.5 ft
PMF flood	From 4500.5 ft (east bank of flood way) to 4477.4 ft (west bank).

The above water surface elevations are calculated using Manning's  $n = 0.035$ . Note that these elevations, as well as other elevations in this calculation, are based on the USGS 1:24,000 topographic map datum.

## 8, Discussion

Three main factors that affect the calculation result of PMF are: (1), precipitation, (2), land surface interception and infiltration, and (3), Concentration time. The approach for defining the three factors in this calculation is summarized as follows.

### (1), Precipitation

The precipitation data is evaluated based on NOAA report (Ref. 2). The report gives a procedure to estimate PMP (probable maximum precipitation) in the Great Basin area including the Skull Valley where PFSF is located. Therefore, the PMP data developed in this calculation should have been reasonably defined.

### (2), Land Surface Interception and Infiltration

This is related to the SCS (Soil Conservation Service) curve number (CN). The Water Resources Department of Utah suggested  $CN=70$  for the type of soil surface condition in the Skull Valley. ( $CN=100$  is impervious). Consequently,  $CN=70$  is assumed in the calculation.

Several additional HEC-1 analyses were made to test the effect of CN to the PMF. It was found that CN is not a very sensitive factor to the result of PMF.

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There are 6 cases analyzed, each assumed CN = 75, 80, 85, 90, and 96, respectively; all other data remain unchanged. The results of these runs are presented in Figure 12. The HEC-1 input and outputs are documented as Attachment 4 in this calculation.

The highest CN = 96 produces PMF = 67759 cfs. However, this number does not describe the soil condition in the Skull Valley. The soil condition for CN=96 is characterized in Table 2-2a of Ref.10 as below:

Western desert urban areas - Artificial desert landscaping with impervious weed barrier, desert shrub with 1 to 2 inch sand or gravel mulch and basin borders.

The Skull Valley drainage basin is an undeveloped area and the climate is semi-arid. The precipitation runoff, mostly occurs in the surrounding mountain ranges, is intercepted by the pervious unconsolidated sand in the valley to recharge to the groundwater system. Field data has shown that groundwater level is more than 100 ft below the ground. Consequently, CN=96, being close to total impervious or the saturated condition, should not be applied to the area. The hydrologic condition in the area has been described in detail in the SAR (Ref. 11). Based on the SAR and suggestion from Water Resource Department of Utah, CN=70 should be appropriate for this PMF analysis.



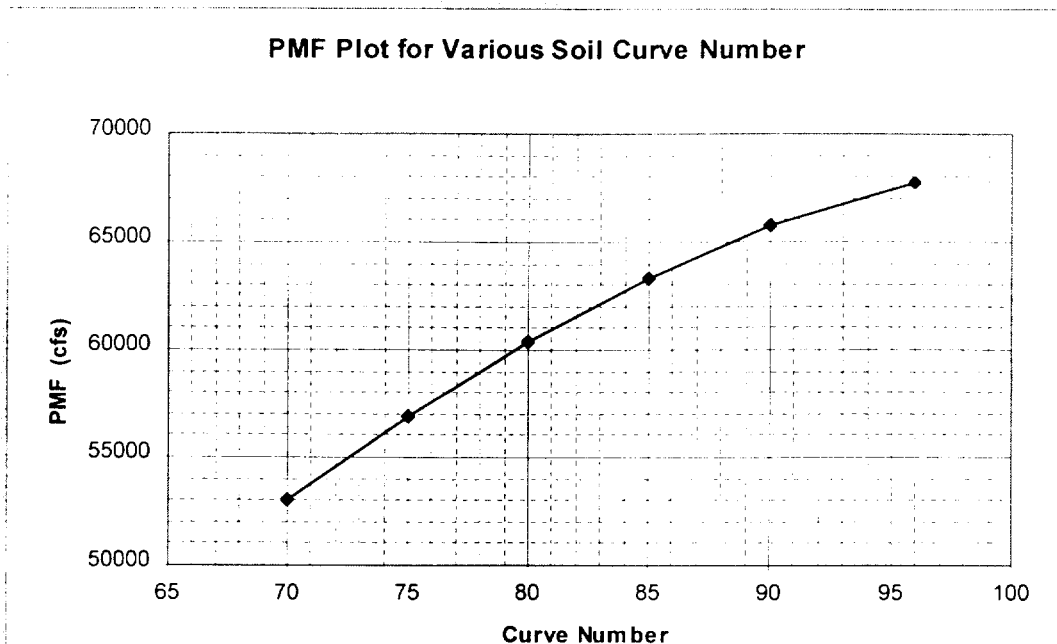
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**Figure 12**

Values of PMF Corresponding to Different CN,  $T_c=18.31$  hour

Curve No	PMF
70	53000
75	56887
80	60341
85	63287
90	65734
96	67759



**(3) Concentration Time**

Most of the empirical methods for estimating the concentration time,  $T_c$ , are based on small watershed in a specific geographic region. For example, the Kirpich's method was established on the small agricultural watersheds in Tennessee with drainage area smaller than 0.3 square miles (200 acres). For a large watershed such as the Skull Valley watershed which has an area = 270 square miles, the watershed characteristic and the land cover type should be fully considered. The Skull Valley runoff is dominated by the sheet flows; the roughness coefficient should be included in determining  $T_c$  to reflect basin characteristic for each sector of the basin.

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The Hathaway formula is selected because it included the roughness. Another method that may be used for the Skull Valley basin is the SCS formula. The SCS has established an equation for estimating the watershed lag, which is defined as the time in hours from the center of mass of the excess rainfall to the peak discharge. This formula, after divided by 0.6 (approximate ratio of lag time and Tc), can be used to calculate Tc. Using this formula the Tc calculated in Table 7. For CN=70, the calculated Tc is 58.9 hours, and for CN=96, it is 23.4 hours. It is believed that the Hathaway method is reasonable and is conservative comparing with the SCS method.

**Table 7**

PFSF, Estimate Concentration Time From South Rim of Basin to Access Road  
SCS Formula

$$T_c = 0.00526L^{0.8}((1000/CN)-9)^{0.7}S^{-0.5}$$

L=Length (ft)

S=slope ft/ft

Tc=Concentration time (min)

(1), CN=70

From Elev 1 ft	To Elev 2 ft	L mile	L ft	S ft/ft	SCS Tc Min	SCS Tc hour
6400	5400	3.5	18480	0.054113	197.88	3.3
5400	5200	1.0	5280	0.037879	82.42	1.4
5200	5000	2.5	13200	0.015152	271.26	4.5
5000	4800	4.9	25872	0.007730	850.61	14.2
4800	4600	8.4	44352	0.004509	1311.08	21.9
4600	4465	6.0	31680	0.004261	1030.41	17.2
Total		26.3			3533.68	58.9

(2), CN=96

From Elev 1 ft	To Elev 2 ft	L mile	L ft	S ft/ft	SCS Tc Min	SCS Tc hour
6400	5400	3.5	18480	0.054113	74.75	1.2
5400	5200	1.0	5280	0.037879	32.79	0.5
5200	5000	2.5	13200	0.015152	107.92	1.8
5000	4800	4.9	25872	0.007730	258.84	4.3
4800	4600	8.4	44352	0.004509	521.61	8.7
4600	4465	6.0	31680	0.004261	409.95	6.8
Total		26.3			1405.86	23.4

### An Unrealistic PMF Case

As a reference for comparison, one additional PMF case that is unlikely to happen in the Skull Valley basin is also analyzed:

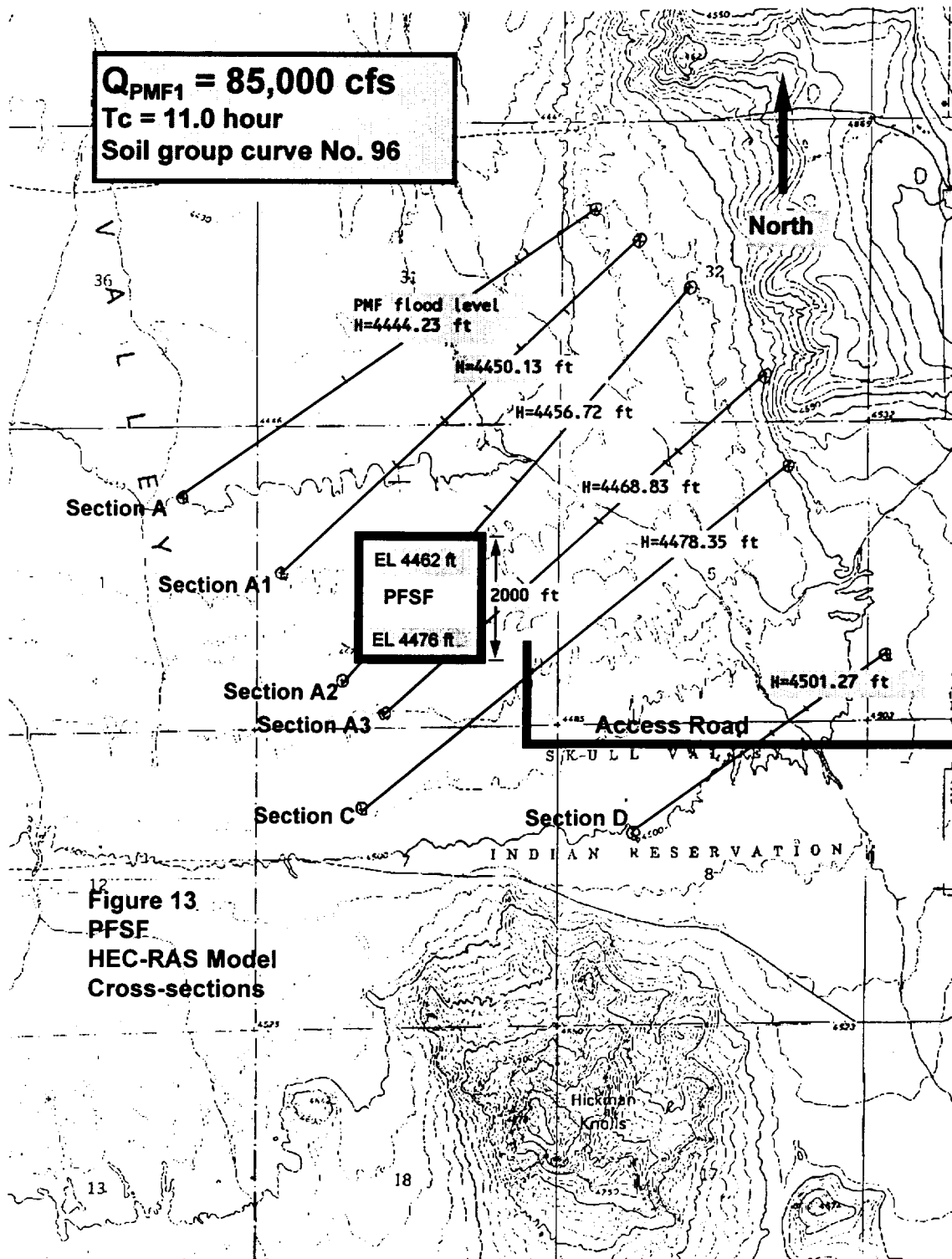
Assuming CN=96 and Tc=11 hours, the calculated PMF = 85,000 cfs (84,857 cfs). The result of water surface is tabulated in the revised portion of Table 6, and plotted in Figure 13. The HEC-1 input and output files are included in Attachment 6. The HES-RAS hydraulic report is included in the revised portion of Attachment 3.

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<p>Comparing to the analyzed case (PMF=53,000 cfs), the water level increases about 1 ft. The lowest corner in the PFSF site is still 5.3 ft above the flood level.</p>				

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## Attachment 1, HEC-1 File

### General Storm PMF

#### HEC-1 Input

```
ID PFSF (Private Fuel Storage Facility Project)
ID General PMF AT ACCESS RD
ID FILE=GEN_PMF.DAT
ID
IT 60 200
IO 2
PG 60
IN 180
PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98
PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17
PI 0.16 0.16 0.15 0.14
KK 010
KM SCS DIMENSIONLESS UNIT HYDROGRAPH
BA 270.0
BF -1 1.06
PR 60
LS 0 70 1
UD 11.0
ZZ
```

#### HEC-1 Output

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
*
* RUN DATE 02/07/1999 TIME 12:05:44
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
```

X X XXXXXXX XXXXX X

```

X   X X   X   X   XX
X   X X   X   X   X
XXXXXX XXXX X   XXXX X
X   X X   X   X   X
X   X X   X   X   X
X   X XXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

## HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID PFSF (Private Fuel Storage Facility Project)
2	ID General PMF AT ACCESS RD
3	ID FILE=GEN_PMF.DAT
4	ID
5	IT 60 200
6	IO 2
7	PG 60
8	IN 180
9	PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98
10	PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17
11	PI 0.16 0.16 0.15 0.14
12	KK 010
13	KM SCS DIMENSIONLESS UNIT HYDROGRAPH
14	BA 270.0
15	BF -1 1.06
16	PR 60
17	LS 0 70 1
18	UD 11.0
19	ZZ

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
*

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
*

```

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*          VERSION 4.0          *
*                               *
* RUN DATE 02/07/1999 TIME 12:05:44 *
*                               *
*****

```

```

*          609 SECOND STREET    *
*          DAVIS, CALIFORNIA 95616 *
*          (916) 756-1104      *
*                               *
*****

```

PFSF (Private Fuel Storage Facility Project)  
 General PMF AT ACCESS RD  
 FILE=GEN\_PMF.DAT

6 IO      OUTPUT CONTROL VARIABLES

```

      IPRNT      2  PRINT CONTROL
      IPLOT      0  PLOT CONTROL
      QSCAL      0.  HYDROGRAPH PLOT SCALE

```

8 IN      TIME DATA FOR INPUT TIME SERIES

```

      JXMIN      180  TIME INTERVAL IN MINUTES
      JXDATE     1    0  STARTING DATE
      JXTIME     0    0  STARTING TIME

```

IT        HYDROGRAPH TIME DATA

```

      NMIN      60  MINUTES IN COMPUTATION INTERVAL
      IDATE     1    0  STARTING DATE
      ITIME     0000  STARTING TIME
      NQ        200  NUMBER OF HYDROGRAPH ORDINATES
      NDDATE    9    0  ENDING DATE
      NDTIME    0700  ENDING TIME
      ICENT     19  CENTURY MARK

```

```

      COMPUTATION INTERVAL 1.00 HOURS
      TOTAL TIME BASE 199.00 HOURS

```

ENGLISH UNITS

```

      DRAINAGE AREA      SQUARE MILES
      PRECIPITATION DEPTH INCHES
      LENGTH, ELEVATION FEET
      FLOW              CUBIC FEET PER SECOND
      STORAGE VOLUME    ACRE-FEET
      SURFACE AREA      ACRES
      TEMPERATURE       DEGREES FAHRENHEIT

```

\*\*\* \*\*

\*\*\*\*\*  
\*  
12 KK \* 010 \*  
\*  
\*\*\*\*\*

# SCS DIMENSIONLESS UNIT HYDROGRAPH

## SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS  
TAREA 270.00 SUBBASIN AREA

15 BF BASE FLOW CHARACTERISTICS  
STRTO 270.00 INITIAL FLOW  
QRCSN .00 BEGIN BASE FLOW RECESSON  
RTIOR 1.06000 RECESSON CONSTANT

## PRECIPITATION DATA

16 PR RECORDING STATIONS 60  
0 PW WEIGHTS 1.00

17 LS SCS LOSS RATE  
STRTL .86 INITIAL ABSTRACTION  
CRVNBR 70.00 CURVE NUMBER  
RTIMP 1.00 PERCENT IMPERVIOUS AREA

18 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 11.00 LAG

\*\*\*

## PRECIPITATION STATION DATA

STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

## TEMPORAL DISTRIBUTIONS

STATION	60, WEIGHT = 1.00								
.06	.06	.06	.09	.09	.10	.10	.10	.12	
.12	.12	.12	.12	.12	.13	.13	.13	.21	.21
.21	.23	.23	.23	.31	.31	.33	.33	.33	.33



.36	.36	.36	.94	.94	.94	.21	.21	.21	.16
.16	.16	.14	.14	.14	.14	.14	.14	.13	.13
.13	.13	.13	.13	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05								

UNIT HYDROGRAPH  
57 END-OF-PERIOD ORDINATES

296.	927.	1755.	2805.	4146.	5798.	7642.	9219.	10329.	11019.
11290.	11290.	11019.	10407.	9712.	8924.	7957.	6823.	5758.	4905.
4245.	3668.	3175.	2815.	2455.	2140.	1844.	1588.	1391.	1199.
1051.	903.	786.	678.	587.	513.	443.	388.	334.	293.
254.	220.	191.	164.	144.	125.	113.	101.	89.	77.
66.	54.	44.	35.	25.	15.	5.			

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HYDROGRAPH AT STATION 010

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	.00	.00	.00	270.	*	5	0400	101	.00	.00	.00	526.		
1	0100	2	.06	.06	.00	255.	*	5	0500	102	.00	.00	.00	453.		
1	0200	3	.06	.06	.00	241.	*	5	0600	103	.00	.00	.00	389.		
1	0300	4	.06	.06	.00	228.	*	5	0700	104	.00	.00	.00	334.		
1	0400	5	.09	.09	.00	217.	*	5	0800	105	.00	.00	.00	286.		
1	0500	6	.09	.09	.00	208.	*	5	0900	106	.00	.00	.00	245.		
1	0600	7	.09	.09	.00	201.	*	5	1000	107	.00	.00	.00	209.		
1	0700	8	.10	.10	.00	195.	*	5	1100	108	.00	.00	.00	179.		
1	0800	9	.10	.10	.00	192.	*	5	1200	109	.00	.00	.00	152.		
1	0900	10	.10	.10	.00	190.	*	5	1300	110	.00	.00	.00	130.		
1	1000	11	.12	.12	.00	191.	*	5	1400	111	.00	.00	.00	110.		
1	1100	12	.12	.11	.00	193.	*	5	1500	112	.00	.00	.00	94.		
1	1200	13	.12	.11	.01	200.	*	5	1600	113	.00	.00	.00	80.		
1	1300	14	.12	.10	.02	216.	*	5	1700	114	.00	.00	.00	68.		
1	1400	15	.12	.10	.02	246.	*	5	1800	115	.00	.00	.00	58.		
1	1500	16	.12	.09	.03	295.	*	5	1900	116	.00	.00	.00	49.		
1	1600	17	.13	.09	.03	374.	*	5	2000	117	.00	.00	.00	41.		
1	1700	18	.13	.09	.04	490.	*	5	2100	118	.00	.00	.00	35.		
1	1800	19	.13	.09	.04	653.	*	5	2200	119	.00	.00	.00	29.		
1	1900	20	.21	.13	.08	877.	*	5	2300	120	.00	.00	.00	23.		
1	2000	21	.21	.12	.09	1178.	*	6	0000	121	.00	.00	.00	19.		
1	2100	22	.21	.11	.09	1566.	*	6	0100	122	.00	.00	.00	15.		
1	2200	23	.23	.11	.11	2052.	*	6	0200	123	.00	.00	.00	11.		
1	2300	24	.23	.11	.12	2650.	*	6	0300	124	.00	.00	.00	8.		

2	0000	25	.23	.10	.13	3373.	*	6	0400	125	.00	.00	.00	6.
2	0100	26	.31	.12	.18	4243.	*	6	0500	126	.00	.00	.00	4.
2	0200	27	.31	.11	.19	5274.	*	6	0600	127	.00	.00	.00	2.
2	0300	28	.31	.10	.20	6466.	*	6	0700	128	.00	.00	.00	1.
2	0400	29	.33	.10	.22	7820.	*	6	0800	129	.00	.00	.00	0.
2	0500	30	.33	.09	.23	9337.	*	6	0900	130	.00	.00	.00	0.
2	0600	31	.33	.09	.24	11016.	*	6	1000	131	.00	.00	.00	0.
2	0700	32	.36	.09	.27	12862.	*	6	1100	132	.00	.00	.00	0.
2	0800	33	.36	.08	.28	14855.	*	6	1200	133	.00	.00	.00	0.
2	0900	34	.36	.07	.28	16971.	*	6	1300	134	.00	.00	.00	0.
2	1000	35	.94	.17	.77	19327.	*	6	1400	135	.00	.00	.00	0.
2	1100	36	.94	.14	.80	22059.	*	6	1500	136	.00	.00	.00	0.
2	1200	37	.94	.12	.82	25246.	*	6	1600	137	.00	.00	.00	0.
2	1300	38	.21	.02	.18	28792.	*	6	1700	138	.00	.00	.00	0.
2	1400	39	.21	.02	.18	32595.	*	6	1800	139	.00	.00	.00	0.
2	1500	40	.21	.02	.18	36664.	*	6	1900	140	.00	.00	.00	0.
2	1600	41	.16	.02	.14	40923.	*	6	2000	141	.00	.00	.00	0.
2	1700	42	.16	.02	.14	45025.	*	6	2100	142	.00	.00	.00	0.
2	1800	43	.16	.02	.14	48512.	*	6	2200	143	.00	.00	.00	0.
2	1900	44	.14	.01	.13	51014.	*	6	2300	144	.00	.00	.00	0.
2	2000	45	.14	.01	.13	52459.	*	7	0000	145	.00	.00	.00	0.
2	2100	46	.14	.01	.13	52983.	*	7	0100	146	.00	.00	.00	0.
2	2200	47	.14	.01	.13	52701.	*	7	0200	147	.00	.00	.00	0.
2	2300	48	.14	.01	.13	51718.	*	7	0300	148	.00	.00	.00	0.
3	0000	49	.14	.01	.13	50175.	*	7	0400	149	.00	.00	.00	0.
3	0100	50	.13	.01	.12	48210.	*	7	0500	150	.00	.00	.00	0.
3	0200	51	.13	.01	.12	45982.	*	7	0600	151	.00	.00	.00	0.
3	0300	52	.13	.01	.12	43485.	*	7	0700	152	.00	.00	.00	0.
3	0400	53	.13	.01	.12	40830.	*	7	0800	153	.00	.00	.00	0.
3	0500	54	.13	.01	.12	38259.	*	7	0900	154	.00	.00	.00	0.
3	0600	55	.13	.01	.12	35992.	*	7	1000	155	.00	.00	.00	0.
3	0700	56	.06	.00	.05	34028.	*	7	1100	156	.00	.00	.00	0.
3	0800	57	.06	.00	.05	32280.	*	7	1200	157	.00	.00	.00	0.
3	0900	58	.06	.00	.05	30700.	*	7	1300	158	.00	.00	.00	0.
3	1000	59	.06	.00	.05	29236.	*	7	1400	159	.00	.00	.00	0.
3	1100	60	.06	.00	.05	27846.	*	7	1500	160	.00	.00	.00	0.
3	1200	61	.06	.00	.05	26436.	*	7	1600	161	.00	.00	.00	0.
3	1300	62	.05	.00	.05	25017.	*	7	1700	162	.00	.00	.00	0.
3	1400	63	.05	.00	.05	23608.	*	7	1800	163	.00	.00	.00	0.
3	1500	64	.05	.00	.05	22227.	*	7	1900	164	.00	.00	.00	0.
3	1600	65	.05	.00	.05	20898.	*	7	2000	165	.00	.00	.00	0.
3	1700	66	.05	.00	.05	19615.	*	7	2100	166	.00	.00	.00	0.
3	1800	67	.05	.00	.05	18407.	*	7	2200	167	.00	.00	.00	0.
3	1900	68	.05	.00	.05	17266.	*	7	2300	168	.00	.00	.00	0.
3	2000	69	.05	.00	.05	16218.	*	8	0000	169	.00	.00	.00	0.
3	2100	70	.05	.00	.05	15256.	*	8	0100	170	.00	.00	.00	0.
3	2200	71	.05	.00	.04	14380.	*	8	0200	171	.00	.00	.00	0.

3	2300	72	.05	.00	.04	13598.	*	8	0300	172	.00	.00	.00	0.
4	0000	73	.05	.00	.04	12906.	*	8	0400	173	.00	.00	.00	0.
4	0100	74	.00	.00	.00	12290.	*	8	0500	174	.00	.00	.00	0.
4	0200	75	.00	.00	.00	11714.	*	8	0600	175	.00	.00	.00	0.
4	0300	76	.00	.00	.00	11160.	*	8	0700	176	.00	.00	.00	0.
4	0400	77	.00	.00	.00	10606.	*	8	0800	177	.00	.00	.00	0.
4	0500	78	.00	.00	.00	10038.	*	8	0900	178	.00	.00	.00	0.
4	0600	79	.00	.00	.00	9434.	*	8	1000	179	.00	.00	.00	0.
4	0700	80	.00	.00	.00	8787.	*	8	1100	180	.00	.00	.00	0.
4	0800	81	.00	.00	.00	8107.	*	8	1200	181	.00	.00	.00	0.
4	0900	82	.00	.00	.00	7410.	*	8	1300	182	.00	.00	.00	0.
4	1000	83	.00	.00	.00	6713.	*	8	1400	183	.00	.00	.00	0.
4	1100	84	.00	.00	.00	6026.	*	8	1500	184	.00	.00	.00	0.
4	1200	85	.00	.00	.00	5360.	*	8	1600	185	.00	.00	.00	0.
4	1300	86	.00	.00	.00	4725.	*	8	1700	186	.00	.00	.00	0.
4	1400	87	.00	.00	.00	4135.	*	8	1800	187	.00	.00	.00	0.
4	1500	88	.00	.00	.00	3592.	*	8	1900	188	.00	.00	.00	0.
4	1600	89	.00	.00	.00	3100.	*	8	2000	189	.00	.00	.00	0.
4	1700	90	.00	.00	.00	2661.	*	8	2100	190	.00	.00	.00	0.
4	1800	91	.00	.00	.00	2282.	*	8	2200	191	.00	.00	.00	0.
4	1900	92	.00	.00	.00	1961.	*	8	2300	192	.00	.00	.00	0.
4	2000	93	.00	.00	.00	1691.	*	9	0000	193	.00	.00	.00	0.
4	2100	94	.00	.00	.00	1462.	*	9	0100	194	.00	.00	.00	0.
4	2200	95	.00	.00	.00	1267.	*	9	0200	195	.00	.00	.00	0.
4	2300	96	.00	.00	.00	1098.	*	9	0300	196	.00	.00	.00	0.
5	0000	97	.00	.00	.00	949.	*	9	0400	197	.00	.00	.00	0.
5	0100	98	.00	.00	.00	819.	*	9	0500	198	.00	.00	.00	0.
5	0200	99	.00	.00	.00	707.	*	9	0600	199	.00	.00	.00	0.
5	0300	100	.00	.00	.00	610.	*	9	0700	200	.00	.00	.00	0.

\*\*\*\*\*

TOTAL RAINFALL = 12.60, TOTAL LOSS = 3.96, TOTAL EXCESS = 8.64

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	199.00-HR
+	(CFS)	(HR)				
		(CFS)				
+	52983.	45.00	51703.	40677.	20738.	7591.
		(INCHES)	1.780	5.603	8.569	8.670
		(AC-FT)	25638.	80682.	123397.	124843.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND

		TIME IN HOURS, AREA IN SQUARE MILES								
+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	010	52983.	45.00	51703.	40677.	20738.	270.00		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## Attachment 2, HEC-1 File Local Storm PMF

### HEC-1 Input

```
ID PFSF (Private Fuel Storage Facility Project)
ID General PMF AT ACCESS RD
ID FILE=LOC_PMF.DAT
ID
IT 5 200
IO 2
PG 60
IN 15
PI 0.10 0.10 0.10 0.10 0.20 0.20 0.20 0.20 1.20 0.90
PI 0.50 0.50 0.30 0.30 0.30 0.30 0.20 0.10 0.10 0.10
PI 0.10 0.10 0.10 0.10
KK 010
KM SCS DIMENSIONLESS UNIT HYDROGRAPH
BA 270.0
BF -1 1.06
PR 60
LS 0 70 1
UD 11.0
ZZ
```

### HEC-1 Input

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* SEPTEMBER 1990 *
* VERSION 4.0 *
* RUN DATE 02/07/1999 TIME 12:45:39 *
*****
```

```
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
```

```

X   X XXXXXXX XXXXX      X
X   X X      X   X      XX
X   X X      X           X
XXXXXXX XXXX  X      XXXXX X
X   X X      X           X
X   X X      X   X      X
X   X XXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

## HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	PFSF (Private Fuel Storage Facility Project)									
2	ID	General PMF AT ACCESS RD									
3	ID	FILE=LOC_PMF.DAT									
4	ID										
5	IT	5	200								
6	IO	2									
7	PG	60									
8	IN	15									
9	PI	0.10	0.10	0.10	0.10	0.20	0.20	0.20	0.20	1.20	0.90
10	PI	0.50	0.50	0.30	0.30	0.30	0.30	0.20	0.10	0.10	0.10
11	PI	0.10	0.10	0.10	0.10						
12	KK	010									
13	KM	SCS DIMENSIONLESS UNIT HYDROGRAPH									
14	BA	270.0									
15	BF	-1	1.06								
16	PR	60									
17	LS	0	70	1							
18	UD	11.0									

```

19      ZZ
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* SEPTEMBER 1990 *
* VERSION 4.0 *
* RUN DATE 02/07/1999 TIME 12:45:39 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

PFSF (Private Fuel Storage Facility Project)  
 General PMF AT ACCESS RD  
 FILE=LOC\_PMF.DAT

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      2 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

8 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      15 TIME INTERVAL IN MINUTES
          JXDATE      1 0 STARTING DATE
          JXTIME      0 STARTING TIME

IT        HYDROGRAPH TIME DATA
          NMIN      5 MINUTES IN COMPUTATION INTERVAL
          IDATE      1 0 STARTING DATE
          ITIME      0000 STARTING TIME
          NQ        200 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE      1 0 ENDING DATE
          NDTIME      1635 ENDING TIME
          ICENT      19 CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 16.58 HOURS

ENGLISH UNITS
          DRAINAGE AREA      SQUARE MILES
          PRECIPITATION DEPTH INCHES
          LENGTH, ELEVATION  FEET
          FLOW                CUBIC FEET PER SECOND

```

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## TEMPORAL DISTRIBUTIONS



STATION	60, WEIGHT = 1.00								
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.40	.40	.40	.30	.30	.30
.17	.17	.17	.17	.17	.17	.10	.10	.10	.10
.10	.10	.10	.10	.10	.10	.10	.10	.07	.07
.07	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03								

\*\*\* WARNING \*\*\* UNIT HYDROGRAPH TRUNCATED FROM 662 TO 300 INTERVALS

\*\*\* WARNING \*\*\* VOLUME UNDER UNIT GRAPH = .92  
 ORDINATES OF UNIT GRAPH WERE INCREASED TO OBTAIN 1.0 INCH OF RUNOFF.  
 TO PREVENT THIS, INCREASE THE COMPUTATION INTERVAL ON THE "IT" RECORD.

UNIT HYDROGRAPH 300 END-OF-PERIOD ORDINATES VOLUME = 1.00									
29.	58.	88.	117.	146.	175.	204.	234.	263.	292.
321.	350.	379.	438.	506.	574.	642.	710.	778.	846.
915.	983.	1051.	1119.	1187.	1255.	1333.	1421.	1508.	1596.
1683.	1771.	1858.	1946.	2033.	2121.	2209.	2296.	2384.	2479.
2595.	2712.	2829.	2946.	3062.	3179.	3296.	3413.	3529.	3646.
3763.	3880.	3996.	4152.	4308.	4463.	4619.	4775.	4930.	5086.
5242.	5397.	5553.	5709.	5864.	6020.	6198.	6383.	6567.	6752.
6937.	7122.	7307.	7492.	7677.	7861.	8046.	8231.	8416.	8586.
8742.	8898.	9053.	9209.	9365.	9520.	9676.	9832.	9987.	10143.
10299.	10454.	10598.	10705.	10812.	10919.	11026.	11133.	11240.	11347.
11454.	11561.	11668.	11775.	11882.	11989.	12048.	12106.	12164.	12223.
12281.	12339.	12398.	12456.	12515.	12573.	12631.	12690.	12748.	12770.
12780.	12789.	12799.	12809.	12819.	12828.	12838.	12848.	12858.	12867.
12877.	12887.	12887.	12877.	12867.	12858.	12848.	12838.	12828.	12819.
12809.	12799.	12789.	12780.	12770.	12748.	12690.	12631.	12573.	12515.
12456.	12398.	12339.	12281.	12223.	12164.	12106.	12048.	11989.	11921.
11853.	11785.	11717.	11649.	11581.	11512.	11444.	11376.	11308.	11240.
11172.	11104.	11028.	10951.	10873.	10795.	10717.	10639.	10561.	10484.
10406.	10328.	10250.	10172.	10094.	10007.	9910.	9812.	9715.	9618.
9520.	9423.	9326.	9228.	9131.	9034.	8937.	8839.	8737.	8620.
8504.	8387.	8270.	8153.	8037.	7920.	7803.	7686.	7570.	7453.
7336.	7219.	7122.	7025.	6927.	6830.	6733.	6636.	6538.	6441.
6344.	6246.	6149.	6052.	5954.	5879.	5811.	5743.	5675.	5607.
5539.	5470.	5402.	5334.	5266.	5198.	5130.	5062.	4999.	4940.
4882.	4823.	4765.	4707.	4648.	4590.	4532.	4473.	4415.	4356.
4298.	4242.	4193.	4145.	4096.	4047.	3999.	3950.	3902.	3853.

3804.	3756.	3707.	3658.	3610.	3574.	3539.	3503.	3468.	3432.
3397.	3361.	3326.	3290.	3255.	3219.	3183.	3148.	3112.	3077.
3041.	3006.	2970.	2935.	2899.	2864.	2793.	2757.	2722.	
2686.	2654.	2625.	2596.	2566.	2537.	2508.	2479.	2450.	2420.

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# HYDROGRAPH AT STATION 010

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1		0000	1	.00	.00	.00	270.	*	1		0820	101	.00	.00	.00	17219.
1		0005	2	.03	.03	.00	269.	*	1		0825	102	.00	.00	.00	17715.
1		0010	3	.03	.03	.00	267.	*	1		0830	103	.00	.00	.00	18216.
1		0015	4	.03	.03	.00	266.	*	1		0835	104	.00	.00	.00	18722.
1		0020	5	.03	.03	.00	265.	*	1		0840	105	.00	.00	.00	19232.
1		0025	6	.03	.03	.00	264.	*	1		0845	106	.00	.00	.00	19743.
1		0030	7	.03	.03	.00	262.	*	1		0850	107	.00	.00	.00	20252.
1		0035	8	.03	.03	.00	261.	*	1		0855	108	.00	.00	.00	20761.
1		0040	9	.03	.03	.00	260.	*	1		0900	109	.00	.00	.00	21270.
1		0045	10	.03	.03	.00	259.	*	1		0905	110	.00	.00	.00	21777.
1		0050	11	.03	.03	.00	258.	*	1		0910	111	.00	.00	.00	22285.
1		0055	12	.03	.03	.00	257.	*	1		0915	112	.00	.00	.00	22793.
1		0100	13	.03	.03	.00	255.	*	1		0920	113	.00	.00	.00	23302.
1		0105	14	.07	.07	.00	254.	*	1		0925	114	.00	.00	.00	23811.
1		0110	15	.07	.07	.00	253.	*	1		0930	115	.00	.00	.00	24320.
1		0115	16	.07	.07	.00	252.	*	1		0935	116	.00	.00	.00	24828.
1		0120	17	.07	.07	.00	251.	*	1		0940	117	.00	.00	.00	25335.
1		0125	18	.07	.07	.00	250.	*	1		0945	118	.00	.00	.00	25842.
1		0130	19	.07	.07	.00	249.	*	1		0950	119	.00	.00	.00	26343.
1		0135	20	.07	.07	.00	249.	*	1		0955	120	.00	.00	.00	26837.
1		0140	21	.07	.06	.00	248.	*	1		1000	121	.00	.00	.00	27323.
1		0145	22	.07	.06	.00	247.	*	1		1005	122	.00	.00	.00	27801.
1		0150	23	.07	.06	.01	247.	*	1		1010	123	.00	.00	.00	28271.
1		0155	24	.07	.06	.01	246.	*	1		1015	124	.00	.00	.00	28733.
1		0200	25	.07	.06	.01	246.	*	1		1020	125	.00	.00	.00	29190.
1		0205	26	.40	.31	.09	249.	*	1		1025	126	.00	.00	.00	29640.
1		0210	27	.40	.27	.13	256.	*	1		1030	127	.00	.00	.00	30085.
1		0215	28	.40	.23	.17	267.	*	1		1035	128	.00	.00	.00	30522.
1		0220	29	.30	.15	.15	283.	*	1		1040	129	.00	.00	.00	30952.
1		0225	30	.30	.14	.16	304.	*	1		1045	130	.00	.00	.00	31376.
1		0230	31	.30	.13	.17	329.	*	1		1050	131	.00	.00	.00	31795.
1		0235	32	.17	.07	.10	358.	*	1		1055	132	.00	.00	.00	32207.
1		0240	33	.17	.06	.10	390.	*	1		1100	133	.00	.00	.00	32608.
1		0245	34	.17	.06	.11	425.	*	1		1105	134	.00	.00	.00	32997.

1	0250	35	.17	.06	.11	464.	*	1	1110	135	.00	.00	.00	33376.
1	0255	36	.17	.05	.11	505.	*	1	1115	136	.00	.00	.00	33743.
1	0300	37	.17	.05	.11	551.	*	1	1120	137	.00	.00	.00	34099.
1	0305	38	.10	.03	.07	599.	*	1	1125	138	.00	.00	.00	34445.
1	0310	39	.10	.03	.07	652.	*	1	1130	139	.00	.00	.00	34783.
1	0315	40	.10	.03	.07	711.	*	1	1135	140	.00	.00	.00	35112.
1	0320	41	.10	.03	.07	779.	*	1	1140	141	.00	.00	.00	35430.
1	0325	42	.10	.03	.07	855.	*	1	1145	142	.00	.00	.00	35738.
1	0330	43	.10	.03	.07	939.	*	1	1150	143	.00	.00	.00	36037.
1	0335	44	.10	.03	.07	1033.	*	1	1155	144	.00	.00	.00	36329.
1	0340	45	.10	.03	.07	1133.	*	1	1200	145	.00	.00	.00	36612.
1	0345	46	.10	.02	.08	1239.	*	1	1205	146	.00	.00	.00	36882.
1	0350	47	.10	.02	.08	1352.	*	1	1210	147	.00	.00	.00	37140.
1	0355	48	.10	.02	.08	1471.	*	1	1215	148	.00	.00	.00	37384.
1	0400	49	.10	.02	.08	1597.	*	1	1220	149	.00	.00	.00	37615.
1	0405	50	.07	.02	.05	1729.	*	1	1225	150	.00	.00	.00	37832.
1	0410	51	.07	.01	.05	1866.	*	1	1230	151	.00	.00	.00	38037.
1	0415	52	.07	.01	.05	2008.	*	1	1235	152	.00	.00	.00	38232.
1	0420	53	.03	.01	.03	2156.	*	1	1240	153	.00	.00	.00	38416.
1	0425	54	.03	.01	.03	2310.	*	1	1245	154	.00	.00	.00	38590.
1	0430	55	.03	.01	.03	2471.	*	1	1250	155	.00	.00	.00	38753.
1	0435	56	.03	.01	.03	2639.	*	1	1255	156	.00	.00	.00	38906.
1	0440	57	.03	.01	.03	2813.	*	1	1300	157	.00	.00	.00	39052.
1	0445	58	.03	.01	.03	2994.	*	1	1305	158	.00	.00	.00	39189.
1	0450	59	.03	.01	.03	3181.	*	1	1310	159	.00	.00	.00	39318.
1	0455	60	.03	.01	.03	3374.	*	1	1315	160	.00	.00	.00	39438.
1	0500	61	.03	.01	.03	3573.	*	1	1320	161	.00	.00	.00	39549.
1	0505	62	.03	.01	.03	3777.	*	1	1325	162	.00	.00	.00	39651.
1	0510	63	.03	.01	.03	3987.	*	1	1330	163	.00	.00	.00	39743.
1	0515	64	.03	.01	.03	4202.	*	1	1335	164	.00	.00	.00	39826.
1	0520	65	.03	.01	.03	4422.	*	1	1340	165	.00	.00	.00	39901.
1	0525	66	.03	.01	.03	4648.	*	1	1345	166	.00	.00	.00	39968.
1	0530	67	.03	.01	.03	4882.	*	1	1350	167	.00	.00	.00	40028.
1	0535	68	.03	.01	.03	5124.	*	1	1355	168	.00	.00	.00	40080.
1	0540	69	.03	.01	.03	5373.	*	1	1400	169	.00	.00	.00	40126.
1	0545	70	.03	.01	.03	5631.	*	1	1405	170	.00	.00	.00	40166.
1	0550	71	.03	.01	.03	5896.	*	1	1410	171	.00	.00	.00	40199.
1	0555	72	.03	.01	.03	6168.	*	1	1415	172	.00	.00	.00	40223.
1	0600	73	.03	.01	.03	6446.	*	1	1420	173	.00	.00	.00	40236.
1	0605	74	.00	.00	.00	6730.	*	1	1425	174	.00	.00	.00	40237.
1	0610	75	.00	.00	.00	7019.	*	1	1430	175	.00	.00	.00	40227.
1	0615	76	.00	.00	.00	7315.	*	1	1435	176	.00	.00	.00	40204.
1	0620	77	.00	.00	.00	7616.	*	1	1440	177	.00	.00	.00	40170.
1	0625	78	.00	.00	.00	7921.	*	1	1445	178	.00	.00	.00	40127.
1	0630	79	.00	.00	.00	8234.	*	1	1450	179	.00	.00	.00	40075.
1	0635	80	.00	.00	.00	8555.	*	1	1455	180	.00	.00	.00	40015.
1	0640	81	.00	.00	.00	8887.	*	1	1500	181	.00	.00	.00	39947.

1	0645	82	.00	.00	.00	9228.	*	1	1505	182	.00	.00	.00	39870.
1	0650	83	.00	.00	.00	9580.	*	1	1510	183	.00	.00	.00	39786.
1	0655	84	.00	.00	.00	9941.	*	1	1515	184	.00	.00	.00	39696.
1	0700	85	.00	.00	.00	10311.	*	1	1520	185	.00	.00	.00	39600.
1	0705	86	.00	.00	.00	10688.	*	1	1525	186	.00	.00	.00	39498.
1	0710	87	.00	.00	.00	11073.	*	1	1530	187	.00	.00	.00	39388.
1	0715	88	.00	.00	.00	11464.	*	1	1535	188	.00	.00	.00	39271.
1	0720	89	.00	.00	.00	11863.	*	1	1540	189	.00	.00	.00	39148.
1	0725	90	.00	.00	.00	12269.	*	1	1545	190	.00	.00	.00	39017.
1	0730	91	.00	.00	.00	12679.	*	1	1550	191	.00	.00	.00	38880.
1	0735	92	.00	.00	.00	13096.	*	1	1555	192	.00	.00	.00	38737.
1	0740	93	.00	.00	.00	13521.	*	1	1600	193	.00	.00	.00	38587.
1	0745	94	.00	.00	.00	13954.	*	1	1605	194	.00	.00	.00	38433.
1	0750	95	.00	.00	.00	14396.	*	1	1610	195	.00	.00	.00	38273.
1	0755	96	.00	.00	.00	14847.	*	1	1615	196	.00	.00	.00	38109.
1	0800	97	.00	.00	.00	15307.	*	1	1620	197	.00	.00	.00	37942.
1	0805	98	.00	.00	.00	15774.	*	1	1625	198	.00	.00	.00	37770.
1	0810	99	.00	.00	.00	16249.	*	1	1630	199	.00	.00	.00	37594.
1	0815	100	.00	.00	.00	16731.	*	1	1635	200	.00	.00	.00	37415.

\*\*\*\*\*

TOTAL RAINFALL = 6.40, TOTAL LOSS = 3.24, TOTAL EXCESS = 3.16

PEAK FLOW	TIME		6-HR	24-HR	72-HR	16.58-HR
(CFS)	(HR)	(CFS)				
+	40237.	14.42	37871.	19113.	19113.	19113.
		(INCHES)	1.304	1.819	1.819	1.819
		(AC-FT)	18779.	26195.	26195.	26195.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+									
	HYDROGRAPH AT								
+	010	40237.	14.42	37871.	19113.	19113.	270.00		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## Attachment 3

### HRC-RAS File Hydraulic Report

HEC-RAS Version 2.0 April 1997  
U.S. Army Corp of Engineers  
Hydrologic Engineering Center  
609 Second Street, Suite D  
Davis, California 95616-4687  
(916) 756-1104

```

X    X XXXXXX   XXXX   XXXX   XX   XXXX
X    X X        X  X    X  X    X X   X
X    X X        X    X    X  X    X X   X
XXXXXXXX XXXX   X    XXX XXXX   XXXXXX   XXXX
X    X X        X    X  X  X  X    X    X
X    X X        X  X    X  X    X  X    X
X    X XXXXXX   XXXX   X  X  X  X    XXXXX

```

#### PROJECT DATA

Project Title: PFSF, PMF and 100-yr run  
Project File : access.prj  
Run Date and Time: 3/21/99 2:35:58 PM

Project in English units

#### Project Description:

Private Fuel Storage Facility (PFSF), Flood Levels

#### PLAN DATA

Plan Title: Natural flood  
Plan File : c:\a1\ras\access.p01

Geometry Title: USGS 1:24000 map, natural topograph  
Geometry File : c:\a1\ras\access.g01

Flow Title : PMF and 100-yr Q  
Flow File : c:\a1\ras\access.f01

#### Plan Summary Information:

Number of: Cross Sections	=	6	Multiple Openings	=	0
Culverts	=	0	Inline Weirs	=	0
Bridges	=	0			

#### Computational Information

Water surface calculation tolerance	=	0.01
Critical depth calculation tolerance	=	0.01
Maximum number of iterations	=	20
Maximum difference tolerance	=	0.3
Flow tolerance factor	=	0.001

Computational Flow Regime: Subcritical Flow

## FLOW DATA

Flow Title: PMF and 100-yr Q  
Flow File : c:\a1\ras\access.f01

## Flow Data (cfs)

River	Reach	RS	100-year Q	PMF	PMF1
Skull Valey	PFSF	9400	2430	53000	85000

## Boundary Conditions

River	Reach	Profile	Upstream	Downstream
Skull Valey	PFSF	100-year Q		Normal S = 0.0045
Skull Valey	PFSF	PMF		Normal S = 0.0045

## GEOMETRY DATA

Geometry Title: USGS 1:24000 map, natural topograph  
Geometry File : c:\a1\ras\access.g01

CROSS SECTION RIVER: Skull Valey  
REACH: PFSF RS: 9400

## INPUT

Description: Section D

Station Elevation Data		num=	6						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
-1500	4510	0	4500	2400	4500	3300	4495	4500	4500
5800	4510								

Manning's n Values		num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
-1500	.035	2400	.035	4500	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2400	4500		3500	3500	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4496.52	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.39	Wt. n-Val.		0.035	
E.G. Elev (ft)	4496.91	Reach Len. (ft)	3500.00	3500.00	3500.00
Crit W.S. (ft)	4496.52	Flow Area (sq ft)		486.13	
E.G. Slope (ft/ft)	0.019962	Area (sq ft)		486.13	
Q Total (cfs)	2430.00	Flow (cfs)		2430.00	
Top Width (ft)	639.02	Top Width (ft)		639.02	
Vel Total (ft/s)	5.00	Avg. Vel. (ft/s)		5.00	
Max Chl Dpth (ft)	1.52	Hydr. Depth (ft)		0.76	
Conv. Total (cfs)	17199.0	Conv. (cfs)		17199.0	
Length Wtd. (ft)		Wetted Per. (ft)		639.03	
Min Ch El (ft)	4495.00	Shear (lb/sq ft)		0.95	
Alpha	1.00	Stream Power (lb/ft s)		4.74	
Frctn Loss (ft)		Cum Volume (acre-ft)	20.41	190.40	1.30
C & E Loss (ft)		Cum SA (acres)	39.42	277.00	5.82

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4500.51	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.92	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4501.43	Reach Len. (ft)	3500.00	3500.00	3500.00
Crit W.S. (ft)	4500.51	Flow Area (sq ft)	1253.81	6329.74	17.18
E.G. Slope (ft/ft)	0.007939	Area (sq ft)	1253.81	6329.74	17.18
Q Total (cfs)	53000.00	Flow (cfs)	3012.29	49961.43	26.28
Top Width (ft)	4643.96	Top Width (ft)	2477.12	2100.00	66.84
Vel Total (ft/s)	6.97	Avg. Vel. (ft/s)	2.40	7.89	1.53
Max Chl Dpth (ft)	5.51	Hydr. Depth (ft)	0.51	3.01	0.26
Conv. Total (cfs)	594832.3	Conv. (cfs)	33807.7	560729.7	294.9
Length Wtd. (ft)	3500.00	Wetted Per. (ft)	2477.13	2100.02	66.84
Min Ch El (ft)	4495.00	Shear (lb/sq ft)	0.25	1.49	0.13
Alpha	1.21	Stream Power (lb/ft s)	0.60	11.79	0.19
Frctn Loss (ft)	19.48	Cum Volume (acre-ft)	360.53	1430.64	88.46
C & E Loss (ft)	0.11	Cum SA (acres)	269.19	467.04	60.67

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning - During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates

that there is not a valid subcritical answer. The program defaulted to critical depth.

## CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4501.27	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.10	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4502.37	Reach Len. (ft)	3500.00	3500.00	3500.00
Crit W.S. (ft)	4501.27	Flow Area (sq ft)	3160.16	7909.86	104.28
E.G. Slope (ft/ft)	0.007688	Area (sq ft)	3160.16	7909.86	104.28
Q Total (cfs)	85000.00	Flow (cfs)	13432.59	71281.15	286.26
Top Width (ft)	4854.65	Top Width (ft)	2589.99	2100.00	164.66
Vel Total (ft/s)	7.61	Avg. Vel. (ft/s)	4.25	9.01	2.75
Max Chl Dpth (ft)	6.27	Hydr. Depth (ft)	1.22	3.77	0.63
Conv. Total (cfs)	969400.8	Conv. (cfs)	153194.8	812941.3	3264.8
Length Wtd. (ft)	3500.00	Wetted Per. (ft)	2589.99	2100.02	164.66
Min Ch El (ft)	4495.00	Shear (lb/sq ft)	0.59	1.81	0.30
Alpha	1.23	Stream Power (lb/ft s)	2.49	16.29	0.83
Frctn Loss (ft)	20.05	Cum Volume (acre-ft)	608.30	1868.14	153.40
C & E Loss (ft)	0.10	Cum SA (acres)	317.31	489.42	82.21

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning - During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates

that there is not a valid subcritical answer. The program defaulted to critical depth.

Warning - The parabolic search method failed to converge on critical depth. The program will try the

cross section slice/secant method to find critical depth.

CROSS SECTION RIVER: Skull Valley  
REACH: PFSF RS: 5900

INPUT  
Description: Section C



Station Elevation Data		num= 9							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	4490	2500	4480	4000	4480	6100	4473	7000	4474
7600	4474	8500	4480	9100	4490	9500	4500		

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	6100	.035	7600	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	6100	7600		1400	1400	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4474.39	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.05	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4474.44	Reach Len. (ft)	1400.00	1400.00	1400.00
Crit W.S. (ft)	4474.06	Flow Area (sq ft)	289.26	1033.01	11.33
E.G. Slope (ft/ft)	0.003051	Area (sq ft)	289.26	1033.01	11.33
Q Total (cfs)	2430.00	Flow (cfs)	531.90	1889.18	8.91
Top Width (ft)	1974.90	Top Width (ft)	416.60	1500.00	58.30
Vel Total (ft/s)	1.82	Avg. Vel. (ft/s)	1.84	1.83	0.79
Max Chl Dpth (ft)	1.39	Hydr. Depth (ft)	0.69	0.69	0.19
Conv. Total (cfs)	43991.7	Conv. (cfs)	9629.3	34201.0	161.4
Length Wtd. (ft)	1400.00	Wetted Per. (ft)	416.60	1500.00	58.30
Min Ch El (ft)	4473.00	Shear (lb/sq ft)	0.13	0.13	0.04
Alpha	1.01	Stream Power (lb/ft s)	0.24	0.24	0.03
Frctn Loss (ft)	8.73	Cum Volume (acre-ft)	8.79	129.37	0.84
C & E Loss (ft)	0.02	Cum SA (acres)	22.68	191.07	3.47

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4477.40	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.55	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4477.95	Reach Len. (ft)	1400.00	1400.00	1400.00
Crit W.S. (ft)		Flow Area (sq ft)	2908.38	5554.98	868.69
E.G. Slope (ft/ft)	0.004117	Area (sq ft)	2908.38	5554.98	868.69
Q Total (cfs)	53000.00	Flow (cfs)	13407.62	36219.68	3372.70
Top Width (ft)	3331.49	Top Width (ft)	1321.00	1500.00	510.50
Vel Total (ft/s)	5.68	Avg. Vel. (ft/s)	4.61	6.52	3.88
Max Chl Dpth (ft)	4.40	Hydr. Depth (ft)	2.20	3.70	1.70
Conv. Total (cfs)	826041.0	Conv. (cfs)	208966.9	564508.4	52565.7
Length Wtd. (ft)	1400.00	Wetted Per. (ft)	1321.00	1500.00	510.51
Min Ch El (ft)	4473.00	Shear (lb/sq ft)	0.57	0.95	0.44
Alpha	1.10	Stream Power (lb/ft s)	2.61	6.21	1.70
Frctn Loss (ft)	8.88	Cum Volume (acre-ft)	193.32	953.18	52.87
C & E Loss (ft)	0.05	Cum SA (acres)	116.60	322.41	37.47

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4478.35	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.78	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4479.12	Reach Len. (ft)	1400.00	1400.00	1400.00
Crit W.S. (ft)		Flow Area (sq ft)	4291.18	6972.95	1418.30
E.G. Slope (ft/ft)	0.004433	Area (sq ft)	4291.18	6972.95	1418.30
Q Total (cfs)	85000.00	Flow (cfs)	23370.33	54901.09	6728.58
Top Width (ft)	3756.88	Top Width (ft)	1604.59	1500.00	652.29

Vel Total (ft/s)	6.70	Avg. Vel. (ft/s)	5.45	7.87	4.74
Max Chl Dpth (ft)	5.35	Hydr. Depth (ft)	2.67	4.65	2.17
Conv. Total (cfs)	1276630.0	Conv. (cfs)	351003.1	824569.1	101057.7
Length Wtd. (ft)	1400.00	Wetted Per. (ft)	1604.60	1500.00	652.31
Min Ch El (ft)	4473.00	Shear (lb/sq ft)	0.74	1.29	0.60
Alpha	1.11	Stream Power (lb/ft s)	4.03	10.13	2.85
Frctn Loss (ft)	8.98	Cum Volume (acre-ft)	308.95	1270.23	92.24
C & E Loss (ft)	0.05	Cum SA (acres)	148.80	344.79	49.39

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION RIVER: Skull Valley  
 REACH: PFSF RS: 4500

## INPUT

Description: Section A3

Station Elevation Data		num=	6						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	4480	2000	4470	5300	4465	6500	4465	7000	4470
7900	4480								

Manning's n Values		num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	5300	.035	6500	.035

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
5300	6500	1700	1700	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4465.49	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.21	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4465.70	Reach Len. (ft)	1700.00	1700.00	1700.00
Crit W.S. (ft)	4465.49	Flow Area (sq ft)	78.36	584.77	11.87
E.G. Slope (ft/ft)	0.020753	Area (sq ft)	78.36	584.77	11.87
Q Total (cfs)	2430.00	Flow (cfs)	186.97	2214.71	28.33
Top Width (ft)	1570.35	Top Width (ft)	321.62	1200.00	48.73
Vel Total (ft/s)	3.60	Avg. Vel. (ft/s)	2.39	3.79	2.39
Max Chl Dpth (ft)	0.49	Hydr. Depth (ft)	0.24	0.49	0.24
Conv. Total (cfs)	16868.1	Conv. (cfs)	1297.8	15373.6	196.6
Length Wtd. (ft)	1700.00	Wetted Per. (ft)	321.62	1200.00	48.73
Min Ch El (ft)	4465.00	Shear (lb/sq ft)	0.32	0.63	0.32
Alpha	1.05	Stream Power (lb/ft s)	0.75	2.39	0.75
Frctn Loss (ft)	11.31	Cum Volume (acre-ft)	2.89	103.37	0.47
C & E Loss (ft)	0.04	Cum SA (acres)	10.82	147.68	1.75

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning - During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates

that there is not a valid subcritical answer. The program defaulted to critical depth.

Warning - The parabolic search method failed to converge on critical depth. The program will try the

cross section slice/secant method to find critical depth.

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4467.99	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.03	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4469.02	Reach Len. (ft)	1700.00	1700.00	1700.00
Crit W.S. (ft)	4467.99	Flow Area (sq ft)	2944.92	3584.77	446.20
E.G. Slope (ft/ft)	0.011067	Area (sq ft)	2944.92	3584.77	446.20
Q Total (cfs)	53000.00	Flow (cfs)	17186.53	33209.54	2603.93
Top Width (ft)	3470.35	Top Width (ft)	1971.62	1200.00	298.73
Vel Total (ft/s)	7.60	Avg. Vel. (ft/s)	5.84	9.26	5.84
Max Chl Dpth (ft)	2.99	Hydr. Depth (ft)	1.49	2.99	1.49
Conv. Total (cfs)	503795.0	Conv. (cfs)	163367.7	315675.5	24751.9
Length Wtd. (ft)	1700.00	Wetted Per. (ft)	1971.62	1200.00	298.75
Min Ch El (ft)	4465.00	Shear (lb/sq ft)	1.03	2.06	1.03
Alpha	1.15	Stream Power (lb/ft s)	6.02	19.12	6.02
Frctn Loss (ft)	11.06	Cum Volume (acre-ft)	99.25	806.31	31.74
C & E Loss (ft)	0.15	Cum SA (acres)	63.69	279.03	24.47

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning - During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates

that there is not a valid subcritical answer. The program defaulted to critical depth.

#### CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4468.83	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.26	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4470.09	Reach Len. (ft)	1700.00	1700.00	1700.00
Crit W.S. (ft)	4468.83	Flow Area (sq ft)	4831.06	4591.41	731.98
E.G. Slope (ft/ft)	0.010220	Area (sq ft)	4831.06	4591.41	731.98
Q Total (cfs)	85000.00	Flow (cfs)	31952.90	48205.90	4841.19
Top Width (ft)	4107.89	Top Width (ft)	2525.27	1200.00	382.62
Vel Total (ft/s)	8.37	Avg. Vel. (ft/s)	6.61	10.50	6.61
Max Chl Dpth (ft)	3.83	Hydr. Depth (ft)	1.91	3.83	1.91
Conv. Total (cfs)	840816.4	Conv. (cfs)	316076.8	476850.8	47888.9
Length Wtd. (ft)	1700.00	Wetted Per. (ft)	2525.28	1200.00	382.64
Min Ch El (ft)	4465.00	Shear (lb/sq ft)	1.22	2.44	1.22
Alpha	1.16	Stream Power (lb/ft s)	8.07	25.63	8.07
Frctn Loss (ft)	11.06	Cum Volume (acre-ft)	162.35	1084.39	57.68
C & E Loss (ft)	0.16	Cum SA (acres)	82.43	301.40	32.75

Warning - The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning - The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning - The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning - During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates

that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION RIVER: Skull Valley  
REACH: PFSF RS: 2800

## INPUT

Description: Section A2

Station		Elevation Data		num=		6			
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	4470	2400	4460	4500	4450	6300	4455	6800	4460
8200	4470								

Manning's n Values

Sta		n Val		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	2400	.035	6800	.035		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2400	6800		1500	1500	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4451.91	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.09	Wt. n-Val.		0.035	
E.G. Elev (ft)	4451.99	Reach Len. (ft)	1500.00	1500.00	1500.00
Crit W.S. (ft)		Flow Area (sq ft)		1038.28	
E.G. Slope (ft/ft)	0.003234	Area (sq ft)		1038.28	
Q Total (cfs)	2430.00	Flow (cfs)		2430.00	
Top Width (ft)	1087.95	Top Width (ft)		1087.95	
Vel Total (ft/s)	2.34	Avg. Vel. (ft/s)		2.34	
Max Chl Dpth (ft)	1.91	Hydr. Depth (ft)		0.95	
Conv. Total (cfs)	42727.9	Conv. (cfs)		42727.9	
Length Wtd. (ft)	1500.00	Wetted Per. (ft)		1087.96	
Min Ch El (ft)	4450.00	Shear (lb/sq ft)		0.19	
Alpha	1.00	Stream Power (lb/ft s)		0.45	
Frctn Loss (ft)	5.60	Cum Volume (acre-ft)	1.36	71.70	0.24
C & E Loss (ft)	0.00	Cum SA (acres)	4.54	103.03	0.80

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4455.70	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.52	Wt. n-Val.		0.035	
E.G. Elev (ft)	4456.21	Reach Len. (ft)	1500.00	1500.00	1500.00
Crit W.S. (ft)		Flow Area (sq ft)		9184.57	
E.G. Slope (ft/ft)	0.004278	Area (sq ft)		9184.57	
Q Total (cfs)	53000.00	Flow (cfs)		53000.00	
Top Width (ft)	3065.85	Top Width (ft)		3065.85	
Vel Total (ft/s)	5.77	Avg. Vel. (ft/s)		5.77	
Max Chl Dpth (ft)	5.70	Hydr. Depth (ft)		3.00	
Conv. Total (cfs)	810318.5	Conv. (cfs)		810318.5	
Length Wtd. (ft)	1500.00	Wetted Per. (ft)		3065.87	
Min Ch El (ft)	4450.00	Shear (lb/sq ft)		0.80	
Alpha	1.00	Stream Power (lb/ft s)		4.62	
Frctn Loss (ft)	6.54	Cum Volume (acre-ft)	41.79	557.14	23.04
C & E Loss (ft)	0.02	Cum SA (acres)	25.22	195.79	18.64

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4456.72	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.72	Wt. n-Val.		0.035	
E.G. Elev (ft)	4457.44	Reach Len. (ft)	1500.00	1500.00	1500.00
Crit W.S. (ft)		Flow Area (sq ft)		12492.89	
E.G. Slope (ft/ft)	0.004501	Area (sq ft)		12492.89	
Q Total (cfs)	85000.00	Flow (cfs)		85000.00	
Top Width (ft)	3383.87	Top Width (ft)		3383.87	
Vel Total (ft/s)	6.80	Avg. Vel. (ft/s)		6.80	
Max Chl Dpth (ft)	6.72	Hydr. Depth (ft)		3.69	
Conv. Total (cfs)	1266931.0	Conv. (cfs)		1266931.0	
Length Wtd. (ft)	1500.00	Wetted Per. (ft)		3383.90	

Min Ch El (ft)	4450.00	Shear (lb/sq ft)		1.04	
Alpha	1.00	Stream Power (lb/ft s)		7.06	
Frctn Loss (ft)	6.68	Cum Volume (acre-ft)	68.08	751.02	43.40
C & E Loss (ft)	0.04	Cum SA (acres)	33.16	211.96	25.29

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION RIVER: Skull Valley  
REACH: PFSF RS: 1300

## INPUT

Description: Section A1

Station Elevation Data		num= 6							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	4460	2400	4450	4500	4445	6300	4447	6900	4450
7700	4460								

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	2400	.035	6300	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2400	6300		1300	1300	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4446.32	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.07	Wt. n-Val.		0.035	
E.G. Elev (ft)	4446.39	Reach Len. (ft)	1300.00	1300.00	1300.00
Crit W.S. (ft)	4445.96	Flow Area (sq ft)		1147.98	
E.G. Slope (ft/ft)	0.004331	Area (sq ft)		1147.98	
Q Total (cfs)	2430.00	Flow (cfs)		2430.00	
Top Width (ft)	1740.88	Top Width (ft)		1740.88	
Vel Total (ft/s)	2.12	Avg. Vel. (ft/s)		2.12	
Max Chl Dpth (ft)	1.32	Hydr. Depth (ft)		0.66	
Conv. Total (cfs)	36923.5	Conv. (cfs)		36923.5	
Length Wtd. (ft)	1300.00	Wetted Per. (ft)		1740.88	
Min Ch El (ft)	4445.00	Shear (lb/sq ft)		0.18	
Alpha	1.00	Stream Power (lb/ft s)		0.38	
Frctn Loss (ft)	5.73	Cum Volume (acre-ft)	1.36	34.06	0.24
C & E Loss (ft)	0.00	Cum SA (acres)	4.54	54.33	0.80

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4449.21	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.45	Wt. n-Val.		0.035	0.035
E.G. Elev (ft)	4449.66	Reach Len. (ft)	1300.00	1300.00	1300.00
Crit W.S. (ft)		Flow Area (sq ft)		9491.21	487.31
E.G. Slope (ft/ft)	0.004435	Area (sq ft)		9491.21	487.31
Q Total (cfs)	53000.00	Flow (cfs)		51528.43	1471.57
Top Width (ft)	4008.66	Top Width (ft)		3567.16	441.50
Vel Total (ft/s)	5.31	Avg. Vel. (ft/s)		5.43	3.02
Max Chl Dpth (ft)	4.21	Hydr. Depth (ft)		2.66	1.10
Conv. Total (cfs)	795811.3	Conv. (cfs)		773715.1	22096.1
Length Wtd. (ft)	1300.00	Wetted Per. (ft)		3567.16	441.51
Min Ch El (ft)	4445.00	Shear (lb/sq ft)		0.74	0.31
Alpha	1.02	Stream Power (lb/ft s)		4.00	0.92
Frctn Loss (ft)	5.80	Cum Volume (acre-ft)	41.79	235.58	14.65
C & E Loss (ft)	0.01	Cum SA (acres)	25.22	81.58	11.04

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

## CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4450.13	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.59	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4450.72	Reach Len. (ft)	1300.00	1300.00	1300.00
Crit W.S. (ft)		Flow Area (sq ft)	1.93	12945.12	976.82
E.G. Slope (ft/ft)	0.004412	Area (sq ft)	1.93	12945.12	976.82
Q Total (cfs)	85000.00	Flow (cfs)	0.87	81229.45	3769.68
Top Width (ft)	4540.63	Top Width (ft)	30.47	3900.00	610.16
Vel Total (ft/s)	6.10	Avg. Vel. (ft/s)	0.45	6.27	3.86
Max Chl Dpth (ft)	5.13	Hydr. Depth (ft)	0.06	3.32	1.60
Conv. Total (cfs)	1279673.0	Conv. (cfs)	13.1	1222907.0	56752.4
Length Wtd. (ft)	1300.00	Wetted Per. (ft)	30.47	3900.01	610.16
Min Ch El (ft)	4445.00	Shear (lb/sq ft)	0.02	0.91	0.44
Alpha	1.03	Stream Power (lb/ft s)	0.01	5.74	1.70
Frctn Loss (ft)	5.77	Cum Volume (acre-ft)	68.05	313.04	26.58
C & E Loss (ft)	0.01	Cum SA (acres)	32.63	86.55	14.78

Warning - The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION RIVER: Skull Valey  
REACH: PFSF RS: 0

## INPUT

Description: Section A

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	4450	5100	4440	7000	4440	7900	4450	8700	4470

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	5100	.035	7000	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	5100	7000		0	0	.1	.3

## CROSS SECTION OUTPUT Profile #100-year Q

W.S. Elev (ft)	4440.60	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.06	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4440.66	Reach Len. (ft)			
Crit W.S. (ft)	4440.36	Flow Area (sq ft)	90.94	1134.62	16.05
E.G. Slope (ft/ft)	0.004509	Area (sq ft)	90.94	1134.62	16.05
Q Total (cfs)	2430.00	Flow (cfs)	115.81	2293.75	20.44
Top Width (ft)	2258.30	Top Width (ft)	304.56	1900.00	53.75
Vel Total (ft/s)	1.96	Avg. Vel. (ft/s)	1.27	2.02	1.27
Max Chl Dpth (ft)	0.60	Hydr. Depth (ft)	0.30	0.60	0.30
Conv. Total (cfs)	36188.2	Conv. (cfs)	1724.7	34159.2	304.3
Length Wtd. (ft)		Wetted Per. (ft)	304.56	1900.00	53.75
Min Ch El (ft)	4440.00	Shear (lb/sq ft)	0.08	0.17	0.08
Alpha	1.03	Stream Power (lb/ft s)	0.11	0.34	0.11
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

## CROSS SECTION OUTPUT Profile #PMF

W.S. Elev (ft)	4443.31	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.53	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4443.84	Reach Len. (ft)			
Crit W.S. (ft)	4442.56	Flow Area (sq ft)	2800.50	6296.53	494.21
E.G. Slope (ft/ft)	0.004500	Area (sq ft)	2800.50	6296.53	494.21
Q Total (cfs)	53000.00	Flow (cfs)	11168.44	39860.73	1970.82
Top Width (ft)	3888.38	Top Width (ft)	1690.12	1900.00	298.26
Vel Total (ft/s)	5.53	Avg. Vel. (ft/s)	3.99	6.33	3.99
Max Chl Dpth (ft)	3.31	Hydr. Depth (ft)	1.66	3.31	1.66
Conv. Total (cfs)	790055.8	Conv. (cfs)	166484.7	594192.6	29378.5
Length Wtd. (ft)		Wetted Per. (ft)	1690.13	1900.00	298.28
Min Ch El (ft)	4440.00	Shear (lb/sq ft)	0.47	0.93	0.47

Alpha	1.12	Stream Power (lb/ft s)	1.86	5.89	1.86
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

## CROSS SECTION OUTPUT Profile #PMF1

W.S. Elev (ft)	4444.23	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.71	Wt. n-Val.	0.035	0.035	0.035
E.G. Elev (ft)	4444.94	Reach Len. (ft)			
Crit W.S. (ft)	4443.38	Flow Area (sq ft)	4558.44	8033.25	804.43
E.G. Slope (ft/ft)	0.004502	Area (sq ft)	4558.44	8033.25	804.43
Q Total (cfs)	85000.00	Flow (cfs)	21389.48	59836.06	3774.46
Top Width (ft)	4436.82	Top Width (ft)	2156.29	1900.00	380.52
Vel Total (ft/s)	6.35	Avg. Vel. (ft/s)	4.69	7.45	4.69
Max Chl Dpth (ft)	4.23	Hydr. Depth (ft)	2.11	4.23	2.11
Conv. Total (cfs)	1266775.0	Conv. (cfs)	318772.5	891751.2	56251.7
Length Wtd. (ft)		Wetted Per. (ft)	2156.30	1900.00	380.55
Min Ch El (ft)	4440.00	Shear (lb/sq ft)	0.59	1.19	0.59
Alpha	1.13	Stream Power (lb/ft s)	2.79	8.85	2.79
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

## SUMMARY OF MANNING'S N VALUES

River: Skull Valley

Reach	River Sta.	n1	n2	n3
PFSF	9400	.035	.035	.035
PFSF	5900	.035	.035	.035
PFSF	4500	.035	.035	.035
PFSF	2800	.035	.035	.035
PFSF	1300	.035	.035	.035
PFSF	0	.035	.035	.035

## SUMMARY OF REACH LENGTHS

River: Skull Valley

Reach	River Sta.	Left	Channel	Right
PFSF	9400	3500	3500	3500
PFSF	5900	1400	1400	1400
PFSF	4500	1700	1700	1700
PFSF	2800	1500	1500	1500
PFSF	1300	1300	1300	1300
PFSF	0	0	0	0

# **ATTACHMENT 4** **HEC-1 INPUT DATA FOR THE SOIL CURVE NUMBER SENTIVITY RUNS**

## **SOIL CURVE NO. 75, TC = 18.31 HOUR**

ID PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
ID GENERAL PMF AT ACCESS RD  
ID TC = 18.31 HOUR, SOIL CURVE NO. 75  
ID  
IT 60 200  
IO 2  
PG 60  
IN 180  
PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98  
PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17  
PI 0.16 0.16 0.15 0.14  
KK 010  
KM SCS DIMENSIONLESS UNIT HYDROGRAPH  
BA 270.0  
BF -1 1.06  
PR 60  
LS 0 75 1  
UD 11.0  
ZZ

## **SOIL CURVE NO. 80, TC = 18.31 HOUR**

ID PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
ID GENERAL PMF AT ACCESS RD  
ID TC = 18.31 HOUR, SOIL CURVE NO. 80  
ID  
IT 60 200  
IO 2  
PG 60  
IN 180  
PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98  
PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17  
PI 0.16 0.16 0.15 0.14  
KK 010  
KM SCS DIMENSIONLESS UNIT HYDROGRAPH  
BA 270.0  
BF -1 1.06  
PR 60  
LS 0 80 1  
UD 11.0  
ZZ

## **SOIL CURVE NO. 85, TC = 18.31 HOUR**

ID PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
ID GENERAL PMF AT ACCESS RD  
ID TC = 18.31 HOUR, SOIL CURVE NO. 85  
ID  
IT 60 200  
IO 2  
PG 60  
IN 180  
PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98  
PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17  
PI 0.16 0.16 0.15 0.14  
KK 010  
KM SCS DIMENSIONLESS UNIT HYDROGRAPH  
BA 270.0



BF -1 1.06  
 PR 60  
 LS 0 85 1  
 UD 11.0  
 ZZ

### SOIL CURVE NO. 90, TC = 18.31 HOUR

ID PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
 ID GENERAL PMF AT ACCESS RD  
 ID TC = 18.31 HOUR, SOIL CURVE NO. 90  
 ID  
 IT 60 200  
 IO 2  
 PG 60  
 IN 180  
 PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98  
 PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17  
 PI 0.16 0.16 0.15 0.14  
 KK 010  
 KM SCS DIMENSIONLESS UNIT HYDROGRAPH  
 BA 270.0  
 BF -1 1.06  
 PR 60  
 LS 0 90 1  
 UD 11.0  
 ZZ

### SOIL CURVE NO. 96, TC = 18.31 HOUR

ID PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
 ID GENERAL PMF AT ACCESS RD  
 ID TC = 18.31 HOUR, SOIL CURVE NO. 96  
 ID  
 IT 60 200  
 IO 2  
 PG 60  
 IN 180  
 PI 0.18 0.27 0.29 0.35 0.36 0.38 0.62 0.68 0.92 0.98  
 PI 1.07 2.83 0.62 0.48 0.43 0.43 0.38 0.38 0.17 0.17  
 PI 0.16 0.16 0.15 0.14  
 KK 010  
 KM SCS DIMENSIONLESS UNIT HYDROGRAPH  
 BA 270.0  
 BF -1 1.06  
 PR 60  
 LS 0 96 1  
 UD 11.0  
 ZZ

# ATTACHMENT 5

## HEC-1 PROGRAM OUTPUTS - SOIL CURVE NUMBER SENTIVITY RUNS

SOIL CURVE NO. 75, TC = 18.31 HOUR

```

X   X   XXXXXXX   XXXXX   X
X   X   X   X   X   X   XX
X   X   X   X   X   X   X
XXXXXXX   XXXX   X   XXXXX   X
X   X   X   X   X   X   X
X   X   X   X   X   X   X
X   X   XXXXXXX   XXXXX   XXX

```

PFSP (PRIVATE FUEL STORAGE FACILITY PROJECT)  
GENERAL PMF AT ACCESS RD  
TC = 18.31 HOUR, SOIL CURVE NO. 75

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRT      2   PRINT CONTROL
          IPLOT      0   PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

8 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      180  TIME INTERVAL IN MINUTES
          JXDATE      1   0   STARTING DATE
          JXTIME      0   STARTING TIME

IT        HYDROGRAPH TIME DATA
          NMIN       60  MINUTES IN COMPUTATION INTERVAL
          IDATE       1   0   STARTING DATE
          ITIME      0000  STARTING TIME
          NQ         200  NUMBER OF HYDROGRAPH ORDINATES
          NDDATE      9   0   ENDING DATE
          NDTIME     0700  ENDING TIME
          ICENT       19  CENTURY MARK

          COMPUTATION INTERVAL 1.00 HOURS
          TOTAL TIME BASE 199.00 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FeET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

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*   *
12 KK  010 *
*   *
*****

```

SCS DIMENSIONLESS UNIT HYDROGRAPH

SUBBASIN RUNOFF DATA

```

14 BA      SUBBASIN CHARACTERISTICS
          TAREA      270.00  SUBBASIN AREA

15 BF      BASE FLOW CHARACTERISTICS
          STRTQ      270.00  INITIAL FLOW
          QRCSN      .00    BEGIN BASE FLOW RECESSON
          RTIOR      1.06000  RECESSON CONSTANT

```

PRECIPITATION DATA

```

16 PR      RECORDING STATIONS      60
0 PW      WEIGHTS      1.00

17 LS      SCS LOSS RATE
          STRTL      .67  INITIAL ABSTRACTION
          CRVNR      75.00  CURVE NUMBER
          RTIMP      1.00  PERCENT IMPERVIOUS AREA

18 UD      SCS DIMENSIONLESS UNITGRAPH

```





STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

## TEMPORAL DISTRIBUTIONS

STATION 60, WEIGHT = 1.00

.06	.06	.06	.09	.09	.09	.10	.10	.10	.12
.12	.12	.12	.12	.12	.13	.13	.13	.21	.21
.21	.23	.23	.23	.31	.31	.31	.33	.33	.33
.36	.36	.36	.94	.94	.94	.21	.21	.21	.16
.16	.16	.14	.14	.14	.14	.14	.14	.13	.13
.13	.13	.13	.13	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05								

## UNIT HYDROGRAPH

57 END-OF-PERIOD ORDINATES

296.	927.	1755.	2805.	4146.	5798.	7642.	9219.	10329.	11019.
11290.	11290.	11019.	10407.	9712.	8924.	7957.	6823.	5758.	4905.
4245.	3668.	3175.	2815.	2455.	2140.	1844.	1588.	1391.	1199.
1051.	903.	786.	678.	587.	513.	443.	388.	334.	293.
254.	220.	191.	164.	144.	125.	113.	101.	89.	77.
66.	54.	44.	35.	25.	15.	5.			

TOTAL RAINFALL = 12.60, TOTAL LOSS = 2.55, TOTAL EXCESS = 10.05

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	199.00-HR	
+		(CFS)				
+	60341.	45.00	58960.	46381.	24051.	8826.
		(INCHES)	2.030	6.389	9.939	10.080
		(AC-FT)	29237.	91995.	143115.	145158.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

TIME OF	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	MAX
STAGE					6-HOUR	24-HOUR	72-HOUR			
+										
+	HYDROGRAPH AT	010	60341.	45.00	58960.	46381.	24051.	270.00		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## SOIL CURVE NO. 85, TC = 18.31 HOUR

X	X	XXXXXX	XXXXX	X
X	X	X	X	XX
X	X	X	X	X
XXXXXX	XXXX	X	XXXXX	X
X	X	X	X	X
X	X	X	X	X
X	X	XXXXXX	XXXXX	XXX

PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
 GENERAL PMF AT ACCESS RD  
 TC = 18.31 HOUR, SOIL CURVE NO. 85

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 2 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

8 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 180 TIME INTERVAL IN MINUTES  
 JXDATE 1 0 STARTING DATE  
 JXTIME 0 STARTING TIME

IT HYDROGRAPH TIME DATA  
 NMNIN 60 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE

ITIME 0000 STARTING TIME  
 NQ 200 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 9 0 ENDING DATE  
 NDTIME 0700 ENDING TIME  
 ICBNT 19 CENTURY MARK

COMPUTATION INTERVAL 1.00 HOURS  
 TOTAL TIME BASE 199.00 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

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 12 KK \* 010 \*  
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#### SCS DIMENSIONLESS UNIT HYDROGRAPH

##### SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS  
     TAREA 270.00 SUBBASIN AREA  
 15 BF BASE FLOW CHARACTERISTICS  
     STRTQ 270.00 INITIAL FLOW  
     QRCSN .00 BEGIN BASE FLOW RECESSION  
     RTIOR 1.06000 RECESION CONSTANT

##### PRECIPITATION DATA

16 PR RECORDING STATIONS 60  
 0 PW WEIGHTS 1.00  
 17 LS SCS LOSS RATE  
     STRTL .35 INITIAL ABSTRACTION  
     CRVNR 85.00 CURVE NUMBER  
     RTIMP 1.00 PERCENT IMPERVIOUS AREA  
 18 UD SCS DIMENSIONLESS UNITGRAPH  
     TLAG 11.00 LAG

\*\*\*

##### PRECIPITATION STATION DATA

STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

##### TEMPORAL DISTRIBUTIONS

STATION	60	WEIGHT	=	1.00						
.06	.06	.06	.09	.09	.09	.10	.10	.10	.12	
.12	.12	.12	.12	.12	.13	.13	.13	.21	.21	
.21	.23	.23	.23	.31	.31	.31	.33	.33	.33	
.36	.36	.36	.94	.94	.94	.21	.21	.21	.16	
.16	.16	.14	.14	.14	.14	.14	.14	.13	.13	
.13	.13	.13	.13	.06	.06	.06	.06	.06	.06	
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	
.05	.05									

##### UNIT HYDROGRAPH

57 END-OF-PERIOD ORDINATES									
296.	927.	1755.	2805.	4146.	5798.	7642.	9219.	10329.	11019.
11290.	11290.	11019.	10407.	9712.	8924.	7957.	6823.	5758.	4905.
4245.	3668.	3175.	2815.	2455.	2140.	1844.	1588.	1391.	1199.
1051.	903.	786.	678.	587.	513.	443.	388.	334.	293.
254.	220.	191.	164.	144.	125.	113.	101.	89.	77.
66.	54.	44.	35.	25.	15.	5.			

TOTAL RAINFALL = 12.60, TOTAL LOSS = 1.88, TOTAL EXCESS = 10.72

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	199.00-HR
63287.	45.00	61878.	48791.	25605.	9413.

(INCHES)	2.131	6.721	10.580	10.750
(AC-FT)	30683.	96775.	152358.	154802.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

TIME OF STAGE	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	MAX
+					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	010	63287.	45.00	61878.	48791.	25605.	270.00		

SOIL CURVE NO. 90, TC = 18.31 HOUR

```

      X  X  XXXXXXX  XXXXX      X
      X  X  X      X  X      XX
      X  X  X      X      X
      XXXXXXX  XXXX  X      XXXXX  X
      X  X  X      X      X
      X  X  X      X  X      X
      X  X  XXXXXXX  XXXXX      XXX
  
```

PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
GENERAL PMF AT ACCESS RD  
TC = 18.31 HOUR, SOIL CURVE NO. 90

6 IO      OUTPUT CONTROL VARIABLES  
           IPRNT      2    PRINT CONTROL  
           IPLOT      0    PLOT CONTROL  
           QSCAL      0.    HYDROGRAPH PLOT SCALE

8 IN      TIME DATA FOR INPUT TIME SERIES  
           JXMIN      180    TIME INTERVAL IN MINUTES  
           JXDATE      1    0    STARTING DATE  
           JXTIME      0    0    STARTING TIME

IT        HYDROGRAPH TIME DATA  
           NMIN      60    MINUTES IN COMPUTATION INTERVAL  
           IDATE      1    0    STARTING DATE  
           ITIME      0000    STARTING TIME  
           NQ        200    NUMBER OF HYDROGRAPH ORDINATES  
           NDDATE      9    0    ENDING DATE  
           NDTIME      0700    ENDING TIME  
           ICENT      19    CENTURY MARK

          COMPUTATION INTERVAL    1.00 HOURS  
           TOTAL TIME BASE    199.00 HOURS

ENGLISH UNITS

DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-Feet
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

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*      *
*      *
*      *
*      *
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SCS DIMENSIONLESS UNIT HYDROGRAPH

## SUBBASIN RUNOFF DATA

14 BA      SUBBASIN CHARACTERISTICS  
           TAREA      270.00    SUBBASIN AREA

15 BF      BASE FLOW CHARACTERISTICS  
           STRTQ      270.00    INITIAL FLOW  
           QRCSN      .00    BEGIN BASE FLOW RECBSSION

RTIOR 1.06000 RECESSION CONSTANT

## PRECIPITATION DATA

16 PR RECORDING STATIONS 60  
 0 PW WEIGHTS 1.00

17 LS SCS LOSS RATE  
 STRTL .22 INITIAL ABSTRACTION  
 CRVNR 90.00 CURVE NUMBER  
 RTIMP 1.00 PERCENT IMPERVIOUS AREA

18 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 11.00 LAG

\*\*\*

## PRECIPITATION STATION DATA

STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

## TEMPORAL DISTRIBUTIONS

STATION	60	WEIGHT	1.00							
.06	.06	.06	.09	.09	.09	.10	.10	.10	.12	
.12	.12	.12	.12	.12	.13	.13	.13	.21	.21	
.21	.23	.23	.23	.31	.31	.31	.33	.33	.33	
.36	.36	.36	.94	.94	.94	.21	.21	.21	.16	
.16	.16	.14	.14	.14	.14	.14	.14	.13	.13	
.13	.13	.13	.13	.06	.06	.06	.06	.06	.06	
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	
.05	.05									

## UNIT HYDROGRAPH

## 57 END-OF-PERIOD ORDINATES

296.	927.	1755.	2805.	4146.	5798.	7642.	9219.	10329.	11019.
11290.	11290.	11019.	10407.	9712.	8924.	7957.	6823.	5758.	4905.
4245.	3668.	3175.	2815.	2455.	2140.	1844.	1588.	1391.	1199.
1051.	903.	786.	678.	587.	513.	443.	388.	334.	293.
254.	220.	191.	164.	144.	125.	113.	101.	89.	77.
66.	54.	44.	35.	25.	15.	5.			

TOTAL RAINFALL = 12.60, TOTAL LOSS = 1.23, TOTAL EXCESS = 11.37

PEAK FLOW	TIME	6-HR	24-HR	72-HR	199.00-HR
(CFS)	(HR)				
+					
65734.	44.00	64222.	50846.	27081.	9979.
		(INCHES)	2.212	7.004	11.191
		(AC-FT)	31846.	100852.	161144.

CUMULATIVE AREA = 270.00 SQ MI

1

## RUNOFF SUMMARY

FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

TIME OF	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD	BASIN AREA	MAXIMUM STAGE	MAX
STAGE					6-HOUR	24-HOUR	72-HOUR	
+								
	HYDROGRAPH AT	010	65734.	44.00	64222.	50846.	27081.	270.00

SOIL CURVE NO. 96, TC = 18.31 HOUR

```

X   X   XXXXXX   XXXX   X
X   X   X       X   X   XX
X   X   X       X       X
XXXXXX   XXXX   X       XXXX   X
X   X   X       X       X
X   X   X       X   X   X
X   X   XXXXXX   XXXX   XXX

```

PFSF (PRIVATE FUEL STORAGE FACILITY PROJECT)  
 GENERAL PMF AT ACCESS RD  
 TC = 18.31 HOUR, SOIL CURVE NO. 96



6 IO        OUTPUT CONTROL VARIABLES  
              IPRNT        2    PRINT CONTROL  
              IPLOT        0    PLOT CONTROL  
              QSCAL        0.   HYDROGRAPH PLOT SCALE

8 IN        TIME DATA FOR INPUT TIME SERIES  
              JXMIN        180   TIME INTERVAL IN MINUTES  
              JXDATE       1    0   STARTING DATE  
              JXTIME        0    0   STARTING TIME

IT        HYDROGRAPH TIME DATA  
              NMIN        60   MINUTES IN COMPUTATION INTERVAL  
              IDATE        1    0   STARTING DATE  
              ITIME        0000   STARTING TIME  
              NQ        200   NUMBER OF HYDROGRAPH ORDINATES  
              NDDATE       9    0   ENDING DATE  
              NDTIME       0700   ENDING TIME  
              ICENT        19   CENTURY MARK

             COMPUTATION INTERVAL    1.00 HOURS  
              TOTAL TIME BASE    199.00 HOURS

ENGLISH UNITS  
      DRAINAGE AREA        SQUARE MILES  
      PRECIPITATION DEPTH   INCHES  
      LENGTH, ELEVATION    FEET  
      FLOW                CUBIC FEET PER SECOND  
      STORAGE VOLUME       ACRE-FOOT  
      SURFACE AREA        ACRES  
      TEMPERATURE        DEGREES FAHRENHEIT

\*\*\*  
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12 KK        \*\*\*\*\*  
              \*               \*  
              \*               \*  
              \*               \*  
              \*               \*  
              \*\*\*\*\*

             SCS DIMENSIONLESS UNIT HYDROGRAPH

#### SUBBASIN RUNOFF DATA

14 BA        SUBBASIN CHARACTERISTICS  
              TAREA        270.00   SUBBASIN AREA

15 BF        BASE FLOW CHARACTERISTICS  
              STRTQ        270.00   INITIAL FLOW  
              QRCSN        .00    BEGIN BASE FLOW RECESSION  
              RTIOR        1.06000   RECESSION CONSTANT

#### PRECIPITATION DATA

16 PR        RECORDING STATIONS        60  
      0 PW        WEIGHTS        1.00

17 LS        SCS LOSS RATE  
              STRTL        .08   INITIAL ABSTRACTION  
              CRVNR        96.00   CURVE NUMBER  
              RTIMP        1.00   PERCENT IMPERVIOUS AREA

18 UD        SCS DIMENSIONLESS UNITGRAPH  
              TLAG        11.00   LAG

\*\*\*

#### PRECIPITATION STATION DATA

STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

#### TEMPORAL DISTRIBUTIONS

STATION	60,	WEIGHT =	1.00							
.06	.06	.06	.09	.09	.09	.10	.10	.10	.12	
.12	.12	.12	.12	.12	.13	.13	.13	.13	.21	.21
.21	.23	.23	.23	.31	.31	.31	.33	.33	.33	.33
.36	.36	.36	.94	.94	.94	.21	.21	.21	.16	
.16	.16	.14	.14	.14	.14	.14	.14	.13	.13	
.13	.13	.13	.13	.06	.06	.06	.06	.06	.06	
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	
.05	.05									

#### UNIT HYDROGRAPH

57 END-OF-PERIOD ORDINATES									
296.	927.	1755.	2805.	4146.	5798.	7642.	9219.	10329.	11019.
11290.	11290.	11019.	10407.	9712.	8924.	7957.	6823.	5758.	4905.

4245.	3668.	3175.	2815.	2455.	2140.	1844.	1588.	1391.	1199.
1051.	903.	786.	678.	587.	513.	443.	388.	334.	293.
254.	220.	191.	164.	144.	125.	113.	101.	89.	77.
66.	54.	44.	35.	25.	15.	5.			

TOTAL RAINFALL = 12.60, TOTAL LOSS = .48, TOTAL EXCESS = 12.12

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	199.00-HR
+ (CFS)	(HR)				
+ 67759.	44.00	66108.	52606.	28730.	10634.
	(INCHES)	2.276	7.246	11.872	12.145
	(AC-FT)	32781.	104343.	170954.	174886.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

TIME OF STAGE	OPERATION	STATION	PEAK	TIME OF	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN	MAXIMUM
			FLOW	PEAK	6-HOUR	24-HOUR	72-HOUR	AREA	STAGE
+	HYDROGRAPH AT	010	67759.	44.00	66108.	52606.	28730.	270.00	

\*\*\* NORMAL END OF HEC-1 \*\*\*

## Attachment 6, HEC-1 Input Data and Program Output

### PMF Run with Tc=11 Hour and Soil Group Curve Number = 96

#### Input Data

```

ID  PFSF (Private Fuel Storage Facility Project)
ID  General PMF AT ACCESS RD
ID  Tc = 11.0 hour, Soil curve No. 96
ID
IT  60                      200
IO  2
PG  60
IN  180
PI  0.18  0.27  0.29  0.35  0.36  0.38  0.62  0.68  0.92  0.98
PI  1.07  2.83  0.62  0.48  0.43  0.43  0.38  0.38  0.17  0.17
PI  0.16  0.16  0.15  0.14
KK  010
KM  SCS DIMENSIONLESS UNIT HYDROGRAPH
BA  270.0
BF  -1          1.06
PR  60
LS  0          96          1
UD  6.6
ZZ

```

#### Program Output

```

X  X  XXXXXXX  XXXXX  X
X  X  X      X      XX
X  X  X      X      X
XXXXXXX XXXX  X      XXXXX
X  X  X      X      X
X  X  X      X      X
X  X  XXXXXXX  XXXXX  XXX

```

PFSF (Private Fuel Storage Facility Project)  
 General PMF AT ACCESS RD  
 Tc = 11.0 hour, Soil curve No. 96

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      2  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

8 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      180  TIME INTERVAL IN MINUTES
          JXDATE      1  0  STARTING DATE
          JXTIME      0  STARTING TIME

IT        HYDROGRAPH TIME DATA
          NMIN      60  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000  STARTING TIME
          NQ        200  NUMBER OF HYDROGRAPH ORDINATES
          NDDATE      9  0  ENDING DATE
          NDTIME      0700  ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL  1.00 HOURS
          TOTAL TIME BASE  199.00 HOURS

```

## ENGLISH UNITS

DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-FEET
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

\*\*\* \*\*

\*\*\*\*\*  
 \*  
 12 KK \* 010 \*  
 \*  
 \*\*\*\*\*

## SCS DIMENSIONLESS UNIT HYDROGRAPH

## SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS  
 TAREA 270.00 SUBBASIN AREA

15 BF BASE FLOW CHARACTERISTICS  
 STRTQ 270.00 INITIAL FLOW  
 QRCSN .00 BEGIN BASE FLOW RECESSION  
 RTIOR 1.06000 RECESSION CONSTANT

## PRECIPITATION DATA

16 PR RECORDING STATIONS 60  
 0 PW WEIGHTS 1.00

17 LS SCS LOSS RATE  
 STRTL .08 INITIAL ABSTRACTION  
 CRVNB 96.00 CURVE NUMBER  
 RTIMP 1.00 PERCENT IMPERVIOUS AREA

18 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 6.60 LAG

\*\*\*

## PRECIPITATION STATION DATA

STATION	TOTAL	AVG. ANNUAL	WEIGHT
60	12.60	.00	1.00

## TEMPORAL DISTRIBUTIONS

STATION		60,	WEIGHT =	1.00					
.10	.12	.06	.06	.06	.09	.09	.09	.10	.10
.21	.21	.12	.12	.12	.12	.12	.13	.13	.13
.33	.33	.21	.23	.23	.23	.31	.31	.31	.33
.21	.16	.36	.36	.36	.94	.94	.94	.21	.21
.13	.13	.16	.16	.14	.14	.14	.14	.14	.14
.06	.06	.13	.13	.13	.13	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
		.05	.05						

UNIT HYDROGRAPH									
35 END-OF-PERIOD ORDINATES									
14175.	1076.	3188.	6358.	10847.	15150.	17583.	18346.	17893.	16216.
1380.	11406.	8632.	6823.	5403.	4389.	3508.	2732.	2204.	1756.
152.	1096.	875.	695.	553.	444.	352.	275.	223.	183.
	121.	91.	65.	39.	13.				

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## HYDROGRAPSTA 010

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	.00	.00	.00	.00	270.	*	5	0400	101	.00	.00	.00	.00	32.
1	0100	2	.06	.06	.00	.00	255.	*	5	0500	102	.00	.00	.00	.00	24.
1	0200	3	.06	.06	.00	.00	246.	*	5	0600	103	.00	.00	.00	.00	16.
1	0300	4	.06	.04	.02	.02	259.	*	5	0700	104	.00	.00	.00	.00	10.
1	0400	5	.09	.05	.04	.04	336.	*	5	0800	105	.00	.00	.00	.00	6.
1	0500	6	.09	.04	.05	.05	534.	*	5	0900	106	.00	.00	.00	.00	3.
1	0600	7	.09	.03	.06	.06	914.	*	5	1000	107	.00	.00	.00	.00	1.
1	0700	8	.10	.02	.07	.07	1536.	*	5	1100	108	.00	.00	.00	.00	1.
1	0800	9	.10	.02	.08	.08	2408.	*	5	1200	109	.00	.00	.00	.00	0.
1	0900	10	.10	.02	.08	.08	3490.	*	5	1300	110	.00	.00	.00	.00	0.
1	1000	11	.12	.02	.10	.10	4741.	*	5	1400	111	.00	.00	.00	.00	0.
1	1100	12	.12	.01	.10	.10	6110.	*	5	1500	112	.00	.00	.00	.00	0.
1	1200	13	.12	.01	.11	.11	7540.	*	5	1600	113	.00	.00	.00	.00	0.
1	1300	14	.12	.01	.11	.11	8995.	*	5	1700	114	.00	.00	.00	.00	0.
1	1400	15	.12	.01	.11	.11	10428.	*	5	1800	115	.00	.00	.00	.00	0.
1	1500	16	.12	.01	.11	.11	11785.	*	5	1900	116	.00	.00	.00	.00	0.
1	1600	17	.13	.01	.12	.12	13053.	*	5	2000	117	.00	.00	.00	.00	0.
1	1700	18	.13	.01	.12	.12	14222.	*	5	2100	118	.00	.00	.00	.00	0.
1	1800	19	.13	.00	.12	.12	15282.	*	5	2200	119	.00	.00	.00	.00	0.
1	1900	20	.21	.01	.20	.20	16328.	*	5	2300	120	.00	.00	.00	.00	0.
1	2000	21	.21	.01	.20	.20	17431.	*	6	0000	121	.00	.00	.00	.00	0.
1	2100	22	.21	.00	.20	.20	18673.	*	6	0100	122	.00	.00	.00	.00	0.
1	2200	23	.23	.00	.22	.22	20191.	*	6	0200	123	.00	.00	.00	.00	0.
1	2300	24	.23	.00	.22	.22	21997.	*	6	0300	124	.00	.00	.00	.00	0.
2	0000	25	.23	.00	.22	.22	23978.	*	6	0400	125	.00	.00	.00	.00	0.
2	0100	26	.31	.00	.30	.30	26124.	*	6	0500	126	.00	.00	.00	.00	0.
2	0200	27	.31	.00	.30	.30	28424.	*	6	0600	127	.00	.00	.00	.00	0.
2	0300	28	.31	.00	.30	.30	30838.	*	6	0700	128	.00	.00	.00	.00	0.
2	0400	29	.33	.00	.32	.32	33443.	*	6	0800	129	.00	.00	.00	.00	0.
2	0500	30	.33	.00	.32	.32	36171.	*	6	0900	130	.00	.00	.00	.00	0.
2	0600	31	.33	.00	.32	.32	38877.	*	6	1000	131	.00	.00	.00	.00	0.
2	0700	32	.36	.00	.35	.35	41559.	*	6	1100	132	.00	.00	.00	.00	0.
2	0800	33	.36	.00	.35	.35	44167.	*	6	1200	133	.00	.00	.00	.00	0.
2	0900	34	.36	.00	.36	.36	46634.	*	6	1300	134	.00	.00	.00	.00	0.
2	1000	35	.94	.00	.94	.94	49597.	*	6	1400	135	.00	.00	.00	.00	0.
2	1100	36	.94	.00	.94	.94	53593.	*	6	1500	136	.00	.00	.00	.00	0.
2	1200	37	.94	.00	.94	.94	59190.	*	6	1600	137	.00	.00	.00	.00	0.
2	1300	38	.21	.00	.21	.21	66398.	*	6	1700	138	.00	.00	.00	.00	0.
2	1400	39	.21	.00	.21	.21	74338.	*	6	1800	139	.00	.00	.00	.00	0.
2	1500	40	.21	.00	.21	.21	81148.	*	6	1900	140	.00	.00	.00	.00	0.
2	1600	41	.16	.00	.16	.16	84857.	*	6	2000	141	.00	.00	.00	.00	0.
2	1700	42	.16	.00	.16	.16	84839.	*	6	2100	142	.00	.00	.00	.00	0.
2	1800	43	.16	.00	.16	.16	81737.	*	6	2200	143	.00	.00	.00	.00	0.
2	1900	44	.14	.00	.14	.14	76527.	*	6	2300	144	.00	.00	.00	.00	0.
2	2000	45	.14	.00	.14	.14	69689.	*	7	0000	145	.00	.00	.00	.00	0.
2	2100	46	.14	.00	.14	.14	62217.	*	7	0100	146	.00	.00	.00	.00	0.
2	2200	47	.14	.00	.14	.14	55012.	*	7	0200	147	.00	.00	.00	.00	0.
2	2300	48	.14	.00	.14	.14	48906.	*	7	0300	148	.00	.00	.00	.00	0.
3	0000	49	.14	.00	.14	.14	44243.	*	7	0400	149	.00	.00	.00	.00	0.
3	0100	50	.13	.00	.13	.13	40425.	*	7	0500	150	.00	.00	.00	.00	0.

3	0200	51	.13	.00	.13	37272.	*	7	0600	151	.00	.00	.00	0.
3	0300	52	.13	.00	.13	34639.	*	7	0700	152	.00	.00	.00	0.
3	0400	53	.13	.00	.13	32417.	*	7	0800	153	.00	.00	.00	0.
3	0500	54	.13	.00	.13	30572.	*	7	0900	154	.00	.00	.00	0.
3	0600	55	.13	.00	.13	28991.	*	7	1000	155	.00	.00	.00	0.
3	0700	56	.06	.00	.06	27585.	*	7	1100	156	.00	.00	.00	0.
3	0800	57	.06	.00	.06	26263.	*	7	1200	157	.00	.00	.00	0.
3	0900	58	.06	.00	.06	24909.	*	7	1300	158	.00	.00	.00	0.
3	1000	59	.06	.00	.06	23405.	*	7	1400	159	.00	.00	.00	0.
3	1100	60	.06	.00	.06	21750.	*	7	1500	160	.00	.00	.00	0.
3	1200	61	.06	.00	.06	20051.	*	7	1600	161	.00	.00	.00	0.
3	1300	62	.05	.00	.05	18390.	*	7	1700	162	.00	.00	.00	0.
3	1400	63	.05	.00	.05	16835.	*	7	1800	163	.00	.00	.00	0.
3	1500	64	.05	.00	.05	15453.	*	7	1900	164	.00	.00	.00	0.
3	1600	65	.05	.00	.05	14241.	*	7	2000	165	.00	.00	.00	0.
3	1700	66	.05	.00	.05	13238.	*	7	2100	166	.00	.00	.00	0.
3	1800	67	.05	.00	.05	12443.	*	7	2200	167	.00	.00	.00	0.
3	1900	68	.05	.00	.05	11788.	*	7	2300	168	.00	.00	.00	0.
3	2000	69	.05	.00	.05	11244.	*	8	0000	169	.00	.00	.00	0.
3	2100	70	.05	.00	.05	10784.	*	8	0100	170	.00	.00	.00	0.
3	2200	71	.05	.00	.05	10399.	*	8	0200	171	.00	.00	.00	0.
3	2300	72	.05	.00	.05	10081.	*	8	0300	172	.00	.00	.00	0.
4	0000	73	.05	.00	.05	9803.	*	8	0400	173	.00	.00	.00	0.
4	0100	74	.00	.00	.00	9499.	*	8	0500	174	.00	.00	.00	0.
4	0200	75	.00	.00	.00	9118.	*	8	0600	175	.00	.00	.00	0.
4	0300	76	.00	.00	.00	8612.	*	8	0700	176	.00	.00	.00	0.
4	0400	77	.00	.00	.00	7921.	*	8	0800	177	.00	.00	.00	0.
4	0500	78	.00	.00	.00	7056.	*	8	0900	178	.00	.00	.00	0.
4	0600	79	.00	.00	.00	6105.	*	8	1000	179	.00	.00	.00	0.
4	0700	80	.00	.00	.00	5141.	*	8	1100	180	.00	.00	.00	0.
4	0800	81	.00	.00	.00	4220.	*	8	1200	181	.00	.00	.00	0.
4	0900	82	.00	.00	.00	3396.	*	8	1300	182	.00	.00	.00	0.
4	1000	83	.00	.00	.00	2682.	*	8	1400	183	.00	.00	.00	0.
4	1100	84	.00	.00	.00	2108.	*	8	1500	184	.00	.00	.00	0.
4	1200	85	.00	.00	.00	1671.	*	8	1600	185	.00	.00	.00	0.
4	1300	86	.00	.00	.00	1325.	*	8	1700	186	.00	.00	.00	0.
4	1400	87	.00	.00	.00	1052.	*	8	1800	187	.00	.00	.00	0.
4	1500	88	.00	.00	.00	831.	*	8	1900	188	.00	.00	.00	0.
4	1600	89	.00	.00	.00	655.	*	8	2000	189	.00	.00	.00	0.
4	1700	90	.00	.00	.00	519.	*	8	2100	190	.00	.00	.00	0.
4	1800	91	.00	.00	.00	410.	*	8	2200	191	.00	.00	.00	0.
4	1900	92	.00	.00	.00	323.	*	8	2300	192	.00	.00	.00	0.
4	2000	93	.00	.00	.00	255.	*	9	0000	193	.00	.00	.00	0.
4	2100	94	.00	.00	.00	201.	*	9	0100	194	.00	.00	.00	0.
4	2200	95	.00	.00	.00	158.	*	9	0200	195	.00	.00	.00	0.
4	2300	96	.00	.00	.00	124.	*	9	0300	196	.00	.00	.00	0.
5	0000	97	.00	.00	.00	96.	*	9	0400	197	.00	.00	.00	0.
5	0100	98	.00	.00	.00	74.	*	9	0500	198	.00	.00	.00	0.
5	0200	99	.00	.00	.00	57.	*	9	0600	199	.00	.00	.00	0.
5	0300	100	.00	.00	.00	43.	*	9	0700	200	.00	.00	.00	0.

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TOTAL RAINFALL = 12.60, TOTAL LOSS = .48, TOTAL EXCESS = 12.12

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	199.00-HR	
+						
+	84857.	40.00	80187.	56040.	29075.	10634.
		(CFS)				
		(INCHES)	2.761	7.719	12.014	12.145
		(AC-FT)	39762.	111154.	173006.	174886.

CUMULATIVE AREA = 270.00 SQ MI

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

MAXIMUM STAGE +	TIME OF OPERATION MAX STAGE	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA
					6-HOUR	24-HOUR	72-HOUR	
+	HYDROGRAPH AT	010	84857.	40.00	80187.	56040.	29075.	270.00

\*\*\* NORMAL END OF HEC-1 \*\*\*